

BOOK 46

DR 14

OFFICE OF COUNTY ENGINEER
RAMSEY CO. MINN.

Plan Survey

CAMPBELL AVE.

From Birch Lake Ave To Sixth St.

Road Acc't. No.

Date Filed 3-16-44

File

W.B. City
BK 46-DR14

Plan Survey
Campbell Ave
From Birch Lake Ave to Sixth St.

5-18-43

HAW

AM

L.G.

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Drawn up 7/12/43.

Sta

Pt.

Alt

ΔE1

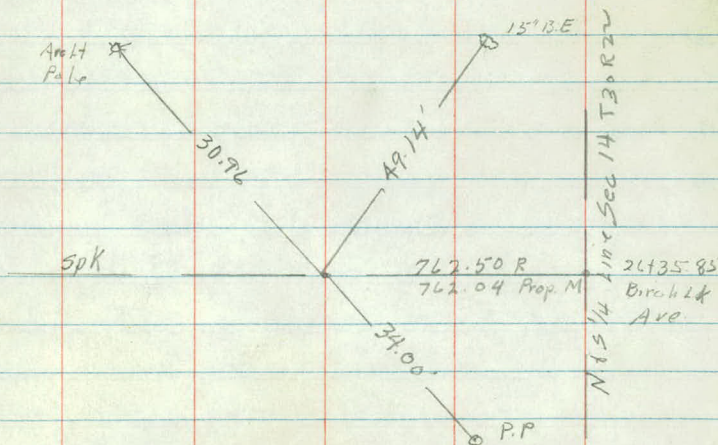
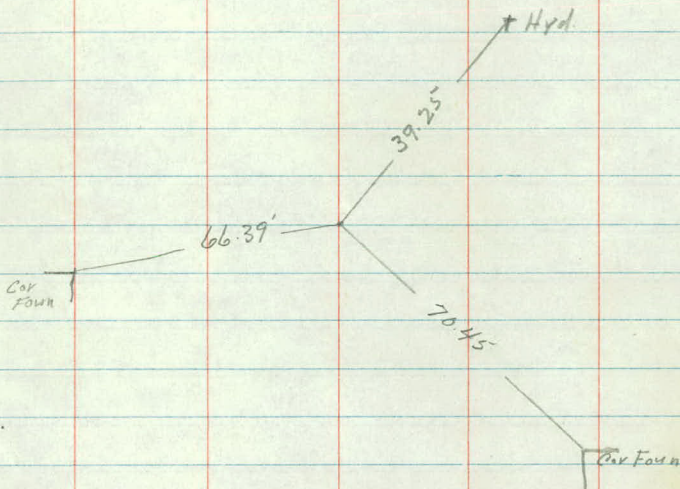
5+41.80

Δ Third St

0+00 = P.O.T.
18+73.81

Δ Birch Lake Ave

Description



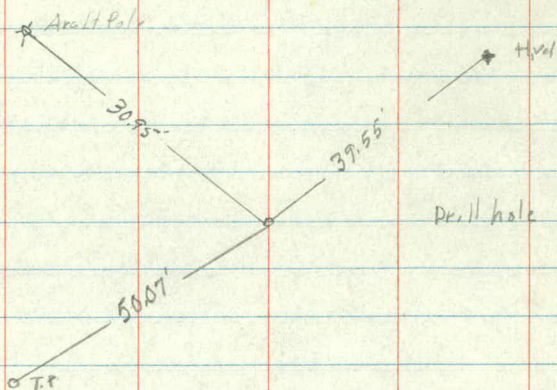
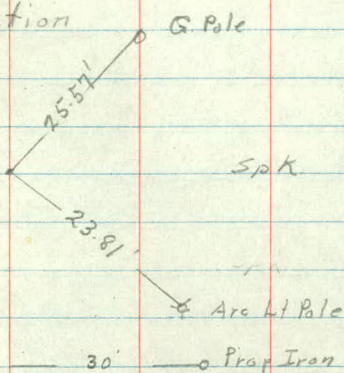
Sta	Pt	Alt	Art
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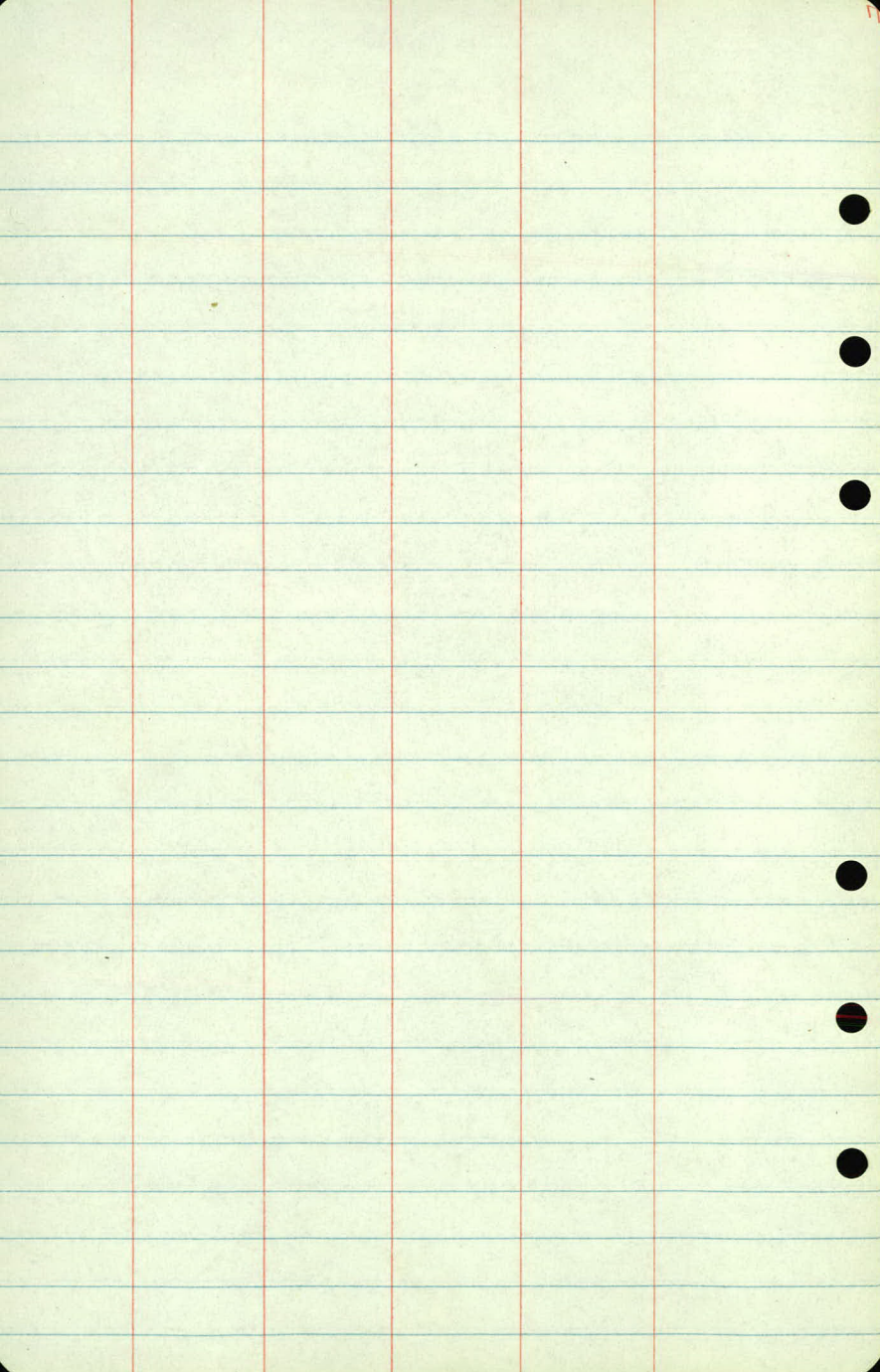
16+83 ⁵⁰	POT	\$	Sixth St
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16+53 ⁵⁰			So Prepline
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9+31.36	POT	\$	Fourth
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Description





TOPOGRAPHY

Campbell Ave

6

Ed 15 Ed 7

+44 59m M.H

5

12' 10'

+78 Ent

+89 X Hedge 30'
+84 6" Tree 35'

4

12' 12'

3

12' 12'

2

12' 12'

+89 P.P. 20'
+87 Beg. Hedge 30'
+85 End 10" OM 15'
+58 Beg 10" OM 10'

+92 2" P.M. 45'
+87 2" P.M. 32'
+82 2" P.M. 44'

1

12' 12'

+93 Stn 30'

0

19'

+17 X Drain 15" x 40'

21'

0-13 Edge Blacktop

Garden

- +50 Arch. Pole 21'
- +42 End Hedge 30'
- +23 Cen 2' Walk 27'
- +17 15" Oak 26'
- +106 Beg Hedge 30'
- +106 12" Oak 39'
- +77 Ent
- +72 X Fe 30'
- +72 End Hedge 30'
- +66 10" Ash 37'
- +57 Cen 3' Walk 50'
- +51 10" Ash 38'
- +43 Lilac Bush 33'
- +21 2" Pine 38'
- Hedge 30'
- +94 8" Pine 38'
- +56 3" Elm 38'
- +51 5' 4"
- +50 End Fe + Beg Hedge 30'
- +48 P.R. 21'
- +39 5' 2"

- +99 20" Oak 37'
- +86 Cen 3.5' Walk 30'
- +46 24" Oak 32'
- +33 Ent
- +23 Fe Cor 30'
- +18 Ent
- +13 Fe Cor 30'
- +12 End Hedge 30'
- +85 Apple Tr 45'
- +83 12" Elm 34'
- +81 Fe Cor 29'
- +72 Ent 10" x 26" CM 15'
- +59 Cor Hedge 29'

- Hedge 30'
- +80 24" Oak 40'
- +61 15" Oak 38'
- +34 Cor Hedge 29'
- +30 Ent Rad
- +33 Edge Walk 95'
- +29 Edge Walk 95'
- +24 Arch. Pole 20'
- +12 Beg Rad 24'

Yard

Garden

Yard

Yard

- +92 End Rad 9'
- +75 Bush 33'
- +75 Hpl 20'
- +64 Beg Rad 39'
- +39 End Rad 45'
- +100 Beg Rad 10'
- +95 12" Elm 22'
- +67 12" Elm 22'
- +60 SW Cor Ho 43'
- +24 Ent

- +47 6" Tree 37'
- +15 12" Ash 33'
- +100 3" Oak 24'

- +91 6" Tr 33'
- +75 12" Ash 35'
- +51 24" Oak 31'
- +25 5' 4"
- +101 2" Pine 32'
- +73 2" Pine 32'
- +63 T.P. 22'
- +60 X Hedge 31'
- +54 Ent
- +47 X Hedge 31'
- +38 2-2" Pine 31-40'
- +30 2" Pine 31'

- +30 End Rad 14'
- +45 T.P. 23'
- +36 18" BE 33'
- +33 Edge Walk 145'
- +29 Edge Walk 145'
- +12 Beg Rad 25'

13

Rd 10' Rd 10'

12

12' 18'

11

13' 10'

10

13' 10'

+61 End Rad 13'
+63 End 13" CM 16'
+62 Cor Walk 16.5'
+58 Cor Walk 16.5'
+57 Beg 12" CM 16'

+4136 Edge Pave.
+3136 Gen Pave
+2136 Edge Pave
+18 San M.H. 0

+9' 20" Elm 22'
+67 25" Elm 23'
+62 Cor Walk 16'
+58 Cor Walk 16'

9

8

14' 8'

7

14' 8'

San M.H.
+26

6

15' 9'

+92 10" B.E 39'
+67 15" B.E 44'
+46 P.P. 22'
+40 Ent

+60 Cen 2.5' Walk 16'

+84 15" Elm 19'
+75 Ent
+66 8" Elm 19'
+60 End Cull.
+11 P.P. 22'

+67 X Hedge 24' + Beg Cull
+54 Arch 21'
+41 Beg Rad 25'

+21 End Rad 48'

+11 T.P. 46
+01 Fe Cor 30'

+92 Beg Rad 15'

+49 3" Elm 30'
+33 Fe Cor 30'

+24 End Hedge 30'
+17 Stn 30'
+11 P.P. 22'

Hedge 30'

+91 15" Oak 37'
+86 Cen 2' Walk 29'
+73 15" Elm 37'
+71 Cor Hedge 29'
+64 Ent

+57 12" B.E 33'

+94 24" Oak 45'
+82 Ent

+77 P.P. 21'

+29 24" Oak 41'
+20 Ent Garden

+92 Ent
+70 15" Elm 21'
+47 15" Elm 21'
+26 15" Elm 21'
+06 15" Elm 21'

+83 15" Elm 21'
+61 6" Elm 22'
+38 12" Elm 22'
+14 26" Elm 23'

+92 15" Elm 22'
+69 X Hedge 26'
+68 12" Elm 23'

+55 Ent
+34 12" Elm 23'
+14 12" Elm 23'

+76 End Rad 10'
+54 Hyd. 32
+54 Cen C.B. 9' 15" Hyd. 27
+41 Beg Rad 37'

+21 End Rad 30'
+18 C Basin 26'
+02 Cor Hedge 30'

+89 Beg Rad 7'

+20 Beg Hedge 28'

+78 Cen 2' Walk 21'
+75 6" Elm 23'
+69 S.W. Cor No 34
+62 Ent
+53 6" Tree 24'
+53 Elm 24'
+41 8" Elm 41'
+38 5" Tr. 28'

+61 X Hedge 31'
+58 1" Tree 32
+51 Ent

+19 18" Oak 31
+02 Stn. 33

17

+96 Edge Rd
+83.30 R S 1/4 1-h

+83.30

16

11' 9'

15

12' 8'

14

11' 10'

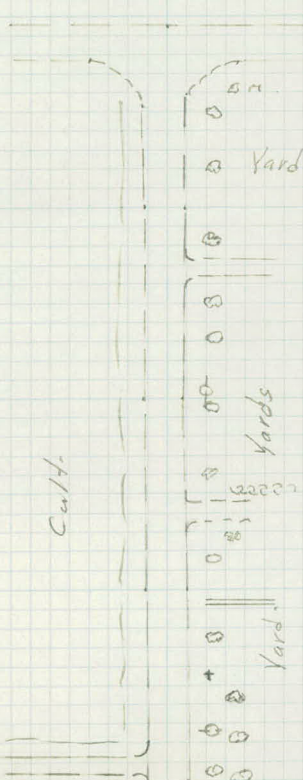
+93 Cen 3' Wa/K 22

13

10' 10'

+78 End Rad 38'
 +66 End Cult
 +53 Beg Rad 13'

+20 Beg Cult
 +10 End



+77 End Rad 37'
 +68 P.P. 18'
 +62 3rd 37'
 +62 12" Pop 32'
 +59 Beg Rad 10'

+50 12" Pop 22'
 +22 12" Elm 22'

+80 15" Elm 21'
 +70 End

+50 12" Pop 23'

+92 8" Tr. 22'

+04 P.P. 20'

+98 15" Elm 22'

+59 15" Elm 21'

+43 X Hedge 34'

+37 End

+25 Con 3 2" in Bushes 33'

+17 15" Elm 21'

+76 6" Elm 22'

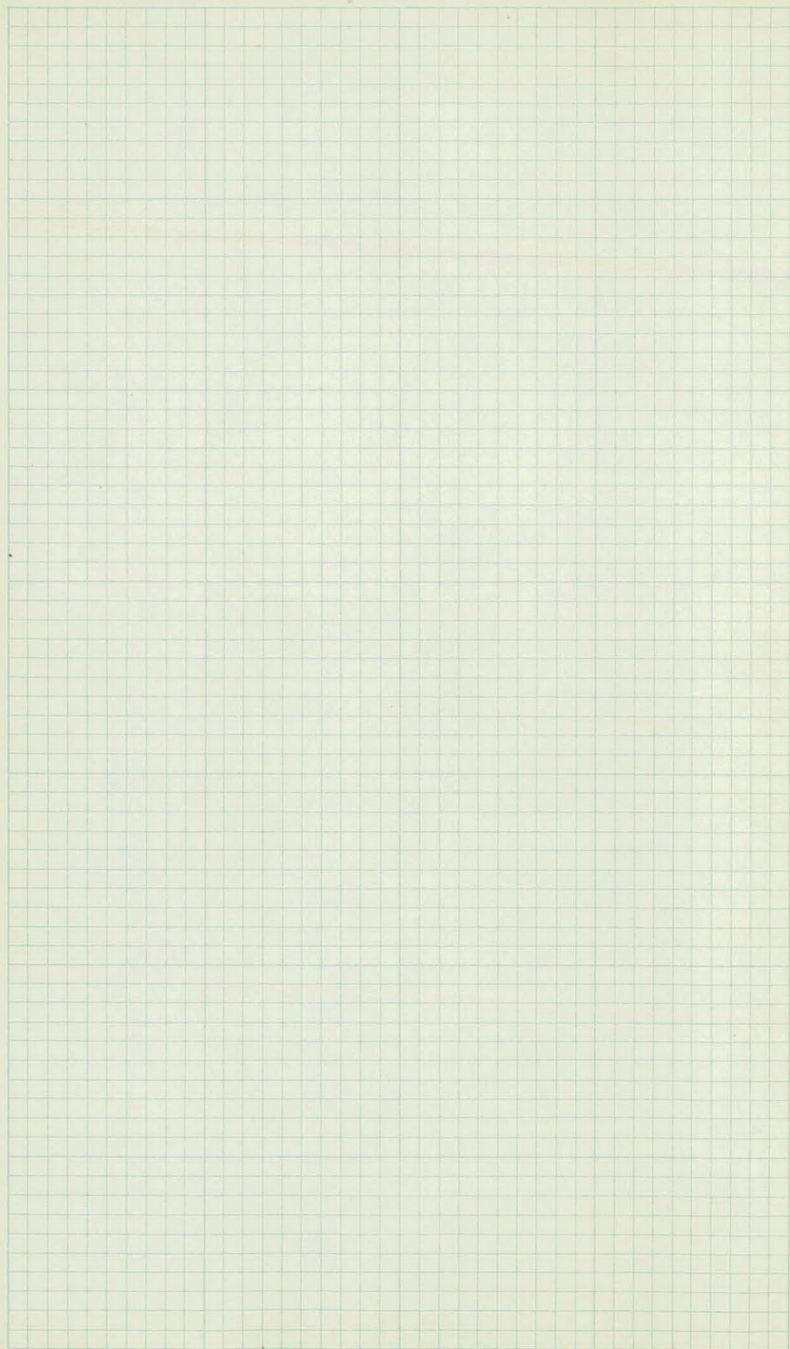
+55 Hydr 21'

+42 10" Elm 22'

+27 T.P. 22'

+24 24" Oak 38'

+03 15" Elm 22'



Bench Levels

Sta	+	-	Elev
B.M	3.01	938.26	935.25
	4.21	938.49	934.28
B.M	1.38	938.37	936.99
B.M	1.60	938.12	936.52
B.M	1.55	938.93	937.38
		3.07	935.86

Description

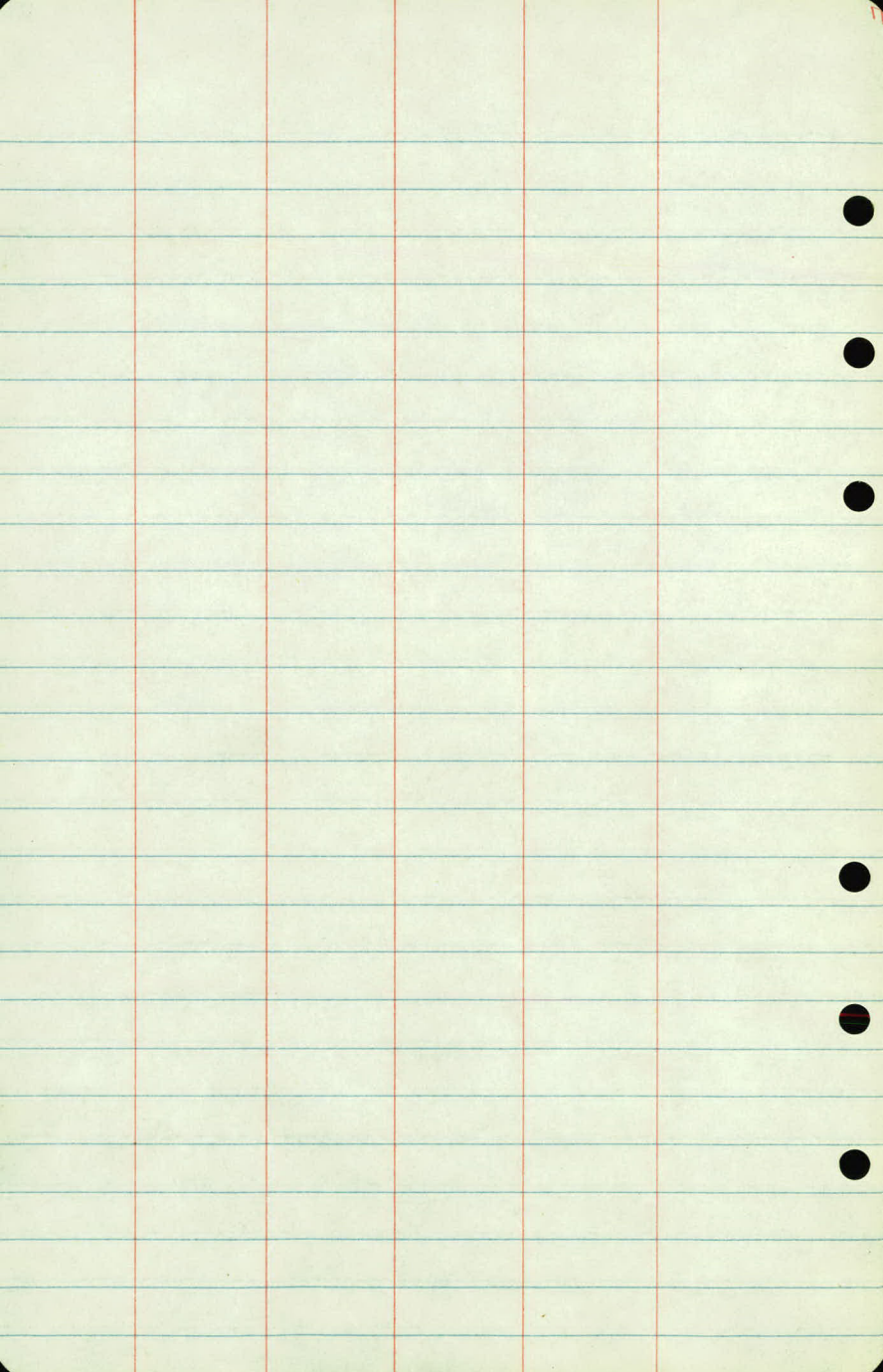
Top Hyd 200' L1 Sta 0+21

Top Hyd N.E Cor Third & Campbell Str

" " " Fourth & "

" " 21' Rt Sta 13+55'

Top N. West Cor Btm Conc Stop Ho S. E Cor Int.



X Sect.

Sta	+	Δ	-	Elev
13.M	2.75	938.00		935.25
0+00	(Note see	Profile Birch Lake Ave)		32.60
		Plan Survey Elev same 8 M.		
+18		15" x 40 CM	X Drain	33.0
+23				33.2
+33				33.2
+50				33.2
1+00				33.3
+50				33.5
+59				
		Side Dr. 8" x 10" X 20 CM	Plugged	
+85				
1+00				33.6
T.P.	3.27	938.62	2.65	935.35
+50				33.5
+86				

Lt

R

Rt

Top Hrd 200' Lt Sta 0 + 21

$$\frac{5.5}{50}$$

5.4

$$\frac{5.5}{50}$$

		Inv						Inv				
$\frac{6.1}{50}$	$\frac{6.1}{19}$	$\frac{6.0}{19}$	$\frac{5.5}{18}$	$\frac{5.1}{8}$	5.0	$\frac{5.1}{18}$	$\frac{5.1}{21}$	$\frac{6.75}{21}$	$\frac{6.0}{21}$	$\frac{6.2}{50}$		

$\frac{5.4}{50}$	$\frac{5.3}{19}$	$\frac{5.5}{13}$	$\frac{5.1}{9}$	4.8	$\frac{5.0}{10}$	$\frac{5.2}{21}$	$\frac{5.6}{50}$
------------------	------------------	------------------	-----------------	-----	------------------	------------------	------------------

$\frac{4.98}{50}$	$\frac{4.90}{30}$	$\frac{5.10}{15}$	$\frac{5.2}{10}$	4.8	$\frac{5.2}{17}$	$\frac{5.08}{30}$	$\frac{4.98}{50}$
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$\frac{4.8}{50}$	$\frac{5.0}{30}$	$\frac{5.0}{21}$	$\frac{5.1}{13}$	4.8	$\frac{4.7}{15}$	$\frac{5.4}{19}$	$\frac{5.6}{30}$	$\frac{5.6}{50}$
------------------	------------------	------------------	------------------	-----	------------------	------------------	------------------	------------------

$\frac{4.1}{50}$	$\frac{4.5}{30}$	$\frac{4.7}{18}$	$\frac{5.4}{12}$	4.7	$\frac{5.1}{11}$	$\frac{4.9}{14}$	$\frac{5.4}{20}$	$\frac{5.2}{30}$	$\frac{4.7}{50}$
------------------	------------------	------------------	------------------	-----	------------------	------------------	------------------	------------------	------------------

$\frac{4.0}{50}$	$\frac{4.1}{30}$	$\frac{4.5}{17}$	$\frac{5.1}{12}$	4.5	$\frac{5.0}{11}$	$\frac{4.7}{30}$	$\frac{4.7}{50}$
------------------	------------------	------------------	------------------	-----	------------------	------------------	------------------

Inv 32.3
 $\frac{5.70}{15}$

32.65
Inv
 $\frac{5.35}{15}$

$\frac{3.8}{50}$	$\frac{3.8}{30}$	$\frac{4.4}{14}$	$\frac{4.8}{11}$	$\frac{4.5}{7}$	4.4	$\frac{4.9}{12}$	$\frac{4.4}{14}$	$\frac{4.9}{30}$	$\frac{4.9}{50}$
------------------	------------------	------------------	------------------	-----------------	-----	------------------	------------------	------------------	------------------

$\frac{3.9}{50}$	$\frac{4.2}{30}$	$\frac{5.0}{14}$	$\frac{5.3}{11}$	$\frac{5.2}{5}$	5.1	$\frac{5.4}{8}$	$\frac{5.6}{11}$	$\frac{5.1}{13}$	$\frac{5.1}{30}$	$\frac{5.4}{50}$
------------------	------------------	------------------	------------------	-----------------	-----	-----------------	------------------	------------------	------------------	------------------

Top Walk 34.16
 $\frac{4.46}{30}$

Sta + Σ - Elev

938.62

3+00

33.6

+50

33.5

4

33.9

+50

33.8

+57

Walk Lt.

5

33.8

+23

Top Walk Lt

+40

So Gutter Line 34.0 Third

+44

+50

& Travelled Str 34.0

+66

No Gutter Line 34.2

+77

34.2

BM

1.27

938.26

1.62

937.00

936.99

6

34.1

+26

Lt

K

Rt

$$\begin{array}{r} 3.9 \quad 4.7 \quad 4.8 \quad 5.4 \\ \hline 50 \quad 30 \quad 20 \quad 12 \end{array} \quad \begin{array}{r} 5.5 \quad 5.2 \quad 5.7 \quad 5.4 \quad 5.2 \\ \hline 50 \quad 11 \quad 13 \quad 19 \quad 30 \quad 50 \end{array}$$

$$\begin{array}{r} 5.0 \quad 5.5 \quad 5.3 \quad 5.7 \quad 5.4 \\ \hline 50 \quad 30 \quad 14 \quad 12 \quad 9 \end{array} \quad \begin{array}{r} 5.5 \quad 4.7 \quad 4.7 \quad 4.7 \\ \hline 50 \quad 11 \quad 9 \quad 13 \quad 30 \quad 50 \end{array}$$

$$\begin{array}{r} 5.2 \quad 5.3 \quad 5.0 \quad 5.3 \quad 5.0 \\ \hline 50 \quad 30 \quad 14 \quad 12 \quad 9 \end{array} \quad \begin{array}{r} 4.7 \quad 5.2 \quad 4.7 \quad 4.6 \quad 4.4 \\ \hline 50 \quad 10 \quad 13 \quad 30 \quad 50 \end{array}$$

$$\begin{array}{r} 3.9 \quad 4.7 \quad 4.8 \quad 5.2 \\ \hline 50 \quad 30 \quad 17 \quad 13 \end{array} \quad \begin{array}{r} 4.8 \quad 4.2 \quad 4.1 \quad 3.9 \\ \hline 48 \quad 14 \quad 26 \quad 33 \quad 50 \end{array}$$

$$\begin{array}{r} \text{Top Walk} \\ 4.56 \\ \hline 30 \end{array} \quad 34.06$$

$$\begin{array}{r} 4.7 \quad 5.0 \quad 5.1 \\ \hline 50 \quad 30 \quad 14 \end{array} \quad \begin{array}{r} 4.8 \quad 5.1 \quad 4.7 \quad 4.3 \quad 3.8 \\ \hline 48 \quad 10 \quad 13 \quad 30 \quad 50 \end{array}$$

$$\text{T. Walk } 4.54 \quad -34.08$$

$$\begin{array}{r} 4.0 \quad 4.1 \quad 4.5 \quad 4.7 \quad 5.1 \quad 4.9 \\ \hline 50 \quad 37 \quad 30 \quad 15 \quad 13 \quad 10 \end{array} \quad \begin{array}{r} 4.6 \quad 4.4 \quad 4.6 \\ \hline 46 \quad 23 \quad 30 \quad 50 \end{array}$$

Top San MH

$$4.72 \rightarrow 33.90$$

$$\begin{array}{r} 4.5 \quad 4.5 \quad 4.7 \quad 4.5 \quad 5.0 \quad 4.7 \\ \hline 50 \quad 32 \quad 30 \quad 14 \quad 12 \quad 8 \end{array} \quad \begin{array}{r} 4.6 \quad 4.2 \quad 4.0 \quad 4.1 \quad 4.3 \quad 5.0 \\ \hline 46 \quad 30 \quad 50 \quad 75 \quad 100 \quad 150 \end{array}$$

$$\begin{array}{r} 4.9 \quad 4.9 \quad 4.5 \quad 5.0 \quad 4.5 \\ \hline 50 \quad 30 \quad 14 \quad 12 \quad 9 \end{array} \quad \begin{array}{r} 4.4 \quad 4.3 \quad 4.6 \quad 4.4 \\ \hline 44 \quad 16 \quad 30 \quad 50 \end{array}$$

$$\begin{array}{r} 5.0 \quad 5.1 \quad 4.5 \quad 5.0 \quad 4.5 \\ \hline 50 \quad 30 \quad 14 \quad 12 \quad 8 \end{array} \quad \begin{array}{r} 4.6 \quad 5.0 \quad 3.9 \quad 3.6 \quad 3.3 \\ \hline 44 \quad 12 \quad 15 \quad 22 \quad 30 \quad 50 \end{array}$$

Top Hyd N.E Cor Third & Campbell

$$\begin{array}{r} 4.2 \quad 4.3 \quad 4.3 \quad 4.8 \quad 4.3 \\ \hline 50 \quad 30 \quad 15 \quad 13 \quad 10 \end{array} \quad \begin{array}{r} 4.5 \quad 4.0 \quad 3.5 \quad 3.1 \quad 2.7 \\ \hline 42 \quad 8 \quad 10 \quad 17 \quad 36 \quad 50 \end{array}$$

$$33.64$$

$$\begin{array}{r} \text{Top MH} \\ 4.62 \end{array}$$

Sta	+	π	-	Elev
		938.26		
6+26				33.9
+50				33.7
7				33.6
+50				33.5
+78		Top Walk Pt		34.68
+86		" " Lt		33.57
B M	1.37	937.89	1.74	936.52
8				936.52
				33.10
+50				33.0
9				32.8
+14				32.8
+18				32.75
+21 ³⁶		So Edge Pavc		32.64

Lt

~~R~~

Rt

$$\begin{array}{r} 3.2 \\ 50 \end{array} \quad \begin{array}{r} 3.2 \\ 30 \end{array} \quad \begin{array}{r} 4.2 \\ 25 \end{array} \quad \begin{array}{r} 4.4 \\ 15 \end{array} \quad \begin{array}{r} 4.9 \\ 14 \end{array} \quad \begin{array}{r} 4.6 \\ 9 \end{array} \quad 44 \quad \begin{array}{r} 4.5 \\ 8 \end{array} \quad \begin{array}{r} 4.1 \\ 10 \end{array} \quad \begin{array}{r} 3.3 \\ 19 \end{array} \quad \begin{array}{r} 2.7 \\ 30 \end{array} \quad \begin{array}{r} 2.3 \\ 50 \end{array}$$

$$\begin{array}{r} 3.3 \\ 50 \end{array} \quad \begin{array}{r} 3.2 \\ 30 \end{array} \quad \begin{array}{r} 4.3 \\ 25 \end{array} \quad \begin{array}{r} 4.5 \\ 15 \end{array} \quad \begin{array}{r} 4.8 \\ 14 \end{array} \quad 46 \quad \begin{array}{r} 4.4 \\ 8 \end{array} \quad \begin{array}{r} 3.2 \\ 12 \end{array} \quad \begin{array}{r} 2.9 \\ 27 \end{array} \quad \begin{array}{r} 2.7 \\ 48 \end{array} \quad \begin{array}{r} 936.30 \\ \text{Elev} \\ \text{Garfield} \\ 1.90 \\ 48 \end{array}$$

$$\begin{array}{r} 4.7 \\ 50 \end{array} \quad \begin{array}{r} 4.3 \\ 30 \end{array} \quad \begin{array}{r} 4.5 \\ 15 \end{array} \quad \begin{array}{r} 5.0 \\ 13 \end{array} \quad \begin{array}{r} 4.7 \\ 8 \end{array} \quad 4.7 \quad \begin{array}{r} 4.7 \\ 7 \end{array} \quad \begin{array}{r} 3.8 \\ 9 \end{array} \quad \begin{array}{r} 4.1 \\ 30 \end{array} \quad \begin{array}{r} 3.7 \\ 50 \end{array}$$

$$\begin{array}{r} 4.6 \\ 50 \end{array} \quad \begin{array}{r} 4.6 \\ 30 \end{array} \quad \begin{array}{r} 4.7 \\ 16 \end{array} \quad \begin{array}{r} 5.3 \\ 13 \end{array} \quad \begin{array}{r} 4.8 \\ 7 \end{array} \quad 48 \quad \begin{array}{r} 4.8 \\ 7 \end{array} \quad \begin{array}{r} 3.4 \\ 13 \end{array} \quad \begin{array}{r} 3.5 \\ 30 \end{array} \quad \begin{array}{r} 3.2 \\ 50 \end{array}$$

$$\begin{array}{r} 34.68 \\ 358 \end{array}$$

933.57

469

Top Hyd N.E. Cor Fourth & Campbell

$$\begin{array}{r} 4.5 \\ 50 \end{array} \quad \begin{array}{r} 4.4 \\ 30 \end{array} \quad \begin{array}{r} 4.3 \\ 17 \end{array} \quad \begin{array}{r} 5.2 \\ 13 \end{array} \quad \begin{array}{r} 4.9 \\ 9 \end{array} \quad 4.8 \quad \begin{array}{r} 5.0 \\ 7 \end{array} \quad \begin{array}{r} 3.7 \\ 11 \end{array} \quad \begin{array}{r} 3.7 \\ 30 \end{array} \quad \begin{array}{r} 4.0 \\ 50 \end{array}$$

$$\begin{array}{r} 5.2 \\ 50 \end{array} \quad \begin{array}{r} 5.3 \\ 30 \end{array} \quad \begin{array}{r} 4.9 \\ 15 \end{array} \quad \begin{array}{r} 5.2 \\ 14 \end{array} \quad 4.9 \quad \begin{array}{r} 5.1 \\ 7 \end{array} \quad \begin{array}{r} 4.2 \\ 11 \end{array} \quad \begin{array}{r} 4.9 \\ 19 \end{array} \quad \begin{array}{r} 4.8 \\ 30 \end{array} \quad \begin{array}{r} 5.0 \\ 50 \end{array}$$

$$\begin{array}{r} 5.2 \\ 50 \end{array} \quad \begin{array}{r} 5.0 \\ 30 \end{array} \quad \begin{array}{r} 5.0 \\ 18 \end{array} \quad \begin{array}{r} 4.9 \\ 11 \end{array} \quad 5.1 \quad \begin{array}{r} 5.4 \\ 8 \end{array} \quad \begin{array}{r} 4.5 \\ 11 \end{array} \quad \begin{array}{r} 4.7 \\ 18 \end{array} \quad \begin{array}{r} 4.6 \\ 30 \end{array} \quad \begin{array}{r} 4.8 \\ 50 \end{array}$$

$$\begin{array}{r} 4.9 \\ 50 \end{array} \quad \begin{array}{r} 5.2 \\ 30 \end{array} \quad \begin{array}{r} 5.2 \\ 10 \end{array} \quad 5.1 \quad \begin{array}{r} 5.4 \\ 11 \end{array} \quad \begin{array}{r} 5.2 \\ 18 \end{array} \quad \begin{array}{r} 4.5 \\ 21 \end{array} \quad \begin{array}{r} 4.3 \\ 30 \end{array} \quad \begin{array}{r} 4.1 \\ 50 \end{array}$$

$$\begin{array}{r} 4.8 \\ 50 \end{array} \quad \begin{array}{r} 5.2 \\ 30 \end{array} \quad \begin{array}{r} 4.9 \\ 19 \end{array} \quad 5.14 \quad \begin{array}{r} 5.2 \\ 12 \end{array} \quad \begin{array}{r} 5.2 \\ 26 \end{array} \quad \begin{array}{r} 8.35 \\ 26 \end{array} \quad \begin{array}{r} 4.9 \\ 30 \end{array} \quad \begin{array}{r} 4.3 \\ 50 \end{array}$$

$$\begin{array}{r} 5.02 \\ 50 \end{array} \quad \begin{array}{r} 5.01 \\ 30 \end{array} \quad 5.25 \quad \begin{array}{r} 4.92 \\ 30 \end{array} \quad \begin{array}{r} 4.90 \\ 50 \end{array}$$

Sta	+	Δ	-	Elev
		937.89		
9+31.36		±	Pave	32.84
		Note Pave Sagged at Int		
+4136				32.79
+50				33.0
+53				33.1
+61				33.1
+69				33.1
10				33.0
+50				33.2
11				33.3
+50				32.9
12		Walk Lt		33.2
+50				33.4

Lt 2 Rt

$$\frac{494}{50}$$

5.05

$$\frac{484}{50}$$

Note & Drain
West of Int

$$\frac{5.00}{50}$$

$$\frac{4.98}{30}$$

5.10

$$\frac{4.94}{30}$$

$$\frac{4.88}{50}$$

In V.

32.03 In V Drop
In 12 in. - 29.89

$$\frac{7.18}{171}$$

$$\frac{6.6}{150}$$

$$\frac{6.2}{100}$$

$$\frac{6.1}{50}$$

$$\frac{5.6}{19}$$

$$\frac{4.9}{12}$$

$$\frac{4.9}{12}$$

$$\frac{5.2}{12}$$

$$\frac{5.3}{18}$$

$$\frac{5.86}{27}$$

$$\frac{8.00}{27}$$

$$\frac{5.6}{50}$$

$$\frac{5.1}{50}$$

$$\frac{5.0}{20}$$

$$\frac{5.9}{17}$$

$$\frac{5.0}{14}$$

$$\frac{4.8}{12}$$

$$\frac{5.1}{12}$$

$$\frac{5.1}{18}$$

$$\frac{5.1}{30}$$

$$\frac{5.0}{50}$$

Side Walk Dr
No Int

T Walk

Ta Walk

$$\frac{5.01}{50}$$

$$\left(\frac{6.24}{17} \frac{6.10}{17} \right)$$

$$\frac{5.15}{17}$$

$$\frac{4.8}{14}$$

$$\frac{4.60}{10}$$

$$\frac{4.8}{12}$$

$$\frac{5.4}{12}$$

$$\frac{4.80}{17}$$

$$\frac{4.88}{30}$$

$$\frac{4.88}{50}$$

$$\frac{4.3}{50}$$

$$\frac{4.4}{30}$$

$$\frac{4.2}{23}$$

$$\frac{4.3}{18}$$

$$\frac{5.5}{16-15}$$

$$\frac{4.6}{14}$$

$$\frac{4.8}{11}$$

$$\frac{5.4}{11}$$

$$\frac{5.0}{14}$$

$$\frac{4.8}{21}$$

$$\frac{5.1}{30}$$

$$\frac{4.8}{50}$$

$$\frac{4.5}{50}$$

$$\frac{4.8}{30}$$

$$\frac{4.4}{18}$$

$$\frac{5.1}{13}$$

$$\frac{4.8}{10}$$

$$\frac{4.9}{6}$$

$$\frac{5.3}{9}$$

$$\frac{4.8}{12}$$

$$\frac{5.1}{21}$$

$$\frac{5.1}{30}$$

$$\frac{4.9}{50}$$

$$\frac{5.1}{50}$$

$$\frac{5.2}{30}$$

$$\frac{4.8}{25}$$

$$\frac{4.8}{17}$$

$$\frac{5.3}{14}$$

$$\frac{4.7}{10}$$

$$\frac{5.2}{10}$$

$$\frac{4.9}{30}$$

$$\frac{4.7}{50}$$

$$\frac{5.1}{50}$$

$$\frac{5.1}{30}$$

$$\frac{4.9}{27}$$

$$\frac{4.8}{15}$$

$$\frac{5.4}{13}$$

$$\frac{4.9}{8}$$

$$\frac{4.6}{10}$$

$$\frac{4.9}{12}$$

$$\frac{5.3}{10}$$

$$\frac{4.7}{19}$$

$$\frac{5.1}{30}$$

$$\frac{5.0}{40}$$

$$\frac{4.7}{50}$$

$$\frac{4.9}{50}$$

$$\frac{4.9}{30}$$

$$\frac{4.7}{16}$$

$$\frac{5.4}{12}$$

$$\frac{5.1}{8}$$

$$\frac{5.0}{10}$$

$$\frac{5.2}{10}$$

$$\frac{4.5}{12}$$

$$\frac{4.9}{30}$$

$$\frac{4.7}{50}$$

Top Walk

32.99

$$\frac{4.3}{50}$$

$$\frac{4.7}{30}$$

$$\frac{4.90}{16}$$

$$\frac{5.0}{12}$$

$$\frac{4.7}{7}$$

$$\frac{4.7}{10}$$

$$\frac{5.2}{10}$$

$$\frac{4.5}{12}$$

$$\frac{4.9}{30}$$

$$\frac{4.7}{50}$$

$$\frac{3.6}{50}$$

$$\frac{4.7}{30}$$

$$\frac{4.8}{13}$$

$$\frac{5.0}{12}$$

$$\frac{4.7}{6}$$

$$\frac{4.5}{10}$$

$$\frac{5.1}{10}$$

$$\frac{4.6}{12}$$

$$\frac{4.7}{30}$$

$$\frac{4.2}{50}$$

Sta + π - Elev

937.85

13

33.9

+50

34.10

B.M

146

938.84

0.52

937.37

937.38

+93

Walk Rt

?

14

14

34.1

+50

34.0

15

34.1

+50

34.5

16

34.6

+40

34.3

+53⁵⁰

So Prop Line

34.1

+70

33.9

+77

33.8

Lt

Z

Rt

$$\frac{3.8}{50} \quad \frac{4.0}{30} \quad \frac{4.3}{17} \quad \frac{4.6}{11} \quad \frac{4.3}{7} \quad 4.0 \quad \frac{4.8}{9} \quad \frac{4.1}{12} \quad \frac{4.4}{30} \quad \frac{4.6}{50}$$

$$\frac{3.5}{50} \quad \frac{3.7}{30} \quad \frac{3.5}{14} \quad \frac{4.2}{11} \quad \frac{4.0}{7} \quad 3.8 \quad \frac{4.4}{9} \quad \frac{3.7}{11} \quad \frac{4.0}{30} \quad \frac{4.0}{50}$$

Top Hyd 21' Lt Sta 13+55

34.33

4.51

$$\frac{4.6}{50} \quad \frac{4.4}{25} \quad \frac{4.1}{22} \quad \frac{4.0}{14} \quad \frac{5.1}{11} \quad \frac{4.8}{6} \quad 4.7 \quad \frac{5.1}{9} \quad \frac{4.6}{12} \quad \frac{4.7}{30} \quad \frac{4.5}{50}$$

$$\frac{5.2}{50} \quad \frac{4.9}{30} \quad \frac{4.6}{23} \quad \frac{4.5}{15} \quad \frac{5.4}{12} \quad \frac{4.8}{6} \quad 4.8 \quad \frac{5.4}{9} \quad \frac{5.0}{10} \quad \frac{5.0}{30} \quad \frac{5.1}{50}$$

$$\frac{5.1}{50} \quad \frac{5.1}{30} \quad \frac{4.8}{16} \quad \frac{5.3}{12} \quad \frac{4.7}{6} \quad 4.7 \quad \frac{5.3}{8} \quad \frac{5.0}{10} \quad \frac{4.6}{17} \quad \frac{4.8}{30} \quad \frac{4.7}{50}$$

$$\frac{5.0}{50} \quad \frac{4.7}{30} \quad \frac{4.3}{20} \quad \frac{4.7}{13} \quad \frac{5.1}{12} \quad \frac{4.5}{6} \quad 4.3 \quad \frac{4.5}{7} \quad \frac{4.9}{9} \quad \frac{4.1}{11} \quad \frac{4.1}{30} \quad \frac{4.1}{50}$$

$$\frac{4.4}{50} \quad \frac{4.0}{30} \quad \frac{3.6}{20} \quad \frac{3.6}{15} \quad \frac{4.7}{11} \quad \frac{4.3}{5} \quad 4.2 \quad \frac{4.4}{7} \quad \frac{4.6}{9} \quad \frac{3.8}{12} \quad \frac{3.7}{30} \quad \frac{3.6}{50}$$

$$\frac{4.7}{50} \quad \frac{4.4}{30} \quad \frac{3.7}{17} \quad \frac{4.7}{14} \quad \frac{4.9}{11} \quad \frac{4.5}{6} \quad 4.5 \quad \frac{4.9}{9} \quad \frac{4.3}{11} \quad \frac{4.4}{30} \quad \frac{4.3}{50}$$

$$\frac{4.8}{50} \quad \frac{4.7}{30} \quad \frac{4.2}{20} \quad \frac{5.0}{17} \quad \frac{4.8}{8} \quad 4.7 \quad \frac{5.4}{9} \quad \frac{4.7}{11} \quad \frac{4.5}{18} \quad \frac{4.9}{30} \quad \frac{4.8}{50}$$

$$\frac{5.1}{50} \quad \frac{4.8}{30} \quad \frac{4.7}{28} \quad \frac{5.2}{24} \quad 4.9 \quad \frac{5.2}{9} \quad \frac{5.1}{19} \quad \frac{4.8}{20} \quad \frac{5.1}{30} \quad \frac{5.4}{50}$$

$$\frac{5.3}{50} \quad \frac{5.1}{30} \quad 5.0 \quad \frac{5.1}{12} \quad \frac{5.8}{25} \quad \frac{5.9}{30} \quad \frac{6.1}{50}$$

Sta	+	Δ	-	Elev
		938.84		
16+83 ⁵⁰		Δ Sixth	33.8	
BM		2.98	935.86	935.81

Lt

2

Rt

16

$$\frac{5.2}{50}$$

$$\frac{5.0}{30}$$

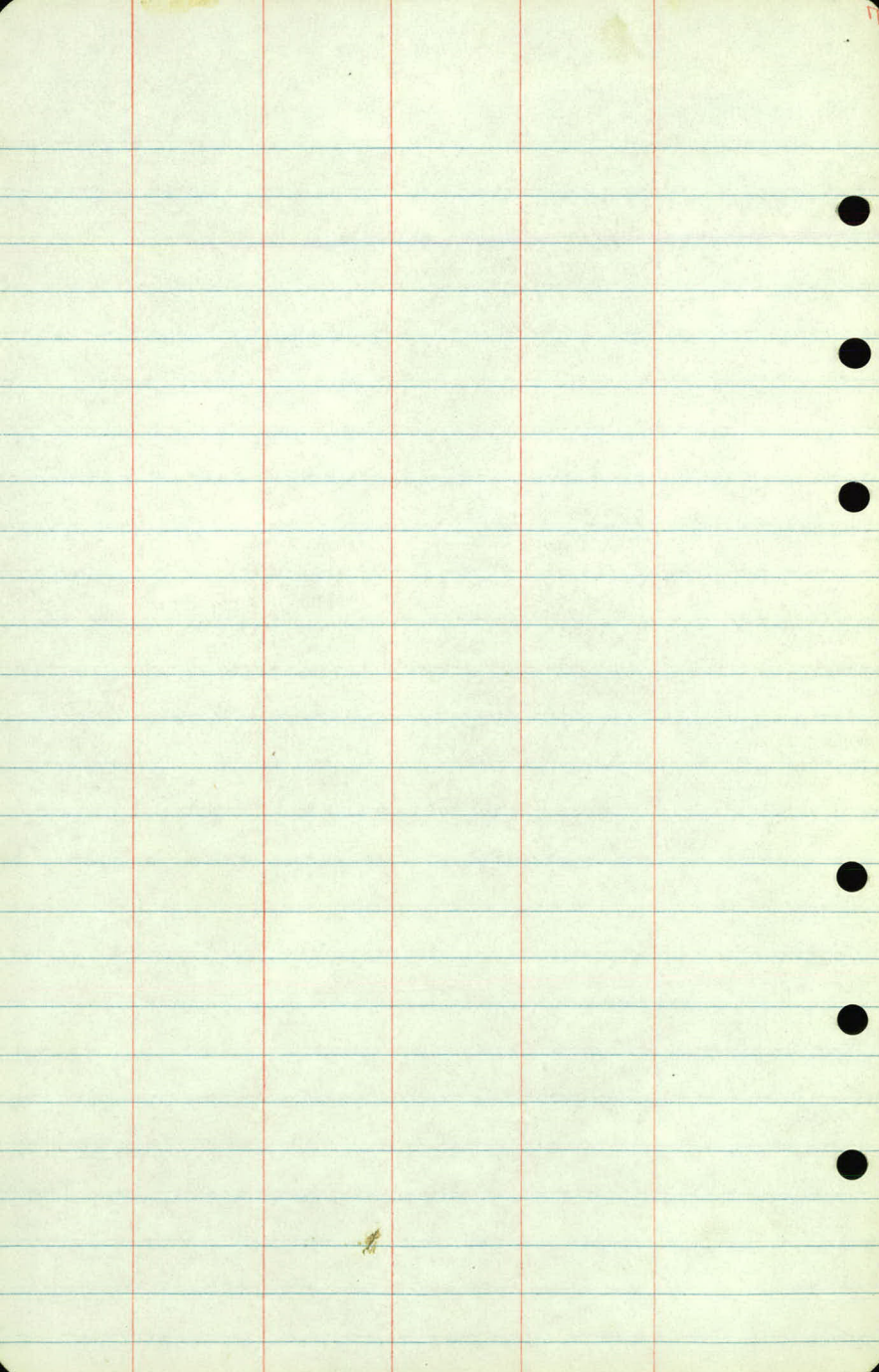
5.0

$$\frac{5.4}{30}$$

$$\frac{5.8}{50}$$

$$\frac{6.4}{100}$$

Top N.W Cor Btm Conc Step Ho S.E Cor Int



Drainage Recommendations

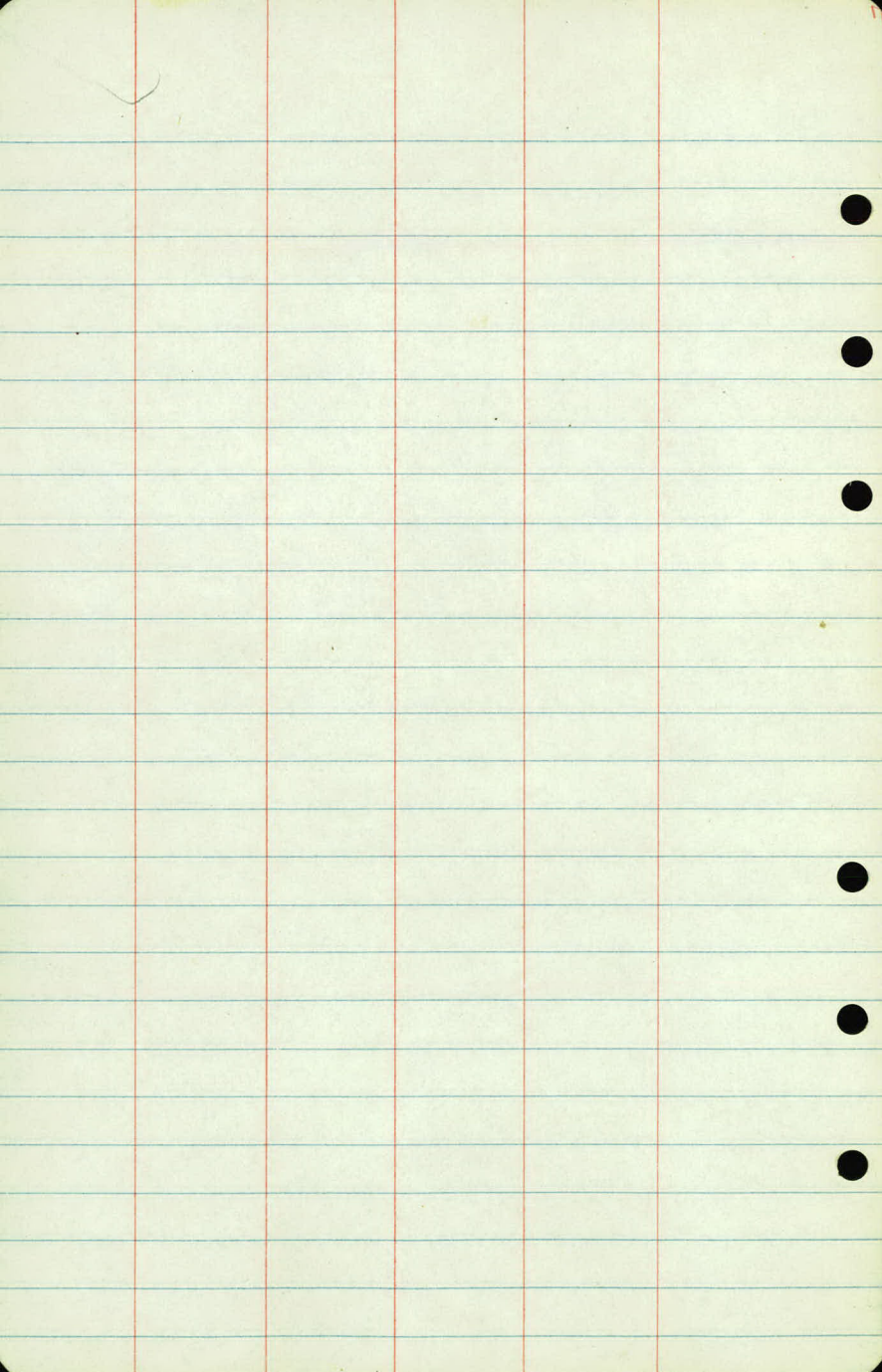
Third Str Int can be
regraded & Water taken East
To Bald Eagle Ave

Drainage Sta 0+00 to Third Str Int
Should be Carried To Sta 0+00

Drainage No From Third St Carried
To Fourth Str. to Storm Sewer in place

Drainage Sta 10+00 to 16+00 Carried
To Fourth Str Int East side To
Drop inlet West side to Gutter
line of Fourth Str Thence 171' West
to X Drain under Fourth Str which
Taps Storm Sewer on South side
of Fourth

Sta 16+00 North T. Int Carried
East on Sixth if desirable



Photomicrograph

Profile Levels

Third Str

+ Sixth Str.

Sta + $\bar{A}$ - Elev

B.M. 2.12 939.11 936.99

34.0

0+00 = $\frac{1}{2}$ Campbell 11 Sta runs Elev

+50

34.5

1

34.4

+50

33.4

2

33.7

+50

33.6

3

33.9

+50

34.0

4

33.9

+50

33.7

5

33.4

+50

33.5

~~6~~

Top Hyd, N.E. Cor Third & Campbell

5.1

4.6

4.7

5.7

5.4

5.5

5.2

5.1

5.2

5.4

5.7

5.6

Sta	+	π	-	Elev
B.M.	2.90	938.76		935.86

0+00 = Δ Campbell

+50

1

+50

2

+50

3

+50

4

+50

5

+50

* Profile West

* Profile East

Top N.W. Cor Btm Step.

33.9 4.9

4.9 33.9

33.8 5.0

5.9 33.1

33.8 5.0

5.7 33.1

33.7 5.1

5.9 32.9

33.7 5.1

5.9 32.9

33.8 5.0

6.0 32.8

33.3 5.5

6.1 32.7

33.1 5.7

6.5 32.3

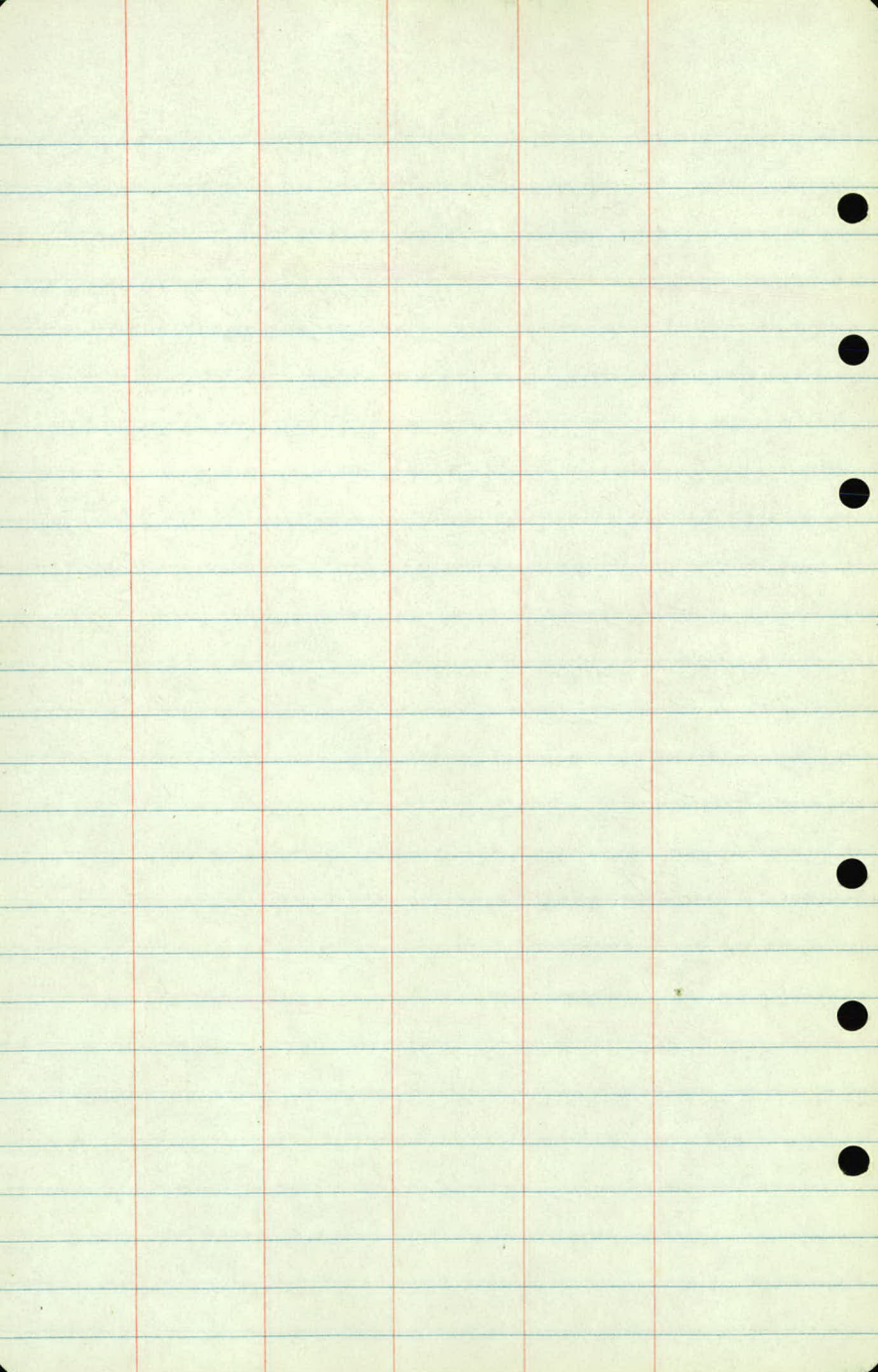
32.9 5.9

6.6 32.2

6.3 32.5

5.8 33.0

5.6 33.2



Profile Levels

Campbell Ave

4th to 6th

10-16-51

HAW

LC

MB

Rec'd. 10-19-51

Drawn up 10-24-51
R.B.

Sta	+	↑	-	Elev
B.M	3.43	939.29		935.86
	4.43	938.19	5.53	933.10
0+00	2	Fourth		33.0

+20

+30 Top Walk Rt + Lt 32.9

+50 32.9

1 33.0

+50 33.2

2 33.2

+50 33.1

LT * Rt

✓

Top N.W. Cor Bo H. Step Front Ho S.E. cor 6th & Campbell

5.2

32.0

$\frac{62}{28}$ Inlet C.B.

Top Walk $\frac{32.73}{165}$

5.3

$\frac{33.24}{165}$ Top Walk

Gr Ho. Lt $\frac{34.4}{3.8}$

5.3

Ho $\frac{33.19}{5.00}$

5.2

Gr Ho $\frac{34.4}{3.8}$ ✓

5.0

5.0

5.1

Sta + π - Elev
93819

2+67 Conc Walk Lt + House 33.2

3 33.2

+33 Ho Rt + Lt

+50 33.5

+72 Top MH 33.76

4 33.9

+13 Conc Walk + Ho Rt

+50 34.1

Lt.

L

Rt

33.63

33.00

Ho
4.565.19
76

50

50

34.9

3333.39
480

4.7

4.3

4.3

34.65

Walk

3.54
23.5

35.01

3.18

41

Sta + π - Elev

938.19

4+60 Conc Walkway 34.0

+75 34.0

5 34.0

+50 Ho Rt 33.9

6 34.2

T.P. 5.07 939.25 4.01 934.18

+50 34.3

+75 34.3

7 34.3

Lt

Z

Rt

34.30
Walk

42

389
235

34.98

Ho

42

3.21

42

35.08

Ho

43

3.11

40

5.0

35.18

Ho

5.0

4.07

5.0

Sta + π — Elev

934.25

7451

33.9

B.M

3.41 93584 93586

Lt

2

Rt

54

Top N.W. Cor. B&H Stop S.E. Cor. Campbell St & Sixth St

