

Book # 16 Dr. 14

OFFICE OF COUNTY ENGINEER
RAMSEY CO. MINN.

_____ Plan _____ Survey

_____ BIRCH LAKE AVENUE, _____

From W. City Limits To Bald Eagle Ave.

Road Acc't. No. _____

Date Filed 5-11-35

File 14

Alignment

Birch Lake Ave - White Bear -

Purcell

BIRCH LAKE AVE.

6+24.45 E. Prop 4th Av.

5+94.45 & 4th

5+64.45 W. Prop. Line 4th Av.

1+95 E. Prop. Line 5th Av.

1+65 & Land W. Prop. Line 5th Av.

0+00 P.O.T. Int. Dillon St. No.

4/18/35

Cloudy.

HTP.

D.N.S.

D.S.

J.B.

East ↑

nail

8" W.h. Ash

58.68

nail

42.300

16 Oak Maple

nail

nail

nail

24" oak



58.96

5px

64.85



24" Cottonwood

11+34.45 E Prop Line 3rd Av

11+04.45 E 3rd Av

10+74.45 W Prop Line 3rd Av

6+89.46 E Prop Line Kreck

6+59.46 E Kreck

6+29.46 W Prop Line Kreck Ave

nail

P.P. 25.85

30.17-0 T.P.

nail

46.33

Conc Post

nail

nail

6" Ev. Gr. Tr.

54.72

nail

40.40

8" w.h. 9.5h

nail

18+44.92 W Prop Line Florence

16+44.45 E Prop Line 2nd Av

16+14.45 ± 2nd Av

15+84.45 W. Prop Line 2nd Av

13+18.92 ± and E Prop Line Wood Av

12+88.92 W Prop Line Wood

12" B.E.

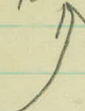
O

48.90

O 31.66

P.P.

18+74.92



nail

nail

nail

Hud

O

56.50

O 25.38

P.P.

nail

42.42

O

P.P.

nail

nail

35.65

nail in Brick Post

nail

47.30

nail in Br. Post

nail

nail

26+04.92 W Prop Line Bald Eagle

21+54.45 E Prop Line 1st

21+24.45 $\pm$ 1st Av.

20+94.45 W Prop Line 1st Av.

19+04.92 E Prop Line Florence

18+74.92 $\pm$ Florence

nail

nail

P.P.
O-37.47

nail

O-47.85
Hyd

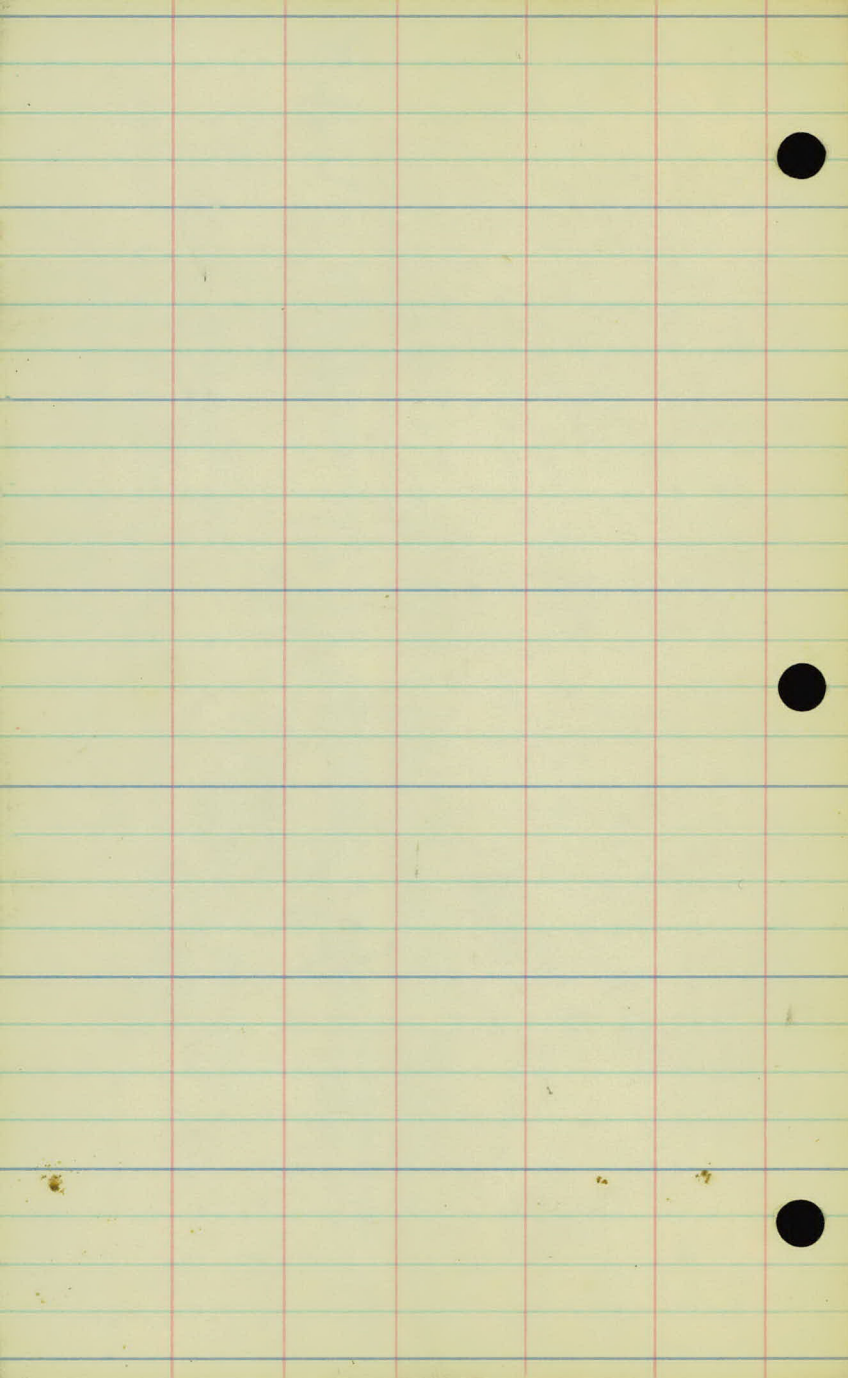
nail

nail

nail

36.2 Measured
26+37.42 ± Bald Eagle (Records)

Hyd Fl. Pole
48.662 67.0



1-6
Cloudy
4-18-35

H.T.P.
D.N.S.
D.S.
J.B. *truck
Driver*

TOPOGRAPHY BIRCH LAKE AVENUE

W. City Limits to Bald Eagle Ave
WHITE BEAR VILLAGE

$$\begin{array}{r} +66 \text{ P.P.} \\ 25 \end{array}$$

$$\begin{array}{r} +28 \text{ Bay Row} \\ 36 \end{array}$$

5+00

Rd
16+11

$$\begin{array}{r} +95 \text{ Str. Rt} - 16' \times 28 \text{ CM} \\ 19 \\ +70 \text{ End Ev Gr Tr.} \\ 35 \end{array}$$

$$\begin{array}{r} +02 \text{ TP} \\ 25 \end{array}$$

$$\begin{array}{r} +29 \text{ P.P.} \\ 24 \\ +03 \text{ Ent-9'x29' V.P.} \\ 22 \end{array}$$

4+00

$$\begin{array}{r} +17 \text{ Bay Row Ever Gr. Tr.} \\ 35 \\ +09 \text{ M. Box} \\ 14 \end{array}$$

$$\begin{array}{r} +92 \text{ Stp} \\ 30 \end{array}$$

$$\begin{array}{r} +54 \text{ SFP} \\ 31 \end{array}$$

$$\begin{array}{r} +17 \text{ Tr} \\ 31 \end{array}$$

3+00

Rd
13-13

$$\begin{array}{r} +71 \text{ TP} \\ 25 \\ +36 \text{ Lamp Pole} \\ 1.5 \\ +17 \text{ Tr} \\ 31 \end{array}$$

$$\begin{array}{r} +88 \text{ P.P.} \\ 24 \end{array}$$

$$\begin{array}{r} +62 \text{ Oak} \\ 29 \end{array}$$

$$\begin{array}{r} +19.24 \text{ Oak} \\ 29 \end{array}$$

$$\begin{array}{r} +52 \text{ Ent-12'x20' CM} \\ 22 \end{array}$$

$$\begin{array}{r} +37 \text{ TP} \\ 25 \\ +36 \text{ Post} \\ 15 \end{array}$$

2+00

Rd
13-13

$$\begin{array}{r} +70 \text{ 15" Oak} \\ 24 \end{array}$$

$$\begin{array}{r} +50 \text{ P.P.} \\ 24 \end{array}$$

$$\begin{array}{r} +01 \text{ Ent-12'x24' CM} \\ 17 \end{array}$$

$$\begin{array}{r} +77-12' \text{ CM} \\ 16.5 \text{ 18} \\ +15 \text{ M. Box} \\ 17 \\ +13 \text{ TP} \\ 25 \end{array}$$

$$\begin{array}{r} +67 \text{ F.C.} \\ 33 \end{array}$$

$$\begin{array}{r} +68 \text{ Fce Cor} \\ 33 \end{array}$$

1+00

$$\begin{array}{r} +54 \text{ Tree} \\ 23 \end{array}$$

$$\begin{array}{r} +20 \text{ Tree} \\ 23 \end{array}$$

$$\begin{array}{r} +15 \text{ PP} \\ 24 \end{array}$$

$$\begin{array}{r} +97 \text{ 15'x24' CM} \\ 21 \\ +89 \text{ Hedge end} \\ 27 \\ +09.5 \text{ MH.} \\ 1.5 \\ +09 \text{ Hedge Cor.} \\ 27 \\ +07 \text{ Sn. Post} \\ 18 \end{array}$$

0+00

Rd
13-13
36' CM
18 18.5

Ent

L.H.

Ent.

12" x 14" CM
9" x 9" V.P. S

Ent

15" x 24" CM

Buried 4'

Ent

M.H.

Pitch

5
in

H. Wall 15' x 5' - 1" Thick Concr

36" CM.
Hd. Wall Section

$\frac{+12 Tr}{21}$ $\frac{+15 PP}{25}$
 $\frac{+48 Tr}{28}$
 +41 Water Shut off
 28

$\frac{+85 TP}{25}$ $\frac{+85 FC}{33.5}$
 $\frac{+35 FC}{33.5}$
 +30 Ent
 +25 F.C.

12

$\frac{+84 Tr}{28}$
 $\frac{+74 Ent}{17}$ 12'x14' CM.
 $\frac{+13 PP}{25}$

$\frac{SW}{28}$
 $\frac{+36 Tr}{26}$ $\frac{+78 Tr}{26}$ $\frac{+85 FC}{28.5}$
 $\frac{+22 TP}{25}$ $\frac{+33 Beg 4' conc. SW.}{28.5}$
 $\frac{+19 FC.}{34}$
 $\frac{+0.5 MH + Str.}{2.0}$

11

$\frac{+70 M.B.}{21}$ $\frac{+91 Tree.}{27}$
 $\frac{+74 X Walk}{17}$ 12'x5' VP
 $\frac{+22 Ent}{16}$ 12'x24' CM

$\frac{+51 SW - 3' Wide}{33.5}$

10

$\frac{+07 Tree}{27}$

Rd
13-13

$\frac{+05 T.P.}{25}$

$\frac{+74 Fce}{33}$
 $\frac{+46 End Row Ex. 6' Tr}{36}$
 $\frac{+09 Ent}{18}$ 12'x20' CM

$\frac{+94 PP}{25}$

9

$\frac{+51 PP}{25}$

$\frac{+13 - 12' x ? CM (Buried)}{20}$?
 $\frac{+05 FC}{32}$

$\frac{+28 MB}{11}$ $\frac{+88 TP}{25}$
 $\frac{+14 Ent}{15}$ 12'x20' CM

8+00

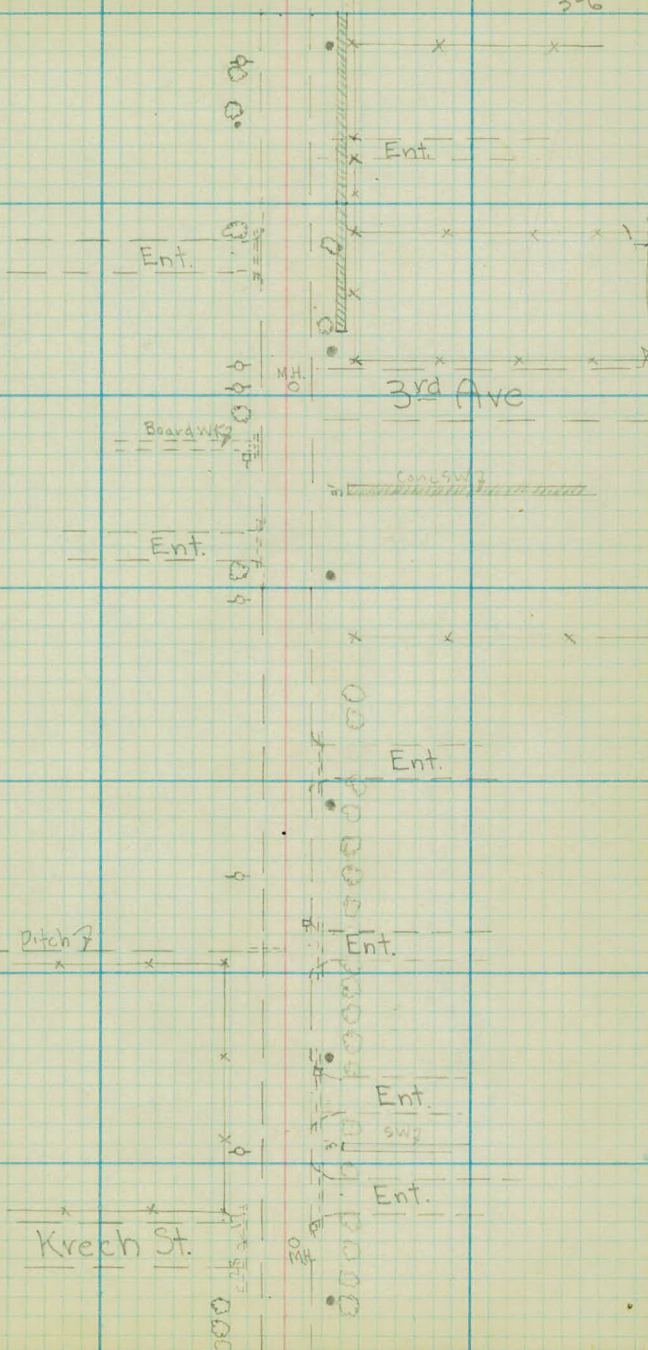
$\frac{+48 MB.}{13}$ $\frac{+55 TP}{25}$
 $\frac{+37 - 12' x 20' CM - Ent}{17}$
 $\frac{+12 3' SW}{30}$

$\frac{+09 PP.}{25}$

$\frac{+15 FC}{32}$
 $\frac{+59 SW Lt.}{22}$ 12'x45' CM
 $\frac{+28 End Row Trees}{35}$

$\frac{+48 Ent}{18}$ 12'x20' CM.
 $\frac{+65 MB.}{13}$ $\frac{+59.5 M.H.}{1.5}$
 $\frac{+29 T.P.}{25}$
 $\frac{+27 Tree Beg Ever Grn Row}{36}$

6+00



SW
29.3

SW
28

+95 TP.
26
+45 Ent

19

SW Rd
29.5 17-17

SW
27.9

+75 Str 10'x33 CM
M
+60 SW Drain
29.5

+97 TP.
25

+37 Ent

+77 Ent

+73.5 MH - 24" Dia

+55 PP
25

+05 TP
25

2.7

SW
29.5

SW
27.7

18

+77 Wash. off.
27

+34 PP
25

+63 Tr
27

+27 Wash. off
27

SW
29

SW
28

17

+65 Hyd
25

+74 TP
25

+80 Walk-3' Brick
23.4

+43 Ent 12'x18 CM
20

+29 SW Drain
28

+55 Water Soff
26

+07 PP
25

+33 Rd
14 17

+15 Str. 12'x28' CM

+15 MH
21

16

+98 12'x36 CM
18-18

+92 U.S. Mail Box
26

+29 Beg 4' Conc. SW
29.3

+45 TP
24

15

Rd
15-16

SW
28

+65 Ent 12'x14' CM.
17

+34 End FC.
34.5

+19 End FC.
34

+70 Tr
33

+14 TP
24

+16 PP
25

SW
28

14

+90 Ent - 12' wide

+25 Ent 9'x14' V.P.
16

+03.5 MH
2

+20 Beg FC.
33

SW
28

13

4-22-35
Clear
H.T.P.
D.N.S.
D.S.
J.B.

Campbell Av.

Florence Av. C.I. S.W. Drain

Ent.

Ent.

Ent.

Ent.

M.H.

C.I. S.W. Drain

2nd Ave.

4' Conc. Wall

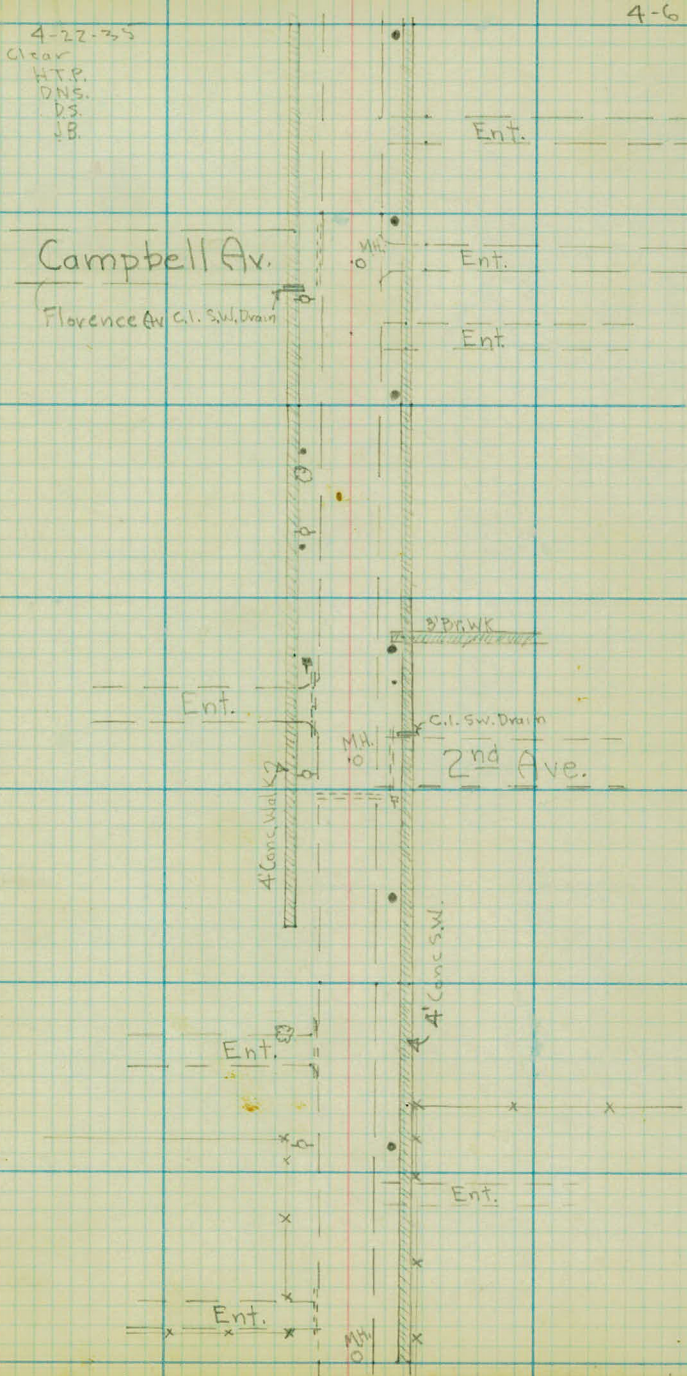
4' Conc. S.W.

Ent.

Ent.

Ent.

M.H.



+69 SW
+63 SW

+19 End 4' Conc SW

+53 C.B.
44
+09 Cor SW
29.1

+12 MH
23.5

Rd

+13 P.P.
28
+09 Cor SW
29.8

+23 MH
4

SW
29.1

20 21

+99 Hyd.
23.5
+52 Cor SW
34.1

+25 Ent

+04 P.P.
25

SW
29.3

+98 Stop Ent
22

+12 TP

+58 Ent

+29 TP

27

SW
29.5

+59 N+S Fce
34.5
+29 Wa. Shop off
29

+66 Ent

+33 T.P.
21.5

SW
29.3

Rd
20-20

SW
28.7

+94 P.P.
25 +43 8' 11' V.P. in SW
24.5

+40 N+S Fce
35

+35 Ent

+52 FC
35.5
+41 TP
26

+80 Ent

SW
29.4

SW
28.8

+74 PP
25

+26 Ent

SW
29.3

+54 TP
26

+53 FC
35.5

+52 SW
22

"School" Cart on

SW
28.4

+75 Ent.

+53 PP
25

+63 SW Dr
29.5

+28 Str

+64 TP
26

+23.5 MH
3.3

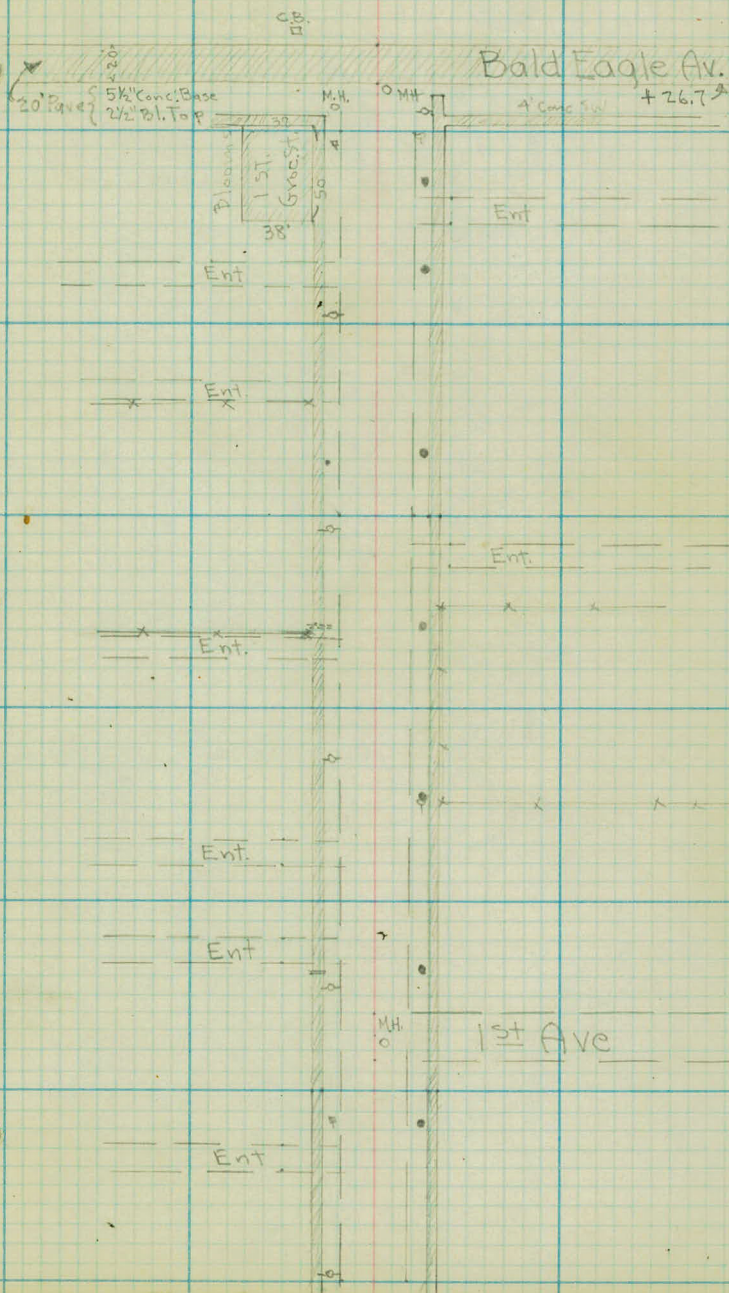
SW
29.5

SW
28.4

+83 Hyd.
23.5
+66 Ent

+84 TP
26

+02 PP
24.5



69 71

+10 Cor School
56

+21 Cor Convent
41

75

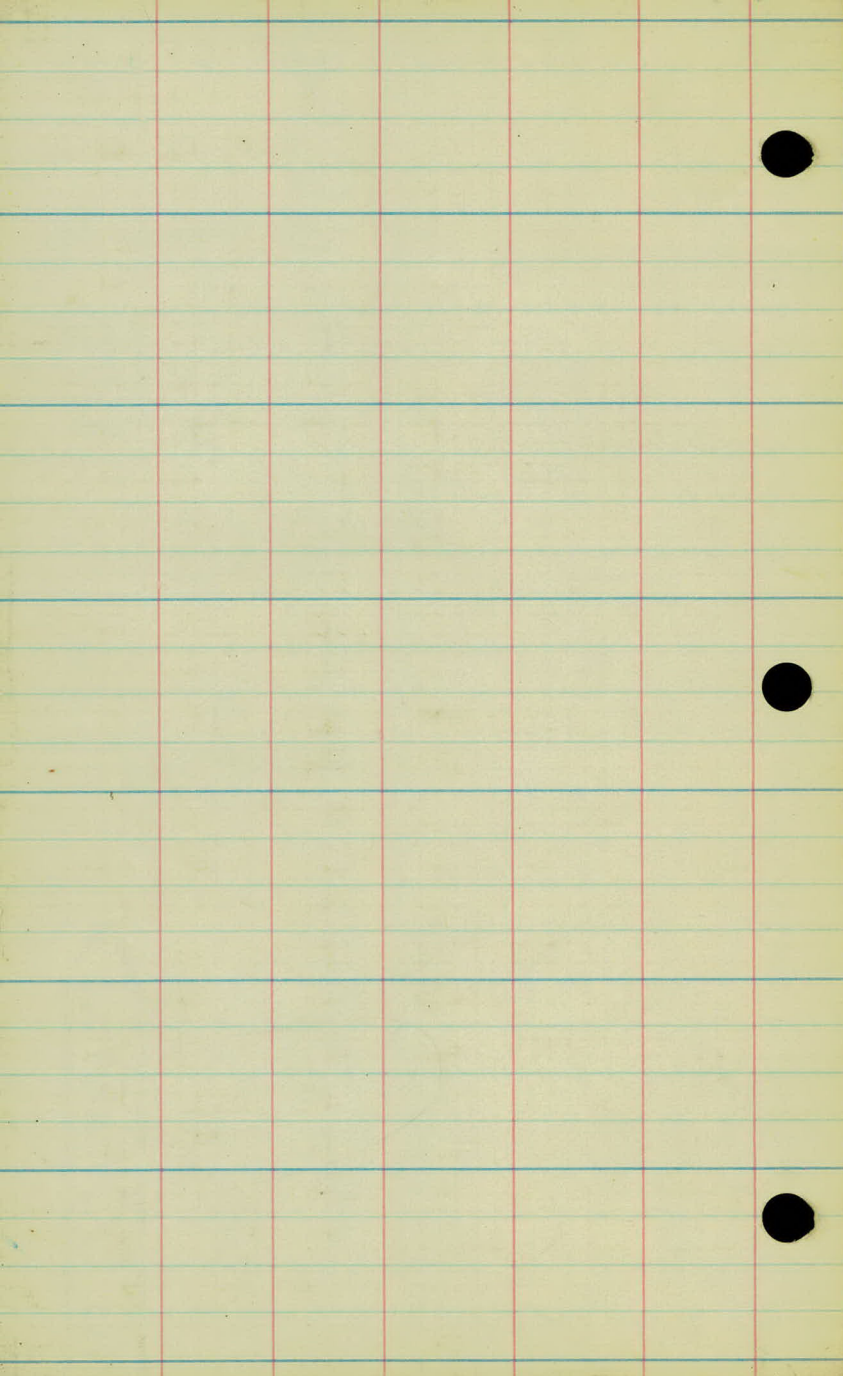
St. Mary's
School

4
6

68

Convent

48



X SECTIONS
BIRCH LAKE AVE

White Bear Village

Sta	+	π	-	Elev
B.M.	4.87	938.16 ✓		933.29 ✓

○	4.79	937.59 ✓	5.36	932.80 ✓
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BM	2.21	937.45 ✓	2.35	935.24 ✓
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○	5.51	936.54 ✓	6.42	931.03 ✓
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BM			4.78	931.76 ✓
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B.M.			4.75	931.79 ✓
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0+00				31.4 ✓
------	--	--	--	--------

+08				31.4 ✓
-----	--	--	--	--------

+25				31.5 ✓
-----	--	--	--	--------

+50				31.5 ✓
-----	--	--	--	--------

+75				31.5 ✓
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U.S. G.S. in Yard St. Marys School

Top Hyd 25' Lt Sta 16+65

SpK in T.P. 25' Rt Sta. 7+55

SpK in 24" Oak 23' Lt. of 0+54

25.1	22.4	24.4
11.4 40	12.2 18	7.1 18
5.6 12	5.1	6.0 14
7.4 18	12.1 40	
30.7	30.2	
5.8 40	5.2 24	9.0 14
9.0 16	5.6 14	5.6 10
5.1	5.7 13	5.6 15
8.4 23	6.6 25	6.3 40
31.2	+09 M.H. Elev 931.52	30.8
5.3 40	5.3 22	8.0 19-17
5.7 14	5.5 11	5.0
5.5 12	5.5 14	8.3 20-22
6.7 24	6.0 29	5.7 40
30.3	31.0	
6.2 40	6.2 21	8.0 18-16
5.7 14	5.5 11	5.0
5.4 13	7.8 19	8.2 22
6.6 24	6.0 29	5.5 40
30.3	30.5	
6.2 40	6.0 21	8.0 18-16
5.5 14	5.4 11	5.0
5.7 12	6.0 13	7.8 19
8.2 22	6.4 24	6.0 40

Sta	+ π -	Elev.
1	936.54 ✓	31.3 ✓
+25		31.3 ✓
+50		
+65	± + W Prop Line 5th Av.	31.2 ✓
+71		
+95	E P.L. 5th Av.	31.3 ✓
2		
+25		31.4 ✓
+50		31.5 ✓
+75		31.6 ✓
3		
		31.5 ✓
+25		31.5 ✓
+50		31.4 ✓
+75		31.6 ✓
4		
		31.6 ✓

30.5

30.3

 $\frac{6.0}{40}$ $\frac{6.0}{21}$ $\frac{7.8}{19}$ $\frac{5.2}{14}$ $\frac{5.4}{11}$ 5.2 $\frac{5.8}{14}$ $\frac{6.0}{15}$ $\frac{7.8}{19}$ $\frac{8.2}{22}$ $\frac{6.4}{24}$ $\frac{6.2}{40}$

30.3

29.8

 $\frac{6.2}{40}$ $\frac{6.0}{21}$ $\frac{7.8}{19-17}$ $\frac{5.5}{15}$ $\frac{5.3}{11}$ 5.2 $\frac{5.8}{12}$ $\frac{6.0}{15}$ $\frac{8.0}{20}$ $\frac{8.2}{23}$ $\frac{6.7}{25}$ $\frac{6.7}{40}$

30.1

29.5

 $\frac{6.4}{40}$ $\frac{6.2}{21}$ $\frac{8.3}{19-17}$ $\frac{6.1}{15}$ $\frac{5.6}{12}$ 5.3 $\frac{5.7}{12}$ $\frac{5.9}{14}$ $\frac{8.1}{20}$ $\frac{8.2}{24}$ $\frac{7.0}{26}$ $\frac{7.0}{40}$

30.1

E Colv $\frac{7.2}{17}$ $\frac{8.2}{19}$

12" C.M.

29.9

 $\frac{6.4}{40}$ $\frac{6.3}{26}$ $\frac{6.0}{20}$ $\frac{8.2}{18-16}$ $\frac{5.7}{14}$ $\frac{5.5}{10}$ 5.2 $\frac{5.7}{12}$ $\frac{6.0}{14}$ $\frac{7.6}{19}$ $\frac{7.6}{22}$ $\frac{6.6}{27-40}$ $\frac{6.6}{40}$

30.7

30.4

 $\frac{5.8}{40}$ $\frac{5.8}{28}$ $\frac{5.1}{21}$ $\frac{7.7}{18-16}$ $\frac{5.6}{14}$ $\frac{5.5}{10}$ 5.1 $\frac{5.5}{12}$ $\frac{6.3}{17}$ $\frac{7.4}{20-23}$ $\frac{6.6}{24}$ $\frac{5.8}{32}$ $\frac{6.1}{40}$

30.8

30.2

 $\frac{5.7}{40}$ $\frac{5.7}{28}$ $\frac{5.3}{21}$ $\frac{7.6}{18-16}$ $\frac{5.6}{15}$ $\frac{5.3}{10}$ 5.0 $\frac{5.2}{9}$ $\frac{5.7}{14}$ $\frac{7.4}{20-23}$ $\frac{6.6}{24}$ $\frac{6.3}{40}$

31.5

30.1

 $\frac{5.0}{40}$ $\frac{4.7}{22}$ $\frac{8.0}{19-17}$ $\frac{5.7}{14}$ $\frac{5.3}{10}$ 4.9 $\frac{5.4}{11}$ $\frac{5.9}{15}$ $\frac{7.4}{20}$ $\frac{7.5}{23}$ $\frac{6.7}{29}$ $\frac{5.7}{31}$ $\frac{6.4}{40}$

31.3

30.7

 $\frac{5.2}{40}$ $\frac{5.6}{22}$ $\frac{7.9}{19-17}$ $\frac{6.1}{15}$ $\frac{5.4}{10}$ 5.0 $\frac{5.4}{11}$ $\frac{5.8}{15}$ $\frac{7.7}{21}$ $\frac{7.2}{27}$ $\frac{6.0}{30}$ $\frac{5.8}{40}$

31.0

30.5

 $\frac{5.5}{40}$ $\frac{5.4}{30}$ $\frac{4.7}{26}$ $\frac{5.7}{22}$ $\frac{7.7}{18-16}$ $\frac{6.4}{15}$ $\frac{5.5}{11}$ 5.0 $\frac{5.4}{10}$ $\frac{5.8}{14}$ $\frac{7.4}{18}$ $\frac{7.6}{24}$ $\frac{5.8}{29}$ $\frac{6.0}{40}$

31.0

+36 LampHole Elev 931.03

30.4

 $\frac{5.5}{40}$ $\frac{5.5}{32}$ $\frac{4.8}{25}$ $\frac{7.8}{19-17}$ $\frac{6.6}{15}$ $\frac{5.5}{11}$ 5.1 $\frac{5.5}{10}$ $\frac{5.7}{13}$ $\frac{7.2}{17}$ $\frac{7.4}{21}$ $\frac{5.8}{24}$ $\frac{6.1}{40}$

30.8

30.4

 $\frac{5.7}{40}$ $\frac{5.6}{31}$ $\frac{5.3}{25}$ $\frac{7.8}{21-19}$ $\frac{5.7}{15}$ $\frac{5.5}{11}$ 4.9 $\frac{5.4}{9}$ $\frac{5.6}{13}$ $\frac{7.2}{17}$ $\frac{7.1}{26}$ $\frac{5.6}{30}$ $\frac{6.1}{40}$

30.8

30.2

 $\frac{5.7}{40}$ $\frac{5.2}{25}$ $\frac{8.1}{21-19}$ $\frac{5.7}{16}$ $\frac{5.2}{11}$ 4.9 $\frac{5.4}{9}$ $\frac{6.1}{14}$ $\frac{7.2}{18-21}$ $\frac{6.2}{25}$ $\frac{6.3}{40}$

Sta.	+	π	-	Elev.
4 + 25		936.54 ✓		31.6 ✓
+50				31.6 ✓
+75				31.6 ✓
5				31.7 ✓
+25				31.8 ✓
+50				31.9 ✓
+64.5		W Prop L. 4th		31.9 ✓
+70		Top Ditch Rt.		31.8 ✓
+76		E Ditch Rt		31.8 ✓
+82		Top Dt. Rt. + Shoulder		31.8 ✓
+94.5		E 4th Av		31.6 ✓

B.M. 444 936.20 ✓ 931.76 ✓

6 + 06		Shoulder Rt		31.6 ✓
+11		Dt Rt		31.6 ✓
+16		Sec Rt		
+25		E. Prop Line 4th		31.7 ✓

30.7

30.0

$$\begin{array}{r} 5.8 \\ 40 \end{array} \quad \begin{array}{r} 5.1 \\ 24 \end{array} \quad \begin{array}{r} 7.9 \\ 21-19 \end{array} \quad \begin{array}{r} 5.7 \\ 16 \end{array} \quad \begin{array}{r} 5.2 \\ 11 \end{array} \quad 4.9 \quad \begin{array}{r} 5.3 \\ 9 \end{array} \quad \begin{array}{r} 6.0 \\ 14 \end{array} \quad \begin{array}{r} 6.8 \\ 17 \end{array} \quad \begin{array}{r} 7.0 \\ 20 \end{array} \quad \begin{array}{r} 6.1 \\ 22 \end{array} \quad \begin{array}{r} 6.5 \\ 40 \end{array}$$

30.8

30.0

$$\begin{array}{r} 5.7 \\ 40 \end{array} \quad \begin{array}{r} 5.7 \\ 27 \end{array} \quad \begin{array}{r} 8.0 \\ 20-22 \end{array} \quad \begin{array}{r} 6.8 \\ 19 \end{array} \quad \begin{array}{r} 5.6 \\ 16 \end{array} \quad \begin{array}{r} 5.3 \\ 11 \end{array} \quad 4.9 \quad \begin{array}{r} 5.5 \\ 11 \end{array} \quad \begin{array}{r} 6.0 \\ 14 \end{array} \quad \begin{array}{r} 7.0 \\ 17 \end{array} \quad \begin{array}{r} 7.1 \\ 20 \end{array} \quad \begin{array}{r} 6.1 \\ 22 \end{array} \quad \begin{array}{r} 6.5 \\ 40 \end{array}$$

31.1

29.7

$$\begin{array}{r} 5.4 \\ 40 \end{array} \quad \begin{array}{r} 5.7 \\ 28 \end{array} \quad \begin{array}{r} 7.9 \\ 21-23 \end{array} \quad \begin{array}{r} 6.6 \\ 20 \end{array} \quad \begin{array}{r} 5.3 \\ 12 \end{array} \quad 4.9 \quad \begin{array}{r} 5.3 \\ 10 \end{array} \quad \begin{array}{r} 6.0 \\ 14 \end{array} \quad \begin{array}{r} 6.8 \\ 16 \end{array} \quad \begin{array}{r} 7.0 \\ 20 \end{array} \quad \begin{array}{r} 6.2 \\ 22 \end{array} \quad \begin{array}{r} 6.1 \\ 30 \end{array}$$

31.8

29.9 $\frac{6.8}{40}$

$$\begin{array}{r} 4.7 \\ 40 \end{array} \quad \begin{array}{r} 5.0 \\ 30 \end{array} \quad \begin{array}{r} 6.3 \\ 27 \end{array} \quad \begin{array}{r} 8.1 \\ 21-23 \end{array} \quad \begin{array}{r} 6.6 \\ 20 \end{array} \quad \begin{array}{r} 5.2 \\ 12 \end{array} \quad 4.8 \quad \begin{array}{r} 5.3 \\ 10 \end{array} \quad \begin{array}{r} 5.6 \\ 14 \end{array} \quad \begin{array}{r} 7.0 \\ 18 \end{array} \quad \begin{array}{r} 7.0 \\ 20 \end{array} \quad \begin{array}{r} 5.7 \\ 24 \end{array} \quad \begin{array}{r} 6.6 \\ 40 \end{array}$$

32.0

30.0

$$\begin{array}{r} 4.5 \\ 40 \end{array} \quad \begin{array}{r} 4.9 \\ 32 \end{array} \quad \begin{array}{r} 6.5 \\ 26 \end{array} \quad \begin{array}{r} 8.0 \\ 23-21 \end{array} \quad \begin{array}{r} 6.3 \\ 18 \end{array} \quad \begin{array}{r} 5.3 \\ 13 \end{array} \quad 4.7 \quad \begin{array}{r} 5.2 \\ 10 \end{array} \quad \begin{array}{r} 5.7 \\ 14 \end{array} \quad \begin{array}{r} 7.1 \\ 18 \end{array} \quad \begin{array}{r} 7.1 \\ 21 \end{array} \quad \begin{array}{r} 5.8 \\ 27 \end{array} \quad \begin{array}{r} 6.5 \\ 40 \end{array}$$

31.7

30.7

$$\begin{array}{r} 4.8 \\ 40 \end{array} \quad \begin{array}{r} 5.0 \\ 33 \end{array} \quad \begin{array}{r} 6.1 \\ 25 \end{array} \quad \begin{array}{r} 7.6 \\ 20-22 \end{array} \quad \begin{array}{r} 5.9 \\ 18 \end{array} \quad \begin{array}{r} 5.2 \\ 13 \end{array} \quad 4.6 \quad \begin{array}{r} 5.1 \\ 11 \end{array} \quad \begin{array}{r} 6.5 \\ 16 \end{array} \quad \begin{array}{r} 6.8 \\ 21 \end{array} \quad \begin{array}{r} 5.4 \\ 29 \end{array} \quad \begin{array}{r} 5.8 \\ 40 \end{array}$$

31.5

30.8

$$\begin{array}{r} 5.0 \\ 40 \end{array} \quad \begin{array}{r} 5.0 \\ 26 \end{array} \quad \begin{array}{r} 7.5 \\ 20-22 \end{array} \quad \begin{array}{r} 5.6 \\ 18 \end{array} \quad \begin{array}{r} 5.1 \\ 12 \end{array} \quad 4.6 \quad \begin{array}{r} 5.2 \\ 10 \end{array} \quad \begin{array}{r} 5.5 \\ 14 \end{array} \quad \begin{array}{r} 6.9 \\ 19-21 \end{array} \quad \begin{array}{r} 5.5 \\ 25 \end{array} \quad \begin{array}{r} 5.7 \\ 40 \end{array} \quad 30.8$$

$$4.7 \quad \begin{array}{r} 5.2 \\ 10 \end{array} \quad \begin{array}{r} 5.5 \\ 14 \end{array} \quad \begin{array}{r} 6.9 \\ 19-21 \end{array} \quad \begin{array}{r} 5.5 \\ 25 \end{array} \quad \begin{array}{r} 5.7 \\ 40 \end{array}$$

$$4.7 \quad \begin{array}{r} 5.2 \\ 10 \end{array} \quad \begin{array}{r} 5.7 \\ 14 \end{array} \quad \begin{array}{r} 6.8 \\ 18 \end{array} \quad \begin{array}{r} 7.2 \\ 40 \end{array} \quad 29.3$$

31.9

30.7

$$\begin{array}{r} 4.6 \\ 40 \end{array} \quad \begin{array}{r} 5.5 \\ 26 \end{array} \quad \begin{array}{r} 7.6 \\ 21-23 \end{array} \quad \begin{array}{r} 5.5 \\ 19 \end{array} \quad \begin{array}{r} 5.1 \\ 12 \end{array} \quad 4.9 \quad \begin{array}{r} 5.2 \\ 10 \end{array} \quad \begin{array}{r} 5.7 \\ 18 \end{array} \quad \begin{array}{r} 5.8 \\ 40 \end{array} \quad 30.7$$

31.7

30.6

$$\begin{array}{r} 4.5 \\ 40 \end{array} \quad \begin{array}{r} 5.3 \\ 27 \end{array} \quad \begin{array}{r} 7.3 \\ 21-23 \end{array} \quad \begin{array}{r} 5.3 \\ 17 \end{array} \quad \begin{array}{r} 4.8 \\ 13 \end{array} \quad 4.6 \quad \begin{array}{r} 5.4 \\ 17 \end{array} \quad \begin{array}{r} 5.3 \\ 25 \end{array} \quad \begin{array}{r} 5.6 \\ 40 \end{array} \quad 2$$

29.4

$$4.6 \quad \begin{array}{r} 5.0 \\ 11 \end{array} \quad \begin{array}{r} 5.7 \\ 18 \end{array} \quad \begin{array}{r} 6.4 \\ 27 \end{array} \quad \begin{array}{r} 6.8 \\ 40 \end{array}$$

Same as 6 + 25

31.4

30.2

$$\begin{array}{r} 4.8 \\ 40 \end{array} \quad \begin{array}{r} 5.2 \\ 26 \end{array} \quad \begin{array}{r} 7.1 \\ 23-21 \end{array} \quad \begin{array}{r} 5.2 \\ 17 \end{array} \quad \begin{array}{r} 4.6 \\ 9 \end{array} \quad 4.5 \quad \begin{array}{r} 4.9 \\ 11 \end{array} \quad \begin{array}{r} 6.6 \\ 18-20 \end{array} \quad \begin{array}{r} 6.1 \\ 21 \end{array} \quad \begin{array}{r} 5.7 \\ 30 \end{array} \quad \begin{array}{r} 6.0 \\ 40 \end{array}$$

Sta + π - Elev.

93620 ✓

6+29.5 Prop Line Lt.

6+60 & Kreck

32.1 ✓

+90 Prop Line Lt.

31.8 ✓

7 31.8 ✓

+50 31.8 ✓

8 31.7 ✓

+50 31.9 ✓

9 31.9 ✓

① 6.00 937.03 ✓ 5.17 931.03 ✓

+50 31.9 ✓

10 31.9

+50 32.0 ✓

+75 Prop Line Rt 32.0 ✓

Same as 6 + 25

31.2

Man hole - 932.18 30.6

$\frac{5.0}{15.0}$ $\frac{5.1}{45}$ $\frac{5.0}{26}$ $\frac{4.6}{13}$ 4.1 $\frac{4.2}{6}$ $\frac{4.9}{12}$ $\frac{6.3}{16}$ $\frac{6.6}{19}$ $\frac{5.6}{22}$ $\frac{5.6}{40}$

31.0

30.8

$\frac{5.2}{40}$ $\frac{5.3}{29}$ $\frac{6.0}{24}$ $\frac{7.3}{22-21}$ $\frac{5.5}{19}$ $\frac{4.6}{11}$ 4.4 $\frac{4.5}{6}$ $\frac{5.0}{12}$ $\frac{6.2}{16}$ $\frac{6.4}{20}$ $\frac{5.4}{24}$ $\frac{5.4}{40}$

4.4

30.8

30.7

$\frac{5.4}{40}$ $\frac{6.0}{24}$ $\frac{7.3}{22-21}$ $\frac{5.6}{16}$ $\frac{4.6}{10}$ 4.4 $\frac{4.7}{7}$ $\frac{5.0}{12}$ $\frac{6.6}{17}$ $\frac{6.4}{22}$ $\frac{5.8}{26}$ $\frac{5.5}{40}$

30.7

30.7

$\frac{5.5}{40}$ $\frac{6.4}{25}$ $\frac{7.5}{22-21}$ $\frac{6.6}{20}$ $\frac{6.7}{17}$ $\frac{5.0}{13}$ 4.5 $\frac{4.8}{6}$ $\frac{5.4}{11}$ $\frac{6.6}{15-18}$ $\frac{5.5}{21}$ $\frac{5.5}{40}$

30.4

30.6

$\frac{5.8}{40}$ $\frac{6.2}{22}$ $\frac{7.4}{20-21}$ $\frac{6.6}{19}$ $\frac{5.1}{14}$ $\frac{4.7}{10}$ 4.3 $\frac{4.9}{10}$ $\frac{5.3}{13}$ $\frac{6.6}{17}$ $\frac{5.7}{22}$ $\frac{5.6}{40}$

30.4

31.1

$\frac{5.8}{40}$ $\frac{6.4}{22}$ $\frac{7.4}{20-19}$ $\frac{6.2}{18}$ $\frac{6.0}{15}$ $\frac{5.0}{13}$ 4.3 $\frac{4.4}{7}$ $\frac{4.8}{13}$ $\frac{5.6}{16}$ $\frac{5.7}{19}$ $\frac{5.2}{25}$ $\frac{5.1}{40}$

Top 6' 4" Rt.

30.6

30.8

$\frac{6.4}{40}$ $\frac{4.5}{21}$ $\frac{7.8}{18-17}$ $\frac{6.6}{15}$ $\frac{5.1}{11}$ 5.1 $\frac{5.2}{8}$ $\frac{5.4}{12}$ $\frac{6.6}{16}$ $\frac{6.7}{19}$ $\frac{6.3}{21}$ $\frac{6.2}{40}$

31.2

30.8

$\frac{5.8}{40}$ $\frac{5.8}{20}$ $\frac{7.4}{17-16}$ $\frac{6.2}{15}$ $\frac{5.5}{12}$ 5.1 $\frac{5.2}{9}$ $\frac{5.8}{15}$ $\frac{6.8}{20-23}$ $\frac{5.8}{28}$ $\frac{6.0}{40}$

32.1

31.7

$\frac{4.9}{40}$ $\frac{5.0}{25}$ $\frac{5.6}{20}$ $\frac{6.9}{17-16}$ $\frac{5.7}{15}$ $\frac{5.4}{13}$ 5.0 $\frac{5.2}{10}$ $\frac{5.6}{15}$ $\frac{6.2}{20}$ $\frac{5.4}{33}$ $\frac{5.3}{40}$

32.1

31.8

$\frac{4.9}{40}$ $\frac{5.2}{20}$ $\frac{6.7}{17-16}$ $\frac{6.0}{15}$ $\frac{5.1}{14}$ 5.0 $\frac{5.4}{11}$ $\frac{5.8}{20}$ $\frac{5.4}{24}$ $\frac{5.2}{40}$

Sta + π - Elev

937.03 ✓

11+05

Street + Rt.

32.3 ✓

+35

Prop Line Rt

32.4 ✓

B.M.

1.66

936.90 ✓
3'

1.78

935.25

935.24 ✓

11+60

32.5 ✓

12

32.5 ✓

+50

32.7 ✓

+89

W Prop Line Wood Av. Lt

32.5 ✓

13

32.5 ✓

+19

E + E Prop Line Wood Av

32.4 ✓

+50

32.4 ✓

14

32.4 ✓

+50

32.1 ✓

15

32.0 ✓

manhole 4.65 = 932.38

4.7 $\frac{5.2}{11}$ $\frac{5.7}{21}$ $\frac{5.5}{50}$ $\frac{4.9}{100}$ ^{82.1}
33.7 33.7

31.4

$\frac{5.6}{40}$ $\frac{5.0}{20}$ $\frac{6.6}{17-16}$ $\frac{5.5}{15}$ $\frac{5.2}{13}$ 4.6 $\frac{4.8}{9}$ $\frac{5.7}{19}$ $\frac{3.3}{28}$ $\frac{3.3}{40}$

Top Hyd. 25' Lt Sta. 16+65

31.9

$\frac{5.0}{40}$ $\frac{4.6}{20}$ $\frac{6.4}{17-18}$ $\frac{5.3}{16}$ $\frac{4.8}{11}$ 4.4 $\frac{4.8}{11}$ $\frac{4.8}{21}$ $\frac{3.5}{28}$ $\frac{3.2}{34}$ ^{SW} 33.7

31.8

$\frac{5.1}{40}$ $\frac{5.5}{21}$ $\frac{6.7}{19-18}$ $\frac{5.4}{16}$ $\frac{4.8}{11}$ 4.4 $\frac{4.7}{14}$ $\frac{4.8}{21}$ $\frac{3.8}{28}$ $\frac{3.8}{35}$ ^{SW} 33.1

32.1

$\frac{4.8}{40}$ $\frac{4.4}{31}$ $\frac{5.1}{21}$ $\frac{6.4}{19-18}$ $\frac{5.2}{16}$ $\frac{4.8}{11}$ 4.2 $\frac{4.6}{14}$ $\frac{4.5}{22}$ $\frac{4.2}{28}$ $\frac{3.8}{35}$ ^{SW} 33.1

31.4

$\frac{5.5}{40}$ $\frac{5.5}{20}$ $\frac{6.7}{17-18}$ $\frac{5.4}{15}$ $\frac{5.0}{10}$ 4.4 $\frac{4.7}{14}$ $\frac{5.0}{22}$ $\frac{4.3}{28}$ $\frac{4.3}{35}$ ^{SW} 32.6

4.4

31.3

32.5 ^{SW} 32.6

$\frac{5.6}{40}$ $\frac{5.6}{20}$ $\frac{6.8}{17-18}$ $\frac{5.1}{15-10}$ 4.5 $\frac{4.8}{13}$ $\frac{5.1}{21}$ $\frac{4.4}{28}$ $\frac{4.3}{35}$

31.7

M.H. E132.54

32.5

$\frac{5.2}{40}$ $\frac{4.9}{21}$ $\frac{6.6}{16-17}$ $\frac{5.5}{14}$ $\frac{5.1}{10}$ 4.5 $\frac{4.9}{14-22}$ $\frac{4.4}{28}$ $\frac{3.5}{35}$ ^{SW}

32.1

32.3 32.2

$\frac{4.8}{40}$ $\frac{5.0}{22}$ $\frac{6.5}{17-18}$ $\frac{5.5}{15}$ $\frac{5.0}{9}$ 4.5 $\frac{4.8}{16}$ $\frac{4.8}{25}$ $\frac{4.6}{28}$ $\frac{4.7}{40}$

31.8

32.0

$\frac{5.1}{40}$ $\frac{5.1}{25}$ $\frac{5.7}{20}$ $\frac{6.3}{16-18}$ $\frac{5.4}{14}$ $\frac{5.0}{10}$ 4.8 $\frac{5.4}{15}$ $\frac{5.6}{22}$ $\frac{4.9}{28-35}$

31.7 31.2

32.0 31.4

$\frac{5.2}{40}$ $\frac{5.7}{24}$ $\frac{5.8}{20}$ $\frac{6.2}{17-19}$ $\frac{5.4}{16}$ $\frac{5.2}{10}$ 4.9 $\frac{5.5}{15}$ $\frac{5.7}{22}$ $\frac{4.9}{28}$ $\frac{4.9}{33}$ $\frac{5.5}{34}$

Sta	+	Σ	-	Elev
15 + 50		936.90		32.4
+85		W Prop Line 2nd Av.		32.6
16				32.5
+15		E 2nd Av		32.5
+45		E Prop Line 2nd Av.		32.3
B.M.	1.90	937.14	1.66	935.24
17				32.1
+50				32.4
18				32.8
+45				32.9
+75		E Florence		33.1
19				32.8
+05		Prop L. Lt.		32.8

32.9

31.6

SW
 $\frac{4.2}{35} \frac{4.4}{29} \frac{4.7}{22} \frac{6.0}{15-20} \frac{5.3}{17} \frac{4.9}{15} 4.5 \frac{4.6}{12} \frac{5.0}{17} \frac{5.2}{26} \frac{4.8}{28-33} \frac{5.3}{35}$

32.9 32.5

32.3 31.9

SW
 $\frac{4.0}{35} \frac{4.4}{29} \frac{4.6}{23} \frac{5.7}{19-21} \frac{4.9}{18} \frac{4.5}{9} 4.3 \frac{4.6}{12} \frac{5.4}{20} \frac{4.6}{28} \frac{5.0}{35}$

4.4

32.9

32.5

$\frac{4.0}{35} \frac{4.3}{29} \frac{4.8}{22} \frac{5.5}{19-21} \frac{4.7}{17-7} 4.4 \frac{4.4}{12} \frac{4.2}{20} \frac{4.4}{30} \frac{4.4}{100}$

32.8 32.6

M.H. El. 932.41
32.3 32.3

$\frac{4.1}{40} \frac{4.3}{29} \frac{4.9}{22} \frac{5.9}{20-21} \frac{4.9}{18} \frac{4.9}{10} 4.6 \frac{4.8}{13} \frac{5.3}{22} \frac{4.6}{28} \frac{4.6}{35}$

Top Hyd

32.7

M.H. @ 2nd 4.73

M.H. @ Woid 4.60

32.3

33.0

$\frac{4.4}{40} \frac{4.4}{29} \frac{5.8}{22} \frac{5.5}{18} \frac{5.3}{12} 5.0 \frac{5.3}{16} \frac{5.2}{22} \frac{4.8}{28} \frac{4.3}{33} \frac{4.1}{40}$

32.3

32.6

$\frac{4.8}{40} \frac{4.4}{29} \frac{4.6}{24} \frac{5.8}{22} \frac{5.2}{18} \frac{5.1}{11} 4.7 \frac{4.9}{13} \frac{4.9}{22} \frac{4.7}{28} \frac{4.5}{40}$

32.7 32.7

32.5 32.8

$\frac{4.4}{40} \frac{4.4}{29} \frac{4.5}{25} \frac{5.6}{22} \frac{5.1}{18} \frac{4.9}{10} 4.3 \frac{4.6}{12} \frac{4.8}{22} \frac{4.6}{28} \frac{4.3}{40}$

33.0

32.8

$\frac{4.1}{40} \frac{4.2}{29} \frac{4.6}{24} \frac{5.4}{21} \frac{5.0}{18} \frac{4.8}{11} 4.2 \frac{4.6}{13} \frac{4.8}{25} \frac{4.5}{28} \frac{4.3}{40}$

33.3

M.H. 4.05 @ Florence

El. 32.09
32.5

$\frac{3.8}{100} \frac{3.8}{50} \frac{4.0}{25} \frac{4.1}{11} 4.0 \frac{4.6}{12} \frac{4.7}{23} \frac{4.4}{28} \frac{4.6}{40}$

4.3

32.3 32.8

32.3

32.7

$\frac{4.8}{40} \frac{4.3}{35} \frac{4.7}{29} \frac{5.2}{21} \frac{4.5}{20} \frac{4.5}{17} \frac{4.5}{12} 4.3 \frac{4.8}{16-28} \frac{4.4}{40}$

Sta	+	π	-	Elev.
19+50		937.14 ✓		32.6 ✓
20				32.6 ✓
B.M.	2.01	937.25 ✓		935.24 ✓
+50				32.8 ✓
+95		W Prop Line		32.9 ✓
21+25		4 1st		32.9 ✓
+55		E Prop Line		32.8 ✓
22				33.0 ✓
+50				33.1 ✓
23				33.1 ✓
+50				33.2 ✓
24				33.1 ✓
⊙	4.71	937.99 ✓	3.97	933.28 ✓
+50				33.1 ✓

32.5

32.7

$$\frac{4.6}{40} \frac{4.2}{32} \frac{4.3}{29}$$

$$\frac{5.3}{21} \frac{5.0}{12} 4.5 \frac{4.9}{17} \frac{4.6}{28} \frac{4.4}{40}$$

32.4

32.9

32.5 32.7

$$\frac{4.7}{40} \frac{4.1}{33} \frac{4.2}{29} \frac{4.8}{21} \frac{5.2}{20} \frac{4.9}{12} 4.5 \frac{5.0}{16} \frac{5.0}{18} \frac{4.6}{28} \frac{4.4}{40}$$

Top Hyd 25' Lt Sta. 16+65

32.9

SW 32.3

$$\frac{4.3}{40} \frac{4.4}{29} \frac{5.5}{20} \frac{4.8}{9} 4.5 \frac{5.0}{14} \frac{5.1}{24} \frac{4.7}{28} \frac{4.9}{36}$$

33.2 32.8

32.5 32.0

$$\frac{4.1}{40} \frac{4.4}{29} \frac{4.7}{22} \frac{5.3}{20} \frac{4.8}{10} 4.4 \frac{5.0}{15} \frac{5.1}{24} \frac{4.5}{26} \frac{4.7}{28} \frac{5.2}{40}$$

33.2

SW

MH 4.33

32.5

$$\frac{4.1}{40} \frac{4.4}{29} \frac{4.7}{22} \frac{5.3}{20} \frac{4.8}{12} 4.4 \frac{5.0}{16} \frac{4.8}{28} \frac{4.8}{50-100}$$

32.9

32.8

$$\frac{4.3}{40} \frac{4.4}{29} \frac{4.9}{21} \frac{5.5}{20} \frac{4.9}{12} 4.5 \frac{4.6}{12} \frac{5.1}{18} \frac{5.2}{24} \frac{4.4}{28} \frac{4.5}{33} \frac{5.5}{36} \frac{4.5}{43}$$

32.7 32.1

32.7 32.2

$$\frac{4.4}{40} \frac{4.4}{29} \frac{4.6}{22} \frac{5.2}{20} \frac{4.7}{10} 4.3 \frac{5.1}{19} \frac{5.3}{24} \frac{4.4}{28} \frac{4.7}{40}$$

33.1

32.4

$$\frac{4.1}{40} \frac{4.3}{29} \frac{4.6}{22} \frac{5.0}{21} \frac{4.6}{9} 4.2 \frac{5.1}{19} \frac{5.2}{26} \frac{4.5}{29} \frac{4.8}{40}$$

32.8 32.9

32.8 32.8

$$\frac{4.4}{40} \frac{4.3}{29} \frac{4.6}{22} \frac{5.0}{21} \frac{4.6}{10} \frac{4.0}{40} 4.2 \frac{5.2}{20} \frac{5.2}{25} \frac{4.4}{29} \frac{4.4}{33}$$

32.8

33.1

$$\frac{4.4}{40} \frac{4.2}{29} \frac{5.1}{21} \frac{4.7}{20} \frac{4.7}{9} 4.1 \frac{5.1}{20} \frac{5.1}{25} \frac{4.4}{29} \frac{4.2}{40}$$

32.8 32.9

33.0 32.8

$$\frac{4.4}{40} \frac{4.3}{29} \frac{4.7}{21} \frac{5.1}{20} \frac{4.8}{13} 4.2 \frac{5.2}{20} \frac{5.2}{26} \frac{4.2}{29} \frac{4.4}{40}$$

32.8

33.3

$$\frac{5.2}{40} \frac{4.9}{30} \frac{5.2}{22} \frac{5.8}{20} \frac{5.3}{7} 4.9 \frac{5.9}{21} \frac{5.7}{25} \frac{5.1}{29} \frac{4.7}{40}$$

Sta	+ X 937.99	-	Elev
25			33.2
+50			33.2
26 +05	W Prop line Bald Eagle		33.2
+20			33.1
+26	Edge Pavement		32.89
	± Pavement		33.00
BM	4.12	933.27	933.29 East SW 933.14

33.2 33.2

33.0 33.2

$\frac{4.8}{40} \frac{4.8}{30} \frac{5.1}{21} \frac{5.6}{20} \frac{5.2}{9} 4.8 \frac{5.1}{13} \frac{5.8}{21} \frac{5.0}{29} \frac{4.8}{40}$

33.5

33.5

$\frac{4.5}{40} \frac{4.8}{29} \frac{5.0}{18} \frac{5.3}{17} 4.8 \frac{4.8}{12} \frac{5.5}{22} \frac{4.9}{29} \frac{4.5}{40}$

34.2 34.0

33.3 33.3

SW SW

$\frac{3.8}{40} \frac{4.0}{29} \frac{4.6}{29} \frac{4.8}{15} 4.8 \frac{4.8}{13} \frac{4.9}{21} \frac{4.7}{29} \frac{4.7}{40}$

+12 M.H.Lt. 4.75 = 933.24

33.5

33.3

SW-Cor.

$\frac{4.7}{40} \frac{4.8}{31} \frac{4.7}{15} 4.9 \frac{5.1}{15} \frac{5.0}{27} \frac{4.62}{30} \frac{4.5}{40}$

Cor SW 4.10 = 933.89

+23 M.H. 4.80 = 933.18

33.0

33.0

$\frac{4.95}{50} \frac{4.95}{25} 5.10 \frac{4.95}{25} \frac{4.95}{50}$

$\frac{4.67}{20} \frac{4.74}{100} \frac{4.76}{50} 4.95 \frac{5.00}{25} \frac{5.03}{50} \frac{5.00}{100} \frac{4.82}{200}$

Lt-C.M. 5.02

U.S.G.S. St. Marys School Yard

SW
18.5
0

11.57 Storm Seyer #
18150. on Built Eagle A
5'E. of E Edge Rave
Elev. 926.42

