

BK 39 Dr 14

755
45.2
30.3

OFFICE OF COUNTY ENGINEER
RAMSEY CO. MINN.

Plan.....Survey

Miller Ave

From 2nd St. To 5th St.

Road Acc't. No.....

Date Filed.....

File.....

PLAN SURVEY
MILLER AVE.
2nd St to 5th St

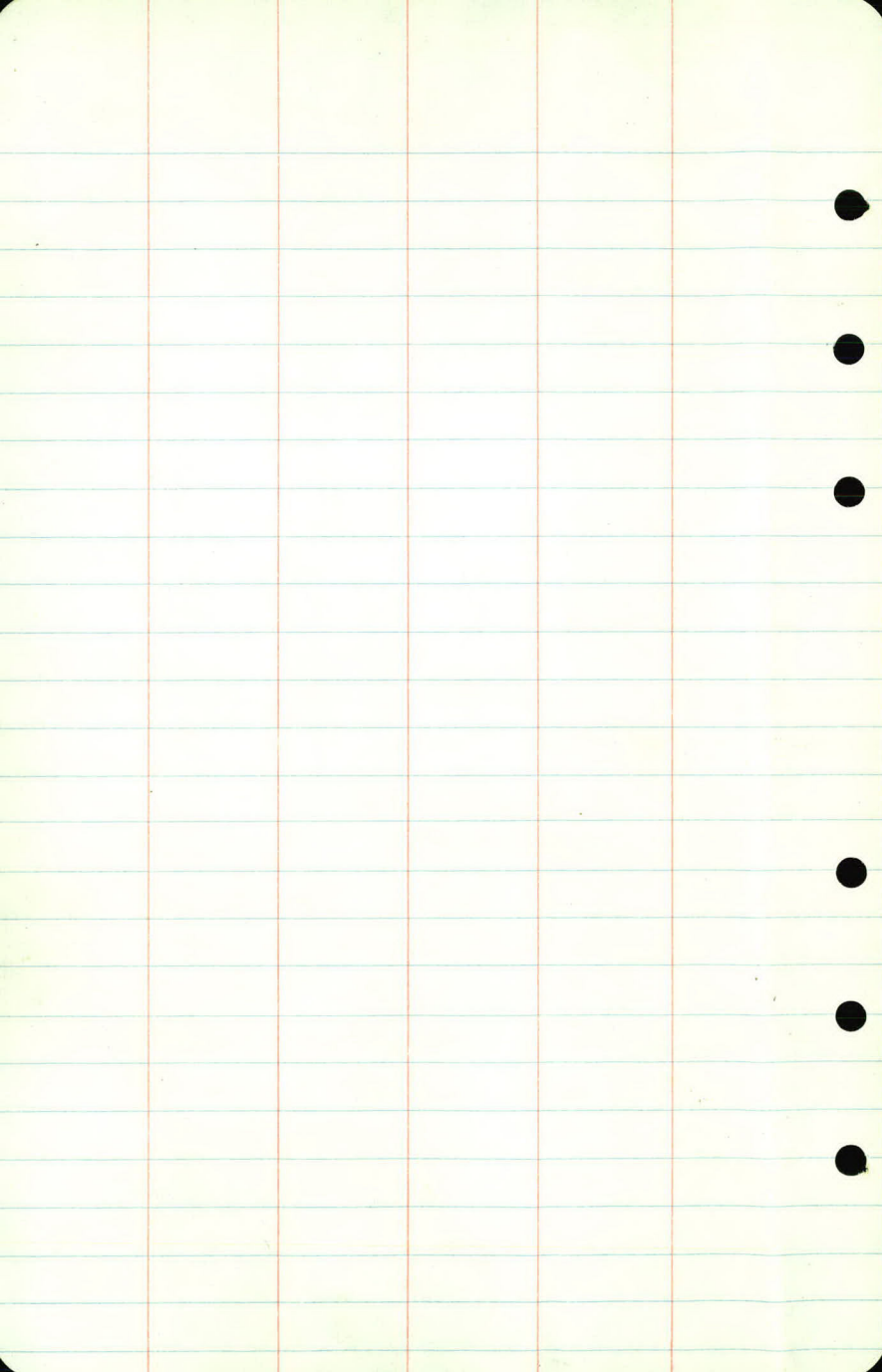
INDEX

Align. 1-2

Topog. 3-5

Xsections 6-10

Completed 5-13-41



1

Alignment

Sta	Point	ΔL	ΔR
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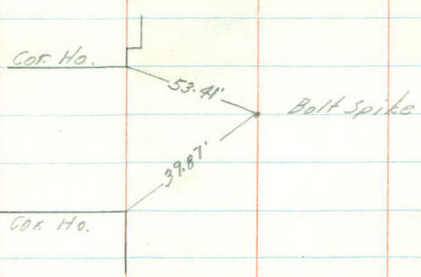
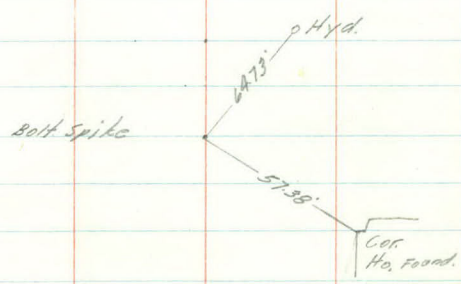
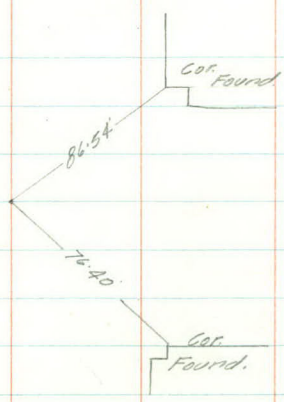
11	+39.35 = & Fifth St		
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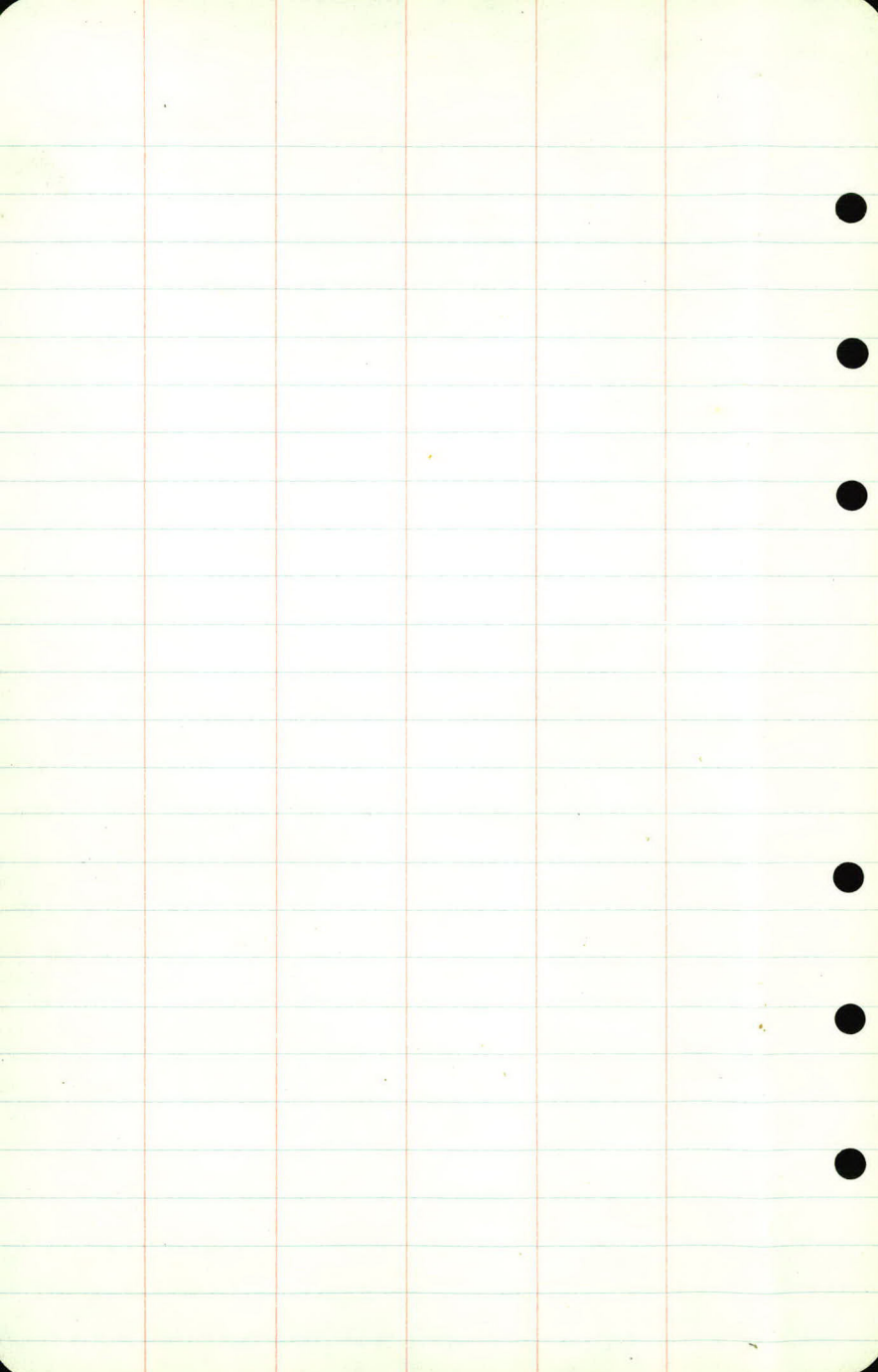
7	+50.94 P.O.T. = & Fourth St (Split of Cords on 4 th St)		
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3	+61.10 P.O.T. = & Third St		
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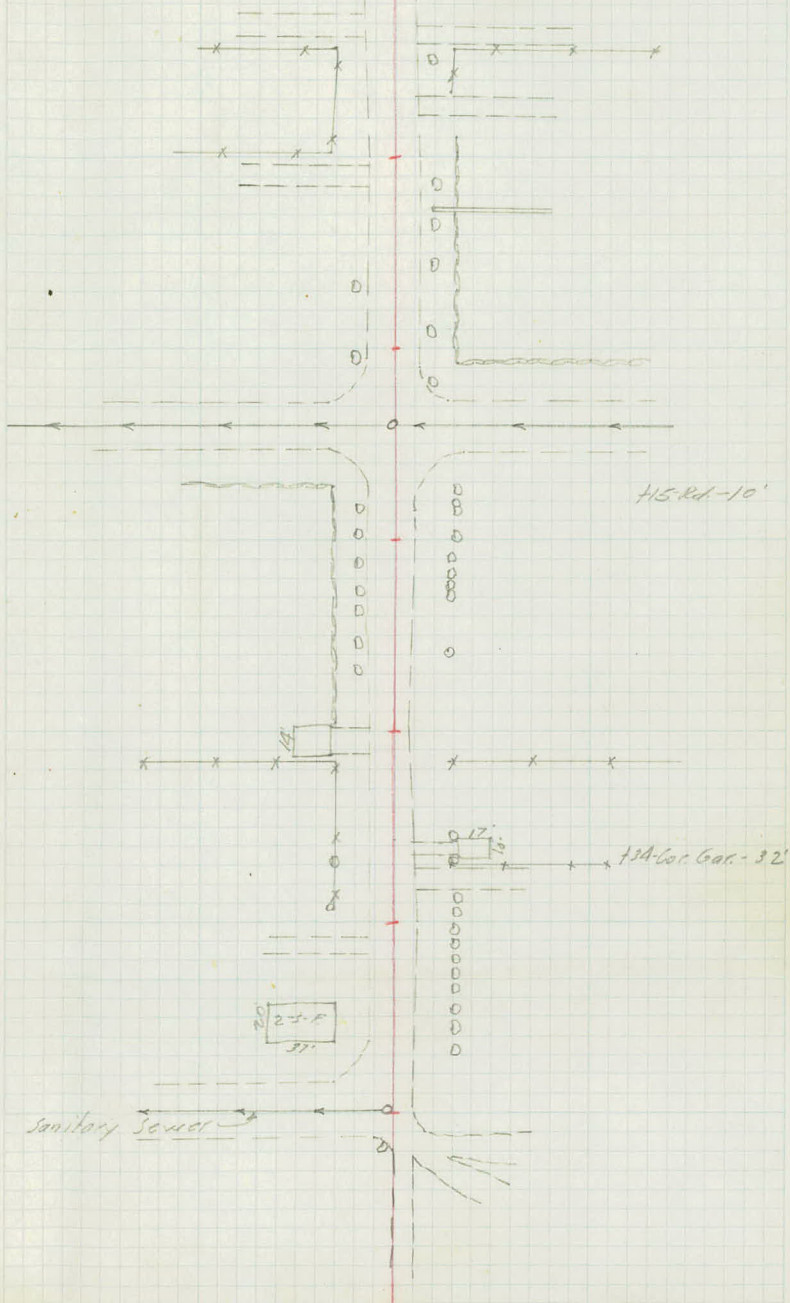
3	+31.10 P.I.	0°26 1/2'	
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0	+00 = & Second St		
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Topography.



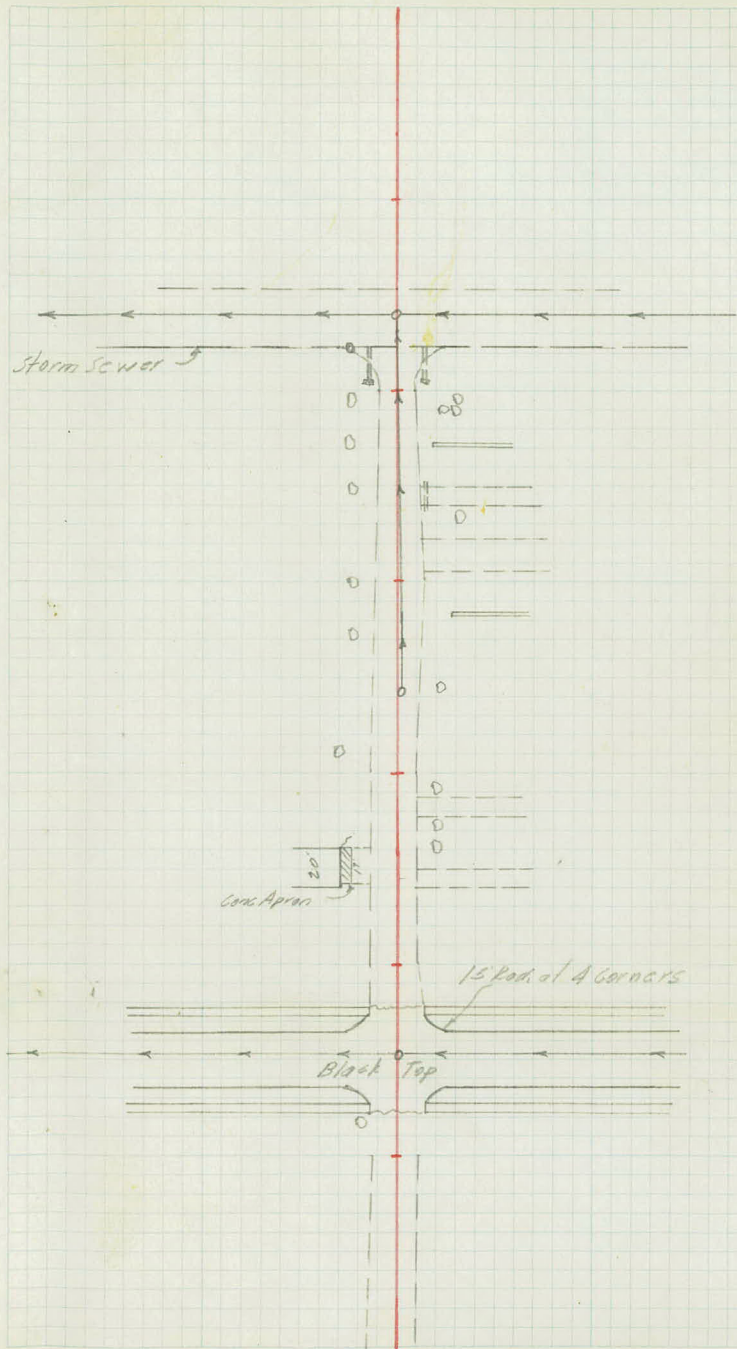
+40-M.H.-0.4' +23-M.H.-23' +1510° Elm-23' 6" x 3' Cor. H. W. +04-End 12° Vix-15.5'	+53-End Sec. Top. Rd	+22-30' 23-123 +05-4" Ash-31' 6" x 2.7' Cor. H. W. +045-End 12° Vix-14.2'
11	10'	9' +96-5° Elm-22.5' +90-30° Maple-23'-3° Elm-30' +71-2.5' Walk-28.8'
+96-18° Elm-24' +73-18° Elm-25' +49-20° Elm-24'		+45-4 Drive. 15' x 14' 6" 14' +34-18° Elm-31' +27-P.P.-22.5' +14-2 Double Drive
10 15° Elm-24'	12'	13'
+77-24° Elm-23.5'		+84-23° wide Walk-29.5' +47-35° Maple-22' +115-M.H.-1.7'
9 +11-24° B.E.-31'	14'	9' +29-PP-21'
+41-Cor. Cor-29.6'		+92-2° Elm-20' +82-4 Drive +74-4° Elm-20' +62-4° Elm-20' +45-4 Drive
8	14' 10'	+78.9-Cor. S.W.-13.9' +78-End Bl. Top. +78.9-Cor. S.W. + End Curb-13.5' +72-P.P. 20.5 +65.9-82.9 Curb Road-26.8' +65.9-82.9 Curb Road-25.4' +51.3-M.H.-0.7' +35.9-End Curb Road-26.2' +28-Cor. S.W. + 82.9 Curb-13.7' +22-Cor. S.W.-13.9'
7	14' 11'	
+48-4 Drive +23-PP-21'		+81-4 Drive +21-2° Pine-31.5' +10-PP-21'
6	16' 10'	

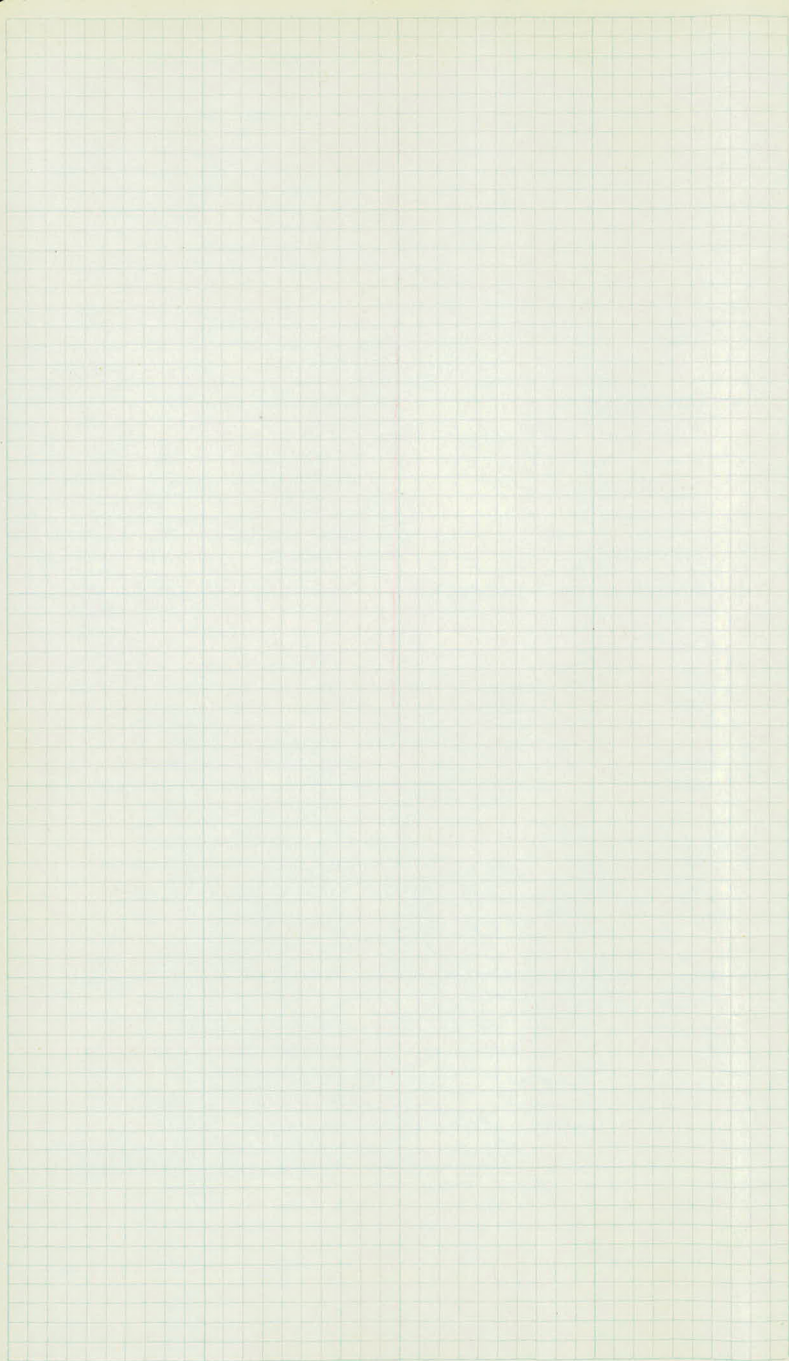
Storm Sewer

20'
Cons. Apron

15' Radi. of 4 Corners

Block Top





X sections

Sta.	+	-	Elev.
B.M.	6.68	939.97	(933.29)
B.M.	4.96	943.70	1.23 938.74
0	100	Also M.H.	38.74
	+30		38.9
	+50		38.2
1			38.6
	+50		38.4 ✓
T.P.	6.21	944.37	5.54 938.16
2			38.17
	+50		38.47
3			38.97
	+31.1		39.47
	+60	M.H.	
	61.1		39.57

Lt

4

Rt

U.S.G.S. B.M. in St. Mary School Yard.

2nd St. ? - W.B.

Top No. Edge M.H. Rinn 1st St. Miller Ave.

$\frac{83}{150} \frac{18}{100} \frac{6.2}{50} \frac{13.41}{FL.} \frac{4.96}{Top} \frac{4.8}{11} \frac{5.2}{17} \frac{5.2}{26} \frac{3.5}{34} \frac{3.2}{50}$

$\frac{63}{50} \frac{53}{30} \frac{50}{22} \frac{53}{17} \frac{60}{13} \frac{48}{20} \frac{51}{25} \frac{46}{30} \frac{31}{30} \frac{2.4}{50}$

$\frac{4.9}{30} \frac{50}{16} \frac{56}{11} \frac{55}{21} \frac{50}{25} \frac{49}{32} \frac{2.4}{50} \frac{2.6}{50}$

$\frac{56}{50} \frac{4.9}{30} \frac{51}{12} \frac{51}{22} \frac{53}{27} \frac{50}{31} \frac{38}{34} \frac{38}{44}$

$\frac{56}{50} \frac{5.2}{30} \frac{55}{12} \frac{53}{10} \frac{54}{30} \frac{51}{L.O.}$

Gar. floor $\frac{6.14}{33} \frac{6.4}{21} \frac{6.2}{7} \frac{6.1}{20} \frac{6.5}{26} \frac{5.7}{30} \frac{5.8}{30} \frac{6.0}{50}$

$\frac{5.9}{30} \frac{6.2}{23} \frac{6.5}{21} \frac{5.9}{21} \frac{6.2}{26} \frac{5.8}{30} \frac{6.1}{30} \frac{5.9}{50}$

$\frac{4.4}{41} \frac{4.5}{30} \frac{5.7}{27} \frac{5.8}{18} \frac{5.4}{20} \frac{5.7}{24} \frac{5.1}{30} \frac{5.0}{30} \frac{4.8}{50}$

$\frac{5.6}{50} \frac{4.5}{30} \frac{5.4}{27} \frac{5.2}{16} \frac{5.6}{13} \frac{4.9}{16} \frac{5.6}{25} \frac{5.2}{30} \frac{4.7}{30} \frac{4.6}{50}$

$\frac{14.87}{FL.} \frac{4.82}{Top}$

$\frac{80}{200} \frac{76}{150} \frac{6.9}{100} \frac{6.3}{50} \frac{4.8}{50} \frac{5.1}{50} \frac{5.3}{100}$

Sta	+	π	-	Elev.
		944.37		
3	+91.1			38.77 ✓
B.M.			1.50	942.87
4				38.47
	+50			38.27
5				38.07
	+50			38.07 ✓
T.P.	4.11	941.66	6.82	937.55
6				37.56
	+50			36.86
7				36.86
	+21.8			36.66
	+25.9			36.31
	+50.9 also M.H.			
B.M.	0.88	941.55	0.99	940.67

Lt

R

Rt

38.47

39.37

$\frac{62}{50}$	$\frac{52}{30}$	$\frac{55}{17}$	$\frac{59}{13}$	$\frac{56}{11}$	$\frac{59}{20}$	$\frac{51}{30}$	$\frac{50}{50}$	$\frac{47}{50}$
-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------

38.27

Top Hyd. N.E. Cor. 3rd St. & Miller Ave.

39.27

$\frac{63}{50}$	$\frac{41}{30}$	$\frac{55}{23}$	$\frac{62}{13}$	$\frac{59}{11}$	$\frac{60}{13}$	$\frac{52}{30}$	$\frac{51}{50}$	$\frac{48}{50}$
-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------

37.97

38.47

$\frac{63}{50}$	$\frac{64}{30}$	$\frac{60}{22}$	$\frac{65}{13}$	$\frac{61}{12}$	$\frac{64}{15}$	$\frac{58}{50}$	$\frac{59}{50}$	$\frac{54}{50}$
-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------

38.37

38.67

$\frac{62}{50}$	$\frac{60}{30}$	$\frac{45}{12}$	$\frac{63}{11}$	$\frac{65}{14}$	$\frac{57}{30}$	$\frac{57}{50}$
-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------

37.87

38.57

$\frac{67}{50}$	$\frac{65}{30}$	$\frac{67}{13}$	$\frac{63}{12}$	$\frac{67}{14}$	$\frac{61}{50}$	$\frac{58}{50}$	$\frac{58}{50}$
-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------

37.76

38.06

$\frac{39}{30}$	$\frac{45}{17}$	$\frac{41}{11}$	$\frac{45}{14}$	$\frac{39}{30}$	$\frac{36}{50}$	$\frac{37}{50}$
-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------

36.96

37.46

$\frac{49}{50}$	$\frac{47}{30}$	$\frac{46}{22}$	$\frac{50}{16}$	$\frac{48}{11}$	$\frac{48}{17}$	$\frac{42}{30}$	$\frac{42}{50}$	$\frac{43}{50}$
-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------

36.66

36.96

$\frac{53}{50}$	$\frac{50}{30}$	$\frac{51}{14}$	$\frac{48}{11}$	$\frac{51}{20}$	$\frac{47}{30}$	$\frac{47}{50}$	$\frac{45}{50}$
-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------

36.63

36.93

$\frac{512}{50}$	$\frac{503}{30}$	$\frac{500}{14}$	$\frac{520}{14}$	$\frac{50}{14}$	$\frac{517}{14}$	$\frac{484}{14}$	$\frac{473}{30}$	$\frac{453}{50}$
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Curb

36.62

Gutter

36.08

36.39

36.88

Curb

$\frac{5.30}{50}$	$\frac{5.04}{26.3}$
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$\frac{5.81}{50}$	$\frac{5.58}{26.3}$
-------------------	---------------------

$\frac{5.35}{26.2}$	$\frac{5.27}{50}$	$\frac{5.14}{50}$
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$\frac{4.78}{26.2}$	$\frac{4.68}{50}$
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36.86

$\frac{4.80}{Top}$	$\frac{12.17}{F.L.}$
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Top Hyd. N.E. Cor. 4th St. & Miller Ave

Sta	+	π	-	Elev
		941.55		
7	+65.9			36.39
	178.9			36.92
8				37.05
	+50			37.05
9				36.45
	+41.5 M.H.			
	+50			36.15
10				35.85
T.P.	4.83	940.67	5.71	935.84 ✓
	+50			35.77
11				35.97
	+0.4			36.07

Lt

R

Rt

(carb 36.62)
 $\frac{5.08}{50} \frac{4.93}{26.8}$

36.46 butter 36.48
 $\frac{5.60}{50} \frac{5.39}{26.8} \frac{5.16}{25.4} \frac{5.07}{50} \frac{5.02}{50}$

(carb 37.02)
 $\frac{4.53}{25.4} \frac{4.52}{50}$

37.09
 $\frac{4.70}{50} \frac{4.46}{30} \frac{4.47}{13.8} \frac{4.84}{13.8} \frac{4.63}{13.8} \frac{4.78}{13.8} \frac{4.45}{13.8} \frac{4.45}{30} \frac{4.38}{50}$

37.15
 $\frac{4.6}{50} \frac{4.4}{30} \frac{4.3}{17} \frac{4.7}{16} \frac{4.5}{13} \frac{4.8}{14} \frac{4.5}{30} \frac{4.4}{30} \frac{4.1}{50}$

(Gar Floor) 37.38
 $\frac{4.17}{29.5}$

(Gar. Area) 37.28
 $\frac{4.27}{25.0} \frac{4.4}{10} \frac{4.5}{13} \frac{4.8}{15} \frac{3.9}{30} \frac{3.9}{30} \frac{3.8}{50}$

36.45
 $\frac{5.1}{50} \frac{5.1}{30} \frac{5.1}{17} \frac{5.6}{14} \frac{5.1}{13} \frac{5.2}{15} \frac{4.6}{30} \frac{4.4}{30} \frac{4.3}{50}$

36.13
 $\frac{5.42}{Top} \frac{12.83}{F.L.}$

36.05
 $\frac{5.1}{50} \frac{5.5}{30} \frac{6.2}{14} \frac{5.4}{12} \frac{5.7}{15} \frac{5.3}{30} \frac{5.6}{30} \frac{5.9}{50}$

35.95
 $\frac{5.5}{50} \frac{5.6}{30} \frac{6.5}{14} \frac{5.7}{14} \frac{6.0}{30} \frac{5.8}{30} \frac{5.7}{50}$

35.67
 $\frac{4.8}{50} \frac{5.0}{30} \frac{5.1}{17} \frac{5.6}{13} \frac{4.9}{12} \frac{4.9}{14} \frac{5.7}{16} \frac{4.8}{30} \frac{4.6}{30} \frac{4.5}{50}$

35.77
 $\frac{4.9}{50} \frac{4.9}{30} \frac{4.8}{19} \frac{6.1}{15} \frac{5.4}{13} \frac{4.7}{12} \frac{5.0}{14} \frac{5.6}{18} \frac{4.2}{30} \frac{4.3}{30} \frac{4.3}{50}$

35.87 34.15 (V.I.) 34.82 36.47
 $\frac{5.0}{50} \frac{4.8}{30} \frac{4.7}{19} \frac{6.52}{15.3} \frac{5.4}{13} \frac{4.6}{12} \frac{5.0}{13.5} \frac{5.85}{18} \frac{4.1}{30} \frac{4.2}{30} \frac{4.2}{50}$

sto + x - E/cr.

940.67

11 +09.35

36.17

+23 M.H.

+39.35 Also M.H.

36.27

B.M.

1.83

938.84

B.M.

4.29

936.38

(936.41)

Lt.

K

Rt.

35.77

36.27

50	49	49	53	45	49	41	44	43
50	30	18	19	9	14	30	50	

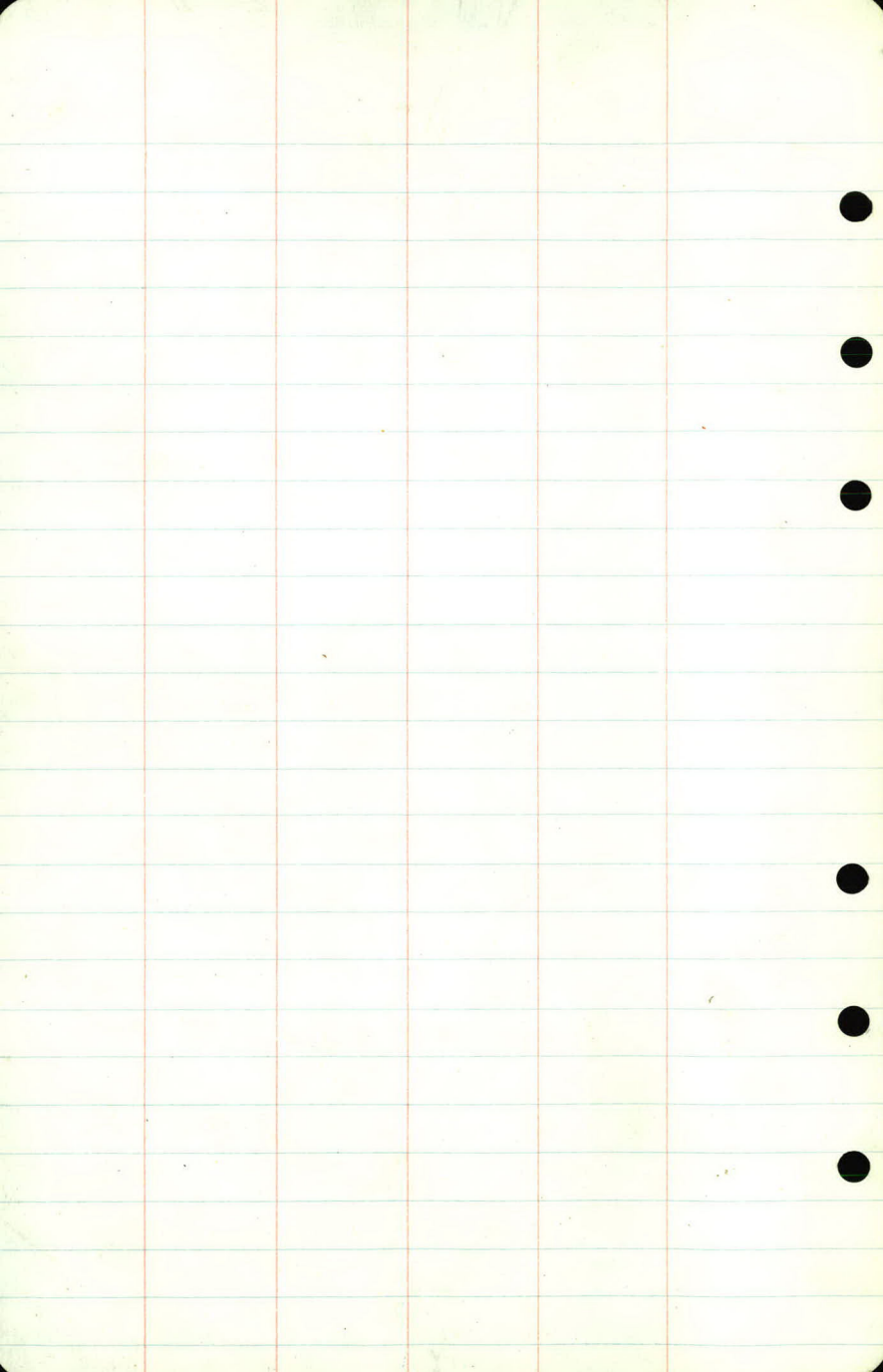
35.64

10.92	5.03
FL.	Top

51	49	15.85	4.40	46	43
100	50	FL.	Top	50	100

Top Hyd. N.W. Cor. 5th St. & Miller Ave

Spt 10 RR N. Side Murray Ave & 5th St.



Curb Stakes
Miller Ave.

Sta	+	π	-	Grade
B.M.	460	943.34		(938.74)
0	+00			
	+30			38.0
	+50			38.03
	+55			38.04
	+75			38.06
	+78.5			
	+80			
1	+00			38.09
	+99			
1	+13			38.11
	+25			38.12
	+49			38.18
	+75			38.19
	+84			38.20
2				38.23

Gr. Rod Lt E Rt

Top N. Edge M. H. Rim Miller 1st 2nd

5.34 ✓

5.31 ✓

5.30 ✓

5.28 ✓

5.25 ✓

5.23 ✓

5.22 ✓

5.18 ✓

5.15 ✓

5.14 ✓

5.11 ✓

Sta	+	π	-	Grade
-----	---	-------	---	-------

943.34

2 +04

38.23

+25

38.26

+50

38.29

+75

38.32

3

38.35

+31.1

38.39

B.M.	0.76	943.63	0.46	942.88	(942.87)
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+91.1

B.M.

0.11

942.98

942.87

4

+25

+50

+75

10-29-41
K.F.
L.G.
M.B.
G.F.

Gr. Rod.	Lt.	Gr. Rod	Gr. Rod	Gr. Rod
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5.11 ✓

5.08 ✓

5.05 ✓

5.02 ✓

4.99 ✓

4.95 ✓

Top Hyd. N.E. Cor. 3rd & Miller Ave.

5.23 ✓	38.4	38.4	5.23 ✓
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✓ 4.63	38.35	38.36	✓ 4.62
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✓ 4.76	38.22	38.25	✓ 4.73
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✓ 4.89	38.09	38.14	✓ 4.84
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✓ 5.02	37.96	38.03	✓ 4.95
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Sta.	+	π	-	Grade
------	---	-------	---	-------

		942.98		
--	--	--------	--	--

4	+84			
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5				
---	--	--	--	--

	+04			
--	-----	--	--	--

	+16			
--	-----	--	--	--

	+25			
--	-----	--	--	--

	+36			
--	-----	--	--	--

	+50			
--	-----	--	--	--

	+54			
--	-----	--	--	--

	+58			
--	-----	--	--	--

	+74			
--	-----	--	--	--

	+78			
--	-----	--	--	--

Lt	Grade	Grade	et.
Gr. Rod	Gr. Rod	Gr. Rod	Gr. Rod

✓ 5.06	37.92		
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	37.83	37.92	5.06 ✓
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✓ 5.16	37.82		
-----------	-------	--	--

		37.85	5.13 ✓
--	--	-------	--------

✓ 5.28	37.70		
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		37.76	5.22 ✓
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✓ 5.41	37.57	37.70	5.28 ✓
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		37.68	5.30 ✓
--	--	-------	--------

✓ 5.45	37.53		
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		37.60	5.38 ✓
--	--	-------	--------

✓ 5.55	37.43		
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Sta.	+	π	-	Elev
------	---	-------	---	------

		942.98		
--	--	--------	--	--

6

I.P.	4.91	941.72	5.67	942.31
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+21

+25

+38

+41

+50

+58

+75

7

+20.94

B.M.	1.03	941.70	1.03	940.69
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+80.94

940.67

Lt	Gr. Red	Grade	Grade	Gr. Red
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✓	5.67	37.31	37.48	5.50 ✓
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			37.39	4.33 ✓
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✓	4.54	37.18		
---	------	-------	--	--

✓	4.60	37.12		
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			37.50	4.42 ✓
--	--	--	-------	--------

			37.26	4.46 ✓
--	--	--	-------	--------

	4.71	37.01		
--	------	-------	--	--

✓	4.80	36.92	37.15	4.59 ✓
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✓	4.9.3	36.79	37.04	4.68 ✓
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		36.68	36.95	
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Top Hyd. N.E. cor. 4th + Miller Ave.

		36.57	36.96	
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Sta.	+	π	-	Elev.
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		941.70		
--	--	--------	--	--

8

+25

+35

+39

+55

+66

+72

+75

+92

9

+25

TP	4.05	940.20	5.55	936.15
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Lt.	Grade	Grade	Rt.
Gr. Rod.	Grade	Grade	Gr. Rod.

✓ 5.18	36.52	36.88	✓ 4.82
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✓ 5.25	36.45	36.78	✓ 4.92
-----------	-------	-------	-----------

		36.73	✓ 4.97
--	--	-------	-----------

✓ 5.30	36.40		
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		36.65	✓ 5.05
--	--	-------	-----------

✓ 5.38	36.32		
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		36.58	✓ 5.12
--	--	-------	-----------

✓ 5.41	36.29		
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	36.29	36.50	✓ 5.20
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✓ 5.48	36.22	36.47	✓ 5.23
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3.73

✓ 5.55	36.15	36.37	✓ 5.33
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3.83

Sta.	+	π	-	Elev.
		940.20		

9 +50

+75

10

+25

+29

+35

+50

+55

+75

11

+09.35

B.M.

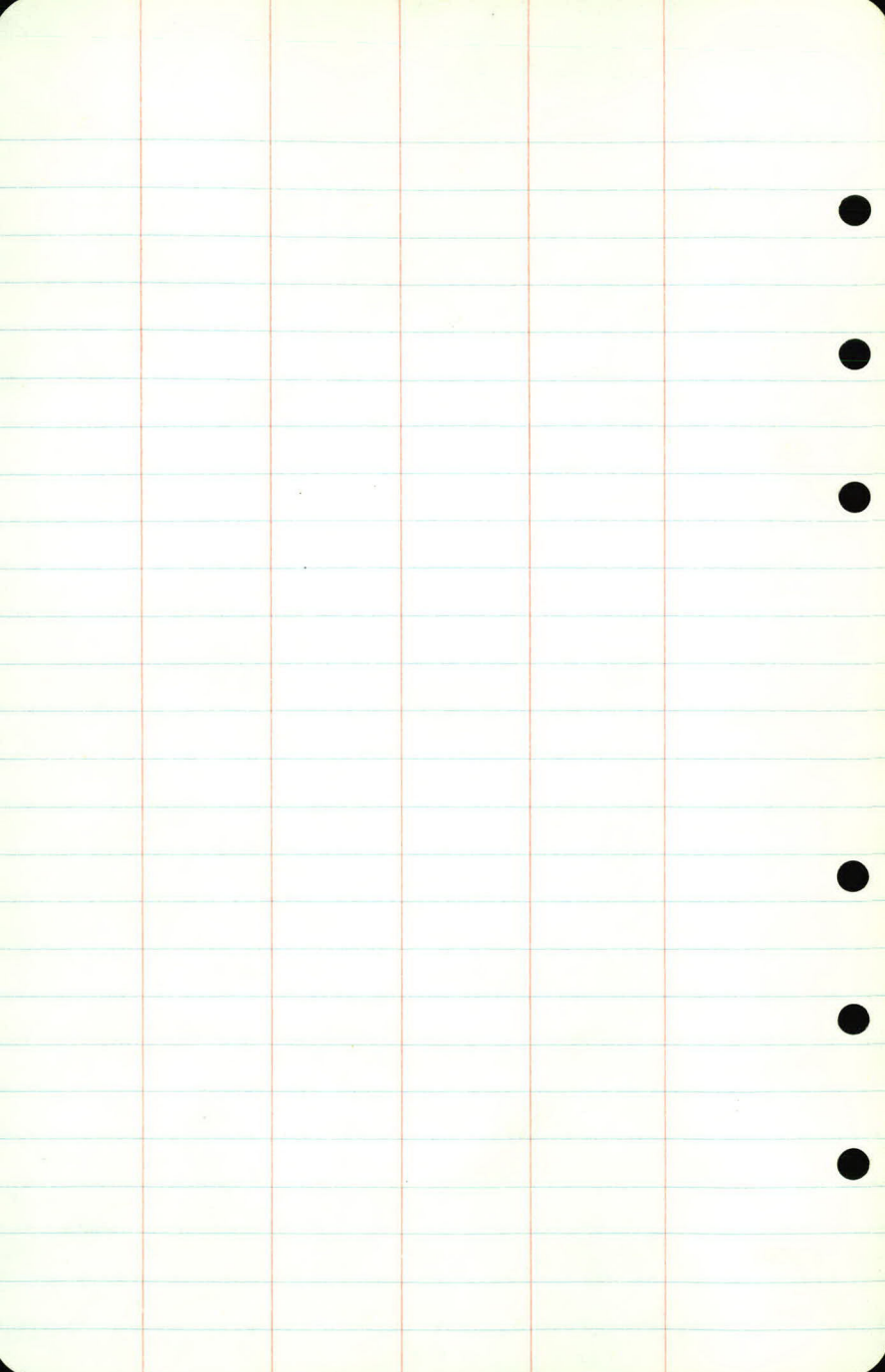
1.36

938.84

938.84

lt	Gr. Rod	Grande	Grande	Gr. Rod
✓	4.13	36.07	36.27	✓ 3.93
✓	4.20	36.00	36.17	✓ 4.03
✓	4.28	35.92	36.06	✓ 4.19
✓	4.35	35.85	35.95	✓ 4.25
			35.94	4.26
			35.92	✓ 4.28
✓	4.43	35.77		
			35.83	✓ 4.37
✓	4.50	35.70	35.75	✓ 4.45
✓	4.58	35.62	35.65	✓ 4.55
✓	4.59	35.61	35.59	✓ 4.61

Top Hyd N.W. Cor 5th + 19.112 r



Slope stakes
White Bear Ave.

Sta.	+	π	-	Elev.
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0	+25			
---	-----	--	--	--

	+70			
--	-----	--	--	--

1				
	+50			

4	+100			
---	------	--	--	--

	+50			
--	-----	--	--	--

	+75			
--	-----	--	--	--

5				
---	--	--	--	--

Lt

Av. 10' Lt.

$$20' / \frac{4.3}{1.1}$$

5.4

$$49.0' / \frac{2.6}{1.28}$$

5.4

$$49.0' / \frac{3.0}{1.23}$$

5.3

$$49.0' / \frac{15.0}{1.08}$$

5.3

$$26.1' / \frac{9.7}{2.09}$$

8.6

$$39.0' / \frac{5.6}{1.20}$$

8.6

$$47.4' / \frac{2.8}{1.58}$$

8.6

$$49.0' / \frac{2.8}{1.68}$$

8.6

5/2 + π - E/24

5 +90

+60

6

L

12

+37

+63

13

44 = Pr 1024.

$$49.0' / \frac{1.7}{46.9} \quad 8.6$$

$$49.0' / \frac{2.2}{46.3} \quad 8.5$$

$$36.0' / \frac{6.9}{42.0} \quad 8.4$$

$$27.6' / \frac{9.3}{41.2} \quad 8.2$$

$$28.5' / \frac{6.1}{40.5} \quad 5.6$$

$$34.8' / \frac{3.7}{41.6} \quad 5.3$$

$$32.7' / \frac{9.3}{40.9} \quad 5.2$$

$$25.8' / \frac{6.2}{40.6} \quad 4.9$$

5/9

+

π

-

E/cx

47 +50

48

+35

+65

49

+50

50

+50

+75

51

+35

Lt Pav. 10' Lt

$$30.3' / \begin{array}{r} 7.2 \\ +0.1 \\ \hline \end{array} \quad 7.2 \quad 6.9$$

$$38.1' / \begin{array}{r} 4.4 \\ +2.7 \\ \hline \end{array} \quad 6.9 \quad 6.5$$

$$42.2' / \begin{array}{r} 2.3 \\ +2.4 \\ \hline \end{array} \quad 6.6 \quad 6.3$$

$$38.4' / \begin{array}{r} 3.5 \\ +2.8 \\ \hline \end{array} \quad 6.2 \quad 5.9$$

$$30.9' / \begin{array}{r} 5.7 \\ +0.3 \\ \hline \end{array} \quad 5.9$$

$$29.1' / \begin{array}{r} 6.2 \\ +1.7 \\ \hline \end{array} \quad \underline{5.8}$$

$$27.3' / \begin{array}{r} 6.7 \\ +1.1 \\ \hline \end{array} \quad \underline{5.7}$$

$$37.2' / \begin{array}{r} 3.2 \\ +2.4 \\ \hline \end{array} \quad 5.6$$

$$40.5' / \begin{array}{r} 2.3 \\ +2.5 \\ \hline \end{array} \quad 5.8$$

$$41.1' / \begin{array}{r} 2.3 \\ +2.7 \\ \hline \end{array} \quad 6.0$$

$$37.5' / \begin{array}{r} 3.8 \\ +2.5 \\ \hline \end{array} \quad 6.3$$

Sta	+	π	-	Elev.
-----	---	-------	---	-------

51	+70			
----	-----	--	--	--

52				
----	--	--	--	--

	+42			
--	-----	--	--	--

56				
----	--	--	--	--

	+50			
--	-----	--	--	--

57				
----	--	--	--	--

	+50			
--	-----	--	--	--

58				
----	--	--	--	--

	+50			
--	-----	--	--	--

Lt.

PAV 10' Lt.

$$\frac{330' / 5.7}{41.0}$$

4.7

$$\frac{30.0' / 7.2}{42.0}$$

7.2

$$\frac{240' / 10.0}{42.0}$$

8.0

~~$$\frac{249' / 8.7 - 2.1}{40.0}$$~~

5.1

$$\frac{30.3' / 5.0}{40.1}$$

5.1

$$\frac{32.7' / 4.2}{40.9}$$

5.1

$$\frac{33.0' / 3.8}{41.4}$$

5.2

$$\frac{31.8' / 4.7}{40.6}$$

5.3

$$\frac{29.7' / 5.4}{41.9}$$

5.3

Sta.	+	π	-	Elev
------	---	-------	---	------

69	+70			
----	-----	--	--	--

70				
----	--	--	--	--

	+50			
--	-----	--	--	--

	+87			
--	-----	--	--	--

41	+20			
----	-----	--	--	--

41	+50			
----	-----	--	--	--

42				
----	--	--	--	--

	+50			
--	-----	--	--	--

	+75			
--	-----	--	--	--

Lt. Per 10 Lt.

$$\frac{33.0}{48.20} \frac{44}{4.4}$$

$$\frac{32.0}{122} \frac{28}{5.0}$$

$$\frac{33.0}{136} \frac{22}{5.8}$$

$$\frac{24.0}{200} \frac{83}{6.3}$$

$$\frac{34.2}{114} \frac{66}{8.0}$$

$$\frac{37.2}{124} \frac{55}{7.9}$$

$$\frac{45.0}{15.0} \frac{2.9}{7.9}$$

$$\frac{46.2}{15.9} \frac{25}{7.9}$$

$$\frac{24.6}{202} \frac{9.7}{7.9}$$

Sta.	+	-	Elev.
------	---	---	-------

62	+91		
----	-----	--	--

63	+50		
----	-----	--	--

64			
----	--	--	--

	+50		
--	-----	--	--

65			
----	--	--	--

	+50		
--	-----	--	--

66			
----	--	--	--

	+50		
--	-----	--	--

67			
----	--	--	--

LA P.M. 10:41

$$320' / \frac{46}{7.5} \quad r1 \quad 8.35 \quad 98$$

$$320' / \frac{88}{8.14} \quad r2 \quad 8.45 \quad 89$$

$$320' / \frac{4.2}{14.0} \quad r.2 \quad 8.45$$

$$320' / \frac{2.8}{15.5} \quad 8.3 \quad 85$$

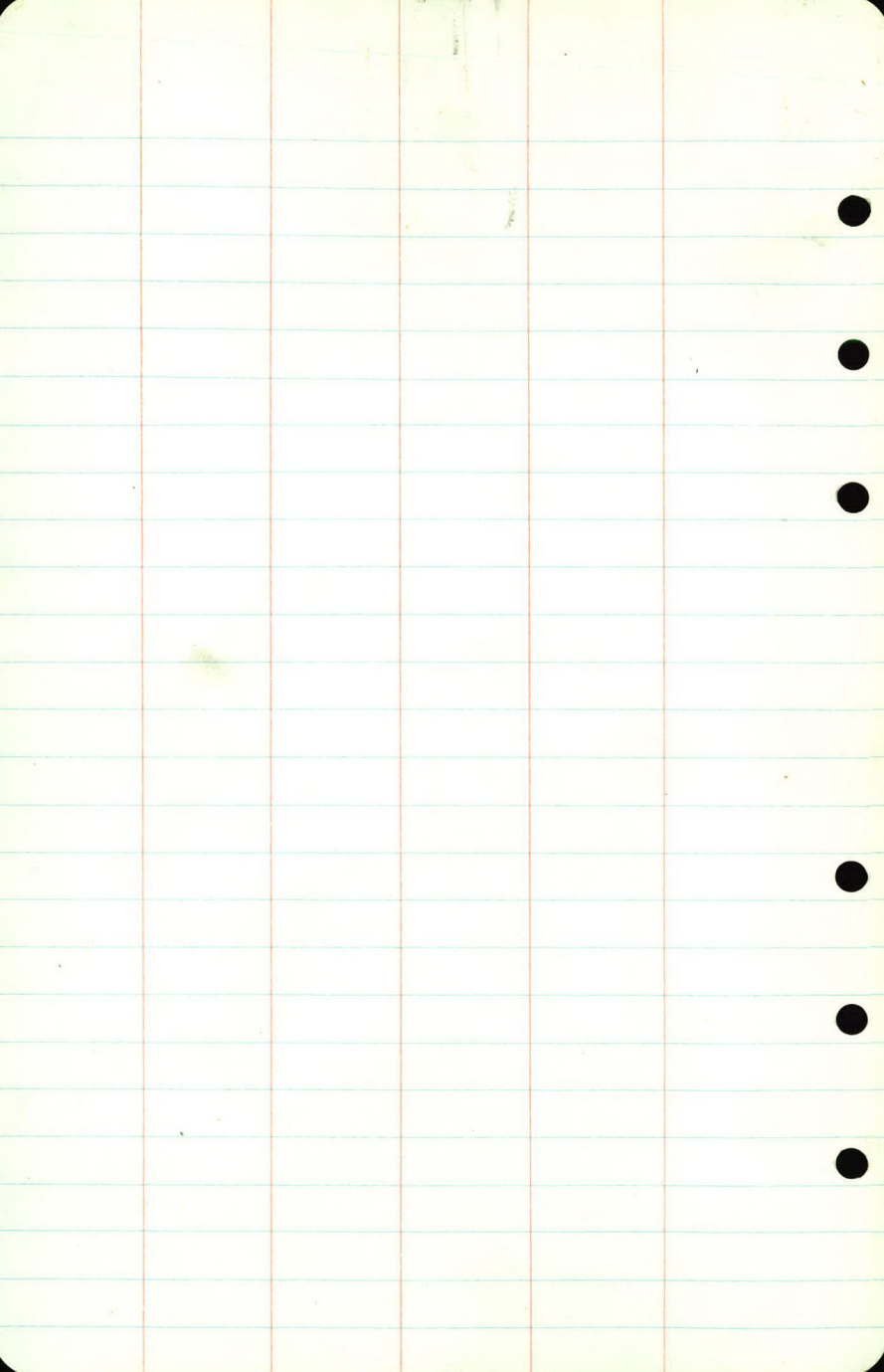
$$320' / \frac{70}{11.9} \quad 8.3 \quad 85$$

$$320' / \frac{38}{4.6} \quad 8.4 \quad 86$$

$$320' / \frac{57}{12.9} \quad 8.6 \quad 88$$

$$320' / \frac{27}{12.3} \quad 5.0 \quad 52$$

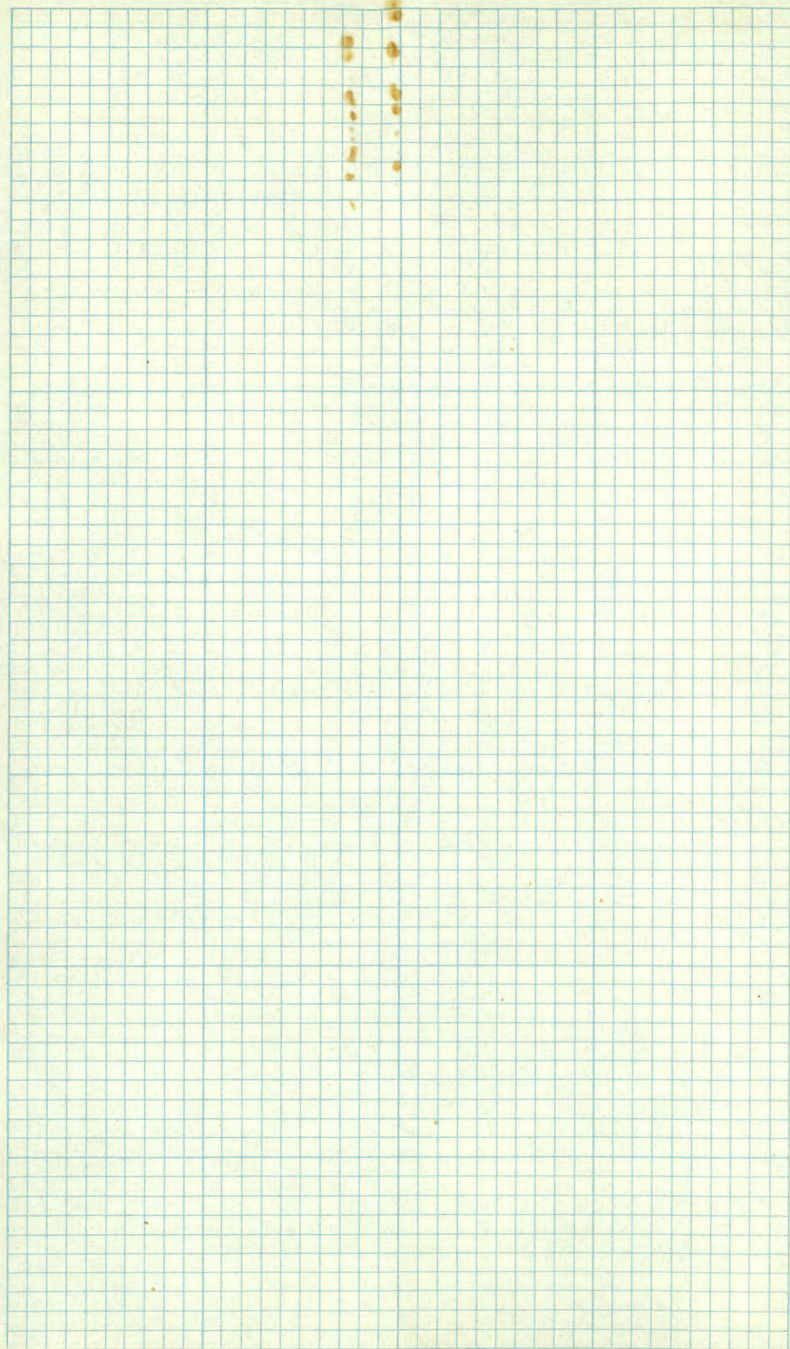
$$320' / \frac{60}{11.8} \quad 5.8 \quad 60$$



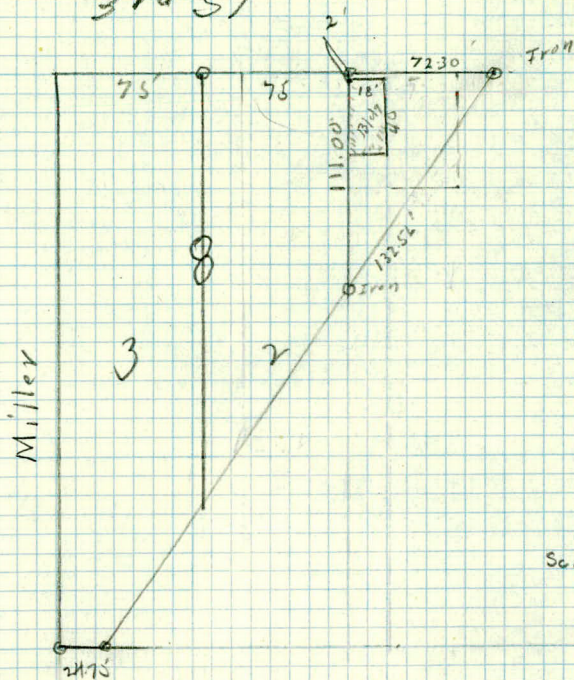
Property Line

Lot 1 Block 8

MURRAY'S Add
Ramaley Park
White Bear

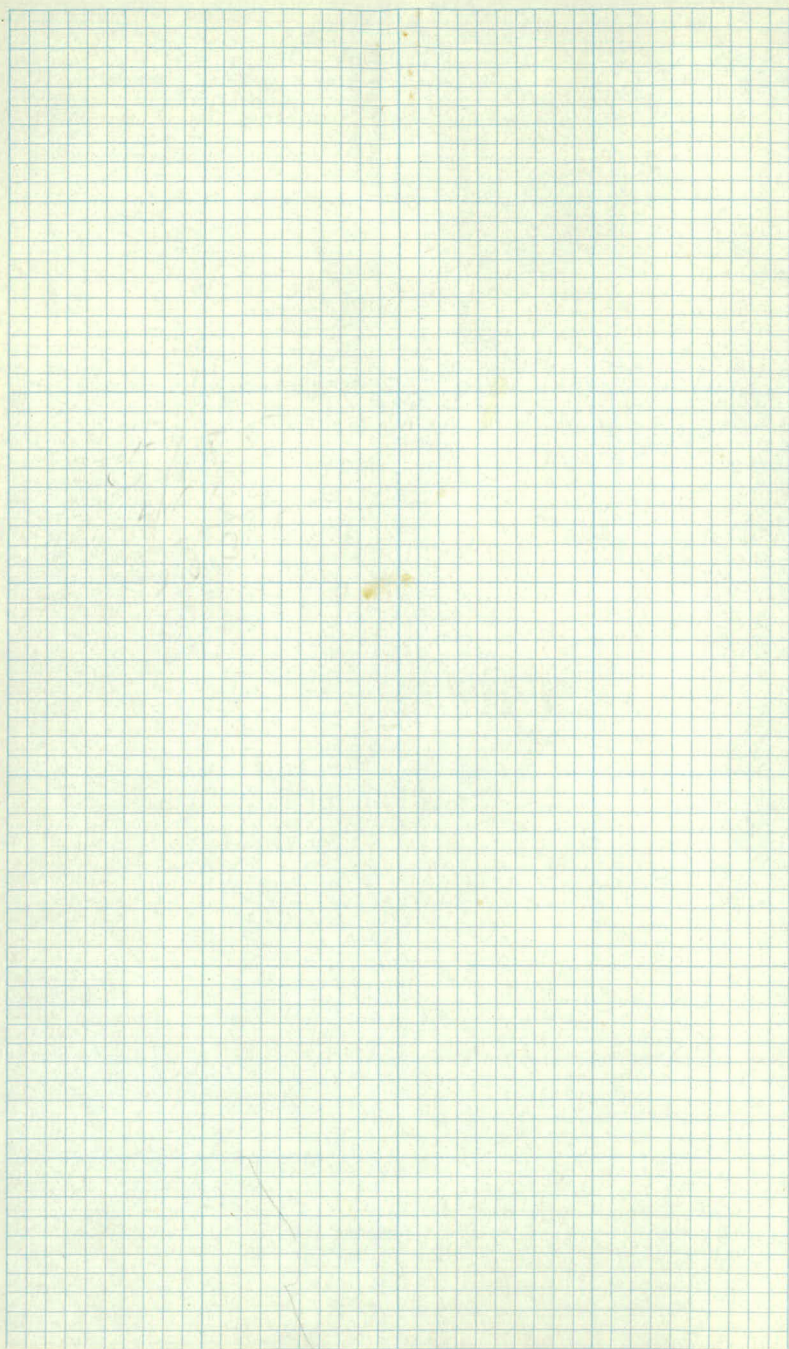


3rd ST



Scale $1'' = 100'$

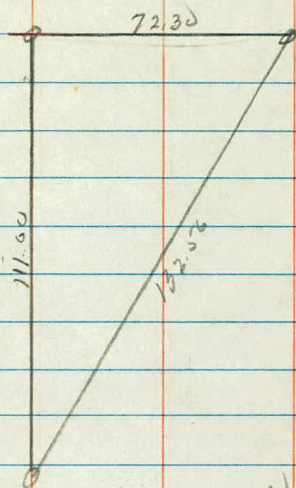
2ND ST.



O.P.P

73.50

64.55 OBE



2nd Block
8

Sta

+

1
2
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92
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94
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98
99
100

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Elev

1.01

95286

95185

770

94516

C-1

1