

OFFICE OF COUNTY ENGINEER
RAMSEY COUNTY, MINN.

PLAN

Survey

Co. Ro. "F"

From

McMenemey

To

Centerville

Road Acc't. No.

12

Date Filed

9-9-81
1976

File

13-54

KP
RJ
GA

26 FEB 1976
SUNNY 55°

1.

Co. RD F

McMenemy to Centerville RD

ALINEMENT

STA	POINT	ΔLT	ΔRT	CURVE DATA
+51 ⁴²	PT		4°04'	Δ 8°08'
+50			4°02.4	D 4°
64			3°02.4	T 101.84
+50	PI		2°02.4	L 203.33
63			1°02.4	R 1432 ³⁹
+50			0°02.4	
62+48 ¹⁶	PC		0°00	
61+02 ⁹⁵	PI	0°16.0		

KP
GA
RJ

LT

Σ

27 FEB 1976
SUNNY 58° RT

2.

□

McMENEMY

STA	POINT	ΔL	ΔR	CURVE DATA
-----	-------	------------	------------	------------

$$68+04.74 = 68+02.77$$

+04.74	PT	4°04'
--------	----	-------

68		3°58.3'
----	--	---------

+50		2°58.3'
-----	--	---------

+03.25	PI	—
--------	----	---

67		1°58.3'
----	--	---------

+50		0°58.3'
-----	--	---------

66+01.41	PC	0°00'
----------	----	-------

KP
GA
RJ

LT

~~E~~

27 FEB 1976 3.
RT

STA	POINT	ΔL_T	ΔR_T	DATA
-----	-------	--------------	--------------	------

100+61 $\xrightarrow{13}$ POT

43
87+31~~40~~ POT

$$73 + 48 \underline{27}$$
 $0^{\circ}24'$

KP
GA
RU
YJ

LT

E

3 14 MK
SUNNY 55° RT

1976 4

SEE COR BAR
PRIVATE SPOT FOUNDATION



84.65

PK 37.78

RR SPIKE

P.R. IN PARKING LOT

84.75

92.38

45.15

PK

PK

TACK IN
HUB



106.49

Iron

50.0

PK

(Make Ties)

DISC IN
PP

37.67

94.05

TACK IN
HUB

GRP

DISC
ON TOP

30.51

MC#20



50.0

SPIKE

59.20

81.44

HUB BY TREE

PK

STA POINT LT Δ RT CURVE DATA

140+01⁴⁹

1319.58

126+81.91

2641.31

2639.16

- 2.15

1321.73

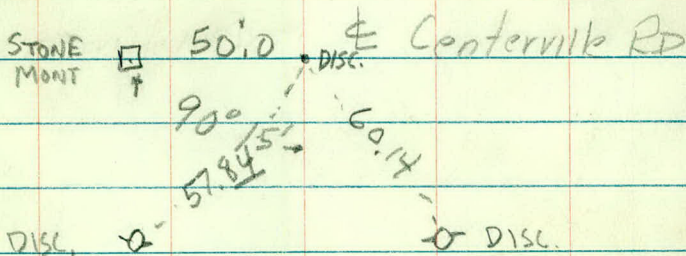
19.53

2.20

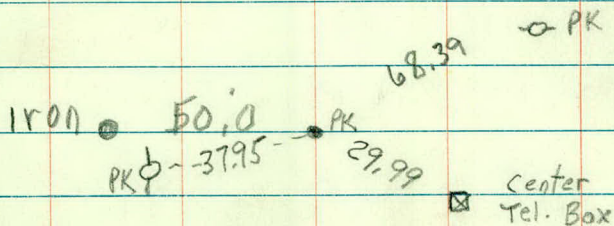
113+60¹⁸ P1 0°14'0

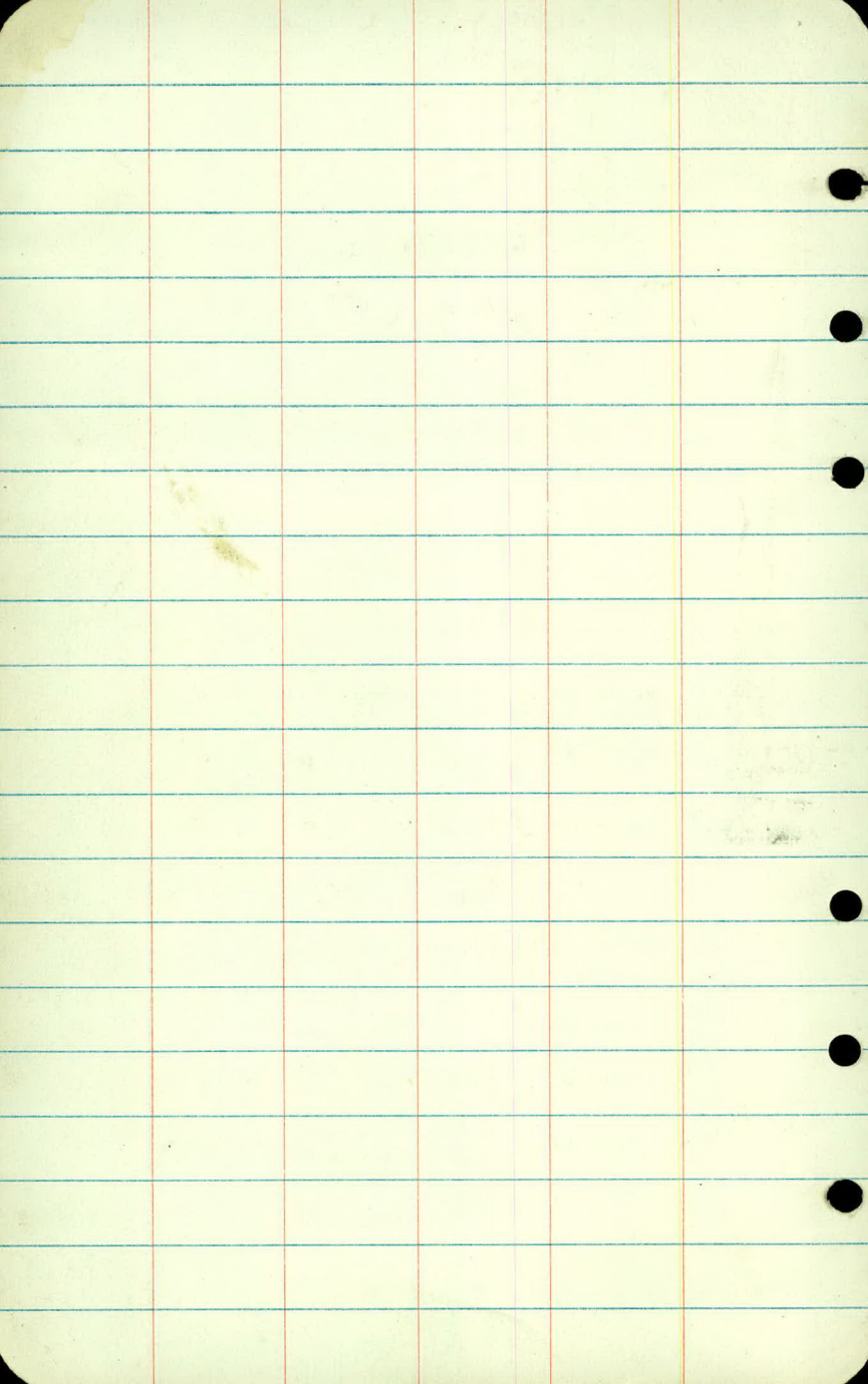
LT

3 MAR 1976 5.
RT



Granite $\square$ 50.05'





WJ
RG
RJ

11-16-76
CLEAR

6

TIES TO IRONS ON CO. RD. F

74+55.74 Rt 42.84

76+10.16 Rt 42.78

77+64.21 Rt 43.38

79+18.31 Rt 42.54

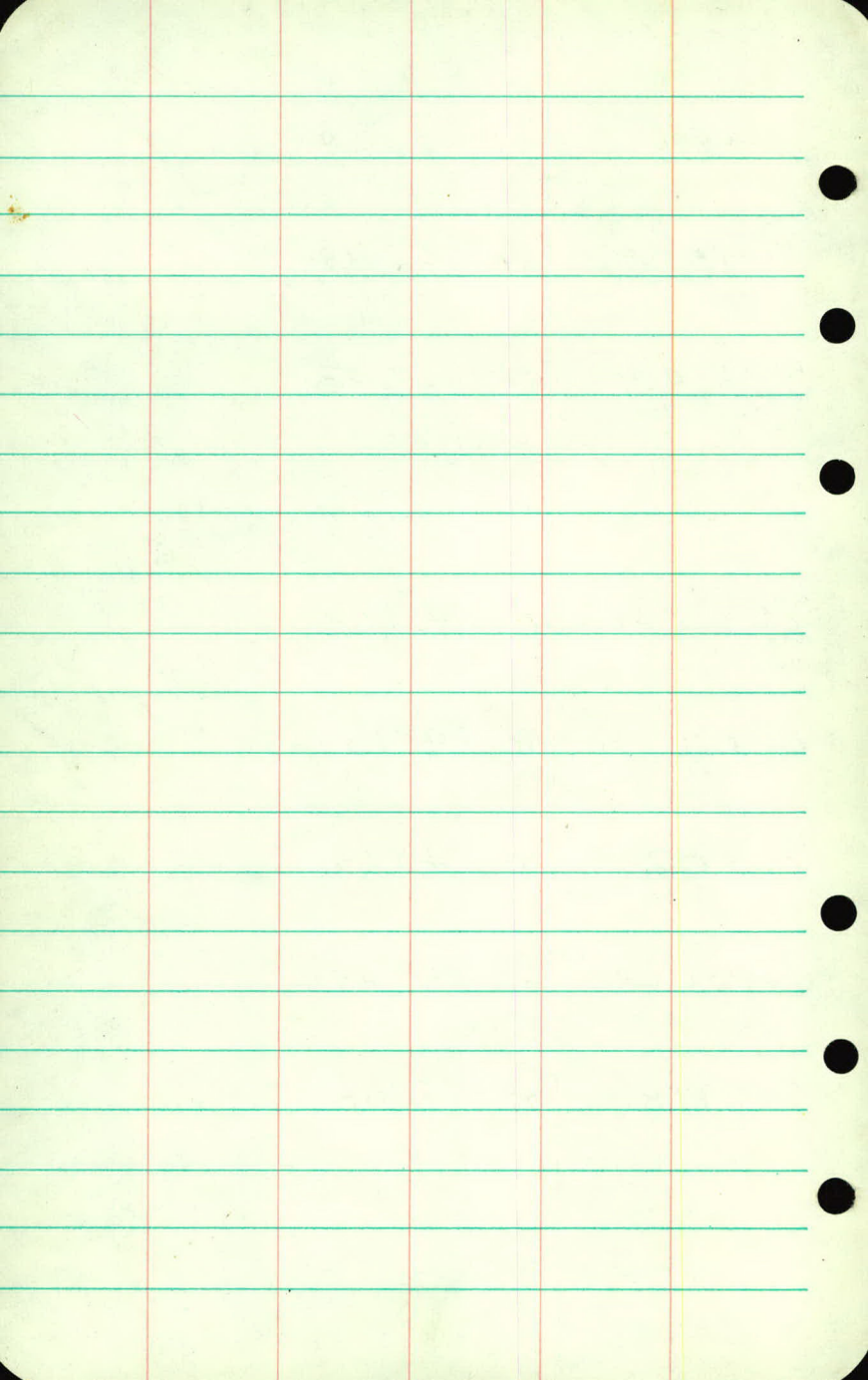
80+72.41 Rt 42.98

82+26.58 Rt 43.13

83+80.80 Rt 43.19

85+56.08 Rt 43.48

86+97.81 Rt 42.98



July 28, 1966

4

TOPOGRAPHY

55

Fe
38

54

+99 E. Fe
38Fe
35

53

Fe
40Fe
35+17 P.P.
27Fe
33Fe
35

52

+84 Rtie
X-Fe+78 X-Cor.
28Fe
26Fe
26

51

+45 FeCor
36+61 Rtie
FeFe
36

50

July 1, 1963

5

x

60

Lx

$$\frac{\text{B.T.}}{2-27}$$

Rt.

$$\frac{\text{B.T.}}{+506-22}$$

59

$$\frac{\text{B.T.}}{10-19.5}$$

$$+82 \frac{\text{PP}}{34}$$

$$+60 \frac{\text{Ent}}{20}$$

$$+71 \frac{\text{IP}}{28}$$

$$+30 \frac{\text{Eh}^+}{5.5}$$

58

$$\frac{\text{BT}}{11-17}$$

$$+87 \frac{\text{N.W. Cor Ho N28S E37W}}{86}$$

$$+81 \frac{\text{PP} \#76}{28}$$

$$+56 \frac{\text{Ent}}{24}$$

$$+41 \frac{\text{NW Cor Gar}}{92}$$

57

$$\frac{\text{BT}}{11-16}$$

$$+39 \frac{\text{IP}}{29}$$

$$+84 \frac{\text{Fe Cor}}{85}$$

56

$$+27 \frac{\text{L in Fe}}{37}$$

$$\frac{\text{B.T.}}{11-11}$$

$$\frac{\text{Fe}}{37}$$

$$+37 \frac{\text{PP}}{28}$$

15

55

$$\frac{\text{B.T.}}{11-11}$$

$$\frac{\text{Fe}}{37}$$

FA
BZ
JM
FK

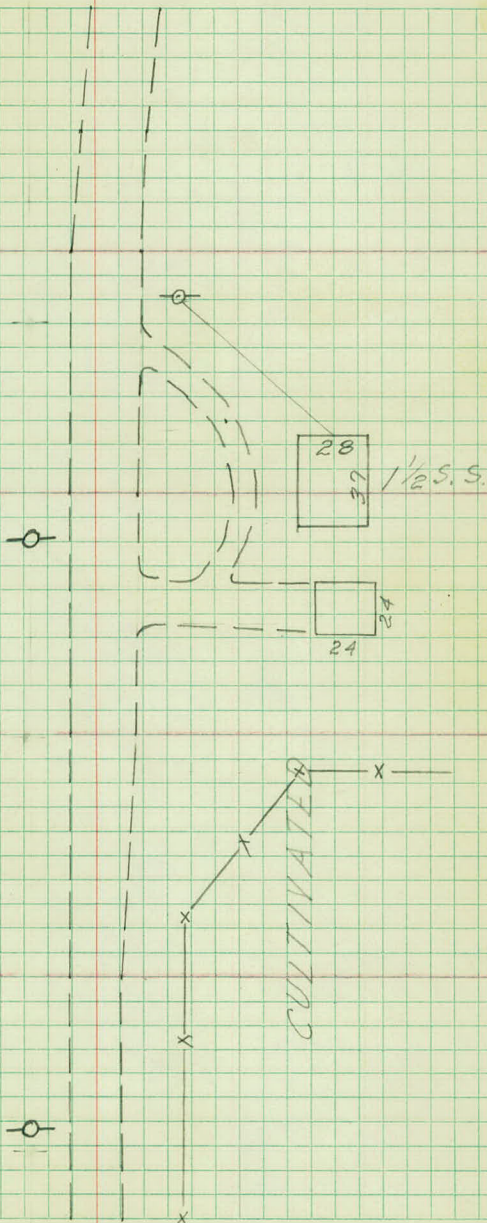
July 3, 1963

Rt

6

Lt

+



65

Lt

£

Rt.

$$+35 \frac{PP}{40}$$

$$+30 \frac{PP}{1}$$

64

$$\frac{BT}{37-62}$$

63

$$\frac{BT}{37-63}$$

62

$$\frac{B.T.}{33-61}$$

$$+51 \frac{ER}{28}$$

End of Brush

$$+35 \frac{TP}{3}$$

$$+53 \frac{ER}{60}$$

$$+38 \frac{PP}{29}$$

150

Begin Brush

$$+29 \frac{POR}{18}$$

$$+23 \frac{TEL}{18}$$

$$+27 \frac{POR}{74}$$

$$+27 \frac{GP}{90}$$

61

$$+16 \frac{BR}{£}$$

$$+13 \frac{BR}{105}$$

$$+90 \frac{ER}{50}$$

$$+90 \frac{ER}{85}$$

$$+41 \frac{G.P.}{29}$$

$$+85 \frac{POR}{30}$$

$$+80 \frac{POR}{60}$$

$$+80 \frac{Arc Lite}{80}$$

$$+53 \frac{BT}{10}$$

$$+72 \frac{BR}{15}$$

$$+61 \frac{BR}{43}$$

$$+30 \frac{BT}{33}$$

60

$$Z$$

RT.

70 Φ Brush Lt
50

Φ BT
11-12

RT

End of Brush

+96 $\frac{PP}{37}$

+05 $\frac{PP}{36}$

+43 $\frac{Tw 6'' 0}{43}$

+12 $\frac{14'' 0}{47}$

+14 $\frac{PP}{34}$

69

BT
10-13

+04 $\frac{Tw 12'' 0}{47}$

+69 $\frac{3-6'' 0}{42}$

+78 $\frac{2-8'' 0}{47}$

+50 BT
11-14

+51 $\frac{7-5'' 0}{45}$

+32 $\frac{18'' 0}{52}$

68

BT
5-17

+06 $\frac{12'' 0}{45}$

+94 $\frac{\Phi Ent}{18''}$

+50 BT
2-21

+65 $\frac{Tw 12'' 0}{48}$

+38 $\frac{PP}{34}$

+37 $\frac{GP}{27}$

+54 $\frac{12'' 0}{47}$

+36 $\frac{12'' 0}{48}$

67

BT
3-28

+14 $\frac{PP}{33}$

66

BT
16-42

+50 BT
23-47

+14 $\frac{SE 18'' SCP}{63}$

65

+06 $\frac{BT NE 18'' SCP}{31-54 20}$

July 3, 1963

8

Lt.

Φ

Rt

000

0

0

0

0

0

111

00

00

00

00

00

00

00

00

00

00

+50

RED
12 13

+28 4" P 37 +40 4" P 37

+11 15" CMP 24 +12 11" Ash 37

72

RD +100 ± 16.0 & tent
12

+92 RD +70 End Conc Steps
14 30-41

+89 15" CMP

+66 Berg Conc Steps 24
30-41

+50

RD
12 14

+44 MH
31

+13 PP
41

71

RD
11 14

+79 PP
35

+75 ± 14.0 B.t. cont.

+50

RD
11 13

+33 TEL CABLE X-SING

70

RD
11 12

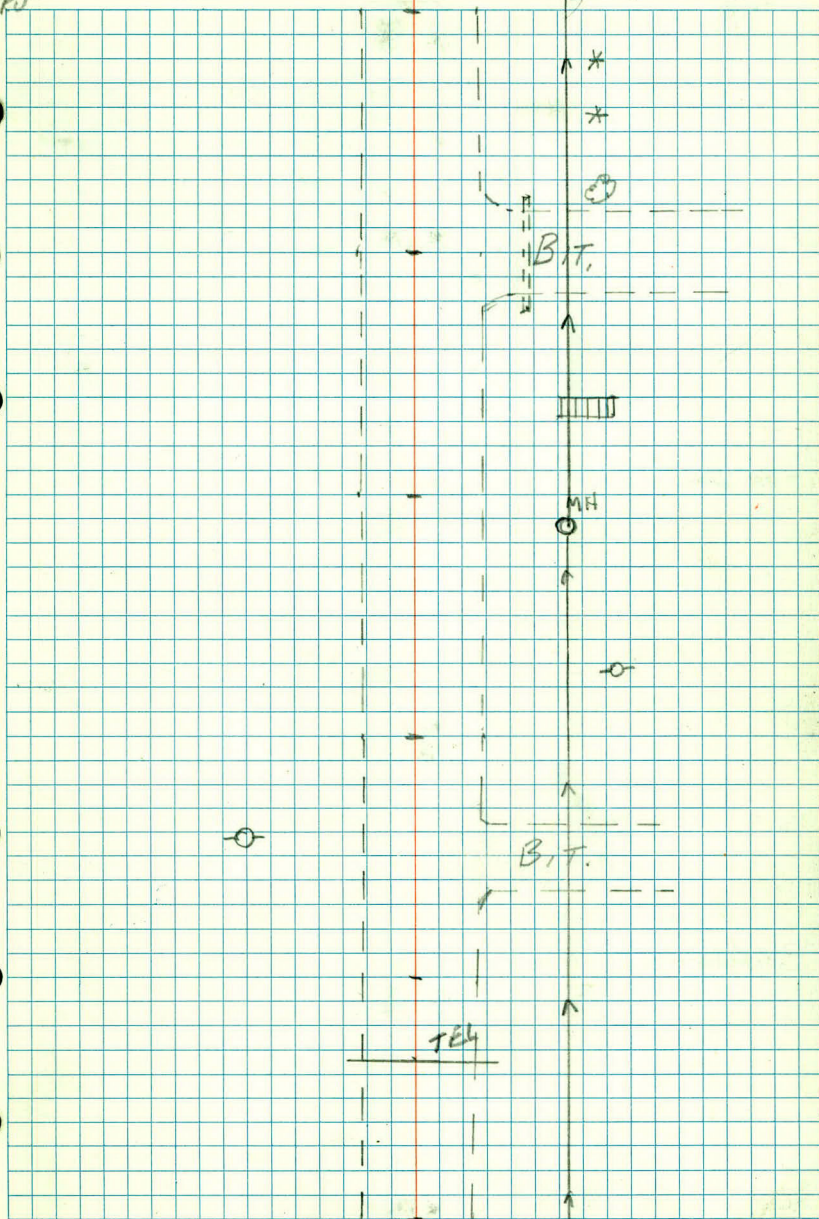
KP
DS
GA
RJ

LT

3 MAR 1976
SUNNY 30°

RT

9.



75

LT

RD FE RT
12 12 50

+75 RT FE

+55 ER
13+69 Fe Cor
50

+50

RD
12

+35 PP

+30 PP

+25 BR

+02 RT
28
23+02 $\frac{1}{2}$ OAK RD

74

+96 RT RD RD
12Fe
46

+90 Cor BT

+96 MH
32+72 GP
26+79 GP
29
26+86 GP
26+65 BT
30+65 GP
26+54 RD
21

+52 RT FE

+50

conc

RD

66-76

+48 MONT

15

+33 SE Cor Ho

+33 15" CM +42 FE Cor

+33 Conc
67+22 $\frac{1}{2}$ 10' DIET COT
31 43

+11 SW Cor Ho

+12 15" CMP
3073 +01 PP +05 TEL Box
34 46RD
12 13+78 (3) 12" O
50+55 4" P
37

72 +50

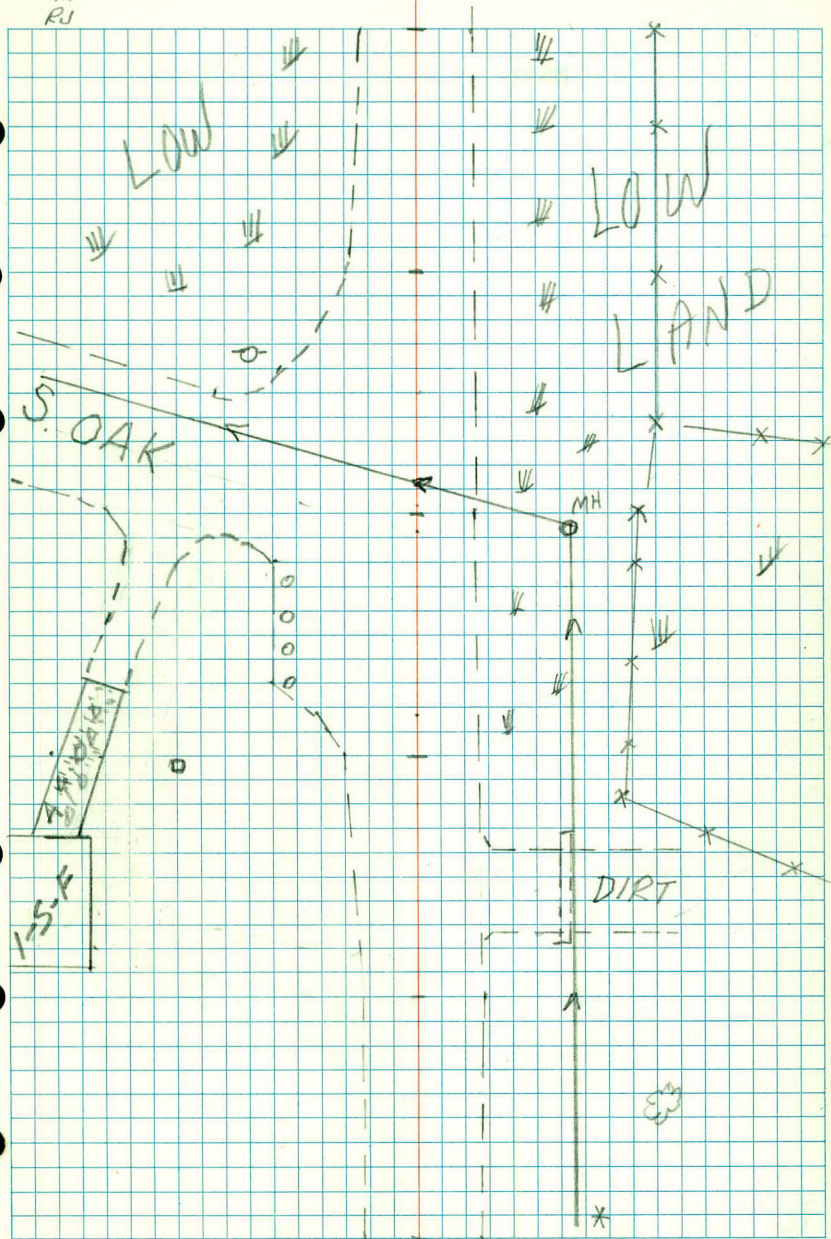
RD
12 13

KP
DS
GA
RJ

3 MAR 76

10.

£



+50

~~RD~~
RD
13 12

FE
59

77

RD
13 12

FE
60

+50

RD
12 12

FE
58

76

RD
11 12

FE
56

+50

RD
12 12

FE
53

75

RD
12 12

FE
50

KP
DS
SA
RU

LT

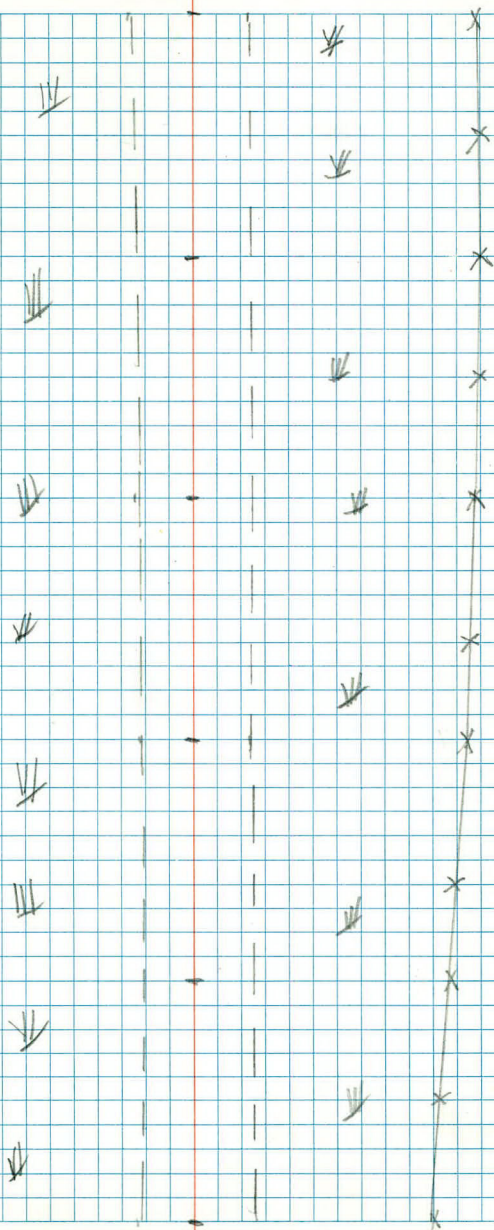
E

3 MAR 76

RT

11.

2007



80

 $\frac{RD}{13/12}$ $\frac{FE}{53}$

+50

 $\frac{RD}{13/12}$ $\frac{FE}{54}$

79

 $\frac{RD}{14/11}$ $\frac{FE}{55}$

+50

 $\frac{RD}{14/12}$ $\frac{FE}{56}$

78

 $\frac{RD}{14/12}$ $\frac{FE}{58}$ +62 PP
35

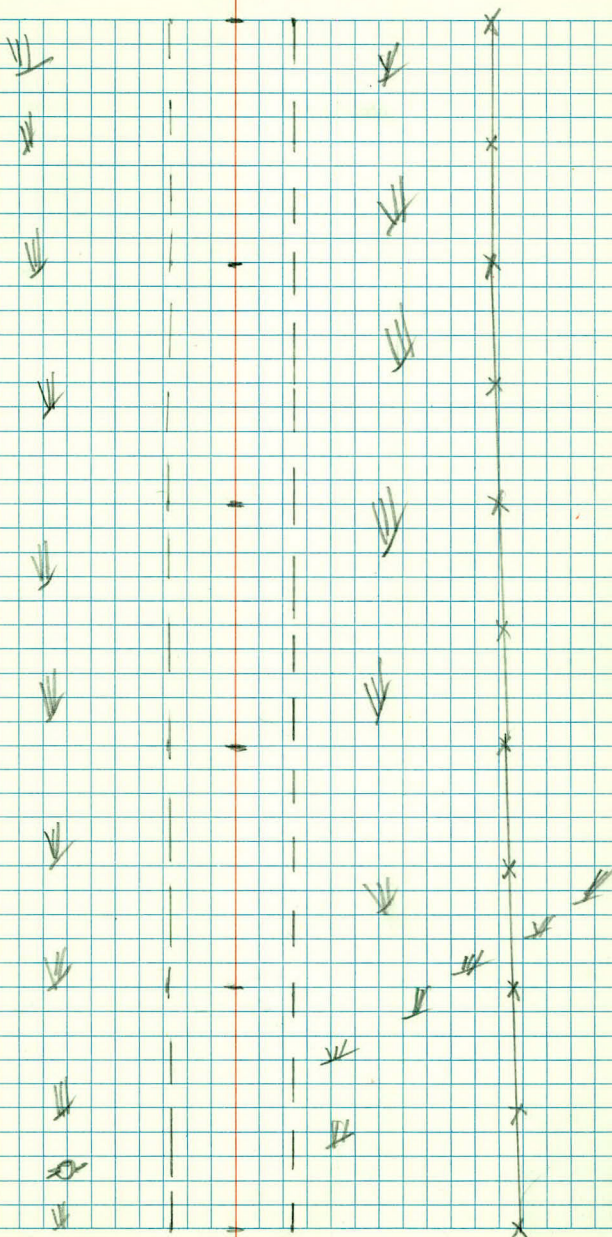
77+50

 $\frac{RD}{13/12}$ $\frac{FE}{59}$

KP
DS
SA
RD

£ 3 MAR 76 12

LOW



+50

✓
RD
12 12

✓
WOODS
49

82

✓
RD
12 12

✓
WOODS
50-5

+68 END FE
48

+50

✓
RD
13 12

✓
FE
49

+45 Begin Woods
65-5

✓
+12 PP
37

81

✓
RD
14 12

✓
FE
51

+50

✓
RD
14 12

✓
FE
52

80

✓
RD
13 12

✓
FE
53

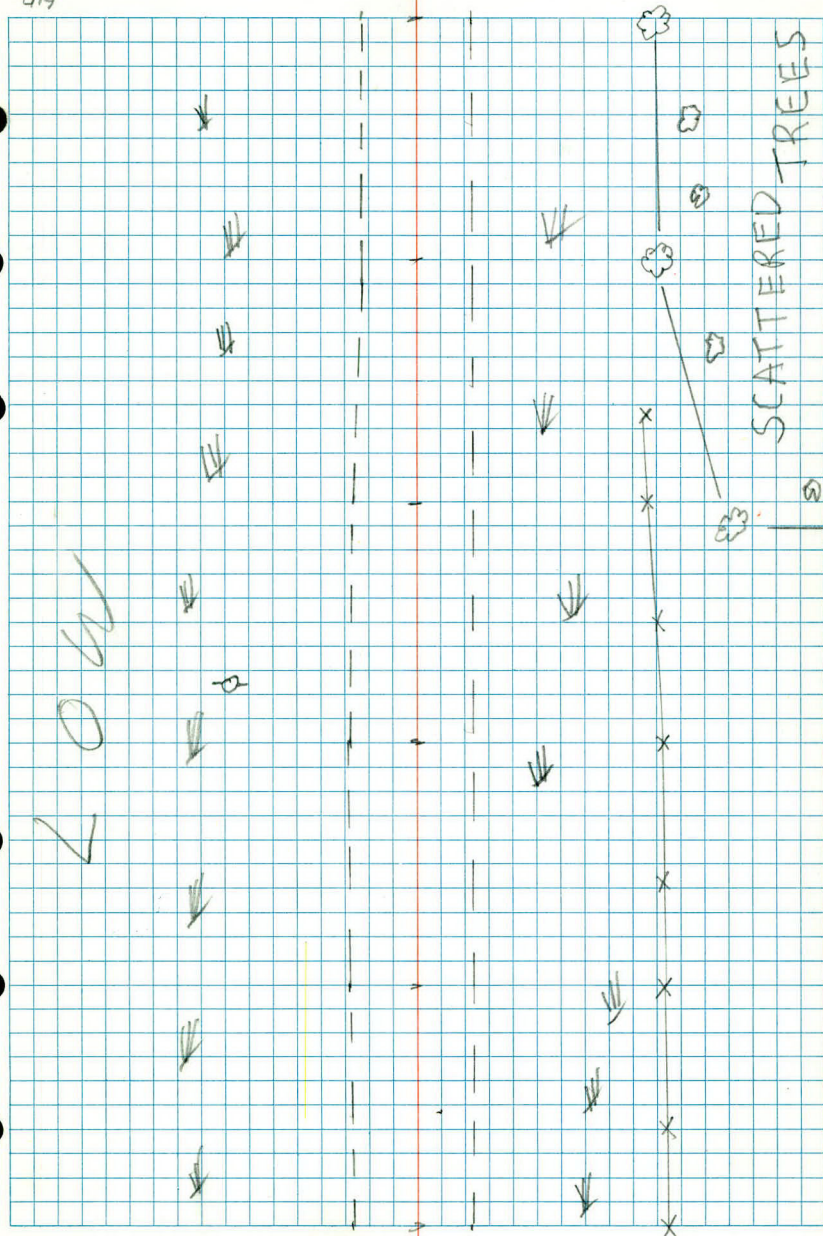
RP RJ
AS TJ
GA

4 MAR 76
CLOUDY 22°

13

LOW

SCATTERED TREES



85

✓
RD
13 12

✓
WOODS
50

+50

✓ ✓
RD
12 12

✓
WOODS
50

↓
+30 PP
38

84

✓ ✓
RD
12 12

✓
WOODS
50

✓
+65 24" Culvert
26

+50

✓
RD
12 12

✓
+65 Culvert
23
↓
WOODS
49

83

✓ ✓
RD
13 12

✓
WOODS
48

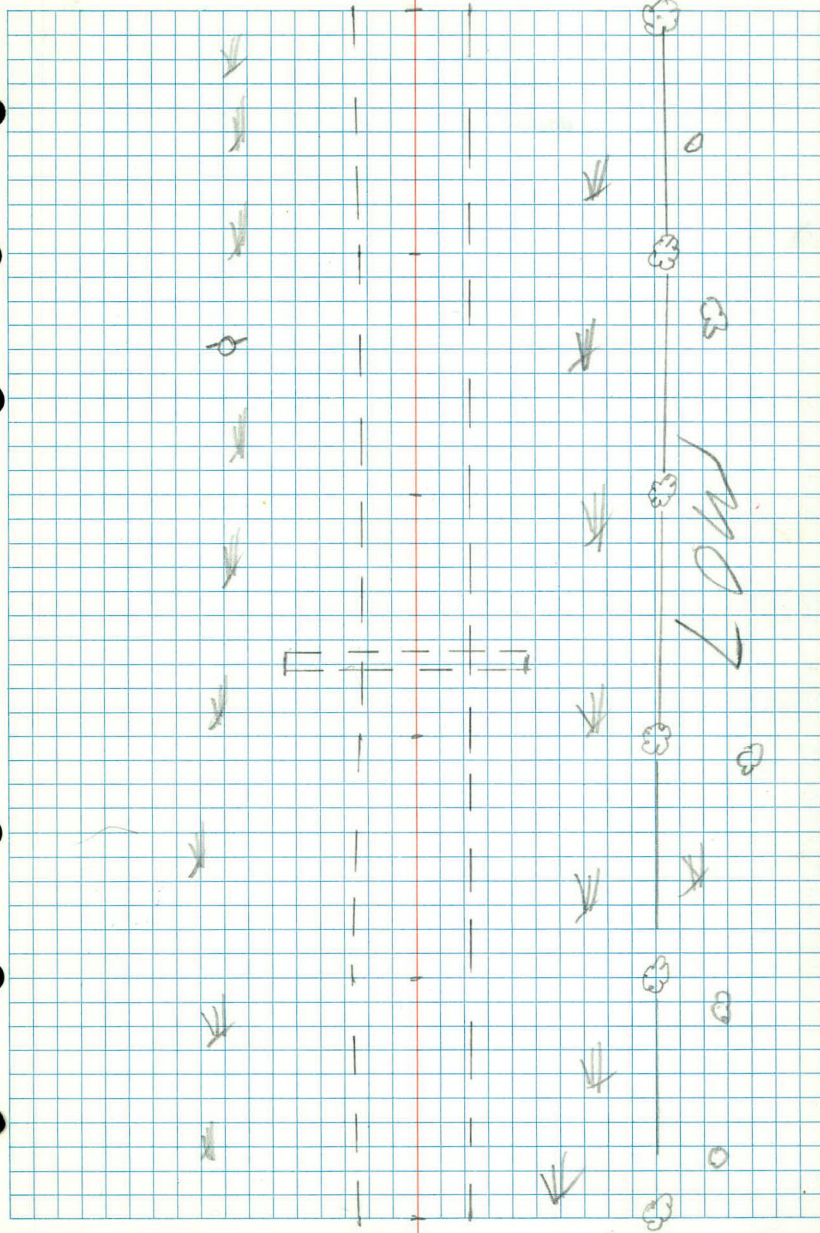
82+50

✓ ✓
RD
12 12

✓
WOODS
49

KPRJ
DS TJ
GA

4 MAR 1976 14



+50 LT

✓
RD
13 11

RT

✓
+31 Iron
50

✓
+31 5' ELM

56 +31 PP

39

87

✓ ✓
RD
14 11

✓
+95 TW 10' ELM
53

✓
+63 END FE
56

+50

✓
RD
13 11

✓
+30 END WOODS
51 - 5

86

✓
RD
13 11

✓
FE
51

✓
WOODS
51

+50

RD
13 12

FE
51

WOODS
50

✓
+40 Begin FE
51

85

✓
RD
13 12

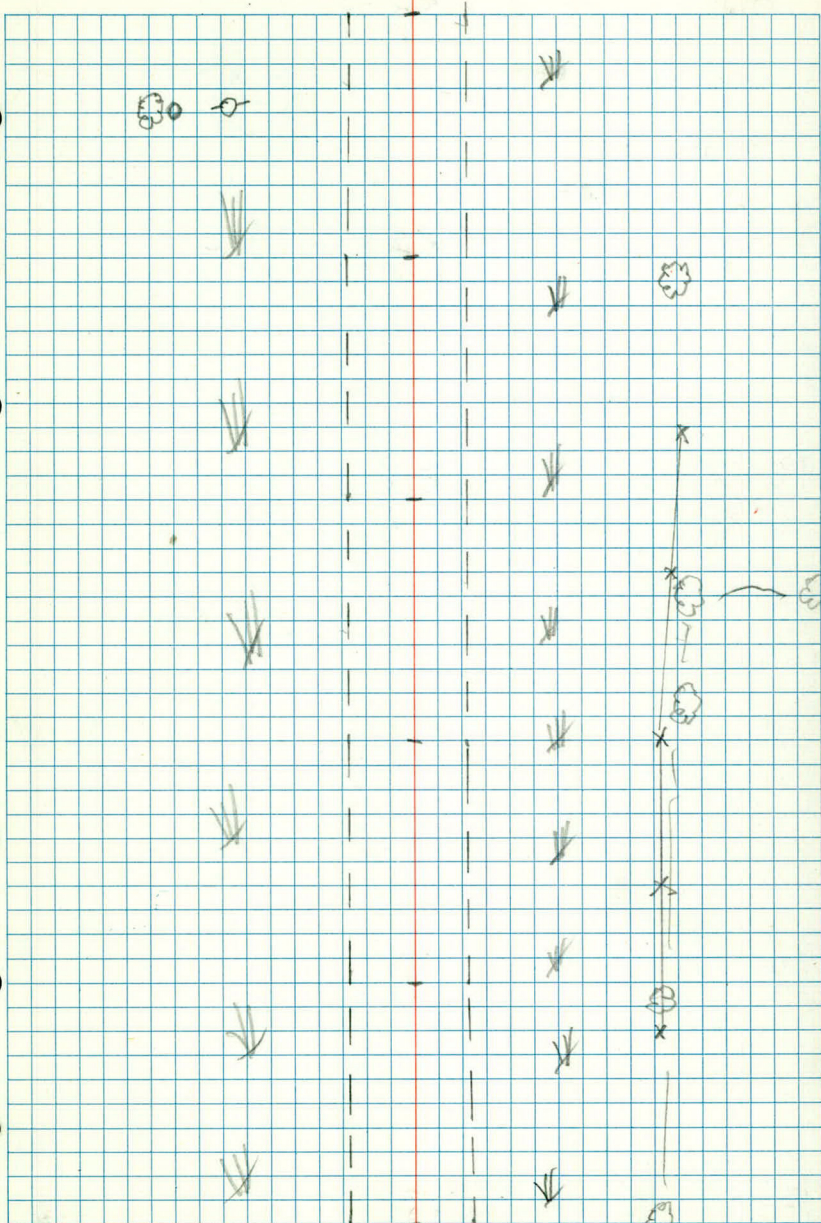
✓
WOODS
50

KP RJ
DS TJ
GA

4 MAR 1976

15

2



90

LT

✓
RD
13 12

RT

WOODS
36✓
+61 Beg Brush
47-57

+50

✓
RD
13 12

89

✓
RD
13 11✓
+05 COR Woods
65

+50

✓
RD
13 11✓
+74 Begin Woods
100

88

✓
RD
13 11

87+50

✓
RD
13 11

KARU
PS TI
GA

4 MAR 1976 16

+

Plush



Low

+50

✓
RD
13 11

✓
WOODS
40

92

✓
RD
13 11

✓
WOODS
39

+50

✓
RD
13 11

✓
WOODS
39

✓
+39 END GATE

³²
+22 ~~E~~ 34' ENT

✓
+43 END FE
57

✓
+05 Begin gate
34

91

RD
13 11

WOODS
42-5

FE
57

✓
+80 Begin FE

✓
+90 END FE
33

✓
+72 ⁴¹ PP
39

+50

✓
RD
13 12

✓
+40 Begin FE
57

✓
+35 END Brush
50-55

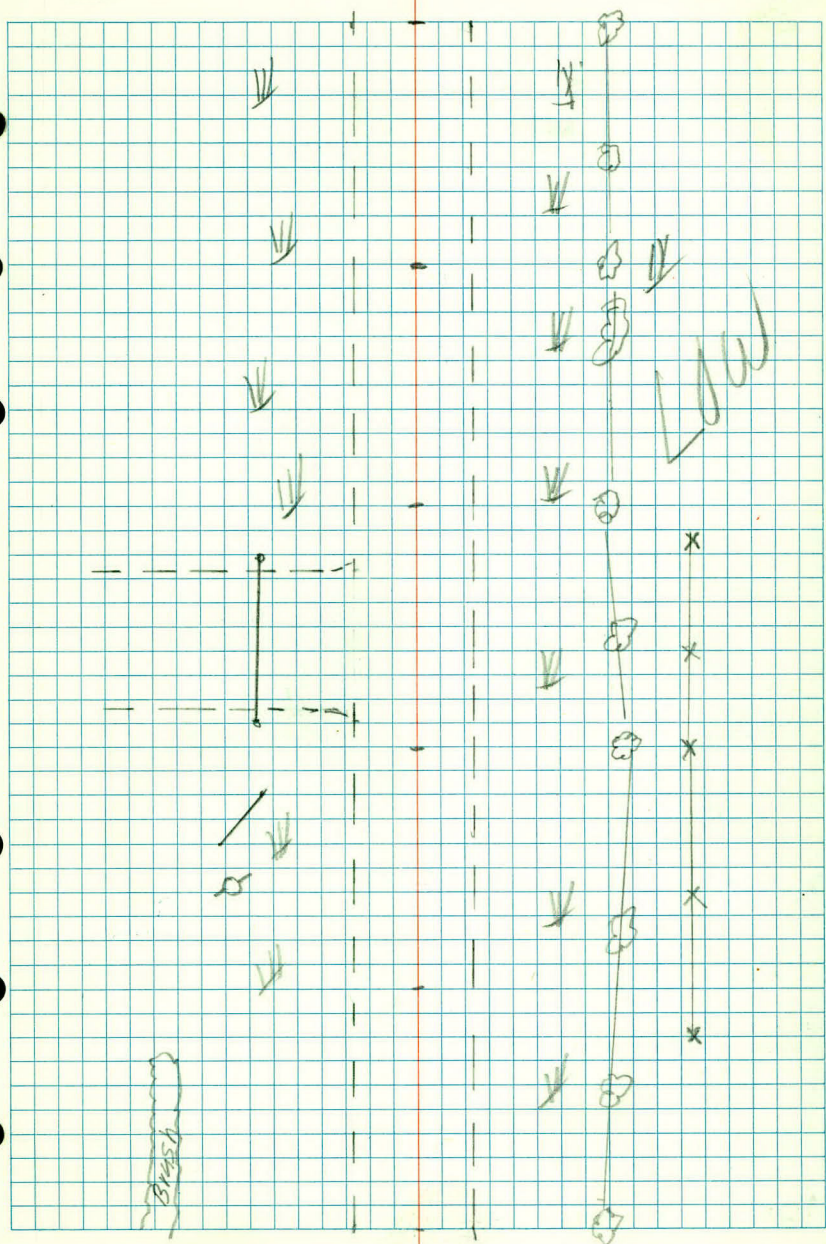
90

✓
RD
13 12

✓
WOODS
36

KP R
DS TV
68

4 MAR 1976 17



95

✓
✓RD✓
12 12

+50

✓
✓RD
12 12

✓
+38 LITE POLE
69

94

✓
✓RD
13 11

✓
+96 PP
39

+50

✓
✓RD
13 11

✓
+12 END WOODS
39-5

93

✓
✓RD
13 11

✓
WOODS
41

92+50

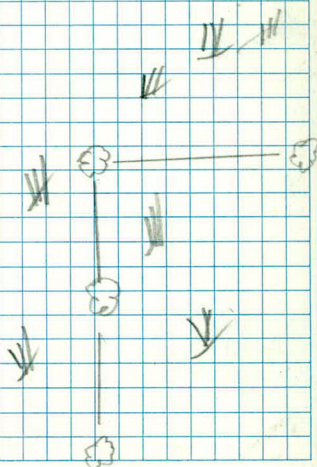
✓
✓RD
13 11

✓
WOODS
40

KP RJ
DS TU
6A

4 MAR 1976

18



+50

RD

+40 ER

38

+36 SW Cor Sta

100

+45 ER

39

+32 PP

39

+27 POR

23

+22 TEL X-SING

+35 POR

+13

BR

13

+24 PP

38

23

+272" P

97

RD

13 12

+09 20" Birch

+88 8" P

+14 BR 45

+86 NE Cor Ho

+74 15" Elm

+60 NW Cor Ho

84

+50

RD

12 12

+46 12" CMP +48 STP

+30 20' BIT ENT.

+13 Bush

+13 5" P

+02 FE

65-79

+13 12" CMP

+13 LITE

96

RD

12 12

+06 3" P

NE Cor Ho

+93 10" Apple

+96 3" P

+74 PP

+87 36" COTT

+65 MH

+64 NW Cor Ho

+55 18" Elm

+62 22" Elm

+50

RD

12 12

+34 5" Apple

+27 18" CMP

+18 13' Gravel

+07 18" CMP

RD

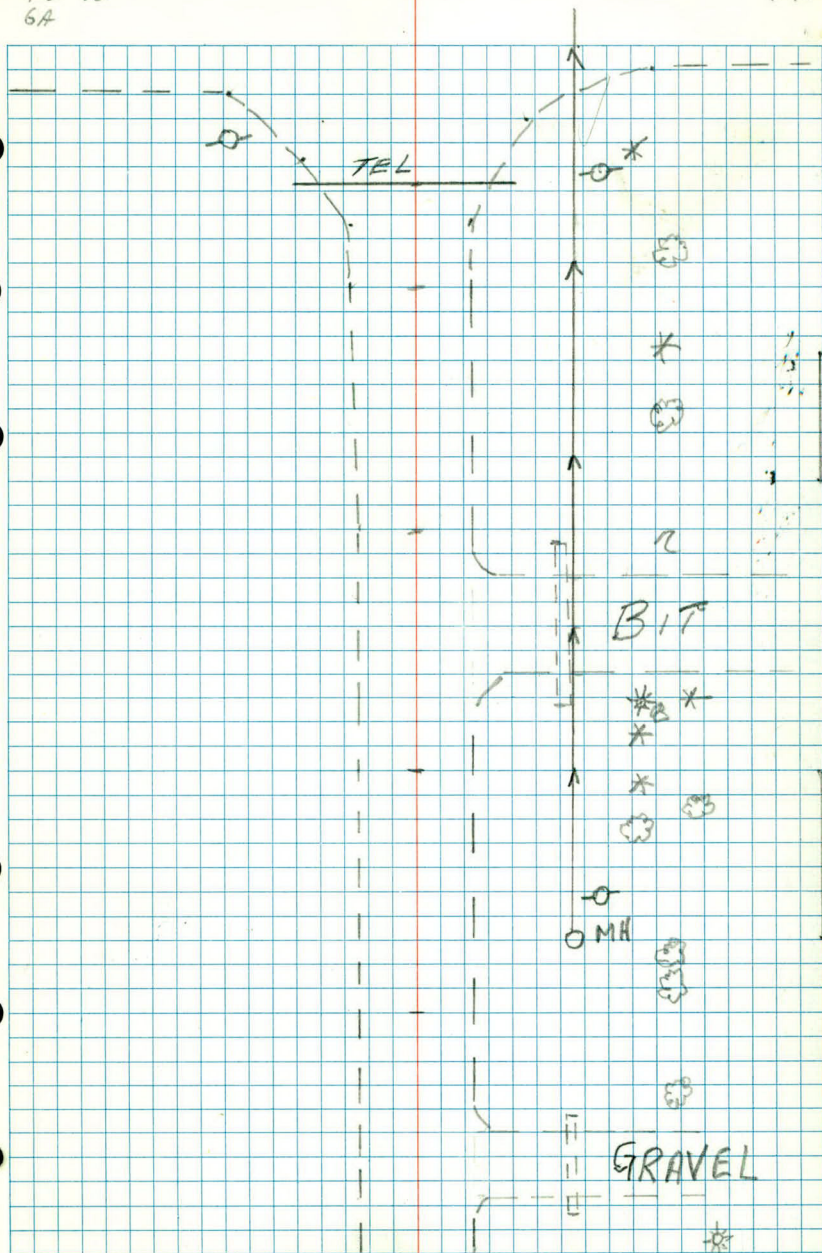
12 12

+04 LITE POLE

95

61

19.



100 ✓

+85 18" CMPT 196 ER

+82 POR 23 34

18 ✓ +76 PP

+66 BR 39

+50 H

RD 15

+97 End hedge

47

+89 STP

+66 Bay hedge

+66 (7) 34 pop

41

RD

+48 10" POP

46

+30 SE Cor

+20 2" M 100

59

+31 End hedge

+30 PP 48

+09 12" EL

47

99 ✓

+71 2" M +71 BUSH

RD 11 14

+99 1" M

38 hedge

+95 NE Combo

96

+63 SW Cor BLDG

+72 NW Cor Ho

+66 STP

+67 3" M

+52 BR

+50 26

+61 ER

12

46

49

RD

+33 ER

30

+48 2" M

47

+17 BR

+07 SE Cor STA

+28 9" EL +14 ER

+06 Cor Parking

LOT

+04 TEL X-SING

+12 10" EL

98 BLDG

100

RD +98 hedge PAR

+99 TEL BOX

+96 TP

+89 POR

25

+75 E 70' BIT ENT

+17 BR

+61 MH

+63 E CLOVER

97+50

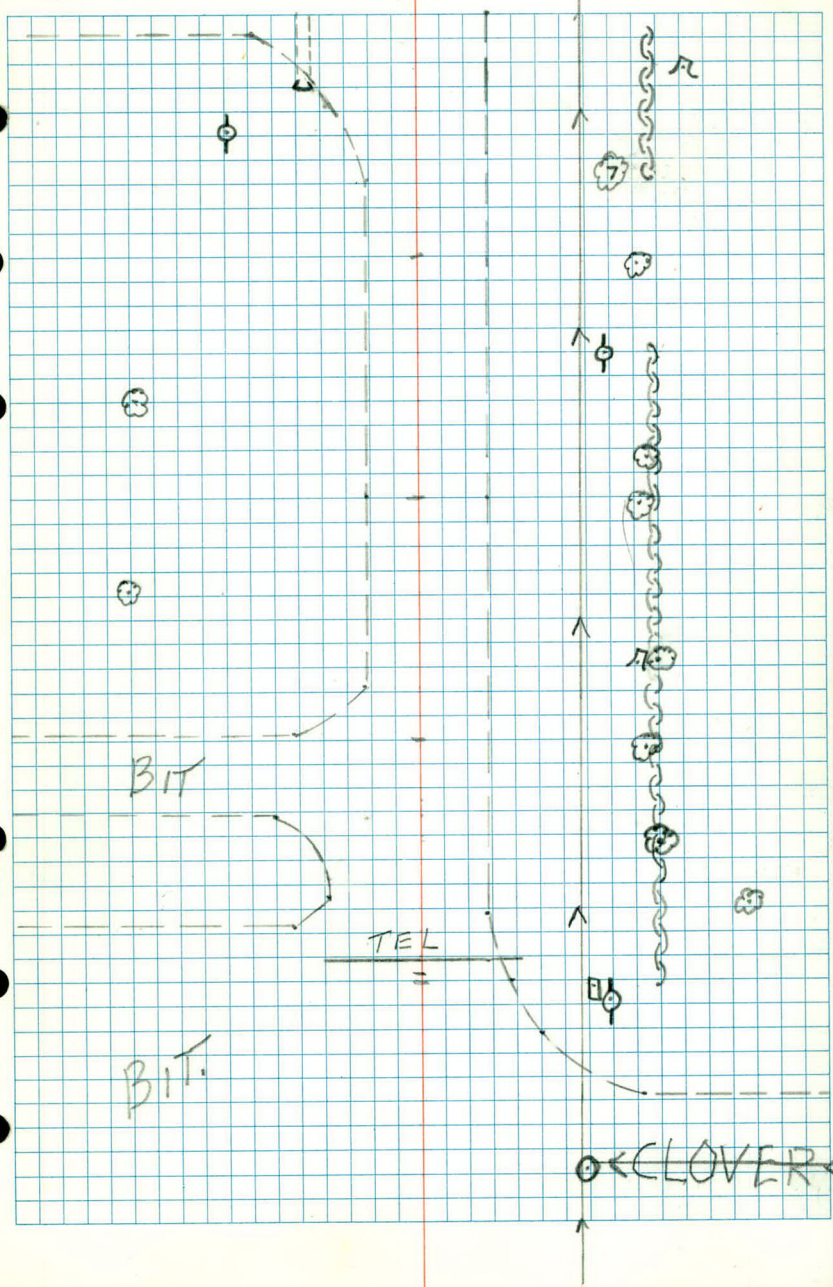
RD

34

KP RJ
DS TU
GA

4 MAR 1976

20.



+50

♀
RD
13 13

+34 PP
39

102

RD
14 14

+63 18" CMP
23

+67 LITE BLE
53

+50

RD
12 14

+44 E 24' GRAVEL ENT

+23 18" CMP
23

101

+99 SE Cor Bldg.
76

RD
10 14

+82 SIGN
47

+65 SW Cor Bldg.
77

+64 PP
40

+61 RR SPIKE
E

+50

RD
11 14

+45 ER

+36 PP
38

+33 18" CMP
23

+29 POR
18

+20 BR
31

+19 MH
33

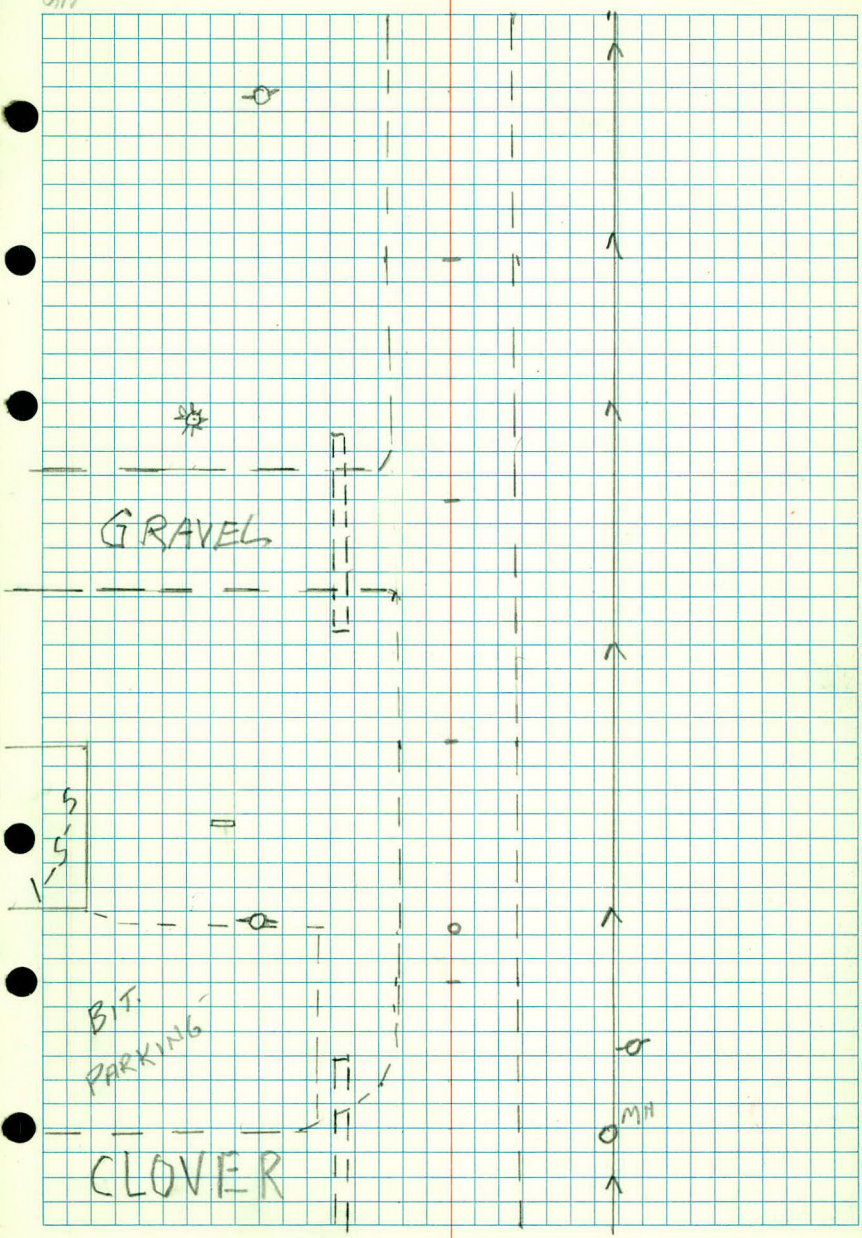
100

RD
15

KP RV
DS TW
GA

8 MAR 1976
CLOUDY 170

21.



105

RD

11 13

+50

RD

11 13

+20 End Brush
38-5

104

RD

11 14

+93 Begin Brush

37-12

+93 PP

39

+50

RD

11 14

+09 Beg Brush
43-5

103

RD

11 13

+77 MH
22

+56 MH
33

102+50

RD

13 13

KP RJ
DS TJ
6A

8 MAR 1976

22

BRUSH

SCATTERED
BRUSH

MH
MH

+50

RD

13/13

+39 5" ELM
67

+19 15" COTT +27 12" COTT

+09 PP +15 TEL Box

39 37

+06 15" CMP

29

+07 PP

67

107

RD

+03 6" P

13/13

53

+96 £12' BIT ENT

+88 15" CMP

30

+86 15" CMP +75 SE Cor Ho

+88 LILACS

+79 £10' ENT

+60 22" ELM

+67 LILACS

+56 SW Cor Ho

+59 NE Cor ho

+69 15" CMP

+50

80

RD

+56 (4) 6" Birch

13/13

46

+40 14" ELM

42

+34 NW Cor ho

83

+087" Locust

68

+20 STP

42

+087" Locust

50

106

RD

13/12

+99 15" ELM

+90 MH

+94 15" CMP

+89 END BRUSH

25

31

+55 4" ELM

+83 £12' GRAVEL ENT

42

+55 5" ELM

+75 15" CMP

+50

41

RD

31

12/12

+43 PP

38

+47 Bush

54

+47 Bush

61

+32 Bushes

56-67

105

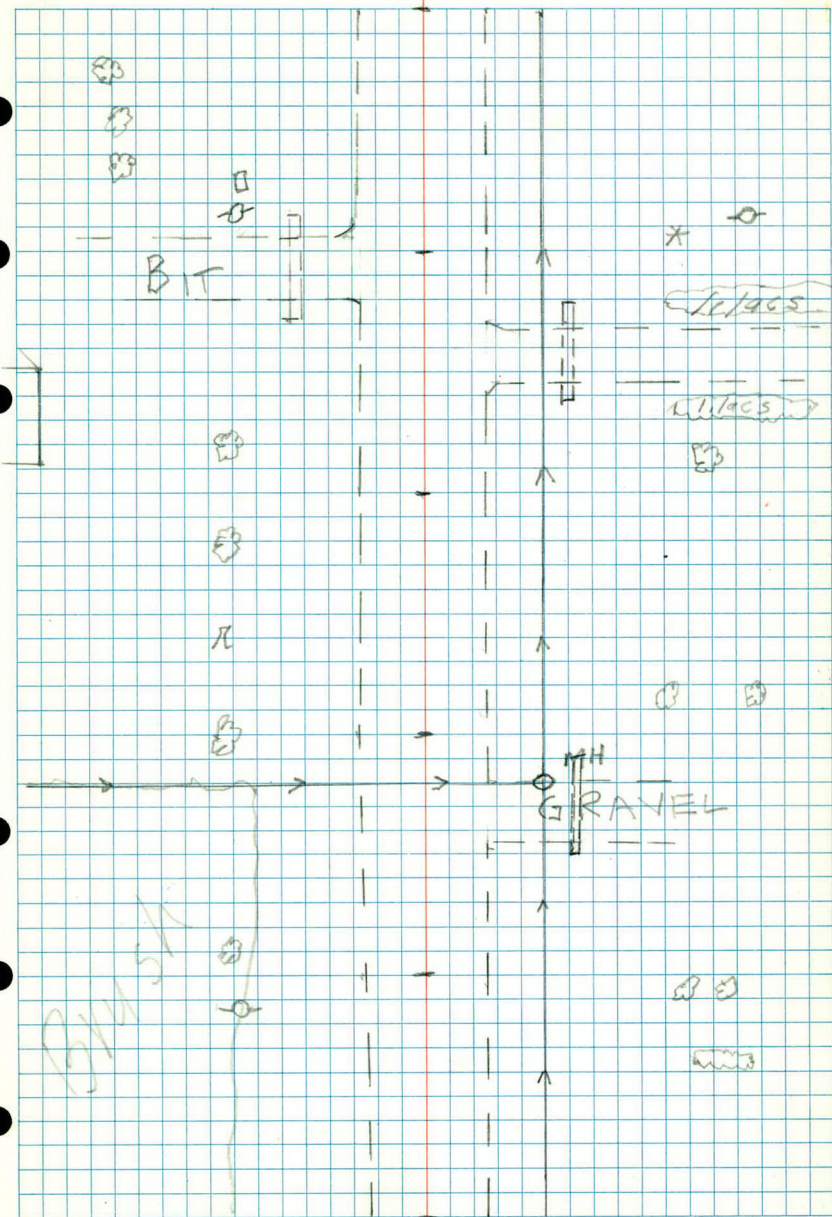
RD

11/13

KP RJ
DS TJ
GA

8 MAR 1976

23



110

SWAMP
27-NRD
12 13+90 MH
25+73 MH
46

+50

SWAMP
27-NRD
12 13+49 END Woods
68-5

+25 END Brush

58-90
+18 Cor SWAMP
27-N

109

RD

+87 PP

+75 Beg Brush

12 13

38

58-78
+75 END Woods
71-90

+50

RD
12 13

108

WOODS

RD

+94

65-N
Begin Woods
65-N

12 13

+69 Beg Brush
49-59+52 7" Cott
43

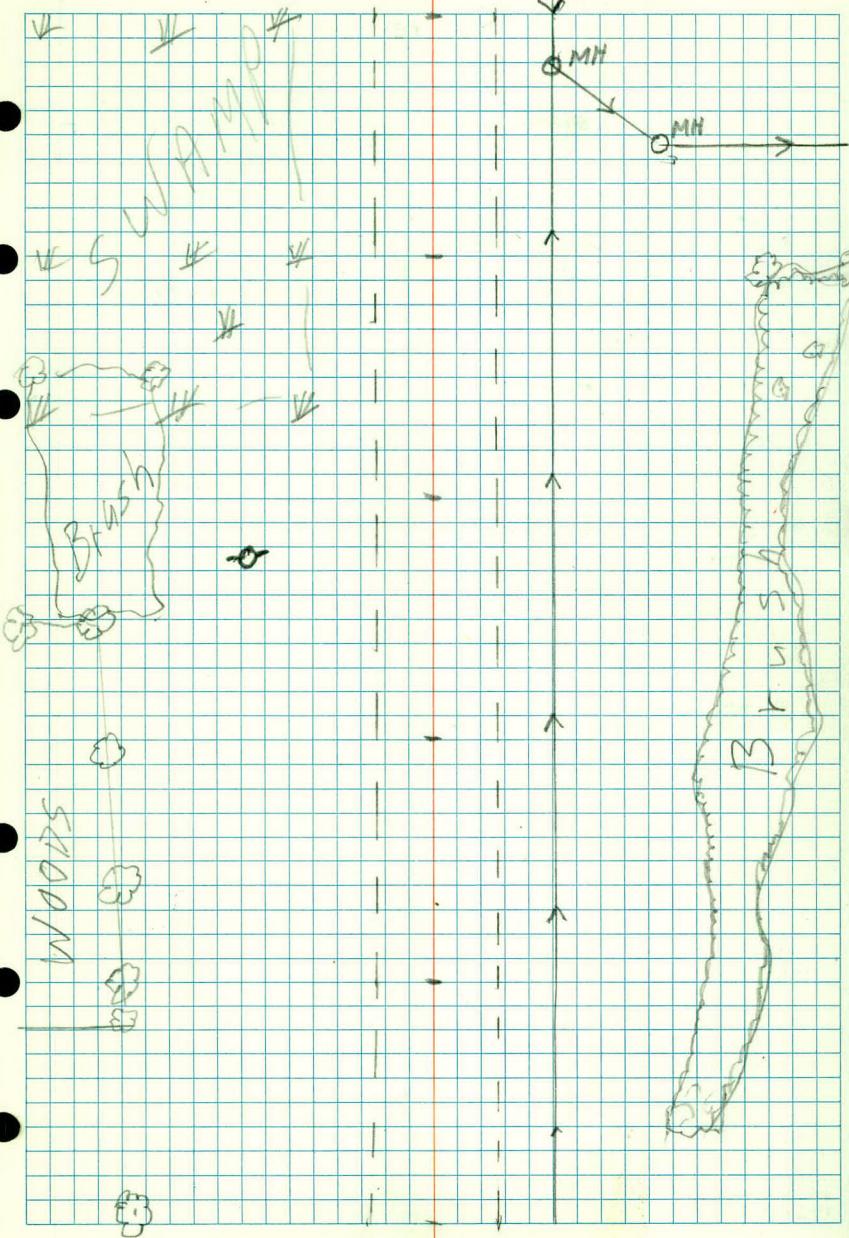
107+50

RD
13 13

KP RV
DS TV
GP

E 8 MAR 1976

24



+50

Swamp
27-N

~~E~~
RD
1213

112^{12"}
~~36~~ CMPAPP Swamp RD
20 39 27-N 1213

Brush ^{12"}
~~36~~ CMPA
74-5 20

+85 Beg Brush
74-5

+50

RD
1213

111

RD
1213

+76 STP

+61 6"Will 53

⁴⁹
+58 7"ELM
54

+50

RD
1213

+48 End brush

+48PP
39

+33 12"Will +36 ⁸⁶⁻⁵ 12"Will

⁵⁹
+24 20"Will +26 ⁵⁹ 6"Will

⁵⁵
+24 8"Will +25 ⁵⁸ 6"Will
⁵⁶

110

SWAMP
27-N

RD
1213

+17 Beg Brush
86-5

KP RJ
DS TJ
GA

8 MAR 1976

25

£

Brush

WA
MP

5

2

2

2

2

115

RD
12 14+82 Tw 6" P
56

+50

+29 15" CMP

RD

+29 Bush +49 10" P 13 13

+49 #9' Gravel cnt

+19 12' 44 56
Gravel cnt+08 30' COTT
13

+28 10" P

+06 End Bush +03 Bush

+16 42 40
10" P

114

END Hedge 46 19 15" CMP

RD

+00 6" Birch +99 Tw 6" Birch

+88 Bay Brush +83 18" P 13 13

+94 Tw 6" Birch +91 MH

+66 Tw 6" Elm 43 56
+60 Cor SWAMP

+84 12" P +86 PP +89 14" P

+61 Begin hedge 27-N

+64 12' Dirt cnt

+60 Iron 44 50
+60 PP+53 12" Elm
40

+50

RD
13 13+51 TEL Box
30

+49 8" Will

+38 12' CMPA
26

+37 12" CMPA 28

+10 (10) 5" Elm +21 End Bush

113

SWAMP
27-NRD
13 13Brush
67-5+91 20' Will
52

+85 STP

+78 12' COTT

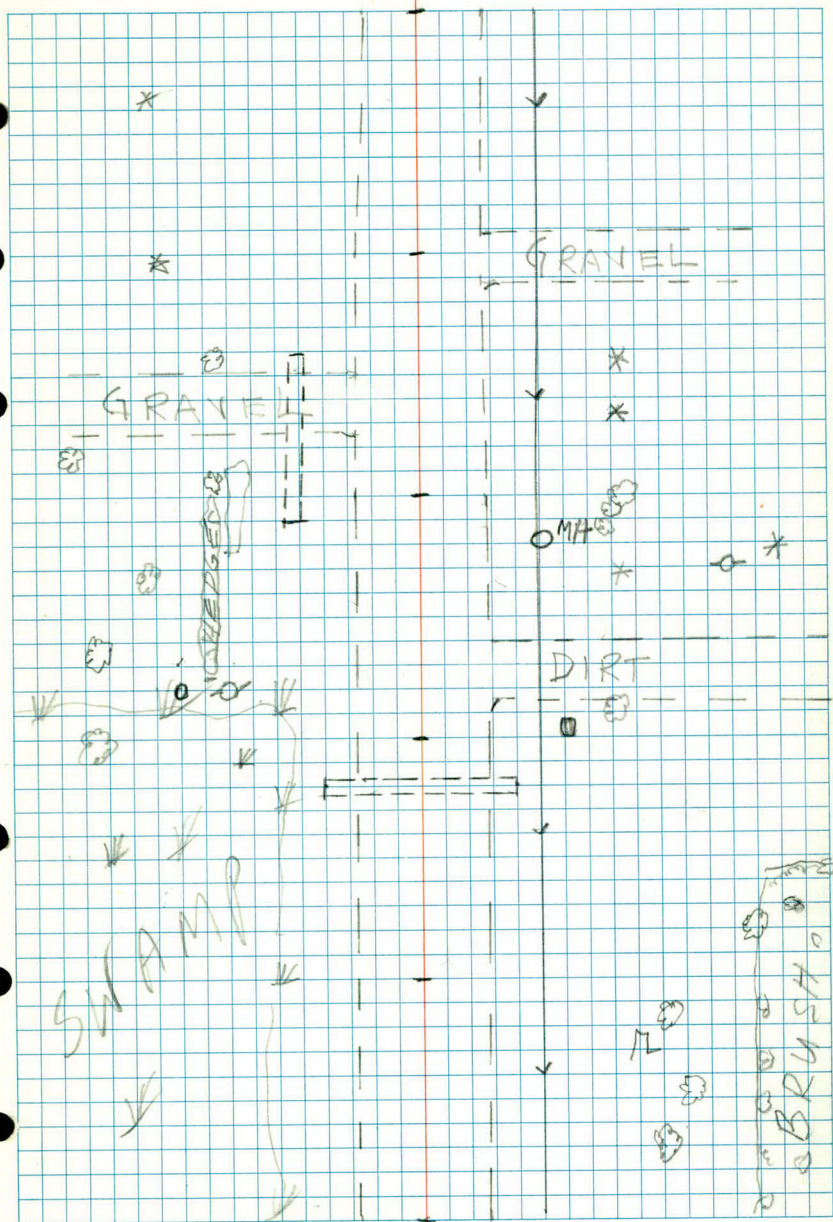
112 +50

RD
12 13+69 7w 6" Elm
50

KP RV
DS TJ
GA

8 MAR 1976

26.



+50

RD
13 14

+31 18" ELM

+30 STONE⁴² planter

+08 FE⁵⁶ +16 18" ELM⁶⁴
42-5

117

Brush

+78 Box²⁹⁻⁵⁰ Brush 13 15

+69 PP³⁸ 29-42

+66 (3) 16" Basswoods⁷⁴

+58 12" COTT

+50

RD
13 15

+48 18" COTT

+41 14" COTT⁵² +38 4" COTT⁵⁰

+28 10" ELM⁷⁴

+35 6" COTT⁵⁴ +41 14" COTT⁵⁰
46

116

+06 32" COTT RD
65 13 15

+02 6" ELM⁶⁶

+11 6" ELM⁶⁹

+77 20" COTT⁶⁶

+71 22" COTT⁶⁵

+81 TW 8" COTT⁷⁴

+61 15" CMP²⁵

+51 E 9' DIVERT²⁵

+67 20" COTT⁶⁶

+68 12" COTT⁶⁹

+50

RD
13 14

+53 5" Ash⁵⁰

+63 7" ELM⁵³

+41 15" CMP²⁵

+49 12" COTT⁶⁷

+48 5" COTT⁶⁷

+48 15" COTT⁵⁴

+32 6" COTT +37 (6) 6" COTT

+28 PP³⁹ +28 Bush⁴⁰

+27 7" ELM⁵²

115: 39 +29 TEL⁵⁵ Box RD
36 12 14

+10 8" Ash⁶⁴

KP RJ
DS TV
LA

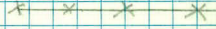
8 MAR 1976

27

Bush

DIRT

DB



120

RD

11 13

+86 NE Cor Ho
69+76 1" M
56+56 NW Cor Ho
69

+50

RD
12 13+45 Bush
68+30 Bush
44+26 5" P
68+26 PP +28 Fe
54 46-5
+13 14' Gravel ent

119

RD

12 12

+98 1" P +98 NE Cor Ho
49 68+60 TEL Box
43

+55 PP

+50

38

+60 1" P +72 1" P
62 50
+58 NW Cor Ho
68RD
13 13+34 15" CMP
22+27 FE
44-5+15(8) 14" ELM +24 TEL Box
60 40

+22 12' DIRT ENT

+08 (5) 12" ELM
79

118

+14 15" CMP
22RD
13 14+90 MH
25+63 End Brush
32-50

+52 10' DIRT ENT

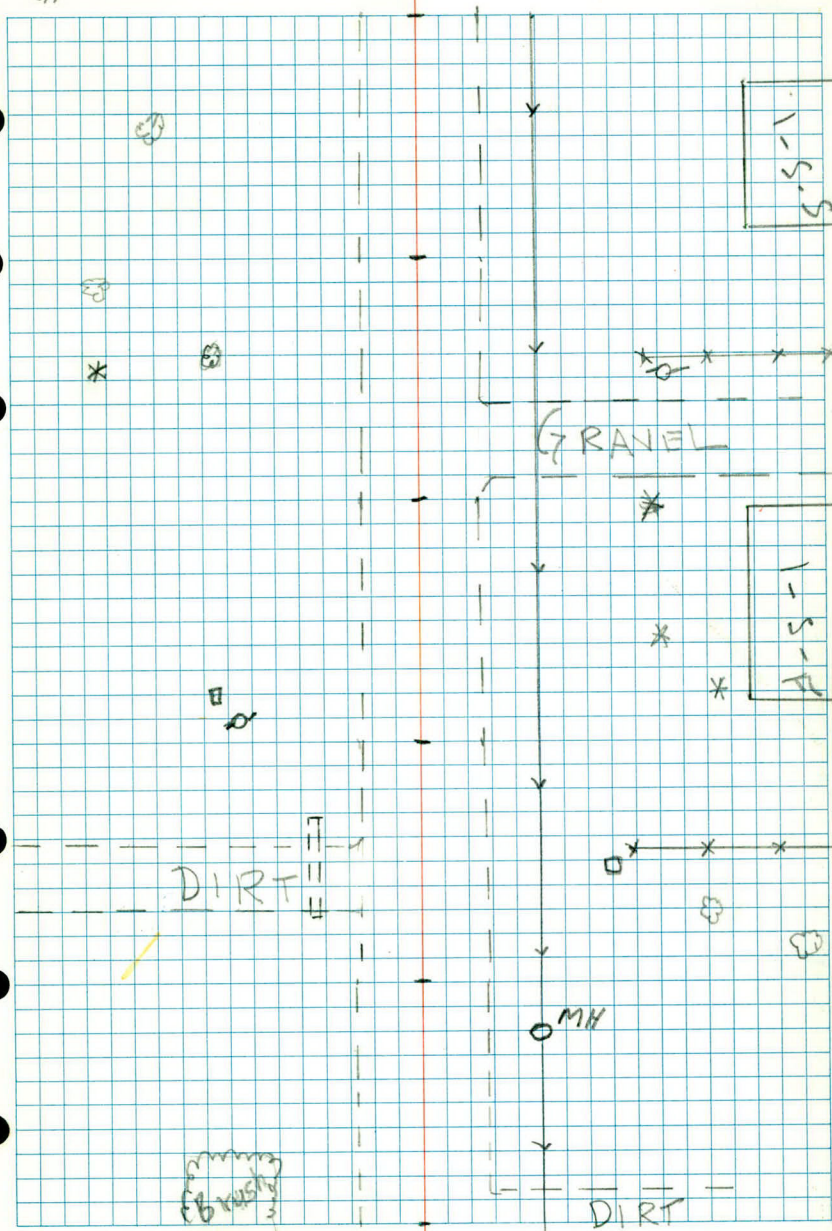
117+50

RD
13 14

RP RJ
DS TJ
6A

8 MAR 1976

28



+50

hedge

48

11 13

+34 NE Cor Ho

+33 Bush

71

55

+21 TW 6" P

55

122 +94 Bush Hedge

RD

+11 8" P

Ho

48

48

11 13

+93 NW Cor Ho

70

+83 TEL Box

+85 PP

+78 15" CMP

+74 Bush Fe

+67 1/2 14' DIRT ENT

+91 7" P

+93 MH

+60 END FE

+86 FE Cor

+62 8" P

+59 30" COTT

25

43

+58 15" CMP

43-N

+55 PP

+51 TW 7" ELM

59

+50

25

RD

+51 TW 5" ELM

47

11 13

+47 NE Cor GA

+41 1/2 10' GRAVEL ENT

+41 6" APPLE

+21 6" APPLE

+31 NW Cor GA

+32 2" P

121 FE

RD

+07 2" M

+12 NE Cor Ho

+96 5" APPLE

11 13

+71 10" M

73

+74 4" APPLE

+54 2" APPLE

+58 9" P

+64 NW Cor Ho

+50

50

RD

+36 6" APPLE

+24 PP

+21 Bushes

+23 15" CMP

+24 FE Cor

+30 Bush

+31 TEL Box

+12 1/2 10' BIT ENT

+02 Bushes

+03 15" CMP

RD

+08 1/2 10' DIRT ENT

120 55-N

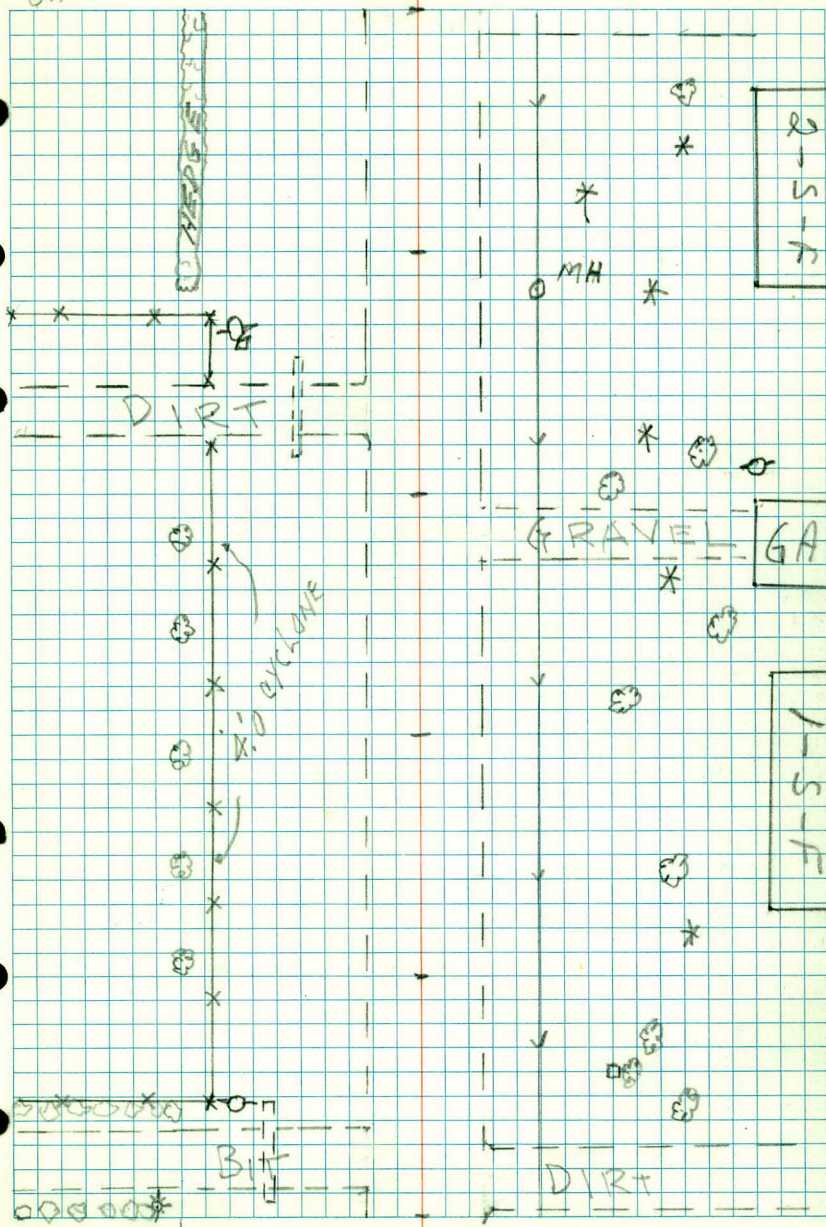
21

+02 LITE

11 13

55

29



125

+94 15" CMP

£

+93 20" ELM +93 3" M 12 12

51

+75 10" OAK

47

+79 Bush

49

+81 Bush

36

+63 ARBOV

+54 3" P +63 2" M

+69 £ 20' BIT ENT

+50 +43 Bush +44 3" P RD

+43 TELBOX +32 8" ELM +39 PP +40 Tel. cable

+22 1" P +23 10" APPLE

+12 1" P

+18 1" P

+42 TELBOX

+39 PP

+08 1" M

+04 1" P

+27 4" P

+25 10" ELM

124

RD +01 36" COTT

+88 1" P +98 3" P

+17 Bush +17 Bush

+75 PP +76 14" APPLE

+74 NE COR HO

+77 Bush

+53 10" BUSH +69 15" CMP

+74 Cor Conc Slab +77 2" P

+53 Bush +53 End Hedge

+54 Cor Conc Slab

+50 +53 15" CMP

+64 £ 20' BIT ENT

RD 11 13

+26 10" M

+47 10" M

+12 HEDGE

+18 10" M

+16 15" CMP + 10' Gravel ENT

+12 NW Cor Ho

123

RD 11 13

+96 15" CMP +98 Cor Hedge

+89 2" P +86 2" P

+89 4" P 48-66

+85 8" ELM

+89 4" P +86 4" P

+82 TEL Box +86 2" P

+65 4" P

53

40

58

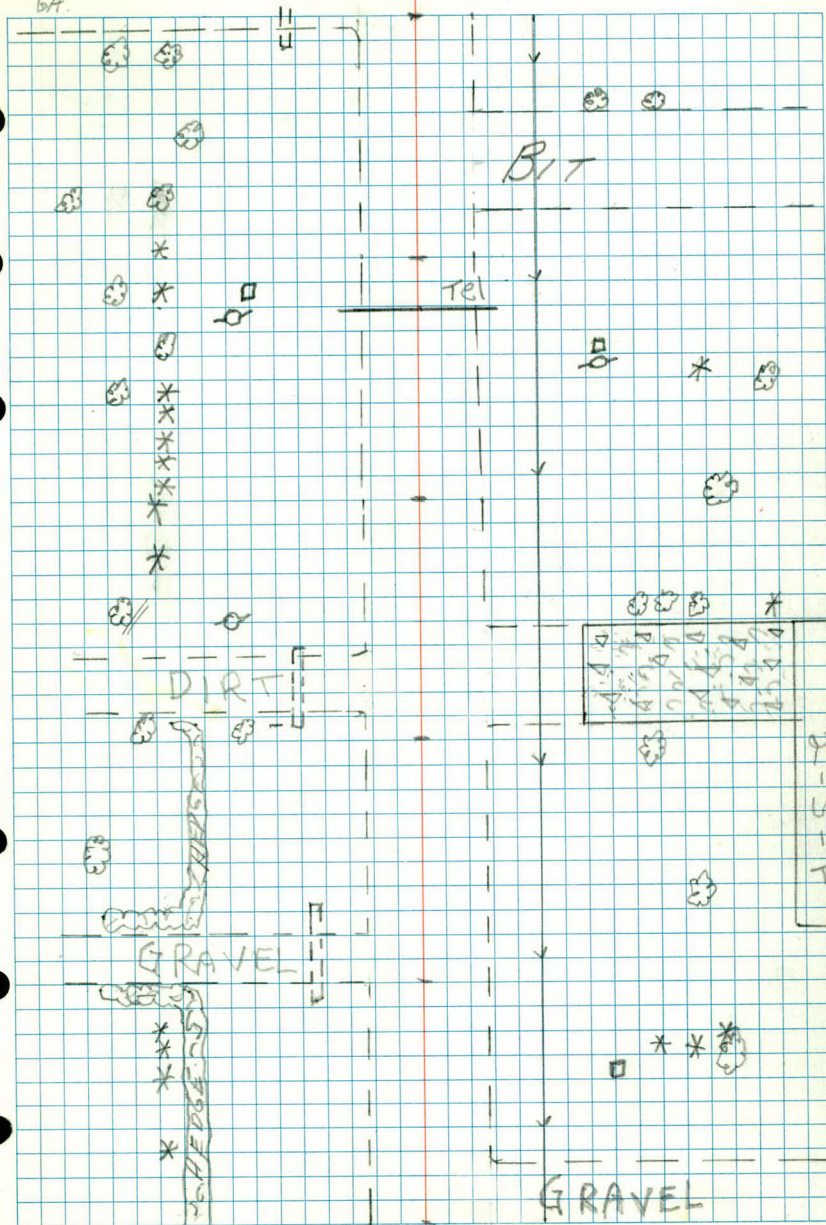
22+50

RD 11 13

+54 £ 18' GRAVEL ENT

KP
DS
6A.

9 MARCH 1976 30,



+50

+47 TW 3" Ash

+39 (4) 3" Ash

+26 36" CMP

+22 PP

127

RD
12 12

+49 Bush

+37 6" APPLE

+20 LITE

+15 E 12' GRAVEL ENT

RD
12 12

+90 PP

+86 14" CAT

+69 PP

+54 MH

RD
12 12

+50

+31 10" ELM

+49 SD

+32 30" OAR

+48 40" COTT

+24 2" P

126

RD
12 12

+92 MH

+89 4" ELM +79 10" APPLE

+56 4" ELM

+79 6" APPLE

+60 10" APPLE

+50

RD
12 12

+43 Bush

+40 N.E. COR HO

+15 12" APPLE

+31 24" M

+14 15" CMP

125

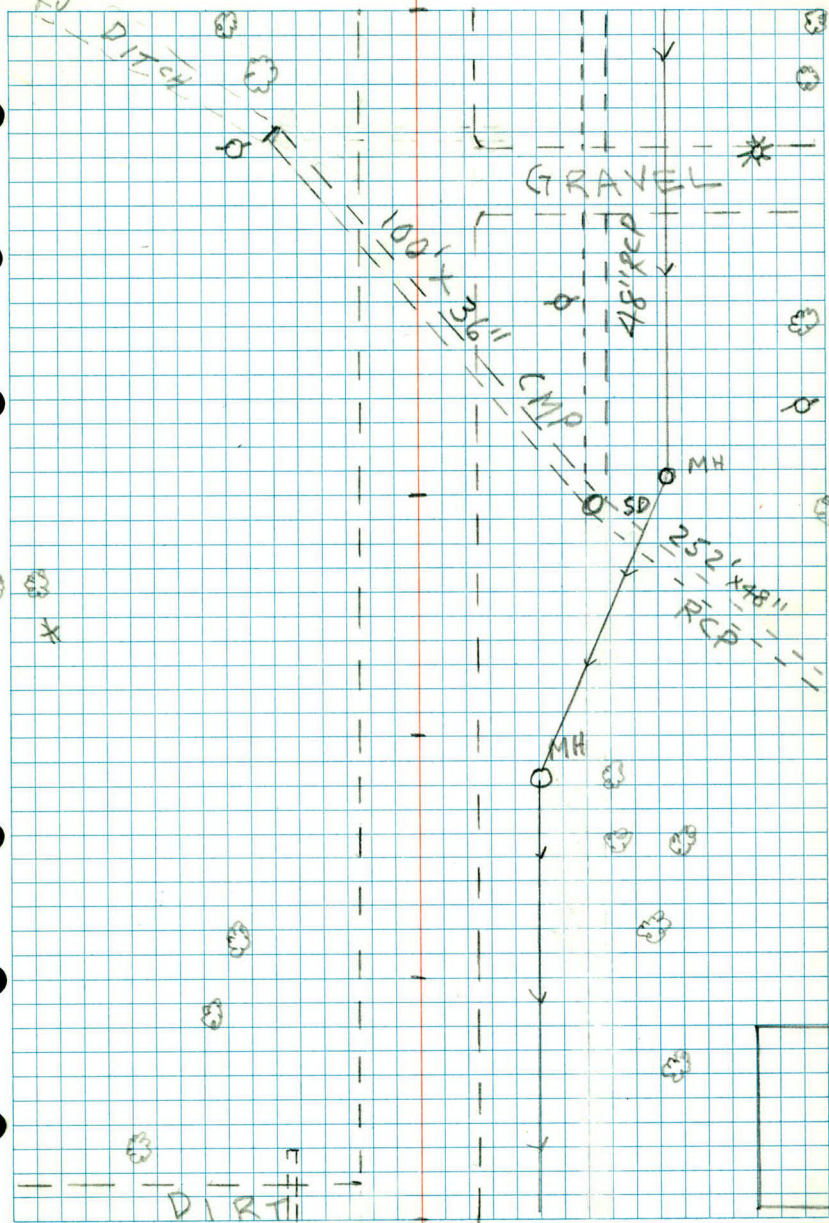
+03 E 10' DIRT ENT

RD
12 12

+02 NW COR HO

KP
DS
RJ

10 MARCH 1976 31



130

£
RD
13 12

+50

RD
13 12

+32 £ 10' DIRT ENT
36

+05 RT ENT.

+10 PP +23 PP
30 85

129

RD
12 13

+88 5" Ash
78

+91 PP
36

+60 15" CMP

+83 4" ELM +85 5" Ash
39

+75 4" Ash +77 4" Ash
62 75
74 66

+50

RD
12 13

+48 £ 12' DIRT ENT

+31 3" Ash

+28 4" Ash +29 4" Ash
56 60

+32 TEL Box +34 8" P 39
35 84

+17 4" Ash +21 4" Ash
60 54

+30 SD +30 Bush
37 71

+13 5" Ash
56

+27 10" ELM +27 12" ELM
82 76

128

RD
13 13

+04 1" P
71

+87 48" COTT

+82 TW 6" ELM

+74 Bush
84

+69 £ 10' DITCH +69 (5) 4" Ash
53 67

+66 (4) 4" Ash
72 31

+59 Bush
83

127+50

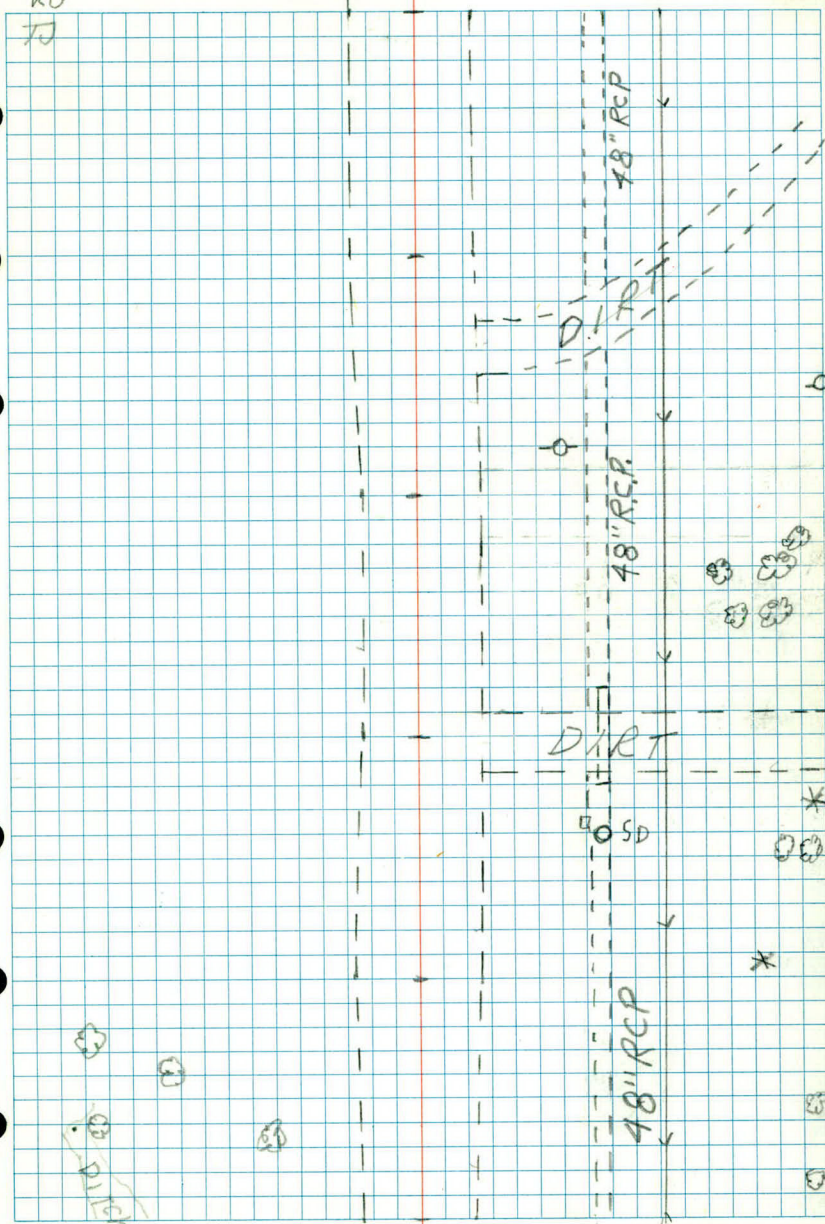
RD
12 12

KP
DS
RJ

11-MAR 1976
P.CLOUDY 25°

32,

TJ



+50

~~2~~
JRD
13 12

✓
+39 PP
37

132

JRD
13 12

✓
+56 SD
37

+50

JRD
13 12

131

JRD
13 11

✓
+70 PP
37

+50

JRD
13 12

130

JRD
13 12

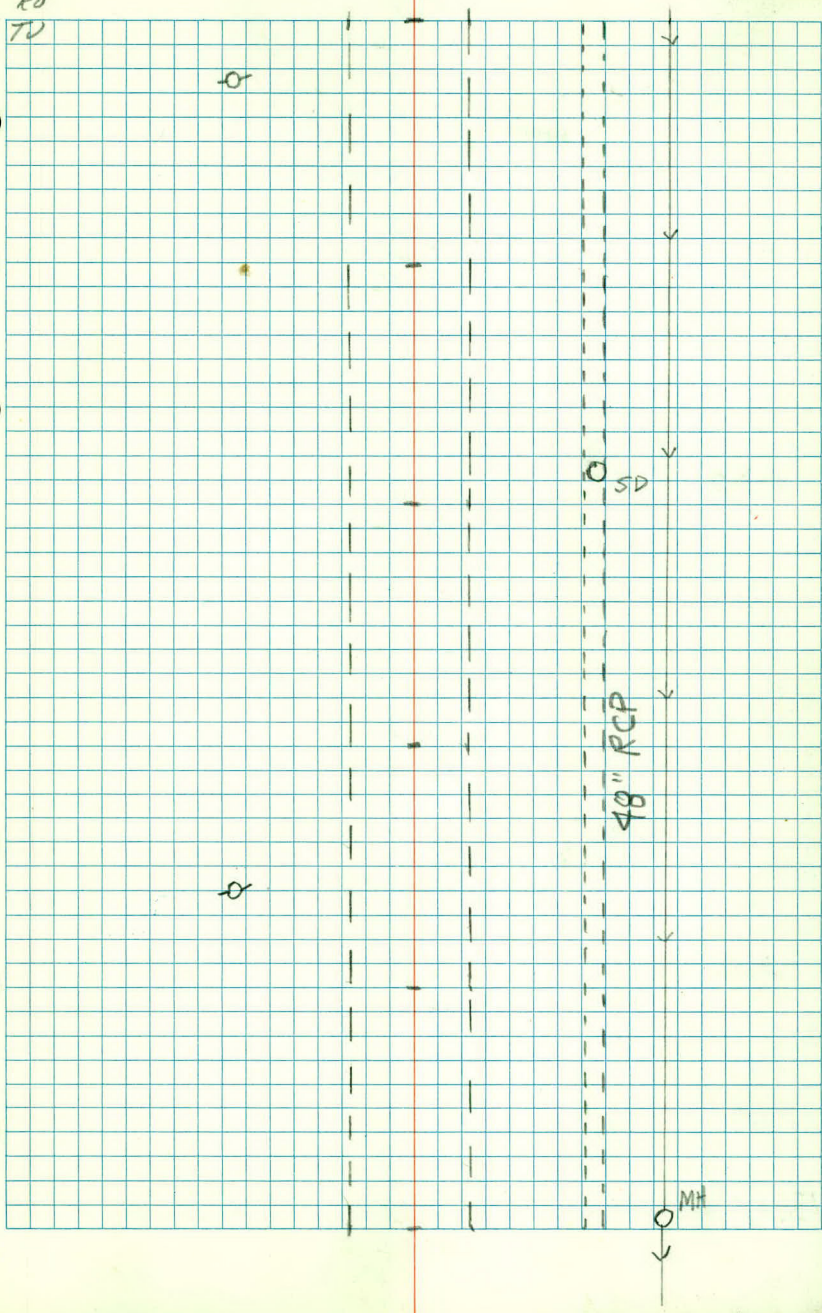
✓
+02 MH
52

KP
DS
RJ
TV

£

11 MAR 1976

33



135

RD
13 12
+93 PP
29

+93 TEL Box
28

+50

RD
13 12

+46 SD
37

+21 PA
38

134

RD
14 12

+50

RD
14 12
+56 MH
55

+48 £ 31' DIRT ENT

133

RD
14 12

132+50

RD
13 12

KP
DS
RU
TV

L

11 MAR 1976

34.

00

0 SP

48" R.C.P.

DIRT

34

+50

RD
13 12

+37 48" RCP
56

137

RD
13 12

+93 PP
39

+50

RD
13 12

136

RD
13 12

+90 24" COTT
84

+80 MH
52

+50

RD
13 12

+32 PP
38

+27 ± 16' Gravel Ent

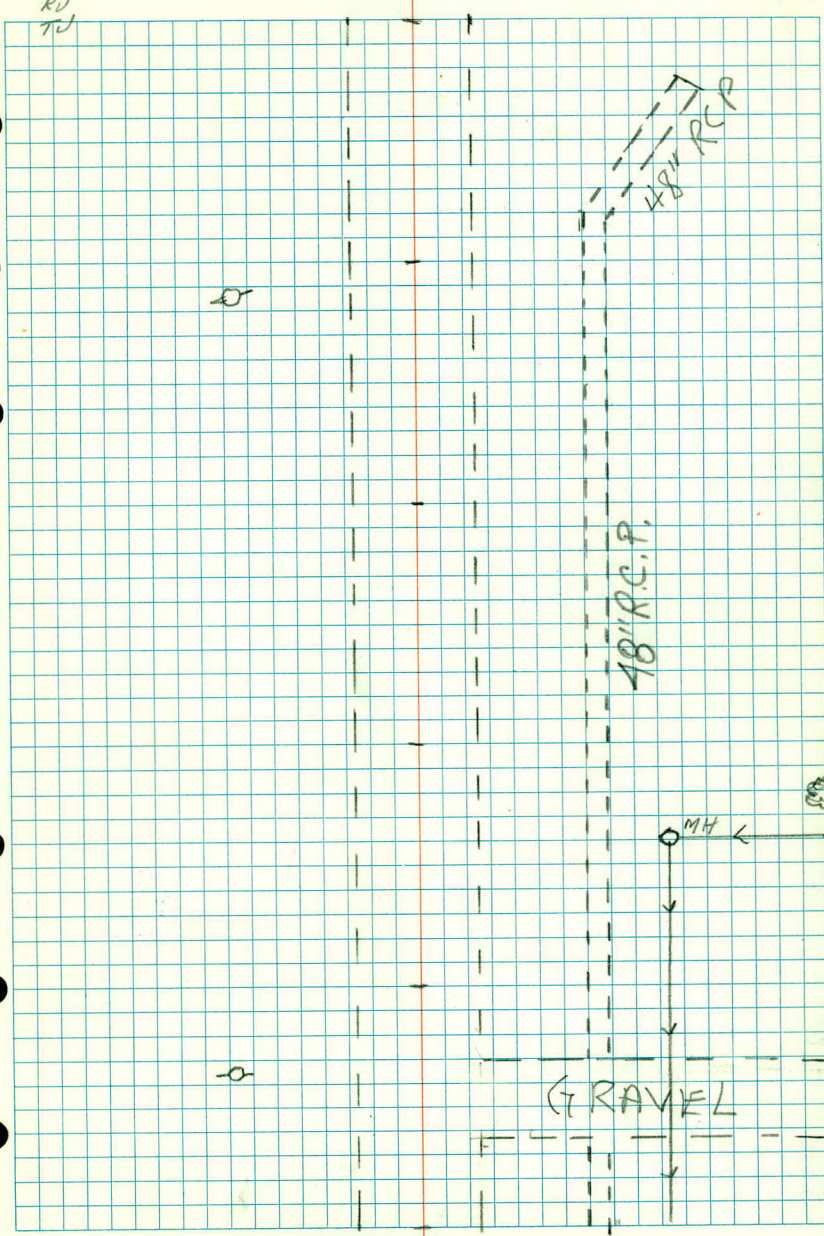
135

RD
13 12

XP
DS
RU
TU

11 MAR 1976

35.



140

LT

RD

RT

RD

68

+68 MH
22

+65 = TEL Conduit

+68 POR

+80 ER

34

+56 PP

+60 POR

38

26

+70 ER

82

+63 POR

+50

RD

+49 PP

29

+37 24" OAK
50

+19 BR

14

+40 BR
20+17 TEL BOX
30

+15 Tel cable

RD
20 14

139

+50

30" OAK
58RD
17 14+43 PP
39

138

RD
14 13

137 +50

RD
13 12

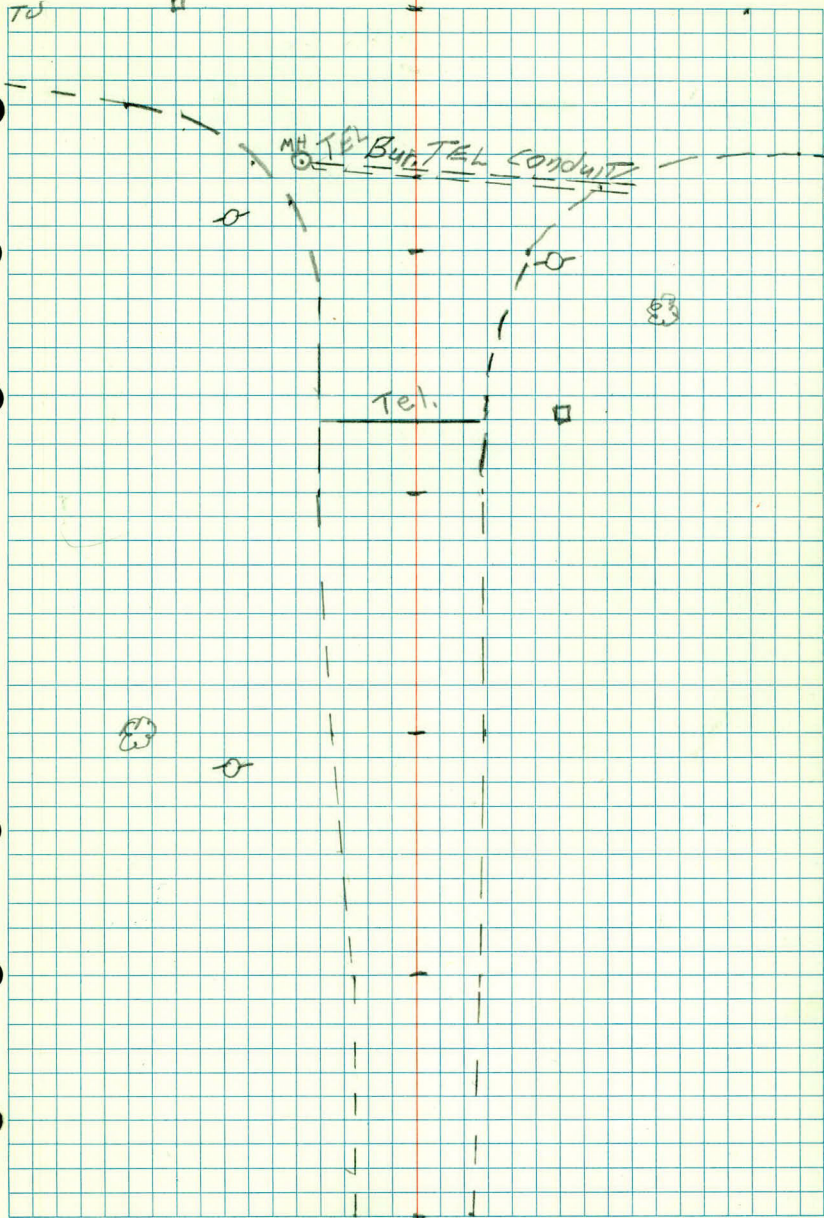
KP
Ds
RJ
TO

LT

E

11 MAR 1976
RT

36.



LT

E

RT

+50

✓
+24 FE

✓
+09 RD
E

✓
+12 RD
56

✓
+15 FE
46

140

+01,49 MONT
50

✓
+00 RD
68

KP
DS
RJ
TV

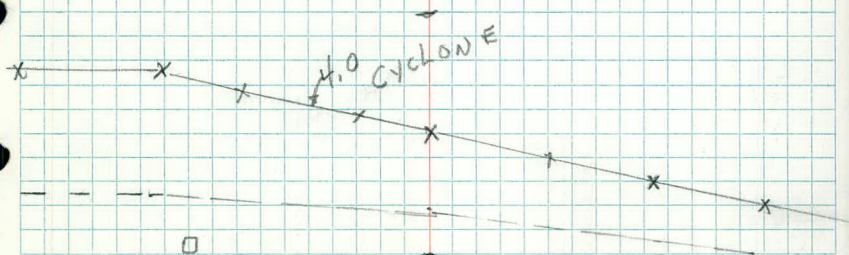
LT

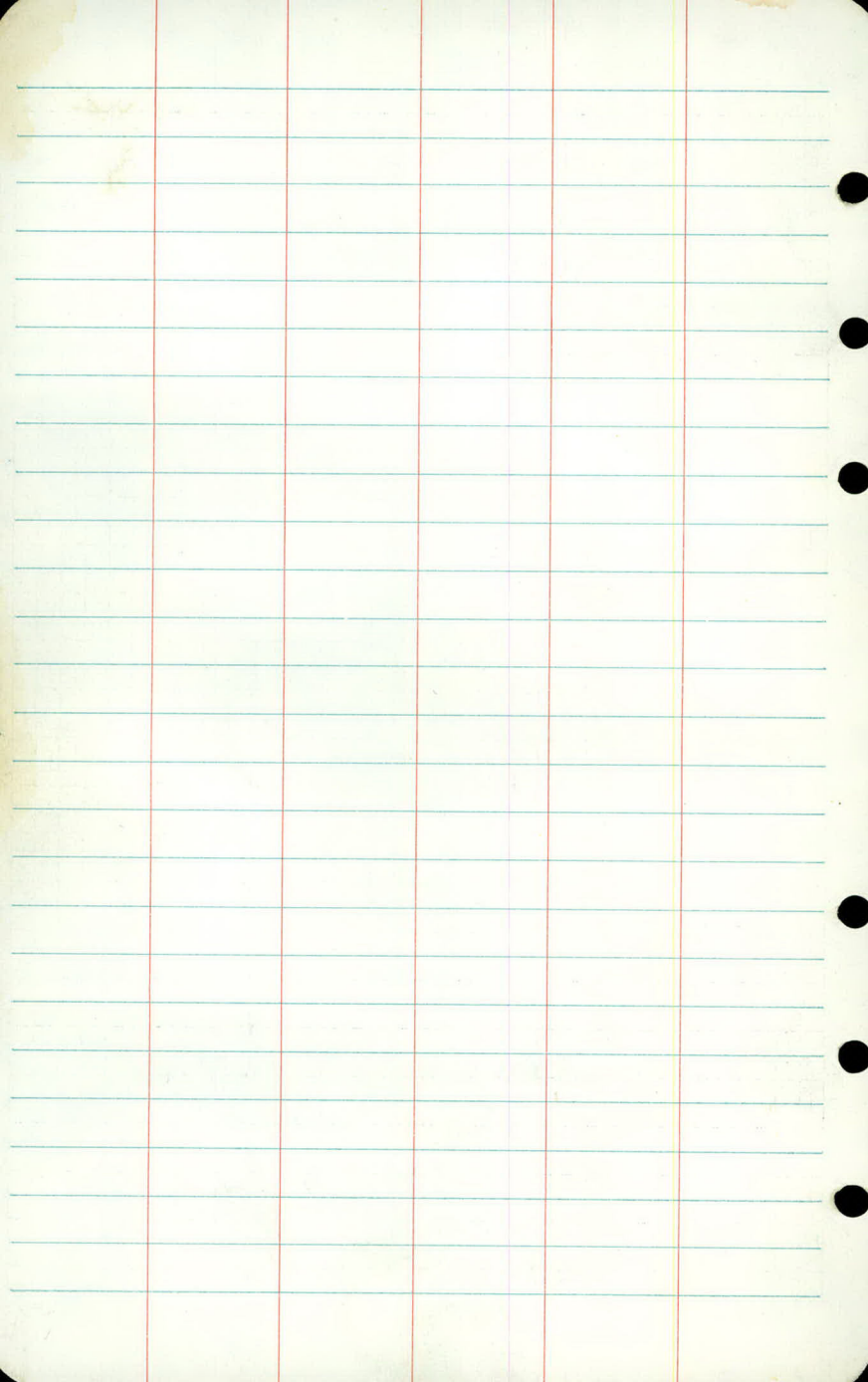
E

11 MAR 1976

37

RT





Add #1

TOPOGRAPHY

CO. RD "F"

McMEUENY

TO

CENTERVILLE RD

ENT'S

STA 91±

STA 138±

LT

C

RT

+50

+39 WOOD POST
32

+39 STEEL POST
34

+33 ENT
34

+10 ENT
27

+22 RANTIL TO E EDGE

+05 STEEL POST
34

+01 RANGE JIL TO W ENT

91

+89 SIGN
85

+96 SIGN
85

+69 PP
38

+50

90+00

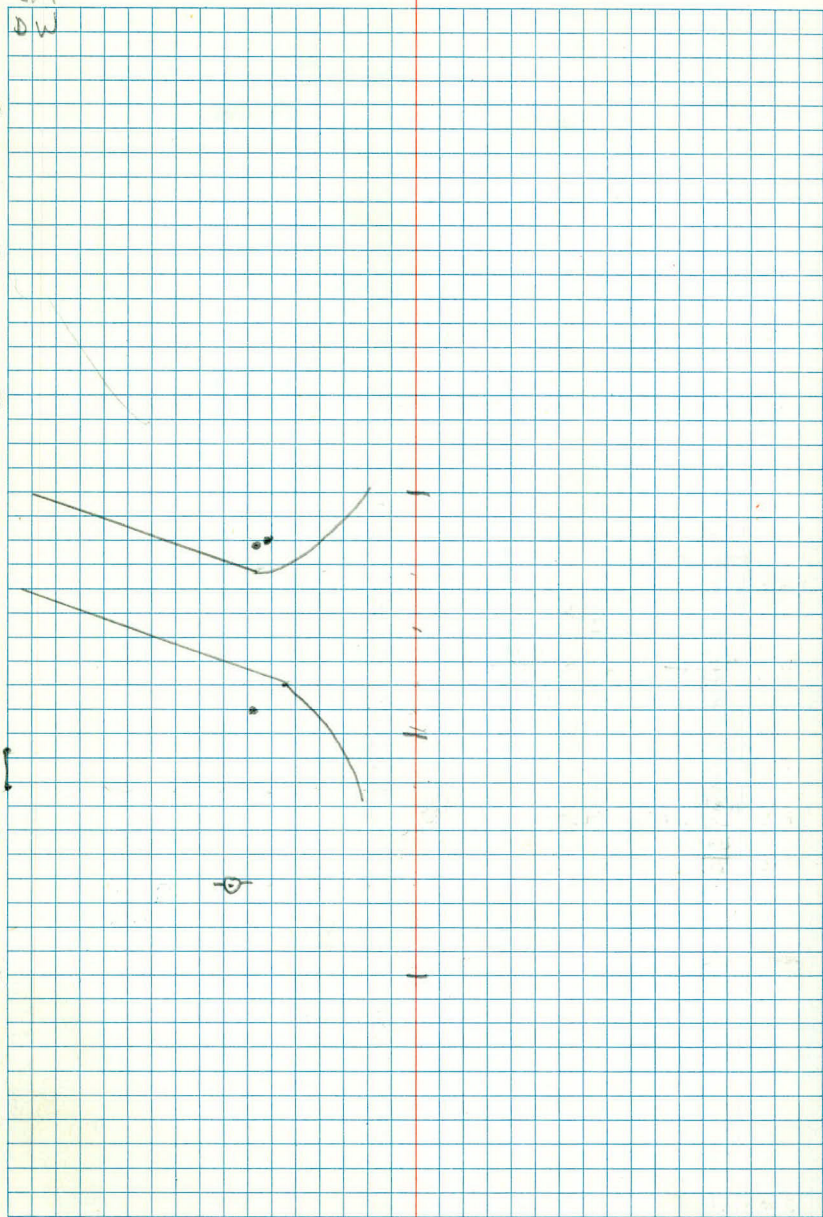
W.S.
B.W.
E.V.
D.W.

LT

Q

8-13-76
RT CL 80.6

2



LT

C

RT

139

+50

+71 $\frac{EWT}{25}$ +54 $\frac{EWT}{40}$ +60 $\frac{EWT}{36}$ +50 $\frac{33" OAK}{69}$ +40 $\frac{EWT}{49-68}$ +47 $\frac{EWT}{26-39-59}$ +30 $\frac{EWT}{59-75}$ +43 $\frac{P.P.}{38}$ +20 $\frac{EWT}{64-78}$ +10 $\frac{EWT}{78-84}$ +05 $\frac{137+78}{RAN TILE EWT}$

138+00

 $\frac{EWT}{77-94}$ +76 $\frac{EWT}{111}$

137+50

W.S
BW
BY
RW

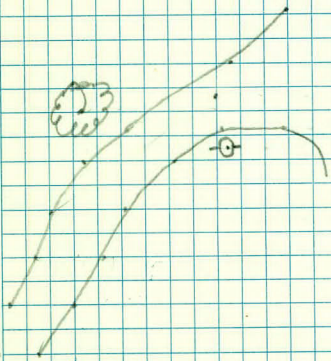
LT

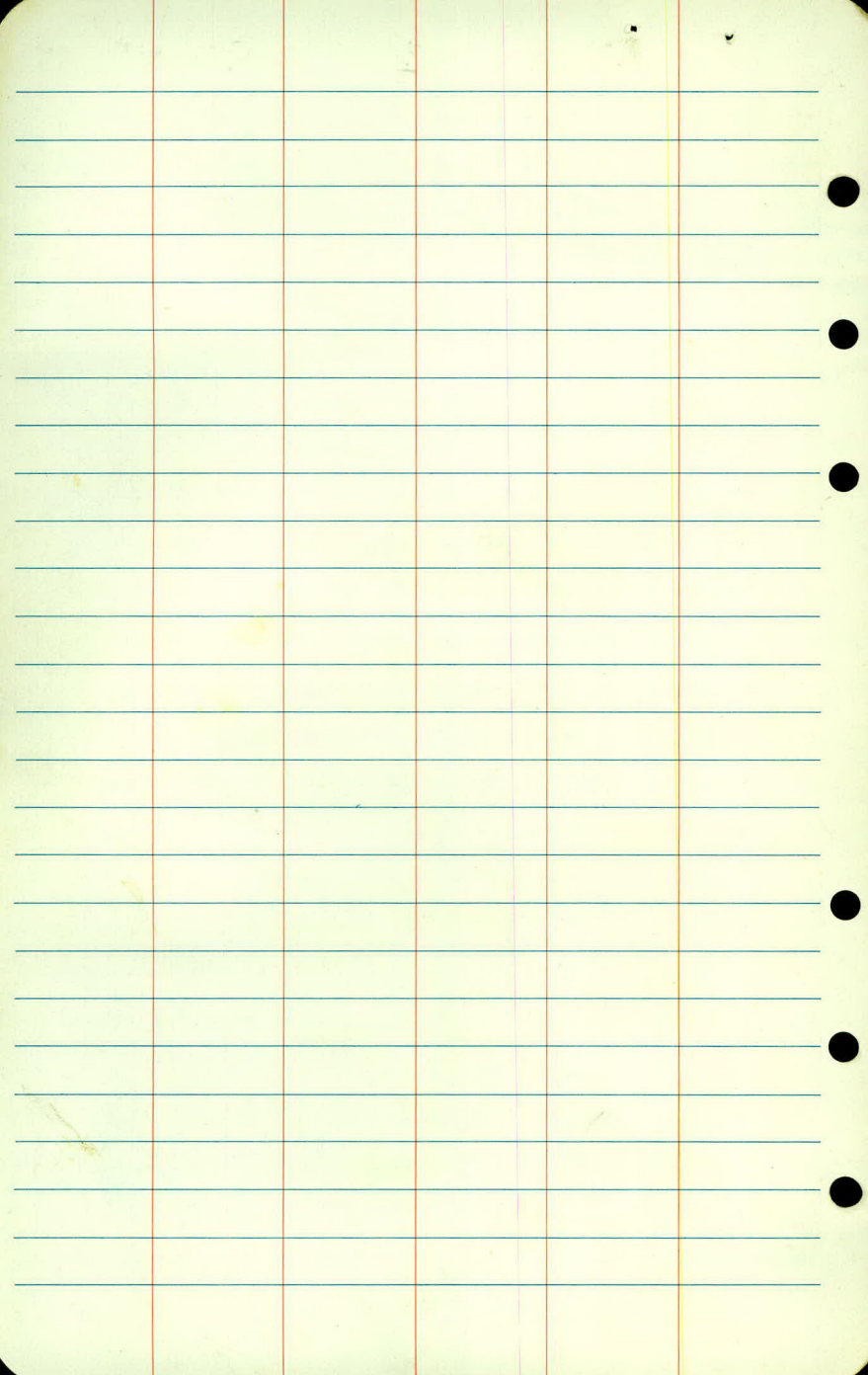
Q

RT

8-13-76
CL: 81°

3





KP
GA
RJ
TJ

27 FEB 1976
SUNNY 40°

1.

Co. Rd F

McMENEMY TO CENTERVILLE RD

TELEPHONE CABLE
LOCATIONS

+50

£

67

TEL
10

+50

TEL
7

66

TEL
2

+89 TEL
£

+50

TEL
8

65

TEL
13

LT

£

27 FEB 1976

RT

2.



LT

£

Rt

2

$$139 + 15 \quad LT \text{ \& } RT$$

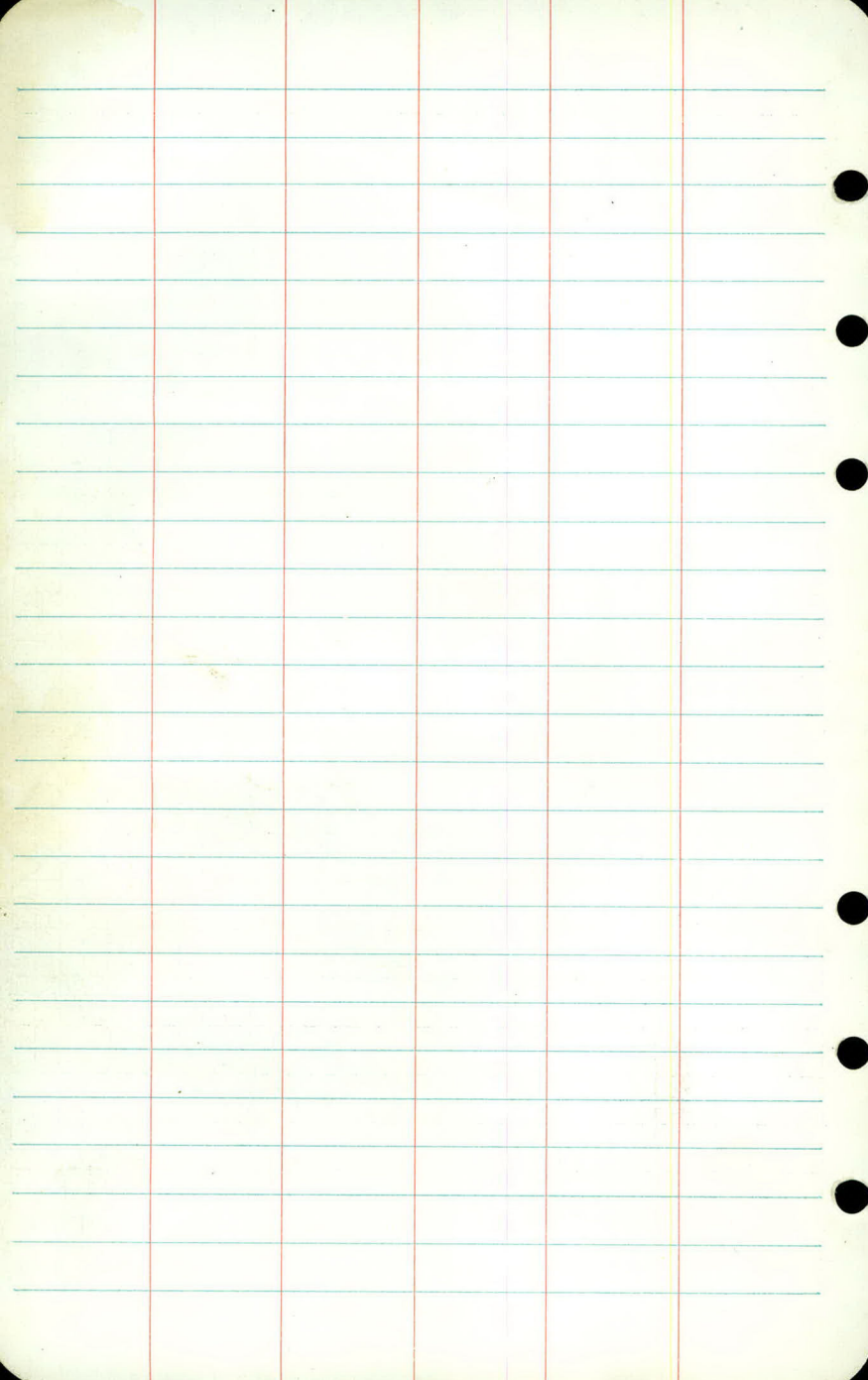
$$124 + 40 \quad LT \text{ \& } RT$$

$$98 + 04 \quad LT \text{ \& } RT$$

$$97 + 22 \quad LT \text{ \& } RT$$

$$70 + 33 \quad LT \text{ \& } RT$$

$$61 + 23 \quad LT \text{ \& } RT$$



RG
LPD

March 3, 1976
cldy 25°

Bench Levels

County Rd "F"

from

McMenemy Rd to Centerville Rd

3 pages

Sta	+	Δ		Elev.	
BM	0.52	943.13		942.61	✓
BM	0.74	932.95	10.92	932.21	✓
TP	0.31	923.95	9.31	923.64	✓
TP	0.03	916.88	7.10	916.85	(916.86)
TP	1.51	907.69	10.70	906.18	(906.19)
TP	7.41	907.30	7.80	899.89	(899.90)
TP	6.85	907.56	6.59	900.71	(900.72)
					904.78
TP	7.69	909.87	5.38	902.18	(902.19)
TP	2.66	906.99	5.54	904.33	(904.34)
TP	3.86	904.04	6.81	900.18	(900.19)
TP	7.04	905.70	5.38	898.66	(898.67)
TP	7.60	910.76	2.54	903.16	(903.17)
TP	6.35	913.01	4.10	906.66	(906.67)
TP	11.45	920.25	4.21	908.80	(908.81)
TP	0.86	920.46	0.65	919.60	(919.61)
TP	4.10	912.91	11.65	908.81	
TP	4.02	910.70	6.23	906.68	
TP	2.55	905.72	7.53	903.17	
TP			7.04	898.68	

RG
LPD

Mar. 3, 1976
Cldy 25°

2

Top NW Cor lower step to #310 Co Rd "F"

spike in Arc Lt pole SW Cor M = M & F

spike in PP^{#79} AT STA. 67+35±

MH RT STA. 71+50

✓ SPIKE IN PP^{#81} NE. COR. OF F. + S. OAK DR.

✓ SPIKE IN PP^{#83} LT. STA. 81+00

✓ SPIKE IN PP^{#85} LT. STA. 87+30

✓ SPIKE IN PP^{#87} LT. STA. 94+~~50~~³⁸ 94+00

✓ SPIKE IN PP^{#89} NE. COR. OF F. + CLOVER ^{NE}

✓ SPIKE IN PP^{#91} LT. STA. 107+00

✓ SPIKE IN PP^{#93} LT. STA. 113+50

✓ SPIKE IN PP^{#95} LT. STA. 120+20

✓ SPIKE IN PP^{#97} LT. STA. 127+20

✓ SPIKE IN PP^{#99} LT. STA. 134+20

✓ SPIKE IN PP^{#101} NW. COR. F. + CENTERVILLE RD.

PP[#] 99

PP[#] 97

PP[#] 95

PP[#] 93

STA	+	Δ	-	FLV.
TP	5.29	903.97		898.68
TP	6.68	906.88	3.77	900.20 (900.19)
TP	5.48	909.83	2.53	904.35 (904.34)
TP	5.35	907.55	7.63	902.20 (902.19)
TP	6.62	907.34	6.83	900.72
TP	7.73	907.64	7.43	899.91 (899.90)
TP	10.77	916.97	1.44	906.20 (906.19)
TP	7.10	923.96	0.11	916.86
TP	10.35	933.99	0.32	923.64
TP	10.98	943.19	1.78	932.21
BM			0.60	942.59 (942.61)

RG
LPD

3-MAR-76
P. CLDY. 30°

3

[#]
PP 93

[#]
PP 91

[#]
PP 89

[#]
PP 87

[#]
PP 85

[#]
PP 83

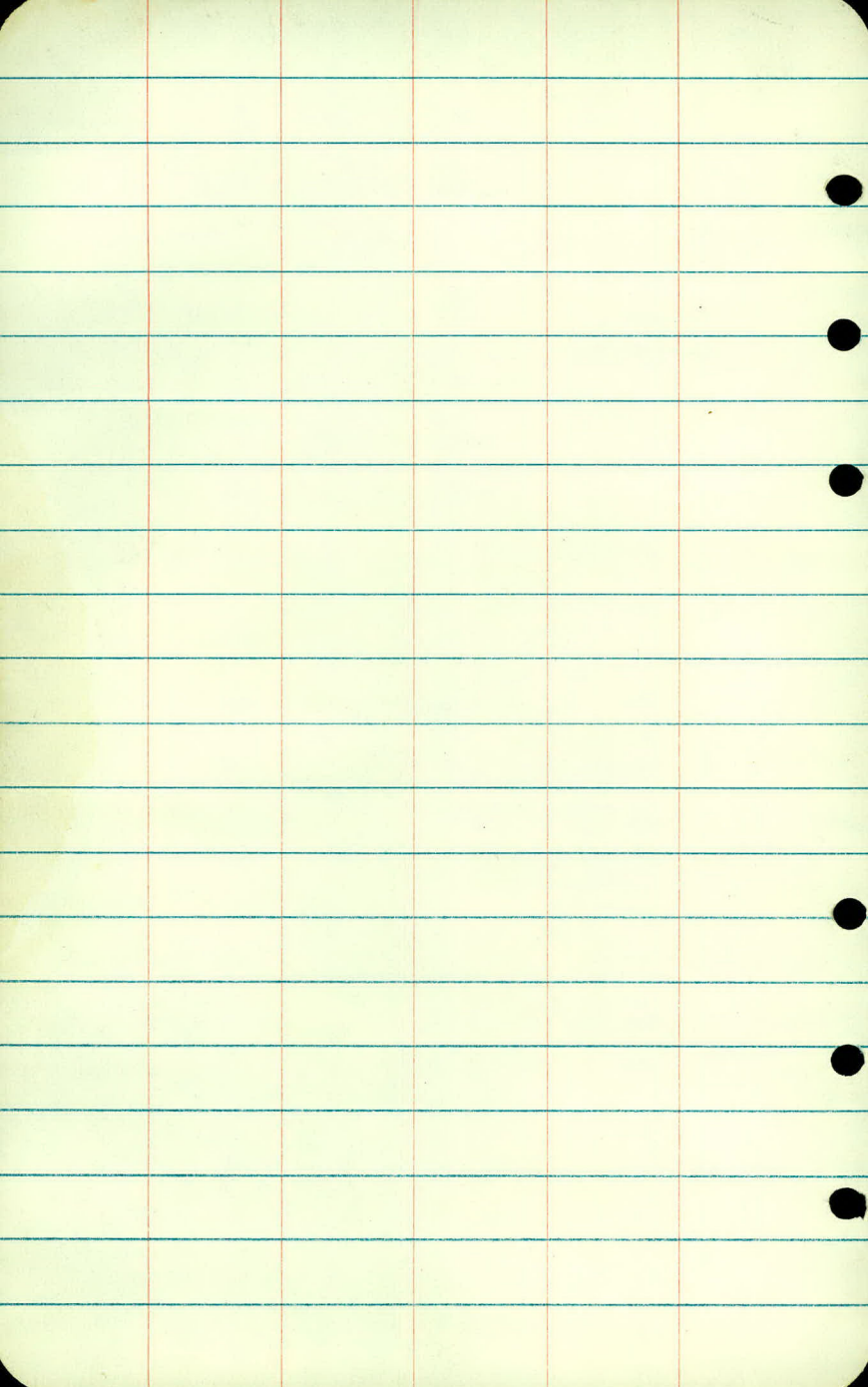
[#]
PP 81

MH RT STA. 71+50

[#]
PP 79

SPIKE IN ARC. LT POLE SW. COR. MEM + F

TOP NW. COR. LOWER STEP 40° 310



19 MAR 1976

a

KP
DS
RJ
TJ

Co. RD, F

McMenemy to Centerville RD

ADDITIONAL X-SECTIONS

STA	+	π	-	ELEV.
-----	---	-------	---	-------

BM	11.74	928.60		
----	-------	--------	--	--

				916.86
--	--	--	--	--------

70+00				
-------	--	--	--	--

✓				
---	--	--	--	--

+50				
-----	--	--	--	--

✓				
---	--	--	--	--

71+00				
-------	--	--	--	--

✓				
---	--	--	--	--

RT
DS
RT
TS

LT

14

RT

b

TOP MH RT STA 71+50

19.3	18.1	18.5	18.8	18.85	18.6	18.2	17.5	19.1	20.2
9.3	10.5	10.1	9.8	9.75	10.0	10.4	11.1	9.5	8.4
25	23	18	11		14	19	28	43	50

23.6	28.4	28.9
5.0	0.2	+0.3
36	47	50

33.1	28.6	23.2	21.6	17.9	17.80	17.9	17.8	16.5	17.7
+4.5	0.0	5.4	7.0	10.7	10.80	10.7	10.8	12.1	10.9
50	41	33	23	11		13	15	19	26

22.2
6.4
50

28.3	21.9	16.2	16.3	16.7	16.70	16.5	15.6	16.1	20.1	23.4
0.3	6.7	12.4	12.1	11.9	11.9	12.1	13.0	12.5	8.5	5.2
41	32	22	16	11		13	18	26	38	50

22.4
+3.8
50

STA

+

π

-

ELEV

928.60

71+50

✓

72+00 ± ENT RT

+50

7 TP

6.26 919.94 14.92 913.68

73+00

BM

13.74

906.20

(906.19)

XP
DS
RJ
TJ

LT

19 MAR 76
RT

C

28.6	21.1	14.8	15.3	15.40	15.3	14.4	15.0	18.6
0.0	7.5	13.8	13.3	13.2	13.3	14.2	13.6	10.0
50	37	23	11		13	20	28	37

21.6
7.0
50

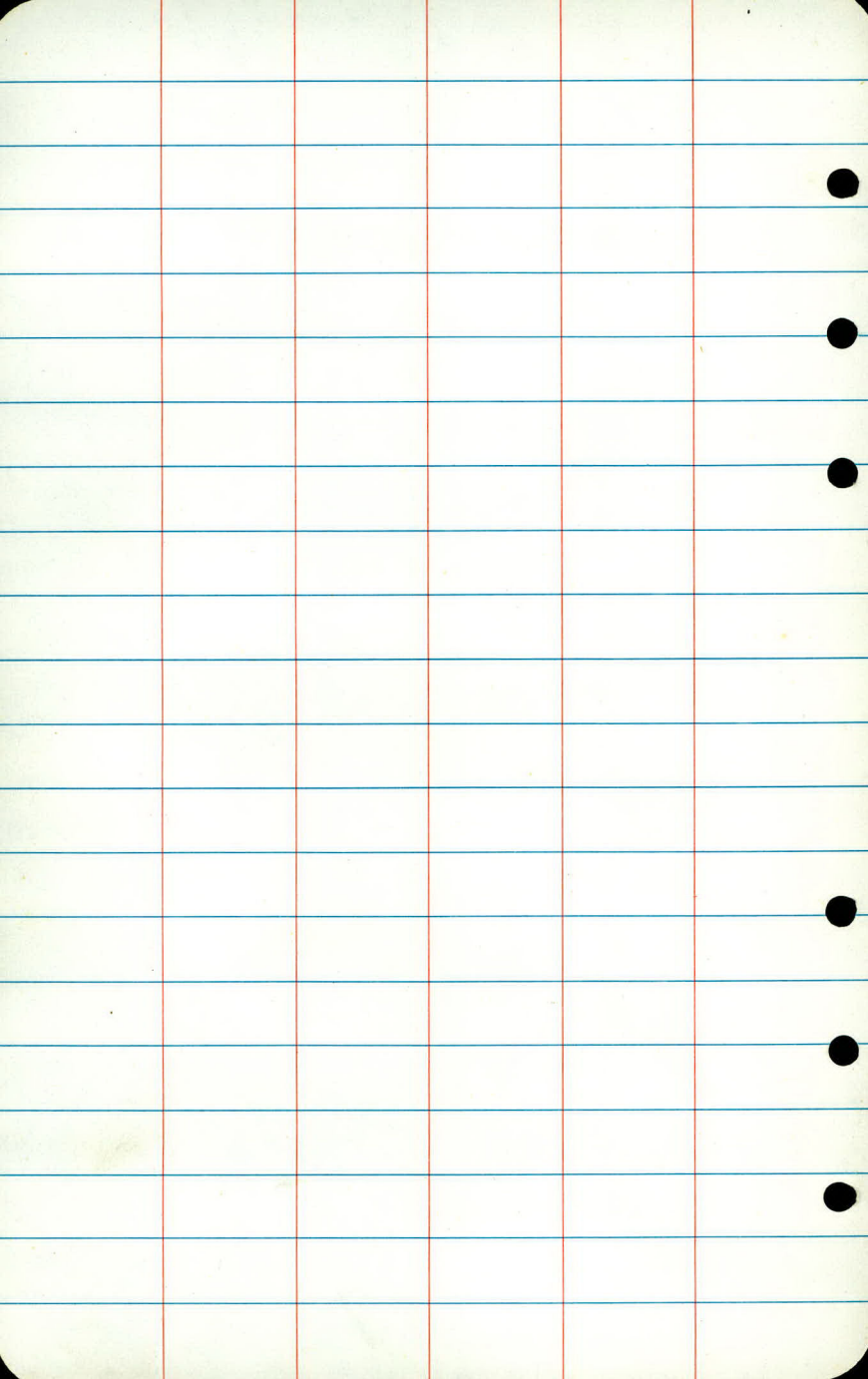
23.3	19.4	13.2	13.7	13.2	14.1	14.6
5.3	9.2	15.4	15.3	14.93	15.4	14.5
50	43	22	11		13	29

2.4	12.1	11.9	12.10	11.6	11.4	10.6	12.4	12.6
6.2	16.5	16.7	16.5	17.0	17.2	18.0	16.0	16.0
50	30	12		12	21	25	40	50

STA 72+00

15.9	11.0	10.6	10.4	10.64	10.1	9.8	8.0	8.3	7.3
4.0	8.9	9.3	9.5	9.3	9.8	10.1	11.9	11.6	12.6
50	37	31	11		12	18	28	38	50

SPIKE IN PP Cor E & S. OAK DR.



KPLW
DS &
GAT
TS

16 MARCH 1976 d=1
SUNNY 30°

CO. RD. F

MC MENEMY TO CENTERVILLE RD.

X-SECTIONS

STA + π - ELEV.

BM 11.38 917.57

906.19

73+50

+76

74+97 1.88 908.54 10.91 906.66

74+14 = $\neq$ S, OAK DR

+23 = SHOULDER LT

+38

KP
DS
GA
TJ

LT

16 MARCH 1976
RT

2.

SPIKE IN PP NELO F = S. OAK DR

14.0 15.2 8.8 8.5 8.0 8.9 909.07 8.5 7.8 5.3 3.6 3.1
3.57 2.4 8.8 9.1 9.6 8.7 8.5 9.1 9.8 12.3 14.0 14.5
66 55 40 28 20 12 11 19 34 56 75
CONC.

7.5 7.7 7.4 8.1 900.47 7.7 7.2 6.1 3.8 1.2
10.1 9.9 10.2 9.5 9.1 9.9 10.4 11.5 13.8 16.4
75 49 23 14 12 17 28 42 75

TOP MH 32' RT

905.44 05.7 06.0 06.2 06.8 907.34 06.7 06.1 04.5 02.3 901.24
3.1 2.8 2.5 2.3 1.7 1.2 1.8 2.4 4.0 6.2 7.3
150 100 75 24 12 11 20 33 46 75

5.3 5.8 5.9 6.8 907.14 6.4 5.7 2.4 900.7 900.0
3.2 2.7 2.6 1.7 1.4 2.1 2.8 6.1 7.6 8.5
75 50 27 11 12 21 40 56 75

2.1 2.9 4.6 5.2 906.84 6.1 5.2 1.9 0.6 899.9
6.4 5.6 3.9 2.3 1.7 2.4 3.3 6.6 7.9 8.6
75 56 29 15 12 21 35 52 75

STA	+	π	-	ELEV
		908.54		
74+50				
75+00				
+50				
76+00				
+50				
77+00				
TP	4.10	907.02	5.62	902.92

KP
DS
GA
TV

LT

16 MAR 1976
RT

3,

901.1 2.1 3.4 5.4 6.3 906.64 5.9 5.1 1.4 0.4 899.7
7.4 6.4 5.1 2.9 2.2 1.9 2.4 3.4 7.1 8.1 8.8
75 58 31 19 13 11 21 35 55 75

0.6 0.4 0.8 4.3 5.1 905.48 4.8 3.6 0.3 899.5 899.5
7.9 8.1 7.7 4.2 3.4 3.06 3.7 4.9 8.2 9.0 9.0
75 59 31 18 11 12 24 32 58 75

99.1 99.4 99.7 03.2 4.0 904.54 3.8 2.9 99.4 99.2 99.2
9.4 9.1 8.8 5.3 4.5 4.0 4.7 5.6 9.1 9.3 9.3
75 63 32 20 12 13 21 33 61 75

99.1 99.3 99.5 02.4 03.1 903.80 02.3 02.8 00.1 99.7 99.2
9.4 9.2 9.0 6.1 5.4 4.74 5.2 5.7 8.4 8.8 9.3
75 59 31 19 13 11 18 21 54 75

899.0 898.9 99.5 02.1 02.6 903.24 02.9 02.3 99.8 00.3 99.2 99.2
9.5 9.6 9.0 6.4 5.9 5.2 5.6 6.2 8.7 8.2 9.3 9.3
75 61 30 18 13 11 20 35 45 63 75

98.9 99.1 99.5 1.7 02.4 902.82 02.4 901.2 899.7 900.5 99.3 99.1
9.6 9.4 9.0 6.8 6.1 5.62 6.1 7.3 8.8 8.0 9.2 9.4
75 58 30 20 12 12 22 38 46 65 75

TOP PK & STA 77+00

STA	+	π	-	ELEV.
		907.02		
77+50				
78+00				
+50				
79+00				
+50				
80+00				
BM	6.32	22	7.10	899.92 (899.90)

KP
DS
6A
TJ

LT

16 MAR. 1976

RT

4.

99.1 99.3 99.0⁰ 02.0 02.5 902.82 02.3 01.7 99.9 99.4 99.3
7.9 7.7 7.0 5.0 4.5 4.2 4.7 5.3 7.2 7.6 7.7
75 53 26 17 11 11 17 25 41 75

99.0 99.2 99.5 02.0 02.3 902.77 02.4 02.0 99.8 00.6 99.6
8.0 7.8 7.5 5.0 4.7 4.25 4.6 5.0 7.2 6.4 7.4
75 51 29 18 13 12 18 27 45 75

98.9 99.3 99.5 902.0 02.4 902.72 02.6 02.3 99.8 00.2 01.2 00.4
8.1 7.7 7.5 5.0 4.6 4.3 4.4 4.7 7.2 6.8 5.8 6.6
75 51 30 18 12 12 17 27 41 48 75

98.9 99.3 99.0 01.6 02.1 902.53 02.3 02.0 00.0 99.3 00.5 99.4
8.1 7.7 8.0 5.4 4.9 4.49 4.7 5.0 7.0 7.7 6.5 7.2
75 50 28 16 12 11 16 29 38 48 75

98.9 99.9 99.1 01.6 02.1 902.42 02.2 01.7 900.0 99.7 99.6 99.4
8.1 8.1 7.9 5.4 4.9 4.6 4.8 5.3 7.0 7.3 7.4 7.6
75 52 28 18 13 11 16 29 40 58 75

98.9 99.3 99.5 01.4 01.9 902.32 02.1 01.6 99.7 99.9 99.4 99.0
8.1 7.7 7.5 5.6 5.1 4.70 4.9 5.4 7.3 7.1 7.6 8.0
75 49 29 18 12 11 16 25 47 60 75

SPIKE IN PP LT STA 81+00

STA

+

 π

-

FLEY,

906. ~~22~~
~~24~~

80+50

81+00

01,25

+50

82+00

01,42

+50

83+00

02,01

KP
DS
GA
RJ
TV

LT

2

17 MAR 76
RT

5.

98.8	99.1	99.5	01.0	901.5	90.04	01.7	00.4	98.9	98.6	98.9
7.4	7.1	6.7	5.2	4.7	4.3	4.5	5.8	7.3	7.6	7.3
75	45	24	18	12		11	20	30	55	75

98.8	98.8	98.8	00.6	01.0	01.24	01.2	00.1	98.8	98.1	98.7
7.4	7.4	7.4	5.6	5.2	4.98	5.0	6.1	7.4	7.5	7.5
75	39	23	10	12		11	22	32	51	75

98.7	98.7	98.8	00.3	00.7	00.9	00.8	00.3	98.9	98.8	98.8
7.5	7.5	7.4	5.9	5.5	5.3	5.4	5.9	7.3	7.4	7.4
75	45	24	16	12		11	18	26	55	75

98.7	98.7	98.8	00.7	01.1	01.42	01.1	00.5	98.6	98.7	98.6
7.5	7.5	7.4	5.5	5.1	4.80	5.1	5.7	7.6	7.5	7.6
75	50	28	18	12		12	18	26	40	75

98.7	98.7	98.8	01.1	01.5	01.7	01.5	00.8	98.7	98.7	98.7
7.5	7.5	7.4	5.1	4.7	4.5	4.7	5.4	7.5	7.5	7.5
75	43	26	17	12		12	18	26	48	75

98.8	98.8	99.2	01.3	01.7	02.03	01.7	01.2	98.8	98.8	98.8
7.4	7.4	7.0	4.9	4.5	4.19	4.5	5.0	7.4	7.4	7.4
75	41	25	18	12		12	18	27	48	75

STA

+

T

-

ELEV.

906.²²~~37~~

2

83+50

+56

Simple Culvert?

84+00

02.15

+50

85+00

02.18

+50

TP

5.45

907.13

907.~~25~~

4.54

901.⁶⁸~~80~~

901.68

KP
DS
GA
RJ
TU

LT

4

17 MAR 76
RT

6.

98.7	98.7	98.8	01.4	01.7	02.0	01.6	01.1	98.4	98.6	98.7
7.5	7.5	7.4	4.8	4.5	4.2	4.6	5.1	7.8	7.6	7.5
75	54	25	16	12	✓	12	16	26	44	75
98.7	98.7	98.7	01.5	01.8	02.1	01.5	01.0	98.7	98.7	98.7
7.5	7.5	7.5	4.7	4.4	4.1	4.7	5.2	7.5	7.5	7.5
75	50	27	17	12		13	17	24	50	75
01.0	98.7	98.9	99.0	01.6	02.0	02.23	01.8	01.4	99.5	98.9
5.2	7.5	7.3	7.2	4.6	4.2	3.99	4.4	4.8	6.7	7.3
75	64	42	26	17	12	✓	11	17	23	37
02.4	98.8	98.8	01.7	02.0	02.3	02.0	01.6	99.2	98.7	98.7
3.8	7.4	7.4	4.5	4.2	3.9	4.2	4.6	7.0	7.5	7.5
75	52	29	17	12	✓	11	17	26	39	60
02.3	98.7	99.0	01.6	01.8	02.25	02.0	01.7	99.1	98.7	98.7
3.9	7.5	7.2	4.6	4.4	3.97	4.2	4.5	7.1	7.5	7.5
75	58	27	17	12	✓	11	16	27	37	60
00.8	98.9	98.9	00.9	01.3	01.8	01.5	01.0	99.6	98.8	98.8
5.4	7.3	7.3	5.3	4.9	4.4	4.7	5.2	7.6	7.4	7.4
75	65	28	17	12		12	18	27	42	60

TOP PK & STA 86+00

STA

+

π

-

ELEV.

907.¹³~~25~~

86+00

+50

87+00

02.05

+50

88+00

+50

KP
DS
GA
RV
TJ

LT

17 MAR 76
RT

7.

✓ 68

901.3	98.0	98.9	00.8	01.1	901.85	01.3	01.1	98.6	98.0	98.9
5.8	8.1	8.2	6.3	6.0	5.45	5.8	6.0	8.5	8.1	8.3
75	60	27	17	12		11	15	23	37	75

02.3	99.3	99.4	00.9	01.3	901.83	01.6	01.3	99.6	98.8	98.9	98.9
4.8	7.8	7.7	6.2	5.8	5.3	5.5	5.8	8.5	8.3	8.4	8.3
75	61	27	18	13		11	15	24	36	55	75

03.7	99.6	99.7	01.2	01.5	902.01	01.7	01.3	99.2	98.9	98.9
3.4	7.5	7.4	5.9	5.6	5.12	5.4	5.8	8.9	8.2	8.2
75	57	26	18	13		11	16	27	44	75

04.4	99.4	99.7	01.6	01.9	902.33	02.0	01.6	98.9	99.2	98.9
2.7	7.7	7.2	5.5	5.2	4.8	5.1	5.5	8.2	7.9	8.2
75	56	26	17	12		11	16	27	45	75

00.3	99.2	00.1	01.8	02.2	902.44	02.2	01.9	99.7	99.7	98.8
2.8	7.9	7.0	5.3	4.9	4.69	4.9	5.2	7.4	7.4	8.3
75	55	28	17	12		11	15	25	42	75

05.0	99.7	99.6	01.7	02.0	902.33	02.0	01.8	99.9	99.8	98.9
2.1	7.4	7.5	5.4	5.1	4.8	5.1	5.3	7.3	7.4	8.3
75	55	28	18	12		11	15	27	44	75

STA	+	π	-	ELEV.
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STA	+	π	-	ELEV.
-----	---	-------	---	-------

907.¹³~~85~~

89+00

+50

90+00

+50

907.40

91 TP

4.86

907.~~54~~

4.57

902.⁵⁶~~68~~

902.54

91+00

KP
DS
GA
RJ
TS

LT

17 MAR 76
RT

8.

04.5 99.6 99.8 02.0 02.3 902.54 02.1 01.7 98.8 99.6 99.3
2.7 7.6 7.4 5.2 4.9 4.69 5.1 5.5 8.4 7.6 7.9
75 54 27 17 12 11 15 26 41 75

03.8 99.6 00.3 01.9 02.2 902.43 02.0 01.7 98.8 900.0 99.2
3.3 7.5 6.8 5.2 4.9 4.7 5.1 5.4 8.3 7.1 7.9
75 53 24 16 12 11 15 25 43 75

03.2 9.5 00.0 01.9 02.3 902.48 02.1 01.8 99.2 99.2 99.2
3.9 7.6 7.1 5.2 4.8 4.65 5.0 5.3 7.9 7.9 7.9
75 48 24 17 12 11 15 27 46 75

03.8 99.6 00.3 01.8 02.2 902.43 02.1 01.9 99.6 99.7 99.3 99.3
3.3 7.5 6.8 5.3 4.9 4.7 5.0 5.2 7.6 7.4 7.8 7.8
75 51 23 17 12 11 15 24 38 52 75

TOP PK & STA 91+00

04.7 02.0 01.0 02.3 02.3 902.54 02.3 02.0 99.7 99.3 99.3
2.7 5.4 6.4 5.1 5.1 4.86 5.1 5.4 7.7 8.1 8.1
75 47 31 21 11 11 16 25 46 75

STA

+

907.40
~~907.54~~
~~907.23~~

—

ELEV

91+22 = $\frac{1}{2}$ ENT LT.

+50

92+00

+50

93+00

+50

KP
DS
6A
RJ
TV

LT

17 MAR 76
RT

9.

03.9 02.8 02.5 02.4 02.60 02.1 01.9 00.1 99.7 99.3
3.5 4.6 4.9 5.0 4.8 5.3 5.5 7.3 8.7 8.1
75 52 31 12 12 16 25 45 75

03.7 02.5 01.2 01.2 02.70 02.3 02.1 00.1 99.3 99.3
3.7 4.9 6.2 6.2 5.1 4.7 5.1 5.3 7.3 8.1 8.1
75 46 34 20 12 11 16 28 49 75

06.6 03.6 01.1 00.7 02.2 02.5 02.75 02.4 02.1 00.4 99.4 99.3
0.8 3.8 6.3 6.7 5.2 4.9 4.6 5.0 5.3 7.0 8.0 8.1
75 60 116 30 17 12 11 15 25 37 75

06.8 04.4 00.9 01.0 02.4 02.6 02.80 02.5 02.4 99.2 99.3 99.3
0.6 3.0 6.5 6.4 5.0 4.8 4.6 4.9 5.2 8.2 8.1 8.1
75 62 48 30 17 12 11 16 28 51 75

07.1 03.9 01.3 01.1 02.0 02.7 02.98 02.7 02.4 99.5 99.4 99.3
0.3 3.5 6.1 6.3 5.4 4.7 4.4 4.7 5.0 7.9 8.0 8.1
75 61 45 26 19 12 11 15 28 50 75

07.4 03.6 00.9 00.8 02.8 03.3 03.30 02.9 02.6 99.8 99.3 99.3
0.0 3.8 6.5 6.6 4.6 4.1 4.1 4.5 4.8 7.6 8.1 8.1
75 57 45 30 18 12 11 15 27 46 75

STA

+

907.40
907.54
~~907.22~~

-

ELEV

94+00

v

908.37
~~908.22~~901.64
~~901.49~~

TP

6.73

5.76

94+50

95+00

+07

8.86

899.51

KP
DS
GA
RV
TJ

LT

17 MAR 1976
RT

10.

01.4	03.9	01.1	00.5	03.4	03.6	03.71	03.3	03.0	00.1	00.0	99.4	99.9
0.0	3.5	5.7	6.9	4.0	3.8	3.69	4.1	4.4	7.3	7.4	8.0	8.2
66	54	43	28	16	12		11	16	29	43	54	75

07.9
+ 0.5
75

TOP MH 34' RT STA 95+65

08.4	07.4	03.4	01.2	03.7	03.9	03.97	03.6	03.2	00.1	00.2	00.2
0.0	1.0	5.0	7.2	4.7	4.5	4.4	4.8	5.2	8.3	8.2	8.2
75	62	49	30	16	12		11	17	31	39	75

07.9	07.7	04.3	01.2	01.4	03.5	03.8	03.4	03.0	00.5	00.1	00.6	01.7
0.5	0.7	4.1	7.2	7.0	4.9	4.6	4.50	5.0	5.4	7.9	8.3	7.8
75	64	49	36	27	15	11		11	17	29	36	46

FL 18" CMP 33' RT

STA

+

~~908.27~~
~~908.31~~
 908.22

-

ELEV

95+18

- ENT RT

+27

8.96

899.41

+50

BM

6.15

~~902.22~~
 36

~~902.27~~
 58

(902.19)

BM

5.53

909.87

3.93

~~904.27~~
 58

904.44

(904.34)

96+00

+13

8.58

901.29

KP
DJ
GA
PJ
TV

LT

17 MAR 1976
RT

11.

0.1	0.1	0.4	0.4	0.1	0.0	0.3	0.3	0.3	0.2	0.2	0.2	0.2
0.8	0.8	4.0	7.4	7.4	5.2	4.8	4.6	5.1	6.2	6.3	6.12	
75	66	54	39	26	16	12		13	31	48	80	
BT Conc												

FL 18" CMP 33' RT

0.7	0.8	0.1	0.9	0.3	0.3	0.3	0.3	0.2	0.1	0.4	0.3	0.2
0.7	4.6	7.4	7.5	5.2	4.9	4.6	5.1	5.6	7.7	8.0	7.1	5.9
75	54	41	25	15	11		12	18	30	38	43	75

SPIKE IN PP LT STA 94+54

SPIKE IN PP NE COR F = CLOVER

0.7	0.1	0.1	0.1	0.1	0.1	0.3	0.3	0.3	0.1	0.1	0.2	0.3	0.4	0.4
2.0	3.8	5.8	8.8	8.8	7.5	6.3	6.10	6.5	6.8	8.9	7.5	6.5	5.7	
75	64	54	40	27	21	12		12	17	31	43	57	75	

FL 12" CMP 30' RT

STA	+	π	-	ELEV
-----	---	-------	---	------

		909.87		
--	--	--------	--	--

96+30	=	E	ENT	RT
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+46				
-----	--	--	--	--

			7.85	
--	--	--	------	--

				902.02
--	--	--	--	--------

				907.85
--	--	--	--	-------------------

+50				
-----	--	--	--	--

97+00				
-------	--	--	--	--

+50				
-----	--	--	--	--

+61				
-----	--	--	--	--

			4.62	
--	--	--	------	--

				905.25
--	--	--	--	--------

KP
DS

LT

17 MAR 1976
RT

12

GA
RT

07.2 01.2 03.9 01.9 02.2 03.6 03.8 03.97 03.8 03.5 03.9 04.3
2.7 2.7 6.0 8.0 7.7 6.3 6.1 5.9 6.1 6.4 6.0 5.6
75 65 47 36 26 17 12 11 29 52 75

FL 12" CMP 29' RT

06.9 06.9 02.4 02.0 03.8 03.9 04.17 03.8 03.7 02.5 05.5 06.5
3.0 3.0 7.5 7.9 6.1 6.0 5.7 6.1 6.2 7.4 4.4 3.4
75 66 40 30 17 12 11 17 27 44 75

07.0 04.7 03.0 04.1 04.6 04.8 04.3 04.0 02.8 06.2 06.8
2.9 5.2 6.9 5.8 5.3 5.07 5.6 5.9 7.1 3.8 3.1
75 43 34 18 12 12 18 30 44 75

06.8 06.3 05.2 04.9 05.07 05.0 05.2 05.5
3.1 3.6 4.7 5.0 4.8 4.9 4.7 4.4
75 55 30 11 13 48 75

TOP MH 34' RT

STA	+	π	-	ELEV
-----	---	-------	---	------

		909.87		
--	--	--------	--	--

97+63	= E CLOVER AVE S.			
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98+00				
-------	--	--	--	--

+50				
-----	--	--	--	--

99+00				
-------	--	--	--	--

+50				
-----	--	--	--	--

+85				
-----	--	--	--	--

		7.65	902.22	
--	--	------	--------	--

TP	4.06	908.52	5.41	904.46
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KP
BS
GA
EV
TJ

LT

£

17 MAR 1976

13

RT

06.8	06.5	06.0	05.1	04.9	05.07	05.3	05.5	06.0	06.4	06.7
3.1	3.4	3.9	4.8	5.0	4.8	4.6	4.4	3.9	3.5	3.2
75	62	45	25	11		25	64	100	150	200

06.6	06.3	05.3	04.8	05.03	04.4	04.5	05.4	05.7
3.3	3.6	4.6	5.1	4.84	5.5	5.4	4.5	4.2
75	58	34	11		20	36	44	75

06.6	05.5	04.5	04.5	04.77	04.5	04.1	03.5	04.9	05.8
3.3	4.4	5.4	5.4	5.1	5.4	5.8	6.4	5.0	4.1
75	45	25	12		12	18	28	42	75

06.5	06.1	04.0	03.2	04.3	04.6	04.71	04.4	04.1	03.3	04.9	05.7
3.4	3.8	5.9	6.7	5.6	5.3	5.16	5.5	5.8	6.6	5.0	4.2
75	56	41	30	17	10		13	18	28	45	75

05.7	04.7	03.7	03.7	04.4	04.57	04.3	04.0	02.9	04.0	03.7
4.2	5.2	6.6	6.2	5.5	5.3	5.6	5.9	7.0	5.9	6.2
75	39	34	24	11		14	20	29	40	75

FL 18" CMP 23' LT

TOP PK £ STA 100+00

STA	+	π	-	ELEV
-----	---	-------	---	------

		908.52		
--	--	--------	--	--

100+00				
--------	--	--	--	--

+11	= E	CLOVER	N	
-----	-----	--------	---	--

+19				
-----	--	--	--	--

		5.42	903.10	
--	--	------	--------	--

+33				
-----	--	--	--	--

		6.60	901.92	
--	--	------	--------	--

+50				
-----	--	--	--	--

101+00				
--------	--	--	--	--

KP
DS
6A
RJ
TU

LT

E

17 MAR 1974
RT

14,

04.2 04.0 03.9 04.3 ✓ 04.1 03.6 02.4 03.3 02.7
4.3 4.5 4.6 4.2 4.06 4.4 4.9 6.1 5.2 5.8
75 56 35 10 14 20 30 44 75

04.5 04.2 04.3 04.4 ✓ 03.9 03.6 02.3 02.8 02.5
4.0 4.3 4.2 4.1 4.1 4.6 4.9 6.2 5.7 6.0
100 53 27 10 14 19 29 44 75

TOP MH 33' RT

FL 18" CMP 23' LT

04.4 03.7 03.0 01.6 02.2 03.1 03.8 ✓ 04.12 03.7 03.2 01.3 01.5 01.6
4.1 4.8 5.5 6.9 6.3 5.4 4.7 4.4 4.8 5.3 7.2 7.0 6.9
75 40 26 24 20 18 11 13 19 31 49 75

04.1 06.3 02.9 01.1 03.0 03.5 ✓ 03.75 03.4 02.7 00.2 00.5 00.4
4.4 5.2 5.6 7.4 5.5 5.0 4.77 5.1 5.8 8.3 8.0 8.1
75 41 26 20-23 17 10 13 19 33 48 75

STA	+	π	-	ELEV
		908.52		
101+23			8.05	900.47
+44	E	ENT	LT.	
+63			9.12	899.40
TP	4.57	907.18	5.91	902.61
102+00				
+50				

KP
DS
GA
RU
TD

LT

17 MAR 76
RT

15

FL 18" CMP 23' LT

✓
903.02 903.02 903.02 903.42 903.62 903.22 02.7 99.4 99.6 99.2
5.5 5.5 5.5 5.1 4.9 5.3 5.8 9.1 8.9 9.3
75 64 32 10 14 18 31 48 75

FL 18" CMP 23' LT

TOP PK & STA 103+00

✓
01.3 01.3 01.3 02.3 02.3 02.3 02.9 02.6 00.0 99.9 99.0
5.9 5.9 5.9 4.3 3.9 3.8 4.3 4.6 7.2 7.3 8.2
75 37 23 15 11 14 18 29 48 75

✓
01.3 01.3 01.3 02.3 02.6 02.6 02.9 01.9 99.4 99.6 99.4
5.9 5.9 5.9 4.9 4.6 4.5 4.9 5.3 7.8 7.6 7.8
75 50 26 18 11 14 19 30 50 75

STA	+	π	-	ELEV
		907.18		
102+56			6.25	900.93
+77			6.06	901.12
103+00				
+50				
104+00				
+50				

KP
DS
RJ
TU

LT

18 MAR 1976
SUNNY 50° RT

16

TOP MH 33' RT

TOP MH 22' RT

01.3 01.3 01.4 02.2 02.6 02.6 02.2 02.0 02.3
5.9 5.9 5.8 5.0 4.6 4.57 5.0 5.2 7.9 7.5 7.5
75 45 23 16 11 15 20 32 65 75

01.1 01.1 01.1 01.8 02.2 02.7 01.4 00.3 00.5 00.4
6.1 6.1 6.1 5.3 5.0 4.8 4.5 5.8 7.9 7.8 7.8
75 47 24 17 11 13 21 32 54 75

00.6 00.8 01.4 01.0 01.8 01.9 01.7 01.1 00.4 00.5 00.0
6.6 6.4 5.8 6.2 5.4 5.3 5.07 5.5 6.1 7.8 7.7 7.2
75 62 38 22 17 11 15 20 32 53 75

00.1 01.2 01.0 02.5 01.7 01.6 01.4 00.8 00.4 00.0
7.1 6.0 6.2 5.7 5.4 5.2 5.6 5.8 7.4 7.8 7.4
75 49 28 18 11 13 17 25 48 75

STA	+	π	-	ELEV
		907.18		

105+00

BM	6.33	906.52	6.90	900.28	900.19
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105+25

+50

+75

7.20 899.32

+83 - $\pm$ ENT RT

KP
DS
RJ
TV

LT

18 MAR 76

RT

17

00.4 01.0 00.5 01.8 02.1 902.14 01.6 01.4 00.0 00.3 99.9
6.8 6.2 6.7 5.4 5.1 5.04 5.6 5.8 7.2 6.9 7.3
75 41 27 17 11 14 17 29 50 75

SPIKE IN PP LT STA 107+00

03.1 03.7 03.1 00.2 01.4 01.6 901.82 01.7 01.5 99.8 01.5 00.0
3.4 2.8 3.4 6.3 5.1 4.9 4.7 4.8 5.0 6.7 6.0 6.5
75 64 48 28 17 11 12 15 30 50 75

04.0 03.7 00.0 01.4 01.6 901.82 01.5 01.2 99.8 00.0 00.8
2.5 2.8 6.5 5.1 4.9 4.7 5.0 5.4 6.7 5.9 6.3
75 45 28 16 11 12 16 33 50 75

FL 15" CMP 31' RT

03.5 03.8 00.0 01.1 01.5 901.82 01.5 01.6 01.7 01.9
3.0 2.7 6.5 5.4 5.0 4.8 5.0 4.9 4.8 4.6
75 43 29 16 11 11 30 48 75

STA	+	π	-	ELEV.
-----	---	-------	---	-------

		906.52		
--	--	--------	--	--

105+90				
--------	--	--	--	--

			5.15	901.37
--	--	--	------	--------

+94				
-----	--	--	--	--

			6.75	899.77
--	--	--	------	--------

106+00				
--------	--	--	--	--

+50				
-----	--	--	--	--

+69				
-----	--	--	--	--

			7.04	899.48
--	--	--	------	--------

+79				
-----	--	--	--	--

	E	ENT	RT	
--	---	-----	----	--

RP
DS
RJ
TJ

LT

£

18 MAR 76
RT

18

TOP MH 25' RT

FL 15" CMP 31' RT

02.9	03.6	09.9	09.7	00.9	01.2	01.4	01.5	00.0	01.8	02.2
3.6	2.9	6.6	6.8	5.6	5.3	4.87	5.1	5.0	6.5	4.7
75	45	30	24	17	12		12	20	32	51

03.0	02.9	09.1	09.5	00.8	01.0	01.0	00.9	09.8	01.7	03.3
3.5	3.6	6.8	7.0	5.7	5.5	5.0	5.5	5.6	6.7	4.8
75	33	30	23	17	12		13	22	28	45

FL 15" CMP 30' RT

02.6	02.7	09.4	09.7	00.6	00.8	00.8	01.0	01.4	02.1
3.7	3.8	7.1	6.8	5.9	5.7	5.5	5.7	5.5	5.1
75	40	30	23	17	13		11	26	48

STA	+	π	-	ELEV.
		906.52		

106+86			7.40	899.12
--------	--	--	------	--------

+88			7.25	899.27
-----	--	--	------	--------

107+00	ENT LT			
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+06			7.67	898.85
-----	--	--	------	--------

+50				
-----	--	--	--	--

108+00				
--------	--	--	--	--

TP	4.74	904.24	7.02	899.50
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KP
DS
RJ
TV

LT

E

18 MAR 76
RT

19.

FL 15" CMP 28' LT

FL 15" CMP 30' RT

00.2	00.3	00.5	00.7	901.05	00.7	00.7	99.5	00.0	00.6	00.8
6.3	6.2	6.0	5.8	5.47	5.8	5.8	7.0	6.5	5.9	5.7
75	49	28	12		12	20	27	38	49	75

FL 15" CMP 29' LT

97.1	98.4	98.2	99.8	00.1	900.42	00.2	10.1	99.0	98.8	98.7
8.8	8.1	8.3	6.7	6.4	6.1	6.3	6.4	7.5	7.7	7.8
75	40	27	16	11		12	19	30	50	75

97.7	97.6	97.9	97.9	97.3	97.7	900.01	99.8	99.5	97.7	97.9	97.0
8.8	8.9	8.6	8.6	7.2	6.8	6.51	6.7	7.0	8.8	8.6	8.9
75	59	37	23	16	11		13	18	29	49	75

TOP PK E STA 109+00

STA	+	π	-	ELEV.
		904.24		
108+50				
109+00				
+50				
+73			6.20	898.04
+90			7.10	897.14
110+00				
TP	4.38	903.50	5.12	899.12

KP
DS
RJ
TJ

LT

18 MAR 76
RT

20.

97.5 97.5 97.6 97.4 98.9 99.4 ✓
6.7 6.7 6.6 6.8 5.3 4.8 4.5 4.8 5.1 6.7 6.7 6.7
75 56 35 24 16 11 12 18 30 50 75

97.4 97.5 97.5 98.9 99.2 ✓
6.8 6.7 6.7 5.3 5.0 4.7 4 5.0 5.4 6.8 7.1 6.5
75 50 26 17 11 12 17 29 56 75

97.5 97.5 97.5 99.4 99.6 ✓
6.7 6.7 6.7 4.8 4.6 4.7 5.1 5.3 7.0 6.8 7.0
75 50 26 17 11 12 18 30 55 75

TOP MH 46' RT

TOP MH 25' RT

97.5 97.5 97.5 99.0 99.2 ✓
6.7 6.7 6.7 5.2 5.0 4.8 5.3 5.7 7.3 7.3 7.2
75 50 26 17 12 12 19 32 56 75

TOP PK 5TH 111400

STA

+

π

-

ELEV.

903.50

110+50

111+00

+50

112

+50

113

113+00

KP
DS
R3
TJ

LT

18 MAR 76
RT

21

97.4 97.4 97.4 98.7 99.1 ✓ 98.7 98.5 96.6 96.9 96.6
6.1 6.1 6.1 4.8 4.4 4.2 4.8 5.0 6.9 6.6 6.9
75 50 26 16 11 12 17 26 55 75

97.4 97.5 97.5 98.5 98.9 ✓ 98.6 98.0 97.0 96.9 96.6
6.1 6.0 6.0 5.0 4.6 4.38 4.9 5.5 6.5 6.6 6.6
75 50 21 16 11 13 20 25 51 75

97.4 97.4 97.4 98.2 98.5 ✓ 98.2 97.7 96.9 96.9 96.6
6.1 6.1 6.1 5.3 5.0 4.7 5.3 5.8 6.6 6.6 6.7
75 50 21 17 11 13 18 23 50 75

97.4 97.4 97.4 98.1 98.3 ✓ 98.1 98.8 96.8 96.8 96.6
6.1 6.1 6.1 5.4 5.2 4.93 5.4 5.7 6.7 6.7 6.7
75 50 21 17 12 13 17 21 50 75

97.5 97.5 97.5 97.8 98.3 ✓ 98.1 97.8 96.7 96.9 97.0
6.0 6.0 6.0 5.7 5.3 4.9 5.4 5.7 6.8 6.6 6.5
75 50 22 17 12 13 19 24 50 75

97.5 97.5 97.5 98.2 98.6 ✓ 98.7 98.5 96.6 96.7 96.6
6.0 6.0 6.0 5.3 4.9 4.55 4.8 5.0 6.9 6.6 6.6
75 50 24 20 12 12 19 27 49 75

STA	+	π	-	ELEV.
		903.50		
113+50				
+64	= ∇	ENT.	Rt	
+91			6.03	897.47
+95			7.23	896.27
114+00				
+19	= ∇	ENT	LT	

KP
DS
RS
TJ

LT

18 MAR 76

RT

22.

97.2 97.2 97.4 98.5 99.1 99.50 99.1 98.7 96.9 97.0 96.0
6.3 6.3 6.1 5.0 4.4 4.0 4.4 4.8 6.6 6.5 6.6
75 42 24 17 12 13 19 27 45 75

97.5 98.1 97.5 97.5 98.1 99.2 99.40 99.1 98.8 98.4 98.5
6.0 5.4 6.0 6.0 4.8 4.3 4.1 4.4 4.7 5.1 5.0
75 55 40 25 18 12 12 34 55 75

TOP MH 25' RT

FL 15' CMP 25' LT

98.8 99.1 98.8 98.0 99.2 99.4 99.59 99.2 98.6 97.1 97.4 97.3
4.7 3.8 4.7 5.5 4.3 4.1 3.9 4.3 4.9 6.4 6.1 6.2 5.0
75 46 40 30 17 11 12 19 27 37 57 75

90.0 99.6 99.3 99.2 99.6 99.60 99.2 98.9 97.3 97.4 97.1 97.0
3.5 3.9 4.2 4.3 3.9 3.9 4.3 4.6 6.2 6.1 6.2 6.2
75 60 40 25 11 12 17 25 39 57 75

STA	+	π	-	ELEV.
-----	---	-------	---	-------

		903.50		
--	--	--------	--	--

114+29				
--------	--	--	--	--

		6.75	896.75	
--	--	------	--------	--

+50				
-----	--	--	--	--

	ENT RT			
--	--------	--	--	--

115+00				
--------	--	--	--	--

BM				
----	--	--	--	--

	6.13			
--	------	--	--	--

		904.80		
--	--	--------	--	--

			4.79	
--	--	--	------	--

				898.71
--	--	--	--	--------

				898.67
--	--	--	--	--------

115+41				
--------	--	--	--	--

			7.71	
--	--	--	------	--

				897.09
--	--	--	--	--------

+50				
-----	--	--	--	--

	=			
--	---	--	--	--

		ENT		
--	--	-----	--	--

			LT	
--	--	--	----	--

KP
DS
RJ
TJ

LT

18 MAR 76

RT

23

FL 15" CMP 25' LT

00.4	00.2	97.5	97.5	99.2	99.5	✓	99.2	98.3	97.8	97.7
3.1	3.3	6.0	6.0	4.3	4.0	899.70	3.8	4.3	5.2	5.8
75	57	37	23	16	11	✓	13	31	53	75

99.5	99.0	97.5	97.6	99.1	99.5	✓	99.1	96.7	97.0	97.1	97.5	
4.0	4.5	6.0	5.9	4.4	4.0	899.59	3.91	4.4	4.8	6.5	6.4	6.0
75	54	40	23	17	11	✓	14	18	25	37	75	

SPIKE IN PP LT 113+50

FL 15" CMP 25' RT

99.2	99.1	98.8	99.8	✓	99.6	99.2	97.4	97.3	96.9
5.6	5.7	6.0	5.0	4.7	5.2	5.6	7.4	7.5	7.9
75	55	32	12	✓	14	17	24	42	75

STA

+

π

-

ELEV.

904.80

115+61

7.87

116+00

+50

117+00

+50 = ENT RT

+90

8.11

907.82

5.09

899.71

KP
DS
RJ
TJ

LT

£

18 MAR 76

RT

24

FL 15" CMP LT 25'

99.0	97.8	97.6	99.7	00.1	900.39	99.9	99.6	97.5	97.0	97.1
5.8	7.0	7.2	5.1	4.7	4.41	4.9	5.2	7.3	7.8	7.7
75	50	24	16	12		12	18	27	52	75

99.0	98.3	97.9	00.0	00.3	900.70	00.2	99.9	98.1	97.9	96.9
5.8	6.5	6.9	4.8	4.5	4.1	4.6	4.9	6.7	6.9	7.9
75	41	25	16	12		13	19	27	49	75

98.4	98.1	97.6	99.9	00.6	900.85	00.5	00.2	98.3	97.9	97.4
6.4	6.7	7.2	4.9	4.2	3.95	4.3	4.6	6.5	6.9	7.4
75	49	28	18	12		13	20	30	60	75

98.5	98.4	98.2	00.9	901.10	00.7	99.9	98.6	98.6
6.3	6.4	6.6	3.9	3.7	4.1	4.9	6.2	6.2
75	44	25	13		13	29	61	75

TOP MH 25' RT

STA	+	π	-	ELEV.
-----	---	-------	---	-------

		907.82		
--	--	--------	--	--

118+00				
--------	--	--	--	--

+14				
-----	--	--	--	--

		9.53		
--	--	------	--	--

			898.29	
--	--	--	--------	--

+22 =	$\neq$	ENT	LT	
-------	--------	-----	----	--

+34				
-----	--	--	--	--

		9.32		
--	--	------	--	--

			898.50	
--	--	--	--------	--

+50				
-----	--	--	--	--

119+00				
--------	--	--	--	--

KP
DS
RJ
TJ

LT

18 MAR 76

RT

25

99.1	98.9	98.2	90.9	91.2	91.1	90.8	98.4	98.1	98.1
8.7	8.9	9.6	6.9	6.6	901.34	6.7	7.0	9.4	9.7
75	41	23	16	11		13	19	35	61

FL 15" CMP 22' LT

90.7	90.6	90.6	91.4	90.52	91.3	91.1	99.2	98.3	98.1
7.1	7.2	7.2	6.4	6.3	6.5	6.7	8.6	9.5	9.6
75	55	30	12		11	19	21	46	75

FL 15" CMP 22' LT

90.4	99.8	99.7	99.3	91.2	91.6	901.72	91.5	91.2	99.5	99.6	99.9
7.4	8.0	8.1	8.5	6.6	6.2	6.1	6.3	6.6	8.3	8.2	7.9
75	48	26	21	16	10		13	20	30	49	75

91.5	90.5	90.3	91.8	92.0	902.17	91.8	91.4	90.2	90.1	90.50
6.3	7.3	7.5	6.0	5.8	5.65	6.0	6.4	7.6	7.7	7.32
75	34	22	15	11		13	20	27	39	66

comp.

STA	+	π	-	ELEV.
-----	---	-------	---	-------

		907.82		
--	--	--------	--	--

119+13 = Φ ENT RT				
------------------------	--	--	--	--

+50				
-----	--	--	--	--

120+00				
--------	--	--	--	--

+03				
-----	--	--	--	--

		7.70	900.12	
--	--	------	--------	--

+12 = Φ ENT LT & ENT RT				
------------------------------	--	--	--	--

+23				
-----	--	--	--	--

		7.57	900.25	
--	--	------	--------	--

KP
PS
RJ
TJ

LT

E

18 MAR 76

RT

26

02.2 00.4 00.3 02.0 02.2 ✓ 01.9 00.7 99.8 99.6
 5.6 7.2 7.3 5.8 5.6 5.6 5.9 7.1 8.0 8.2
 75 43 22 16 12 13 32 53 75

02.6 01.1 00.8 00.1 02.0 02.8 ✓ 01.9 01.5 00.3 00.3 00.6
 5.2 6.7 7.0 7.7 5.8 5.5 5.4 5.9 6.3 7.5 7.5 7.3
 75 48 26 21 17 11 14 22 28 48 75

03.0 02.3 01.6 01.2 02.4 02.1 ✓ 02.3 02.0 00.8 00.0 99.9
 4.8 5.5 6.2 6.6 5.4 5.1 4.99 5.5 5.8 7.0 7.8 7.9
 75 54 39 20 17 10 13 24 38 58 75

FL 15" CMP 21' LT

02.7 02.4 02.4 02.7 ✓ 02.3 00.7 99.8 99.7
 5.1 5.4 5.4 5.1 4.9 5.5 7.1 8.0 8.1
 75 55 34 11 14 37 56 75

FL 15" CMP 21' LT

STA	+	π	-	ELEV.
-----	---	-------	---	-------

		907.82		
--	--	--------	--	--

120+50				
--------	--	--	--	--

121+00				
--------	--	--	--	--

+41	=	$\neq$	ENT	RT
-----	---	--------	-----	----

+50				
-----	--	--	--	--

+58				
-----	--	--	--	--

		6.23	901.59	
--	--	------	--------	--

+67	=	$\neq$	ENT	LT
-----	---	--------	-----	----

KP
DS
RJ
TJ

LT

2

18 MAR 76

RT

27

02.3 01.5 01.7 02.8 03.1 ✓
5.5 6.3 6.1 5.0 4.7 4.6 5.1 5.6 7.4 8.0 8.6
75 42 24 16 11 13 20 26 46 75
FE

02.8 02.1 02.0 03.3 03.4 ✓
5.0 5.7 5.8 4.5 4.4 4.26 4.6 4.8 6.2 6.4 5.7
75 42 22 16 11 13 20 27 46 73
FE Ho

03.1 02.6 02.6 03.7 03.6 ✓
4.7 5.2 5.2 4.1 4.2 4.0 4.5 5.3 5.9 5.80
75 42 23 16 11 13 30 50 68
FE conc.

04.1 02.6 02.4 03.7 03.8 ✓
3.7 5.2 5.4 4.1 4.0 4.0 4.4 4.5 7.2 7.4
75 42 27 18 11 13 21 38 70
FE

FL 15" CMP 25' LT

04.9 04.5 03.7 03.8 ✓
2.9 3.3 4.1 4.0 3.8 4.3 4.5 7.1 7.8
75 51 25 11 13 18 31 75

STA	+	π	-	ELEV.
-----	---	-------	---	-------

		907.82		
--	--	--------	--	--

121+78				
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			5.73	902.09
--	--	--	------	--------

+93	8.43	910.18	6.07	901.75
-----	------	--------	------	--------

122+00				
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+54	=	ENT.	RT	
-----	---	------	----	--

+96				
-----	--	--	--	--

			6.64	903.54
--	--	--	------	--------

123+00	=	ENT	LT	
--------	---	-----	----	--

KP
DS
RJ
TJ

LT

18 MAR 1976
RT

28.

FL 15" CM 25' LT

TOP MH 25' RT

04.7 03.1 02.7 04.2 04.1 ✓
904.29
55 7.1 7.5 6.0 6.1 5.89 6.4 6.8 9.2 8.9 7.7
75 41 25 16 11 13 18 31 51 66

05.3 04.1 03.3 04.4 04.5 ✓
904.68
4.9 6.1 6.9 5.8 5.7 5.5 6.0 7.0 8.0 7.9
75 45 27 16 11 13 28 53 75

FL 15" CM P 23' LT

06.2 05.8 05.3 04.9 ✓
905.12
4.0 4.4 4.9 5.3 5.06 5.5 5.8 6.7 6.5 6.5
75 55 23 10 13 19 26 46 75

STA	+	π	-	ELEV
-----	---	-------	---	------

		910.18		
--	--	--------	--	--

123+16				
--------	--	--	--	--

		6.46	903.72	
--	--	------	--------	--

+50				
-----	--	--	--	--

+53				
-----	--	--	--	--

		5.92	904.26	
--	--	------	--------	--

164	ENT RT & ENT LT			
-----	-----------------	--	--	--

+69				
-----	--	--	--	--

		5.92	904.26	
--	--	------	--------	--

124+00				
--------	--	--	--	--

KP
DS
RJ
TJ

LT

18 MAR 76
RT

29.

FL 15" CMP 23' LT

05.6	05.5	04.3	04.4	05.1	05.3	05.2	05.1	04.2	04.4	04.9
4.6	4.7	5.9	5.8	5.1	4.9	5.0	5.1	6.0	5.8	6.00
75	48	40	27	21	12	13	20	39	58	72
					Conc.					

FL 15" CMP 25' LT

05.8	05.8	05.6	05.4	05.3	04.38	04.29	04.2
4.4	4.4	4.6	4.8	4.5	4.9	5.80	5.89
75	48	24	"	14	36	58	75
				Conc. Conc. Conc.			

FL 15" CMP 25' LT

05.8	05.5	04.3	04.6	05.5	05.7	05.5	05.2	03.7	02.6	02.2
4.4	4.7	5.9	5.6	4.7	4.5	4.7	5.0	6.5	7.6	8.2
75	45	39	27	17	12	13	20	26	46	75

STA + π - ELEV.

910.18

124+50

+69 = ~~E~~ ENT RT

+94

5.04 905.14

125+00

ENT LT

+14

5.17 905.01

+50

BM

5.43

912.10

3.49

906.68

906.67

KP
DS
RJ
TJ

LT

2

18 MAR 76
RT

30.

05.9 06.0 05.1 05.0 06.0 06.2 06.18 05.9 05.6 04.4 03.4 03.3
4.3 4.2 5.1 5.2 4.2 4.0 4.0 4.3 4.6 5.8 6.8 6.1
75 42 35 23 18 12 12 21 39 58 75

06.4 05.9 04.9 04.8 06.1 06.3 06.38 06.0 05.5 05.1 04.7
3.8 4.3 5.3 5.4 4.1 3.9 3.8 4.2 4.7 5.1 5.5
75 46 40 23 18 12 13 33 55 75

FL 15" CMP 26' LT

06.6 06.3 06.1 06.4 06.57 06.2 05.9 05.1 05.0 05.15
3.6 3.9 4.1 3.8 3.6 4.0 4.3 5.1 5.2 5.03
75 57 29 12 13 21 29 47 66
conc.

FL 15" CMP 26' LT

06.5 06.2 05.4 05.6 06.8 07.0 07.08 06.7 06.4 05.4 05.5 05.4
3.7 4.0 4.8 4.6 3.4 3.2 3.1 3.5 3.8 4.8 4.7 4.8
75 42 38 22 17 11 13 20 29 50 75

SPIKE IN PP LT STA 127+20

STA + π - ELEV.

9/2, 10

125+92

6.48 905.62

126+00

+49

7.71

904.39

51

899.29

+50

+54

6.31

905.79

127+00

+47

KP
DS
RJ
TV

LT

19 MAR 1976
Sunny 50° Rt

31

TOP MH 25' Rt

07.7 06.5 05.7 07.0 07.4 907.35 07.1 06.8 05.5 05.1 06.5 07.4
4.4 5.6 6.4 5.1 4.8 4.75 5.0 5.3 6.6 6.4 5.9 6.6
75 43 28 15 11 12 19 28 38 62 75

TOP SD 36' Rt

9.4 6.6 6.4 7.0 7.2 907.50 7.2 6.9 5.2 6.3 7.9
2.7 5.5 5.7 5.1 4.9 4.6 4.9 5.2 6.9 5.8 4.2
75 50 23 16 11 12 18 31 61 75

TOP MH 52' Rt

6.8 6.7 6.4 7.1 907.48 7.2 6.9 5.9 6.3 6.6
5.3 5.4 5.7 5.0 4.62 4.9 5.2 6.2 5.8 5.5
75 HB 17 11 12 18 34 56 75

FL 15" CMP 54 Rt

STA + T - ELEV.

912.10

127+15 = Δ ENT RT

+26

12.80 899.30

+50

128+00 4.76 912.48 4.38 907.72

+30

8.32 904.16

⁵⁰
37' RT

* +40

+50 = ENT RT

* +60

129+00

* 128+40

8.31

904.17

* 128+60

7.80

904.68

KP
DS
RS
TJ

LT

19 MAR 76

RT

32

06.9 06.8 05.5 04.3 06.7 07.1 07.3 07.0 06.4 06.5
5.2 5.3 6.6 7.8 5.4 5.0 4.7 4.8 5.1 5.7 5.6
75 56 39 49 18 12 12 23 43 75

FL 36" CMP 30' LT

07.0 09.5 05.3 07.1 07.3 07.2 06.8 05.0 05.0 06.7
5.1 12.6 6.8 5.0 4.8 4.7 4.9 5.3 7.1 7.1 5.4 5.2
75 51-56 35 16 12 14 18 33 48 66 75

DITCH
03.4 04.5 06.0 05.1 05.1 06.5 07.3 07.3 07.1 04.6 07.3 07.2
9.1 8.0 6.5 7.4 7.4 6.0 5.3 4.76 5.2 5.4 7.9 5.2 5.3
75 56 47 36 24 18 12 14 18 34 65 75

02.5 04.1 04.9 06.8 07.3 07.2 06.7 06.9 07.2 07.6
10.0 8.4 7.6 5.7 5.2 4.7 5.3 5.8 5.6 5.3 4.9
75 51 25 18 13 13 24 37 55 75

02.6 03.9 04.6 06.8 07.4 07.6 07.6 06.3 05.9 07.4 07.1
9.9 8.6 7.9 5.7 5.1 4.77 4.9 4.9 6.2 6.7 5.1 5.4
75 49 26 17 13 13 19 26 42 66 75

FL 15" CMP 39' RT

FL 15" CMP 39' RT

STA + π - ELEV

912,48

29+32 = $\neq$ ENT RT

+50

130+00

+02

5.83 906,65

+50

131+00

XP
DS
RS
TJ

LT

£

19 MAR 76
RT

33

02.7 04.0 04.5 06.9 07.3 ✓ 07.6 07.7 07.7 08.1
9.8 8.5 8.0 5.6 5.2 4.7 4.9 4.8 4.8 4.4
75 49 29 18 13 11 26 48 75

02.8 04.0 04.3 06.7 07.2 ✓ 07.4 07.2 06.8 07.6 08.8
9.7 8.5 8.2 5.8 5.3 4.8 5.1 5.3 5.7 4.9 3.7
75 50 30 18 13 12 23 36 57 75

02.8 04.3 04.8 06.7 07.1 ✓ 07.6 07.1 06.3 06.4 07.2
9.7 8.2 7.7 5.8 5.4 4.68 4.9 5.4 6.2 6.1 5.3
75 50 30 18 13 12 24 40 54 75

TOP MH 52' RT

03.1 04.5 04.9 07.0 07.3 ✓ 07.8 07.6 06.5 06.3 07.0
9.4 8.0 7.6 5.5 5.2 4.6 4.7 4.9 6.0 6.2 5.5
75 48 28 17 13 12 18 30 54 75

03.4 04.5 04.5 07.2 07.6 ✓ 08.1 07.8 06.4 06.2 07.0
9.1 8.0 8.0 5.3 4.9 4.28 4.4 4.7 6.1 6.3 4.9
75 49 29 18 13 11 18 32 51 75

STA	+	π	-	ELEV.
-----	---	-------	---	-------

		912.48		
--	--	--------	--	--

131+50				
--------	--	--	--	--

+56				
-----	--	--	--	--

		7.70	904.78	
--	--	------	--------	--

132+00	5.35	913.87	3.96	908.52
--------	------	--------	------	--------

+50				
-----	--	--	--	--

133+00				
--------	--	--	--	--

+50	=	ENT RT		
-----	---	--------	--	--

KP
DS
RT
TJ

LT

19 MAR 76
RT

34.

03.9	04.5	04.0	07.3	07.9	08.38	08.2	08.0	05.9	06.0	07.5
8.6	8.0	8.5	5.2	4.6	4.1	4.3	4.5	6.7	6.5	5.0
75	50	31	18	12		12	18	33	61	75

TOP (FL) SD 37' RT

04.0	04.4	04.5	07.5	08.0	08.52	08.5	08.0	06.0	06.3	07.5
9.9	9.5	9.4	6.4	5.9	5.35	5.4	5.9	7.9	7.6	6.4
75	50	32	18	13		12	19	36	54	64

04.3	04.8	05.6	07.8	08.3	08.77	08.8	08.4	06.7	06.8	07.6
9.6	9.1	8.3	6.1	5.6	5.10	5.1	5.5	7.2	7.1	6.3
75	51	30	17	13		12	20	37	53	75

04.9	05.5	05.9	07.7	08.7	09.21	09.1	08.8	07.6	07.9	09.3
9.0	8.4	8.0	6.2	5.2	4.66	4.8	5.1	6.3	6.0	4.6
75	52	32	21	14		11	16	36	52	75

05.4	06.1	06.8	08.7	09.1	09.57	09.2	08.7	09.1	09.6
8.5	7.8	7.1	5.2	4.8	4.3	4.7	5.2	4.8	4.3
75	55	34	22	13		12	35	59	75

STA + π - ELEV.

913.87

133+56

5.04 908.83

134+00

+46

7.32 906.55

+50

135+00

+27 = $\neq$ ENT RT.

BM

6.97

915.78

5.02

908.85

908.81

KP
DS
RJ
TS

LT

E

19 MAR 76
RT

35.

TOP MH 55' RT

05.6	06.2	07.1	08.9	09.5	909.83	09.5	09.2	08.0	08.1	09.1	09.1
8.3	7.7	6.8	5.0	4.4	4.04	4.4	4.7	5.9	5.8	4.8	4.2
75	53	31	22	13		12	19	30	35	63	75

FL SD 37' RT

05.3	06.0	06.1	09.3	09.7	909.97	09.6	08.9	07.2	07.0	08.1
8.6	7.9	7.8	4.6	4.2	3.9	4.3	5.0	6.7	6.9	5.8
75	57	32	18	14		14	19	30	45	75

05.1	05.9	06.0	08.9	09.9	910.23	10.1	09.6	08.4	08.6	09.4	09.1
8.8	8.0	7.9	5.0	4.0	3.64	3.8	4.3	5.4	5.3	4.5	4.2
75	63	31	21	13		12	18	28	42	58	75

05.2	06.9	06.0	09.2	10.2	910.47	10.3	09.5	09.9	10.5
8.7	8.0	7.9	4.7	3.7	3.4	3.6	4.4	4.0	3.4
75	58	32	22	13		12	39	61	75

SPIKE IN PP LT STA 134+20

STA	+	π	-	ELEV
		915.78		
135+50				
+80			8.29	907.49
136+00				
+50				
137+00				
+37			18.38	897.40

KP
DS
RJ
TJ

LT

19 MAR 1976
RT

36.

05.1	05.4	05.9	09.5	10.3	10.58	10.3	09.8	07.4	07.7	09.6
10.7	10.4	9.9	6.3	5.5	5.2	5.5	6.0	8.4	8.1	6.2
75	57	33	21	12		13	20	35	51	75

TOP MH 52' RT

02.1	05.8	07.9	10.1	10.9	10.9	10.6	10.1	06.7	06.8	06.9
13.7	10.0	7.9	5.7	4.9	4.69	5.2	5.7	9.1	9.0	8.9
75	67	28	21	13		12	19	35	60	75

04.5	04.5	05.0	06.5	10.8	11.8	11.3	10.8	06.5	06.5	06.3
11.3	11.3	10.8	9.3	5.0	4.0	3.9	4.5	5.0	9.3	9.5
75	56	54	35	22	13		12	19	36	75

05.3	05.6	06.1	12.0	12.9	12.3	12.0	04.6	05.1
10.5	10.2	9.7	3.8	2.9	2.62	3.5	3.8	11.2
75	50	39	21	13		12	18	49

FL 48" RCP 56' RT

STA	+	π	-	ELEV
		915.78		
137+50				
TP	6.76	919.92	2.62	913.16
137+75				
138+00				
+50				
139+00				
BM	5.32	924.93	0.29	919.63 (919.61)

KP
DS
RT
JT

LT

E

19 MAR 1976
RT

37

06.1	06.2	08.7	14.0	14.4	14.78	14.2	13.5	06.8	9.9	9.6	9.1
9.7	9.6	7.1	1.8	1.4	1.0	1.6	2.3	9.0	15.9	18.2	13.9
75	59	34	19	14		14	20	41	52	58-61	75

Ditch

TOP PK E STA 137+00

07.1	07.1	10.9	14.6	15.0	15.42	14.8	14.2	07.9	9.1	9.1
12.8	12.2	9.0	5.3	4.9	4.5	5.1	5.7	12.0	20.8	22.8
75	54	32	19	13		13	20	49	70	75-78

DITCH

9.3	9.6	12.1	15.2	15.6	16.10	15.6	15.2	10.0	07.6	9.1
10.6	10.3	7.8	4.7	4.3	3.82	4.3	4.7	9.9	12.3	22.8
75	58	41	21	14		12	19	38	64	84-87

DITCH

16.8	16.5	15.4	15.8	15.9	17.02	16.5	16.1	11.1	10.1
3.1	3.4	4.5	4.1	4.0	2.9	3.4	3.8	8.8	9.8
75	60	56	38	20		12	19	38	75

20.4	19.6	19.9	17.2	16.9	17.63	16.8	16.2	12.9	11.2	11.2
40.5	0.3	1.0	2.7	3.0	2.29	3.1	3.7	7.1	8.7	8.7
75	62	56	37	24		14	21	39	63	75

SPIKE IN PP NW CORF & Centerville RD.

STA	+	π	-	ELEV.
-----	---	-------	---	-------

		924.93		
--	--	--------	--	--

139+25				
--------	--	--	--	--

+50				
-----	--	--	--	--

+68				
-----	--	--	--	--

			6.99	917.94
--	--	--	------	--------

+78	=	GUTTER	LT & RT	
-----	---	--------	---------	--

+98	=	E Centerville Rd.		
-----	---	-------------------	--	--

BM				
----	--	--	--	--

			5.32	
--	--	--	------	--

				919.61
--	--	--	--	--------

				919.61
--	--	--	--	--------

KP
DS
RJ
TJ

LT

LT

19 MAR 1976
LT

38

21.5 20.4 18.6 17.4 17.4 17.73 17.1 16.5 15.9 15.3 12.9
3.4 4.5 6.3 7.5 7.5 7.2 7.8 8.4 9.2 9.6 12.7
75 66 48 30 20 13 29 36 59 75

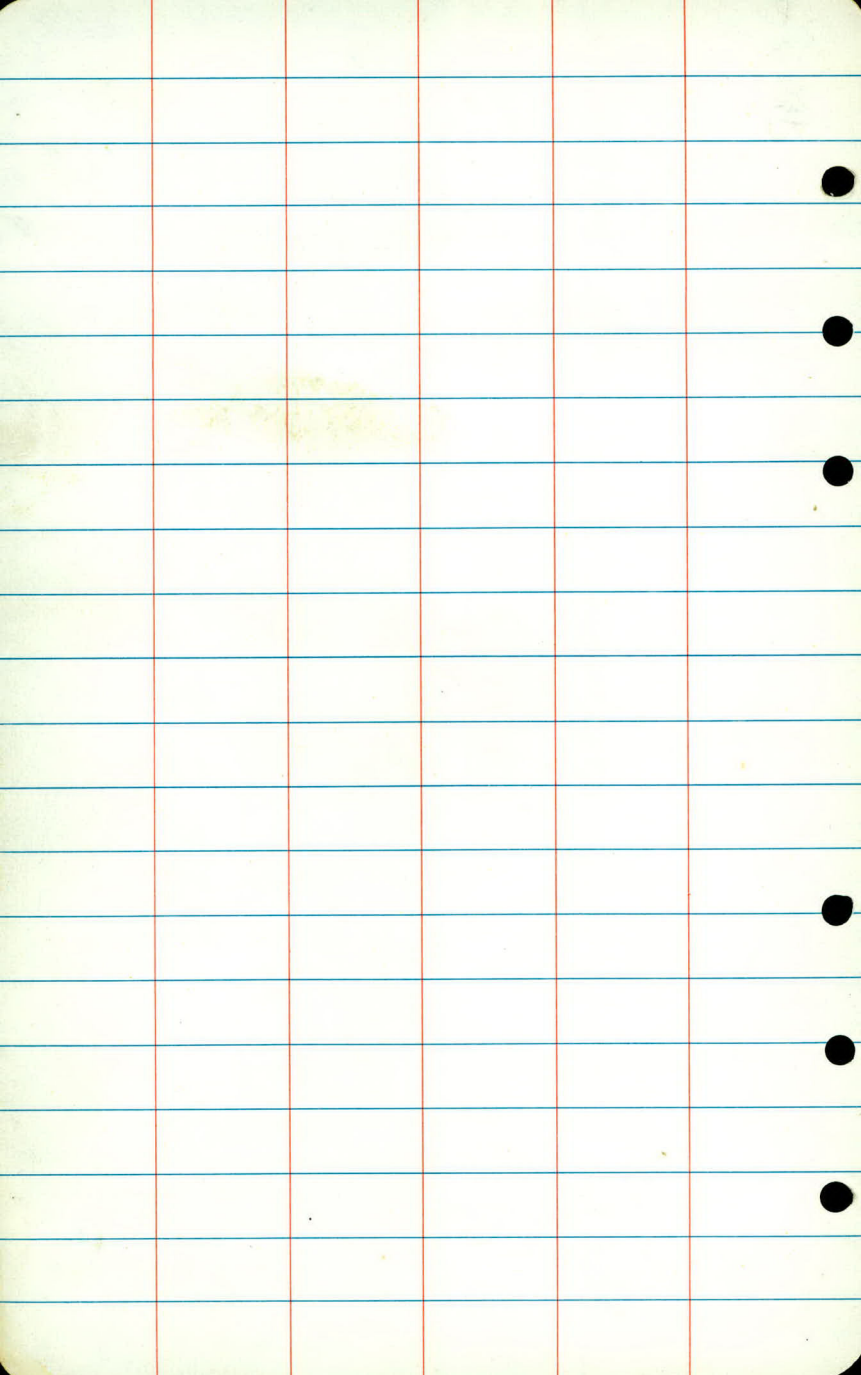
21.9 19.3 18.4 17.9 17.93 17.3 16.3 16.1 15.9 14.5
3.0 5.6 6.5 7.0 7.0 7.6 8.6 8.8 9.0 10.4
75 52 35 23 13 23 39 58 75

TOP TEL MH 22' LT

19.2 18.9 18.2 17.9 17.33 16.5 15.5 14.5
5.7 6.0 6.7 7.0 7.6 8.4 9.4 10.4
75 54 36 19 23 48 75

23.5 22.3 21.0 20.3 19.6 18.8 18.13 17.2 16.3 15.2 13.7 12.7
1.4 2.6 3.7 4.6 5.3 6.1 6.8 7.7 8.6 9.7 11.2 12.9
200 150 100 76 52 26 35 66 100 150 200

SPIKE IN PP NW COR F & Centerville RD.



KP
DS
RJ
TJ

22 MARCH 1976
SUNNY 35°

1.

Bench Check

STA

+

 π

BM

4.45

906.77

902.32

5.26

906.94

5.09

901.68

901.80

BM

6.24

906.96

6.24

900.70

900.72

5.00

907.49

4.47

902.49

902.56

4.95

902.54

902.68

BM

7.76

909.95

5.28

902.21

902.19

8.32

901.63

901.49

5.64

904.31

904.34

KP
DS
RU
TJ

22 MAR 1976

2

DESCRIPTION

TOP PK & STA 80+00

TOP PK & STA 86+00 ✓

SPIKE IN PP LT STA 87+30

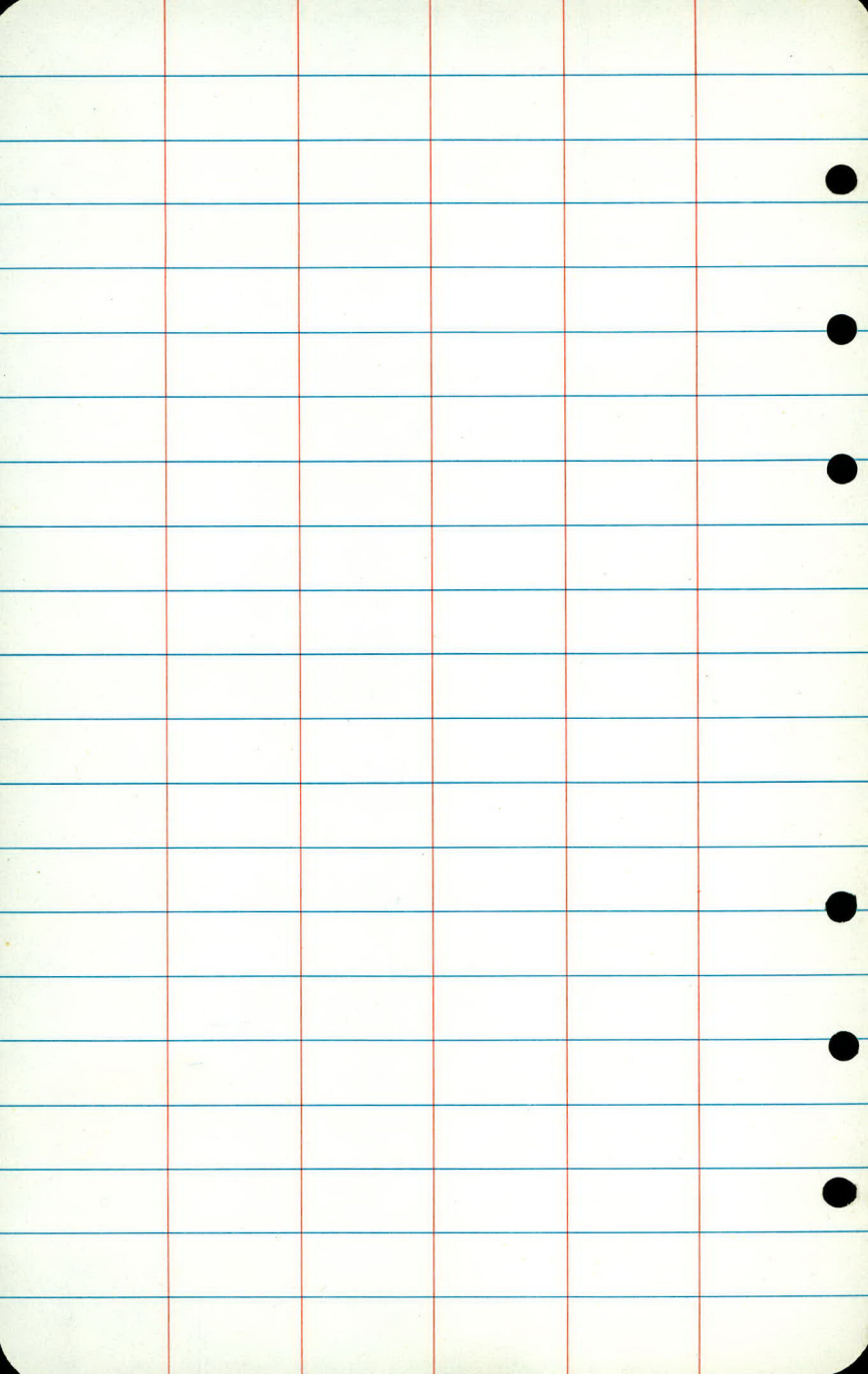
TOP PK & STA 89+00

TOP PK & STA 91+00

SPIKE IN PP LT STA 94+54

TOP MH 34' RT STA 95+65

SPIKE IN PP N.E. COR FF' CLOVER



24 MAR 1976

1.

KP
DS,
TJ

CO. RD F
McMenemy to Centerville Rd

± Profile grades

STA	+	π	-	ELEV.	87
BM	6.67	906.57			899.90
81+00			5.32	901.25	
82			5.15	901.42	
83			4.56	902.01	
84			4.42	902.15	
85			4.39	902.18	
87			4.52	902.05	
BM			4.97	901.60	901.68

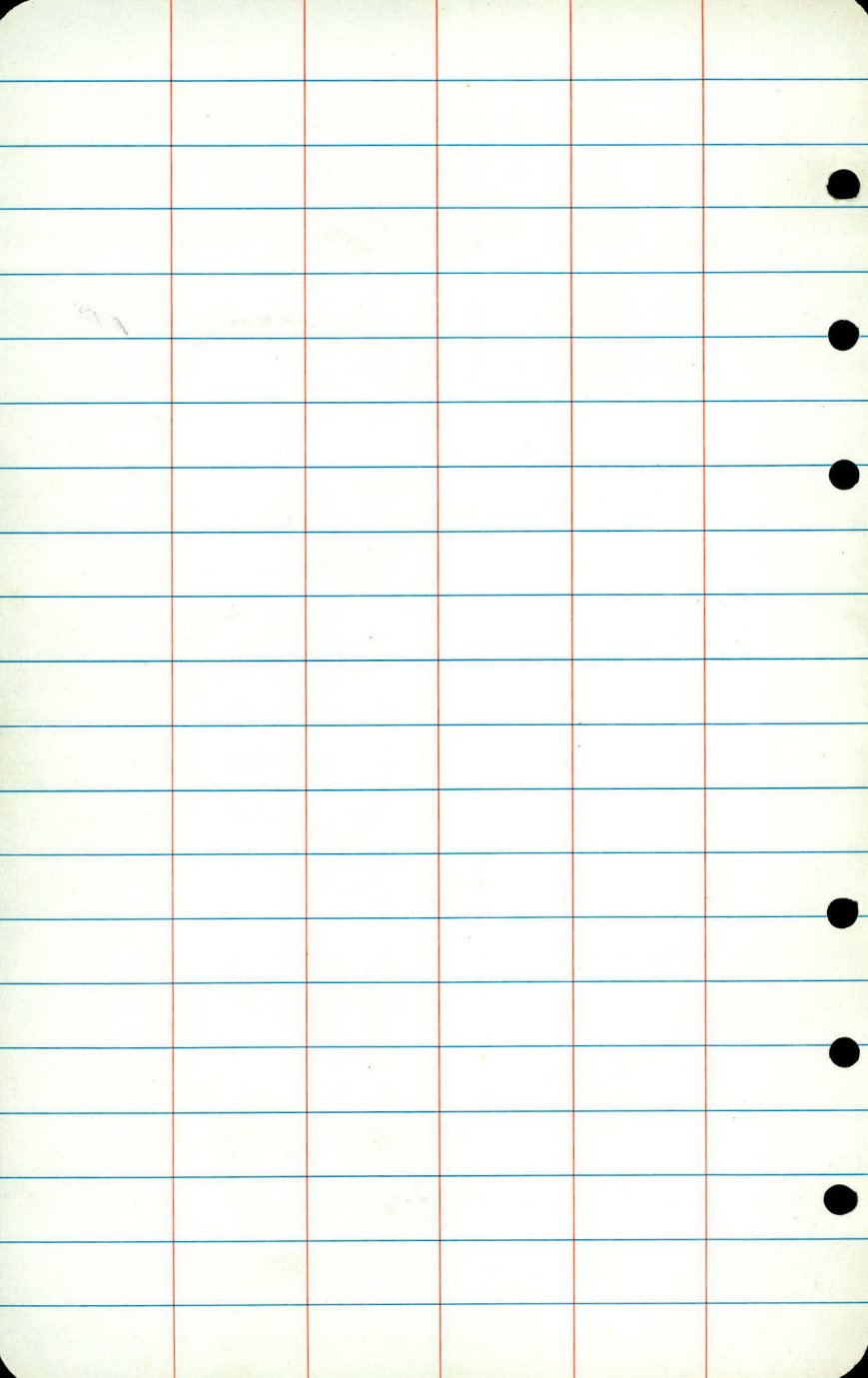
KP
DS
TJ

24 MAR 1976

2.

DESCRIPTION

TOP PK & STA 86+00



KP
WS
GA
RJ

19 MAY 1976
SUNNY 60°

Co. Rd F

McMENEMY TO CENTERVILLE RD

A22+1.

TOPOGRAPHY

+50

Lt

E

+58 $\frac{12"CM}{32}$ RT

+40 $\frac{12"CM}{32}$

114

+50

+37 $\frac{12" \times 18"CM}{28}$

+37 $\frac{12" \times 18"CM}{26}$

113

+50

+02 $\frac{12" \times 18"CM}{20}$

+02 $\frac{12" \times 18"CM}{20}$

1/2

Lt

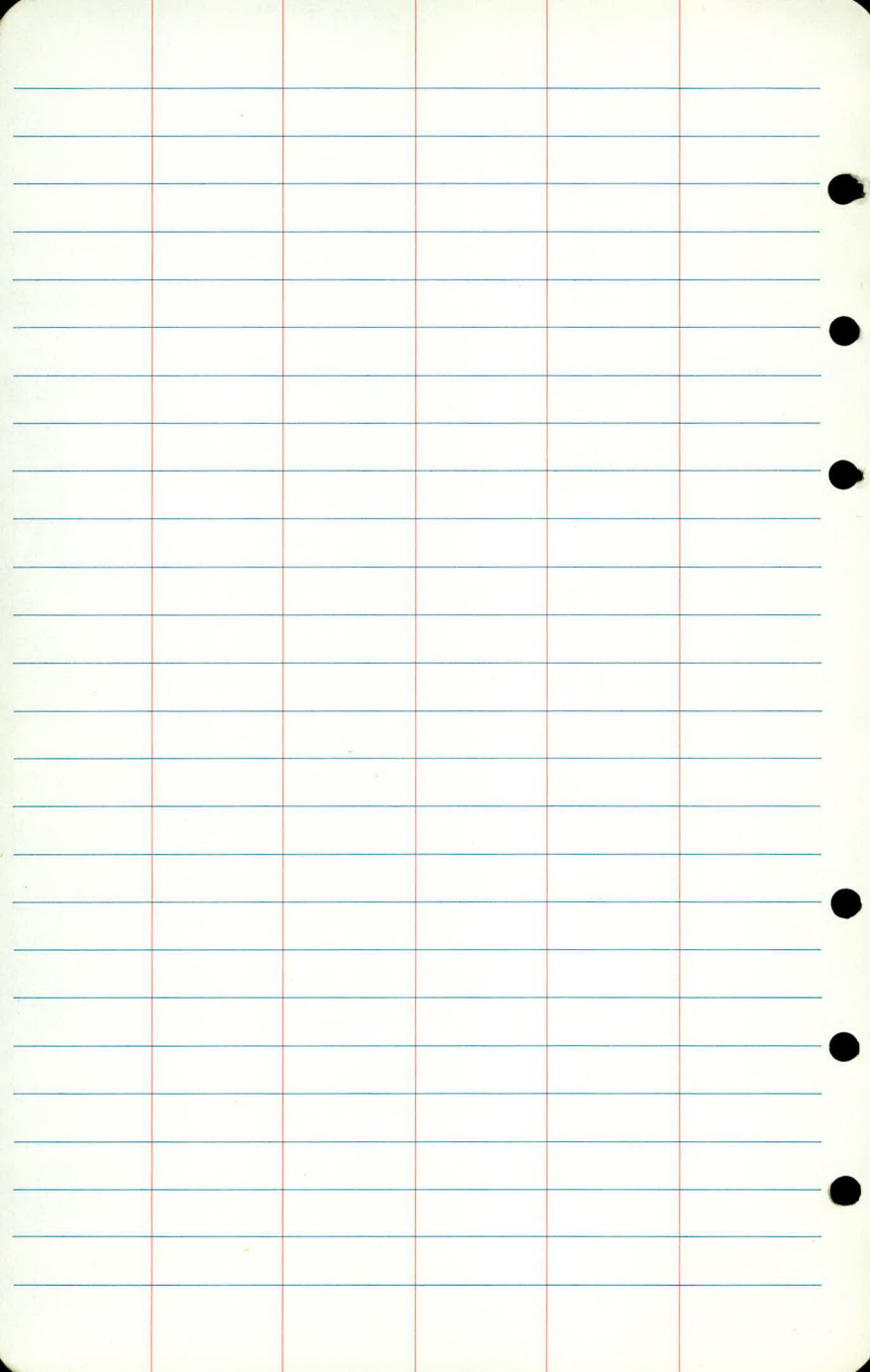
119 MAY 1976

Rt



OLDEST





KP
WS
GA
RD

19 MAY 1976 1.

CO. RD F

H₂O ELEVATIONS

STA	+	π	-	ELEV	
BM	4.16	902.83			(898.67)
BM			5.38	897.45	(897.47)
112+02			7.62	895.21	
112+02			6.81	896.02	
				892.70	
113+37			9.18	893.65	
				893.48	21
113+37			8.39	894.44	
114+40			7.92	894.91	
114+58			8.12	894.71	

LT

±

19 MAY 1976

2.

RT

SPIKE IN PP LT STA 113+50

TOP MAH 25.0 RT STA 113+91

FL 12" X 18" CM 20' RT

FL 12" X 18" CM 20' LT

24"

FL ~~12" X 18"~~ CM 26' RT

24"

FL ~~12" X 18"~~ CM 28' LT

FL W. END 12" CM 32' RT

FL E. END 12" CM 32' RT

STA	+	π	-	ELEV
		902.83		
113+35			6.98	895.85
112+98			6.71	895.12
BM	6.32	906.22		(899.90)
83+66			9.86	892.97
83+66			10.23	892.60
83+66			7.63	895.20
83+66			7.70	895.13
BM			4.13	902.09 (902.23)
BM			4.72	901.50 (901.68)
BM			4.89	901.33 (901.42)

LT

19 MAY 1976
E RT

3.

H2O RT STA 113+35

H2O LT

SPIKE IN PP LT STA 81+00

FL 24" CM 24.0 RT

FL 24" CM 24.0 LT

H2O LT

H2O RT

TOP PK E STA 84+00

TOP PK E STA 86+00

TOP PK E STA 82+00

