

B-28-D-14

Dr. 14 - Bk. 28

OFFICE OF COUNTY ENGINEER
RAMSEY CO. MINN.

_____PLAN_____
Survey

_____MOREHEAD AVE. - W.B.C. -_____

From Lake St To S.T.H #96

Road Acc't. No. _____

Date Filed 12-23-38

File _____

City of W.B.

1

Morehead St.

White Bear.

9/38

Grading Plan

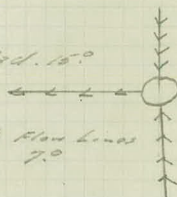
Lake St. to S.T.H. # 96

Walks 6'0"

Corb Rad. 15°

3 + 44.15 - 4th 54.

Cover to Flow lines
7.0



Cover to Flow line
5.3'

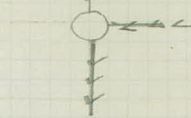


13

12

11
10 + 98.30 - 6th St.

Cover to Flow Line
8.0'



10

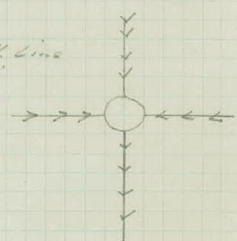
9

0 - Denotes Iron Pipe
property corners found.

8

7 + 35.18 - 5th St.

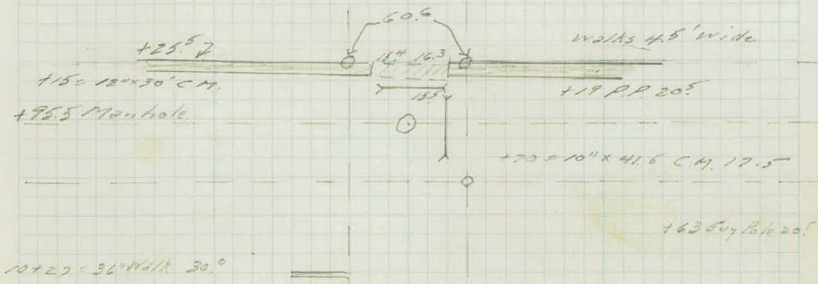
Cover to Fl. Line
6.4'



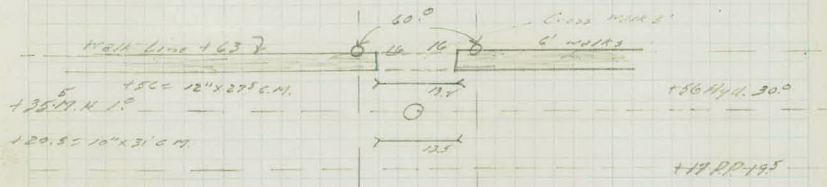
7

6

+34 RP 20.5
18+23=6' Dist. E.L.



9451 36" Walk 30°
9400 36" Walk 30°



+35.14 N 1.0
+20.55 10\"/>

20

19

18 + 23.67 - 8th St.

18

Cover to Flow line
7.8



17

16

15

14 + 21.50 - 7th St.

14

Cover to Flow line
9.58



13

+04.5 End Fe. 27

+81 = 30" Walk 27.5

+55 Fe 29.4

+11.10 P.P. 21.0

+11 P.P. 21.0

+19.5 = 0.5 19.11.

+99 = P.P. 22.0

+24.5 H. 23.5
+92 = P.P. 21.5

+73 = 36" Walk 22.0

+14 = 4" Walk 27.3

+66 P.P. 21.0

Note:
Walks off Ctr. 7th St.

60.35

Walks 4.5 wide

+86.2

+59.14 H. 0.5

+41 P.P. 20.5

Walks 4.5 wide

+31.5

197 16.3

+85 = 36" Walk 30.4

+30 P.P. 20.5

28

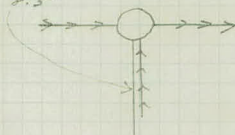
Center To Flow Lines

3 Pipes 124

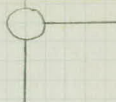
1" 8.5

27

26 + 20.61 - N.P.R.R.



26

25 + 47.90 - 10th St.Center To Flow Line

4.8

25

24

23

22

21 + 86.37 - 9th St.

21

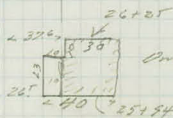
20

+07 End 1c.

+53 = 36" Walk 59.5

+89 To 69. P 26

+96



+06 = 36" Tr. 8.0

Opening Leads Garages
Note Encroachment

60.26

+89 = 8" Tr. 26.0

+69 P.P. 21.5

+51 = 14" H. 10.14

+07 P.P. 19.0

60.35

+87 = 7" Tr. 23

+45 = 10" Tr. 15.7

+37 P.P. 20.5

+89 = 3" Tr. 14

+91 = 4" Tr. 14

+69 = 12" Tr. 22.0

+54
Flagstone
Walk 28.0

+72 = Triple 6" Tr. 24

+54 = Ent. 10' Dirt

+99 P.P. 20.5

+90 = 36" Walk 30.5

+26 = Triple 20" - 25.5

+86 M.H.

+71 P.P. 21.5

+47 = 2" Tr. 15.5

+44 = 4" Tr. 17.0

+38 = 3" Tr. 17.5

+17 = 2" Tr. 17.5

+04 = 14" Tr. 17.0

+35
Flagstone
Walk 15.5

20081. 24.7. 50.15.0
24. 27.5. 14. 12. 18.5
15. 36. 14. 28.5
20. 49. Ent. 10' 24.5
134 P.P. 21.5

+55 = 10" Tr. 17.5

+24 = 6" Tr. 16.5

+13 = 12" Tr. 16.5

30+22.83 - 10th 5th

32

31

30

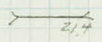
39+10.55 - 11th 5th
2nd

28

This is rolled wood Hub.

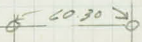


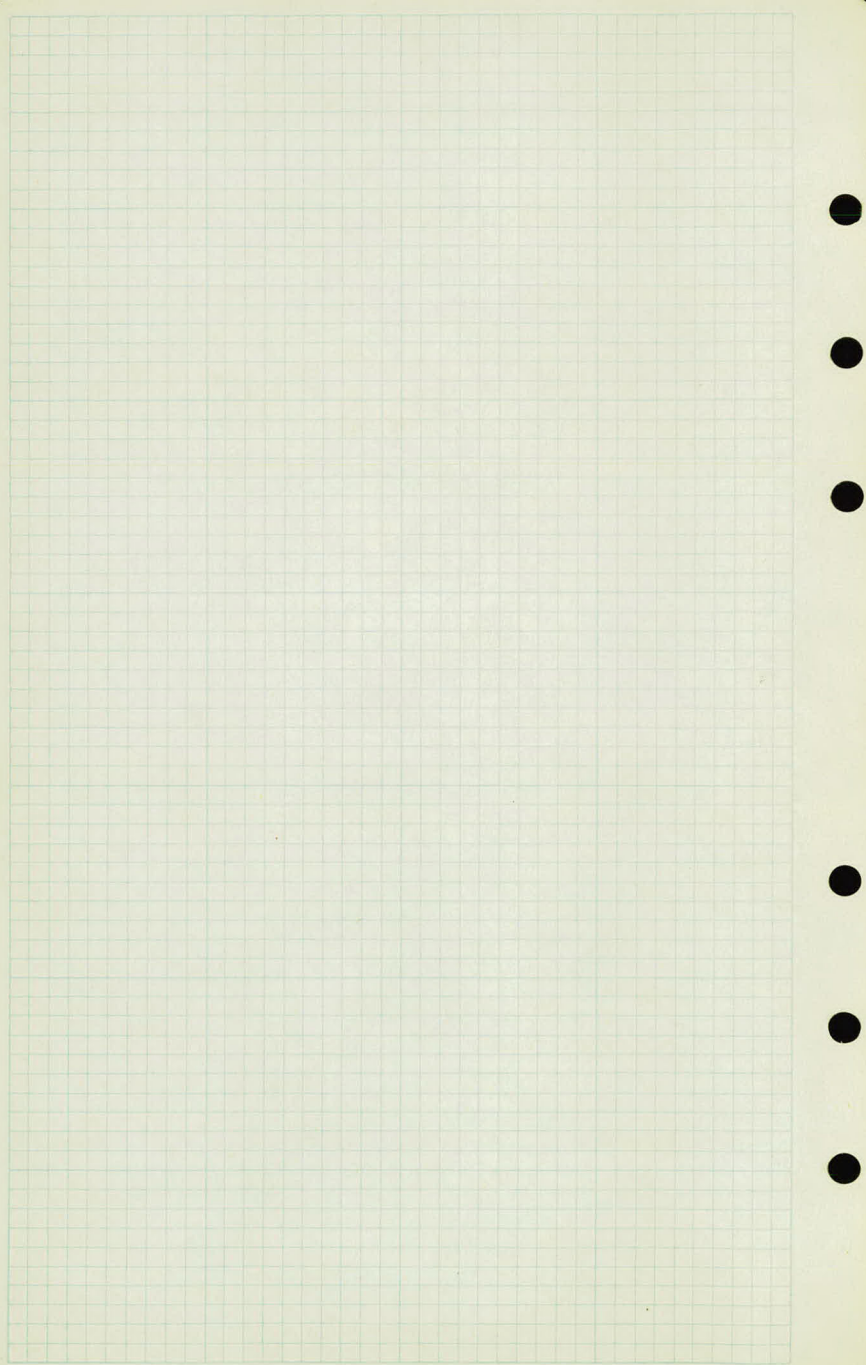
+96 = 18" x 43' C.M.



+77 1/2 4" Fr. Elm 16"

30+18 = 10" Willow 34"





7

Marehead St.

White Bear.

9/38

Sta.	+	-	Elev.
B.M.	2.25	943.25	941.00
0+00			34.50
End of Curb			
Gate Drain Rt.			
+50			35.3
1+00			36.5
1+43	Top Manhole		
+50			37.8
2+00			38.2
+37	Walk Lt.		3
+50			38.7
3+00			38.8
B.M.	2.18	943.76	941.58

Lt.

E

Rt.

8

Top of Hyd. N.E. Cor. 5th & Morehead.

$$\frac{86}{50}$$

$$\frac{875}{1000}$$

$$\frac{91}{50}$$

$$\frac{8.52}{34.73}$$

$$\frac{8.72}{35.03}$$

$$\frac{8.79}{1000}$$

$$\frac{20}{50} \quad \frac{27}{43} \quad \frac{76}{27} \quad \frac{78}{11} \quad \frac{81}{4} \quad \frac{80}{14} \quad \frac{81}{14} \quad \frac{78}{16} \quad \frac{75}{28} \quad \frac{82}{50}$$

$$\frac{63}{40} \quad \frac{63}{29} \quad \frac{64}{18} \quad \frac{67}{14} \quad \frac{67}{8} \quad \frac{68}{7} \quad \frac{68}{7} \quad \frac{71}{7} \quad \frac{72}{10} \quad \frac{68}{11} \quad \frac{69}{27} \quad \frac{68}{40}$$

$$\frac{5.69}{37.56}$$

$$\frac{52}{40} \quad \frac{53}{26} \quad \frac{55}{10} \quad \frac{58}{8} \quad \frac{55}{8} \quad \frac{58}{8} \quad \frac{53}{9} \quad \frac{51}{27} \quad \frac{52}{40}$$

$$\frac{48}{40} \quad \frac{52}{9} \quad \frac{51}{9} \quad \frac{52}{9} \quad \frac{48}{13} \quad \frac{47}{27} \quad \frac{45}{40}$$

$$\frac{4.18}{39.07}$$

$$\frac{24}{40} \quad \frac{38}{24} \quad \frac{47}{18} \quad \frac{46}{8} \quad \frac{50}{8} \quad \frac{47}{14} \quad \frac{42}{40}$$

$$\frac{29}{40} \quad \frac{35}{23} \quad \frac{45}{18} \quad \frac{47}{13} \quad \frac{45}{8} \quad \frac{46}{8} \quad \frac{47}{27} \quad \frac{43}{40}$$

Top of Hyd. N.E. Cor. 4th & Morehead

Sta.	+	X	-	Elev.	
		943.76			
3+16		X-Walks		38.5	
+29		Curb			
+29				37.6	
+44.15				38.1	
+43		Manhole.			
+59		Curb Top.			
+59				37.6	
+70 ⁵		Cross Walks		38.4	
4+00				39.1	
+38		Walk Rt.			
+50				39.4	
5				39.7	
B.M.	2.40	943.40	2.76	941.00	941.00

Lt.

E

Rt.

9

$$\begin{array}{r}
 W \\
 49 \\
 \hline 40
 \end{array}
 \begin{array}{r}
 W \\
 48 \\
 \hline 16
 \end{array}
 \begin{array}{r}
 52 \\
 \hline 16
 \end{array}
 \begin{array}{r}
 53 \\
 \hline 15
 \end{array}
 \begin{array}{r}
 52 \\
 \hline 15
 \end{array}
 \begin{array}{r}
 W \\
 452 \\
 \hline 15
 \end{array}
 \begin{array}{r}
 W \\
 51 \\
 \hline 40
 \end{array}$$

$$\begin{array}{r}
 507 \\
 \hline 38.69
 \end{array}$$

$$\begin{array}{r}
 610 \\
 \hline 37.66
 \end{array}$$

$$\begin{array}{r}
 55 \\
 \hline 40
 \end{array}
 \begin{array}{r}
 58 \\
 \hline 16
 \end{array}
 \begin{array}{r}
 62 \\
 \hline 21
 \end{array}
 \begin{array}{r}
 64 \\
 \hline 21
 \end{array}
 \begin{array}{r}
 67 \\
 \hline 40
 \end{array}$$

$$\begin{array}{r}
 51 \\
 \hline 40
 \end{array}
 \begin{array}{r}
 54 \\
 \hline 18
 \end{array}
 \begin{array}{r}
 57 \\
 \hline 26
 \end{array}
 \begin{array}{r}
 61 \\
 \hline 26
 \end{array}
 \begin{array}{r}
 62 \\
 \hline 40
 \end{array}$$

$$\begin{array}{r}
 568 \\
 \hline 38.08
 \end{array}$$

$$\begin{array}{r}
 510 \\
 \hline 38.66
 \end{array}$$

$$\begin{array}{r}
 616 \\
 \hline 37.60
 \end{array}$$

$$\begin{array}{r}
 55 \\
 \hline 40
 \end{array}
 \begin{array}{r}
 58 \\
 \hline 17
 \end{array}
 \begin{array}{r}
 62 \\
 \hline 24
 \end{array}
 \begin{array}{r}
 65 \\
 \hline 24
 \end{array}
 \begin{array}{r}
 66 \\
 \hline 40
 \end{array}$$

$$\begin{array}{r}
 W \\
 47 \\
 \hline 40
 \end{array}
 \begin{array}{r}
 W \\
 450 \\
 \hline 16
 \end{array}
 \begin{array}{r}
 54 \\
 \hline 16
 \end{array}
 \begin{array}{r}
 54 \\
 \hline 16
 \end{array}
 \begin{array}{r}
 55 \\
 \hline 16
 \end{array}
 \begin{array}{r}
 W \\
 450 \\
 \hline 16
 \end{array}
 \begin{array}{r}
 W \\
 51 \\
 \hline 40
 \end{array}$$

$$\begin{array}{r}
 35 \\
 \hline 40
 \end{array}
 \begin{array}{r}
 38 \\
 \hline 32
 \end{array}
 \begin{array}{r}
 43 \\
 \hline 30
 \end{array}
 \begin{array}{r}
 48 \\
 \hline 16
 \end{array}
 \begin{array}{r}
 50 \\
 \hline 15
 \end{array}
 \begin{array}{r}
 47 \\
 \hline 13
 \end{array}
 \begin{array}{r}
 51 \\
 \hline 13
 \end{array}
 \begin{array}{r}
 47 \\
 \hline 17
 \end{array}
 \begin{array}{r}
 42 \\
 \hline 40
 \end{array}$$

$$\begin{array}{r}
 440 \\
 \hline 39.36
 \end{array}$$

$$\begin{array}{r}
 30 \\
 \hline 40
 \end{array}
 \begin{array}{r}
 38 \\
 \hline 17
 \end{array}
 \begin{array}{r}
 45 \\
 \hline 13
 \end{array}
 \begin{array}{r}
 44 \\
 \hline 13
 \end{array}
 \begin{array}{r}
 48 \\
 \hline 13
 \end{array}
 \begin{array}{r}
 44 \\
 \hline 17
 \end{array}
 \begin{array}{r}
 44 \\
 \hline 27
 \end{array}
 \begin{array}{r}
 37 \\
 \hline 35
 \end{array}
 \begin{array}{r}
 35 \\
 \hline 40
 \end{array}$$

$$\begin{array}{r}
 26 \\
 \hline 40
 \end{array}
 \begin{array}{r}
 27 \\
 \hline 19
 \end{array}
 \begin{array}{r}
 43 \\
 \hline 14
 \end{array}
 \begin{array}{r}
 41 \\
 \hline 13
 \end{array}
 \begin{array}{r}
 48 \\
 \hline 13
 \end{array}
 \begin{array}{r}
 36 \\
 \hline 18
 \end{array}
 \begin{array}{r}
 38 \\
 \hline 40
 \end{array}$$

Top of Hyd. N.E. Cor. 5th & Morehead.

Sta.	+	T	-	Elev.
		942.40		

5+50				39.3
------	--	--	--	------

+63	Walk			
-----	------	--	--	--

6				38.7
---	--	--	--	------

+08	Walk			
-----	------	--	--	--

+50				38.3
-----	--	--	--	------

7				38.1
---	--	--	--	------

+20.5	G.M. Culvert.			
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+35	Top M. Hole.			38.1
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+20				38.1
-----	--	--	--	------

+35.18				38.1
--------	--	--	--	------

+49				37.9
-----	--	--	--	------

+56	G.M. Culvert.			
-----	---------------	--	--	--

				37.9
--	--	--	--	------

+60	X-Walks.			
-----	----------	--	--	--

Lt.

E

Rt.

10

$$\frac{27}{40} \quad \frac{27}{19} \quad \frac{44}{14} \quad \frac{41}{14} \quad \frac{47}{21} \quad \frac{37}{21} \quad \frac{39}{40}$$

$$\frac{411}{39.29}$$

$$\frac{47}{40} \quad \frac{43}{19} \quad \frac{51}{13} \quad \frac{47}{13} \quad \frac{52}{28} \quad \frac{48}{28} \quad \frac{49}{40}$$

$$\frac{508}{38.31}$$

$$\frac{56}{40} \quad \frac{56}{34} \quad \frac{53}{15} \quad \frac{57}{9} \quad \frac{51}{13} \quad \frac{56}{17} \quad \frac{52}{17} \quad \frac{54}{29} \quad \frac{54}{40}$$

$$\frac{51}{40} \quad \frac{49}{20} \quad \frac{53}{15} \quad \frac{59}{14} \quad \frac{53}{13} \quad \frac{58}{13} \quad \frac{58}{28} \quad \frac{58}{40}$$

$$\frac{141}{68} 36.60$$

$$\frac{141}{72} 36.20$$

$$\frac{63}{50} \quad \frac{69}{18} \quad \frac{60}{17} \quad \frac{60}{14} \quad \frac{53}{8} \quad \frac{57}{8} \quad \frac{69}{14} \quad \frac{71}{50}$$

$$\frac{59}{50} \quad \frac{53}{50} \quad \frac{62}{50}$$

$$\frac{69}{50} \quad \frac{62}{19} \quad \frac{58}{11} \quad \frac{55}{13} \quad \frac{61}{13} \quad \frac{66}{21} \quad \frac{69}{50}$$

$$\frac{141}{65} 36.90$$

$$\frac{141}{76.9} 36.50$$

$$\frac{561}{50} \quad \frac{559}{39} \quad \frac{561}{17} \quad \frac{566}{13} \quad \frac{55}{11} \quad \frac{58}{11} \quad \frac{586}{16} \quad \frac{587}{50}$$

Sta.	+	π	-	Elev.
------	---	-------	---	-------

942.40

8				38.3
---	--	--	--	------

+50				38.6
-----	--	--	--	------

9				38.8
---	--	--	--	------

+50				39.0
-----	--	--	--	------

10				39.2
----	--	--	--	------

+27 Walk

+50				39.4
-----	--	--	--	------

+72				39.9
-----	--	--	--	------

B.M.	6.01	945.73	3.68	939.75
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+80				39.9
-----	--	--	--	------

+98.3				40.1
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+93.5	M. Hole.			40.1
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Lt.

E

Rt.

11

$$\frac{51}{40} \quad \frac{54}{15} \quad \frac{58}{15} \quad \frac{52}{6} \quad \frac{51}{13} \quad \frac{58}{13} \quad \frac{54}{15} \quad \frac{52}{40}$$

$$\frac{52}{40} \quad \frac{51}{17} \quad \frac{56}{15} \quad \frac{48}{6} \quad \frac{48}{6} \quad \frac{51}{6} \quad \frac{55}{14} \quad \frac{50}{17} \quad \frac{53}{40}$$

$$\frac{417}{40} \quad \frac{454}{30} \quad \frac{53}{15} \quad \frac{47}{6} \quad \frac{46}{9} \quad \frac{51}{9} \quad \frac{54}{14} \quad \frac{49}{17} \quad \frac{52}{40}$$

$$\frac{33}{40} \quad \frac{418}{30} \quad \frac{47}{19} \quad \frac{50}{14} \quad \frac{46}{8} \quad \frac{44}{6} \quad \frac{47}{6} \quad \frac{54}{15} \quad \frac{49}{17} \quad \frac{46}{40}$$

$$\frac{29}{40} \quad \frac{41}{18} \quad \frac{48}{15} \quad \frac{42}{7} \quad \frac{42}{7} \quad \frac{53}{15} \quad \frac{50}{16} \quad \frac{52}{40}$$

$$\frac{302}{40.38}$$

$$\frac{28}{40} \quad \frac{35}{18} \quad \frac{46}{15} \quad \frac{39}{5} \quad \frac{40}{5} \quad \frac{42}{5} \quad \frac{44}{10} \quad \frac{50}{14} \quad \frac{45}{15} \quad \frac{50}{40}$$

$$\frac{18}{40} \quad \frac{30}{36} \quad \frac{35}{34} \quad \frac{33}{19} \quad \frac{42}{17} \quad \frac{37}{7} \quad \frac{35}{13} \quad \frac{40}{13} \quad \frac{39}{19} \quad \frac{43}{26} \quad \frac{41}{40}$$

Top of property, iron N.E. Cor. 6th & Morehead

$$\frac{63}{50} \quad \frac{65}{24} \quad \frac{61}{10} \quad \frac{58}{23} \quad \frac{64}{23} \quad \frac{69}{50}$$

$$\frac{56}{40}$$

$$\frac{56}{40}$$

$$\frac{61}{50}$$

$$\frac{561}{40.12}$$

<i>Sta.</i>	<i>+</i>	<i>X</i>	<i>-</i>	<i>Elev.</i>
		945.73		
11+13				39.9
+15		C.M. X - Culvert.		
		C.M. Culvert East Side Mouth @ 674		
+22		X Walks		39.7
+50				39.7
12				39.9
+50				40.33
13				40.6
+50				40.9
+85		Walk		
14				41.3
+30				41.6
+33		X - Walks		41.7

Lt.

E

Rt.

12

$\frac{64}{50}$ $\frac{67}{17}$ $\frac{63}{15}$ $\frac{59}{5}$ $\frac{58}{5}$ $\frac{63}{14}$ $\frac{71}{16}$ $\frac{67}{50}$

100
 6.9 3883

100
 38.43 7.3

South End.
 8.1 37.63

North End.
 38.43 7.3

$\frac{583}{50}$ $\frac{592}{16}$ $\frac{60}{5}$ $\frac{605}{16}$ $\frac{592}{50}$

$\frac{50}{40}$ $\frac{51}{33}$ $\frac{60}{28}$ $\frac{63}{19}$ $\frac{67}{15}$ $\frac{60}{8}$ $\frac{60}{5}$ $\frac{64}{10}$ $\frac{68}{16}$ $\frac{60}{20}$ $\frac{65}{31}$ $\frac{50}{40}$

$\frac{52}{40}$ $\frac{54}{31}$ $\frac{58}{20}$ $\frac{66}{14}$ $\frac{60}{8}$ $\frac{58}{5}$ $\frac{65}{16}$ $\frac{58}{20}$ $\frac{65}{30}$ $\frac{51}{33}$ $\frac{47}{40}$

$\frac{53}{40}$ $\frac{56}{16}$ $\frac{61}{14}$ $\frac{55}{7}$ $\frac{54}{5}$ $\frac{56}{6}$ $\frac{61}{5}$ $\frac{58}{17}$ $\frac{55}{29}$ $\frac{50}{34}$ $\frac{49}{40}$

$\frac{41}{40}$ $\frac{39}{30}$ $\frac{45}{19}$ $\frac{58}{14}$ $\frac{53}{7}$ $\frac{51}{5}$ $\frac{57}{13}$ $\frac{55}{17}$ $\frac{45}{19}$ $\frac{46}{40}$

$\frac{29}{40}$ $\frac{33}{31}$ $\frac{39}{20}$ $\frac{54}{14}$ $\frac{48}{8}$ $\frac{49}{5}$ $\frac{51}{10}$ $\frac{53}{14}$ $\frac{52}{17}$ $\frac{44}{18}$ $\frac{39}{26}$ $\frac{34}{28}$ $\frac{32}{40}$

2.4
 2.40
 242
 43.31

$\frac{24}{31}$ $\frac{32}{30}$ $\frac{32}{28}$ $\frac{40}{20}$ $\frac{45}{18}$ $\frac{50}{13}$ $\frac{44}{6}$ $\frac{44}{5}$ $\frac{47}{10}$ $\frac{45}{17}$ $\frac{38}{19}$ $\frac{34}{27}$ $\frac{34}{40}$

$\frac{26}{40}$ $\frac{27}{33}$ $\frac{32}{19}$ $\frac{35}{20}$ $\frac{46}{14}$ $\frac{42}{15}$ $\frac{41}{5}$ $\frac{44}{8}$ $\frac{40}{16}$ $\frac{34}{18}$ $\frac{30}{30}$ $\frac{30}{40}$

$\frac{352}{50}$ $\frac{316}{20}$ $\frac{46}{13}$ $\frac{41}{6}$ $\frac{40}{5}$ $\frac{43}{9}$ $\frac{363}{16}$ $\frac{331}{50}$

Sta.	+	π	-	Elev.
		945.73		

14+48				42.1
-------	--	--	--	------

+59	Manhole			
-----	---------	--	--	--

+61.3				42.3
-------	--	--	--	------

+73				42.2
-----	--	--	--	------

+84				42.1
-----	--	--	--	------

15				41.9
----	--	--	--	------

B.M.	5.37	942.62	3.48	942.75
------	------	--------	------	--------

+50				41.6
-----	--	--	--	------

16				41.6
----	--	--	--	------

+14	Walk			
-----	------	--	--	--

+50				41.4
-----	--	--	--	------

+73	Walk			
-----	------	--	--	--

+90				41.4
-----	--	--	--	------

17				41.4
----	--	--	--	------

+50				41.1
-----	--	--	--	------

LT.

2

RT.

$\frac{43}{50}$ $\frac{44}{24}$ $\frac{40}{10}$ $\frac{36}{21}$ $\frac{41}{21}$ $\frac{40}{50}$
 $\frac{40}{50}$ $\frac{38}{19}$ $\frac{34}{19}$ $\frac{36}{19}$ $\frac{36}{50}$

$\frac{43}{50}$ $\frac{44}{29}$ $\frac{38}{13}$ $\frac{35}{10}$ $\frac{38}{10}$ $\frac{40}{21}$ $\frac{38}{30}$ $\frac{39}{50}$

$\frac{354}{50}$ $\frac{345}{25}$ $\frac{42}{15}$ $\frac{37}{6}$ $\frac{36}{8}$ $\frac{40}{8}$ $\frac{41}{11}$ $\frac{348}{15}$ $\frac{336}{50}$

$\frac{29}{30}$ $\frac{27}{31}$ $\frac{36}{16}$ $\frac{42}{14}$ $\frac{41}{10}$ $\frac{38}{10}$ $\frac{42}{10}$ $\frac{36}{15}$ $\frac{36}{24}$ $\frac{36}{30}$ $\frac{30}{31}$ $\frac{30}{40}$

Top walk cts. 15' RT. 14 + 84

$\frac{52}{40}$ $\frac{52}{31}$ $\frac{55}{18}$ $\frac{63}{13}$ $\frac{59}{8}$ $\frac{60}{11}$ $\frac{64}{11}$ $\frac{63}{15}$ $\frac{59}{17}$ $\frac{58}{28}$ $\frac{50}{31}$ $\frac{47}{40}$

$\frac{48}{40}$ $\frac{48}{30}$ $\frac{51}{19}$ $\frac{64}{14}$ $\frac{60}{6}$ $\frac{60}{11}$ $\frac{66}{11}$ $\frac{62}{20}$ $\frac{61}{40}$

$\frac{42}{40}$ $\frac{43}{30}$ $\frac{44}{22}$ $\frac{58}{16}$ $\frac{61}{13}$ $\frac{62}{11}$ $\frac{67}{11}$ $\frac{61}{21}$ $\frac{61}{40}$

$\frac{45}{41}$ $\frac{45}{30}$ $\frac{45}{19}$ $\frac{65}{17}$ $\frac{64}{8}$ $\frac{62}{10}$ $\frac{67}{10}$ $\frac{63}{16}$ $\frac{57}{20}$ $\frac{57}{40}$

$\frac{59}{40}$ $\frac{63}{24}$ $\frac{66}{11}$ $\frac{64}{8}$ $\frac{62}{10}$ $\frac{67}{10}$ $\frac{56}{17}$ $\frac{52}{40}$

$\frac{56}{40}$ $\frac{57}{34}$ $\frac{63}{28}$ $\frac{66}{20}$ $\frac{69}{13}$ $\frac{65}{7}$ $\frac{65}{9}$ $\frac{68}{17}$ $\frac{68}{40}$

Sta.	+	π	-	Elev.
		947.67		
18				41.3
+02				41.3
+19.5	Manhole			
+23.67				41.3
+43				41.2
+57				41.1
19				40.1
+11	Entr.			39.9
+48				39.7
+57				39.7
+81	Walk			
20				39.6
T.P.	3.88	943.80	7.70	939.97
+50				39.4
+65	Walk			

11.

2

8.

$$\frac{54}{40} \quad \frac{61}{21} \quad \frac{71}{18} \quad \frac{65}{8} \quad \frac{63}{\cancel{7}} \quad \frac{70}{16} \quad \frac{68}{21} \quad \frac{74}{40}$$

$$\frac{61}{40} \quad \frac{65}{24} \quad \frac{69}{22} \quad \frac{64}{8} \quad \frac{63}{\cancel{7}} \quad \frac{65}{7} \quad \frac{71}{17} \quad \frac{67}{25} \quad \frac{72}{40}$$

$$\frac{643}{\cancel{63}} \quad 41.19$$

$$\frac{55}{50}$$

$$\frac{68}{50}$$

$$\frac{63}{40} \quad \frac{66}{34} \quad \frac{70}{27} \quad \frac{63}{10} \quad \frac{64}{\cancel{7}} \quad \frac{71}{14} \quad \frac{68}{17} \quad \frac{74}{26} \quad \frac{75}{40}$$

$$\frac{37}{40} \quad \frac{38}{36} \quad \frac{65}{28} \quad \frac{71}{20} \quad \frac{64}{8} \quad \frac{65}{\cancel{7}} \quad \frac{68}{8} \quad \frac{66}{10} \quad \frac{74}{19} \quad \frac{82}{31} \quad \frac{81}{40}$$

$$\frac{32}{50} \quad \frac{36}{40} \quad \frac{70}{30} \quad \frac{76}{27} \quad \frac{78}{12} \quad \frac{75}{\cancel{7}} \quad \frac{76}{7} \quad \frac{83}{21} \quad \frac{81}{40}$$

$$\frac{58}{50} \quad \frac{63}{38} \quad \frac{75}{26} \quad \frac{80}{12} \quad \frac{75}{3} \quad \frac{77}{\cancel{7}}$$

$$\frac{55}{50} \quad \frac{57}{36} \quad \frac{76}{30} \quad \frac{86}{20} \quad \frac{82}{12} \quad \frac{79}{\cancel{7}} \quad \frac{81}{8} \quad \frac{83}{14} \quad \frac{74}{40}$$

$$\frac{85}{50} \quad \frac{85}{29} \quad \frac{87}{18} \quad \frac{82}{11} \quad \frac{79}{\cancel{7}} \quad \frac{81}{7} \quad \frac{80}{9} \quad \frac{80}{17} \quad \frac{71}{40}$$

$$\frac{800}{\cancel{800}}$$

$$\frac{86}{40} \quad \frac{85}{11} \quad \frac{80}{\cancel{7}} \quad \frac{82}{7} \quad \frac{78}{10} \quad \frac{74}{16} \quad \frac{70}{20} \quad \frac{68}{40}$$

$$\frac{51}{40} \quad \frac{49}{21} \quad \frac{44}{14} \quad \frac{47}{11} \quad \frac{44}{\cancel{7}} \quad \frac{46}{7} \quad \frac{30}{23} \quad \frac{20}{40} \quad \frac{15}{50}$$

$$\frac{1.20}{\cancel{1.20}} \quad 42.0$$

Sta. + π - Elev.

943.80

21

38.9

+15

38.8

+35 Walk

+58

38.5

+76

38.7

+86 Manhole Top

+86.37

38.9

B.M.

0.83

941.69

2.94

940.86

940.85

22

38.6

+50

38.0

+90 Walk

23

37.9

+50

37.3

24

36.8

+94 Walk

+50

36.3

LT.

E

RT.

$\frac{6.0}{40}$ $\frac{5.1}{13}$ $\frac{5.3}{14}$ $\frac{4.8}{3}$ $\frac{4.9}{8}$ $\frac{5.1}{8}$ $\frac{4.6}{11}$ $\frac{2.7}{23}$ $\frac{1.7}{40}$ $\frac{1.7}{50}$

$\frac{4.2}{40}$ $\frac{4.2}{28}$ $\frac{5.6}{22}$ $\frac{5.5}{12}$ $\frac{5.0}{4}$ $\frac{5.0}{7}$ $\frac{5.2}{7}$ $\frac{5.0}{11}$ $\frac{3.8}{29}$ $\frac{3.1}{40}$

{ Bottom Tread 5.21 938.59

{ Top " 4.45 39.35

$\frac{4.3}{46}$ $\frac{4.4}{29}$ $\frac{5.8}{22}$ $\frac{5.8}{13}$ $\frac{5.2}{5}$ $\frac{5.3}{7}$ $\frac{5.4}{7}$ $\frac{5.5}{19}$ $\frac{4.6}{29}$ $\frac{4.3}{40}$

$\frac{6.2}{50}$ $\frac{6.0}{27}$ $\frac{5.4}{13}$ $\frac{5.1}{21}$ $\frac{5.6}{21}$ $\frac{5.1}{50}$

4.84 38.96

$\frac{5.9}{50}$ $\frac{4.9}{50}$ $\frac{4.7}{50}$

Top of bolt in 2" iron pipe N.E. Cor. 9th & Murdoch

$\frac{3.8}{40}$ $\frac{3.8}{33}$ $\frac{3.9}{27}$ $\frac{3.3}{13}$ $\frac{3.1}{7}$ $\frac{3.3}{14}$ $\frac{3.4}{17}$ $\frac{3.0}{22}$ $\frac{3.0}{40}$

$\frac{3.6}{40}$ $\frac{3.7}{16}$ $\frac{4.3}{13}$ $\frac{3.7}{5}$ $\frac{3.7}{7}$ $\frac{3.8}{10}$ $\frac{3.4}{13}$ $\frac{3.3}{40}$

38.09

$\frac{3.6}{40}$ $\frac{4.0}{11}$ $\frac{4.4}{12}$ $\frac{3.8}{7}$ $\frac{4.0}{11}$ $\frac{3.7}{12}$ $\frac{3.3}{21}$ $\frac{3.2}{40}$

$\frac{5.2}{40}$ $\frac{5.0}{33}$ $\frac{4.6}{30}$ $\frac{4.6}{15}$ $\frac{5.0}{12}$ $\frac{4.4}{7}$ $\frac{4.6}{11}$ $\frac{4.5}{40}$

$\frac{4.3}{40}$ $\frac{4.7}{28}$ $\frac{5.0}{14}$ $\frac{5.4}{12}$ $\frac{5.0}{4}$ $\frac{4.9}{7}$ $\frac{5.0}{9}$ $\frac{4.7}{10}$ $\frac{5.2}{14}$ $\frac{4.1}{40}$

37.09

$\frac{5.7}{40}$ $\frac{5.7}{32}$ $\frac{5.7}{14}$ $\frac{5.4}{5}$ $\frac{5.4}{7}$ $\frac{5.4}{8}$ $\frac{5.1}{9}$ $\frac{5.6}{11}$ $\frac{5.1}{40}$

Sta.	+	π	-	Elev.
		941.69		
25				35.9
+47 ⁹⁰				35.7
+51	Mann hole			
26				34.8
T.P.	3.44	938.96	6.17	935.52
+54				34.8
				32.2
+60				
26+70 ⁶	Top of Rail			
+81				32.2
+89				34.56
27				33.9
+50				33.6
+53	Walk			
28				34.3
+50				33.0

Lt.

E

Rt.

16

$$\frac{6.3}{40} \quad \frac{6.1}{16} \quad \frac{6.0}{8} \quad \frac{5.8}{10} \quad \frac{6.0}{10} \quad \frac{5.8}{12} \quad \frac{5.5}{40}$$

$$\frac{6.1}{40} \quad \frac{6.5}{25} \quad \frac{5.9}{11} \quad \frac{6.0}{10} \quad \frac{6.3}{16} \quad \frac{6.3}{50}$$

$$\frac{5.76}{35.93}$$

$$\frac{7.6}{40} \quad \frac{7.6}{34} \quad \frac{6.9}{4} \quad \frac{6.9}{10} \quad \frac{6.4}{7} \quad \frac{6.1}{26}$$

$$\frac{6.2}{43} \quad \frac{6.0}{37} \quad \frac{6.3}{14} \quad \frac{6.6}{11} \quad \frac{6.6}{5} \quad \frac{4.2}{40}$$

$$\frac{3.7}{42} \quad \frac{1.0}{34} \quad \frac{6.3}{25} \quad \frac{6.3}{5} \quad \frac{6.8}{5} \quad \frac{4.8}{5} \quad \frac{4.2}{40}$$

$$\frac{5.80}{33.16}$$

$$\frac{4.9}{40} \quad \frac{4.5}{10} \quad \frac{6.8}{5} \quad \frac{7.1}{5} \quad \frac{6.1}{5} \quad \frac{6.7}{21} \quad \frac{7.0}{28} \quad \frac{4.6}{34} \quad \frac{4.5}{40}$$

$$\frac{4.8}{40} \quad \frac{5.2}{20} \quad \frac{4.4}{5} \quad \frac{7.5}{8} \quad \frac{6.8}{15} \quad \frac{6.8}{30} \quad \frac{7.2}{35} \quad \frac{4.8}{40} \quad \frac{4.8}{50}$$

$$\frac{5.0}{40} \quad \frac{5.3}{30} \quad \frac{5.1}{10} \quad \frac{4.6}{16} \quad \frac{7.7}{27} \quad \frac{7.0}{34} \quad \frac{6.8}{40}$$

$$\frac{4.2}{40} \quad \frac{4.6}{33} \quad \frac{5.4}{13} \quad \frac{5.4}{10} \quad \frac{5.6}{40}$$

4.21

$$\frac{4.0}{40} \quad \frac{4.3}{25} \quad \frac{4.2}{6} \quad \frac{4.7}{10} \quad \frac{5.8}{40}$$

$$\frac{4.4}{40} \quad \frac{5.1}{30} \quad \frac{5.6}{10} \quad \frac{6.0}{10} \quad \frac{6.7}{40}$$

Sta.	+	π	-	Elev.
		938.96		
28+80				32.3
+87				31.9
T.P.	4.67	936.77	6.86	934.10
+94				31.6
+96				30.9
+98				30.9
29				31.7
29+10.55				32.0
+21				31.3
+26				31.0
+31				31.0
+39				32.0
+41				32.9

Lt.

E

Rt.

17

$$\frac{54}{40}$$

$$\frac{58}{30}$$

$$\frac{64}{3}$$

$$\frac{67}{40}$$

$$\frac{74}{40}$$

$$\frac{67}{40}$$

$$\frac{66}{28}$$

$$\frac{71}{40}$$

$$\frac{74}{40}$$

$$\frac{46}{40}$$

$$\frac{52}{40}$$

$$\frac{57}{40}$$

$$\frac{54}{40}$$

$$\frac{59}{40}$$

$$\frac{62}{40}$$

$$\frac{54}{40}$$

$$\frac{59}{40}$$

$$\frac{62}{40}$$

$$\frac{47}{40}$$

$$\frac{51}{40}$$

$$\frac{58}{40}$$

$$\frac{44}{40}$$

$$\frac{48}{40}$$

$$\frac{54}{40}$$

$$\frac{54}{40}$$

$$\frac{55}{40}$$

$$\frac{59}{40}$$

$$\frac{54}{40}$$

$$\frac{58}{40}$$

$$\frac{64}{40}$$

$$\frac{45}{40}$$

$$\frac{49}{16}$$

$$\frac{58}{16}$$

$$\frac{58}{16}$$

$$\frac{51}{16}$$

$$\frac{56}{40}$$

$$\frac{40}{40}$$

$$\frac{47}{12}$$

$$\frac{48}{12}$$

$$\frac{52}{40}$$

$$\frac{30}{40}$$

$$\frac{35}{13} \frac{47}{14} \frac{39}{14}$$

$$\frac{46}{40}$$

Sta.	+	π	-	Elev.
		936.77		
29+50				32.5
30				30.27
+50				29.17
T.P.	7.87	934.44	10.20	926.57
31				26.4
+28				26.0
+96	C.M. Culvert			
32			934.44 94 933.50	28.1
+22				29.0
+30	Shoulder 96 Conn.			29.2
+50	Approach	# 96 Hy Conn		28.8
+72.83				28.3
B.M.		0.94	933.50	933.51

Lt.

E

Rt.

18

$$\frac{32}{40}$$

$$\frac{37}{14}$$

$$\frac{43}{/}$$

$$\frac{46}{29}$$

$$\frac{46}{40}$$

$$\frac{49}{40}$$

$$\frac{54}{30}$$

$$\frac{62}{15}$$

$$\frac{70}{13}$$

$$\frac{65}{/}$$

$$\frac{67}{11}$$

$$\frac{64}{29}$$

$$\frac{65}{40}$$

$$\frac{85}{40} \quad \frac{84}{25} \quad \frac{85}{12} \quad \frac{87}{10} \quad \frac{86}{4} \quad \frac{76}{/} \quad \frac{76}{13} \quad \frac{72}{29} \quad \frac{71}{33} \quad \frac{70}{40}$$

$$\frac{84}{40}$$

$$\frac{80}{/}$$

$$\frac{70}{40}$$

1/2r.

$$\frac{53}{40}$$

$$\frac{87}{14}$$

$$\frac{84}{/}$$

$$\frac{84}{10}$$

$$\frac{80}{29}$$

$$\frac{80}{40}$$

Begin

Approach

10.8 23.64

23.54 1/2r. 10.9

$$\frac{10.7}{40}$$

$$\frac{10.2}{22}$$

$$\frac{6.4}{12}$$

$$\frac{6.3}{/}$$

$$\frac{6.4}{10}$$

$$\frac{7.6}{15}$$

$$\frac{10.5}{23}$$

$$\frac{10.7}{40}$$

$$\frac{7.7}{40}$$

$$\frac{6.7}{19}$$

$$\frac{5.3}{12}$$

$$\frac{5.4}{/}$$

$$\frac{6.0}{12}$$

$$\frac{8.2}{21}$$

$$\frac{8.2}{40}$$

$$\frac{5.2}{40}$$

$$\frac{5.2}{/}$$

$$\frac{5.3}{40}$$

$$\frac{5.4}{/}$$

$$\frac{5.6}{/}$$

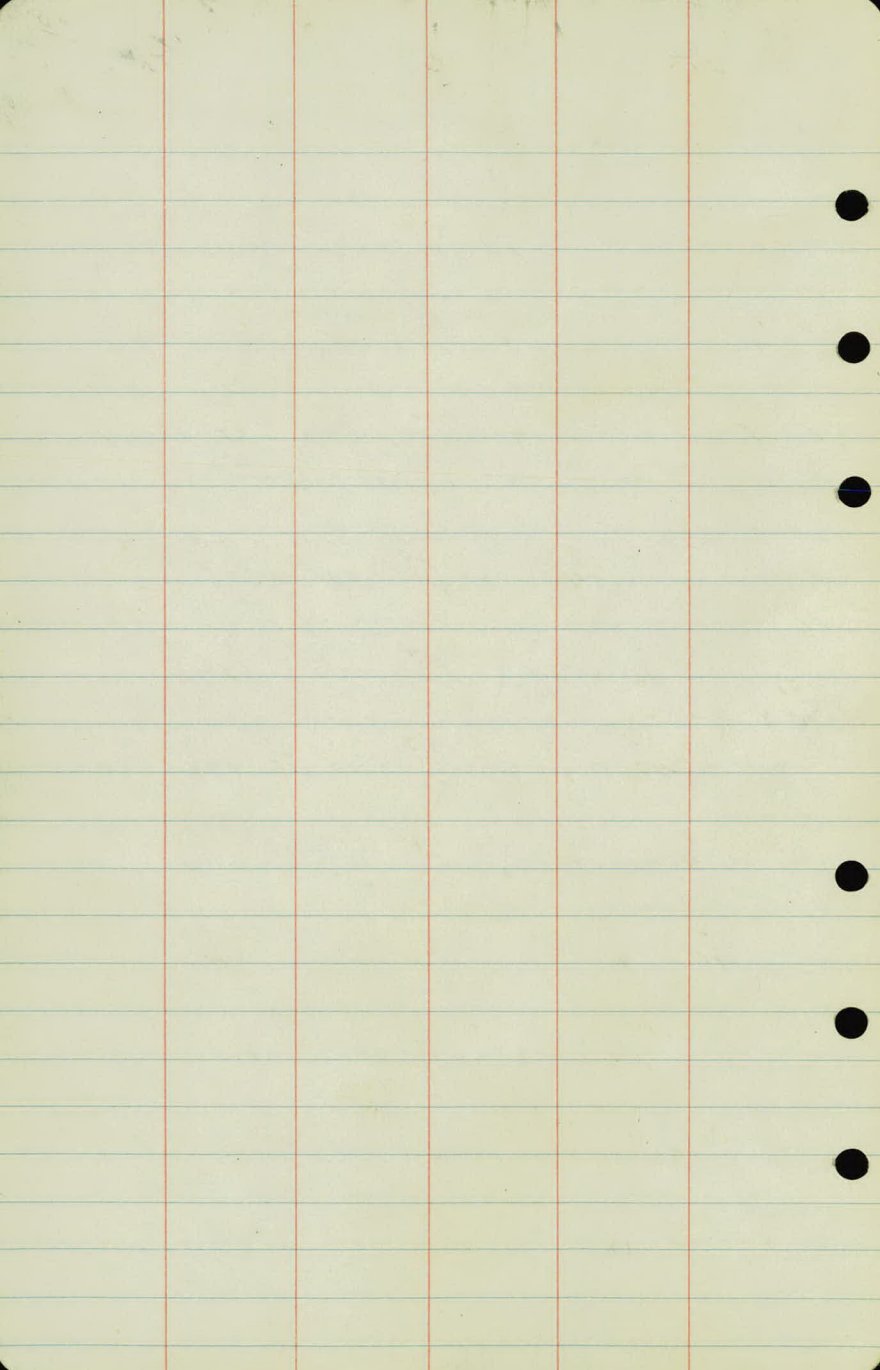
$$\frac{5.8}{50}$$

$$\frac{6.1}{40}$$

$$\frac{6.1}{/}$$

$$\frac{6.5}{40}$$

Top of Hyd. N.E. Cor. 12th & Stewart



Morhead Street

Slope stakes from Lake
St. to S.T.H. #96.

11/15/38

Sta.	+	Σ	-	Grade
B.M.	7.63	943.63		941.00

0+00				34.3
------	--	--	--	------

+50				35.5
-----	--	--	--	------

1				36.6
---	--	--	--	------

+50				37.7
-----	--	--	--	------

2				38.0
---	--	--	--	------

+50				38.2
-----	--	--	--	------

3				38.4
---	--	--	--	------

+14				38.4
-----	--	--	--	------

Lt.

E

Rt.

2

Top of Hyd. NE Cor. 5th

9.3
9.88.1
8.6
$$\begin{array}{r} 83 \\ 8603 \\ \hline 10.5 \end{array}$$
$$\begin{array}{r} 84 \\ 803 \\ \hline \end{array}$$
$$\begin{array}{r} 86 \\ 81 \\ \hline 10.0 \end{array}$$
7.0
7.5
$$\begin{array}{r} 72 \\ 8603 \\ \hline 10.4 \end{array}$$
$$\begin{array}{r} 72 \\ 802 \\ \hline \end{array}$$
$$\begin{array}{r} 75 \\ 8110 \\ \hline \end{array}$$
5.9
6.4
$$\begin{array}{r} 57 \\ 8602 \\ \hline 11.4 \end{array}$$
$$\begin{array}{r} 59 \\ 600 \\ \hline \end{array}$$
$$\begin{array}{r} 56 \\ 8608 \\ \hline 11.6 \end{array}$$
5.6
6.1
$$\begin{array}{r} 55 \\ 8606 \\ \hline 11.4 \end{array}$$
$$\begin{array}{r} 58 \\ 603 \\ \hline \end{array}$$
$$\begin{array}{r} 53 \\ 8608 \\ \hline 11.6 \end{array}$$
5.4
5.9
$$\begin{array}{r} 52 \\ 8602 \\ \hline 11.4 \end{array}$$
$$\begin{array}{r} 50 \\ 604 \\ \hline \end{array}$$
$$\begin{array}{r} 52 \\ 8602 \\ \hline 11.4 \end{array}$$
5.2
5.7
$$\begin{array}{r} 50 \\ 8602 \\ \hline 11.4 \end{array}$$
$$\begin{array}{r} 49 \\ 603 \\ \hline \end{array}$$
$$\begin{array}{r} 49 \\ 8602 \\ \hline 11.4 \end{array}$$
5.2
5.7
$$\begin{array}{r} 52 \\ 601 \\ \hline \end{array}$$

Sta.	+	π	-	Grade
B.M.	7.68	943.68		941.00
3+74				38.4

4				38.7
---	--	--	--	------

+50				39.1
-----	--	--	--	------

5				39.5
T.P.	2.64	943.64	2.68	941.00

+50				39.1
-----	--	--	--	------

6				38.7
---	--	--	--	------

+50				38.3
-----	--	--	--	------

7				37.8
---	--	--	--	------

Lt.

£

Rt.

5.3

$$\begin{array}{r} 48 \\ 605 \\ \hline 30 \end{array}$$

$$\begin{array}{r} 52 \\ 601 \\ \hline 30 \end{array}$$

$$\begin{array}{r} 49 \\ 604 \\ \hline 30 \end{array}$$

5.0

$$\begin{array}{r} 42 \\ 608 \\ \hline 30 \end{array}$$

$$\begin{array}{r} 47 \\ 603 \\ \hline 30 \end{array}$$

$$\begin{array}{r} 46 \\ 604 \\ \hline 30 \end{array}$$

4.6

$$\begin{array}{r} 35 \\ 611 \\ \hline 30 \end{array}$$

$$\begin{array}{r} 43 \\ 603 \\ \hline 30 \end{array}$$

$$\begin{array}{r} 41 \\ 605 \\ \hline 30 \end{array}$$

4.2

$$\begin{array}{r} 27 \\ 615 \\ \hline 30 \end{array}$$

$$\begin{array}{r} 41 \\ 601 \\ \hline 30 \end{array}$$

$$\begin{array}{r} 37 \\ 605 \\ \hline 30 \end{array}$$

4.5

$$\begin{array}{r} 28 \\ 617 \\ \hline 30 \end{array}$$

$$\begin{array}{r} 43 \\ 602 \\ \hline 30 \end{array}$$

$$\begin{array}{r} 38 \\ 606 \\ \hline 30 \end{array}$$

4.9

$$\begin{array}{r} 45 \\ 604 \\ \hline 30 \end{array}$$

$$\begin{array}{r} 49 \\ 600 \\ \hline 30 \end{array}$$

$$\begin{array}{r} 53 \\ 604 \\ \hline 30 \end{array}$$

5.3

$$\begin{array}{r} 56 \\ 603 \\ \hline 30 \end{array}$$

$$\begin{array}{r} 53 \\ 600 \\ \hline 30 \end{array}$$

$$\begin{array}{r} 57 \\ 604 \\ \hline 30 \end{array}$$

5.8

$$\begin{array}{r} 54 \\ 604 \\ \hline 30 \end{array}$$

$$\begin{array}{r} 56 \\ 602 \\ \hline 30 \end{array}$$

$$\begin{array}{r} 60 \\ 602 \\ \hline 30 \end{array}$$

Sta. + π - Grade

943.64

7+65.2

38.1

8

38.2

+50

38.4

9

38.6

+50

38.8

10

39.0

+50

39.2

+68.3

39.3

~~T.P. 5.30 945.43 3.51 940.13~~

Lat.

E

Alt.

5.5

$$\begin{array}{r} 5.8 \\ \hline 50.3 \\ 30 \end{array}$$

$$\begin{array}{r} 5.8 \\ \hline 50.3 \end{array}$$

$$\begin{array}{r} 5.8 \\ \hline 50.4 \\ 30 \end{array}$$

5.4

$$\begin{array}{r} 5.6 \\ \hline 50.2 \\ 30.0 \end{array}$$

$$\begin{array}{r} 5.4 \\ \hline 50.0 \end{array}$$

$$\begin{array}{r} 5.2 \\ \hline 50.3 \\ 30 \end{array}$$

5.2

$$\begin{array}{r} 5.3 \\ \hline 50.1 \\ 30.0 \end{array}$$

$$\begin{array}{r} 5.0 \\ \hline 50.2 \end{array}$$

$$\begin{array}{r} 5.4 \\ \hline 50.2 \\ 30.0 \end{array}$$

5.0

$$\begin{array}{r} 4.8 \\ \hline 50.2 \\ 30.0 \end{array}$$

$$\begin{array}{r} 4.8 \\ \hline 50.2 \end{array}$$

$$\begin{array}{r} 5.3 \\ \hline 50.3 \\ 30.0 \end{array}$$

4.8

$$\begin{array}{r} 4.4 \\ \hline 50.4 \\ 30.0 \end{array}$$

$$\begin{array}{r} 4.7 \\ \hline 50.1 \end{array}$$

$$\begin{array}{r} 5.2 \\ \hline 50.4 \\ 30 \end{array}$$

4.6

$$\begin{array}{r} 3.7 \\ \hline 50.9 \\ 30.0 \end{array}$$

$$\begin{array}{r} 4.5 \\ \hline 50.1 \end{array}$$

$$\begin{array}{r} 5.4 \\ \hline 50.8 \\ 30.0 \end{array}$$

4.4

$$\begin{array}{r} 3.3 \\ \hline 51.1 \\ 30.0 \end{array}$$

$$\begin{array}{r} 4.2 \\ \hline 50.2 \end{array}$$

$$\begin{array}{r} 5.0 \\ \hline 50.6 \\ 30 \end{array}$$

4.3

$$\begin{array}{r} 3.4 \\ \hline 50.9 \\ 30.0 \end{array}$$

$$\begin{array}{r} 3.8 \\ \hline 50.5 \end{array}$$

$$\begin{array}{r} 4.5 \\ \hline 50.2 \\ 30 \end{array}$$

Sta.	+	x	-	Grade
B.M.	5.24	947.49		942.25
11+28.3				39.8

+60				40.0
-----	--	--	--	------

12				40.4
----	--	--	--	------

+50				40.8
-----	--	--	--	------

13				41.2
----	--	--	--	------

+50				41.6
-----	--	--	--	------

14				42.1
----	--	--	--	------

+31.3				42.3
-------	--	--	--	------

Lt.

E

Rt.

Top E Walk 15' Rt. Sta. 14+84

7.7

$$\begin{array}{r} 74 \\ \hline 6.0 \\ 30 \end{array}$$

$$\begin{array}{r} 77 \\ \hline 6.0 \end{array}$$

$$\begin{array}{r} 76 \\ \hline 6.0 \\ 30 \end{array}$$

7.5

$$\begin{array}{r} 73 \\ \hline 6.0 \\ 30 \end{array}$$

$$\begin{array}{r} 78 \\ \hline 6.0 \end{array}$$

$$\begin{array}{r} 75 \\ \hline 6.0 \\ 30 \end{array}$$

7.1

$$\begin{array}{r} 73 \\ \hline 6.0 \\ 30 \end{array}$$

$$\begin{array}{r} 75 \\ \hline 6.0 \end{array}$$

$$\begin{array}{r} 73 \\ \hline 6.0 \\ 30 \end{array}$$

6.7

$$\begin{array}{r} 71 \\ \hline 6.0 \\ 30 \end{array}$$

$$\begin{array}{r} 71 \\ \hline 6.0 \end{array}$$

$$\begin{array}{r} 71 \\ \hline 6.0 \\ 30 \end{array}$$

6.3

$$\begin{array}{r} 57 \\ \hline 6.0 \\ 30 \end{array}$$

$$\begin{array}{r} 69 \\ \hline 6.0 \end{array}$$

$$\begin{array}{r} 65 \\ \hline 6.0 \\ 30 \end{array}$$

5.9

$$\begin{array}{r} 53 \\ \hline 6.0 \\ 30 \end{array}$$

$$\begin{array}{r} 66 \\ \hline 6.0 \end{array}$$

$$\begin{array}{r} 51 \\ \hline 6.0 \\ 30 \end{array}$$

5.4

$$\begin{array}{r} 49 \\ \hline 6.0 \\ 30 \end{array}$$

$$\begin{array}{r} 62 \\ \hline 6.0 \end{array}$$

$$\begin{array}{r} 48 \\ \hline 6.0 \\ 30 \end{array}$$

5.2

$$\begin{array}{r} 51 \\ \hline 6.0 \\ 30 \end{array}$$

$$\begin{array}{r} 58 \\ \hline 6.0 \end{array}$$

$$\begin{array}{r} 51 \\ \hline 6.0 \\ 30 \end{array}$$

Sta.	+	π	-	Elev.
		947.49		
14+91.3				42.1
15				42.0
+50				41.8
16				41.6
+50				41.4
+90				41.2
17				41.2
+50				41.0

Lt.

E

Rt.

5.4

$$\begin{array}{r} 49 \\ 60.5 \\ \hline 30 \end{array}$$

$$\begin{array}{r} 54 \\ 60.0 \\ \hline \end{array}$$

$$\begin{array}{r} 52 \\ 60.2 \\ \hline 30 \end{array}$$

5.5

$$\begin{array}{r} 45 \\ 61.0 \\ \hline 30.0 \end{array}$$

$$\begin{array}{r} 56 \\ 60.1 \\ \hline \end{array}$$

$$\begin{array}{r} 54 \\ 60.4 \\ \hline 30.0 \end{array}$$

5.7

$$\begin{array}{r} 51 \\ 60.6 \\ \hline 30.0 \end{array}$$

$$\begin{array}{r} 58 \\ 60.1 \\ \hline \end{array}$$

$$\begin{array}{r} 51 \\ 60.6 \\ \hline 30.0 \end{array}$$

5.9

$$\begin{array}{r} 47 \\ 61.2 \\ \hline 30.0 \end{array}$$

$$\begin{array}{r} 59 \\ 60.0 \\ \hline \end{array}$$

$$\begin{array}{r} 62 \\ 60.3 \\ \hline 30 \end{array}$$

6.1

$$\begin{array}{r} 42 \\ 61.9 \\ \hline 30.0 \end{array}$$

$$\begin{array}{r} 60 \\ 60.1 \\ \hline \end{array}$$

$$\begin{array}{r} 60 \\ 60.1 \\ \hline 30.0 \end{array}$$

6.3

$$\begin{array}{r} 41 \\ 62.2 \\ \hline 30.0 \end{array}$$

$$\begin{array}{r} 60 \\ 60.3 \\ \hline \end{array}$$

$$\begin{array}{r} 56 \\ 60.7 \\ \hline 30.0 \end{array}$$

6.3

$$\begin{array}{r} 59 \\ 60.4 \\ \hline 30 \end{array}$$

$$\begin{array}{r} 61 \\ 60.2 \\ \hline \end{array}$$

$$\begin{array}{r} 54 \\ 60.9 \\ \hline 30 \end{array}$$

6.5

$$\begin{array}{r} 58 \\ 60.7 \\ \hline 30 \end{array}$$

$$\begin{array}{r} 64 \\ 60.1 \\ \hline \end{array}$$

$$\begin{array}{r} 66 \\ 60.1 \\ \hline 30 \end{array}$$

Sta.	+	K	-	Elev.
		947.49		
17+93.7				40.8
18+53.7				40.4
19				40.1
T.P.	3.97	944.05	7.41	440.08
+11				40.0
+48 +50				39.8
+57				39.7
20				39.4
+50				39.0

Lt.

E

Rt.

6.7

$$\begin{array}{r} 57 \\ C 1.0 \\ \hline 30 \end{array}$$

$$\begin{array}{r} 62 \\ C 0.5 \\ \hline \end{array}$$

$$\begin{array}{r} 7.3 \\ F 0.6 \\ \hline 30 \end{array}$$

7.1

$$\begin{array}{r} 58 \\ C 1.3 \\ \hline 30 \end{array}$$

$$\begin{array}{r} 64 \\ C 0.7 \\ \hline \end{array}$$

$$\begin{array}{r} 8.5 \\ F 1.4 \\ \hline 30 \end{array}$$

7.4

$$\begin{array}{r} 70 \\ C 0.4 \\ \hline 30 \end{array}$$

$$\begin{array}{r} 7.3 \\ C 0.1 \\ \hline \end{array}$$

$$\begin{array}{r} 8.2 \\ F 0.8 \\ \hline 30 \end{array}$$

4.0

X

4.2

$$\begin{array}{r} 44 \\ F 0.2 \\ \hline 30 \end{array}$$

$$\begin{array}{r} 4.3 \\ F 0.1 \\ \hline \end{array}$$

$$\begin{array}{r} 4.2 \\ C 0.0 \\ \hline 30 \end{array}$$

4.3

X

4.6

$$\begin{array}{r} 49 \\ F 0.3 \\ \hline 30 \end{array}$$

$$\begin{array}{r} 4.4 \\ C 0.2 \\ \hline \end{array}$$

$$\begin{array}{r} 2.9 \\ C 1.7 \\ \hline 30 \end{array}$$

5.0

$$\begin{array}{r} 53 \\ F 0.3 \\ \hline 30 \end{array}$$

$$\begin{array}{r} 4.7 \\ C 0.3 \\ \hline 30 \end{array}$$

$$\begin{array}{r} 2.9 \\ C 2.1 \\ \hline 30 \end{array}$$

Sta.	+	π	-	Elev.
		944.05		
21				38.7
+15				38.6
+36.4				38.3
T.P.	0.20	941.05	3.20	940.85
22+16.4				38.2
B.M.	0.20	941.05	0.20	940.85 940.85
+50				37.9
23				37.5
+50				37.0
24				36.6

Lt.

L

Rt.

8

5.3

$$\frac{5.8}{\text{FOR}} \\ \frac{30}{30}$$

$$\frac{5.1}{\text{COR}} \\ \frac{30}{30}$$

$$\frac{2.3}{\text{COR}} \\ \frac{30}{30}$$

X

5.7

$$\frac{4.6}{\text{C.I.}} \\ \frac{30}{30}$$

$$\frac{5.4}{\text{C.O.}} \\ \frac{30}{30}$$

$$\frac{4.7}{\text{C.I.}} \\ \frac{30}{30}$$

2.8

$$\frac{3.1}{\text{K.O.}} \\ \frac{30}{30}$$

$$\frac{2.8}{\text{C.O.}} \\ \frac{30}{30}$$

$$\frac{2.6}{\text{C.O.}} \\ \frac{30}{30}$$

Top of bolt in 2" pipe N.E. Cor. @ 9th

3.1

$$\frac{3.1}{\text{C.O.}} \\ \frac{30}{30}$$

$$\frac{3.0}{\text{C.O.}} \\ \frac{30}{30}$$

$$\frac{2.6}{\text{C.O.}} \\ \frac{30}{30}$$

3.5

$$\frac{2.9}{\text{C.O.}} \\ \frac{30}{30}$$

$$\frac{3.1}{\text{C.O.}} \\ \frac{30}{30}$$

$$\frac{2.8}{\text{C.O.}} \\ \frac{30}{30}$$

4.0

$$\frac{4.1}{\text{F.O.}} \\ \frac{30}{30}$$

$$\frac{3.8}{\text{C.O.}} \\ \frac{30}{30}$$

$$\frac{3.6}{\text{C.O.}} \\ \frac{30}{30}$$

4.4

$$\frac{3.9}{\text{C.O.}} \\ \frac{30}{30}$$

$$\frac{4.2}{\text{C.O.}} \\ \frac{30}{30}$$

$$\frac{4.2}{\text{C.O.}} \\ \frac{30}{30}$$

Sta. + R - Elev.

941.05

24+50

36.1

25

35.7

+18

35.5

T.P.

2.17

936.94

6.28

934.77

29+40.6

31.5

+50

31.4

30

30.9

LT.

E

RT.

4.9

$$\frac{5.0}{F.O.}$$

$$\frac{4.8}{C.O.}$$

$$\frac{4.2}{C.O.}$$

5.3

$$\frac{5.4}{F.O.}$$

$$\frac{5.2}{C.O.}$$

$$\frac{4.9}{C.O.}$$

5.5

$$\frac{6.2}{F.O.}$$

$$\frac{5.3}{C.O.}$$

$$\frac{5.2}{C.O.}$$

$$\frac{5.4}{6.9}$$

$$\frac{3.4}{DC 2.5}$$

$$\frac{4.2}{C.I.}$$

$$\frac{4.7}{DC 2.5}$$

$$\frac{5.5}{7.0}$$

X

$$\frac{6.0}{7.5}$$

$$\frac{6.0}{DC 2.5}$$

$$\frac{6.7}{F.O.}$$

$$\frac{6.6}{DC 2.5}$$

Sta.	+	π	-	Elev.
		936.94		
30+50				30.4
31				30.0
+28				29.7
32				29.0
+22				28.8
+30				28.7
+50				28.5
B.M.		3.43	933.51	933.51

Lt.

E

Rt.

6.5
8.0

8.6
F.2.1
19.7

7.8
F.1.3

7.8
V.0.2
21.4

6.9
8.4

10.8
F.3.9
22.8

10.5
F.3.6

8.7
F.2.8
20.6

7.2
8.7

11.5
F.4.3
23.6

11.0
F.3.8

10.8
F.3.2
22.4

7.9
9.4

13.0
F.5.1
25.2

8.8
F.0.9

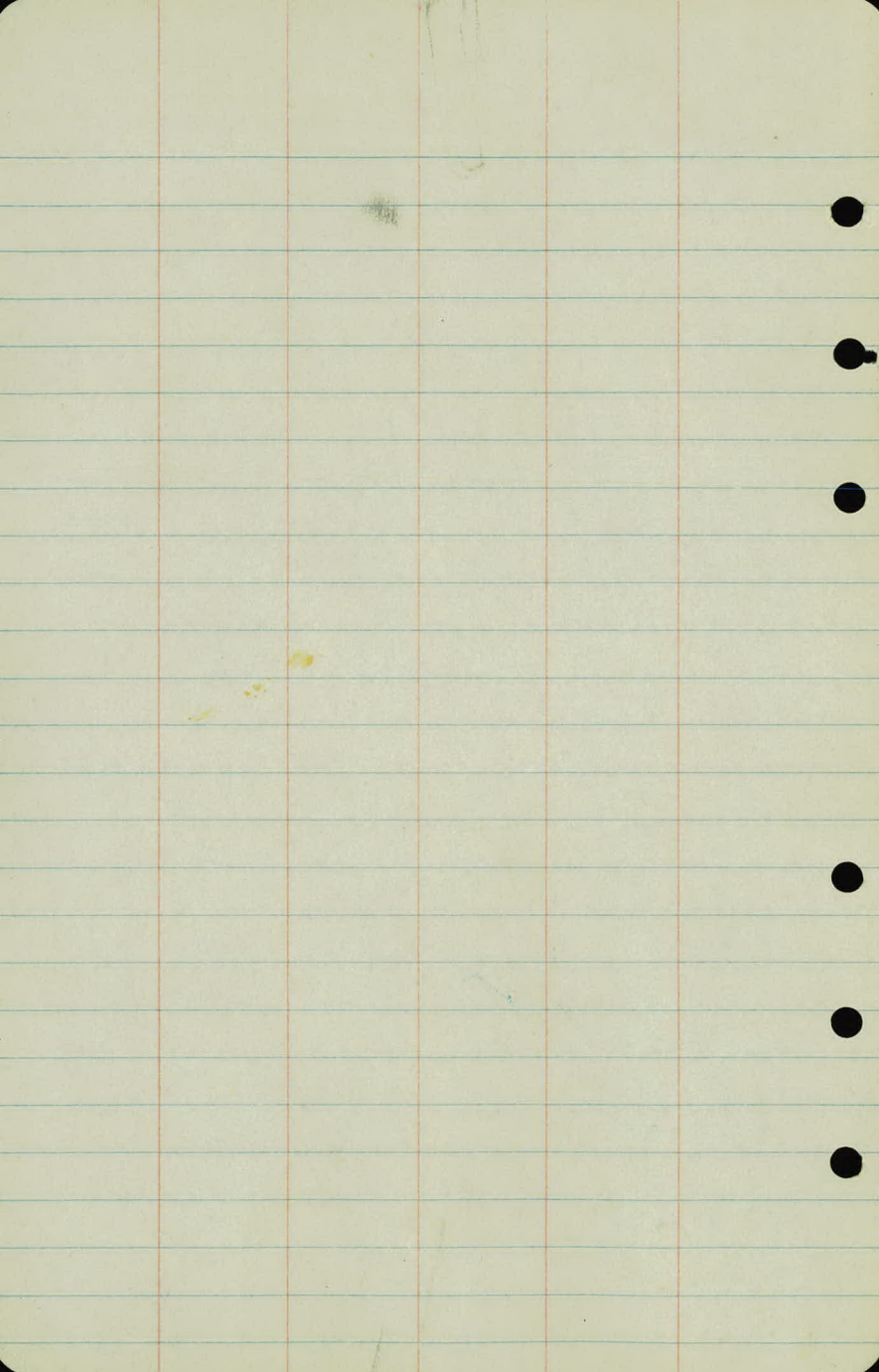
13.2
F.5.3
25.6

8.1
9.6

8.2
9.7

8.4
9.9

Top of Hyd. N.E. Cor. 12th & Stewart



Slope Stokes

Marchwood Ave.

10th to 11th

Sta	+	Σ	-	Grade	nl/b Cor
B.M.	-0.25	940.60			(940.85)
25	+77.9			35.99	33.8
26				34.8	
	+25			34.1	
	+54			33.4	
T.P.	5.81	939.04	7.37	933.23	
	+60			33.2	32.2
	+81			33.0	
	+89			32.9	
27				32.8	
	+25			32.6	
	+50			32.4	
28				32.1	
	+50			31.7	
	+80.5			31.45	
B.M.					

-2.776

6/5/39

Gr. Rod Lt R. Rt.

Top Bolt 2' Pipe N.E. Cor. 9th

5.1	$28.0 / \frac{54}{1.0}$	$\frac{54}{-0.3}$	$\frac{+0.0}{17.5}$ Bl. Top
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5.8		$\frac{58}{0.0}$	$\frac{5.0}{+0.8/19.1}$
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6.5	$28.0 / \frac{1.5}{0.0}$		$\frac{5.6}{+0.9/19.3}$
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7.2	$16.0 / \frac{7.8}{2.05}$	$\frac{6.2}{+1.0}$	$\frac{5.8}{+1.9/20.3}$
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5.84

6.00	$30.0 / \frac{5.1}{+1.1}$	$\frac{7.0}{+1.0}$	
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6.14

6.2	$20.0 / \frac{5.2}{+1.0}$	$\frac{5.2}{+1.0}$	
-----	---------------------------	--------------------	--

6.4		$\frac{5.6}{+0.8}$	$\frac{5.3}{+1.1/30.0}$
-----	--	--------------------	-------------------------

6.6	$30.0 / \frac{4.8}{+1.6}$	$\frac{5.2}{+1.4}$	$\frac{5.6}{+1.0/30.0}$
-----	---------------------------	--------------------	-------------------------

6.8	$30.0 / \frac{4.2}{+2.7}$	$\frac{4.5}{+2.4}$	$\frac{5.4}{+1.5/30.0}$
-----	---------------------------	--------------------	-------------------------

7.3	$30.0 / \frac{5.1}{+2.2}$	$\frac{4.2}{+1.1}$	$\frac{4.7}{+0.4/30.0}$
-----	---------------------------	--------------------	-------------------------

7.6	$30.0 / \frac{5.7}{+1.9}$	$\frac{4.9}{+1.7}$	$\frac{7.2}{+0.4/30.0}$
-----	---------------------------	--------------------	-------------------------

