

BK. 52 Dr. 14

OFFICE OF COUNTY ENGINEER
RAMSEY CO. MINN.

Plan

Survey

Also staking Notes

Gardenette Park Addn.,

White Bear Ave. to East Ave,

From Co. Rd. "F"

To So. Shore Blvd.

Storm Sewer Survey, 1950

Road Acc't. No.

Date Filed. 7-25-47

File

Bench Levels

Gardendale Park Add.

Rec. 5/7/47

Sto	+	π	-	Elev.	
B.M.	4.26	934.86			930.60
T.P.	7.17	938.14	5.89	928.97	
T.P.	7.31	937.12	6.33	929.81	
T.P.	3.48	940.52	0.88	937.04	
T.P.	4.47	936.03	8.96	931.56	
T.P.	5.11	934.53	6.61	929.42	
Lake Elev.			9.31	925.22	
T.P.	4.63	932.89	6.27	928.26	
T.P.	4.59	932.92	4.56	928.33	
T.B.M.	7.48	934.79	5.61	927.31	
T.B.M.	9.45	943.95	0.29	934.50	
T.P.	5.27	947.62	1.60	942.35	
T.P.	5.91	947.68	5.85	941.77	
B.M.	5.35	946.42	6.61	941.07	
T.P.	6.47	949.18	3.71	942.71	
B.M.	6.28	950.49	4.97	944.21	
T.P.	6.58	952.50	4.57	945.92	
B.M.			1.55	950.95	
T.P.	6.65	957.83	1.32	951.18	
T.P.	3.92	961.49	0.26	957.57	
T.P.	0.52	956.14	5.87	955.62	
B.M.			6.20	949.94	
T.P.	1.63	949.61	8.16	947.98	
T.P.	0.21	936.54	13.28	936.33	
B.M.			9.26	927.28	927.31

L.A. 4-21-47
A.M.
M.B.

Description

U.S.G.S. B.M. N 8 N.W. Cor. Co. Rd. "G" & Ditch 13

U.S.B.M. in P.P. So. Shore Blvd & White Bear Ave.
Spk. in P.P. W. of Turn at Cemetery.

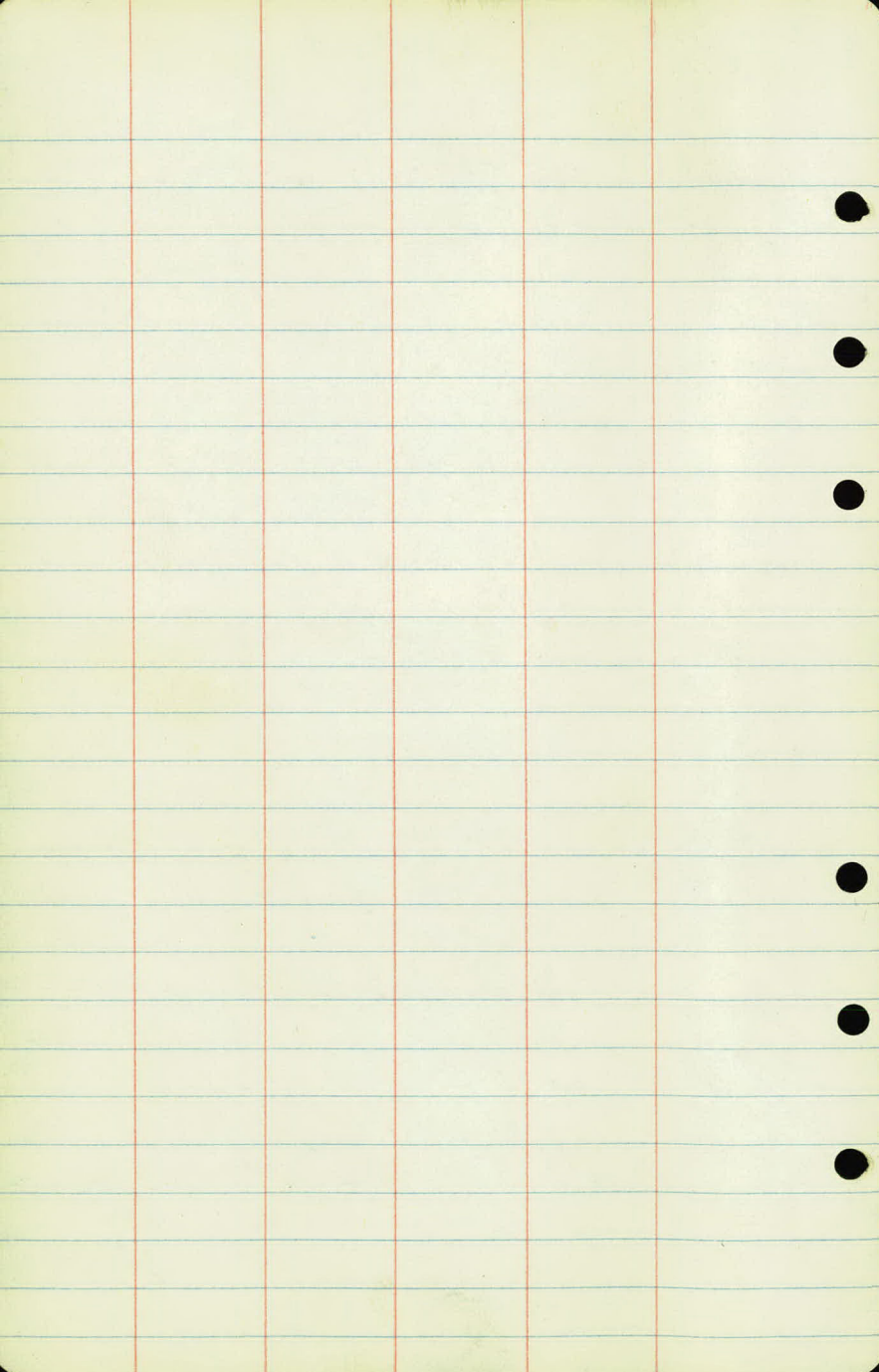
Top Sec. Cor. Iron Co. Rd. "F" & White Bear Ave.

P.R. Spk. in 30" Elm S.W. Cor. Co. Rd. "F" & Bellevue Ave.

P.R. Spk. in 30" Oak 100' S. of East Ave. & Co. Rd. "F"

P.R. Spk. in 8" Elm N. of East Ave. & So. Shore Drive.

U.S.G.S. B.M.



1
X Sections

Gardenette Drive N.

Belt view to Gardenette Dr. S.

4 Pages

Sta	+	π	-	Elev	✓
T.B.M.	8.24	94763			(939.39)

0 +00				38.8	
-------	--	--	--	------	--

+30				39.6	
-----	--	--	--	------	--

+71				41.1	
-----	--	--	--	------	--

1				41.6	
---	--	--	--	------	--

+50				42.1	
-----	--	--	--	------	--

2				42.6	
---	--	--	--	------	--

+50				42.4	
-----	--	--	--	------	--

3				42.2	
---	--	--	--	------	--

5-2-97

2

L

E

E

Top Iron at 150' Rod Pt.

7.1
507.6
308.88.0
2.77.3
50

L

6.3
506.8
308.06.9
156.5
336.5
50

L

5.5
505.9
306.56.0
135.7
305.6
50

L

5.2
505.8
246.05.5
265.1
50

L

4.3
505.2
275.54.8
274.0
50

L

3.7
504.5
26

5.0

4.5
263.9
50

L

4.3
504.9
295.25.2
275.0
50

L

4.6
505.0
285.45.2
275.2
50

L

Sta	+	T.	-	Elev
-----	---	----	---	------

947.63

3+50

42.5

4

43.1

+50

43.3

5

45.0

+19

46.4

T.P

13.38

95925

1.76

945.87

+60

48.5

6

51.0

+45

53.7

7/5/3²

3

L

E

R

$$\begin{array}{r} 4.8 \\ 50 \end{array}$$

$$\begin{array}{r} 5.0 \\ 29 \end{array}$$

$$\begin{array}{r} 5.1 \\ \hline \end{array}$$

$$\begin{array}{r} 4.6 \\ 28 \end{array}$$

$$\begin{array}{r} 4.4 \\ 50 \end{array}$$

$$\begin{array}{r} 4.6 \\ 50 \end{array}$$

$$\begin{array}{r} 4.7 \\ 27 \end{array}$$

$$\begin{array}{r} 4.5 \\ \hline \end{array}$$

$$\begin{array}{r} 3.8 \\ 28 \end{array}$$

$$\begin{array}{r} 3.1 \\ 50 \end{array}$$

$$\begin{array}{r} 4.5 \\ 50 \end{array}$$

$$\begin{array}{r} 4.6 \\ 30 \end{array}$$

$$\begin{array}{r} 4.3 \\ \hline \end{array}$$

$$\begin{array}{r} 3.7 \\ 26 \end{array}$$

$$\begin{array}{r} 2.8 \\ 50 \end{array}$$

$$\begin{array}{r} 3.5 \\ 50 \end{array}$$

$$\begin{array}{r} 3.2 \\ 28 \end{array}$$

$$\begin{array}{r} 2.6 \\ \hline \end{array}$$

$$\begin{array}{r} 1.6 \\ 30 \end{array}$$

$$\begin{array}{r} 0.8 \\ 50 \end{array}$$

$$\begin{array}{r} 2.2 \\ 50 \end{array}$$

$$\begin{array}{r} 1.9 \\ 30 \end{array}$$

$$\begin{array}{r} 1.2 \\ \hline \end{array}$$

$$\begin{array}{r} 0.0 \\ 28 \end{array}$$

$$\begin{array}{r} +1.0 \\ 50 \end{array}$$

$$\begin{array}{r} 12.0 \\ 50 \end{array}$$

$$\begin{array}{r} 11.9 \\ 30 \end{array}$$

$$\begin{array}{r} 10.8 \\ \hline \end{array}$$

$$\begin{array}{r} 9.6 \\ 30 \end{array}$$

$$\begin{array}{r} 9.4 \\ 50 \end{array}$$

$$\begin{array}{r} 9.6 \\ 50 \end{array}$$

$$\begin{array}{r} 9.4 \\ 32 \end{array}$$

$$\begin{array}{r} 8.3 \\ \hline \end{array}$$

$$\begin{array}{r} 7.6 \\ 25 \end{array}$$

$$\begin{array}{r} 7.6 \\ 50 \end{array}$$

$$\begin{array}{r} 7.2 \\ 50 \end{array}$$

$$\begin{array}{r} 6.4 \\ 26 \end{array}$$

$$\begin{array}{r} 5.6 \\ \hline \end{array}$$

$$\begin{array}{r} 5.2 \\ 27 \end{array}$$

$$\begin{array}{r} 5.6 \\ 50 \end{array}$$

STA	+	π	-	ELEV
-----	---	-------	---	------

		959.25		
--	--	--------	--	--

7 + 00				55.1
--------	--	--	--	------

7 + 32				55.4
--------	--	--	--	------

7 + 51.32				55.5
-----------	--	--	--	------

T.P	3.52	959.47	3.30	955.95
-----	------	--------	------	--------

B.M			9.57	949.90
-----	--	--	------	--------

				949.94
--	--	--	--	--------

5-2-41

4

LT

RT

5.9
505.0
76

4.2

3.8
304.4
50

L

5.5
504.8
30

3.9

3.8
304.3
50

L

3.8

2" x 2" Hub at Int. of Gard. Dr. N. & S.

P.R. Spt. in 8" Oak N.W. Cor. of East Av. & 50. Shore Blvd.

Sta. + π - E/er.

1

Alignment
East Ave

INDEX

Align 1-2

Topog 3-6

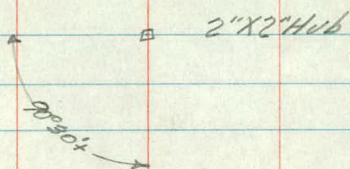
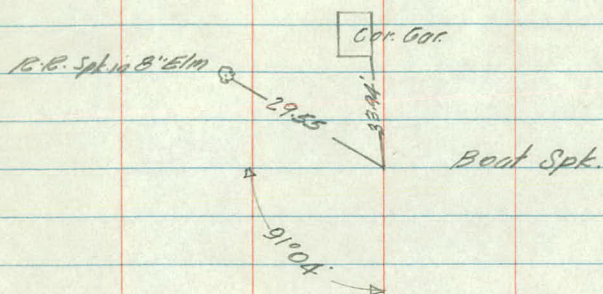
Xsections 7-

17 + 39.31 = $\frac{1}{2}$ So Shore Blvd.

13 + 23.94 P.O.T. = $\frac{1}{2}$ Lilac Lane

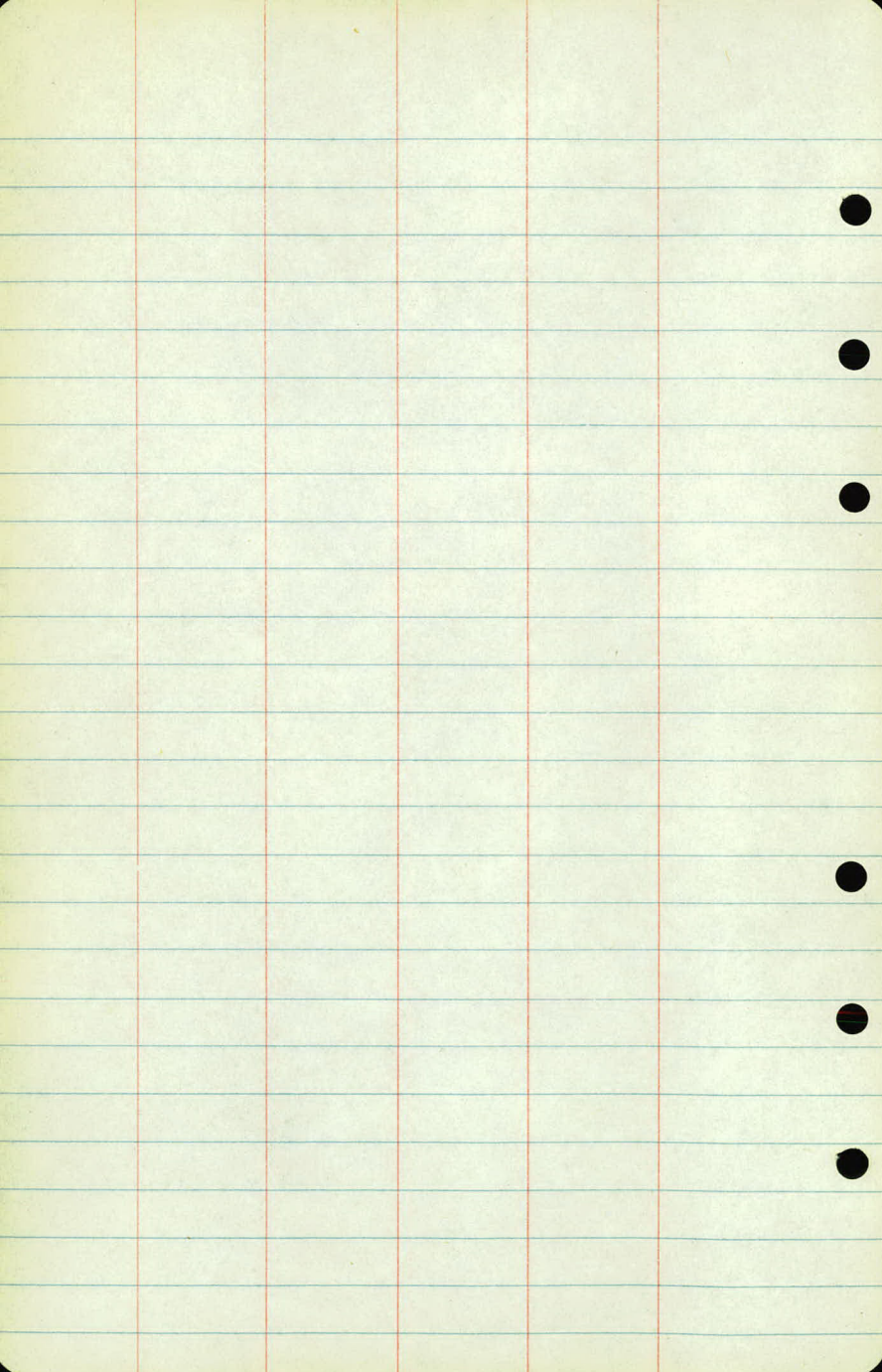
3 + 83.0 P.O.T. = $\frac{1}{2}$ Floral Drive

0 + 00 = $\frac{1}{2}$ Co. Rd. "F"



2\"X2\" Hub

Mont



Topography

5

FC-00

4

3

FC-00

2

+68-Brush-0-8'

1

+45-Brush-2'

+55-End FC-0'

+45-Brush-9'

+23-FC-00

+20-12" CM-6-26'

0

+09-Edge Bl. Top
-09-7

K.D.
A.M.
M.B.

4-29-41

4

Cult.

Cult.



← Plum Brush



Black Top

12

11

10



+14-Fc-0.0
Fc-50'

+38-Fc-Cor-0

9

+17-End of Fc 0.0

8

7

Fc-00

+73-2"BE-1'

~~+72-2"BE~~

6

Pasture

Cult.

▲

▲

Old St. B. R. R. R.O.W

3 strand barbed

72
Brush
105

Cult.

Cult.

+13-PP-29' +34-7 } Edge Bl Top
+01-Fg Cor - 1' +305 }

17

16

15

14

13

Fg-0.5

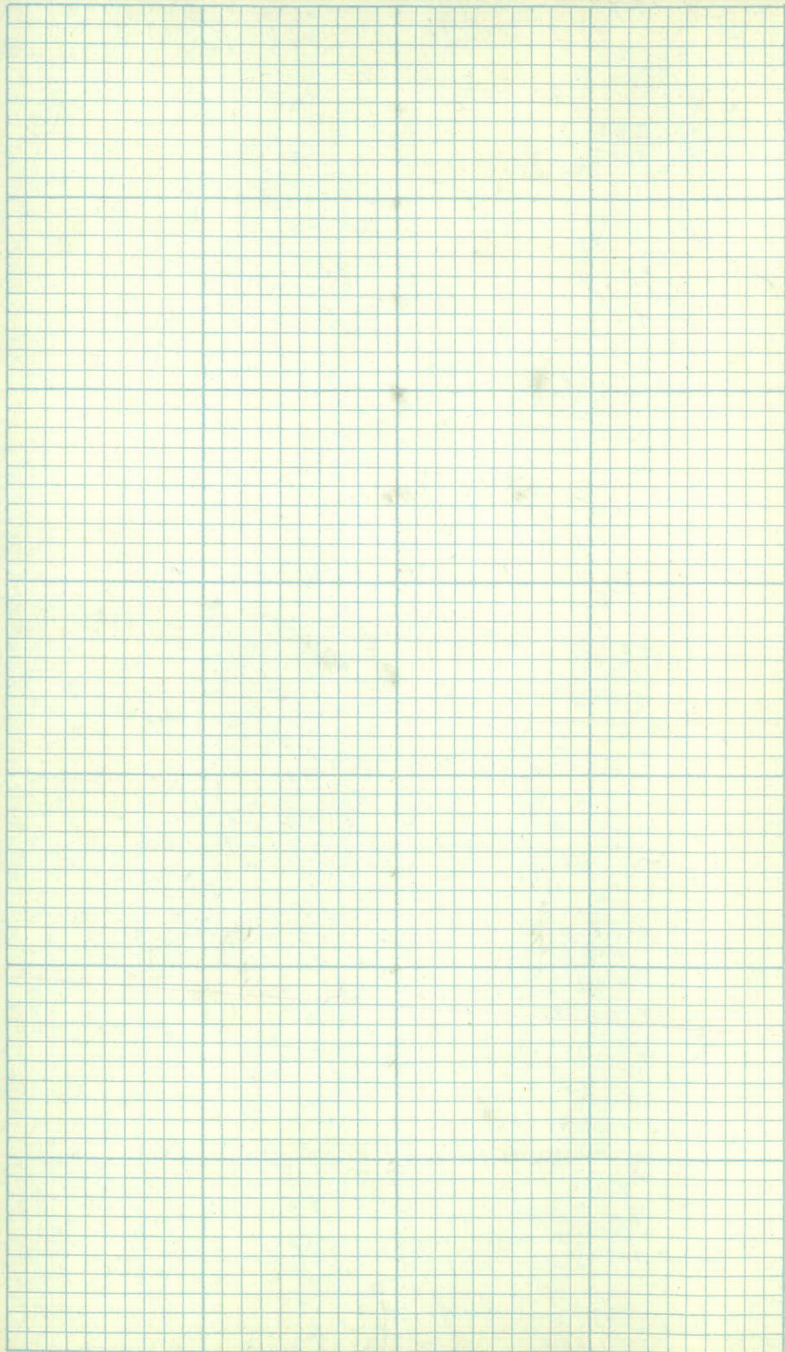
A-2747

6

Se. Shore Blvd.

Pasture

Cult.



X sections
East Ave.

Rec'd. 5/1/47 W.B.

Sta	+	T	-	Elev
B.M.	3.36	954.31 953.31		950.95 <u>(949.95)</u>

0 +00		Co. RD - F		50.9
-------	--	------------	--	------

+15				50.3
-----	--	--	--	------

+21				49.0
-----	--	--	--	------

+24				49.6
-----	--	--	--	------

+58				49.4
-----	--	--	--	------

1				48.4
---	--	--	--	------

+50				49.0
-----	--	--	--	------

2				51.2
---	--	--	--	------

K.A.
A.M.
M.B.

4-29-47

8

L E R

R.R. Spt. in 30" Oak 100.5 of East Ave & Co. Rd. "F"

6.2 5.7 4.9 4.2 3.4 2.9 2.4 ✓
200 150 100 50 — 50 100

4.7 4.0 3.7 3.3 ✓
50 — 26 50

6.1 5.7 5.3 3.8 3.6 4.5 ✓
50 21 — 10 25 50

5.6 5.2 4.7 3.8 3.7 4.5 3.9 ✓
50 25 — 10 23 28 50

6.2 5.8 4.9 4.7 5.4 4.9 4.9 ✓
50 28 — 11 16 27 50

7.4 6.8 5.9 5.3 5.8 5.7 5.7 ✓
50 23 — 9 13 30 50

5.4 5.5 5.3 4.9 5.5 5.9 5.9 ✓
50 27 — 7 10 32 50

4.0 3.8 3.7 3.1 3.3 3.9 4.4 4.9 ✓
50 33 10 — 6 8 28 50

Sta	+	$\bar{T}$	-	Elev
		954.31		
		953.31		

2+50				51.7
------	--	--	--	------

3				51.4
---	--	--	--	------

+50				50.3
-----	--	--	--	------

+83	Φ	FLORAL DR.		49.5
-----	---	------------	--	------

4+13				49.6
------	--	--	--	------

+60				49.4
-----	--	--	--	------

5				51.5
---	--	--	--	------

+50				55.8
-----	--	--	--	------

T.P.		962.94		953.75
9.19		961.94	0.56	952.75

L E R

4.8 4.0 3.5 2.6 2.8 3.3 3.6 ✓
50 30 7 10 30 50

6.5 5.3 4.6 3.6 2.9 3.1 3.4 3.3 ✓
50 32 17 3 7 26 50

7.1 6.9 5.8 5.1 4.0 4.1 4.0 3.6 L
50 32 14 3 10 34 50

7.2 7.0 6.4 5.8 4.8 4.7 4.5 4.0 ✓
50 33 10 3 10 28 50

7.2 6.9 6.4 5.8 4.7 4.5 4.3 L
50 33 10 2 25 50

6.5 6.3 5.6 4.9 4.1 4.0 4.0 L
50 33 1 5 23 50

4.8 4.0 4.0 3.6 2.8 3.1 3.0 2.6 L
50 24 10 2 13 32 50

2.0 1.3 0.5 0.0 0.0 + 1.5 +0.5 +0.8 +0.7 +1.5
50 31 25 10 3 8 14 25 50 L

Sta	+	Σ	-	Elev
		962.94		
		961.94		

6+00				57.2
------	--	--	--	------

+40				59.3
-----	--	--	--	------

+72				60.5
-----	--	--	--	------

7				60.7
---	--	--	--	------

+25				58.7
-----	--	--	--	------

+60				54.6
-----	--	--	--	------

8				52.6
---	--	--	--	------

+50				52.0
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4-29-47

10

L

E

R

8.8	7.8	7.1	6.6	5.7	6.0	5.6	4.8	L
50	25	8	2	—	7	19	50	

5.9	5.3	4.8	4.6	3.6	4.1	4.2	4.0	L
50	30	6	2	—	8	29	50	

4.8	3.7	2.9	2.4	2.6	3.1	3.2	L
50	26	2	—	6	23	50	

6.0	4.0	2.7	2.2	2.8	3.2	3.0	L
50	25	3	—	6	27	50	

8.2	7.8	6.3	5.4	4.2	5.2	5.0	4.3	L
50	40	27	10	—	6	28	50	

10.4	9.6	9.1	8.3	8.4	8.4	7.2	L
50	26	8		8	31	50	

11.3	11.2	11.1	10.3	10.9	10.3	L
50	33	10		28	50	

11.1	11.1	11.2	10.9	11.7	12.2	12.3	L
50	31	10	—	7	29	50	

Sta.	+		-	Elev
		962.94		
		961.94		
9+00		962.66		53.10
T.P.	9.10	961.66	9.38	953.56 952.56

	+50			54.0
--	-----	--	--	------

	10			54.9
--	----	--	--	------

	+26			55.1
--	-----	--	--	------

	+38			52.4
--	-----	--	--	------

	+51			52.0
--	-----	--	--	------

No Xsec.
+38 Profile of N.R.B. ditch

	+71			56.7
--	-----	--	--	------

K.A. 5-30-47
A.M.
M.B.

11

L E R

9.9 10.1 10.3 9.9 11.0 12.4 12.8 ✓
50 31 10 — 6 29 50

Top rock 2 ft. 5 ft. 6 ft. 95

9.1 9.3 8.7 8.7 10.7 9.7 12.2 12.6 ✓
50 25 3 6 17 35 50

8.7 8.7 7.8 7.8 8.2 9.7 10.0 ✓
50 27 8 — 12 32 50

8.4 8.3 7.6 8.1 11.3 ✓
50 16 — 30 50

8.2 8.3 8.5 10.0 10.2 10.7 10.8 ✓
50 33 8 5 25 50

8.1 8.0 8.4 10.7 10.9 8.0 ✓
50 20 7 — 25 50

11.4 11.8 12.5 12.3 12.1
50 100 150 200 250
12.4
300

7.9 7.7 7.5 6.0 5.6 5.0 5.3 ✓
50 28 5 7 30 50

Sta	+	962.66 961.66	-	Elev.
11+00				57.7
+50				59.1
12				58.9
+50				57.9
+93.94				56.9
13+23.94				55.7
+53.94				54.1
14				51.9

L E R

7.4	6.9	6.3	5.5	5.0	4.3	4.8	5.3	5.4	✓
50	28	12	10	—	2	15	24	50	

6.3	5.7	4.0	3.6	3.2	3.4	3.9	3.7	✓
58	23	9	—	1	16	25	50	

5.7	4.7	3.8	4.0	4.8	4.8	✓
50	25	—	10	25	50	

5.4	5.4	4.8	4.8	5.6	6.6	7.5	✓
50	17	2	—	8	25	50	

6.2	6.2	6.3	5.8	6.7	8.4	8.8	✓
50	34	14	—	6	33	50	

7.8	7.7	7.0	7.7	8.7	9.9	✓
50	33	—	6	28	50	

9.0	9.3	9.2	8.6	9.1	9.9	11.3	✓
50	33	16	—	6	27	50	

9.7	10.5	10.8	11.3	11.8	12.6	✓
50	33	—	7	36	50	

Sta	+	Δ	-	Elev.
		962.66		
		961.66		
14+27		963.27		52.1
T.P.	4.78	962.27	4.17	958.49

+70

55.8

15

58.4

+35

60.4

+70

61.7

16

61.0

+50

56.3

17

53.2

L

E

R

9.7	10.3	10.4	10.6	10.8	12.7	12.6	✓
50	33	15		7	17	50	

7.7	7.6	7.5	8.6	10.3	11.1	✓
50	28	—	9	30	50	

5.6	5.4	5.4	4.9	6.2	8.1	9.2
50	33	10	—	9	32	50

3.5	3.2	3.2	2.9	4.4	6.3	7.1	✓
50	30	10	—	7	35	50	

2.4	2.2	2.1	1.6	3.7	5.3	6.5	✓
50	33	7	—	9	32	50	

2.7	2.8	2.0	2.3	4.3	6.3	7.3	✓
50	33	15	—	9	34	50	

5.9	6.5	7.4	7.0	8.6	10.2	10.8	✓
50	33	10	—	8	34	50	

7.6	8.3		10.1	11.3	12.1	12.6	✓
50	33		—	10	34		

Sta.	+	T	-	Elev.
		963.27		
		962.27		

17+14				51.7
-------	--	--	--	------

+20				48.9
-----	--	--	--	------

+39.31	25-shore Blvd.			49.6
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B.M		13.35	949.92	949.94
			948.92	(948.92)

4-30-47

14

L E F

9.2	7.6	11.6		12.6	12.8
50	30			25	50

13.7	14.2	14.4	15.2	15.4
50	38	—	22	50

12.8	12.5	12.7	13.3	13.7	14.5	15.3	16.7
200	150	100	50		50	100	150

R.R. Spk in @ Elm N of East Ave & So. Shore Blvd.

Sta	+ π	-	Elev.
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1

Alignment

Bellevue Ave

INDEX

Align 1-3

Topog 4-6

XSec. 7-

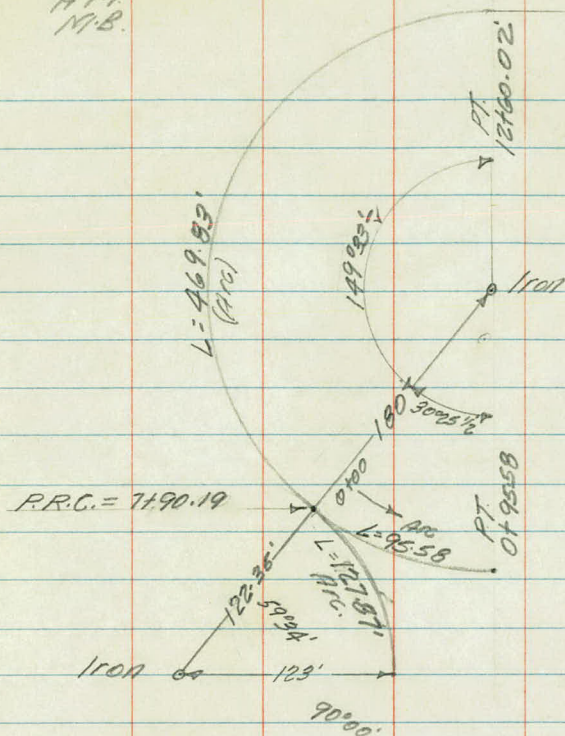
Sta	Point	Lt	Rt
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6 + 62.32	P.O.T.		
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3 + 88.0	P.O.T. = E Floral Drive	13 + 21.52	
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0 + 00	= E Co. Rd. "F"		
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2



2"x2" Hub

Sta Point L Lt L Pt

= E. So. Shore Blvd.

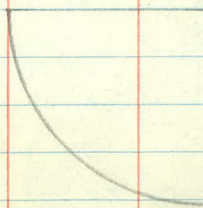
2. + 14.65

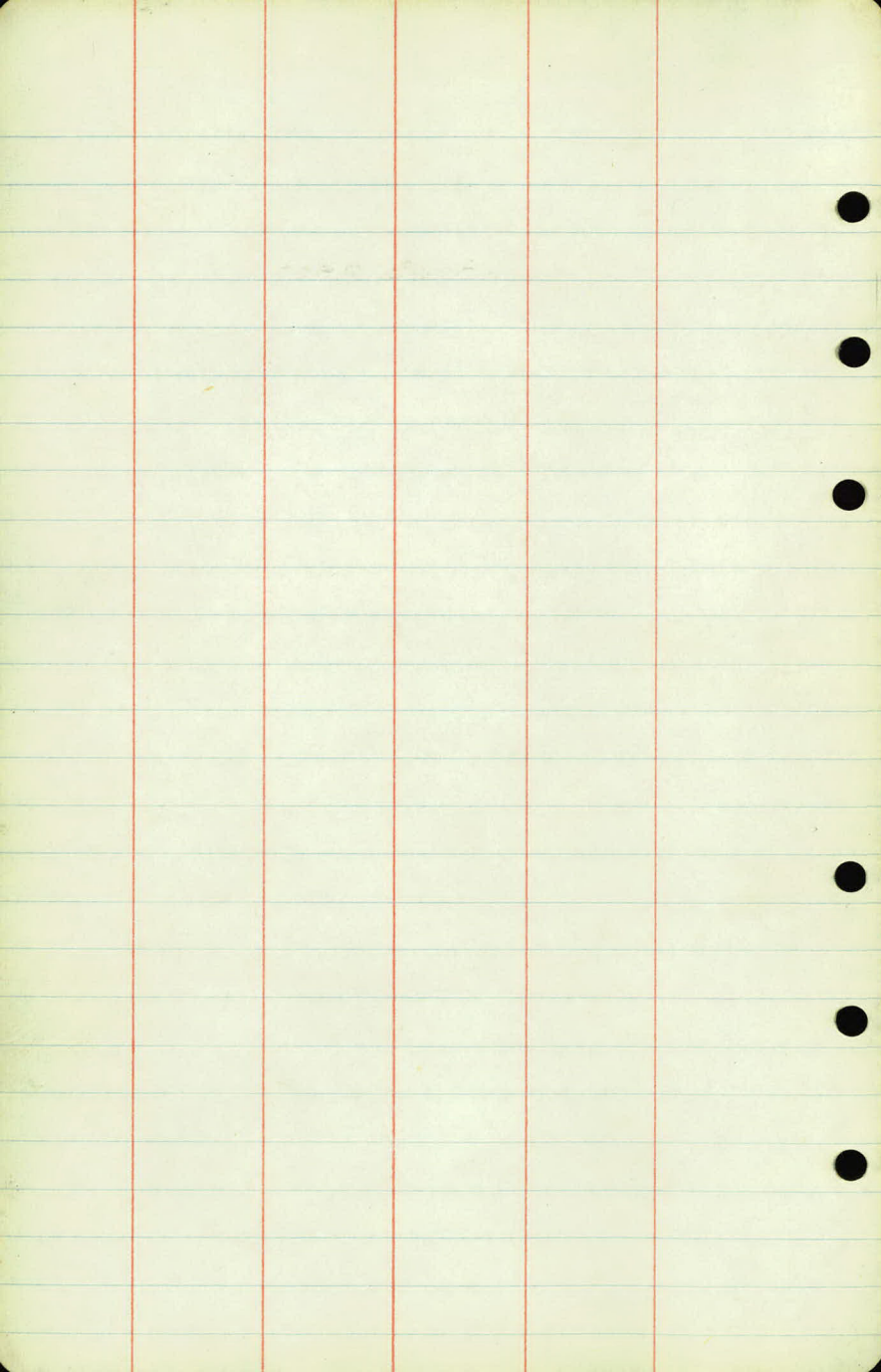
15.00 per knot

16 + 1200 POT = E. Wilcox Lane

13 + 9499 Pl. 90° ± = 0400 Gortner St. Dr. N.

12 + 6002 P.T.





Topography
Belleview

+22-T.P-34'

+28-FC XSE

+09 Edge Bl Top
-08

Cult

Cult

x

x

x

0

x

x

x

x

x

Go. Rd. #11

(Not E. Shore Bl.) +99-Edge Bl. Top +57-End 12" Vit-24'
 +35-P.O.T-Not E. Ave. +12-End 12" Vit-24'
 +04-10" Oak-18' +26-Bl. Top +12-Pk-36'
 +03-16" Pine-33' +04-Fc. Cor-36'
 20

+85-12" Apple Tr-27'
 +67-Pum. Brush-23'
 +42-18" P.E.-27'
 +26-S.E. Cor. Ho-36'
 +20-18" B.E.-37'
 19

+60-10" B.E.-25'
 +52-8" B.E.-10' +39-Edge Bl.
 +29-Brush-18-50' +35-Fc. Cor-39'
 18

+96-6" B.E.-33'
 +70-10" S.E.-25'
 +67-10" Fc.-35' +60-Fc. X 5 E
 17

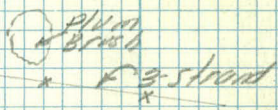
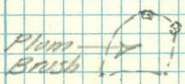
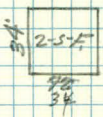
+16-Fc. X 5 E
 +150-6" Lilac Long
 16

15

5-2-47

2 Bottom ditch 6

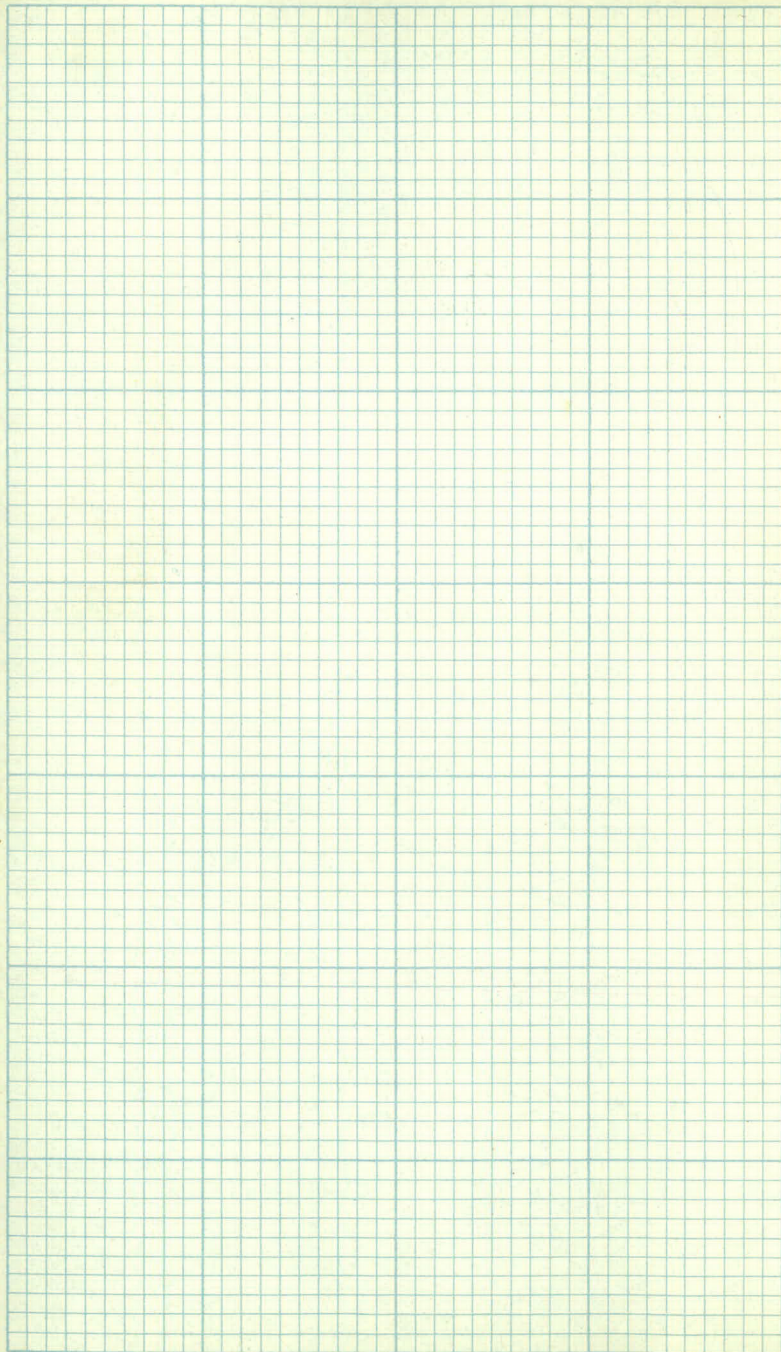
So. Shore Blvd.



Pasture

4-Strand 7

cut.



Xsections
Bellview

Sta	+	π	-	Elev
B.M.	6.32	950.53		(944.21)

0 100 = 2 Co. Rd. F" 44.6.

+15 44.3.

+17 42.7.

+20 42.7.

+22 43.7.

+36 44.1.

1 45.1.

2 45.3.

K.M.
H.M.
N.B.

4-30-41

8

L E R

R.R. Spk. in 30" El. 10 SW Cor. Ballaview & "F"

6.2	6.1	6.1	6.0	5.9	5.8	5.7	5.6	5.5
200	150	100	50		50	100	150	200

6.4		6.2		6.1
50		<u>50</u>		50

7.9		7.9		7.8		7.7		7.8
50		25				25		50

7.9		7.9		7.8		7.7		7.8
50		25		<u>50</u>		25		50

7.0		7.1		6.8		6.8		6.8
50		28		<u>50</u>		23		50

6.4		6.6		6.4		6.5		6.5
50		30		<u>50</u>		30		50

5.4		5.4		5.4		5.4		5.4
50		30		<u>50</u>		30		50

5.2		5.1		5.2		5.2		5.1
50		30		<u>50</u>		30		50

Sta	+	π .	-	Elev.
		950.53		

3+00				45.8
------	--	--	--	------

+53				45.9
-----	--	--	--	------

				45.6
--	--	--	--	------

+83				
-----	--	--	--	--

4+13				45.4
------	--	--	--	------

5				45.8
---	--	--	--	------

+50				46.3
-----	--	--	--	------

6				46.4
---	--	--	--	------

+52				46.7
-----	--	--	--	------

T.P.	1.26	947.91	3.88	946.65
------	------	--------	------	--------

L E E

5.3 5.1 4.7 4.7 4.7 ✓
50 30 30 30 50

4.8 4.8 4.6 4.7 4.7 ✓
50 30 30 30 50

5.4 5.0 4.9 4.8 4.8 ✓
50 30 30 30 50

5.5 5.3 5.1 5.0 5.0 ✓
50 30 30 30 50

5.2 5.0 4.7 4.6 4.3 ✓
50 30 30 30 50

5.2 4.8 4.2 4.1 4.4 ✓
50 30 30 30 50

4.8 4.4 4.1 5.3 6.2 ✓
50 30 30 30 50

4.2 3.7 3.6 3.8 5.3 6.4 ✓
50 30 17 22 50

Sta	+	~ π 1	-	Elev.
-----	---	-----------	---	-------

947.91

6+62.3				46.2
--------	--	--	--	------

7				43.3
---	--	--	--	------

+50				41.9
-----	--	--	--	------

+90.19				41.6
--------	--	--	--	------

8				41.9
---	--	--	--	------

+50				41.9
-----	--	--	--	------

9				40.7
---	--	--	--	------

+50				38.0
-----	--	--	--	------

L E E

1.3 1.1 1.7 3.2 3.6 ✓
50 26 — 30 50

2.5 2.8 3.5 4.6 5.7 6.1 ✓
50 34 19 25 50

3.4 4.8 6.5 7.1 7.3 7.3 ✓
50 27 — 18 35 50

3.9 4.8 6.3 7.2 7.9 ✓
50 23 26 50

3.9 4.3 5.8 6.0 7.4 8.0 ✓
50 30 7 — 30 50

4.5 4.7 5.6 6.0 6.6 7.8 8.4 ✓
50 36 18 — 9 30 50

5.3 6.3 6.5 7.2 8.3 8.9 9.3 ✓
50 30 14 — 19 34 50

7.5 8.3 9.6 9.9 10.4 10.6 ✓
50 35 11 30 50

Sta	+	π ,	-	Elev.
		947.91		
10+00				37.0
+50				36.3
11				35.6
+50				35.0
12				35.7
+60.02				36.5
F.B.M	6.10	945.49	8.52	939.39
13				37.0
+64.93				
		W-PROP-LINE		38.0

L

E

E

7.7 9.6
50 29

10.9 11.5 11.8 ✓
— 32 50

1.1 7.8 9.1 10.7 11.6 12.1 12.3 12.1 ✓
100 50 39 20 — 10 29 50

9.4 10.7 11.7 12.3 12.9 12.8 12.5 ✓
50 30 13 — 17 38 50

12.0 12.1 12.7 12.9 13.0 12.7 12.5 ✓
50 40 18 — 11 30 50

11.2 11.9 12.2 12.2 12.1 ✓
50 30 — 30 50

10.6 11.2 11.4 11.5 11.3 ✓
50 30 — 30 50

Top Iron at 150' Rad. Pt.

8.5 8.7 8.5 8.4 8.3 ✓
50 30 30 50

6.4 6.6 7.5 6.6 6.2 ✓
50 30 30 50

Sta	+	π	-	Elev
		945.49		

14+34.93		No Prop LINE		40.2
----------	--	--------------	--	------

+60				40.7
-----	--	--	--	------

T.P.	0.64	943.28	2.85	942.64
------	------	--------	------	--------

15				41.0
----	--	--	--	------

+40				41.5
-----	--	--	--	------

+82		So. Prop LINE		41.1
-----	--	---------------	--	------

16 +15		£ LILAC		41.5
--------	--	---------	--	------

+48		No. Prop. Line		37.2
-----	--	----------------	--	------

(16) 17				33.7
---------	--	--	--	------

4-30-47

12

L

E

R

7.4

6.4

5.3

4.4

3.8 ✓

50

30

30

50

7.0

6.0

4.8

3.8

3.3 ✓

50

30

30

50

TOP LARGE ROCK LILAC + BELLVIEW

4.5

3.5

2.3

1.2

0.9 ✓

50

30

29

50

4.5

3.4

1.8

1.0

0.7 ✓

50

28

25

50

5.0

3.8

2.2

1.5

1.3 ✓

50

30

30

50

38.8

40.1

42.0

42.1

4.5

3.2

1.8

1.3

1.2 ✓

50

30

30

50

35.3

35.9

37.7

38.4

8.0

7.4

6.1

5.6

4.9 ✓

50

30

30

50

32.6

32.4

35.3

36.8

10.7

10.9

9.6

8.0

6.5 ✓

50

30

28

50

Sta	+	π	-	Elev
17 (16)+38		943.28		33.0

+56				34.4
-----	--	--	--	------

+61				34.8
-----	--	--	--	------

+74				34.4
-----	--	--	--	------

+86				32.3
-----	--	--	--	------

(17) 18				32.0
---------	--	--	--	------

+50				32.0
-----	--	--	--	------

(18) 19				33.0
---------	--	--	--	------

K.A.
A.M.
M.B.

5-2-47

13

L				E				R			
31.8				31.6				34.0	34.2	35.9	36.0 ✓
11.5				11.7		10.3		9.3	9.1	7.4	7.3
50				30				16	28	41	50
32.2				31.7	32.0			35.1		35.6	
11.1				11.6	11.3	8.9		8.2		7.9	✓
50				35	22			20		50	
32.4				32.0	32.5			35.0	35.0	34.1	33.7
10.9				11.3	10.8	8.5		8.3	8.3	9.2	9.6 ✓
50				32	11	-		14	23	35	50
32.5				32.8	34.5			32.3	32.8	33.5	
10.8				10.5	8.9	8.9		11.0	10.5	9.8	✓
50				34	22			14	32	50	
33.0				34.2	34.1			31.7	32.2	32.5	
10.3				9.1	9.2	11.0		11.6	11.1	10.8	✓
50				38	17	-		18	30	50	
33.6				33.0	31.9			31.7	32.4	32.4	
9.7				10.3	11.4	11.3		11.6	10.9	10.9	✓
50				32	18			20	29	50	
33.9				33.7	32.5	32.0		31.9	32.8	33.3	
9.4				9.6	10.8	11.3	11.3	11.4	10.5	10.0	✓
50				41	27	15		23	37	50	
34.0				34.0	33.5			32.4	33.2	33.7	
9.3				9.3	9.8	10.3		10.9	10.1	9.6	✓
50				30	16			20	37	50	

Sta	+	π	-	Elev.
19		943.28		
18+50				32.9
T.P.	5.90	938.35	10.83	932.45

20				31.4
19				

+07				31.0
-----	--	--	--	------

+12				30.6
-----	--	--	--	------

+17				30.5
-----	--	--	--	------

+23				32.1
-----	--	--	--	------

+35?	ϕ	So SHORE BLVD		32.5
------	--------	---------------	--	------

+				
T.P.	3.44	932.42	9.37	928.98
B.M.			5.12	927.30
				(927.31)

5-2-47 - Windy

14

	L		E		R
	34.1	33.8		31.8	31.9 32.1
H.O.	9.2	9.5	10.4	11.5	11.4 11.2 ✓
	36.5	21		18	36 50

	32.7	32.7	31.4	31.7		31.3	30.4	30.6	31.1
L.O.	5.7	5.7	7.0	6.7	7.6	7.1	8.0	7.8	7.3 ✓
	30	23	17	12	—	7	20	36	50

	32.7	30.9		30.2	30.4	31.0
L.O.	5.7	7.5	7.4	8.2	8.6	7.4 ✓
	22	17	—	27	43	50

	30.9	30.2	30.0		30.2	30.4	31.0
	7.5	8.2	8.4	7.8	8.2	8.0	7.4 ✓
	50	44	21		27	43	50

(FL 12" Vit)	30.8	30.0	F.L	30.2	29.9	30.7
8.9	7.6	8.4	8.9	8.2	8.5	7.7 ✓
24	50	24	24	16	36	50

31.1	31.6		32.8	33.3
7.3	6.8	6.3	5.6	5.1
50	26		50	50

928.6	31.6	33.6
FL	7.7	4.8
100	50	50
	59	3.2
	100	100

$\frac{9.67}{24} = 157 = \text{End 12" Vit}$

9.0 + 59 = E Ditch

9.5 - 20.100 = E ditch

9.9 20.100 = " "

Spk in P.P. S.E. Cor White Bear Av. & So Shore Blvd.

Sta	+ π	-	Elev.
-----	---------	---	-------

[illegible]

Page 1 of 1

Page 1 of 1

Page 1 of 1

Page 1 of 1

Page 1 of 1

PLAIN SURVEY

LILAC LANE

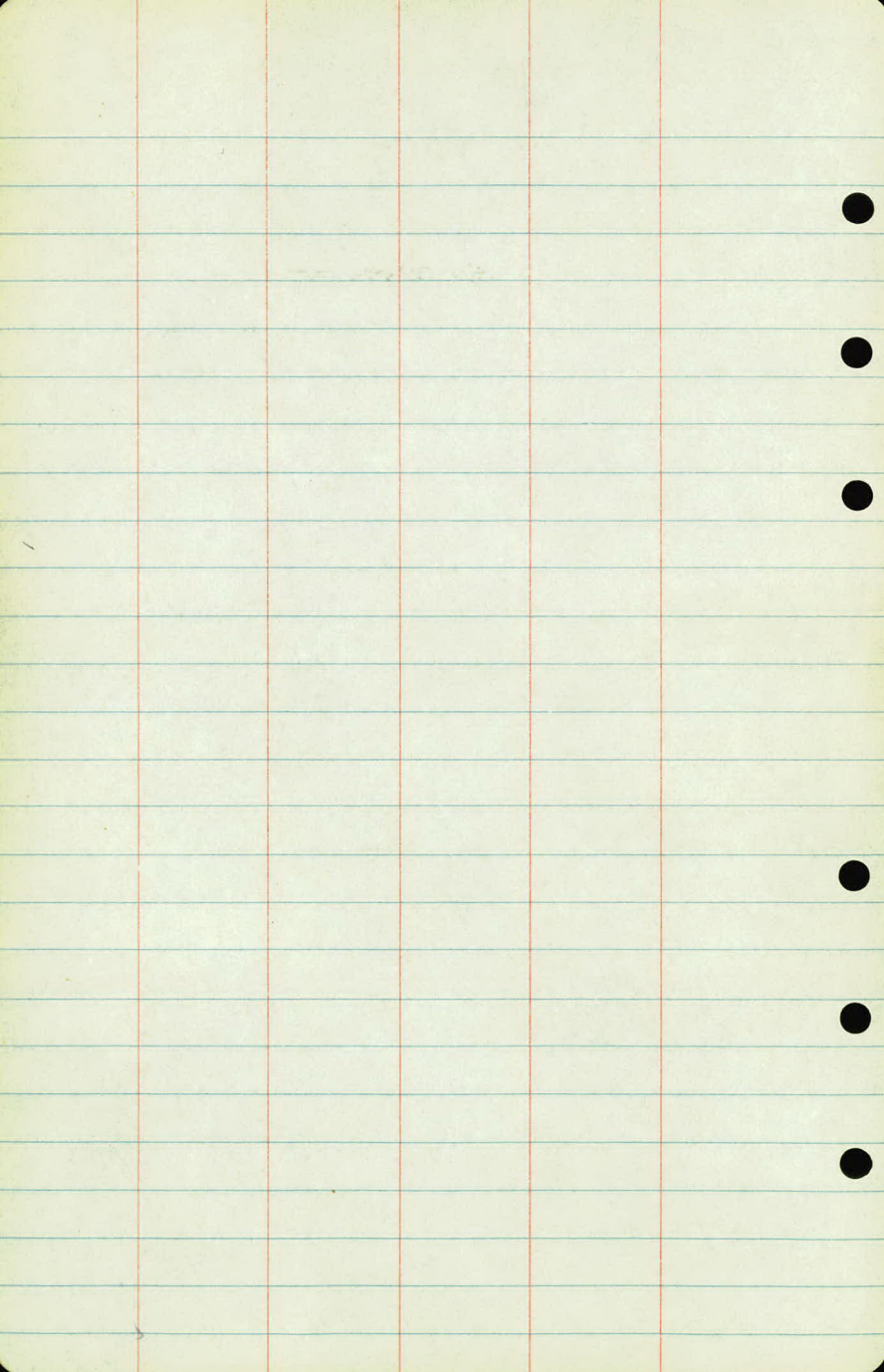
White Bear Ave to East Ave

INDEX

Align -	1-2
Topog. -	3-6
XSec -	7-14

Rec:

5/9/49



Alignment
Lilac

Sta Point

17+24.85 = E East Ave. 13+23.94

13+21.74 P.O.T. = E Cordanette Drive N. 14+34.32^{S.}

9+93.54 P.O.T. = Old R.E. Iron

8+10.98 P.O.T. = Old R.E. Iron

5+70.9 P.O.T. = E Bellevue Ave. = Sta 16+14.65

0+00 = E White Bear Ave.

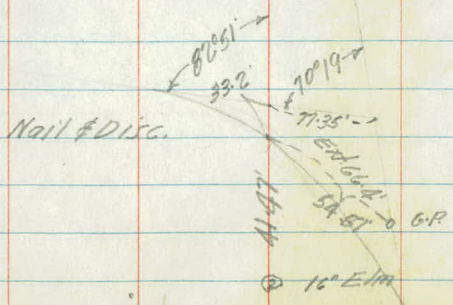
K.A 5-8-47
A.M.
M.B.

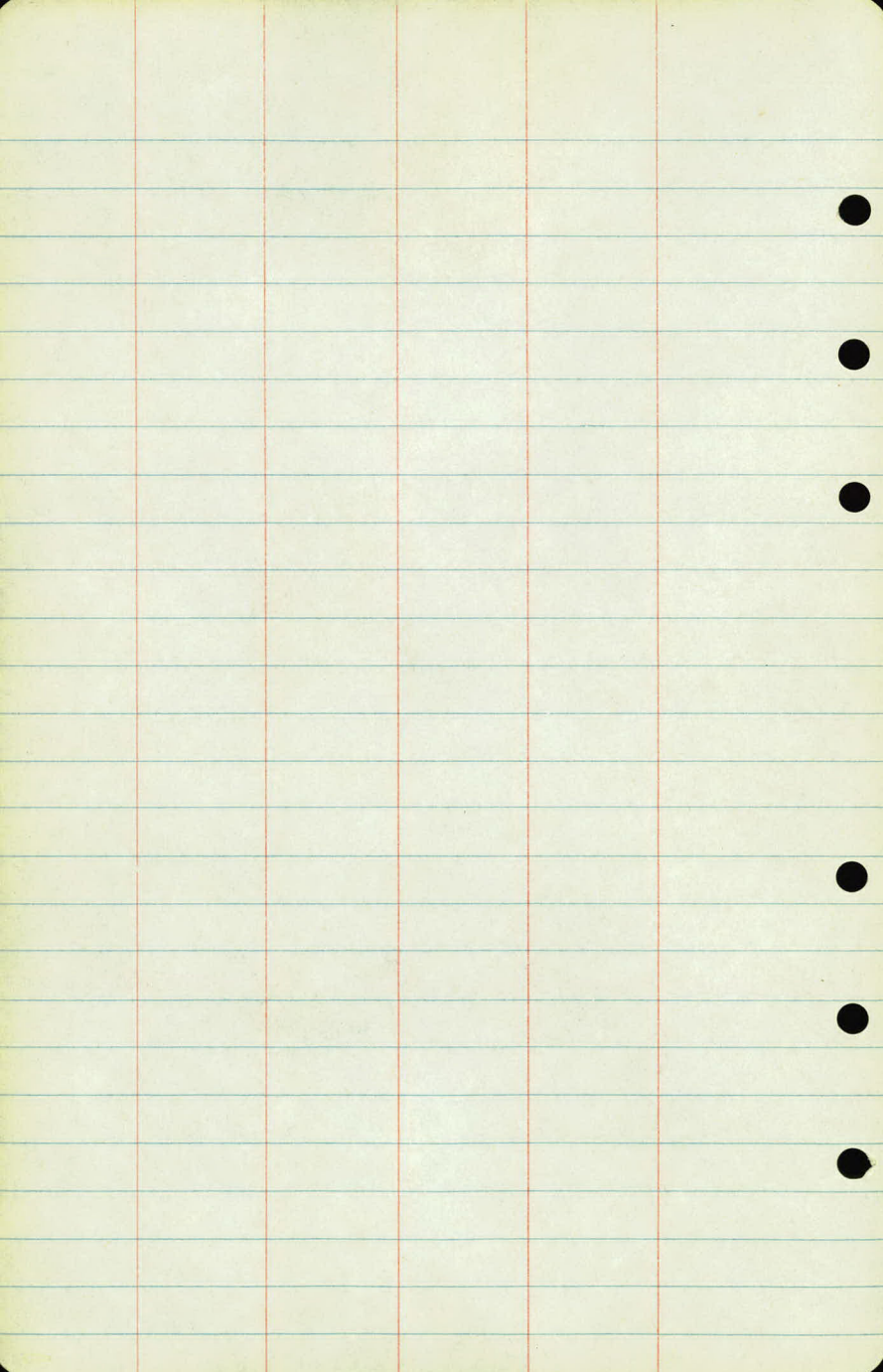
2"X2" HUB

2"X2" HUB

3265

Prop. Line





Topography
Lilas

5 FE-2'

4 +08-FC Cor-4.5'
+06-FC Cor-00

+84-End Row 5" Elm-6'
+05- " "
+06- " "
+06- " "
+07- " "

3 +89- Elm
+70- "
+99- "
+30- "
+11- "

2 Gen. Grave-33'

FE-2'

+73-1 Elm
+66- 5" Elm-31'
+69-SW. Cor. Head-100-355'
+54- Elm
+35- "
+15- "

1 +84-SW. Cor 3" N.W. Pk-2.5'
18'-4'

+97-Reg. Row 5" Elm-4' +75-FC Cor-3'
+72-15' G.M.-33' +61-PP-00
+66-15' G.M.-3' +55-Edge Drive-0

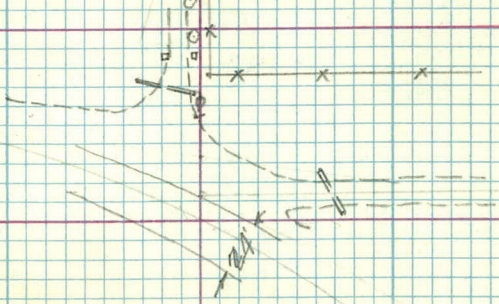
+277 -62'
+143-Edge Pav. +031/2" M-74'

0

Parture

Cult

Cemetery



+57-L in Fe-41'

12

+59-Cor. Silo ^{*14' Dia} Found-4'

+88-Cor Barn-9'

+22-Cor Barn-11'

11

+99-End 8" Vit-7' 15' long

+97-8" Vit-7' -Fe-34'

+66-Fe Cor-2'-15'

10

+66-Fe Cor- ——— +12' → -1'

+37-Fe-17'

9 Fe-31

Fe-13'

8 +03-12" B.E.-8'
Fe-66'

Fe-13'

+82-10" TW B.E.-16'

+58-Fe-11'

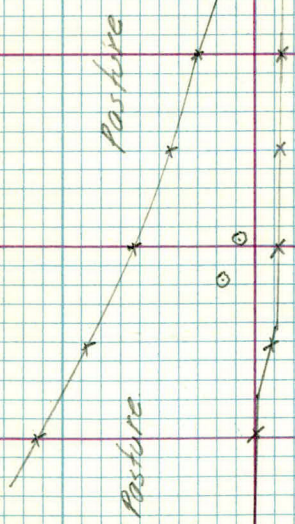
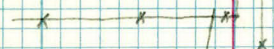
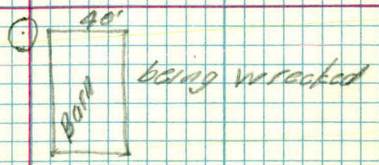
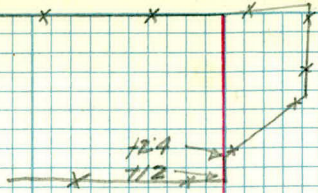
+21-Fe-1'

Fe-1'

7

6

Fe-1'



+25-FG X5 E

17

16

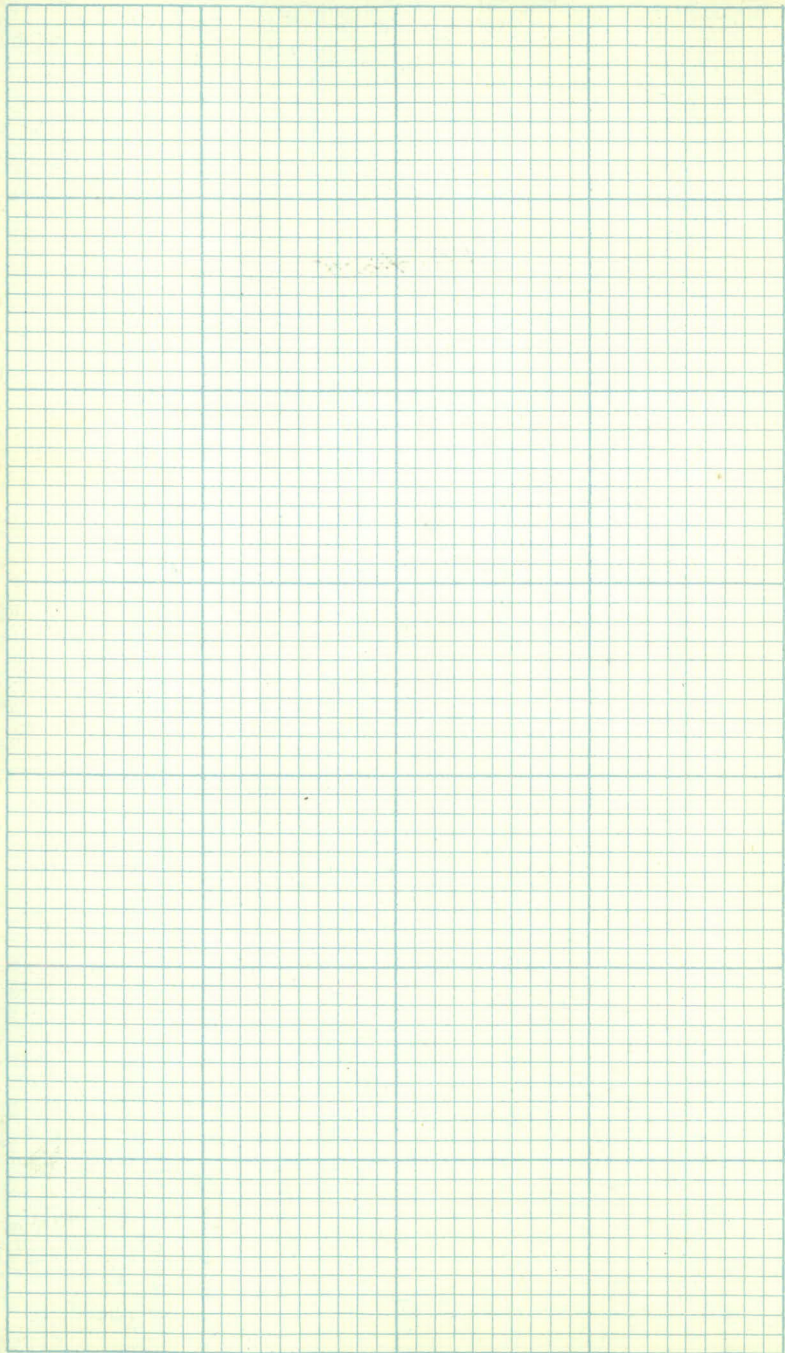
15

14

13

+01-FG X5 G +04-FG Cor - 43'

pasture



Xsections

Lilac

Sta	+	π	-	Elev
T.B.M.	6.24	94074		(93450)
BM			5.27	935.47.
0 +00 =	E White Bear Ave			35.47
+14.9	at edge of pav.			35.94
+30				35.4
+50				35.5
+60				35.4
+65				33.9
+70				35.8
+82				36.5

L

R

Nail in RP N.W. of Turn of Cemetery

Nail & Disc at lot of Lilac Lane & White Bear Ave.

7.50	6.36	5.27	4.20	3.09	L
100	50		50	100	

4.80	4.4	3.4	L
24	50		

EDGE
PHVMT

5.40	5.1	5.4	5.3	5.1	4.5	4.3	5.8	L
29	16	7	—	14	29	90	54	

6.5	6.1	5.2	5.1	6.1	4.7	L
50	27	—	14	26	50	

6.4	5.7	5.1	5.3	6.4	6.0	4.8	4.3
50	23	10	—	9	14	37	50

34.4	35.0	35.6	33.8		34.9	35.3	36.3	
6.3	5.7	5.1	6.9	6.8	5.8	5.4	4.4	L
50	29	6	3	—	8	23	50	

34.3	35.1	35.8		35.6	36.3	36.3	
6.4	5.6	4.9	4.9	5.1	4.4	4.4	L
50	30	13		10	33	50	

35.7	36.2	36.3		36.9	36.6	36.1	L
5.5	4.5	4.4	4.2	3.8	4.1	4.6	
50	22	9		7	32	50	

$\frac{5}{16}$ + π ⁷⁴ - Elev
 940.47

1400 37.1

+50 37.2

2 36.7
 T.P 10.07 ⁴⁰ 945.13 5.41 935.33 06

+45 37.1

+80 35.8

3 34.9

+35 33.1

+65 33.1

37.8	38.1	37.0	37.3		37.1	36.6	35.9	35.6
2.9	2.6	3.7	3.4	3.6	3.6	4.1	4.8	5.1
50	30	25	4		7	18	39	50

38.0	38.2	37.3	37.5		36.8	36.4	35.4
2.7	2.5	3.4	3.2	3.5	3.9	4.3	5.3
50	30	25	8		18	29	50

37.1	37.1	37.1	36.7	37.0	37.1	36.0
3.6	3.6	3.6	4.0	3.7	3.6	4.7
50	38	11		8	27	50

37.4	37.7	37.3	37.5		37.2	36.9	36.0
8.0	7.7	8.1	7.9	8.3	8.2	8.5	9.4
50	31	26	11		8	25	50

37.5	37.4	36.4	36.4	35.8	36.1	35.0	34.3
7.9	8.0	9.0	9.0	9.6	9.3	10.4	11.1
50	32	27	15		4	30	50

36.2	35.9	35.7	35.2		35.1	33.9	33.4
9.2	9.5	9.7	10.2	10.5	10.3	11.5	12.0
50	27	16	11		4	30	50

34.1	33.7	33.6	33.3		32.0	32.9
11.3	11.7	11.8	12.1	12.3	12.4	12.5
50	30	14	10		29	50

32.4	32.5	32.8		33.1	33.3
13.0	12.9	12.6	12.3	12.3	12.1
50	25	10		30	50

Sta	+	T_{40} 945.73	-	Elev.
-----	---	--------------------	---	-------

4+00				33.8
------	--	--	--	------

+50				35.5
-----	--	--	--	------

5				37.4
---	--	--	--	------

+40.9				40.1
-------	--	--	--	------

+70.9				41.4
-------	--	--	--	------

6+00.9				41.7
--------	--	--	--	------

+50				42.4
-----	--	--	--	------

7				43.7
---	--	--	--	------

32.2 31.9 32.1 33.1
13.2 13.5 13.3 12.3 11.6
50 34 24 9 —

33.9 34.2 35.5
11.5 11.2 9.9 ✓
19 36 50

32.4 32.5 33.1 33.9 35.3 35.5
13.0 12.9 12.3 11.5 10.1 9.9
50 34 18 4 2 —

35.4 35.1 35.6 36.3 ✓
10.3 10.3 9.8 9.1
5 20 37 50

34.0 34.6 35.3 36.0 37.0
11.4 10.8 10.1 9.4 8.4 8.0
50 33 30 21 3

36.8 37.0 37.5 ✓
8.6 8.4 7.9
9 30 50

34.7 36.0 37.0 39.1
10.7 9.4 8.4 6.3
50 32 28 7

40.1
5.3

39.0 38.8 39.5 39.8 ✓
6.4 6.6 5.9 5.6
6 17 33 50

35.8 37.1 38.3 40.5 41.4
9.6 8.3 7.1 4.9 4.0
50 33 22 3

40.4 41.1 41.3 ✓
5.0 4.3 4.1
50 30 50
5.7
4.0.

8.5 7.5 6.7 5.1 4.7 3.7 3.3 3.9 4.2 3.6 3.2
50 32 27 9 2 2 4 11 32 50

5.8 5.7 5.3 3.9 3.0
50 33 16 1 —

3.5 3.3 2.7
11 31 50

2.7 3.2 2.9 2.4 1.7 2.4 1.8 0.9 ✓
50 33 13 1 — 11 33 50

Sta	+	T_{40}	-	Elev.
		945.13		44.9
7+36		37		.99
T.P.	5.38	950.40	0.41	944.72

+70				46.0
-----	--	--	--	------

8				46.6
---	--	--	--	------

+40				44.9
-----	--	--	--	------

+64				41.5
-----	--	--	--	------

+84				40.6 X
-----	--	--	--	--------

9				40.6
---	--	--	--	------

+28				41.1
-----	--	--	--	------

5.3	2.4	1.6	1.3	<u>0.5</u>	0.8	0.2	+0.3	✓
53	42	33	16		13	32	50	

11.8	11.3	8.4	5.8	5.6	4.4	3.5	4.2	3.8	3.3	3.0	✓
50	39	29	18	10		6	10	19	36	50	

11.2	11.3	10.2	7.2	6.7	4.7	<u>3.8</u>	3.4	3.3	3.4	✓
50	38	24	15	10	5		7	34	50	

7.5	7.4	9.8	10.6	10.4	8.8	<u>5.5</u>	3.9	3.8	3.9	5.1	✓
50	41	34	29	19	9		9	16	25	50	

7.0	7.1	10.6	10.5	9.8	8.9	<u>5.5</u>	5.1	4.9	5.2	5.9	✓
50	32	25	15	5			11	14	21	35	50

7.0	6.3	6.5	9.1	10.1	<u>9.8</u>	8.7	6.5	5.8	6.2	✓
50	38	26	19	8		9	14	36	50	

7.0	6.1	6.5	9.1	9.8	9.7	7.0	5.9	6.4	✓
50	33	20	12		7	17	40	50	

6.4	6.0	6.3	7.1	7.6	<u>9.3</u>	7.5	8.9	9.7	7.9	7.8	6.7	6.5	✓
50	34	22	18	7		6	16	21	25	32	39	50	

Sta	+	π 930.10 ³⁷	-	Elev
-----	---	-------------------------------	---	------

9+49				42.7
------	--	--	--	------

+80?				43.0
------	--	--	--	------

10				45.2
----	--	--	--	------

+37				45.7
-----	--	--	--	------

+68				45.9
-----	--	--	--	------

11		960.74		46.4
T.P.	12.48	960.47	2.11	948.26
				947.99

+50				48.2
-----	--	--	--	------

12				50.2
----	--	--	--	------

L

Q

R

$\begin{array}{r} 5.5 \\ 50 \end{array}$
 $\begin{array}{r} 5.8 \\ 33 \end{array}$
 $\begin{array}{r} 6.1 \\ 15 \end{array}$
 $\begin{array}{r} 7.2 \\ 12 \end{array}$
 $\begin{array}{r} 7.7 \\ \hline \end{array}$
 $\begin{array}{r} 9.1 \\ 6 \end{array}$
 $\begin{array}{r} 8.5 \\ 23 \end{array}$
 $\begin{array}{r} 9.3 \\ 27 \end{array}$
 $\begin{array}{r} 8.2 \\ 32 \end{array}$
 $\begin{array}{r} 7.8 \\ 42 \end{array}$
 $\begin{array}{r} 6.7 \\ \hline 47-50 \end{array}$

$\begin{array}{r} 4.3 \\ 50 \end{array}$
 $\begin{array}{r} 5.0 \\ 34 \end{array}$
 $\begin{array}{r} 5.7 \\ 22 \end{array}$
 $\begin{array}{r} 5.7 \\ 5 \end{array}$
 $\begin{array}{r} 7.4 \\ \hline \end{array}$

$\begin{array}{r} 8.1 \\ 14 \end{array}$
 $\begin{array}{r} 8.0 \\ 34 \end{array}$
 $\begin{array}{r} 8.5 \\ 38 \end{array}$
 $\begin{array}{r} 8.0 \\ 40 \end{array}$
 $\begin{array}{r} 7.8 \\ 50 \end{array}$

$\begin{array}{r} 4.1 \\ 50 \end{array}$
 $\begin{array}{r} 4.9 \\ 29 \end{array}$
 $\begin{array}{r} 5.3 \\ 11 \end{array}$
 $\begin{array}{r} 5.2 \\ \hline \end{array}$

$\begin{array}{r} 6.5 \\ 5 \end{array}$
 $\begin{array}{r} 6.8 \\ 13 \end{array}$
 $\begin{array}{r} 8.0 \\ 24 \end{array}$
 $\begin{array}{r} 7.6 \\ \hline 39-50 \end{array}$

$\begin{array}{r} 4.8 \\ 50 \end{array}$
 $\begin{array}{r} 5.1 \\ 30 \end{array}$
 $\begin{array}{r} 5.0 \\ 9 \end{array}$
 $\begin{array}{r} 4.7 \\ \hline \end{array}$

$\begin{array}{r} 4.5 \\ 14 \end{array}$
 $\begin{array}{r} 6.0 \\ 24 \end{array}$
 $\begin{array}{r} 7.0 \\ 31 \end{array}$
 $\begin{array}{r} 7.1 \\ 50 \end{array}$

$\begin{array}{r} 4.1 \\ 50 \end{array}$
 $\begin{array}{r} 4.4 \\ 28 \end{array}$
 $\begin{array}{r} 4.5 \\ \hline \end{array}$

$\begin{array}{r} 4.8 \\ 16 \end{array}$
 $\begin{array}{r} 5.1 \\ 30 \end{array}$
 $\begin{array}{r} 6.5 \\ 50 \end{array}$

$\begin{array}{r} 3.5 \\ 43 \end{array}$

$\begin{array}{r} 4.0 \\ \hline \end{array}$

$\begin{array}{r} 4.1 \\ 13 \end{array}$

$\begin{array}{r} 5.0 \\ 35 \end{array}$
 $\begin{array}{r} 5.3 \\ 50 \end{array}$

$\begin{array}{r} 12.1 \\ 50 \end{array}$
 $\begin{array}{r} 12.1 \\ 24 \end{array}$
 $\begin{array}{r} 12.5 \\ \hline \end{array}$

$\begin{array}{r} 4.0 \\ 13 \end{array}$
 $\begin{array}{r} 5.0 \\ 35 \end{array}$
 $\begin{array}{r} 5.3 \\ 50 \end{array}$

$\begin{array}{r} 9.9 \\ 50 \end{array}$

$\begin{array}{r} 9.9 \\ 30 \end{array}$

$\begin{array}{r} 10.5 \\ \hline \end{array}$

$\begin{array}{r} 10.2 \\ 25 \end{array}$

$\begin{array}{r} 9.9 \\ 50 \end{array}$

sto + π_{74} - E/EX
960.47

12+50 51.9

+ 91.74 53.8

13+21.74 54.8

+ 50.74 54.5

14 53.8

+20 53.6

+62 55.0

15 56.8

L E

9.0	8.9	8.8	8.4	7.8	✓
50	29	—	25	50	

7.6	7.2	6.9	6.6	6.2	6.0	✓
50	27	—	24	35	50	

7.6	6.9	5.9	5.7	5.5	5.8	✓
50	25	—	15	33	50	

8.4	7.9	6.2	5.6	5.3	✓
50	33	—	33	50	

8.8	8.2	6.9	6.2	6.1	5.9	✓
50	30	—	19	37	50	

8.3	7.8	7.1	6.5	6.1	✓
50	31		24	50	

5.6	5.3	5.7	5.9	5.8	✓
58	29		30	50	

4.1	3.7	3.6	3.9	4.9	5.4	✓
50	37	11		32	50	

Sta + π_{74} - Elev.
~~98049~~

15+30 58.1

+70 58.7 X

16 58.4

+21 57.5

+56 55.2

91.85
 X 94.85 54.9

17+24.85 ± EAST AVE 55.7
~~55.6~~

+54.85
 B.M. 1087 949.60 .87
 (949.94)

949.94

5-5-47

14

L

E

L

3.6	2.9	2.4	<u>2.6</u>	3.6	5.0 ✓
50	33	10		26	50

3.8	3.2	2.4	2.0	2.1	3.3	4.5 ✓
50	42	22		11	34	50

4.0	3.4	2.8	<u>2.3</u>	2.5	3.9 ✓
50	33	19		22	50

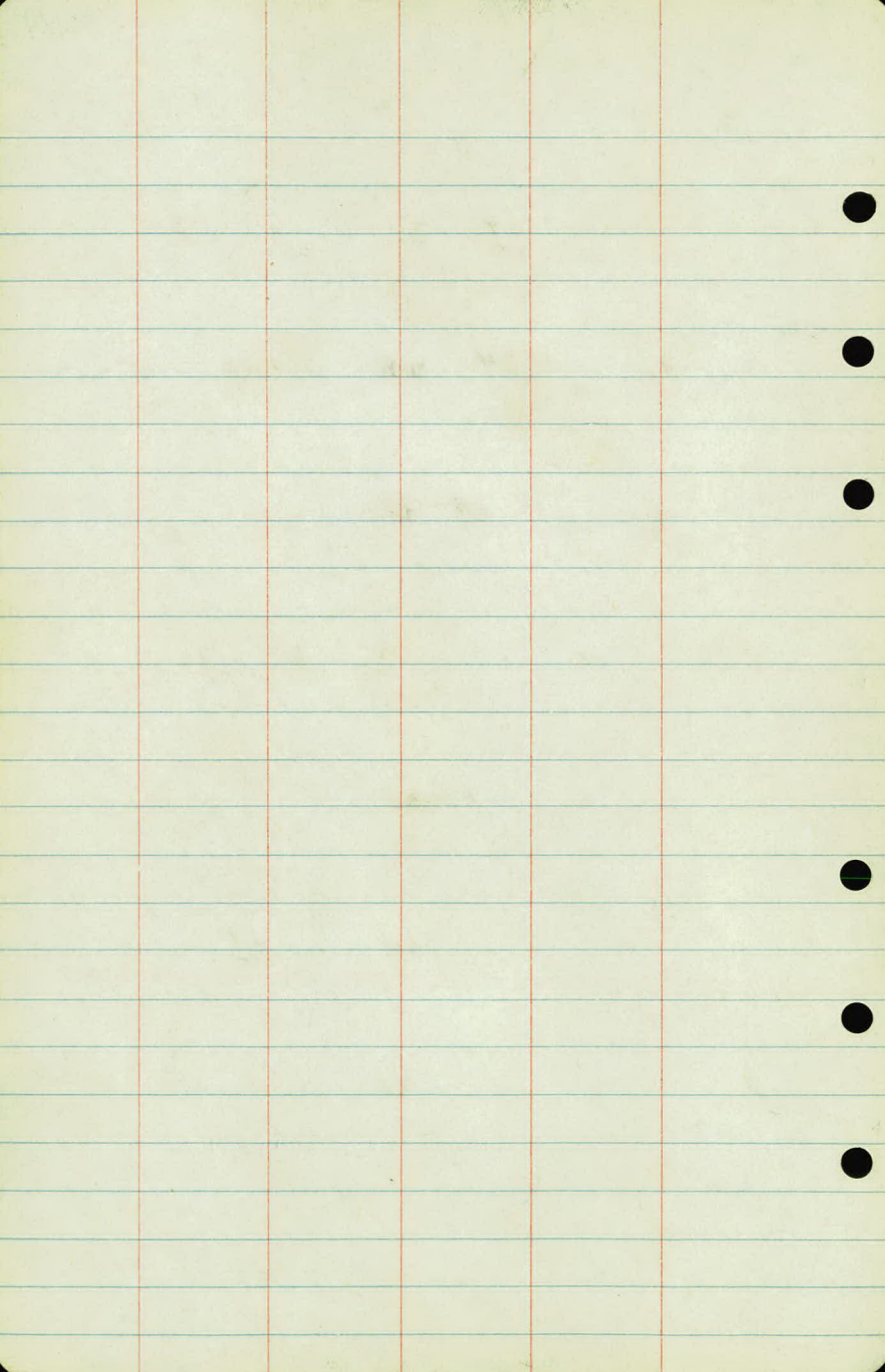
4.8	4.2	<u>3.2</u>	3.1	3.7 ✓
50	33		21	50

6.5	6.4	<u>5.5</u>	4.0	3.5 ✓
50	33		33	50

8.0	7.4	<u>5.8</u>	4.5	3.9 ✓
50	33		33	50

51

P.R. Spt. in 8" Elm N of East Ave & Seashore Blvd.



1

Alignment
Gardnerette Dr. S.

Align
XSCG

1-3
4-9

Rec

5/3/47

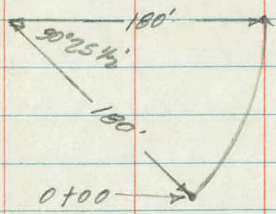
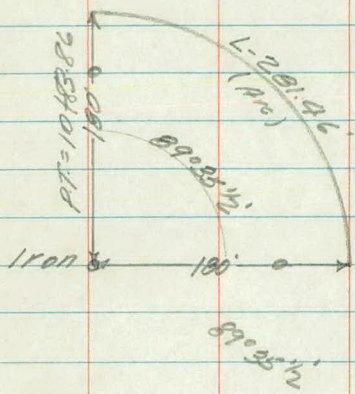
Sta Point

B+024 PC

0+9558 PT.

5-2-47

2



Sta. Point

1418432 = Φ Lilac Lane

1246386 P.O.T. = Φ Gardenette Drive N.

1048386 PT

5-2-47

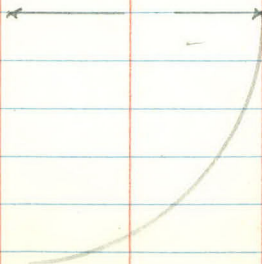
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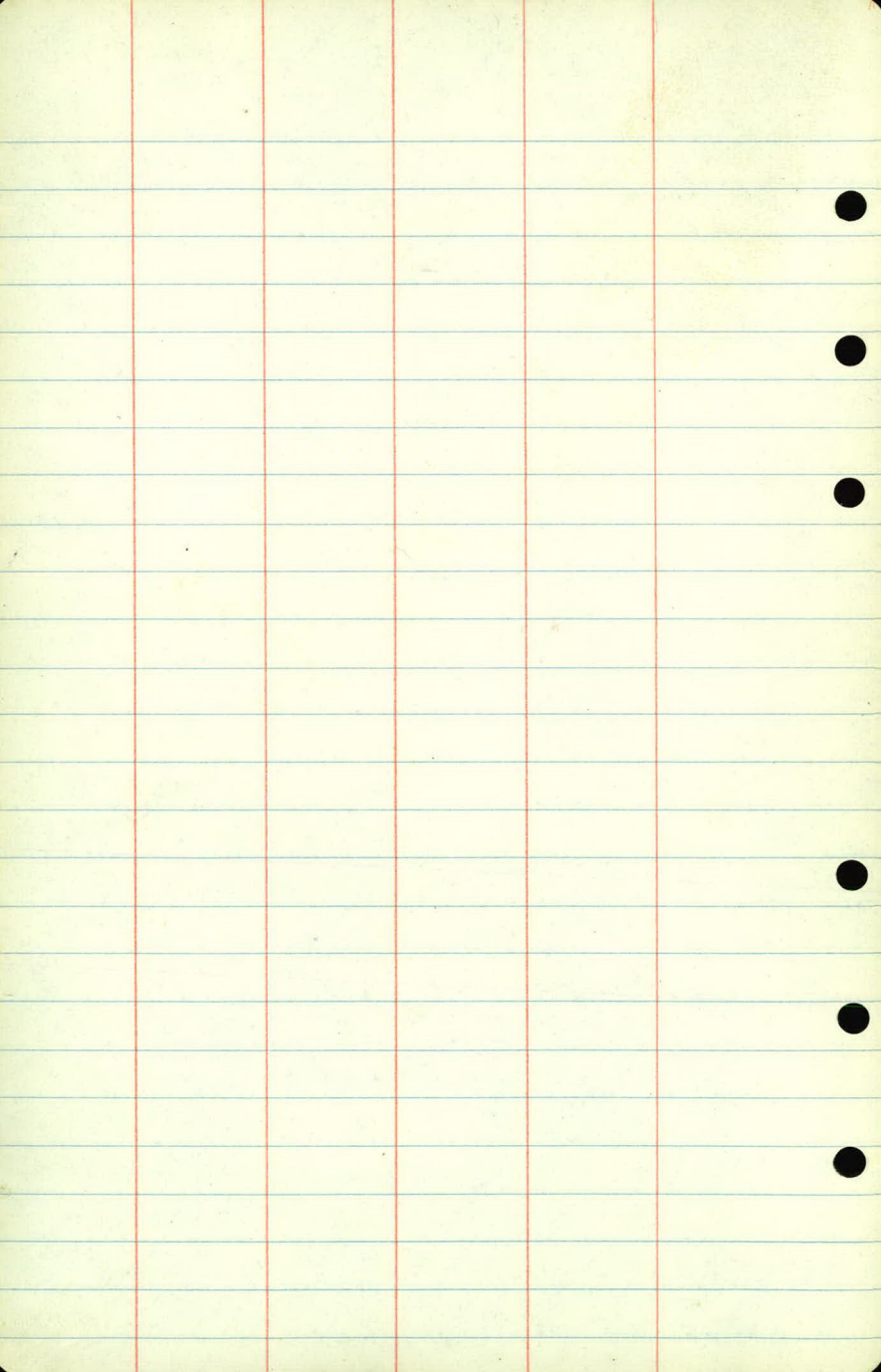


2"X2"Hub



2"X2"Hub





Xsections

Gardendale Drive S.

Sta	+	π	-	Elev.
T.B.M.	8.41	9 47.80		(939.39)

0 +00				41.6
-------	--	--	--	------

+50				41.2
-----	--	--	--	------

+95.58				40.9
--------	--	--	--	------

1				40.9
---	--	--	--	------

2				42.6
---	--	--	--	------

3				43.4
---	--	--	--	------

+35				43.7
-----	--	--	--	------

4				43.3
---	--	--	--	------

5-2-47

5

Top Iron at 150' Rod Pt.

7.5	7.2	6.2	4.8	4.2	3.8
50	27	—	22	36	50

7.1	7.0	6.6	5.6	3.6
50	12		26	50

7.1	7.1	7.36.9	6.7	5.9	4.8
50	30	11	19	31	50

DUP 0 + 95.58

6.2	5.7	5.2	4.9	4.8
50	30		30	50

5.4	4.9	4.4	4.4	4.5
50	30		30	50

4.8	4.7	4.1	3.9	3.8
50	30		30	50

4.3	4.7	4.5	4.4	4.3
50	30		30	50

Sta	+	π	-	Elev
		947.80		
4+50				43.0
5				43.2)
+50				44.2
6				46.1
T.P.	11.65	957.98	1.47	946.33
+50				48.6
7				50.9
+48				51.4
8				47.6

L E R

4.6	4.8	4.8	4.9	4.7
50	30	<u>4.8</u>	30	50

4.1	4.7	4.6	4.5	4.3
50	30		30	50

3.9	4.0	3.6	3.3	3.5
50	30	<u>3.6</u>	30	50

3.5	3.2	1.7	1.1	1.3
50	30		29	50

12.2	11.3	10.3	9.4	8.8	8.6	9.1
50	28	11	<u>9.4</u>	15	31	50

9.4	8.4	7.5	7.1	7.1	7.5	8.1
50	36	17		11	30	50

8.6	7.4	6.6	7.5	7.6
50	26		22	50

9.4	9.5	10.4	11.1	11.6
50	30		29	50

Sta	+	π ✓	—	Elev.
		957.98		
8+28				47.4
+63				49.0
9				49.6
+50				50.4
10				52.5
+50				54.4
+83.86				54.9
11				54.8

L					
8.8	10.4	10.6	11.2	11.3	✓
50	24		29	50	

8.1	8.4	9.0	9.3	9.0	✓
50	30		30	50	

7.0	7.5	8.1	8.4	8.1	8.8	8.9
50	30	7	<u>7</u>	7	33	50

7.0	7.3	7.6	8.1	8.4
50	30	<u>7</u>	30	50

6.3	6.2	6.2	5.5	6.0	6.7
50	30	13		30	50

4.8	4.5	4.0	3.6	3.3	4.0	4.3
50	37	19		14	30	50

4.0	3.7	3.1	2.3	2.9
50	30		30	50

3.6	3.6	3.3	3.2	2.5	2.9
50	30	22	<u>3</u>	30	50

Sta	+	Adj.	-	Elev.
		95798		

11+50				54.2
-------	--	--	--	------

12				55.2
----	--	--	--	------

+33.86				55.5
--------	--	--	--	------

+63.86				55.7
--------	--	--	--	------

T.P	3.52	959.48	2.02	955.96
+93.86				54.8

13				54.8
----	--	--	--	------

+50				53.3
-----	--	--	--	------

14				53.4
----	--	--	--	------

L

E

R

3.5 4.0
50 30

3.8 3.1
30

3.1 ✓
50

3.5 3.4 3.0
58 38 25

2.8

2.2 2.4 ✓
30 50

2.8 2.7
50 27

2.5

1.8
13

1.9 1.9 ✓
30 50

2.9 2.5 2.7 2.3
50 26 15

2.3 2.1 ✓
27 50

5.6 5.3 5.0 4.9
50 35 19

4.3
30

4.5 ✓
50

Dup + 93.86

7.2 6.7 6.2
50 31

5.9 5.5 ✓
29 50

7.5 6.6 6.1
50 29

5.4
31

5.2 ✓
50

STA + π - Elev

959.48

14+51.32

55.2

14+84.32

54.9

B.M.

957

949.91

1
(949.94)

5-2-47

9

LT

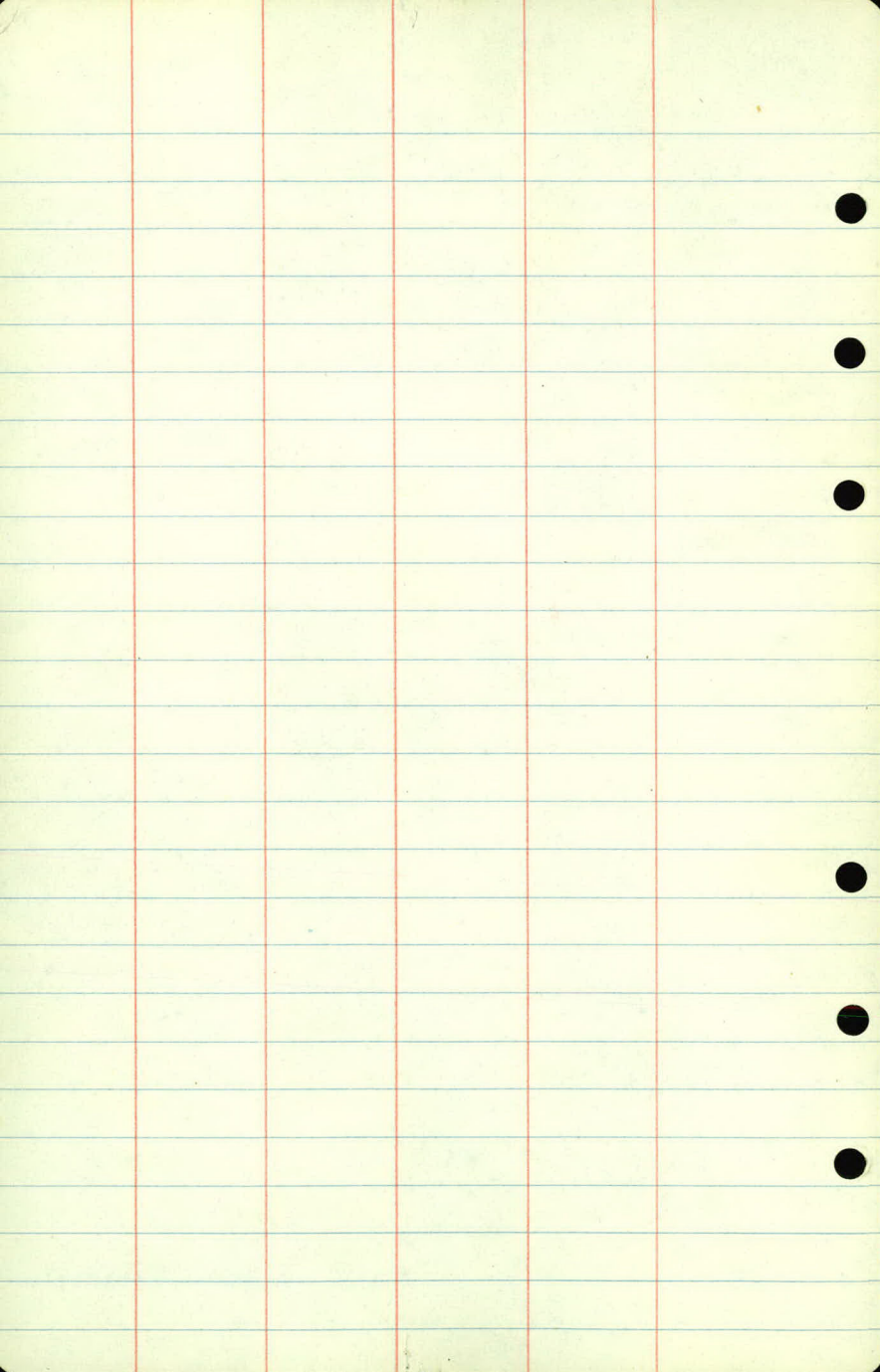
L

RT

6.0	5.2	4.5	4.3	4.4	4.3	L
50	35	21		22	50	

46

R.R. Spk. in 8" Elm N.W. Cor. East Av. & So. Shore Blvd.



1
Alignment

Floral Drive

INDEX

Align 1-2

Topog. 3-4

Xsections 5-13

Drawn up

5/47

Sta Point

26 + 42.94 = Sta. 3 + 83.0 East Ave.

13 + 21.52 P.O.T = 4

0 + 00 = White Bear Ave.

K.P.
A.M.
N.B.

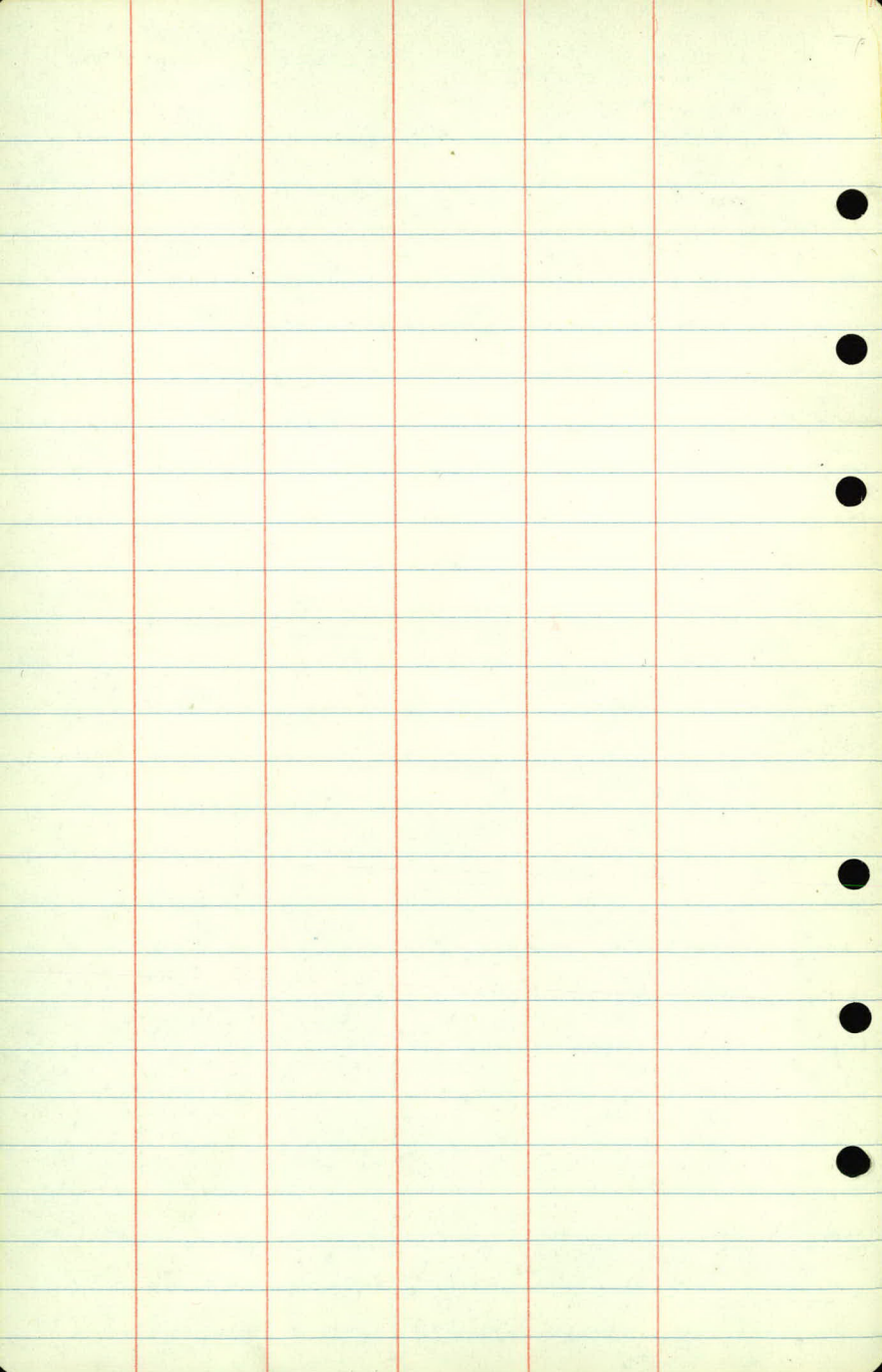
4-25-47

2

2" X 2" Hub

$90^{\circ} 31\frac{1}{2}'$

$89^{\circ} 28' 0''$



Topography
Floral

+42-FC. X5 E

26



136-54-33'

+32-FC. X5 E

139-54-13'

137-54-13'

0

1085 Edgeport

4-25-41

Cult.

4

x x x x x x x

Cult.

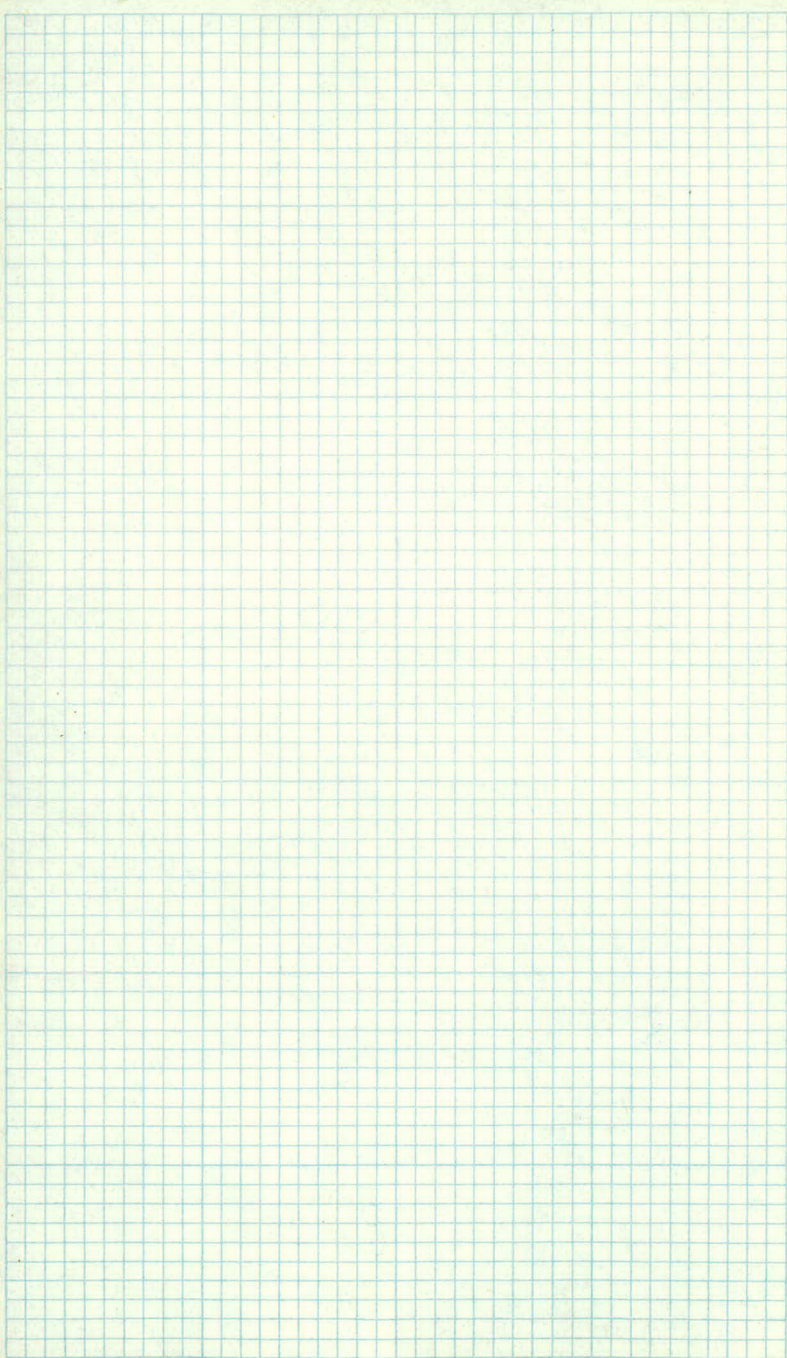
Cult.

|||||

Prov.

20

|||||



Xsections
Floral

Sta	+	Σ	-	Elev.
B.M.	5.37	946.44 946.44		(941.07)

0	+00			42.55
---	-----	--	--	-------

	+035 = Edge Pav.			42.48
--	------------------	--	--	-------

	+12			42.4
--	-----	--	--	------

	+18			40.1
--	-----	--	--	------

	+26			39.8
--	-----	--	--	------

	+29			41.2
--	-----	--	--	------

1				40.9
---	--	--	--	------

2				41.3
---	--	--	--	------

K.A.
A.M.
M.B.

4-29-47

6

L

E

R

Top Iron Sec. Cor Marker at "F" E White Bear Ave

417	417	403	402	393	391	389	404	421	442	460	537
300	250	200	150	100	50		50	100	150	200	383

397
50

396

408
50

40
50

40

41
50

66	63	63	61	59
50	25		27	50

69	66	66	64	62
50	25		25	50

54	54	52	52	52
50	24		25	50

58	57	54	57	55	53	53	51
50	36	25	14		18	30	50

56	54	50	52	51	50	53	48
50	35	27	15		18	31	50

Sta	+	π	-	Elev
		946.44 945.44		

2+55

41.4

3

41.5

+50

42.1

4

42.3

5

T.P. 5.45

949.02

~~948.02~~

2.87

43.1

~~943.57~~
~~942.57~~

+40

44.1

+85

45.3

6

45.4

L Φ R

5.5 5.1 5.0 4.6 4.8 4.4
50 30 18 30 50

5.1 4.8 4.9 4.6 4.9 4.8
50 25 — 20 32 50

4.6 4.3 4.5 4.3 4.2 4.5 4.1
50 30 14 — 18 30 50

4.3 4.0 4.3 4.1 3.8 4.1 3.6
50 27 12 — 18 31 50

3.4 3.1 3.5 3.3 3.3 3.6 3.3
50 31 15 15 31 50

5.2 4.8 4.9 4.9 5.5 5.8
50 31 17 30 50

4.2 3.5 3.8 3.7 4.3 5.1
50 28 10 — 26 50

4.1 3.3 3.6 3.7 4.3 4.1
50 29 — 17 30 50

Sta	+	949.02 948.02	—	Elev
6	+50			45.5
7				44.9
	+50			44.0
8				43.9
	+50			44.0
9				44.2
10				44.0
11				43.7
T.P.	6.77	950.95 949.95	4.84	944.18 943.18

L - 2 R

4.4	3.5	3.7	3.5	3.6	4.0	4.2
50	27	12	<u>—</u>	23	36	50

4.9	4.0	4.1	4.3	4.5	4.6
50	32	<u>—</u>	19	30	50

5.4	4.9	5.0	5.0	5.0
50	27	<u>—</u>	26	50

5.2	5.0	5.1	5.0	4.8
50	26	<u>—</u>	30	50

5.1	4.8	5.0	4.7	4.2
50	28	<u>—</u>	30	50

5.2	4.9	4.8	4.6	4.4
50	28	<u>—</u>	30	50

5.0	5.1	5.2	5.0	4.7	4.5
50	28	11	<u>—</u>	30	50

5.5	5.4	5.3	4.7	4.8
50	31	<u>—</u>	27	50

Sta	+	-	Elev.
		950.95	
		949.95	

11+50

43.7

12

44.4

+45

44.9

12 +91.52 W. Prop Line

45.5

13+21.52 E. Balleriew

B.M

6.73

45.7

944.22
943.22

944.21

943.21

13
13+51.52 E. Prop Line

45.8

14

45.8

15

46.1

L E E

7.7	7.5	7.5	7.3	6.8	6.4	6.4
50	30	9	—	32	41	50

6.8	6.5	6.8	6.6	6.3	6.4
50	30	8	—	30	50

6.1	5.9	6.3	6.1	5.8	5.8
50	31	9	—	26	50

5.9	5.6	5.8	5.5	5.1	5.3
50	34	9	—	27	50

5.6	5.4	5.6	5.3	5.0	5.0
50	27	10	—	26	50

R.R. Spk. 1030' SW. Cor. Co. Rd. F. & Bellevue

5.4	5.3	5.5	5.2	5.0	5.0
50	27	10	—	26	50

5.3	5.3	5.5	5.2	5.1	4.9
50	30	12	—	26	50

5.6	5.2	5.3	4.9	4.7	4.5
50	26	12	—	25	50

Sta	+		-	Elev
		958.95		
		949.95		

15	+50			45.5
----	-----	--	--	------

16				44.0
----	--	--	--	------

	+50			43.4
--	-----	--	--	------

17				43.5
----	--	--	--	------

	+50			44.2
--	-----	--	--	------

	+80			44.2
--	-----	--	--	------

18				43.8
----	--	--	--	------

	+50			42.5
--	-----	--	--	------

		951.44		942.33
T.P.	9.11	950.44	8.62	941.33

L Q R

7.4 6.5 5.5 5.1 4.8
50 28 — 25 50

7.6 8.6 8.0 7.0 6.2 5.6 5.3
50 28 14 — 16 31 50

POCKET 10.3 9.8 8.9 7.6 5.7 5.4
50 32 17 — 31 50

9.6 9.3 8.4 7.5 5.8 5.1 5.1
50 31 12 — 25 31 50

7.4 7.7 6.8 5.7 5.1
50 25 — 27 50

6.8 7.1 7.3 6.8 5.7 5.5
50 27 10 — 33 50

6.8 7.0 7.5 7.2 6.9 6.1 5.8
50 32 11 — 13 35 50

7.1 7.3 8.4 8.5 8.8 8.8
50 36 10 — 18 50

Sta	+	T	-	Elev
-----	---	---	---	------

951.44
950.44

19700

41.9

+50

41.6

20

41.0

+50

40.4

21

40.5

+50

41.5

22

42.1

+50

43.2

L E R

8.9	9.1	9.5	10.0	10.4
50	32		29	50

10.5	10.5	9.8	9.9	10.3
50	30	—	28	50

Picket 7

11.0	10.9	10.4	10.3	11.1
60	26	—	27	50

11.1	11.2	11.0	10.8	11.1
60	28	—	25	50

10.7	10.8	10.9	10.6	10.6
50	25	—	30	50

9.5	9.9	9.9	9.9	9.0	8.5
50	33	—	16	34	50

8.8	9.1	9.3	8.2	6.8
50	23		28	50

8.7	9.1	7.8	6.3	5.2
50	27	—	28	50

Sta	+	-	Elev.
		951.44 950.44	

23	+00		44.3
----	-----	--	------

	+50		44.5
--	-----	--	------

24			45.4
----	--	--	------

	+30		45.9
--	-----	--	------

	+70		47.3
--	-----	--	------

25			47.2
----	--	--	------

	+50		46.9
--	-----	--	------

26			47.0
----	--	--	------

L E R

8.3	7.8	7.1	6.0	5.0
50	28	—	27	50

7.1	7.0	6.9	6.1	5.5
50	28	—	30	50

5.9	5.9	6.0	6.0	5.8
50	32	—	26	50

5.5	5.4	5.5	5.3	5.2
50	30	—	34	50

4.2	4.2	4.1	4.1	4.1
50	30	—	23	50

4.3	4.3	4.2	4.0	4.0
50	30	—	30	50

4.6	4.5	4.5	4.2	4.1
50	29		30	50

4.2	4.3	4.4	4.2	3.9
50	25	—	30	50

Sta + $\begin{matrix} 951.44 \\ 750.44 \end{matrix}$ - Elev.

26+40

48.5

+42.94 = 2 East Ave.

49.4

27

0.6

50.8

+50

0.0

51.4

28

0.2

51.2

55. to east

B.M.

0.52

950.92 950.95

949.92 (949.95)

9-29-47

13

L

E

E

3.1	3.1	2.9	2.5	1.6
50	25	—	25	50

2.2	2.1	2.0	1.5	0.7
50	25	—	25	50

R.R. Spt. 14 30' Oak 100' S. of East Ave & Co. Rd. 'F'

Sta + π — Elev

Floral St.

Staking Notes

Sta	P.G.	P.E.R.	SW.G.R.	P.G.R.	
B.M.	548	94655			(94.07)
	616	94723			
0 +00	42.55	4.00			
+50	42.5	4.0	3.7	4.73	
1	42.5	4.0	3.7	4.73	
+50	42.6	3.9	3.6	4.63	
2	42.6	3.9	3.6	4.63	
+50	42.6	3.9	3.6	4.63	
3	42.7	3.8	3.5	4.53	
+50	42.7	3.8	3.5	4.53	

K.A.
A.M.
M.B.
R.K.

5-12-47

L

Q

R

Top of Iron Sec. Cor Marker Co. Rd. "F" & W. Bear Ave.

336' / -1.8
5.5

-1.6
5.6

-1.8 / 33.6
5.5

344' / -2.2
5.9

-1.7
5.7

-1.8 / 33.6
5.5

344' / -2.2
5.8

-1.6
5.5

-1.8 / 33.6
5.4

336' / -1.8
5.4

-1.7
5.3

-1.7 / 33.4
5.3

338' / -1.9
5.5

-1.3
5.2

-1.4 / 32.0
5.0

332' / -1.6
5.1

-1.2
5.0

-1.5 / 32.0
5.0

32.0 / -1.0
4.5

-0.7
4.5

-1.4 / 32.2
4.6

Sto	PG	P.G.R.	SWGR	
		946.55		
		947.23		
4	427	3.9	9.6	453 ✓

+50	427	3.9	9.6	453 ✓
-----	-----	-----	-----	-------

5	42.8	3.8	3.5	443
T.P.	546	949.01	300	945.55
		947.23		

+50	42.8	6.2	5.9	443
-----	------	-----	-----	-----

6	42.8	6.2	5.9	443
---	------	-----	-----	-----

+50	42.9	6.1	5.8	433
-----	------	-----	-----	-----

7	42.9	6.1	5.8	433
---	------	-----	-----	-----

+50	42.9	6.1	5.8	433
	5.00	947.89	434	942.89

L

C

R

$$314' / -07$$

$$43$$

$$-04$$

$$43$$

$$-07$$

$$43$$

Ground: 9.0

$$BT$$

$$\frac{36}{20}$$

$$-01$$

$$38$$

$$BT \checkmark$$

$$\frac{36}{20.0}$$

3.8 = Ground.

$$904' / +02$$

$$33$$

$$+04$$

$$34$$

$$BT$$

$$\frac{35}{20}$$

37 = 61.

$$926' / +12$$

$$46$$

$$+14$$

$$48$$

$$+03$$

$$56 / 328$$

$$348' / +04$$

$$35$$

$$+8.5$$

$$37$$

$$+1.4$$

$$45 / 328$$

$$94.0' / +2.0$$

$$3.8$$

$$+2.5$$

$$3.6$$

$$+1.8$$

$$40 / 326$$

$$320' / +15$$

$$43$$

$$+2.0$$

$$41$$

$$+1.2$$

$$46 / 324$$

$$316' / +08$$

$$50$$

$$+1.1$$

$$50$$

$$+0.6$$

$$52 / 312$$

Sta	PG	PCR	SWGR	BT	
		949.01			
		94789			
8	430	6.0	57	489	
+50	430	6.0	57	489	
9	430	6.0	57	489	
+50	430	6.0	57	489	
10	431	5.9	56	479	
+50	431	5.9	56	479	
11	43.2	5.9	56	469	
TP	6.58	950.75	4.84	944.17	
		94789			
+50	43.4	7.4	7.1	449	
BM	6.53	950.74	6.53	944.22	(944.21)

L

E

R

32.2' / 4.1
4.510.9
5110.8 / 4.9
31.6'32.0' / 4.1
4.711.1
4911.1 / 4.6
32.2'31.6' / 4.0
4.811.2
4810.9 / 4.8
31.8'31.6' / 4.0
4.910.9
5110.8 / 4.9
31.6'31.2' / 4.0
5.010.9
5010.9 / 4.7
31.8'30.8' / 4.0
5.210.8
5110.8 / 4.8
31.6'30.4' / 4.0
5.410.6
5311.0 / 4.6
32.0'

Gr. 715

BT
71
3010.2
7.210.6 / 6.5
31.2'

R.R. Spk in 24' Oak. S.W. cor. Co. Rd. F" & Bellview

STO	PG	PGR	SWGR	BT	
		95074 94789			
12	43.8	6.9	6.6	409	
+50	44.2	6.5	6.2	3.69	
+91.5 BM	44.7 5.21	6.0 949.42	5.7 3.68	3.19 944.21	944.21
13 + 21.52	45.0	5.74			
+51.5	45.1	5.6	5.3	4.32	
14	45.0	5.7	5.4	4.42	
+50	44.6	6.1	5.8	4.82	
15	44.3	6.4	6.1	5.12	

L

Q

R

$$\frac{30.6'}{3.3} + 0.3$$

$$\frac{+0.5}{6.4}$$

$$\frac{+0.4}{6.2} + 0.5'$$

$$\frac{31.0'}{5.7} + 0.5$$

$$\frac{+0.7}{5.8}$$

$$\frac{+0.7}{5.5} + 0.4'$$

Gr = 56 =

$$\frac{B.T.}{30'} + \frac{5.7}{30'}$$

$$\frac{+0.6}{5.4}$$

$$\frac{+0.7}{5.0} + 0.4'$$

SpK in 30" E/m Co Rd F & Balkview

$$\frac{+0.7}{5.05}$$

Gr = 52

$$\frac{B.T.}{30'} + \frac{5.3}{30'}$$

$$\frac{+0.5}{5.1}$$

$$\frac{+0.4}{4.9} + 0.5'$$

$$\frac{30.6'}{5.1} + 0.3$$

$$\frac{+0.7}{5.0}$$

$$\frac{+0.5}{4.9} + 0.0'$$

$$\frac{31.6'}{5.0} + 0.6$$

$$\frac{+1.3}{4.8}$$

$$\frac{+1.1}{4.7} + 0.2'$$

$$\frac{32.0'}{5.1} + 1.0$$

$$\frac{+1.7}{4.7}$$

$$\frac{+1.6}{4.5} + 0.2'$$

Sta	P.G.	P.G.R.	S.W.G.R.	ZT
		950.74		
		949.42		
15 +50	43.9	6.8	6.5	5.52
16	43.6	7.1	6.8	5.82
T.P.	228	946.95	6.07	944.67
	2.40	949.42	-5.82	943.64
+50	43.2	3.8	3.5	2.84
17	42.9	4.1	3.8	3.14
+50	42.5	4.5	4.2	3.54
18	42.2	4.8	4.5	3.84
+50	41.9	5.1	4.8	4.14
19	41.7	5.3	5.0	4.34

Rain PM.

L

C

R

B.T.
+1.0
65
30

+1.5
53

+1.7
48/32.4

34.0/-2.0
58

+0.3
68

+1.4
54/32.5

35.8/-2.4
59

+0.2
36

+1.8
1.7/32.6

33.2/-1.6
54

+0.6
35

+2.4
19/34.8

31.2/+0.6
36

+1.6
29

+2.7
1.5/35.4

32.8/+1.4
31

+1.6
32

+2.5
2.0/35.0

32.6/+1.3
3.5

+0.6
45

B.T.
48
30 47 = Gr.

30.8/+0.4
5.4

+0.2
51

-0.6
5.6/31.2

Sta.	P.G.	P.G.R.	W.G.R.	
		946.95 746.04		
19 +50	41.6	5.4	5.1	444
20	41.6	5.4	5.1	444
+50	41.7	5.3	5.0	434
21	41.9	5.1	4.8	414 ✓
+50	42.2	4.8	4.5	384 ✓
22	42.6	4.4	4.1	344
+50	43.1	3.9	3.6	294
23	43.8	3.2	2.9	224
T.P.	8.27	253.03 746.04	219	944.76

L

E

E

$$318 / 09$$

$$+0.0$$

$$-0.4 / 30.8$$

$$32.8 / 65$$

$$-0.7$$

$$BT$$

$$5.1$$

$$68 = 61$$

$$334 / -17$$

$$-1.3$$

$$-1.2 / 32.4$$

$$322 / -16$$

$$-1.4$$

$$-1.4 / 32.8$$

$$322 / 11$$

$$-0.7$$

$$BT$$

$$4.5$$

$$4.9 = 61$$

$$320 / -10$$

$$-0.5$$

$$+0.6 / 31.2$$

$$322 / -11$$

$$+0.5$$

$$+2.0 / 34.0$$

$$330 / -1.5$$

$$+0.5$$

$$+1.6 / 33.2$$

S/O	P.G.	P.G.R.	SW-G.R.	B.T.
		953.03 946.04		
23 +50	44.5	8.5	8.2	1.54
T.P	8.28	952.77	1.55	944.49
24	45.3	7.7	7.4	7.48
150	45.8	7.2	6.9	
+50		6.9	6.6	6.2
+70	46.5	6.5	6.2	
25	47.0	6.0	5.7	5.77
+50	47.9	5.1	4.8	4.87
26	48.8	4.2	3.9	3.97
			1.82	950.85
B.M.			2.13	950.90
				(950.95)

K.A. 512-41 R011
A.M.
M.B.
R.K.

L E R

31.2' / -0.6
88

0.0
85

106 / 31.2
76

Gr. 2.5

B.T.
74
30'

10.1
76

B.T.
74
30'

76 Gr.

10.5
84
10.5
84

30.6' / -0.6
84 6.3

10.5
64

10.3 / 30.6
6.3

Gr. = 5.9

B.T.
5.7
30'

10.1
59

B.T.
5.7
30'

56 Gr.

32.8' / -1.4
62

-1.0
61

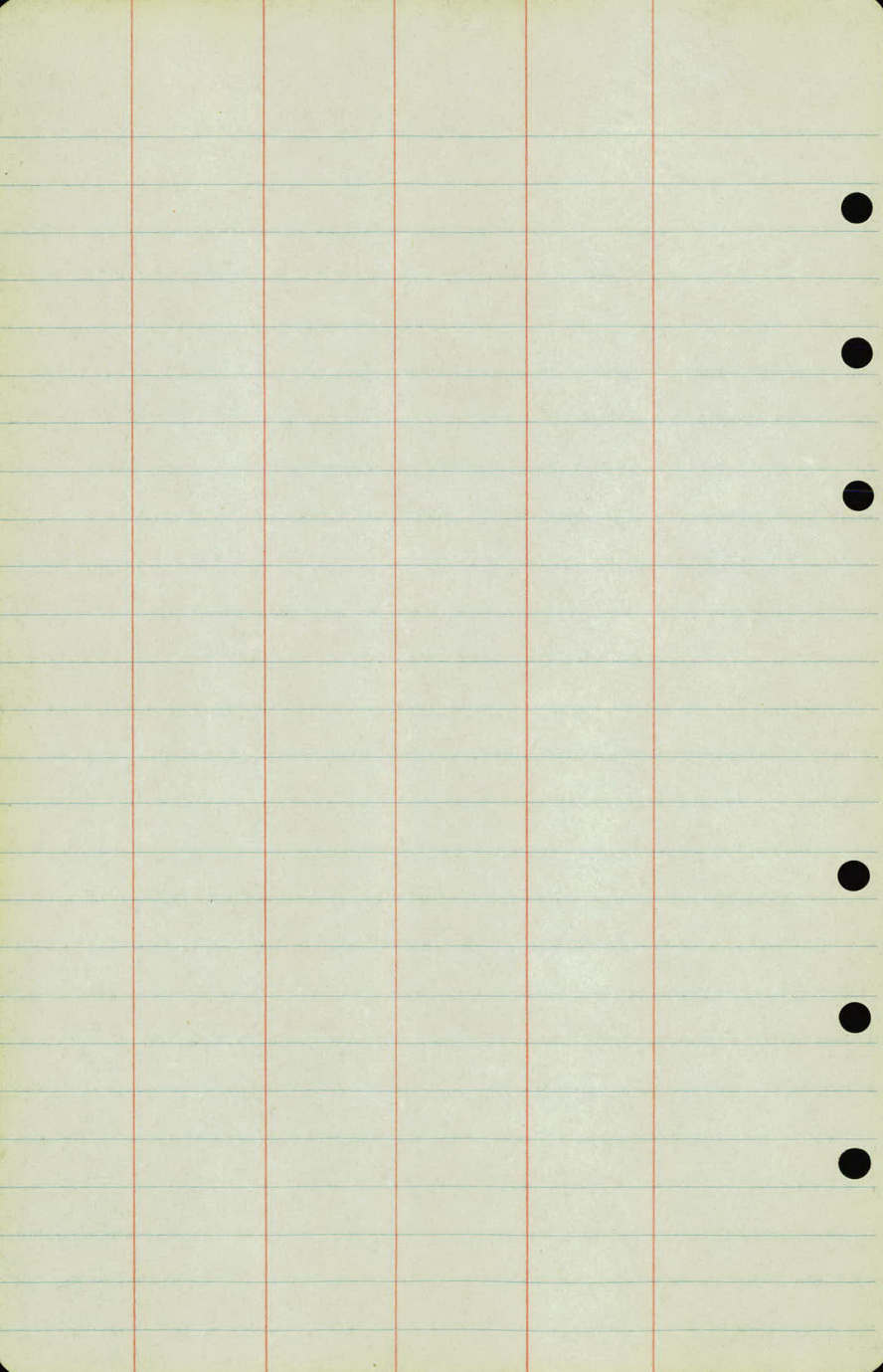
-0.9 / 32.8
57

34.1' / -2.2
61

-2.0
62

-1.8 / 34.1
57 33.6

Spt in 30" 0.100's GORR F" & East Ave



Bellevue

Def-180' Rd.

19.1' Per. Ft.

7+90.19	P.C.	0°00'
8		3°07.4'
+33		13°44'
+66		24°20.6'
9		34°57.2'
+33		45°33.8'
+66		56°10.4'
10		66°47'
+33		77°23.6'
+66		88°00.2'
11		98°36.8'
+33		109°13.4'
+66		119°50'
12		130°26.6'
+30		139°59.6'
+6000	P.T.	149°33'

Bellerive Ave.
Staking Notes

Sta.	P.G.	P.G.R.	S.W.G.R.	B.T.	
B.M.	6.58	950.89			(94421)
	5.66	949.87			
0 +00	44.6	6.3			
+33	44.3	6.6	6.3	5.57	
+60	44.4	6.5	6.2	5.47	2001
1	44.5	6.4	6.1	5.37	* 0.0
+50	44.6	6.3	6.0	5.27	F
2	44.7	6.2	5.9	5.17	F
+50	44.8	6.1	5.8	5.07	F
3	44.9	6.0	5.7	4.97	F

K.A. 5-12-41
A.M.
M.B.
R.F.

L

E

R

R.P. Spk in 30" Elm S.W. Cor. Bellevue & Co. Rd. "F"

31.2/-06
6.9

+0.1
6.5

R.T.
6.3
30

6.5-Gr.

31.0/-05
6.7

-0.1
6.6

R.T.
6.2
30

6.5-Gr.

Gr-6.0

R.T.
6.1
30

+0.3
6.1

R.T.
6.1
30

6.0-Gr.

30.8/+04
56

+0.6
57

+0.4/
56/30.8

30.8/+04
55

+0.7
55

+0.4/
5.5/30.8

31.0/+05
53

+1.1
5.0

+0.7/
5.1/31.4

30.6/+03
54

+0.9
5.1

+0.7/
5.0/31.4

Sta	P.G.	P.G.P.	S.W.G.P.	B.T	
		950.89			
		949.87			
3 +53	45.1	5.8	5.5	4.77	* F0.3
4 +13	45.2	5.7	5.4	4.67	✓
+50	45.3	5.6	5.3	4.57	✓
5	45.4	5.5	5.2	4.47	
+50	45.3	5.6	5.3	4.57	
6	44.7	6.2	5.9	5.17	
+50	43.7	7.2	6.9	6.17	
T.P.	1.49	948.16	4.22	946.67	
42.32	43.5	4.7	4.4	6.37	
T.P.	2.13	945.63	6.37	943.50	

5-12-47

L

Q

R

$$30.8' / 10.4$$

$$10.8$$

$$10.5 / 31.0'$$

$$30.6' / 9.3$$

$$10.2$$

$$\frac{BT.}{5.4}$$

$$Gr = 5.8$$

$$\frac{BT.}{5.3}$$

$$0.0$$

$$\frac{BT.}{5.3}$$

$$5.8 - Gr$$

$$Gr = 5.4$$

$$\frac{BT.}{5.2}$$

$$10.9$$

$$10.2 / 30.4'$$

$$30.4' / 10.2$$

$$11.0$$

$$10.7 / 31.4'$$

$$32.2 / 11.1$$

$$11.8$$

$$10.2 / 20.4'$$

$$35.4 / 12.7$$

$$12.9$$

$$10.8 / 31.6'$$

2x2 Hub of G + 52

$$36.0' / 13.0$$

$$12.7$$

$$11.0 / 22.0'$$

Sta	P.G.	P.G.R.	SW.G.R.
-----	------	--------	---------

		948.16	
--	--	--------	--

		946.63	
--	--	--------	--

7	42.4	5.8	5.5	3.23
---	------	-----	-----	------

+45	40.2	8.0	7.7	5.43
-----	------	-----	-----	------

P.R.C. +90.19	39.9	8.3	8.0	
------------------	------	-----	-----	--

8	39.7	8.5	8.2	5.93
---	------	-----	-----	------

+33	39.0	9.2	8.9	6.63
-----	------	-----	-----	------

+66	38.5	9.7	9.4	7.13
-----	------	-----	-----	------

9	38.0	10.2	9.9	7.63
---	------	------	-----	------

+33	37.6	10.6	10.3	8.03
-----	------	------	------	------

5-13-41 Cold & Windy

L

E

R

35.2 / +26
29

+1.1
47

+2.6 / 29
29.2

37.4 / +3.7
43

+1.7
63

37.0 / +3.5
45

+1.7
66

+0.4 / 76
30.8

37.8 / +3.9
43

+2.1
64

+0.7 / 75
31.4

35.2 / +4.1
48

+2.8
64

+1.0 / 79
32.0

35.8 / +4.4
5.0

+3.2
65

+1.6 / 83
33.2

37.6 / +3.8
6.1

+2.5
7.7

+0.9 / 90
31.8

38.0 / +2.9
7.4

+1.4
9.2

+0.2 / 10.1
30.4

Sta.	P.G.	P.G.R.	S.W.G.R.		
		94816 945.63			
9 +66	37.3	10.9	10.6	8.33	
10	37.0	^{5.6} 11.2	^{1.8} 10.9	8.63	
T.B.M.	317	942.56 945.63	8.76	939.40	(939.39)
+33	36.7	5.9	5.6	8.93	
+66	36.6	6.0	5.7	9.03	
11	36.6	6.0	5.7	9.03	
+33	36.5	6.1	5.8	9.13	
+66	36.5	6.1	5.8	9.13	
12	36.6	6.0	5.7	9.03	

L Φ R

32.2' / +1.1
9.5 +0.2
10.7 -0.6 / 31.2'

32.4' / +1.2
9.7 0.0
11.2 -1.0 / 32.0'

Top Rod. / run

33.0' / +1.5
4.1 -0.3
6.2 -1.0 / 32.0'

33.0' / +1.5
4.2 -0.6
6.6 -1.5 / 32.0'

31.0' / +1.0
5.2 -0.8
6.8 -1.8 / 33.6'

31.4' / -0.7
6.5 -1.4
7.5 -1.5 / 33.6'

33.6' / +1.0
7.6 -1.2
7.3 -1.3 / 32.6'

31.2' / -0.6
6.3 -0.8
6.8 -1.2 / 32.4'

Sta.	P.G.	P.G.P.	SW.G.P.	
		942.56		
		945.63		
12 +30	36.7	5.9	5.6	8.93
P.T. +6002	36.8	5.8	5.5	8.83
13	37.0	5.6	5.3	8.63
+4493	37.4	5.2	4.9	8.23
T.B.M			6.45	939.18
W. Prop Line +6493	37.6	5.0	4.7	
	9.04	944.51		935.47
N Prop Line 14 +2493	38.3	5.7		6.21
+450	38.5	4.1	3.8	6.01
T.P	2.36	944.22	0.90	941.66
+60	38.7			
15	39.2	5.0	4.7	5.3

L

E

R

$$31\frac{1}{2} / +0.6 \\ 5.0$$

$$-0.5 \\ 0.4$$

$$-0.9 / 31.8'$$

$$Gr = 5.6$$

$$B.T. \\ 55 \\ 30$$

$$-0.3 \\ 0.1$$

$$-0.8 / 31.6'$$

$$Gr = 5.6$$

$$B.T. \\ 53 \\ 30$$

$$+0.0 \\ 5.6$$

$$B.T. \\ 53 \\ 30$$

$$5.5 = Gr$$

$$31\frac{1}{2} / +0.6 \\ 4.3$$

$$+0.2 \\ 5.0$$

$$+0.7 / 31.4'$$

150' Rq L Iron

$$30\frac{5}{8} / +0.4 \\ 3.4$$

$$+1.9 \\ 2.2$$

$$+2.7 / 35.4'$$

$$E 5/0.15$$

$$+1.8 \\ 3.2$$

$$+2.7 / 35.4'$$

$$304' / 4.5$$

$$+1.8 \\ 3.2$$

$$+2.7 / 35.4'$$

Sta	PG	P.G.R.	S.W.G.R.		
		94422			
		94407			
13 +40	39.7	4.5	4.2	4.8 ✓	
14 +45	39.9	4.3	4.0	4.6	
16 +14.65	38.8	5.4			
16 +48	36.9	7.3	7.0	7.61 ✓	Rt 0.6°
+70	35.5	8.7	8.4	9.01 ✓	
17	33.9	10.3	10.0	10.61	
+38	32.9	11.3	11.0	11.41	
+50	32.9	11.3	11.0		

L

E

R

Gr=4.5 L BT 4.2 11.8 12.4/
30' 2.7 1.8/34.5

Gr=4.9 BT 4.2 11.4 12.0/
30' 2.9 2.0/34.0

BT
12.7
2.7

32.6' / -1.3 10.2 10.6/
7.0 7.1 6.4/31.2

32.8' / -1.4 9.0 10.6/
9.8 8.7 7.8/31.2

33.2' / -1.6 -0.3 11.0/
11.6 10.6 9.0/32.0

11.6
9.4 / 33.2

33.4' / 1.7 10.2 12.2/
12.7 11.1 8.8/34.4

Sta	PG	PGP	S.W.G.P.
		944.22	

17 + 56	328	11.4	
---------	-----	------	--

161	328	11.4	11.1
-----	-----	------	------

174	328	11.4	11.1	11.71
-----	-----	------	------	-------

186	328	11.4	11.1
-----	-----	------	------

18	327	⁴³ 11.5	⁴⁰ 11.2	11.81
T.P.	474	937.01	11.95	932.27

150	326	4.4	4.1	11.91
-----	-----	-----	-----	-------

19	324	4.6	4.3	12.11
----	-----	-----	-----	-------

150	323	4.7	4.4	12.21
-----	-----	-----	-----	-------

L

E

R

$$\begin{array}{r} +15 \\ 96/33.0 \end{array}$$

$$\begin{array}{r} +12 \\ 98 \end{array}$$

$$\begin{array}{r} +15 \\ 96/33.0 \end{array} \quad 11.5 = 61$$

$$\begin{array}{r} 94.1' / -0.7 \\ 11.8 \end{array}$$

$$\begin{array}{r} +12 \\ 9.9 \end{array}$$

$$\begin{array}{r} BT \\ 11.1 \\ 30' \end{array}$$

$$11.5 = 61$$

$$\begin{array}{r} 32.6' / +1.3 \\ 9.8 \end{array}$$

$$\begin{array}{r} -0.6 \\ 12.0 \end{array}$$

$$\begin{array}{r} -1.0 \\ 12.1/32.0' \end{array}$$

$$\begin{array}{r} 30.2' / +0.1 \\ 11.1 \end{array}$$

$$\begin{array}{r} -0.8 \\ 12.3 \end{array}$$

$$\begin{array}{r} -0.9 \\ 12.1/31.8' \end{array}$$

$$\begin{array}{r} BT \\ 4.1 \\ 30' \end{array}$$

$$\begin{array}{r} -0.7 \\ 5.1 \end{array}$$

$$\begin{array}{r} -0.7 \\ 4.6/31.4' \end{array}$$

$$\begin{array}{r} 30.0' / +1.1 \\ 32 \\ 30' \end{array}$$

$$\begin{array}{r} +0.5 \\ 4.1 \end{array}$$

$$\begin{array}{r} BT \\ 4.3 \\ 30' \end{array}$$

$$4.4 = 61$$

$$\begin{array}{r} 27.0' / +1.3 \\ 31 \end{array}$$

$$\begin{array}{r} +0.4 \\ 4.3 \end{array}$$

$$\begin{array}{r} -0.9 \\ 5.3/31.8' \end{array}$$

Sta	PG	PGR.	S.VGR.
		937.01	

20+00	32.2	4.8	4.5
-------	------	-----	-----

20+35	32.5		
-------	------	--	--

TBM Check

4.54 932.47 o/s

B.M.

1.45 935.56

K.A.
A.M.
M.B.
B.K.

5-13-47

L

E

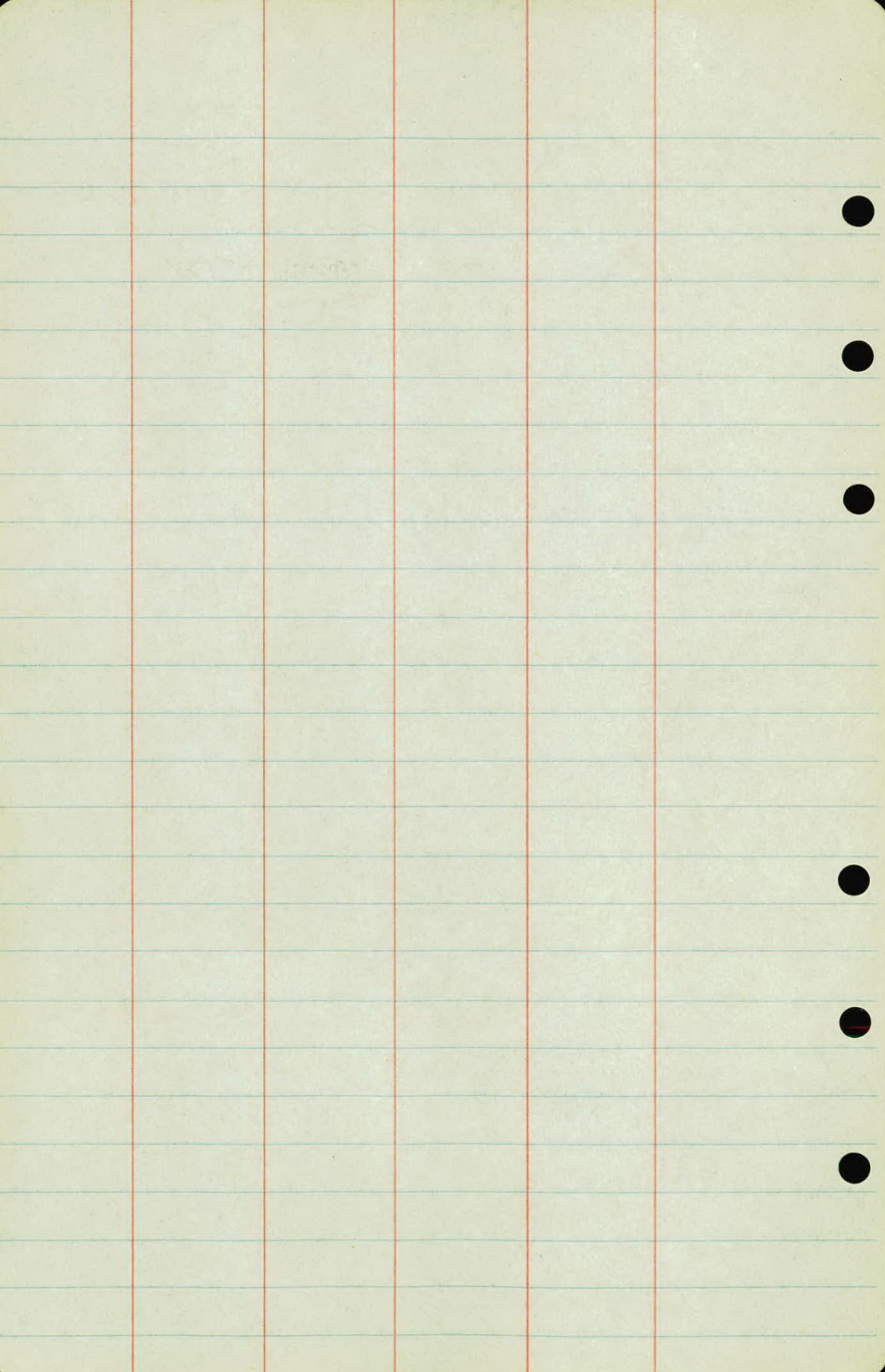
R

230' / 4.5

109
57

-20 / 340'
65

Top R.R. Iron near S.E. cor. Ho.



Gardenette Dr. S.

130' Rod.

19.1' Def. Per. Ft.

8	102.4	P.C.	0°00'
	+33		10°03.6'
	+66		20°40.2'
9			31°16.8'
	+33		41°53.4'
	+66		52°30'
10			63°06.6'
	+40		75°50.6'
	+83.86	P.T.	89°35'±

11

Gardnette Drive So.

stating Notes

Sta.	P.G.	P.G.R.	S.W.G.R.	B.T.
T.B.M.	861	948.00		(939.39)
	162	945.80		939.18
	39.9	81	7.8	
0 +00	940.0	80	7.8	
+50	40.3	7.7	7.4	
+95.38	40.6	7.4	7.1	
1 +15.6	40.7	7.3	7.0	5.1
+50	40.9	7.1	6.8	4.9
2	41.2	6.8	6.5	4.6
+50	41.5	6.5	6.2	4.3
3	41.8	6.2	5.9	4.0

K.A. 5-13-47
A.M.
M.B.
C. Klock

L

E

E

Top 150' Rad. Iron.

30'2" / 101
73

+11
66

+101
73 / 30'2"

B.T.

71
30'

+102
72

Gr = 73

-0.1
71

+109
61 / 31.5'

B.T.

65
30'

+106
65

Gr = 71

+112
56 / 32.4'

31'2" / 106
59

+110
55

+114
51 / 32.5'

30'8" / 104
58

+112
53

+113
49 / 32.6'

31'8" / 109
50

+116
46

+113
46 / 32.6'

Sta P.G. P.G.R. SW.G.R.

948.00

945.90

3 +50 42.1 5.9 5.6 3.7

4 42.4 5.6 5.3 3.4

+50 42.8 11.2 10.9 3.0
5.2 4.9

5 43.3 4.7 4.4 2.5

T.P. 1040 954.00 440 943.60

9.69 952.97 2.52 943.28

+50 44.0 10.0 9.7 8.97

6 44.9 9.1 8.8 8.07

+50 45.3 8.2 7.9 7.17

7 46.7 7.3 7.0 6.97

L

E

R

$$31.6' / \begin{matrix} +0.5 \\ 48 \end{matrix}$$

$$\begin{matrix} +1.4 \\ 45 \end{matrix}$$

$$\begin{matrix} +1.4 \\ 42/32.6' \end{matrix}$$

$$30.6' / \begin{matrix} +0.4 \\ 49 \end{matrix}$$

$$\begin{matrix} +0.9 \\ 47 \end{matrix}$$

$$\begin{matrix} +0.8 \\ 45/31.6' \end{matrix}$$

Gr=51

$$\begin{matrix} B.T. \\ 4.9 \\ 30' \end{matrix}$$

$$\begin{matrix} +0.2 \\ 50 \end{matrix}$$

$$\begin{matrix} B.T. \\ 4.9 \\ 30' \end{matrix}$$

51=Gr.

Gr=48

$$\begin{matrix} B.T. \\ 4.4 \\ 30' \end{matrix}$$

$$\begin{matrix} -0.2 \\ 49 \end{matrix}$$

$$\begin{matrix} B.T. \\ 4.4 \\ 30' \end{matrix}$$

47=Gr.

Top Blue Top of sta. 5

Gr=102

$$\begin{matrix} B.T. \\ 9.7 \\ 30' \end{matrix}$$

$$\begin{matrix} +0.1 \\ 99 \end{matrix}$$

$$\begin{matrix} +0.2 \\ 9.5/30.4' \end{matrix}$$

Gr=95

$$\begin{matrix} B.T. \\ 8.8 \\ 30' \end{matrix}$$

$$\begin{matrix} +1.0 \\ 81 \end{matrix}$$

$$\begin{matrix} +1.6 \\ 7.2/33.2' \end{matrix}$$

$$31.0' / \begin{matrix} +0.5 \\ 7.4 \end{matrix}$$

$$\begin{matrix} +2.8 \\ 5.4 \end{matrix}$$

$$\begin{matrix} +3.1 \\ 4.8/36.2' \end{matrix}$$

$$35.2' / \begin{matrix} +2.6 \\ 4.4 \end{matrix}$$

$$\begin{matrix} +4.1 \\ 3.2 \end{matrix}$$

$$\begin{matrix} +3.3 \\ 3.7/36.6' \end{matrix}$$

Sta	P.G.	P.G.C.	S.W.G.R.	
		954.00		
		952.97		
7 +50	47.8	6.2	5.9	5.17

8	48.6	5.4	5.1	4.37
---	------	-----	-----	------

P.G. +02.4	48.6			
---------------	------	--	--	--

+33	49.2	4.8	4.5	3.77
-----	------	-----	-----	------

+66	49.8	4.2	3.9	3.17
-----	------	-----	-----	------

9	50.4	3.6	3.3	2.57
---	------	-----	-----	------

+33	51.0	3.0	2.7	1.97
-----	------	-----	-----	------

+66	51.5	2.5	2.2	1.47
T.P	6.97	958.47	1.47	951.50

5-15-47

L

E

R

$$84.0 / 12.0 \\ 3.9$$

$$12.0 \\ 3.2$$

$$11.6 / 4.3 / 33.2'$$

$$Gr = 5.7$$

$$B.T. \\ 31 \\ 30'$$

$$-0.9 \\ 6.5$$

$$-1.2 / 7.3 / 32.4'$$

$$31.8 / -0.9 \\ 4.6$$

$$-1.5 \\ 6.3$$

$$-1.5 / 7.0 / 33.0'$$

$$Gr = 4.2$$

$$B.T. \\ 39 \\ 30'$$

$$-0.5 \\ 4.7$$

$$-1.1 / 5.0 / 32.2'$$

$$Gr = 3.5$$

$$B.T. \\ 3.3 \\ 30'$$

$$-0.8 \\ 4.4$$

$$-1.7 / 5.0 / 33.4'$$

$$Gr = 3.4$$

$$B.T. \\ 27 \\ 30'$$

$$-0.9 \\ 3.9$$

$$-2.1 / 4.8 / 34.2'$$

$$Gr = 2.8$$

$$B.T. \\ 22 \\ 30'$$

$$-1.0 \\ 3.5$$

$$-1.4 / 3.6 / 32.8'$$

Sto.	PG	PG.R	S.W.G.R	
		954.00		
		95847		
10	52.2	1.8	1.5	6.27
T.P.	6.35	958.84	1.51	952.49
		95847		
+40	52.7	6.1	5.8	5.77
P.T. +8386	53.2	5.6	5.3	5.27
11	53.9	5.5	5.2	5.17
+50	53.6	5.2	4.9	4.87
12	53.8	5.0	4.7	4.67
+1386	53.9	4.9	4.6	4.57
+386	54.0	4.8	4.5	4.47

L

C

R.

Gr = 2.1

$$\begin{array}{r} \text{B.T.} \\ 15 \\ \hline 30 \end{array}$$

10.1

1.7

$$\begin{array}{r} 10.8 \\ 2.3 \\ \hline 31.6 \end{array}$$

$$\begin{array}{r} 30.2' \\ 10.1 \\ \hline 57 \end{array}$$

11.4

4.7

$$\begin{array}{r} 10.8 \\ 5.0 \\ \hline 31.6 \end{array}$$

$$\begin{array}{r} 31.0' \\ 10.5 \\ \hline 4.8 \end{array}$$

11.7

3.9

$$\begin{array}{r} 12.1 \\ 3.2 \\ \hline 34.2 \end{array}$$

$$\begin{array}{r} 31.0' \\ 10.5 \\ \hline 4.7 \end{array}$$

11.4

4.1

$$\begin{array}{r} 11.8 \\ 3.4 \\ \hline 33.6 \end{array}$$

$$\begin{array}{r} \text{B.T.} \\ 19 \\ \hline 30 \end{array}$$

Gr = 2.1

10.4

4.8

$$\begin{array}{r} 10.8 \\ 4.1 \\ \hline 31.6 \end{array}$$

$$\begin{array}{r} 30.2' \\ 10.1 \\ \hline 4.6 \end{array}$$

11.3

3.7

$$\begin{array}{r} 11.2 \\ 4.1 \\ \hline 32.2 \end{array}$$

$$\begin{array}{r} 31.6' \\ 10.8 \\ \hline 3.8 \end{array}$$

11.5

3.3

$$\begin{array}{r} 11.4 \\ 3.1 \\ \hline 32.8 \end{array}$$

Sta. PG. PGR S.WGR

95884

95847

13 +13.86 53.9 4.9 4.6 457

150 53.5 5.3 5.0 497

14 52.8 6.0 5.7 567

+13432 52.3 6.5 6.2 617

B.M. 896 949.88 (94994)

146
34
587
430
4964

K.A.
A.M.
M.B.
E.K.

5-15-41

L

E

F

Gr. = 52

B.T.
46
30

10.4
45

105
41/30

32.4 / 1.2
6.2

10.3
36

B.T.
5.0
30

53-61

Gr. = 63

B.T.
5.7
30

10.5
35

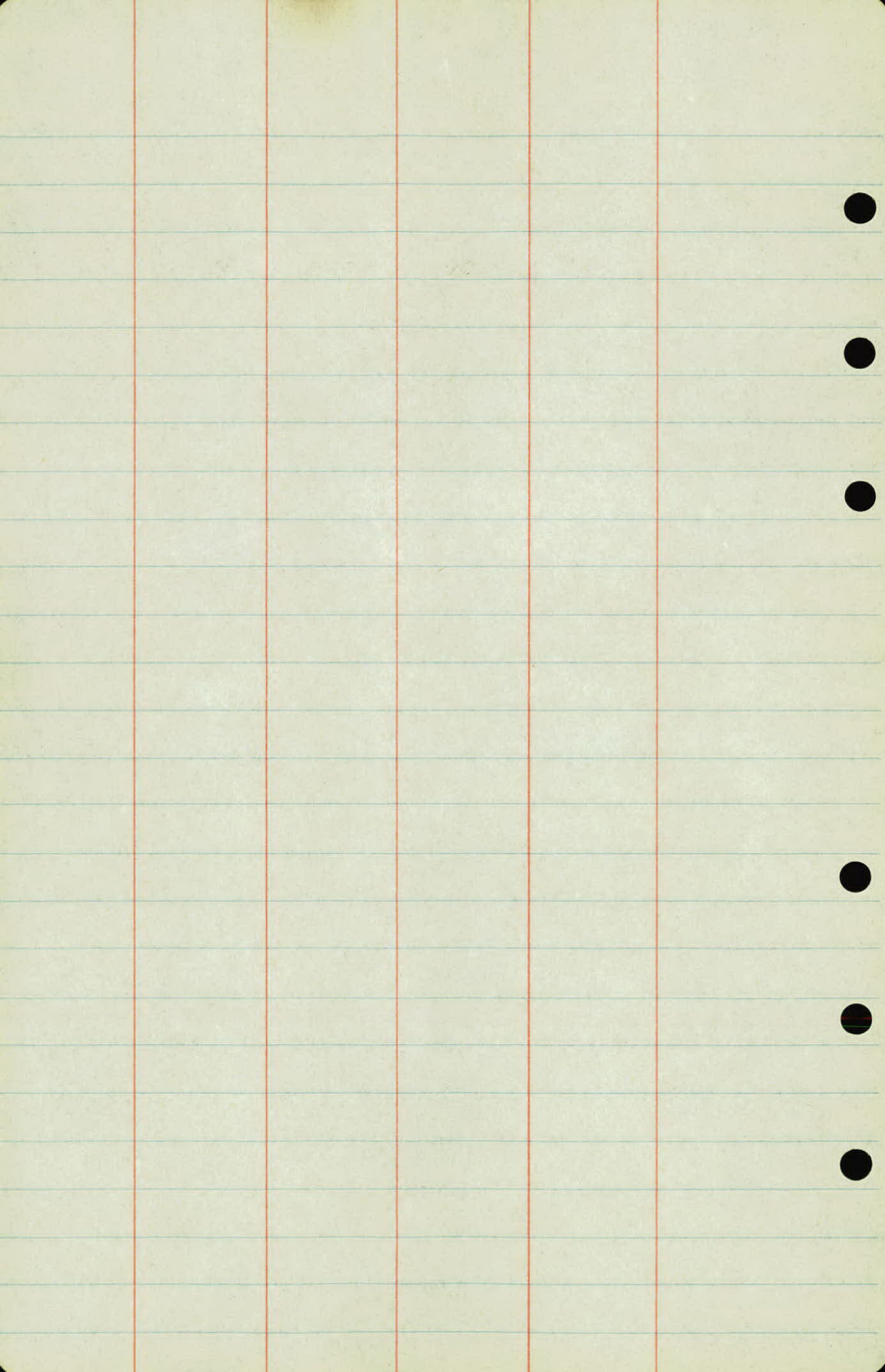
10.8
4.9/31.6

33.4 / 4.7
45

12.6
39

12.1
4.1/34.2

R.R. Spt. in 8" Elm N. of East Av. & So Shore Dr.



Gardenette Drive No.

Staking Notes

Sto.	P.G.	P.G.B.	SW.G.C.	
B.M.	573	941.20		
T.R.	9.10	947.88	2.42	938.78
0 +00	37.9	10.0	9.7	9.00
	6.70	945.88		939.18
+50	39.3	8.6	8.3	6.6 v
1	40.4	7.5	7.2	5.50 v
+50	40.9	7.0	6.7	5.00 v
2	41.1	6.8	6.5	4.8 v
+50	41.3	6.6	6.3	4.6 v
3	41.5	6.4	6.1	4.4 v
+50	41.7	6.2	5.9	4.2 v

(935.47)

K.A. 5-15-41
 A.M.
 M.B.
 E.K.

2 Pcs at 0100 Lilac Lane.

+0.9
 91

+1.8 / 33.6'
 7.9 / 33.6'

Top Rad Iron

344' / +2.2
 6.1

+1.4
 7.4

+2.4 / 348'
 5.9 / 348'

328' / +1.4
 5.8

+1.3
 6.2

+1.7 / 324'
 5.5 / 324'

330' / +1.3
 5.2

+1.3
 5.7

+2.2 / 344'
 4.5 / 344'

342' / +2.1
 4.4

+1.7
 5.1

+2.1 / 342'
 4.4 / 342'

328' / +1.4
 4.9

+1.0
 5.6

+1.0 / 320'
 5.3 / 320'

320' / +1.0
 5.1

+0.9
 5.5

+0.7 / 314'
 5.4 / 314'

312' / +0.6
 5.9

+0.9
 5.3

+1.2 / 324'
 4.7 / 324'

				26	
Sta	P.G.	P.G.R.	S.W.G.R.		
		947.88			
		946.88			
		14.6	14.3		
4	41.9	6.0	5.7	4.0 ✓	
T.P.	11.86	956.49	3.25	944.63	
		946.88			
+50	42.7	13.8	13.5	3.2 ✓	
5	44.6	11.9	11.6	1.3 ✓	
+19	45.6	10.9	10.6	0.3	
T.P.	9.14	954.74	0.28	945.60	
+60	47.6	8.9	8.6	7.14	
6	49.6	6.9	6.6	5.14	
+50	51.7	4.8	4.5	3.04	
7	53.1	3.4	3.1	1.64	
B.M.	6.59	956.53	6.59	949.90	(949.94)
B.M.			5.63	950.90	

L

E

R

31.6/40.5
4.911.2
4.612.0/34.0
3.7Gr. $\rightarrow$ $\frac{B.T.}{135}$
30'10.6
13.211.2/32.4
12.3

Gr. = 12.1

B.T.
116
30'10.4
11.511.2/32.4
10.9

Gr. = 10.8

B.T.
106
30'10.8
10.112.2/34.4
8.9

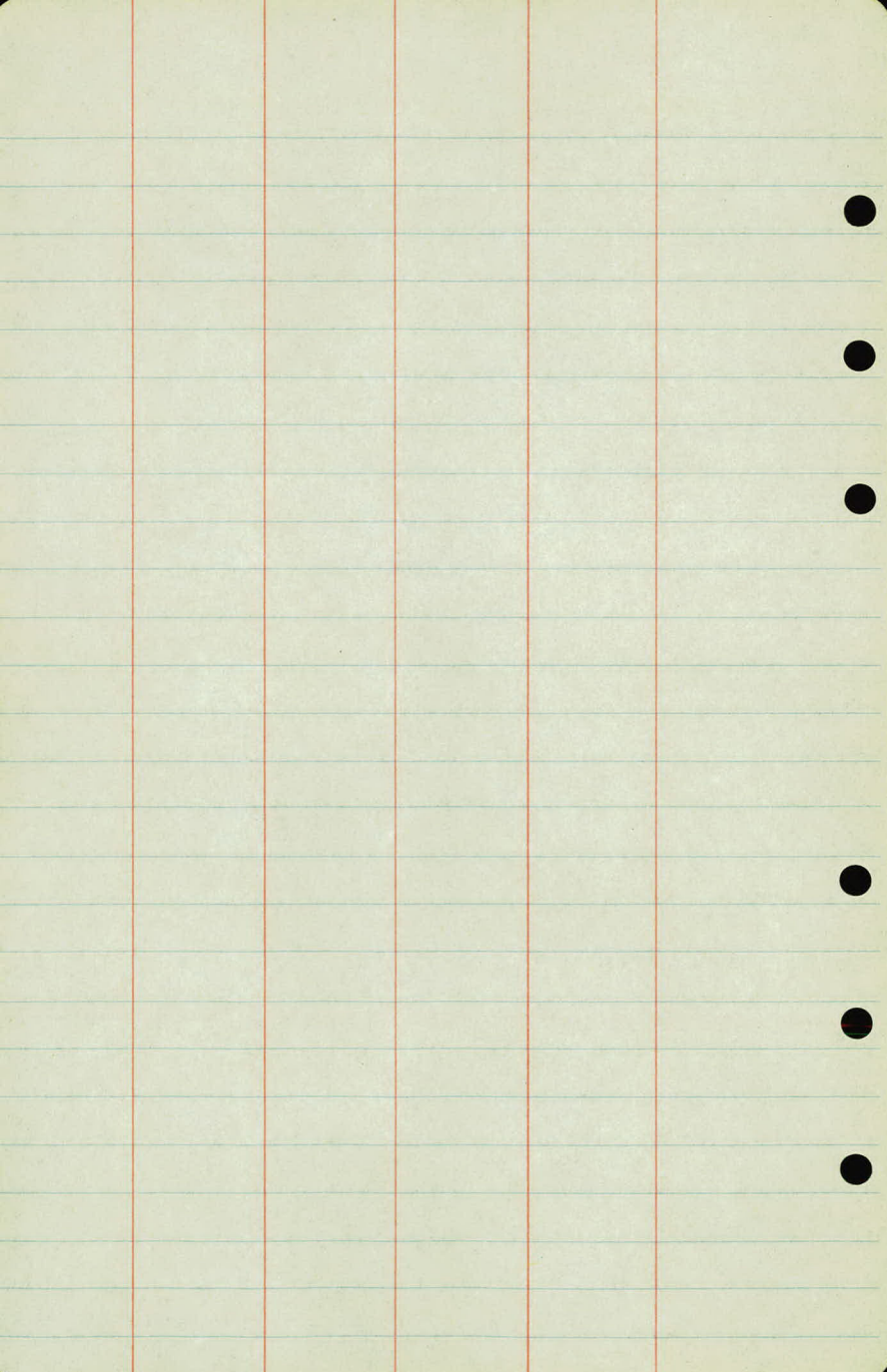
Gr. = 9.2

B.T.
86
30'10.9
8.011.9/33.5
6.7

Gr. = 6.7

B.T.
66
30'11.3
5.612.0/34.0
4.631.8/40.9
3.612.1
2.712.1/34.2
2.431.2/40.6
2.512.0
1.412.1/34.0
1.0

R.R. Spk in 8' Elm N of East Ave & So. Shore Blvd.
 Spk. 10 16" E/W S.E. of V. road. Barn S.W. of Liloa Lane &



Lilac Lane

Staking Notes

Sta	PG	P.G.R	S.W.G.R.
-----	----	-------	----------

BM.	615	941.62	
-----	-----	--------	--

(93547)

0 +00	3547		
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+14	3594		
-----	------	--	--

+30	359		
-----	-----	--	--

+50	358		
-----	-----	--	--

+70	358		
-----	-----	--	--

+82	357	5.9	5.6
-----	-----	-----	-----

1	357	5.9	5.6
---	-----	-----	-----

+50	356	6.0	5.7
-----	-----	-----	-----

Lilac

L

E

E

E Par sta 0100

$$\begin{array}{r} 300 \cancel{0} / 100 + 06 \quad 10.9' \\ 36 \quad 0 \quad 90 \end{array}$$

$$\begin{array}{r} 106 \\ 50 \overline{) 542} \end{array}$$

$$\begin{array}{r} 300 \cancel{0} / 120 + 12 \quad 11.7' \\ 36 \quad 0 \quad 44 \end{array}$$

$$\begin{array}{r} 101 \\ 55 \overline{) 552} \end{array}$$

$$\begin{array}{r} 300 \cancel{0} / 118 + 11.3' \\ 34 \quad 0 \quad 44 \end{array}$$

$$\begin{array}{r} 103 \\ 54 \overline{) 556} \end{array}$$

100 = 30' Lt.

Sta.	P.G.	P.G.R.	SW.G.R.	
		941.62		
		5.0	5.1	
2	354	6.2	5.9	
B.M.	5.35	940.82	6.15	935.47
+45	353	5.5	5.2	
+80	352	5.6	5.3	
3	351	5.7	5.4	
+35	350	5.8	5.5	
+65	350	5.8	5.5	
4	351	5.7	5.4	
+50	356	12.5 5.2	12.2 4.9	
T.P.	8.08	948.06	0.84	939.98

5-16-47

L1106

L

E

F

$$\begin{array}{r}
 300 \cancel{0} \times 11.8 \quad +1.0 \quad 11.9 \\
 \underline{46} \quad 0 \quad 49
 \end{array}$$

$$\begin{array}{r}
 11.0 \\
 49 \cancel{0} / 350
 \end{array}$$

$$\begin{array}{r}
 30 \cancel{0} \times 12.1 \quad +1.5 \quad 12.6 \\
 \underline{31} \quad 00 \quad 37
 \end{array}$$

$$\begin{array}{r}
 11.0 \\
 42 \cancel{0} / 35.0
 \end{array}$$

$$\begin{array}{r}
 300 \cancel{0} \times 1.5 \quad +0.5 \quad 10.6 \\
 \underline{08} \quad 0 \quad 50
 \end{array}$$

$$\begin{array}{r}
 8T \\
 \underline{53} \\
 37
 \end{array}$$

59 = 61

$$\begin{array}{r}
 30.0 \cancel{0} \times 10.5 \quad -0.4 \quad 10.1 \\
 \underline{49} \quad 00 \quad 48
 \end{array}$$

$$\begin{array}{r}
 -1.7 \\
 71 \cancel{0} / 36.4
 \end{array}$$

$$\begin{array}{r}
 35.8 \cancel{0} \times 1.9 \quad -2.0 \quad -1.2 \\
 \underline{69} \quad 0 \quad 76
 \end{array}$$

$$\begin{array}{r}
 -2.4 \\
 7.9 \cancel{0} / 37.6
 \end{array}$$

$$\begin{array}{r}
 39.0 \cancel{0} \times 3.0 \quad -2.2 \quad 1.8 \\
 \underline{45} \quad 0 \quad 17
 \end{array}$$

$$\begin{array}{r}
 -2.1 \\
 7.6 \cancel{0} / 37.2
 \end{array}$$

$$\begin{array}{r}
 39.4 \cancel{0} \times 2.2 \quad -1.6 \quad -1.3 \\
 \underline{66} \quad 0 \quad 70
 \end{array}$$

$$\begin{array}{r}
 -1.0 \\
 6.4 \cancel{0} / 35.0
 \end{array}$$

$$\begin{array}{r}
 39.8 \cancel{0} \times 1.34 \\
 \underline{83}
 \end{array}$$

$$\begin{array}{r}
 +0.1 \\
 51
 \end{array}$$

$$\begin{array}{r}
 8T \\
 \underline{49} \\
 33
 \end{array}$$

Sta	P.G.	P.G.R.	-	Elev.
		948.06		
5	366	11.5	11.2	
+209	371	11.0	107	
+70.9	387	9.4	91	
B.M.	10.8v	946.29		935.47
6 +209	404	7.7	7.4	5.9
+60	417	6.4	6.1	4.6
7	430	5.1	4.8	3.3
+36	442	4.1	3.8	
+70	446	3.5	3.2	

L1106

L

E

R

376' / -2.3
19.5

11.0
10.5

10.9
10.9 / 33.6

372' / -2.1
12.8

11.6
9.4

11.0
9.7 / 35.0

376' / -2.3
9.7

11.4
6.3

11.3
6.1 / 35.6

366' / -1.8
7.9

10.8
5.6

10.5
5.6 / 34.0

376' / -0.8
5.6

10.6
4.5

10.5
4.3 / 34.0

Gr=4.1

BT
3.8
3.0

11.0
3.1

10.9
2.9 / 34.0

448' / -5.9
9.1

11.5
2.0

12.4
0.8 / 37.8

Sta	P.G	P.G.R.	S.W.G.R.	
		94806		
8	44.8	3.3	3.0	
+40	45.0	3.1	2.8	
+64	45.1	3.0	2.7	
+84	45.2	2.9	2.6	
9	45.2	7.5 2.9	7.2 2.6	
T.P.	7.36	952.66	2.76	945.30
+128	45.4	7.3	7.0	
+148	45.5	7.2	6.9	
+180	45.6	7.1	6.8	

L1106

L

E

R

45.0' / -6.0
9.0

11.9
14

12.0' / 37.0'
1.0

38.2' / 2.6
5.4

10.1
30

10.1' / 34.4'
2.1

36.6' / -1.5
4.5

-3.5
6.5

B.T.
27
33

35.0' / -1.4
4.0

-4.6
7.5

-0.8
3.4 / 34.6'

35.0' / -1.2
3.8

-4.6
7.5

-1.2
3.8 / 35.4'

35.4' / -1.2
8.2

-4.3
11.6

-1.9
8.9 / 36.3'

35.2' / -1.1
8.0

-3.0
10.2

-3.1
10.0 / 37.0'

B.T.
6.8
35'

-2.5
9.6

-3.4
10.2 / 37.5'

Gr=73

Sto	P.G.	P.G.R.	SW.G.R.	Elev.
		952.66		
10	45.7	7.0	6.7	
+37	45.8	6.9	6.6	
+68	46.0	6.7	6.4	
11	46.4	6.8	6.0	
+50	47.3	^{14.4} 5.4	5.1	
T.P.	10.51	961.70	1.47	951.19
12	48.6	13.1	12.8	
+50	49.8	11.9	11.6	
+71.7	50.3	11.4	11.1	

2/100

L

E

R

Gr=7.2

BT
67
35

-0.4
74

-3.2
9.9/374

Gr=7.3

BT
66
33

-0.1
70

-2.8
9.4/386

Gr=6.5

BT
64
33

-0.2
69

-2.2
8.6/374

Gr=6.1

BT
60
33

+0.1
62

-1.2
7.2/354

94.6/403
43

+1.1
43

320/120
108

+1.8
11.3

+1.8
11.8/366

96.8/11.7
9.9

+2.1
9.8

+2.4
9.2/376

368/11.9
9.2

+2.6
8.8

+3.0
8.0/392

Sta	P.G.	P.G.R.	S.W.G.R.
		961.70	

13	+21.74	51.5	102	9.9
----	--------	------	-----	-----

	+71.7	52.4	9.3	9.0
--	-------	------	-----	-----

14		53.0	87	8.4
----	--	------	----	-----

	+20	53.4	83	8.0
--	-----	------	----	-----

	+50	54.0	77	7.4
--	-----	------	----	-----

	+62	54.2	75	7.2
--	-----	------	----	-----

15		54.9	6.8	6.5
----	--	------	-----	-----

	+30	55.4	63	6.0
--	-----	------	----	-----

	+70	55.6	6.1	5.8
--	-----	------	-----	-----

21100

L

E

R

$$36.4' / 11.7$$

$$13.4$$

$$6.8$$

$$\begin{array}{r} 8.7 \\ 90 \\ \hline 33 \end{array}$$

$$\begin{array}{r} 12.0 \\ 73 \end{array}$$

$$\begin{array}{r} 12.6 \\ 4.4 / 38.2' \end{array}$$

$$Gr = 9.1$$

$$\begin{array}{r} 8.7 \\ 8.4 \\ \hline 33 \end{array}$$

$$\begin{array}{r} 10.9 \\ 78 \end{array}$$

$$\begin{array}{r} 11.4 \\ 7.0 / 35.0' \end{array}$$

$$34.4' / 10.7$$

$$\begin{array}{r} 10.7 \\ 70 \end{array}$$

$$\begin{array}{r} 10.4 \\ 70 / 33.0' \end{array}$$

$$36.8' / 11.9$$

$$\begin{array}{r} 12.0 \\ 4.8 \end{array}$$

$$\begin{array}{r} 10.7 \\ 5.8 / 34.4' \end{array}$$

$$37.2' / 12.1$$

$$\begin{array}{r} 12.8 \\ 3.5 \end{array}$$

$$\begin{array}{r} 10.9 \\ 5.1 / 34.8' \end{array}$$

$$36.8' / 11.9$$

$$\begin{array}{r} 12.2 \\ 2.9 \end{array}$$

$$\begin{array}{r} 11.4 \\ 4.4 / 35.8' \end{array}$$

Sta	R.G.	P.G.R.	S.W.G.R.
		961.70	

16	55.6	6.1	5.8
----	------	-----	-----

+21	55.5	6.2	5.9
-----	------	-----	-----

+35	55.4	6.3	6.0
-----	------	-----	-----

+56	55.3		
-----	------	--	--

+70	55.2	6.5	6.2
-----	------	-----	-----

B.M.		11.76	949.94	(949.94)
------	--	-------	--------	----------

K.A. 5-16-47
A.M.
M.B.
R.F.

L1106

L

E

R

35.6' / 4.3
4.5

12.9
32

41.7 / 36.4'
4.1

33.2' / 10.1
5.9

4.3
5.0

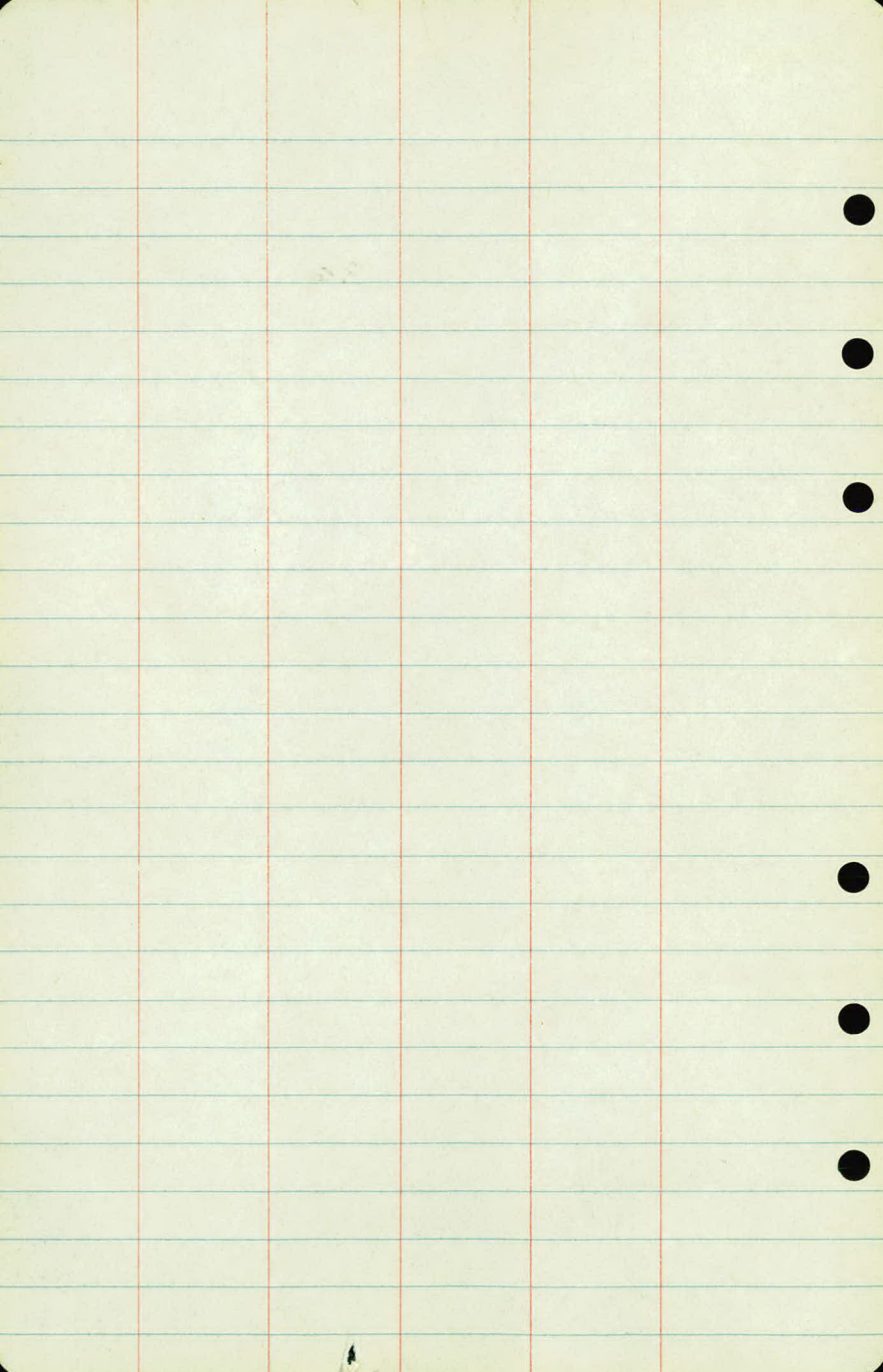
41.5 / 36.0'
4.5

36.2' / 16
7.8

-0.1
66

41.3 / 35.6'
4.9

RR-Spk. in 8" Elm N. of So. Shore Bnd & East Ave.



EAST AVE.

Staking Notes.

Sta	P.G.	P.G.R	-	Elev.
B.M.	300	953.95		950.95

0	100	50.9	3.1
---	-----	------	-----

+53	50.2	3.8
-----	------	-----

1	50.1	3.9
---	------	-----

+50	49.9	4.1
-----	------	-----

2	49.8	4.2
---	------	-----

+50	49.7	4.3
-----	------	-----

3	49.6	4.4
---	------	-----

+33	49.5	4.5
-----	------	-----

K.A. 5-19-41
A.M.
M.B.
E.K.

L

E

R

R.B. Spt in 24" oak 100' S W of F & East Ave.

16.3 / -1.6
54

-1.5
53

-0.9 / 2
47 / 14.2

20.5 / -3.0
69

-2.5
64

-1.8 / 16.3
55

14.2 / -0.8
56

-1.0
51

-1.1 / 14.8
52

16.9 / 10.8
34

10.9
33

11.4 / 16.5
28

16.0 / 10.5
38

11.2
31

12.0 / 16.5
23

12.7 / -0.4
58

10.2
42

11.9 / 16.5
25

16.0 / -1.5
60

-0.6
51

11.1 / 16.5
34

Sta	t	π	-	Elev
		953.95		
3	+83	49.5	4.5	
4	+33	50.1	3.9	
	+60	50.7	3.3	
5		52.0	2.0	
T.P.	10.95	961.92	2.95	950.97
	+50	54.0	7.9	
6		55.8	6.1	
	+40	56.3	5.6	
	+72	56.2	5.7	

L

E

R

49.2

$$\begin{array}{r} -0.8 \\ 5.3/19.9 \end{array}$$

$$\begin{array}{r} 19.3/2.6 \\ 6.5 \end{array}$$

$$\begin{array}{r} -2.0 \\ 5.9 \end{array}$$

$$\begin{array}{r} -1.2 \\ 5.1/15.1 \end{array}$$

$$\begin{array}{r} 19.9/-2.8 \\ 6.1 \end{array}$$

$$\begin{array}{r} -2.2 \\ 5.5 \end{array}$$

$$\begin{array}{r} -1.5 \\ 4.8/16.0 \end{array}$$

$$\begin{array}{r} 17.5/-2.0 \\ 4.0 \end{array}$$

$$\begin{array}{r} -1.6 \\ 5.6 \end{array}$$

$$\begin{array}{r} -1.0 \\ 3.0/14.5 \end{array}$$

$$\begin{array}{r} 14.5/-1.0 \\ 8.9 \end{array}$$

$$\begin{array}{r} 0.0 \\ 7.9 \end{array}$$

$$\begin{array}{r} 11.3 \\ 6.6/16.5 \end{array}$$

$$\begin{array}{r} 14.8/-1.1 \\ 7.2 \end{array}$$

$$\begin{array}{r} -0.3 \\ 6.4 \end{array}$$

$$\begin{array}{r} 11.5 \\ 4.6/16.5 \end{array}$$

$$\begin{array}{r} 17.5/11.0 \\ 4.6 \end{array}$$

$$\begin{array}{r} 11.3 \\ 4.3 \end{array}$$

$$\begin{array}{r} 12.9 \\ 2.7/16.5 \end{array}$$

$$\begin{array}{r} 19.0/11.5 \\ 3.2 \end{array}$$

$$\begin{array}{r} 13.1 \\ 2.6 \end{array}$$

$$\begin{array}{r} 14.4 \\ 1.3/16.5 \end{array}$$

Sta.	P.G.	P.G.R.	-	Elev.
		961.92		

7	56.2	57		
---	------	----	--	--

+25	56.1	58		
-----	------	----	--	--

+60	56.1	58		
-----	------	----	--	--

8	56.0	59		
---	------	----	--	--

+50	55.9	60		
-----	------	----	--	--

9	55.8	61		
---	------	----	--	--

+50	55.7	6.6 6.2		
-----	------	------------	--	--

T.P.	7.13	962.33	6.72	955.20
------	------	--------	------	--------

10	55.6	6.7		
----	------	-----	--	--

L

E

R

199' / +1.8
39131
26+4.5
1.2 / 16.5'157' / -14
6.2+1.2
46+2.8
3.0 / 16.5'206' / -3.1
89-2.2
80-1.3
7.5 / 16.0253' / -4.6
10.5-4.0
99-3.4
9.5 / 16.5'238' / -4.1
10.1-4.1
10.1-3.7
9.7 / 16.5'230' / -3.0
9.1-3.1
9.2-2.7
8.9 / 16.5'190' / -2.3
8.7-2.0
8.2-1.6
7.8 / 16.5'172' / -1.9
8.6-1.3
8.0-1.8
7.5 / 16.5'

Sta.	P.G.	P.G.R.	-	Elev.
------	------	--------	---	-------

962.33

10	+26	556	6.7	
----	-----	-----	-----	--

+38	555			
-----	-----	--	--	--

+51	555	6.8		
-----	-----	-----	--	--

+71	555	6.8		
-----	-----	-----	--	--

11	554	6.9		
----	-----	-----	--	--

+50	553	7.0		
-----	-----	-----	--	--

12	552	7.1		
----	-----	-----	--	--

+50	551	7.2		
-----	-----	-----	--	--

L

E

R

14.0 / -1.1
2.8-1.3
80-0.8
75 / 13914.5 / -1.0
78-1.2
80-3.5
103-0.3
7110.9
60 / 16515.4 / 10.3
6610.9
6012.4
4518.4 / 11.3
5711.4
4612.9
31 / 16520.8 / 12.8
5012.1
4013.8
33 / 16520.5 / 12.0
5212.1
5112.8
44 / 165

Sta	P.G.	P.G.R.	-	Elev.
		962.33		

12 + 74	55.1	7.2		
---------	------	-----	--	--

13 + 2394	55.0	7.3		
-----------	------	-----	--	--

+ 7394	54.8	7.5		
--------	------	-----	--	--

14	54.8	7.5		
----	------	-----	--	--

+ 22	54.8	7.5		
------	------	-----	--	--

+ 70	54.7	7.6		
------	------	-----	--	--

T.P.	365	962.89	3.09	959.24
------	-----	--------	------	--------

15	54.7	8.2		
----	------	-----	--	--

+ 35	54.6	8.3		
------	------	-----	--	--

L

E

R

193' / +16
54+1.6
56+2.3 / 16.5'
49+0.8 / 16.5'
65175' / -2.0
95-2.1
96-1.5 / 16.0'
90193' / +2.6
104-2.8
103-2.9 / 16.5'
104181' / -2.4
99-2.6
101-2.8 / 16.5'
103181' / +1.2
64+1.0
66+1.2 / 16.5'
64241' / +3.2
5.0+3.3
49+3.7 / 16.5'
45301' / +5.2
31+5.5
28+6.3 / 16.5'
20

Sta	P.G.	P.C.R.	-	Elev.
		962.89		
		82		
15 +70	54.5	84		
B.M.	12.77	962.71	12.95	949.94 (949.94)
16	53.9	8.8		
+50	51.8	10.9		
+76	50.5	12.2		
17 +063	49.7	13.0		
B.M.			12.70	949.93

12.77

10150	4.4	4.9
11	4.5	5.0
150	4.6	5.1
12	4.7	5.2
150	4.8	5.3
174	4.8	5.3
13124	4.9	5.4
174	5.1	5.6
14	5.1	5.6
127	5.1	5.6
190	5.2	5.7
15	5.2	5.7
135	5.3	5.8
170	5.4	5.9
16	6.0	6.5
150	5.4	5.9
176	9.4	9.9
171063	10.2	

955.10
 + 4.77

 H.I. = 959.87
 9.95

 969.82

59.9

~~10 5.3 5.8~~
~~9 5.1 5.5~~
~~8 4.9 5.4~~
~~7 4.7 5.2~~
~~6 5.1 5.6~~
~~5 4.6 5.1~~
~~4 4.3 4.8~~
~~3 4.1 4.6~~
~~2 3.8 4.3~~
~~1 3.5 4.0~~
~~0.5 3.2 3.7~~
~~10 5.3 5.8~~
~~9 5.1 5.5~~
~~8 4.9 5.4~~
~~7 4.7 5.2~~
~~6 5.1 5.6~~
~~5 4.6 5.1~~
~~4 4.3 4.8~~
~~3 4.1 4.6~~
~~2 3.8 4.3~~
~~1 3.5 4.0~~
~~0.5 3.2 3.7~~

3.M. 950.95
 + 3.60
 954.55
 - 1.06
 953.49
 + 7.39
 960.88
 5.78
 955.10

L

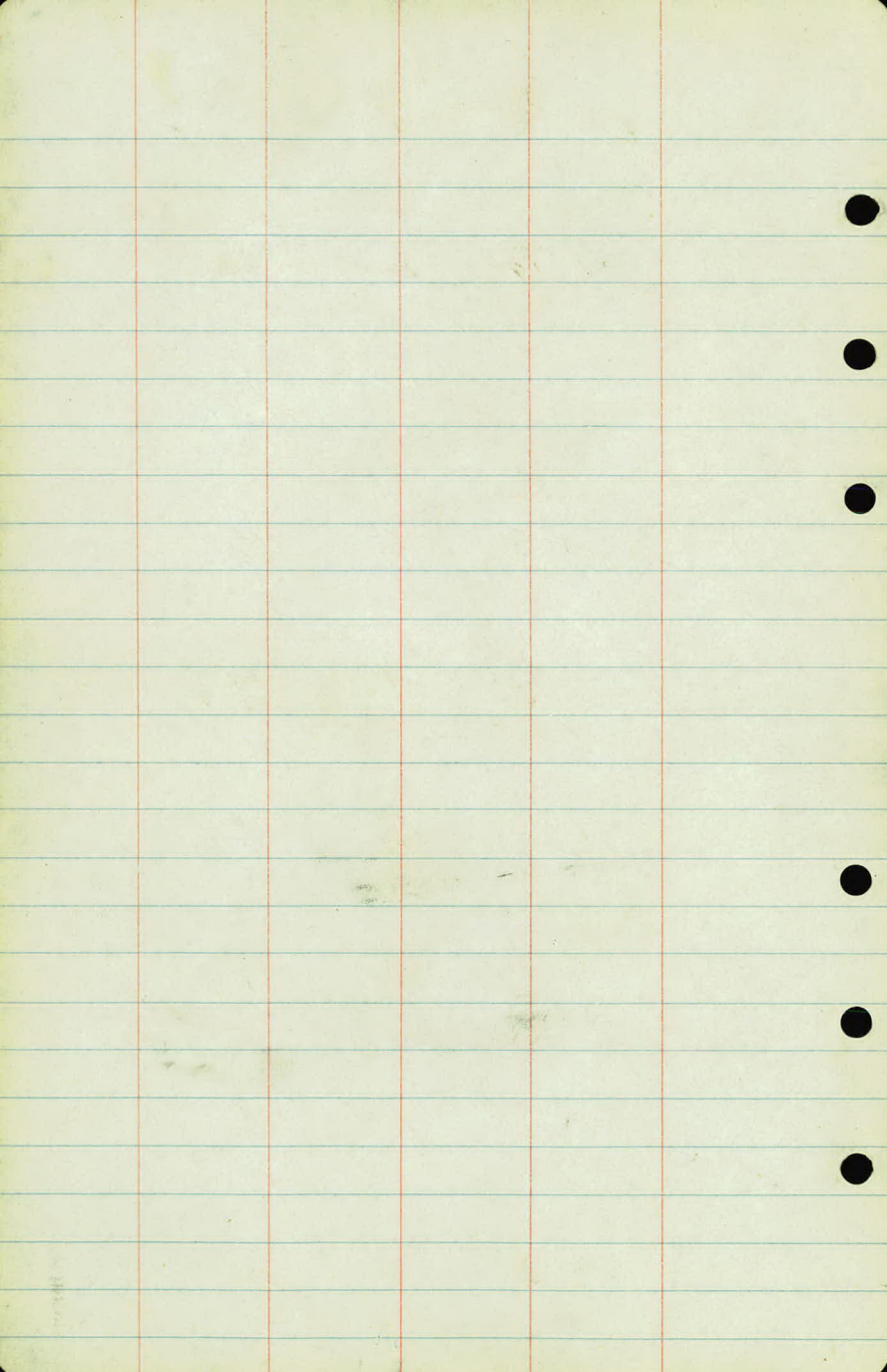
Q

R

34.0' / 16.5
1.916.6
1.817.2 / 16.6
1.2

P.R. Spk in @ Elm N. of Seashore Blvd & East Av.

34.3' / 16.6
2.216.4
2.417.0 / 16.5
1.830.4' / 15.3
5.613.2
6.714.3 / 16.5
6.631.0' / 15.5
6.714.1
8.113.9 / 16.5
8.312.9 / 16.5
10.1



GARDENETTE Park.

Storm Sewer Survey

Floral Drive to Gardenette Drive S

Through Path 621' E of Φ Bellevue - Page 1-3

Gardenette Drive So. to Gardenette Drive No
along line 192' E of Φ Bellevue - Page 3-4
also $\frac{1}{4}$ $\frac{1}{4}$ Line $\rightarrow$

Φ Lilac Lane to 250' No

along Line 20' E Φ Bellevue Ave Page 5

Platted
8/20/50

8-18-50

GB

AM

MB

KR

Sta	+	π	-	Elev
BM	5.65	949.86		944.21
TP	8.05	951.45	6.46	943.40

0 +00 = 15' So. of ϕ of Floral Drive 41.3

+02 41.2

+15 ϕ Floral Drive 41.8

+23 41.0

+45 N. Prop. Line 41.7

1 42.3

+50 42.6

2 43.7

+50 45.5

3 47.5

+40 47.0

£

SPK. in 30" Elm, S.W. Cor. Bellevue + Co. Rd. "F"

10.2

10.3

9.7

10.5

9.8

9.2

8.9

7.8

6.0

4.0

4.5

Sta	+	π	-	Elev
		951.45		
3+60		Ditch		46.5
3+64				46.8
+75		ϕ Gardenette So		
T.P.	3.71	953.81	1.35	950.10
T.P.	3.00	945.34	11.47	942.34
0+00		ϕ Gardenette Drive So		41.6
+14				41.0
+19				41.4
+34				42.2
+50				42.6
1				43.1

Dist

5.0

4.7

Top SW cor Lower Step front of 2265 Gardenette Sq

3.7

4.3

3.9

3.1

2.7

2.2

Sta	+	π	-	Elev.
		945.34		
1	+50.			41.2
2				40.2
	+50			41.0
3				41.2
	+25			41.1
	+32			38.8
	+44			38.6
	+46			38.2
	+60			39.0

4.1

5.1

4.3

4.1

4.2

6.5

6.7

7.1

6.3

Sta	+	π	-	El _{pv}	
		945.34			
0+00	E Lilac Lane 10' W of Prop Line of Bellevue			39.9	
+14				39.3	
+26				37.4	
+50				34.6	
1				33.3	
+50				32.6	
2				31.2	
+50				30.6	
B.M			10.94	934.40	934.50

5

→

5.4

6.0

7.9

10.7

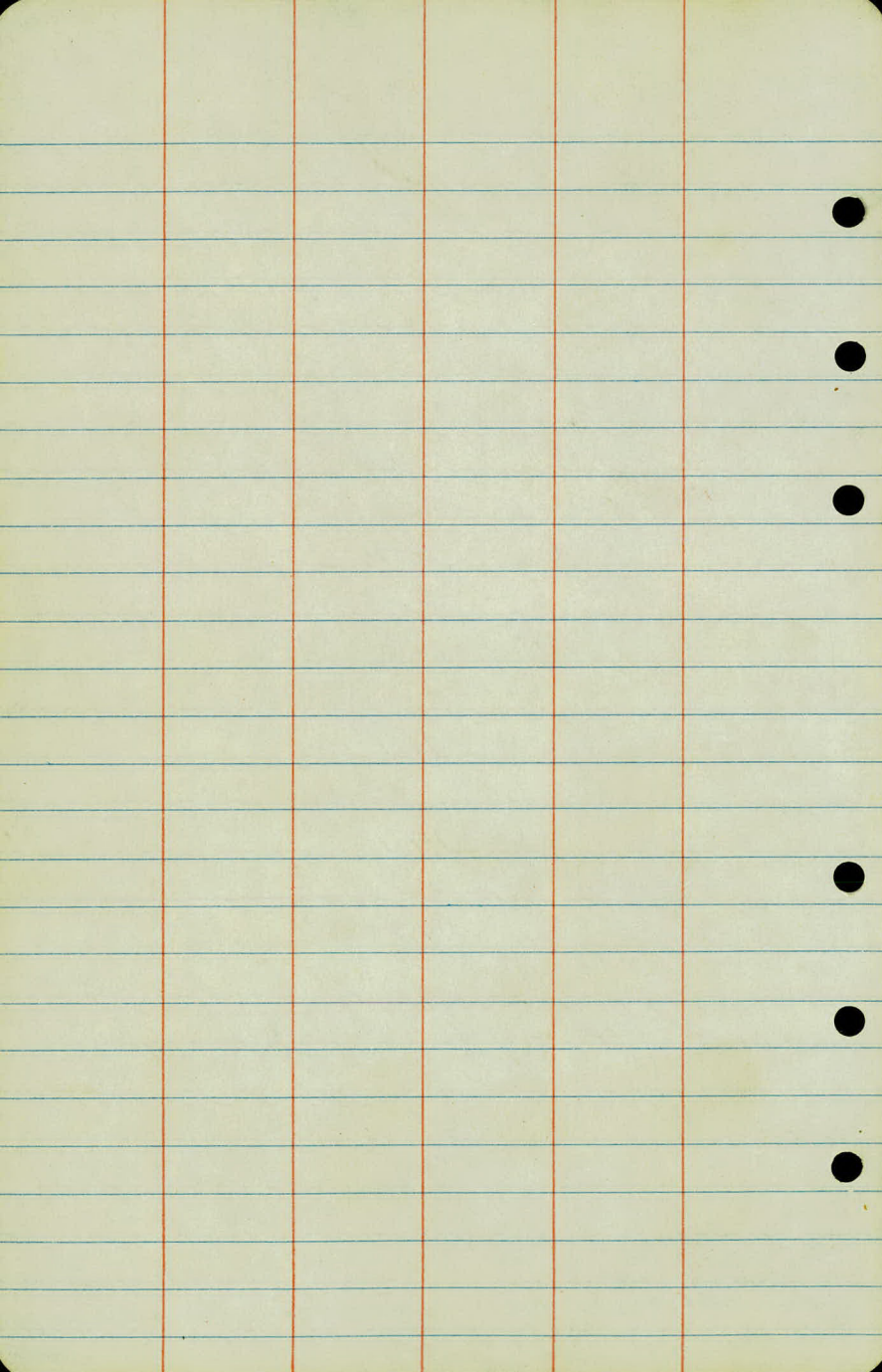
12.0

12.7

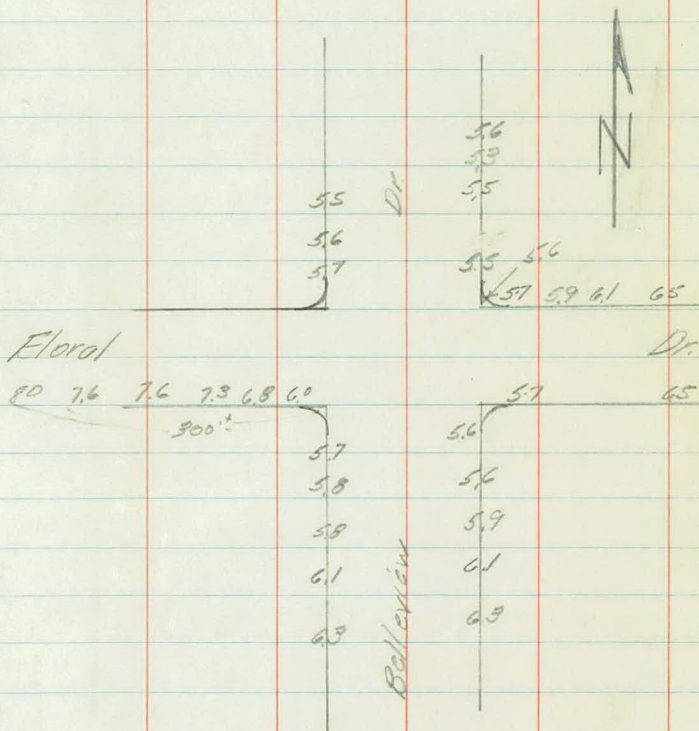
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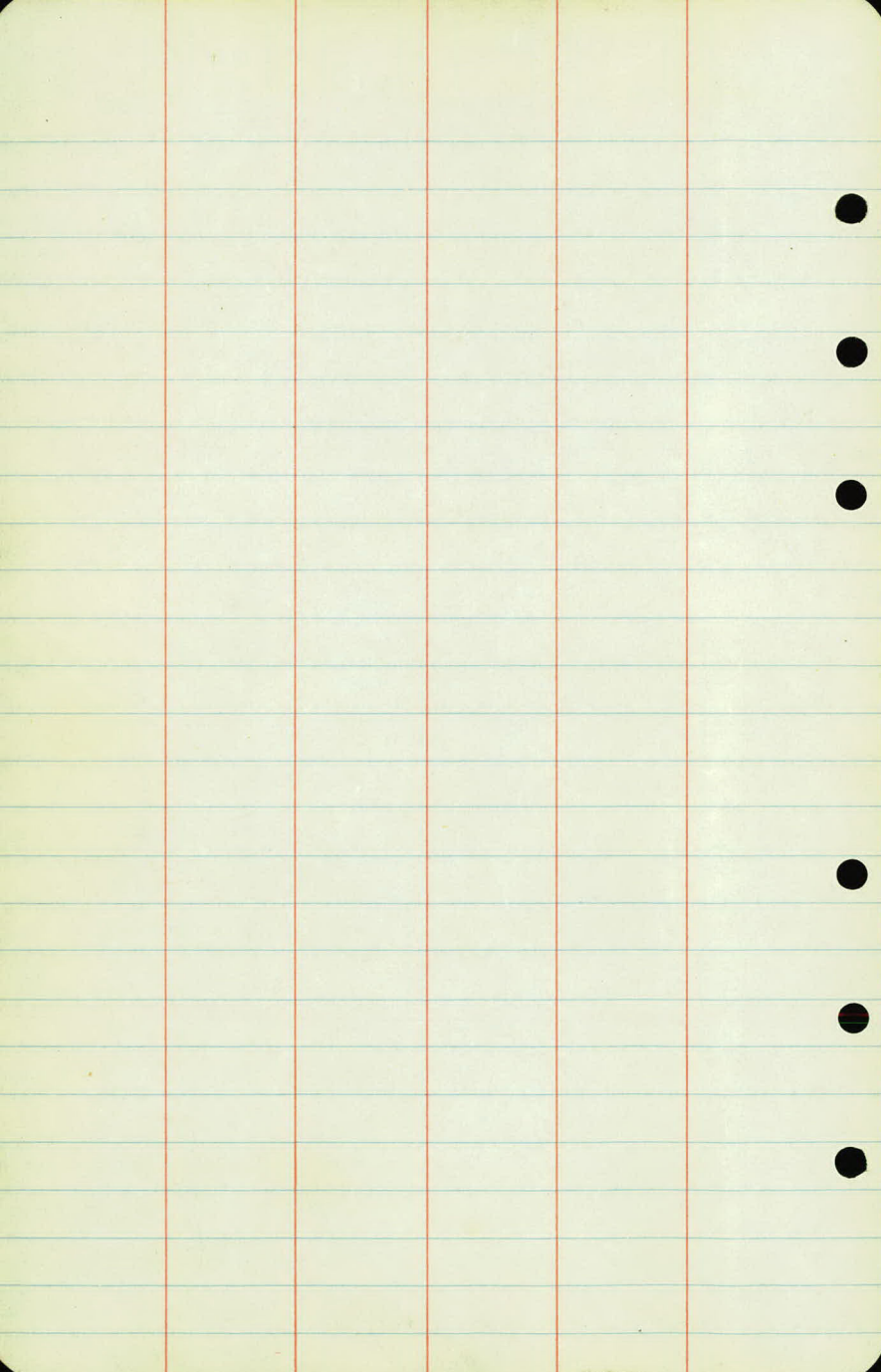
14.7

Spk Bent & Driven into Hole
Sp K. in. PP West of Turn @ Cemetery.

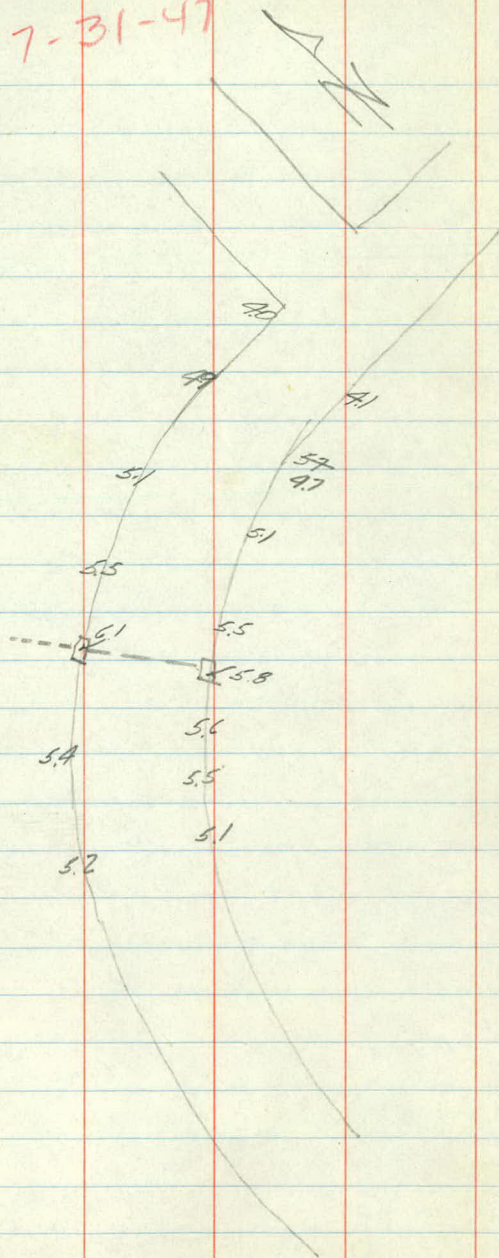


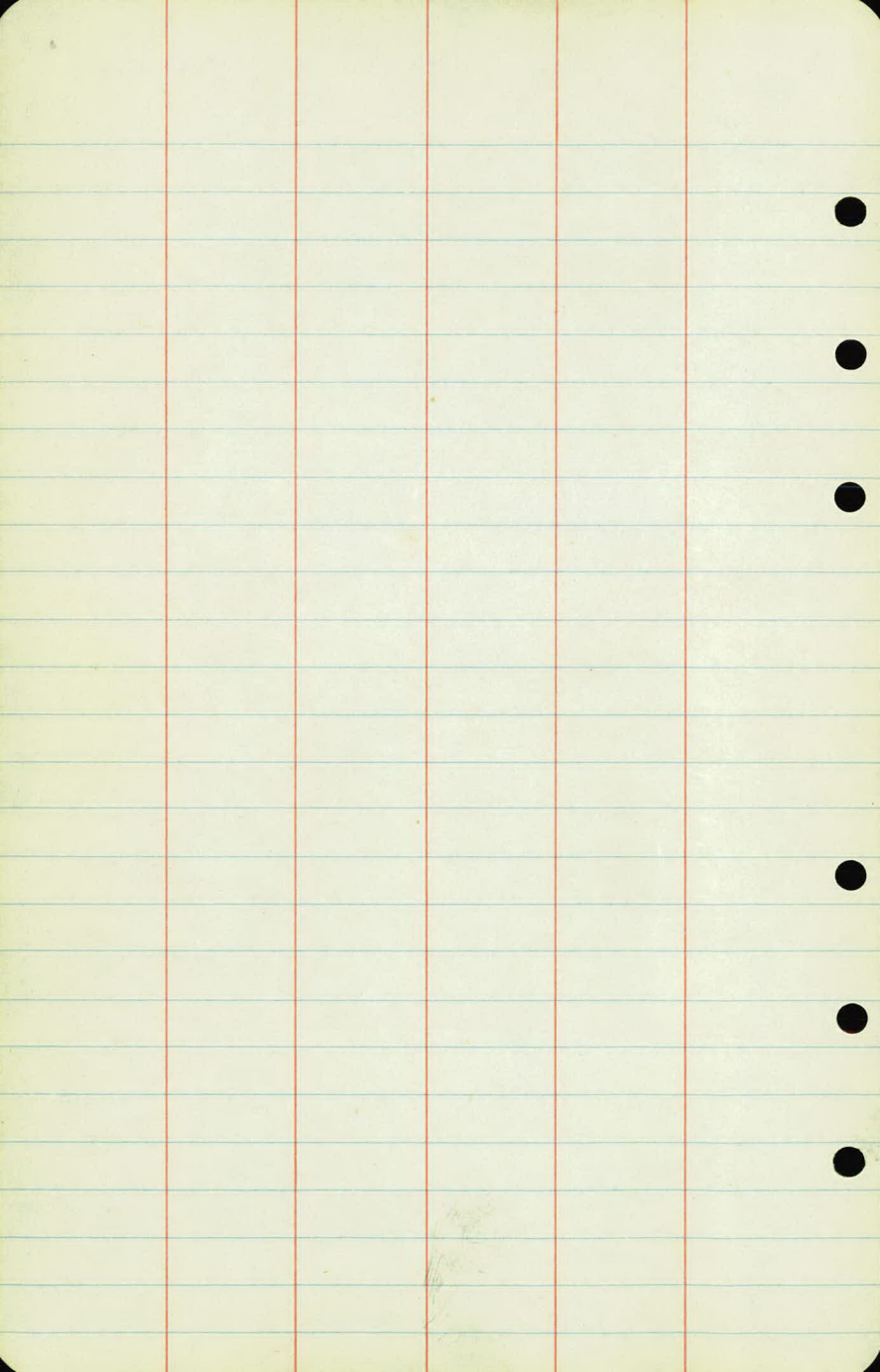
7-31-47





7-31-47

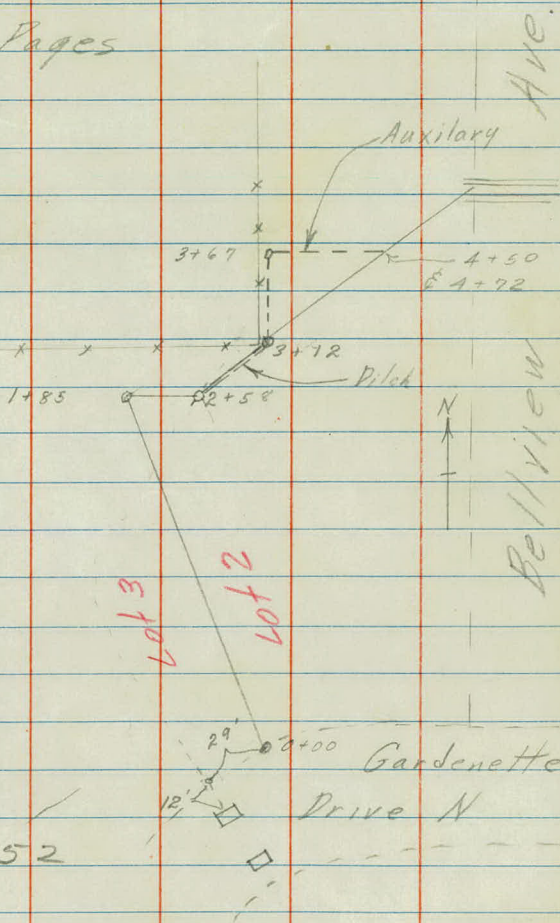




Gardenette Park

Drainage Profile

4 Pages



Rec'd. 6-2-52
R.C.

Sta	+	Δ	-	Elev
B M	2.99	942.97		939.98
South Catch Basin FL			9.00	33.97
" " g rate			7.23	35.74
size of pipe Tap catch Basin				
- 41.5				
FL North Catch Basin			8.95	34.02
- 29			9.2	33.8
0 + 00			6.4	36.6
+ 50			6.5	36.5
1			8.8	34.2
+ 50			9.5	33.5
+ 85 PL			8.2	34.8
2			8.3	34.7
+ 58 PL			9.6	33.4
3			9.4	33.6

2 May 1952
Hvidera
Moeschter
Clark
Benson

2

Spike in T.P.Lt. Bolview Btwn. Gardenett & Lilac Lane

Page 5 Bk. 61 Pr 14

Sta	+	Δ	-	Elev
		942.97		

3 + 12			10.0	33.0
--------	--	--	------	------

+ 29			8.3	34.7
------	--	--	-----	------

+ 50			7.5	35.5
------	--	--	-----	------

4			9.4	33.6
---	--	--	-----	------

+ 50			10.7	32.3
------	--	--	------	------

5			10.9	32.1
---	--	--	------	------

+ 44	West End FL Necess Drain		11.22	31.75
------	-----------------------------	--	-------	-------

+ 76	East End FL Cross drain		11.32	31.65
------	----------------------------	--	-------	-------

Auxiliary

3 + 50			10.5	32.5
--------	--	--	------	------

+ 67			11.5	31.5
------	--	--	------	------

+ 78			10.0	33.0
------	--	--	------	------

4			10.2	32.8
---	--	--	------	------

A
942.97

4 + 50

10.3 32.7

+ 72 Same as 4+50

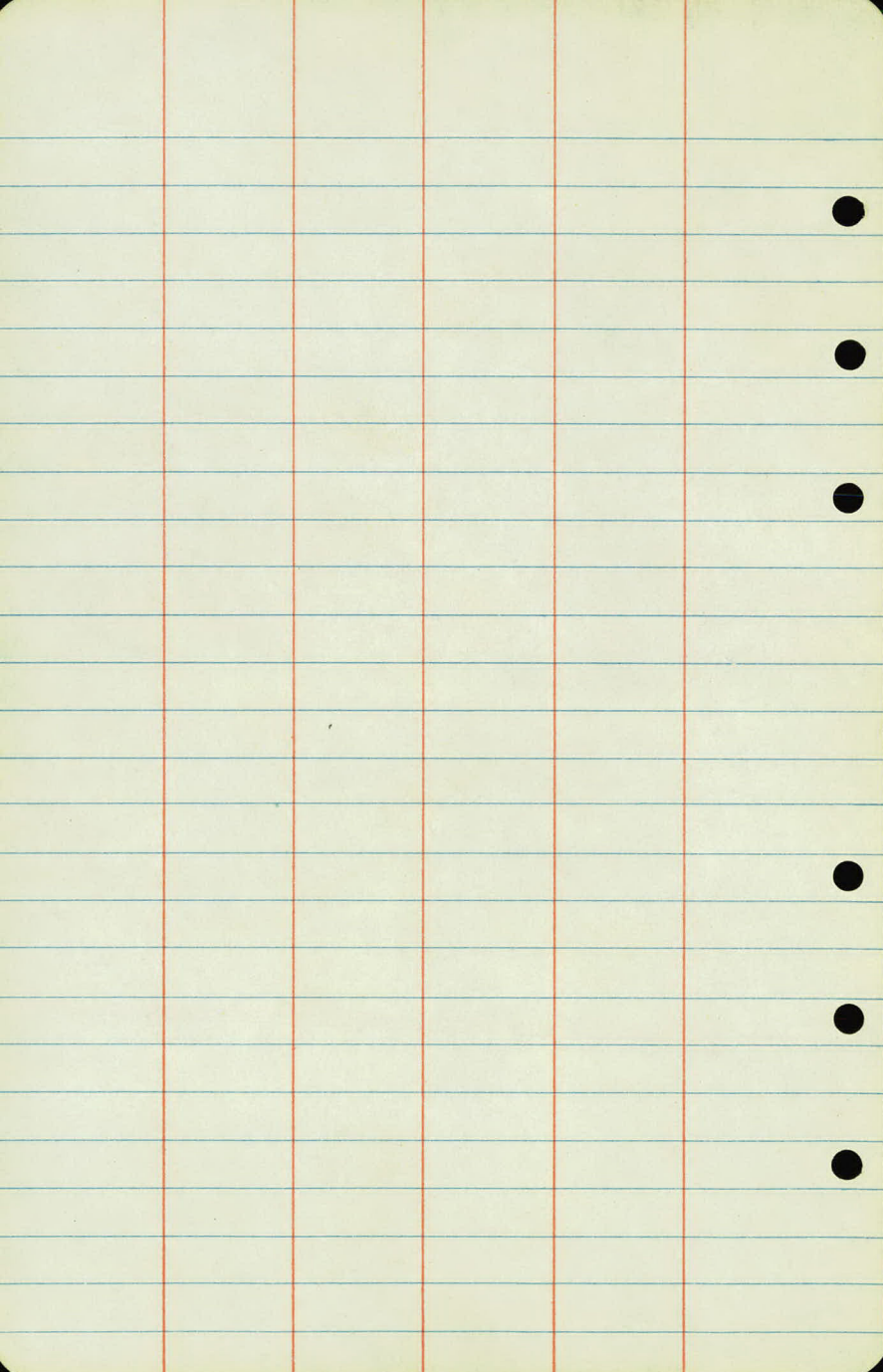
10.7 32.3

BM

2.99 939.98

4

Spike in T. Plt Bellview Btwn. Guardenett & Lilac Lane



1
East Ave.

North from Co. Rd. "F"

29 Oct. 1952

FK

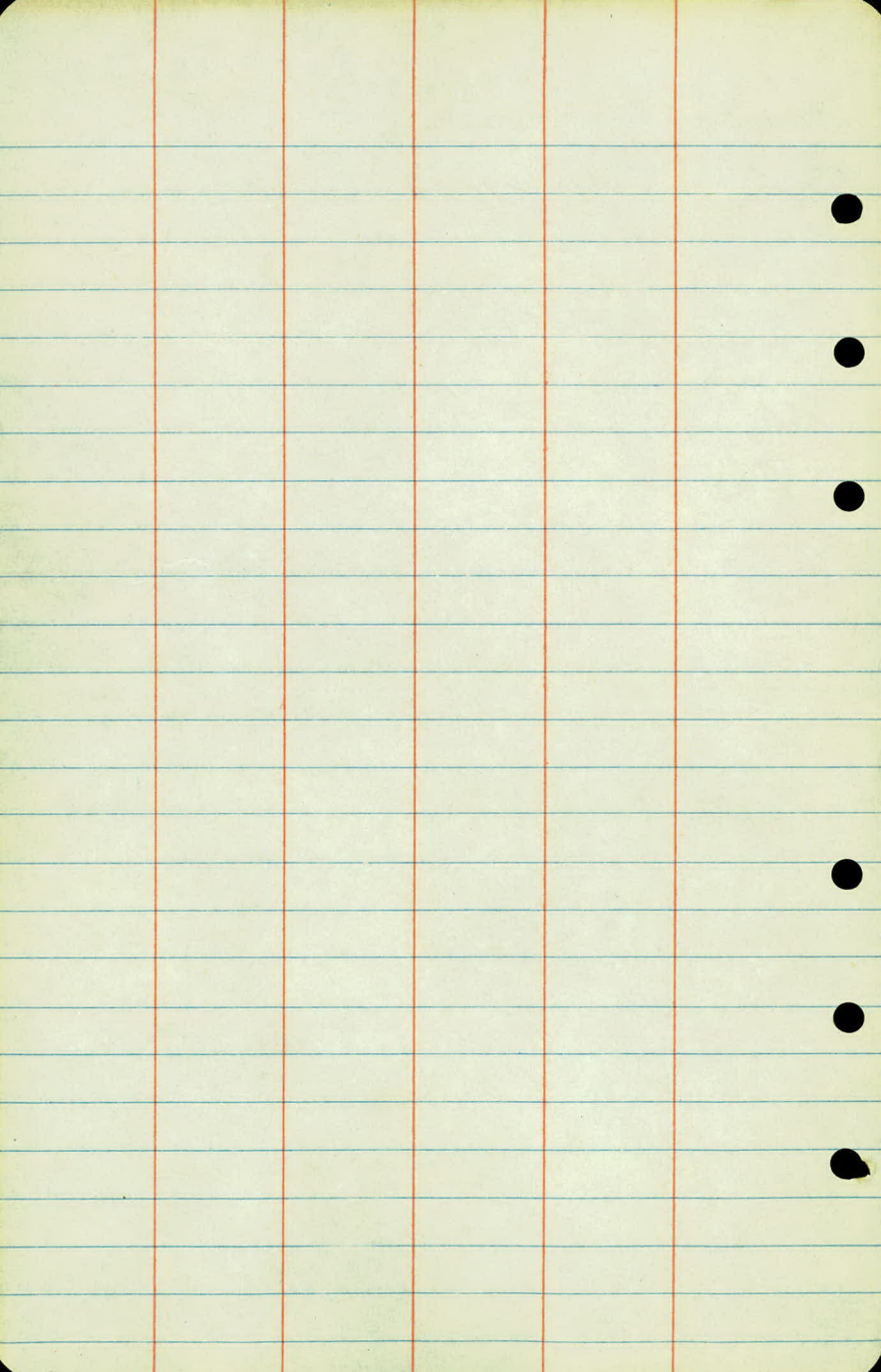
LC

MB

6 pages

Rec'd. Oct 30, 1952

R.C.



Floral Drive

East Ave

Section Line

89° 27 1/2'

Co. Rd

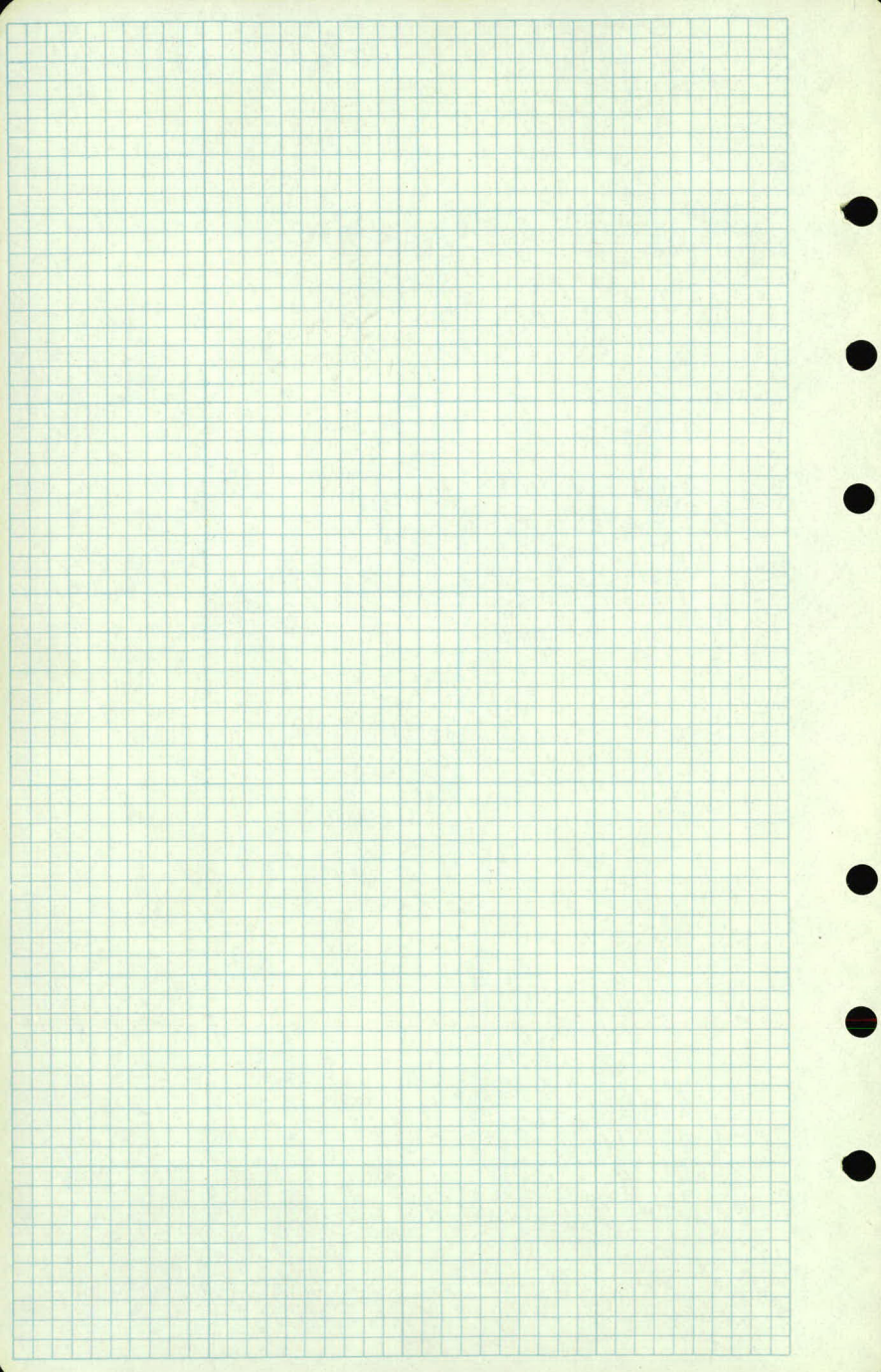
"F"

16.5'

0+00

0+00

0+00



x-sections

Sta	+	π	-	Elev
BM	3.55	954.50		950.95

3				49.6
---	--	--	--	------

+50				49.6
-----	--	--	--	------

+85	ϕ Laurel			49.7
-----	---------------	--	--	------

4				49.8
---	--	--	--	------

+11				49.9
-----	--	--	--	------

+19				49.9
-----	--	--	--	------

+50				50.4
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5				51.9
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Lt.

2

Rt.

R.R. spk. in 30" Oak 100' SW East Ave E "F"

49.1	48.3	48.4	48.9	49.3	49.1	49.4	51.5	50.9	50.9
5.4	6.2	6.1	5.6	5.2	4.9	5.4	5.1	3.6	3.6
50	26	21	13	9	10	13	17	30	50
House									
48.0	48.8	49.1			49.0	49.7	50.6	50.1	50.3
6.5	5.7	5.4	4.9	5.5	4.8	3.9	4.4	4.2	
25	13	6		10	15	20	27	50	
47.5	48.4	48.8	49.4		49.3	49.2	49.6	49.7	50.0
7.0	6.1	5.7	5.1	4.8	5.2	5.3	4.9	4.8	4.5
100	50	36	15		7	14	25	38	50
48.5	48.4	49.6	49.9		49.4	49.2	49.8	49.5	49.9
6.0	6.1	4.9	4.6	4.7	5.1	5.3	4.7	5.0	4.6
38	29	12	3		10	15	22	33	50
49.0	49.3	48.8	49.9		49.5	49.3	49.8	49.5	49.9
5.5	5.2	5.7	4.6	4.6	5.0	5.2	4.7	5.0	4.6
25	20	18	6		10	15	21	35	50
47.6	48.9	49.5	49.3	50.0	49.7	49.4	49.9	49.5	49.9
6.9	5.6	5.0	5.2	4.5	4.6	4.8	5.1	4.6	5.0
25	19	14	12	3	9	16	21	33	50
47.9	48.3	49.9	50.0	50.4		50.7	49.9	50.3	50.0
									50.2
6.6	6.2	4.6	4.5	4.1	4.1	4.3	4.6	4.2	4.5
25	21	14	10	3		9	15	21	36
									50
50.4	50.9	51.4	51.2	51.9	51.3	51.3	51.2	51.4	
4.1	3.6	3.1	3.3	2.6	2.6	3.2	3.2	3.3	3.1
25	19	13	12	4		7	15	27	50

Sta	+	π	-	Elev
		954.50		
TP	10.56	964.66	0.40	954.10
5+50				54.1

+50

55.7

6

+50

56.1

7

56.3

+50

55.9

8

55.9

+30

Lt

P

Pt

52.4	52.7	53.7	53.4	54.1		53.7	53.5	53.9	54.7	55.6
12.3	12.0	11.0	11.3	10.6	10.6	11.0	11.2	10.8	10.0	9.1
25	22	14	13	4		7	10	13	14	20

54.7	55.1
10.0	9.6
24	50

54.5	54.8	55.1	54.8	55.7	55.2	55.5	57.4	57.7	57.1	57.3	57.6
10.2	9.9	9.6	9.9	9.0	9.5	9.2	7.3	7.0	7.6	7.4	7.1
25	22	15	13	4	8	12	16	21	27	39	50

55.3	55.9	56.0	55.6	56.1		55.9	55.7	56.3	59.9	59.4	59.0	59.3
9.4	8.8	8.7	9.1	8.6	8.6	8.8	9.0	8.4	4.8	5.3	5.7	5.4
25	18	15	13	4		6	9	13	17	26	28	50

55.9	56.1	55.8	56.3		56.0	56.5	59.0	60.7	60.9	60.2	60.0	60.0
8.8	8.6	8.9	8.4	8.4	8.7	8.2	5.7	4.0	3.8	4.5	4.7	4.7
25	16	14	6	5	8	11	14	17	21	23	37	50

54.0	55.4	55.4		55.9		55.6	56.0	56.0	55.5	55.2	55.5
10.7	9.3	9.3		8.8	8.8	9.1	8.7	8.7	9.2	9.5	9.2
25	17	14		4		9	10	21	25	35	50

53.4	54.8	55.1	55.9		55.2	55.5	53.1		52.2	52.4
11.3	9.9	9.6	8.8	8.8	9.5	9.2	11.6		12.5	12.3
25	19	15	3		10	12	16		35	50

56.51	55.81
8.15	8.85
90	29
Garage	Cono. Driveway

Sta	+	π	-	Elev.
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		964.66		
--	--	--------	--	--

8+50				
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				55.7
--	--	--	--	------

BM				
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		796		956.70
--	--	-----	--	--------

9				
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				55.7
--	--	--	--	------

+35				
-----	--	--	--	--

+50				
-----	--	--	--	--

				55.9
--	--	--	--	------

BM				
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		1372		950.94
--	--	------	--	--------

				950.95
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56.1 55.5 54.6 54.8 55.7 55.1 55.1 53.0 51.7 51.1 51.0
 8.6 9.2 10.1 9.9 9.0 9.0 9.6 9.6 11.7 13.0 13.6 13.7
 House 25 22 15 5 10 12 16 22 32 50
 62

Top SE Cor of 1st step Front of Ho. 4159 East Ave

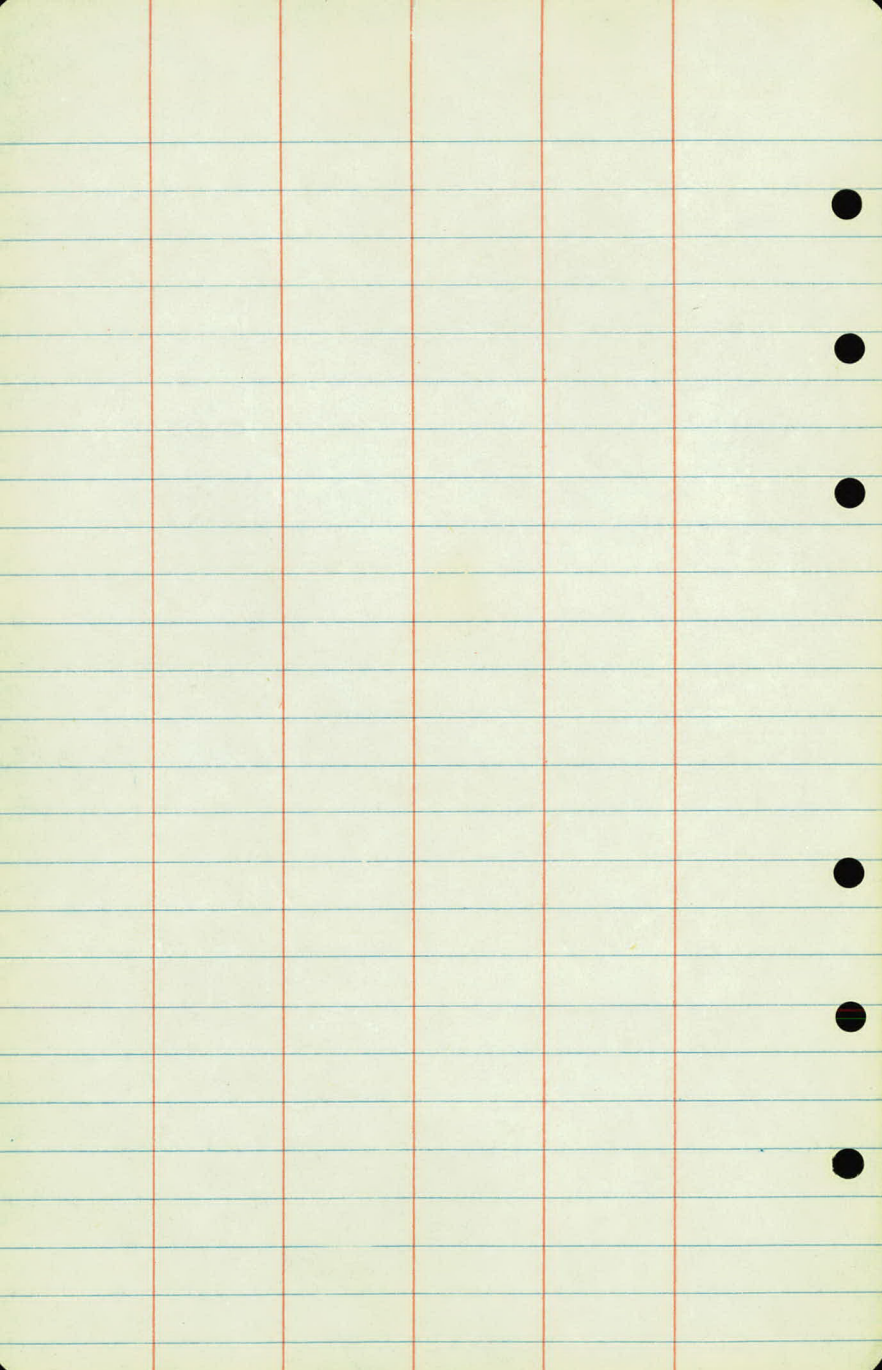
56.5 55.5 54.7 54.7 55.8 55.1 55.4 55.4 53.0 52.2 51.2 50.4
 8.2 9.2 10.0 10.0 8.9 9.0 9.6 9.3 9.3 11.7 12.5 13.5 14.3
 87 26 22 14 3 10 11 12 17 23 32 50
 Garage

56.2
8.6

62 House

55.3 55.3 54.3 54.8 55.7 55.3 55.6 54.5 53.0 51.9 50.9
 9.4 9.4 10.4 9.9 9.0 8.8 9.4 9.1 10.2 11.7 12.8 13.8
 25 23 22 17 5 11 12 17 25 39 50

RR Spk in 30" Oak 100' SW East ave of "F"



East Ave

Profile No. of F

30 Oct

FK

LC

MB

3 pages

Sta + X - Elev

BM 4.43

0+00 L Co Rd "F"

+50

1

+50

2

+50

BM 3.11

10

Lt £ Rt.

B.R. Spt. in 30" Oak 100' SW East Ave & Cor 1 "F"

62 5.45 4.63 4.00 3.4
50 50

70 48 6.1
25 50

7.8 51 6.7
25 50

6.7 53 6.8
25 50

4.9 5.4 5.7
25 50

5.7 5.6 4.5
25 50

Top SE Cor 1st step Front of house 4159 East Ave

5.1 3.9 6.2
25 50

sta +

10+50

11

+50

12

+50

13

11

2

Rt.

4.7
25

41

7.2
504.1
25

1.0

2.0

4.0

4.2

4.5

4.2

