

OFFICE OF COUNTY ENGINEER
RAMSEY COUNTY, MINN.

PLAN Survey

LEXINGTON AVENUE
From S.T.H. 36 To Co. Rd. "C"

Road Acc't. No. 51

Date Filed _____

File _____

FK
GM
RR

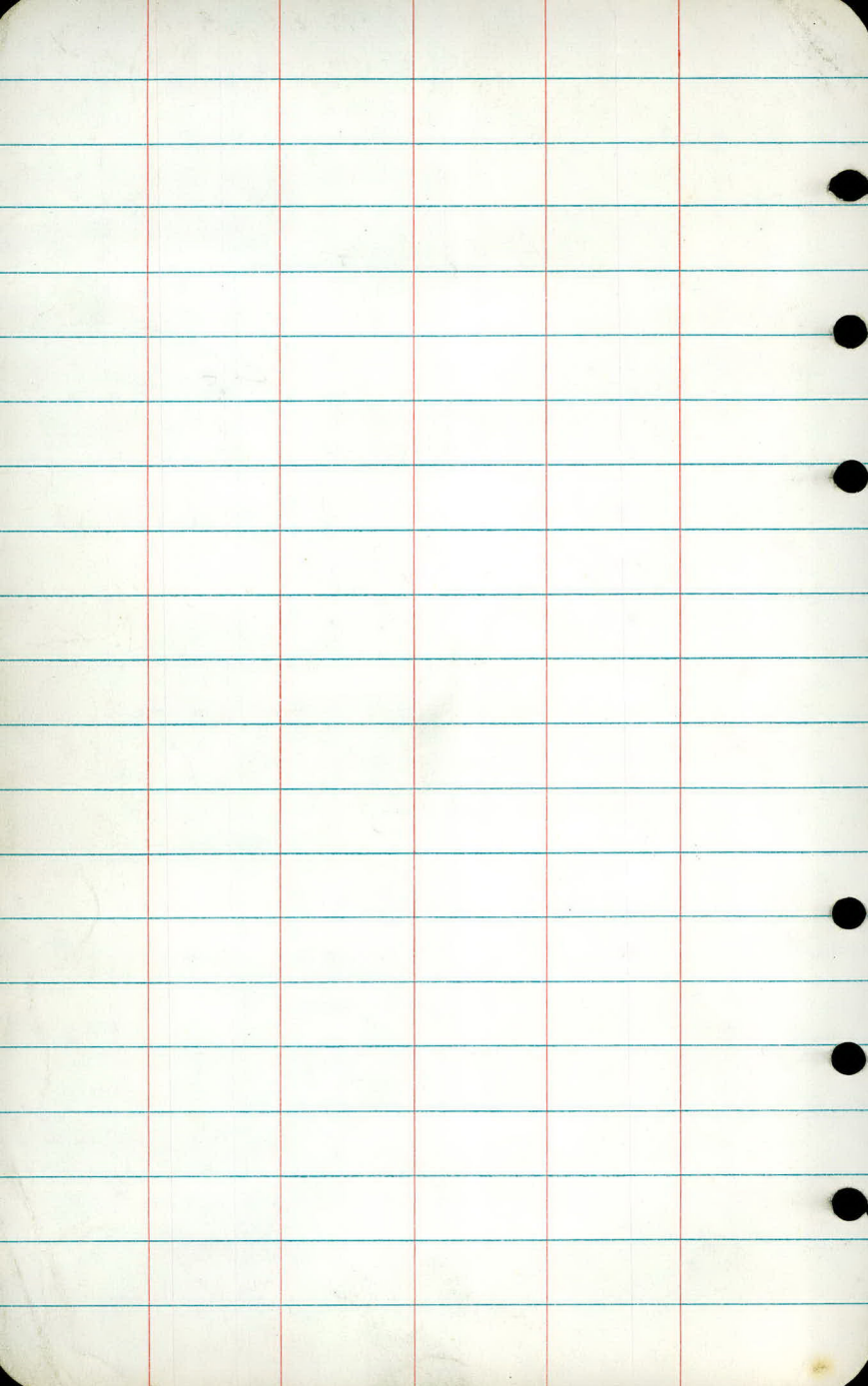
Oct. 26, 1971

1

LEXINGTON

TH #36 to "E"

PLAN SURVEY



FK
GM
RR

Oct. 26, 1971

2

Alinement

62-651-03 CTB

Sta Point ΔL_t ΔR_t

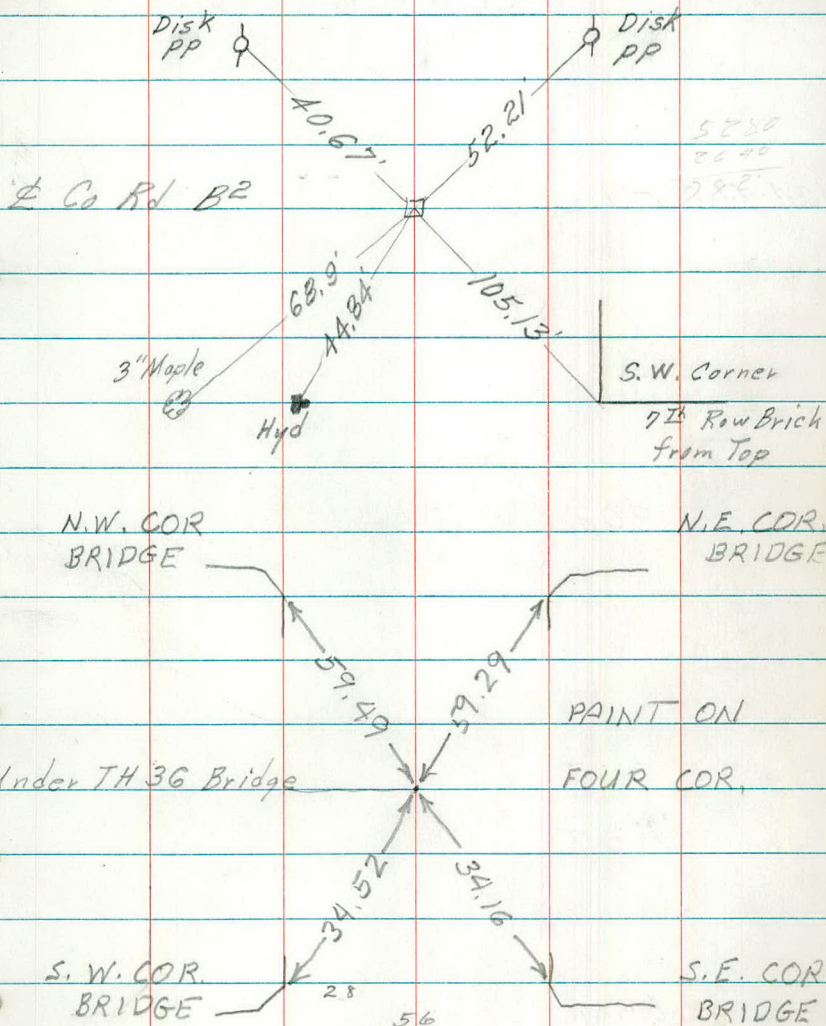
78+79.58 P.I.

67+00 P.O.T

FK
GM
RR

Oct. 26, 1971

3



Sta Point Δ Lt. Δ Rt.

104+60.06 P.I.

0°22' $\frac{1}{2}$ from Angle Sheet

103+22.37 P.O.T.

83+00 P.O.T.

FK
GN
RR

Oct. 26, 1971

4

HYD.

749.84

Section Corner

29.02

45.53

C. L. Man.

N.W. COR

HO # 2630

S.W. COR.

HO # 2630

60.10

ctr. CB
Cover

Cor CB at Curb

E Co Rd "C"

PK Nail

55.71

54.40

56.49

76.17

ctr. C.B.
Cover

Face
PP

N.E. COR
HO # 1115

N.W. COR
HO # 2438

88.23

95.40

84.23

52.52

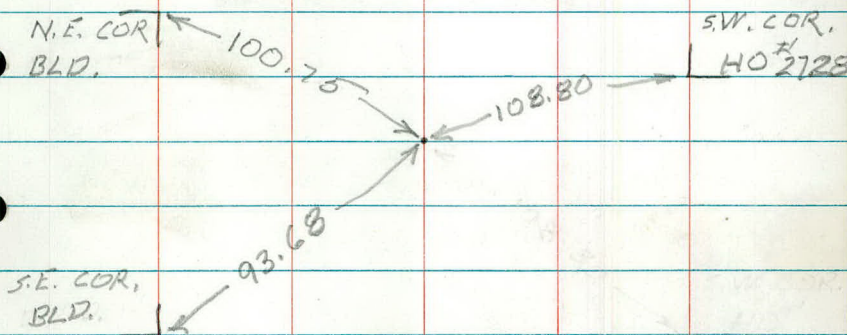
HYD.

N.W. COR
CONC. DR

Sta	Point	$\Delta Lt.$	$\Delta Rt.$
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113	POT		
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	POT		
--	-----	--	--



£ old "C"

Sta	Point	$\Delta Lt.$	$\Delta Rt.$
+98.37		$11^{\circ}21'45''$	
+50		$10^{\circ}45'28''$	
128		$10^{\circ}07'58''$	
+50		$9^{\circ}30'28''$	
127		$8^{\circ}52'58''$	
+50		$8^{\circ}15'28''$	
126		$7^{\circ}37'58''$	Measured $\Delta = 22^{\circ}43'25''$
+50		$7^{\circ}00'28''$	Used $\frac{1}{2} \Delta = 11^{\circ}21'45''$
125		$6^{\circ}22'58''$	Used $\Delta = 22^{\circ}43'30''$
+50		$5^{\circ}45'28''$	$D = 2^{\circ}30'$
24+49.92	P.I.		$T = 460.55'$
124		$5^{\circ}07'58''$	$L = 909.00'$
+50		$4^{\circ}30'28''$	$R = 2291.83'$
123		$3^{\circ}52'58''$	
+50		$3^{\circ}15'28''$	
122		$2^{\circ}37'58''$	
+50		$2^{\circ}00'28''$	
121		$1^{\circ}22'58''$	
+50		$0^{\circ}45'28''$	
120		$0^{\circ}07'58''$	
119+89.37	P.C.	$0^{\circ}00'$	

FK
LPD
GM
RR

Oct. 28, 1971

6

3 N
4° C. Elm

68.60
72.45

Spike in old
Road Bed

646.75
646.31
127.86

Hyd

No good ties

Found Iron pin

1107.3
460.55
646.75

12449.92
460.55
11989.37

12449.92
112+10.00
12+39.92

1239.29

460.55
646.75
1107.30
1106.30

Hyd

85.05

77.49
Sight

83.08 3 N
7" Elm

Sta Point Δ Lt Δ Rt

+03.41 P.T. $16^{\circ} 28'$

+50 $15^{\circ} 17.8'$

142 $13^{\circ} 32.8' \frac{1}{2} \Delta = 16^{\circ} 28'$

+50 $11^{\circ} 47.8' \Delta = 32^{\circ} 56'$

141 $10^{\circ} 02.8' D = 7^{\circ}$

140+54.87 P.I. $T = 241.94'$

+50 $8^{\circ} 17.8' L = 470.48'$

140 $6^{\circ} 32.8' R = 818.51'$

+50 $4^{\circ} 47.8'$

139 $3^{\circ} 02.8'$

+50 $1^{\circ} 17.8'$

138+12.93 P.C. $0^{\circ} 00'$

FK
LPD
GM
RR

Nov. 3, 1971

7

29558

52.30

Disk
R.P. 

Hyd 

120.16
59.53

3 N O
G.P.

110.32

85.77

Sign 

Iron

459.70

Sta Point Δ Lt. Δ Rt.

+99.51	P.T.	$10^{\circ}20'10''$	
+50		$9^{\circ}20'45''$	
156		$8^{\circ}20'45''$	
+50		$7^{\circ}20'45''$	$\frac{1}{2} \Delta = 10^{\circ}20'10''$
155		$6^{\circ}20'45''$	$\Delta = 20^{\circ}40'20''$
+50		$5^{\circ}20'45''$	$D = 4^{\circ}$
154+43.95	P.I.		$T = 261.24'$
154		$4^{\circ}20'45''$	$L = 516.80'$
+50		$3^{\circ}20'45''$	$R = 1432.39'$
153		$2^{\circ}20'45''$	
+50		$1^{\circ}20'45''$	
152		$0^{\circ}20'45''$	
151+82.71	P.C.	$0^{\circ}00'$	

PK
LPD
GM
RR

Nov. 3, 1971

8

PK nail
in Conc
slab  Disk
46.39
Disk
22" Elm 
44.46
28.94
49.02
71.64
Hyd. 

PK nail
in Curb

P.K. nail

73.12  Disk
Quad Maple

Sta Point Δ Lt. Δ Rt.+79.50 P.T. $15^{\circ} 22' 30''$ +50 $14^{\circ} 29.4'$ 163 $12^{\circ} 59.4'$ M $30' 44' 45''$ +50 $11^{\circ} 29.4'$ $\frac{1}{2}\Delta = 15^{\circ} 22' 30''$ 162 $9^{\circ} 59.4'$ $\Delta = 30^{\circ} 45'$ +50 $8^{\circ} 29.4'$ $D = 6^{\circ}$

161+29.58 P.I.

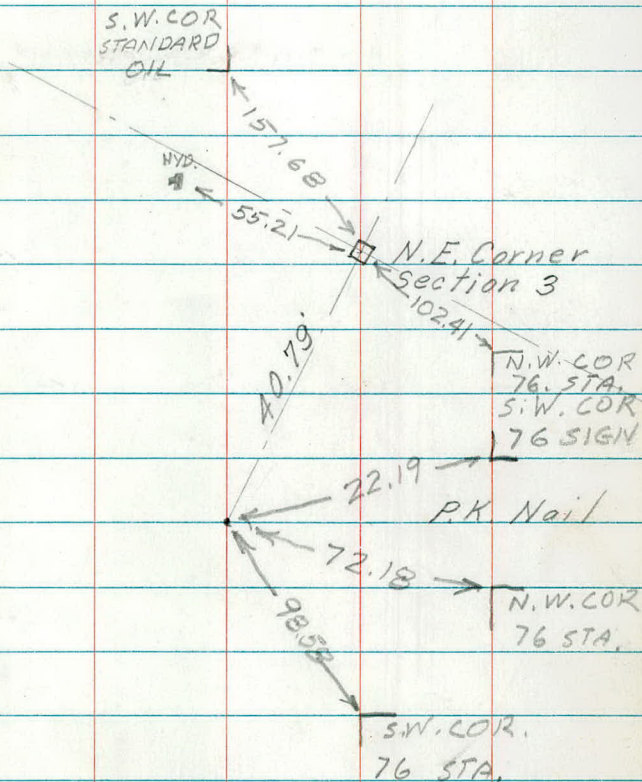
 $T = 262.58'$ 161 $6^{\circ} 59.4'$ $L = 512.50'$ +50 $5^{\circ} 29.4'$ $R = 954.93'$ 160 $3^{\circ} 59.4'$ +50 $2^{\circ} 29.4'$ 159 $0^{\circ} 59.4'$ 158+67.00 P.C. $0^{\circ} 00'$

$$\begin{array}{r}
 359 \ 5960 \\
 95 \ 1648 \\
 \hline
 264 \ 4312
 \end{array}$$

FK
LPD
GM
RR

Nov. 3, 1971

9



359 5960
10 4628
349 1332

Sta Point ΔL_t ΔR_t

187+93.36 P.I.

$0^{\circ}00'40''$

177+30.21 P.O.T.

171+00 P.O.T.

Lee O'ing D^r

~~mm~~

Dist

✓

Mat to

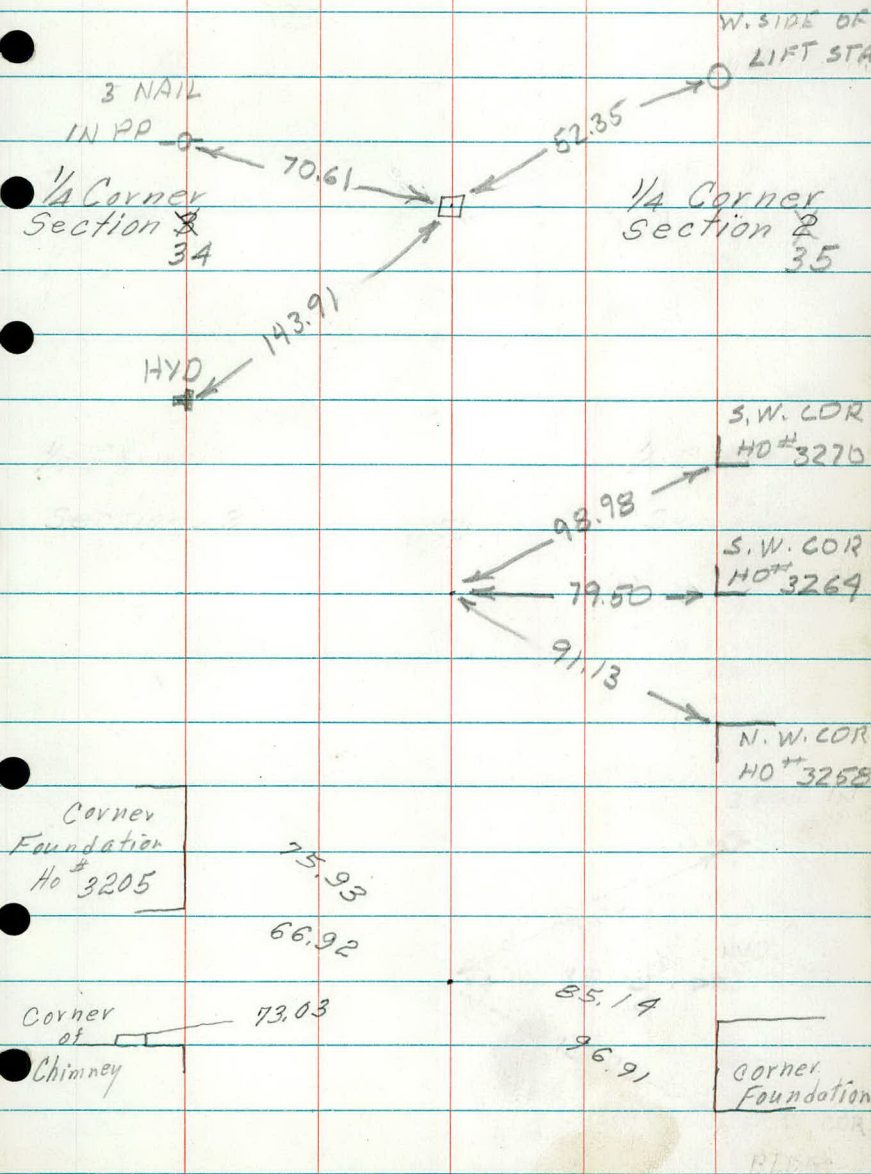
P. 1.

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FK
GM
RR

Nov. 4, 1971

10



Sta Point Δ Lt. Δ Rt.

214+28.53 P.I. $0^{\circ}09'45''$

211+00 POT

FR
GM
RR

Nov. 8, 1971

11

S.W. COR

R.C. ASP. PLT.

93.07

Co. Rd. "E"

Monument

3 NAIL
IN PP

77.70

63.64

HYD

3 NAIL IN
PP

56.59

HYD

38.39

109.52

3 NAIL IN
PP

Sta	Point	ΔL	ΔR
-----	-------	------------	------------

240+69.31			
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		0°06'30"	
--	--	----------	--

	POT		
--	-----	--	--

KP
DS
LPD
DK
PH

1 DEC. 1971
CLOUDY 15° 17

TOPOGRAPHY

LEXINGTON AVE.

T.H. 36 TO CO. RD E +

+50	LT FE 51	Curb 35	MEDIAN 2 2	RT +43 SD 31 26
+22 BR 28				+46 Arc Lite Pole 32
+10 PP 39				+40 Cor Island 79
				+10 Cor Island 31

69 FE 42	Curb 28	MEDIAN 2 2	POR 59
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+61 POR 34	+61 FE 49
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+15 Arc Lite Pole
36

+20 BR
26

68 FE 37	Curb 27	MEDIAN 2 2	Curb 27	FE 37
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+91 PP
31

+57 FE
36

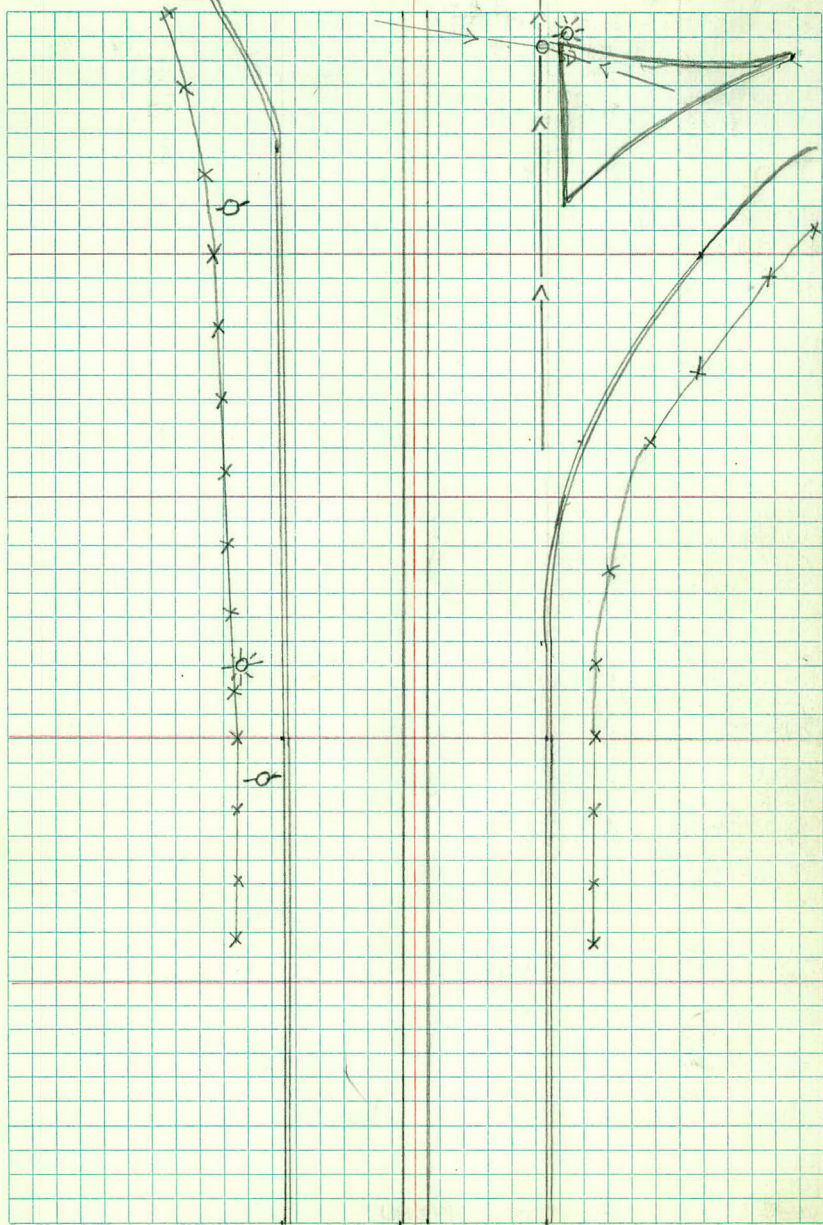
+57 FE
36

67	Curb 27	MEDIAN 2 2	Curb 27
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1 DEC, 1971

RT

18



72

LT

RD

RD

R7

+98 S. END 18" CM

23

23

+84 NW Corbs

106

+96 FE +96 FELOR

61-71

71

+61 END MED.

2 2

+63 Life

68

+60 50

32

+60 PP

37

+55 8" M ✓

72

+50

+30 8" M ✓

72

+31 ER ✓

28

+22 SW Corbs

107

+26 Arc life Pole

+17 BEGIN MED.

2 2

+20 HVD

40

+20 CB 39

30

+15 18" EL

40

71

POR ✓

39

ENT

+95 END SUB

36

+87 END MEDIAN

2 2

+92 10" ELMS ✓

54-66-

+61 MH ✓

59

+63 POR ✓

80

+63 Cor Is ✓

32

+52 SW Corbs

109

+50 12" EL ✓

41

+31 12" EL ✓

41

+22 FE ✓

60-E

+34 Cor Is ✓

83

+27 PP ✓

37

+20 6" Pinc ✓

48

+13 PP ✓

38

+26 11" RES ✓

45-E

+05 CB

78

+04 SD ✓

47

70 POR

Corb

Sub

ER

35

+84 POR ✓

80

49

+84 Cor Is.

32

+84 FE 57

76

+75 BR ✓

58

+89 POR ✓

38

+75 CB

53

+63 POR ✓

42

+63 RAMP

+50

FE

51

Sub

35

MEDIAN

2 2

36

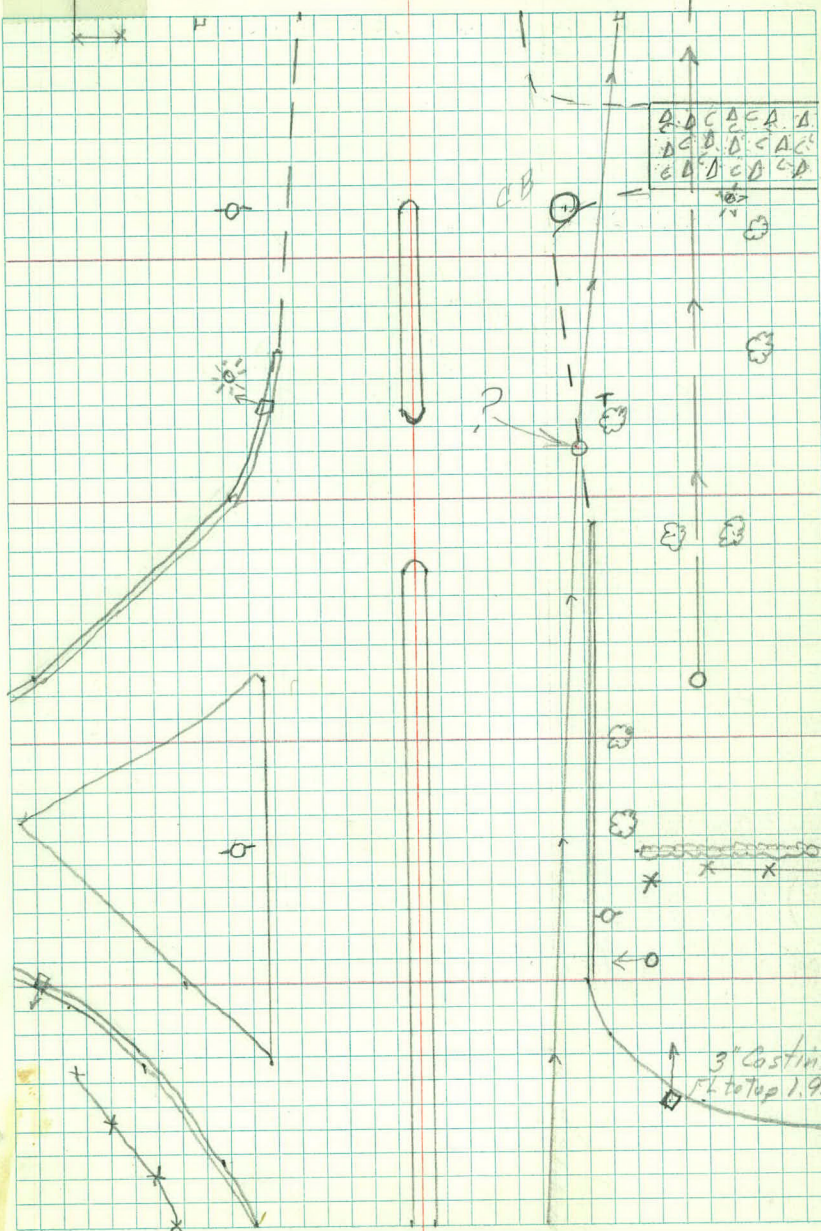
1 DEC. 1971

LT

F

RT

19



+50 FE LT PP
75 29

ROAD
12 12

RT

+39 PP
56

+32 END WOODS

39-75

+93 Apron
48

74 FE +00 W. END 24" SCP ROAD
75 36 14 14

+00 E. END 24" SCP
39

+55 WOODS
59

+50 FE
75

ROAD
16 17

+41 10" COTT
58

+48 10" COTT
59

+18 12" Willow
61

+16 PP
57

73 FE
73

ROAD
14 19

+80 W. END 18" CMT
24

+96 MH

+92 E. END 12" CMT
51

+96 PP
32

+70 N. END 30" RCP
56

+62 MH
60

+91 MH
31

+50 FE
70

ROAD
20 21

+52 MH
53

+23 N. END 18" CMT
44

+35 MH
60

+09 PP
57

72 FE
70

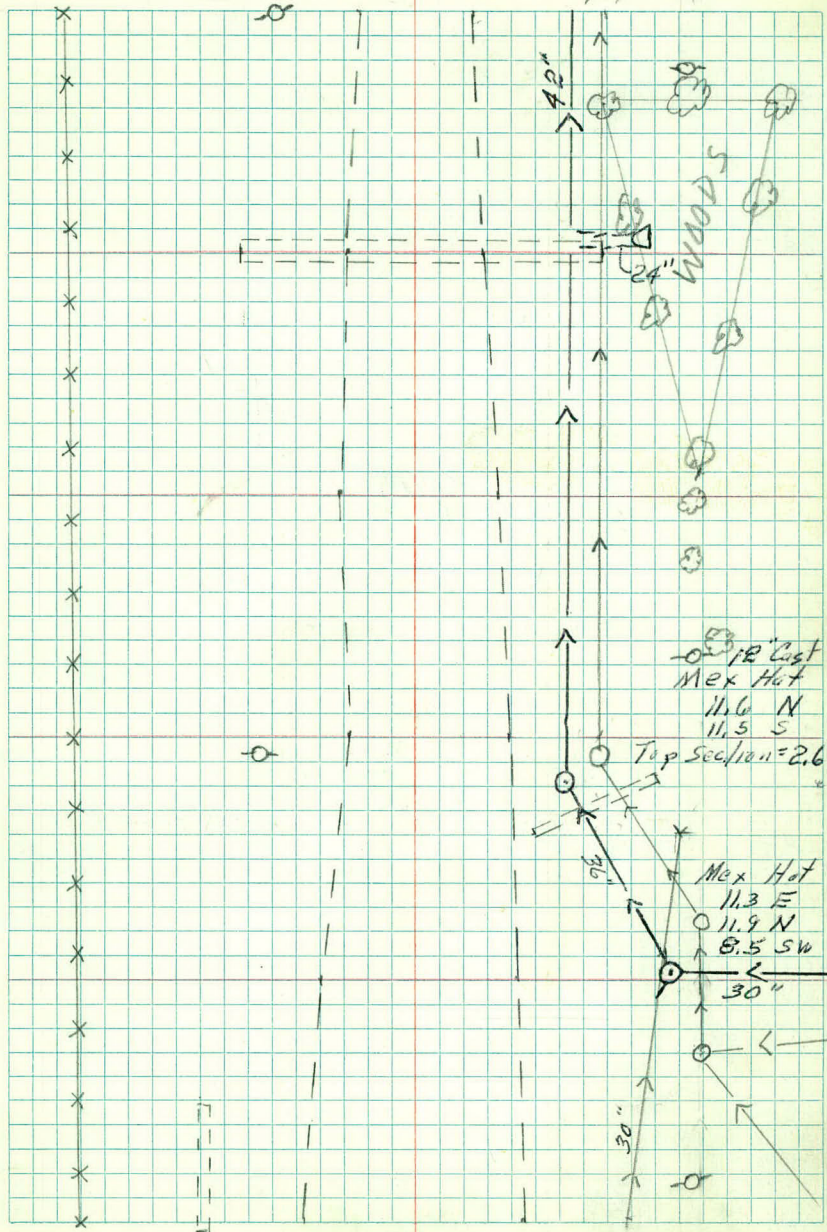
RD RD
23 23

FK
GF
RC

LT

1 DEC. 1971
Nov 23, 1972
RT

20



77

LT
FE
64E
ROAD
11 13

RT

+50

FE
67ROAD
11 13

76

FE
74+03 PD
28ROAD
11 13

+11 8" TW COTT ✓

+08 8" BE
63+04 10" BE
72+98 6" ELM
62+93 15" ELM
63+97 16" ELM
65

+68 E GRANDVIEW

+60 MH ✓
39+55 MH
32

+50

FE
74ROAD
12 12+88 HYD
46

+47 WOODS

+47 MH
46+35 SD
20+35 MH
35+34 WOODS
57+15 20" OAK
29+23 WOODS ✓
55

75

FE
75ROAD
12 12

+75 4" COTT ✓

+72 6" COTT
54

+50

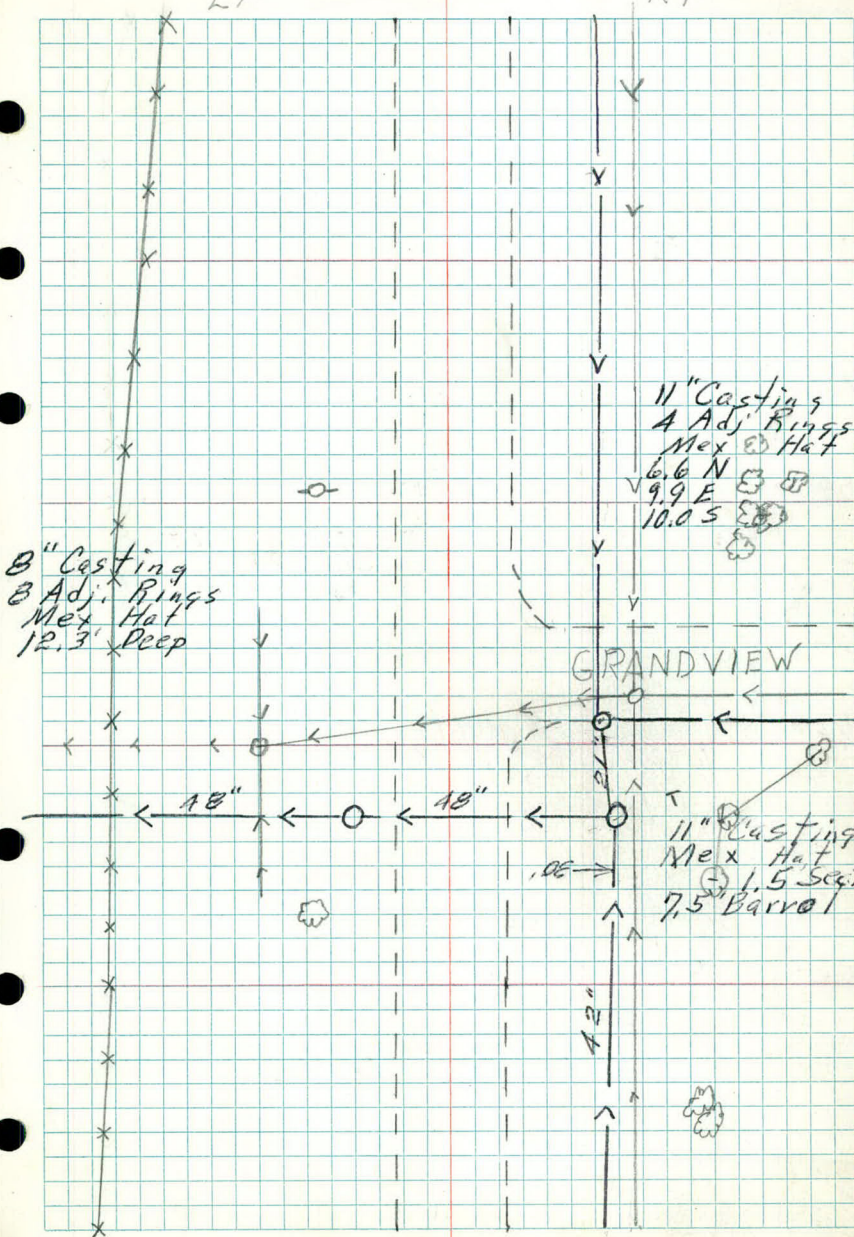
ROAD
12 12

1 DEC. 1971

21

LT

RT



+50

LT

£

RT

+40 $\frac{1" P}{51}$ +36 $\frac{3" MA}{60}$

+25 $\frac{51}{51}$

+19 $\frac{CB}{25}$

+15 $\frac{PP}{28}$

+13 $\frac{CB}{24}$

+03 MH

38

+17 N.END 12" CM

25

+12 N.END 12" CM

+08 $\frac{PP}{25}$

+07 Guy Wire

79

+10 $\frac{PP}{28}$

+97 $\frac{CB}{75}$

+79 £ B2

+07 31

+65 $\frac{MH}{74}$

+79 MH

+65 $\frac{MH}{21}$

+65 $\frac{CB}{73}$

+62 $\frac{CB}{74}$

+56 $\frac{MH}{44}$

+50

+45 $\frac{HYD}{29}$

+38 $\frac{5" F.R.}{44}$

+41 $\frac{24" E}{63}$ +43 $\frac{10" BE}{45}$

+34 $\frac{15" BE}{45}$ +36 $\frac{22" EV}{56}$

+23 $\frac{CH}{64}$ +24 $\frac{20" E}{59}$

+34 S.END 12" CM

26

+17 20" BE

+18 $\frac{24" E}{59}$

+22 $\frac{21" BE}{39}$

+14 N.END 12" CM

25

78

ROAD

SW COR 46

66

+77 WALL

+92 12" OAK

18 18

+79 N.END 12" CM

56

+87 END HEDGE

47

+76 13" BMV

+66 £ ENT

+76 8" ELM

+76 10" ELM

76

56

+50 18" ELM S.END 12" CM

59

23

+28 Begin Hedge

+39 PP

+17 4" PIPE

30

+19 S.END 12" CM

59

+47 END FE

59

+42 PP

48

+17 SIP

47

+17 SIP

56

77

FE

ROAD

11 13

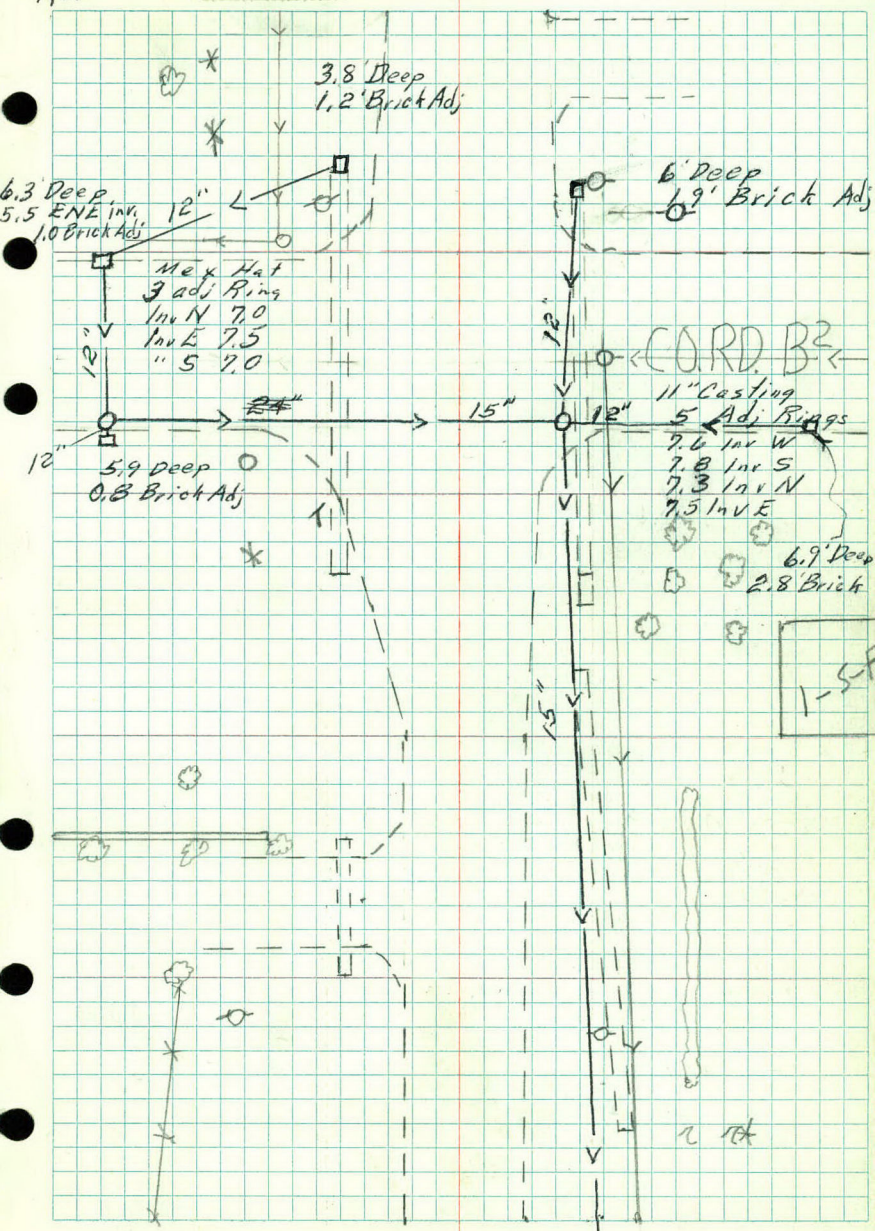
64

EK
RC
GF
RW

LT

1 DEC. 1971
Nov. 23, 1972 RT

22



82

LT

ROAD
11 13

ART

$$\begin{array}{r} +184 \text{ PP} \\ 28 \\ \hline +170 \text{ 1"} \text{P} \\ 52 \end{array}$$

$$\begin{array}{r} +93 \text{ PP} \\ 29 \\ \hline +72 \text{ NW Cor Ho} \\ 103 \\ \hline +53 \text{ MHV} \\ 36 \end{array}$$

+50

ROAD
11 13
$$\begin{array}{r} +48 \text{ N.E. Cor Ho} \\ 106 + 36 \text{ 1"} \text{PV} \\ 56 \\ \hline +29 \text{ 1"} \text{P} \\ 52 \end{array}$$

$$\begin{array}{r} +42 \text{ LITE} \\ 50 \\ \hline +07 \text{ 5"} \text{M} \\ 75 \end{array}$$

$$\begin{array}{r} +20 \text{ 1"} \text{P} \\ 57 \\ \hline +02 \text{ 2"} \text{P} \\ 59 \\ \hline +04 \text{ 8"} \text{P} \\ 74 \end{array}$$

$$\begin{array}{r} +34 \text{ MH} \\ 53 \\ \hline +12 \text{ 2"} \text{P} \\ 53 \end{array}$$

$$\begin{array}{r} +12 \text{ SE Cor Ho} \\ 100 \end{array}$$

$$\begin{array}{r} +02 \text{ SW Cor Ho} \\ 103 \end{array}$$

ROAD

$$\begin{array}{r} +75 \text{ 10"} \text{MH} \\ 59 \\ \hline +93 \text{ 8"} \text{P} \\ 73 \end{array}$$

$$\begin{array}{r} +92 \text{ 7"} \text{PV} \\ 71 \\ \hline +69 \text{ N.E. Cor Ho} \\ 100 \end{array}$$
ROAD
11 13

+91 E ENT.

$$\begin{array}{r} +64 \text{ Bush} \\ 51 \end{array}$$

$$\begin{array}{r} +73 \text{ 8"} \text{P} \\ 38 \\ \hline +74 \text{ 8"} \text{P} \\ 55 \\ \hline +59 \text{ 20"} \text{ELM} \\ 59 \end{array}$$

+50

ROAD

$$\begin{array}{r} +33 \text{ SE Cor Ho} \\ 105 \\ \hline +27 \text{ 10"} \text{E} \\ 59 \end{array}$$

$$\begin{array}{r} +38 \text{ PP} \\ 28 \\ \hline +36 \text{ Bush} \\ 51 \end{array}$$

$$\begin{array}{r} +26 \text{ N.END 12"} \text{CM} \\ 23 \end{array}$$

+16 E ENT.

$$\begin{array}{r} +37 \text{ PP} \\ 29 \\ \hline +39 \text{ 4"} \text{Pine} \\ 48 \end{array}$$

$$\begin{array}{r} +19 \text{ 8"} \text{Pine} \\ 39 \\ \hline +03 \text{ 4"} \text{Pine} \\ 50 \end{array}$$

$$\begin{array}{r} +04 \text{ 8"} \text{Pine} \\ 75 \end{array}$$

$$\begin{array}{r} +94 \text{ 1"} \text{Pine} \\ 51 \\ \hline +98 \text{ 3"} \text{Pine} \\ 57 \\ \hline +96 \text{ S.END 12"} \text{CM} \\ 23 \end{array}$$
ROAD
11 13
$$\begin{array}{r} +89 \text{ 3"} \text{MA} \\ 60 \\ \hline +81 \text{ 1"} \text{Pine} \\ 51 \\ \hline +67 \text{ 1"} \text{Pine} \\ 51 \\ \hline +52 \text{ 1"} \text{Pine} \\ 51 \end{array}$$

$$\begin{array}{r} +73 \text{ 5"} \text{Pine} \\ 52 \\ \hline +65 \text{ 9"} \text{Pine} \\ 58 \\ \hline +60 \text{ 8"} \text{Pine} \\ 42 \end{array}$$

$$\begin{array}{r} +79 \text{ 12"} \text{Pine} \\ 42 \end{array}$$

+50

ROAD
11 13

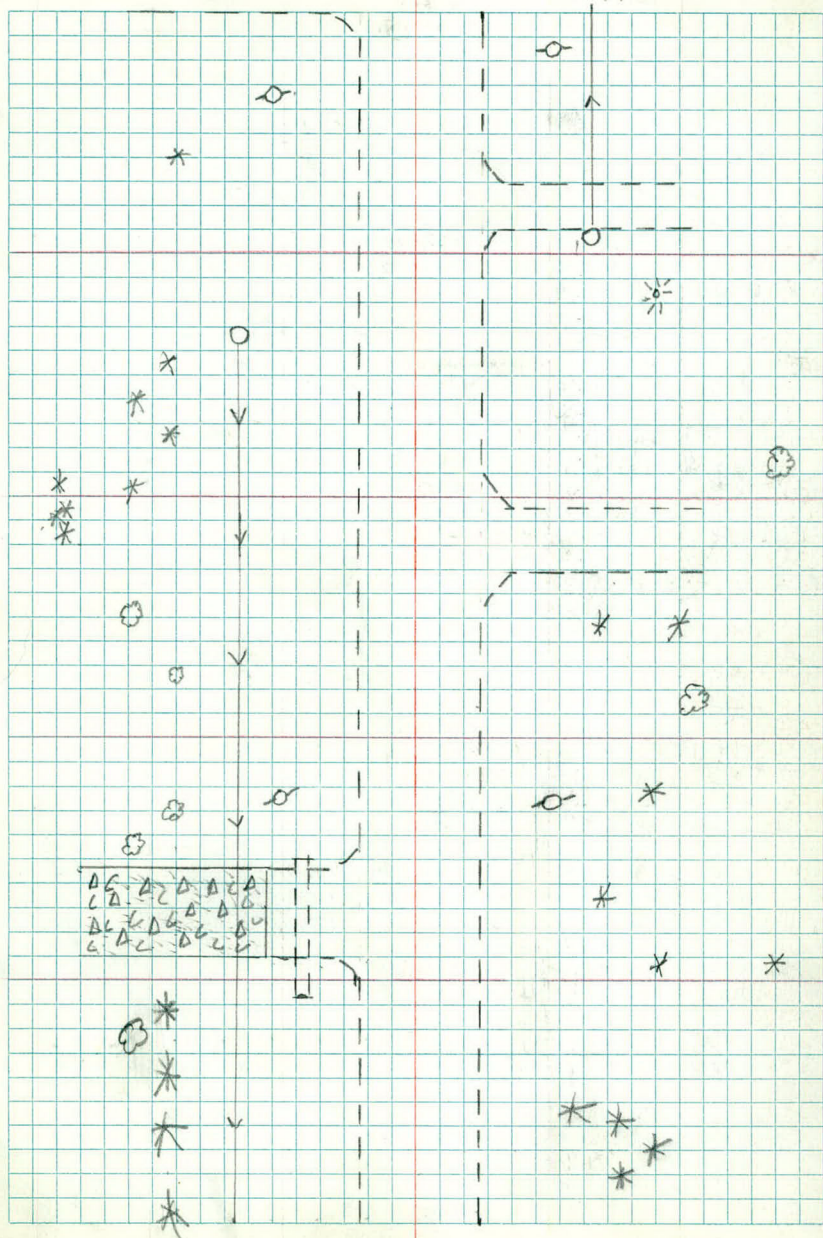
1 DEC. 1971

23

LT

E

R₇



+50 LT

ROAD
11 13

RT.

+44 PP
28

+33 SW COR HO

+28 12° E

+19 1" P

+21 PP

54 CK-7 34° BEV

34

+95 8" E

+86 5" LOCUST

+94 NW N +77 SW COR HO

+83 3" LOCUST

+81 8" LOCUST

+75 20° BEV

+68 10" E

74 +66 5" E

+51 ENT.

+50

ROAD
11 13

+24 8" COR

+14 2" M

+05 3" M

+18 PP

+08 NE COR HO

+93 2" M

+24 BUSH

+13 22° E

83

+84 3" M

+84 SE COR HO

+81 1" P

+86 NW N +74 2" M

+8 3 10° D

+67 2" M

+69 13 54

+69 ENT.

+67 SW COR HO

+54 4 11" M

+63 1" MV

+59 24° BE

+50 50 +51 3" M

ROAD
11 13

+35 1" M

+44 2" M

+34 1" M

+34 HYP

+13 ENT. SEXTANT

+18 5° E

82

ROAD
11 13

87

LT E ENT

ROAD

11 13

RT

FE

49

+64 S. COR HO
91+60 FE COR
49+56 12" COTT
76

+50

ROAD

11 13

+31 E ENT

+41 NW COR HO
88

86

ROAD

11 13

+99 8" COTT
64

+67 9" ASH

+47 3" P

+82 PP
28+63 NW COR HO
85+92 SW COR HO
88+63 3" P
45

+50

HYD

52

ROAD

11 13

+48 5" ASH

+42 N. END 15" CM
24

+23 Trip Birch

+05 SW COR HO

+24 MH
38

+24 E TRANSIT

+28 N. END 15" CM

+03 S. END 15" CM
24

+11 E ENT

+02 HEDGE

85

ROAD

11 13

S. END 15" CM
24

+10 MH

37 + 89 NW COR HO

+77 E ENT

90

+51 18" COTT

+50

75

ROAD

11 13

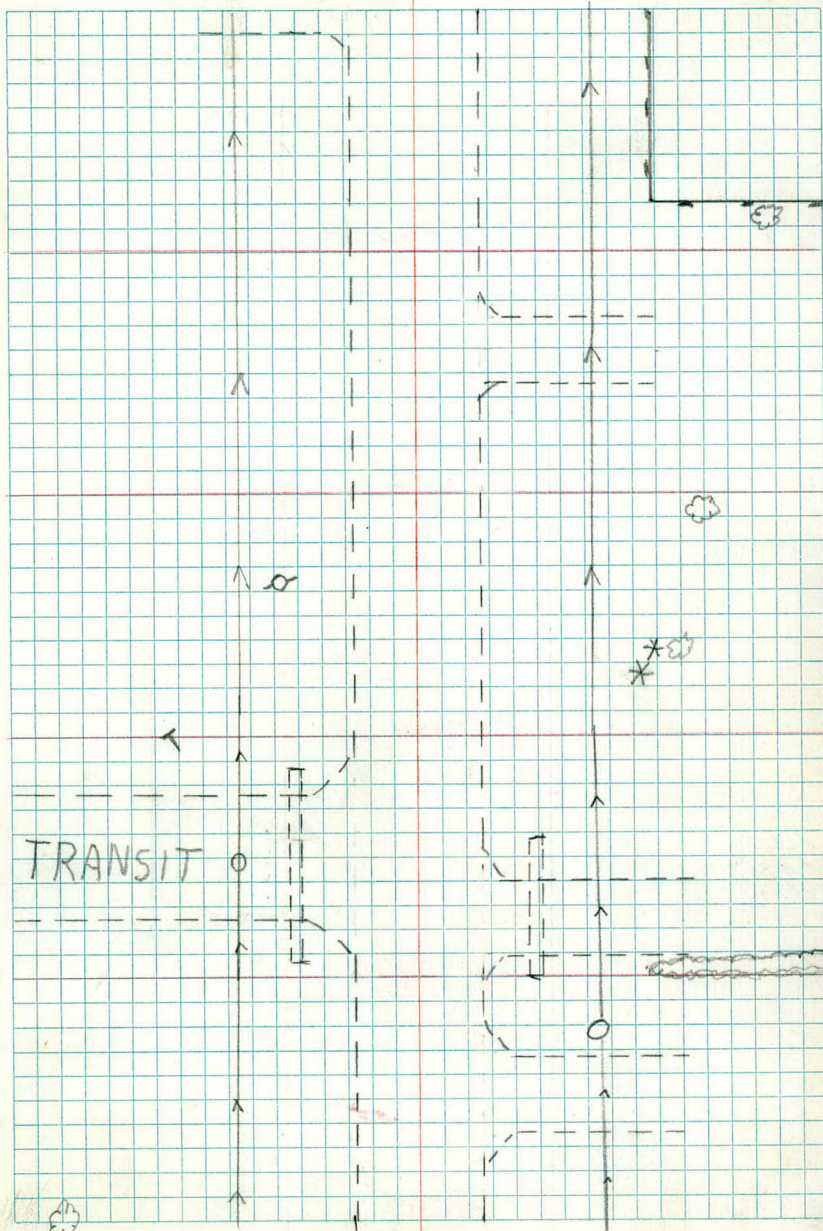
2 DEC. 1971

25

LT

E

RT



+50

LT

ROAD

RT

+46 5" COTT +36 12" COTT
54 52

+29 10" COTT

+44
+07 12" COTT
44+17 4 18" COTT
50+01 7" COTT
66

89

ROAD

+98 8" COTT +83 5" COTT
62 69+88 8" COTT
66+70 N. END 15" CM
33+73 HYD
52

+50

ROAD

+46 MH
37

+46 & BROOKS

+46 MH
37+24 PP
28+22 S. END 15" CM
27+18 END FE
50-57

88

ROAD

11 13 +79 10" POP
51 +78 NW COR HO
+36 8" POP
+64 10" POP +70 6" POP 81
51 +95 FE COR 51
+60 SW COR HO
80+51 2" P +57 4" POP
52 51

+50

ROAD

11 13 +45 2" P +39 2" P 49
53 53+14 N.E. COR HO
91+25 2" P +31 2" P
55 53+19 PP
28+12 2" P +19 2" P
64 58

87

ROAD

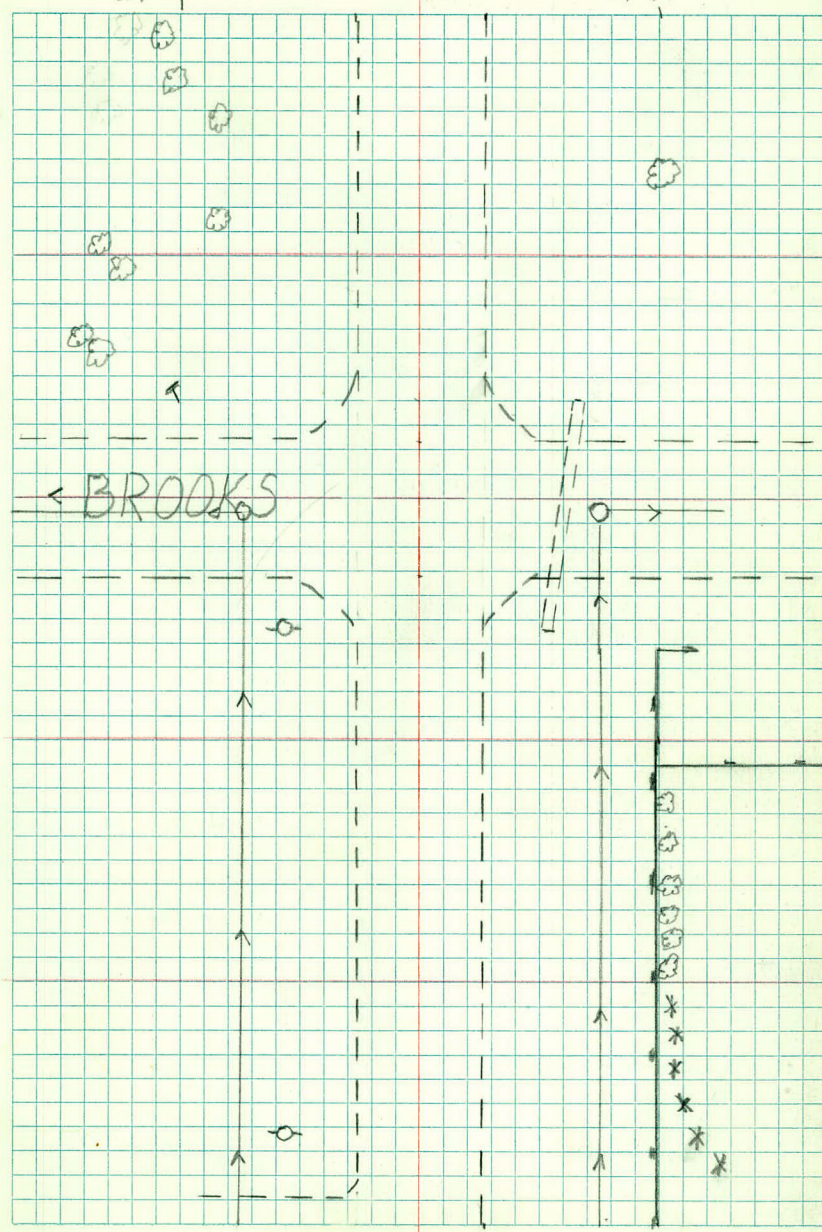
11 13

FE
49

LT

E

RT



92

LT

ROAD

11 13

RT

+96 PIPE LINE
31

+50 +47 PIPE LINE ROAD

31

11 13

+43 PIPE LINE
30

+39 PIPE LINE
36

+29 10-14" COTT

+15 MH
37

+135 PP
28

+34 PIPE LINE
38

91

ROAD

11 12

+89 14" COTT +91 9" COTT

59

+85 10" TW COTT

+71 8" COTT
56

54

+50

ROAD

11 12

+48 10" COTT
62

+41 12" COTT
56

+27 14" COTT
59

+24 MH

38

+34 BRUSH
38

+09 10" COTT

51

+09 BRUSH
35

90

ROAD

11 12

+86 5" COTT
53

+86 PP
28

+77 5" COTT
47

+58 8" COTT
53

+56 5" COTT
45

+52 5" COTT

55

+62 26" COTT
45

+50

ROAD

11 13

LT

E

2 DEC. 1971

Rt

27

Gas Pipe Line

PIPE LINES

BRUSH

+50	16" <u>COTT</u> 47	+50 4" <u>P</u> 57	
+50	LT +48 6" <u>P</u> 52	ROAD	RT
+38	HYD +47 4" <u>P</u> 53	11 13	
+36	N. END 18" <u>ARCH</u> CM		+37 2" <u>P</u> 73
	+15 MH 38		+35 HYD 48
			+16 <u>ENT</u>
94	+100 MH 46	ROAD	<u>BIKEWAY END</u> 39-47
+82	6" <u>P</u>	11 13	+96 36" <u>COTT</u> 71
+75	PP 56	+94 S. END 18" <u>ARCH</u> CM	
28		+70 25 TRIP <u>BIRCH</u> 67	+60 <u>BIKEWAY</u> 57-65
+63	20" <u>P</u> 30		
+50	+48 NE <u>CORR</u> HO 29	ROAD	
+25	SE <u>COR</u> HO 69	11 13	
+10	END <u>HEDGE</u>	+31 12" <u>COTT</u> 53	
+100	BEGIN <u>HEDGE</u> 64		+32 END <u>BRUSH</u> 51-60
+86	14" <u>COTT</u> 46	+90 20" <u>COTT</u> 46	
93	PP +85 TRIP 15" <u>COTT</u>	ROAD	BEGIN <u>BRUSH</u> 51-60
+83	49	12 12	
+61	20" <u>P</u> 30	+75 4" <u>APPLE</u> 64	+85 END <u>BRUSH</u> 39-60
+57	20" <u>COTT</u> 50		
+50	TRIP 18" <u>COTT</u> 57		
+50	+48 <u>PP</u> 28	ROAD	
+22	NW <u>COR</u> tower	+24 NE <u>COR</u> +40	<u>BUSH</u> 28
+08	SE <u>COR</u> tower	60	+25 BEGIN <u>BRUSH</u> 41-60
	58		
+06	SW <u>COR</u> Tower		+10 PIPE <u>LINE</u> 29
92	72	ROAD	
		11 13	

KP
DS
DK
PH

3 DEC. 1971
CLOUDY
25°
RT 28

OAKCREST

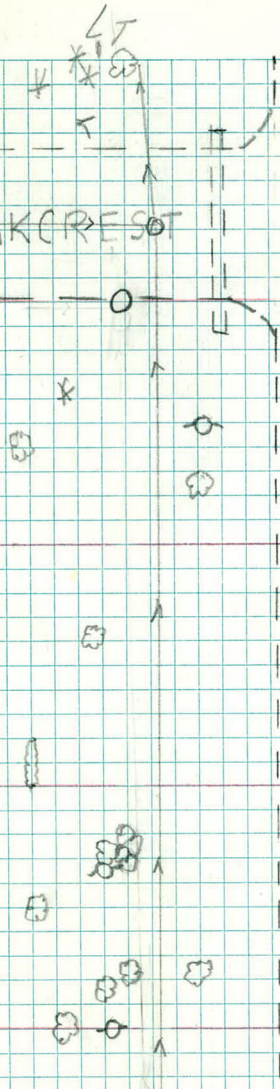


GAS PIPE LINE

BRUSH

BRUSH

BIHEVA

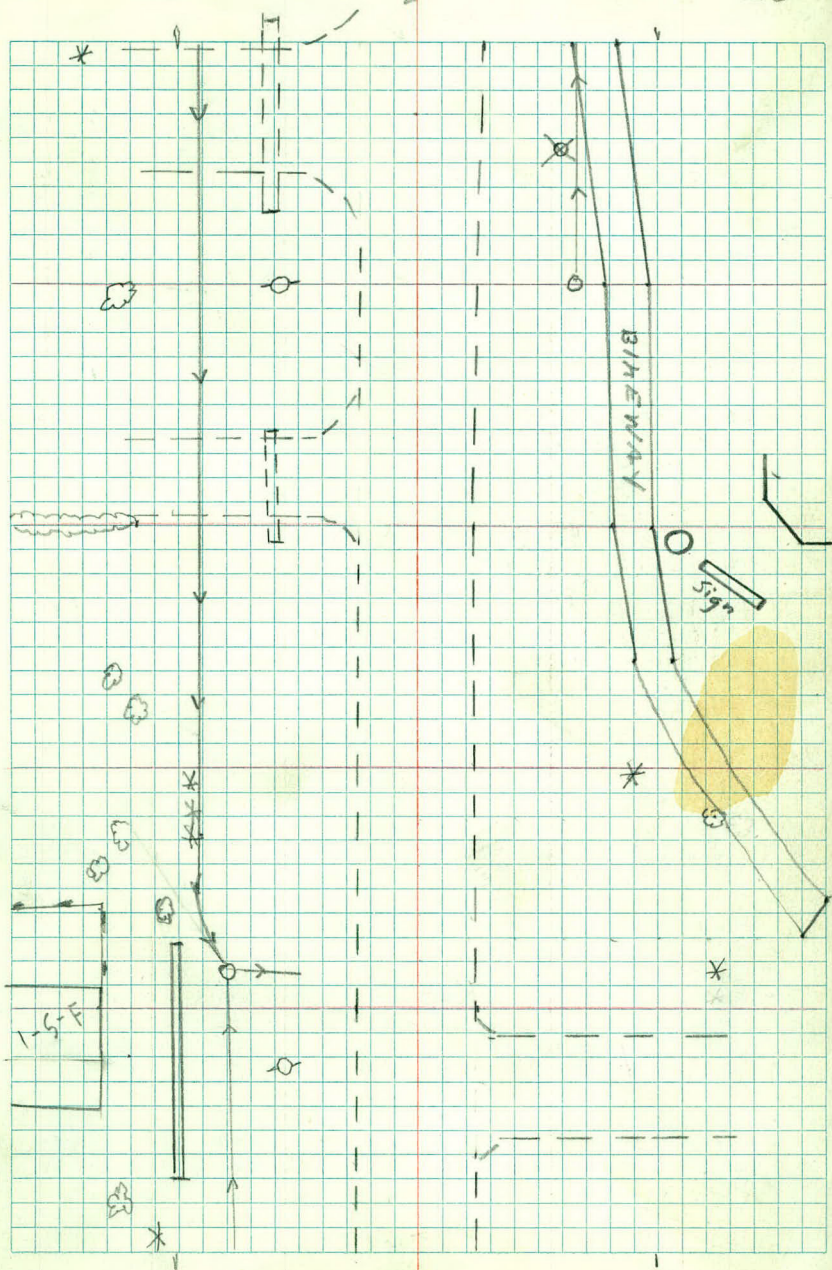


97	LT	ROAD	RT
+98 $\frac{2^{\circ}P}{70}$		11 13	+100 <u>BIKEWAY</u>
+184 $\frac{E}{ENT.}$			33-41
+65 S. END $\frac{15^{\circ}CM}{30}$			+78 $\frac{6^{\circ}P}{30}$
+50 $\frac{PP}{28}$	ROAD		+50 <u>BIKEWAY</u>
	11 13		39-47 50
			33
+48 $\frac{24^{\circ}Willow}{61}$			<u>Backstop</u>
+20 N. END $\frac{15^{\circ}CM}{30}$			96+11 7121
+11 $\frac{E}{ENT.}$			96+04 <u>Large, 5th</u>
			95+92 <u>59</u>
			95+94 <u>Backstop</u>
96 +102 <u>HEDGE</u>	ROAD		131-142
$\frac{63-W}{63-W}$	11 13		<u>Sign</u>
+96 S. END $\frac{15^{\circ}CM}{28}$			40-42 +89 <u>65</u>
+69 $\frac{4^{\circ}APPLE}{28}$			+72 <u>BIKEWAY</u>
+47 $\frac{1^{\circ}P}{46}$ +61 $\frac{15^{\circ}Willow}{58}$			45-53 +76 <u>Sign</u>
+37 $\frac{Trip Birch}{46}$ +42 $\frac{1^{\circ}P}{46}$			
+50 +35 $\frac{1^{\circ}P}{46}$	ROAD		
+21 Cor Fe $\frac{66-W}{66-W}$	11 13		+48 $\frac{2^{\circ}P}{45}$
+103 $\frac{Begin Fe}{66}$ +21 $\frac{4^{\circ}APPLE}{58}$			+39 $\frac{2^{\circ}M}{62}$
+13 $\frac{END Wall}{50}$			+29 $\frac{1^{\circ}P}{61}$
+103 $\frac{N.E. Cor Ho}{66}$ +108 $\frac{MH}{40}$			+17 <u>86-6' BIKEWAY</u>
			82
95	ROAD		
	11 13		
+80 S.E. Cor Ho $\frac{66-W}{66-W}$			
+65 $\frac{Begin Wall Ho}{50}$ +89 $\frac{PP}{28}$			+85 $\frac{E}{ENT}$
+60 $\frac{6^{\circ}Birch}{62}$ +54 $\frac{5^{\circ}P}{53}$	ROAD		
+50	11 13		

LT

3 DEC 1971 RT

29



+50

Lt

ROAD

Rt

+46 S. END 15" CM ✓ " 13

+35 2" P ✓

+44 BUSH ✓ 32

+30 GP

+52 ~~44~~ Backstop

+47 N. END 12" CM ✓

28 ✓

+42 ~~97~~

+48 BUSH ✓ 30

+16 7" M ✓

+16 Backstop

99

ROAD ✓

+100 BIKEWAY

+100 fence
100

+89 £ ENT. ✓ " 13

33-41

+94 fence
45

+68 S. END 12" CM ✓

+54 20" EV 31

+50

55
+46 MH

ROAD ✓

+37 N. END 15" RCP (APRON) " 13

+49 HYD ✓ 34

+25 2" P ✓

+13 MH ✓ +21 PP ✓

32

28

+107 ~~GP~~ ✓

29

+100 BIKEWAY
30-38

98

+103 MH

54

ROAD ✓

+94 8" P ✓

" 13

+75 S. END 15" RCP (APRON) -

+88 9" P ✓
68

30

+50 fountain
59

+50

ROAD

" 13

+21 10" Birch

78

+49 8" P

+55 N. END 15" CM

30

ROAD

+100 BIKEWAY

33-41

97 +103 0" P

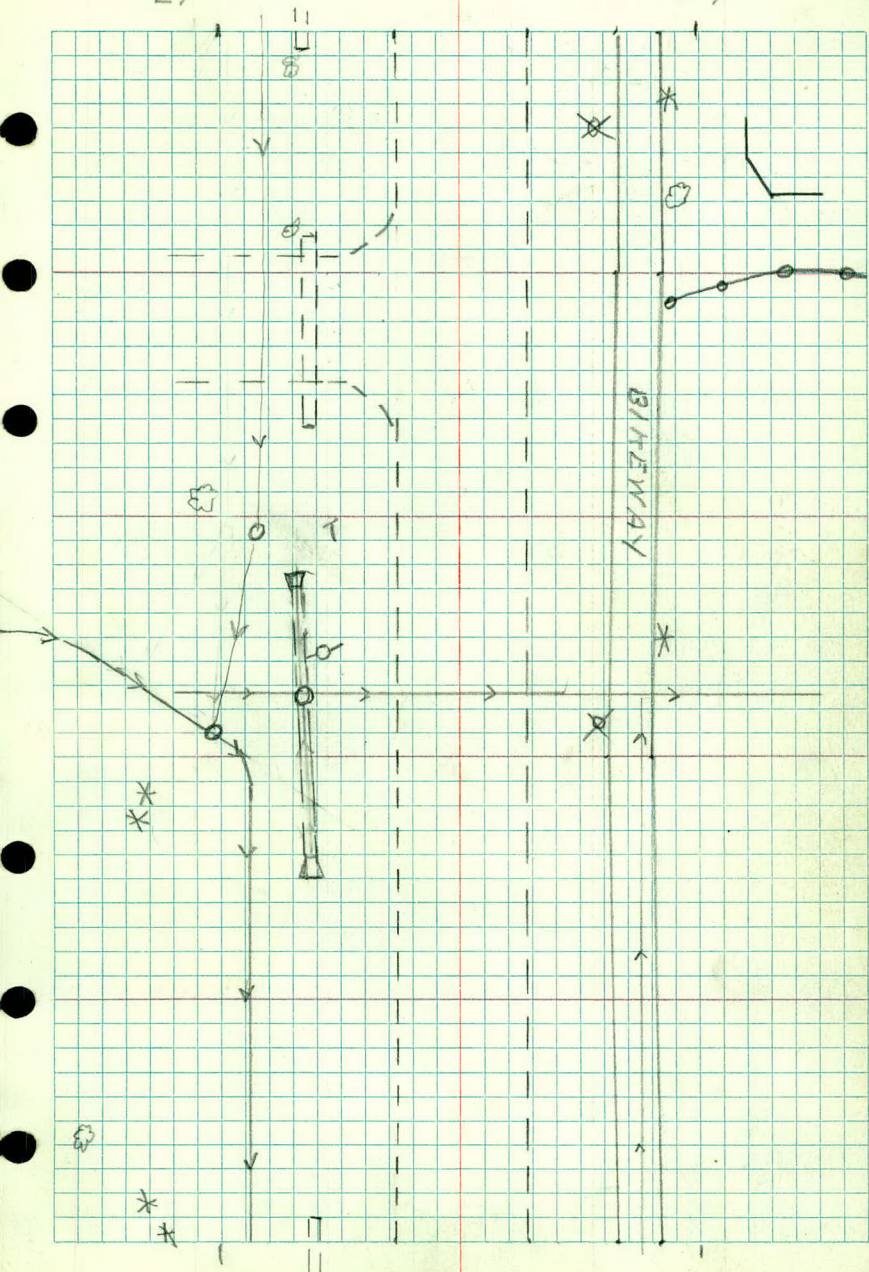
61

" 13

LT

3 DEC, 1971

RT 30



$+89 \frac{PP}{28} LT$
 102 ROAD 11 13 RT
 $+80 \frac{H.V.}{27} \checkmark +85 \frac{2'P}{43} \checkmark$
 $+77 \frac{NE \text{ END } 12'' \text{ CMV}}{33}$
 $+79 \frac{10'' \text{ POP}}{35-W 5' \text{ close}} \checkmark$
 $+87 \frac{MH}{43}$
 $+86 \frac{GP}{56}$
 $+94 \frac{\text{END BIKEWAY}}{17-38-46} \checkmark$

$+50$
 ROAD 11 13

$+44 \frac{S. \text{ END } 12'' \text{ CMV}}{27} \checkmark$
 $+24 \frac{PP \checkmark}{27} +26 \frac{6'P}{56} \checkmark$
 $+20 \frac{10''P}{69} \checkmark +22 \frac{14''M}{30} \checkmark$
 $101 \frac{28'EV}{53} \frac{8'P}{37} \checkmark$
 ROAD 11 13 $+00 \frac{\text{BIKEWAY}}{31-39}$

$+83 \frac{8''P}{45} \checkmark +81 \frac{NE \text{ CORNER}}{89} \checkmark$
 $+66 \frac{20'EV}{54}$

$+50$
 ROAD 11 13

$+32 \frac{22''E}{54} \checkmark$
 $+19 \frac{SE \text{ CORNER}}{89} \checkmark$

$+01 \frac{8''P}{39} \checkmark$

100 ROAD 11 13 $+00 \frac{\text{BIKEWAY}}{32-40} \checkmark$
 $24''E \checkmark$
 $+93 \frac{2''P}{54} \checkmark$

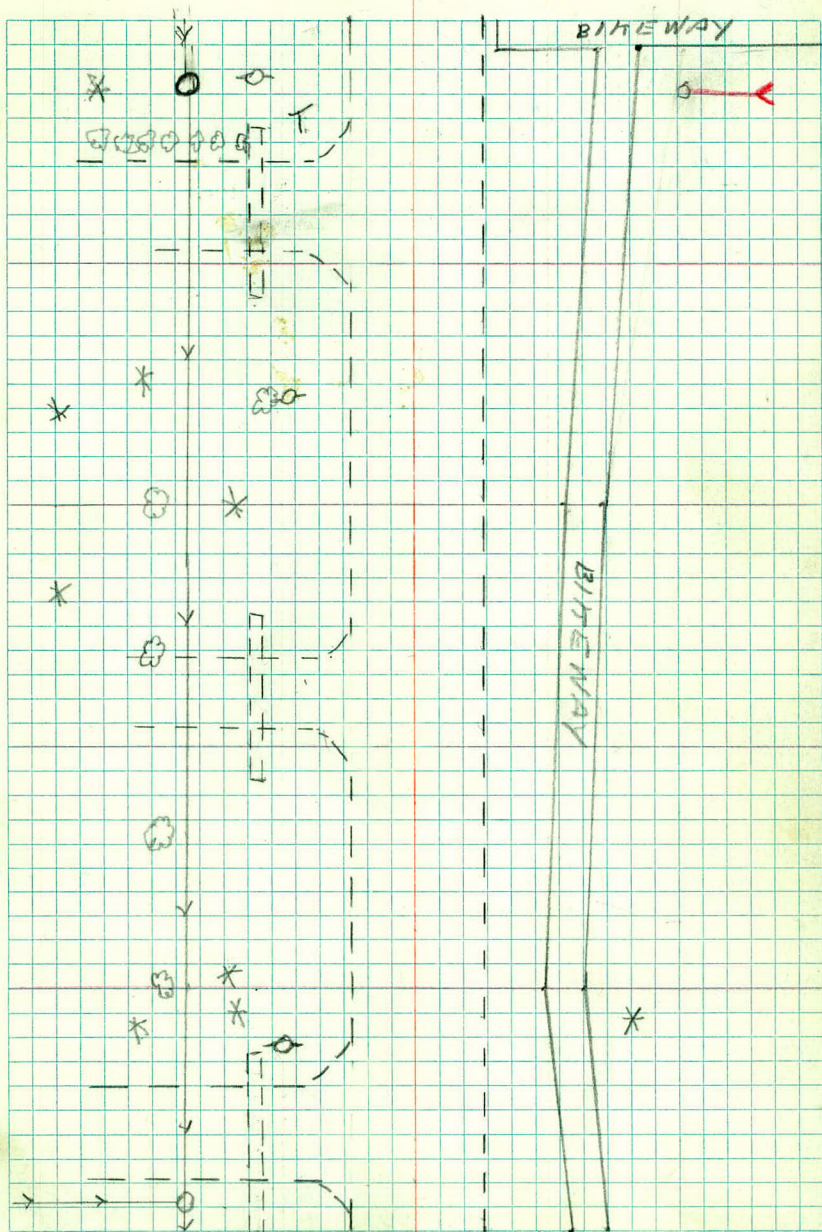
$+90 \frac{9''P}{37} \checkmark$
 $+88 \frac{PP}{28} \checkmark$
 $+56 \frac{MH \checkmark}{48}$

$+94 \frac{2'P}{45} \checkmark$

$+50$
 ROAD 11 13

3 DEC, 1971

31



99+56

101187

+50

LT

ROAD

24 24

RT

+47 2" PINE ✓
41
+45 2" PINE ✓
41

+33 MH ✓
44

+312" PINE ✓
41
+21 S.W. COR HO ✓
44
+07 18" ELM ✓
69

+05 Sign
84

104

ROAD

24 24

18" ELM ✓
41

+73 MH ✓
83

+65 MH (Storm)
52

+89 E ENT. ✓
+80 15" ELM ✓
42

+81 CB
24

+61 ~~TS~~ ✓
41

+77 15" ELM ✓
36

+79 13" ELM ✓
63
+65 CB
36

+50

+48 CB ✓
52

+28 MH ✓
43

+22 E COR DC

+33 MH ✓
37

103

CB ✓
52

+75 SD ✓
51
+80 PP ✓
29

+56 MH ✓
31

+69 24" RCP E. END ✓
92

+68 MH ✓

+65 PP 30
51

+50

ROAD

+45 RR SIGNAL ✓
18

+21 SIGNAL Box ✓
25-31-38

+16 RR SIGNAL ✓
18

102

ROAD

11 13

+02 END BIKEWAY
17

"C"

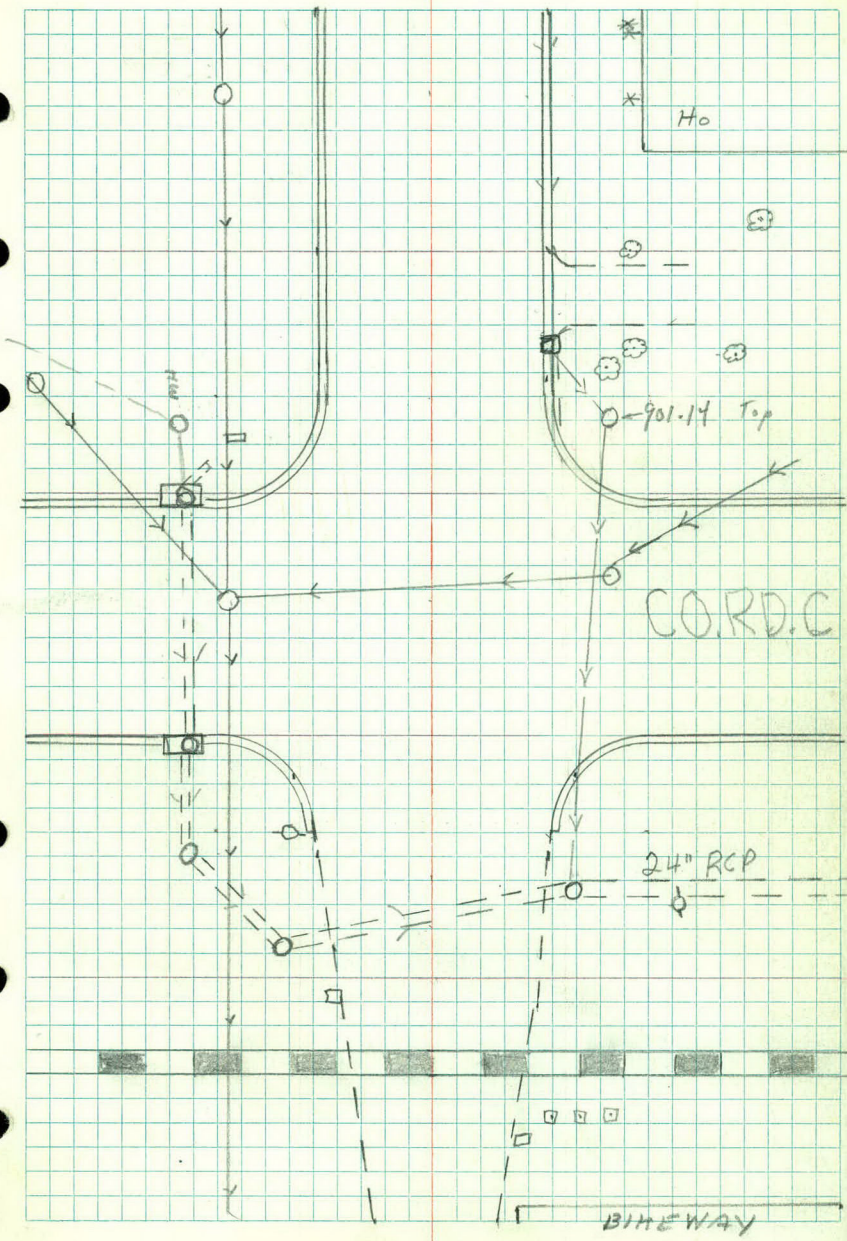
3 DEC. 1971

LT

E

RT

32



107

LT

11 ROAD 13

$$\begin{array}{r}
 + 81 \text{ 18" ELM} \quad + 86 \text{ P.P.} \quad + 97 \text{ N.W. COR. H.} \\
 \underline{30} \quad \quad \quad \underline{29} \quad \quad \quad \underline{99} \\
 + 75 \text{ 10" ELM} \quad + 80 \text{ 12" BIRCH} \\
 \underline{30} \quad \quad \quad \underline{53} \\
 + 61 \text{ 18" ELM} \quad + 71 \text{ S.W. COR. H.} \\
 \underline{30} \quad \quad \quad \underline{69} \\
 + 54 \text{ 16" ELM} \quad + 54 \text{ 12" ELM} \\
 \underline{30} \quad \quad \quad \underline{52}
 \end{array}$$

+50

11 ROAD 13

$$\begin{array}{r}
 + 56 \text{ N.E. END 15" CM} \\
 \underline{22} \\
 + 41 \text{ E ENT} \\
 + 28 \text{ S. END 15" CM} \\
 \underline{22} \\
 + 29 \text{ END HEDGE} \quad + 27 \text{ N.W. COR. H.} \\
 \underline{30} \quad \quad \quad \underline{64} \\
 + 103 \text{ 20" ELM} \quad + 103 \text{ E. HEDGE} \\
 \underline{34} \quad \quad \quad \underline{30}
 \end{array}$$

$$\begin{array}{r}
 + 33 \text{ MH} \\
 \underline{46}
 \end{array}$$

106

11 ROAD 13

$$\begin{array}{r}
 + 81 \text{ P.P.} \\
 \underline{29}
 \end{array}$$

$$\begin{array}{r}
 + 106 \text{ FL N.E. END 15" CM} \\
 \underline{24} \\
 + 82 \text{ 24" ELM} \\
 \underline{27} \\
 + 71 \text{ BUSH} \\
 \underline{49}
 \end{array}$$

+50

ROAD

$$\begin{array}{r}
 + 32 \text{ 5" ELM} \\
 \underline{44}
 \end{array}$$

$$\begin{array}{r}
 18 \text{ 24} + 49 \text{ HEDGE} \quad + 43 \text{ P.P.} \\
 \underline{52} \text{ TO E} \quad \quad \quad \underline{29} \\
 + 43 \text{ TEL CABLE} \\
 \underline{32}
 \end{array}$$

$$\begin{array}{r}
 08 \text{ SE. Cor wooded area} \\
 80 \quad + 23 \text{ CB} \\
 + 06 \text{ 5" ELM} \\
 \underline{45} \quad \quad \quad \underline{24}
 \end{array}$$

$$\begin{array}{r}
 + 23 \text{ CB} \\
 \underline{24}
 \end{array}$$

105

ROAD 24 24

$$\begin{array}{r}
 + 56 \text{ H 40} \\
 \underline{27} \\
 + 51 \text{ P.P.} \\
 \underline{28}
 \end{array}$$

+50

ROAD 24 24

$$\begin{array}{r}
 + 53 \text{ N.W. COR. H.} \\
 \underline{44}
 \end{array}$$

KP
ML
DS

8 MAR 1978
Sunny +35°

ADDITIONAL TOPOGRAPHY

HWY. 36 to Co. Rd. C

LT

~~E~~

RT

+50

+10 PP
24

+07 PP
29

79+00

+50

+46 PP
26

+41 PP
27

78+00

KP
ML
DS

LT

£

8 MAR 1978
SUNNY +35°
RT

Additional
To pg. 1

+50

LT

E

SW

RT

Fountain

33-41

58

97+00

+97 SW

33-41

+50

+53 SW

45-53

96+00

BIT SW

45-53

+97

45-53

+75 SIGN

78

+85 SIGN

67

+50

BIT WALK

58-66

+22 BIT WALK(E)

88

+32 TEL.

93

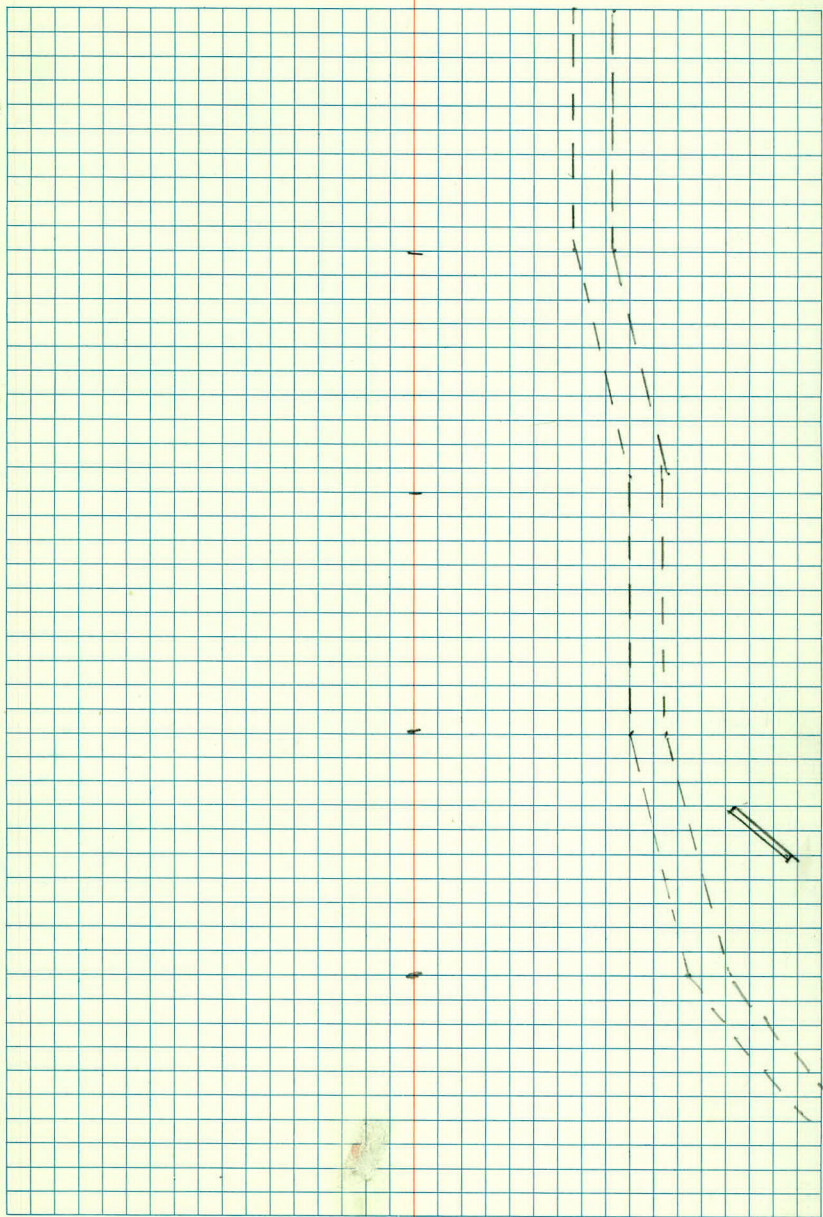
+32 Junction Box

+18 BIT WALK(W)

82

95+00

8 MAR. 1978



100

SW
33-41

+50

99

SW
33-41

+87 FE
45-E

+50

98

97+50

SW
33-41

6.0 CYCLON

+50

102

+50

101

+50

100

1
SURFACE DRAINS - CATCH BASINS

MAN HOLES

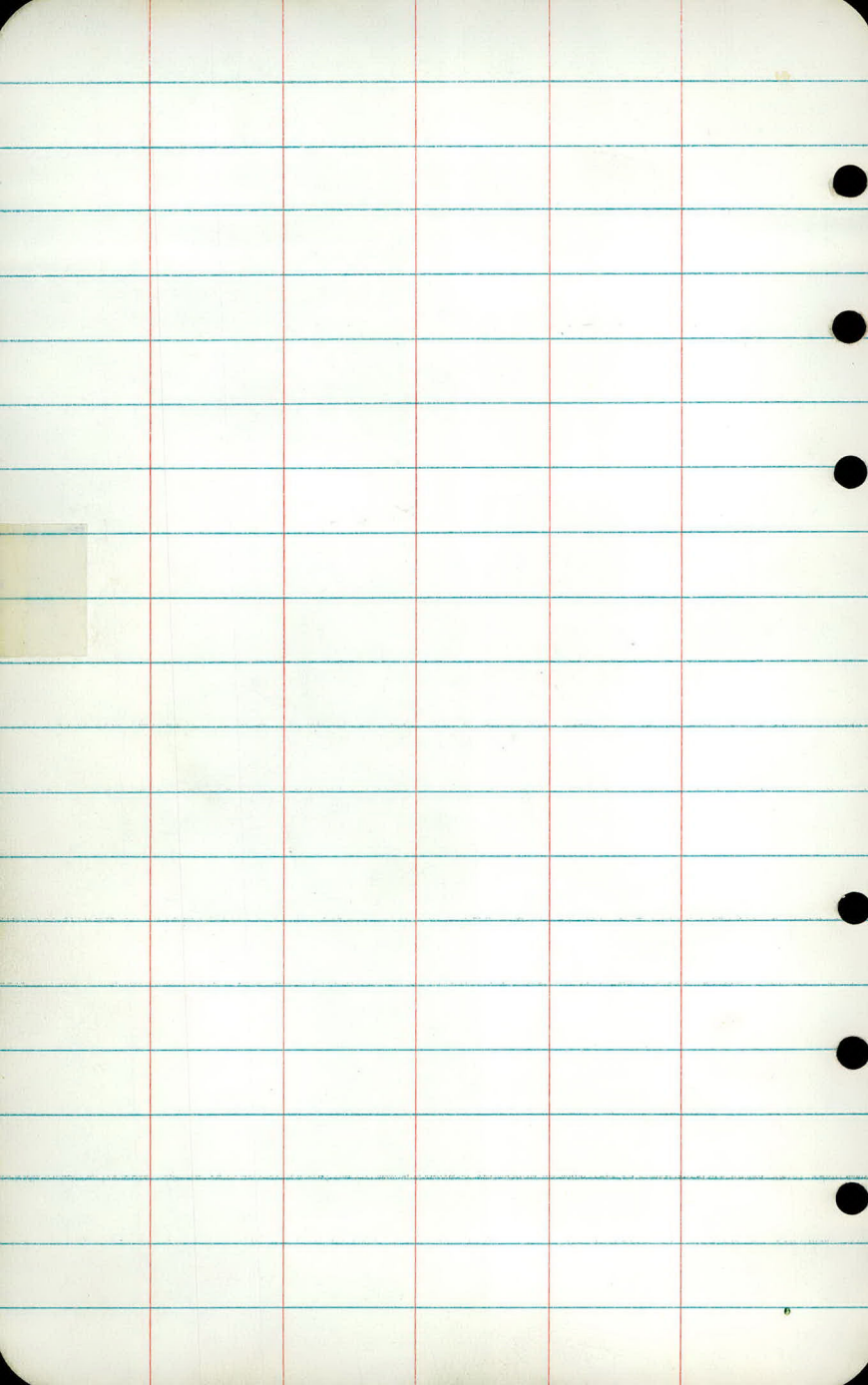
LEXINGTON AVENUE

TH. 36

LARPENTEUR TO HWY 96

PROJECT NO - 62-651-03 C.T.B

TOP OF PAGE = NORTH



69 + 43 26'RT SD

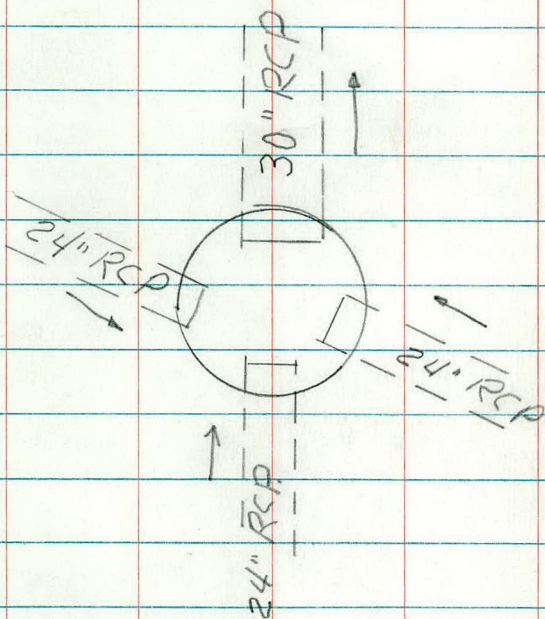
2

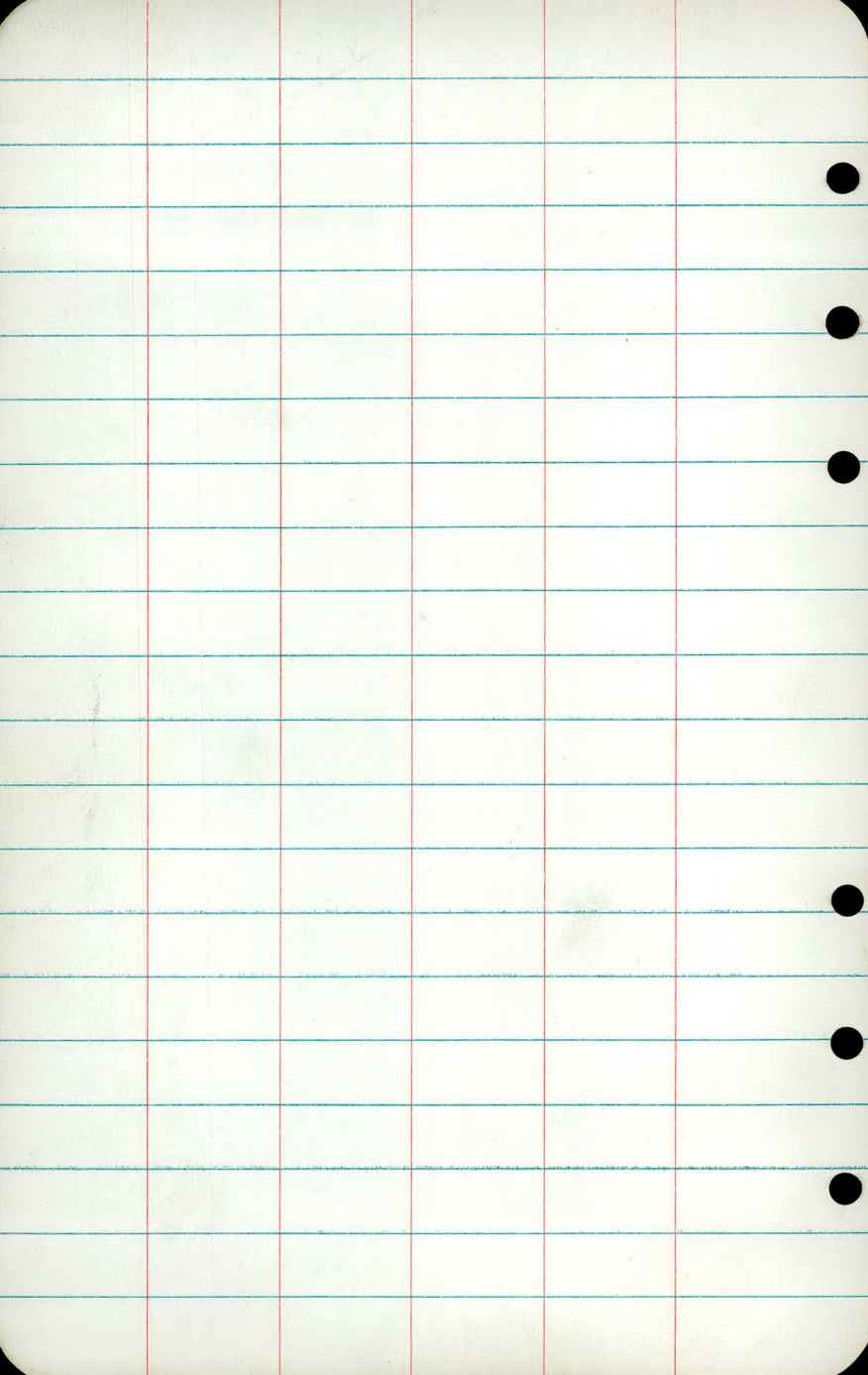
STORM

FL TO TOP = 9.22

BLOCKS

11" CASTING



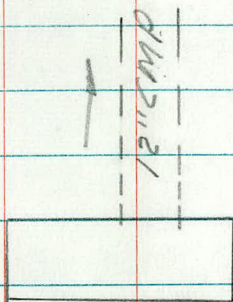


69475

53'RT

C.B

2A

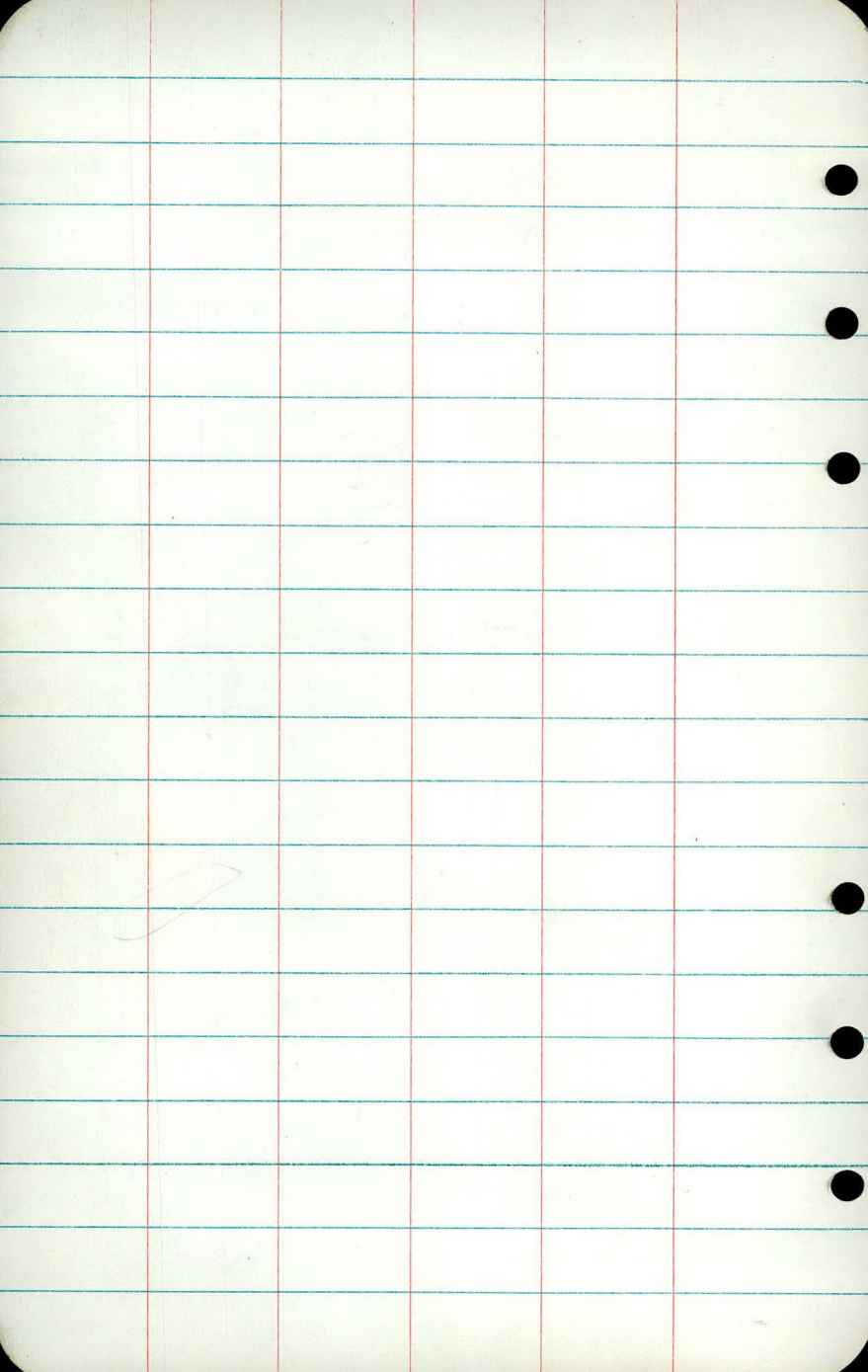


FL TO TOP = 1.95

CONC.

3" CASTING

no rings

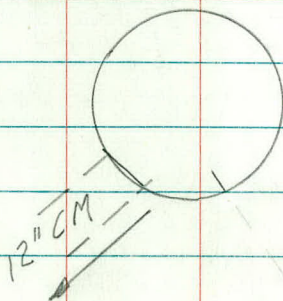


69+78

49'LT

CB

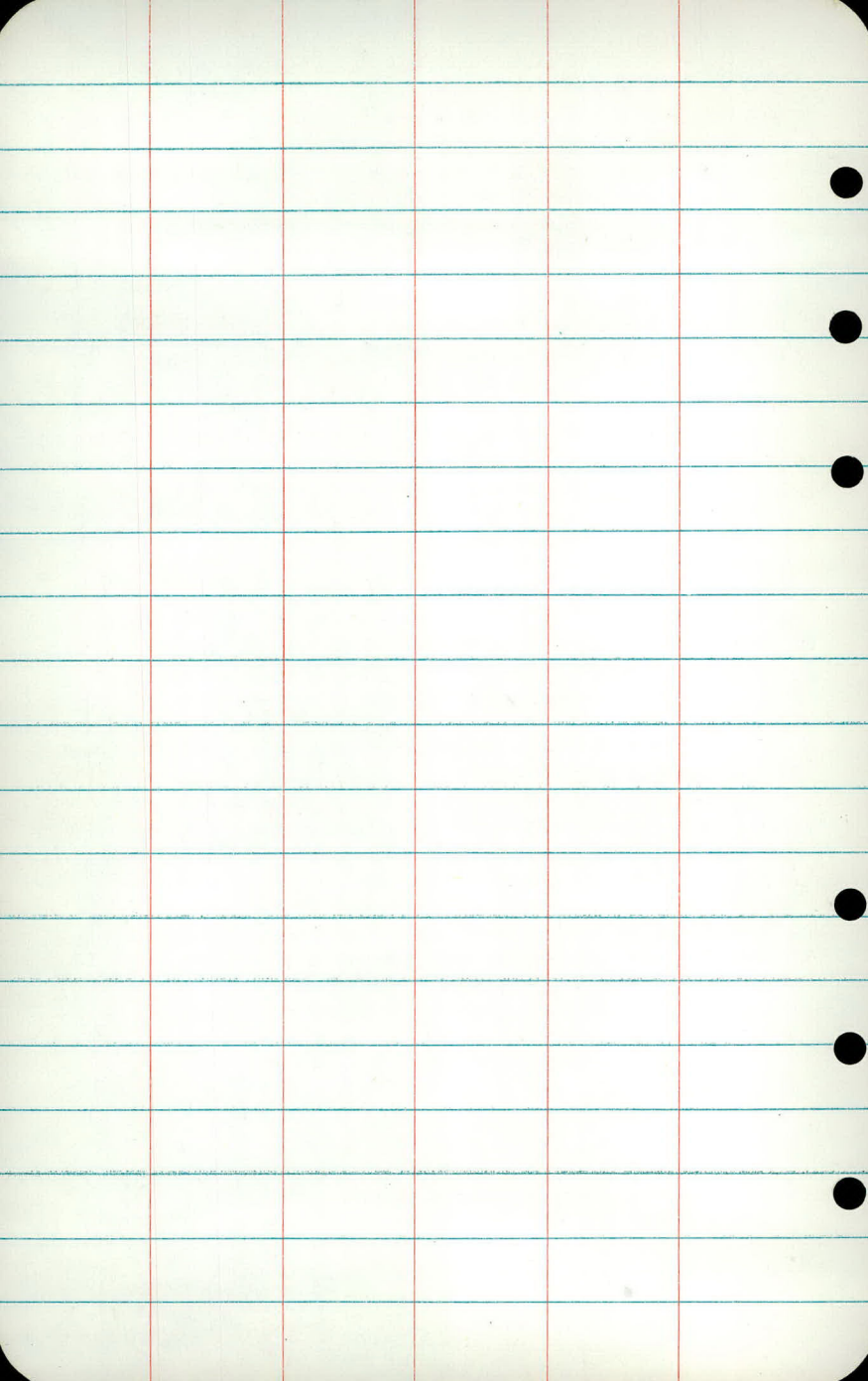
2B



FL TO TOP = 2.35

BLOCK

11" CASTING



70+04 40' RT SD

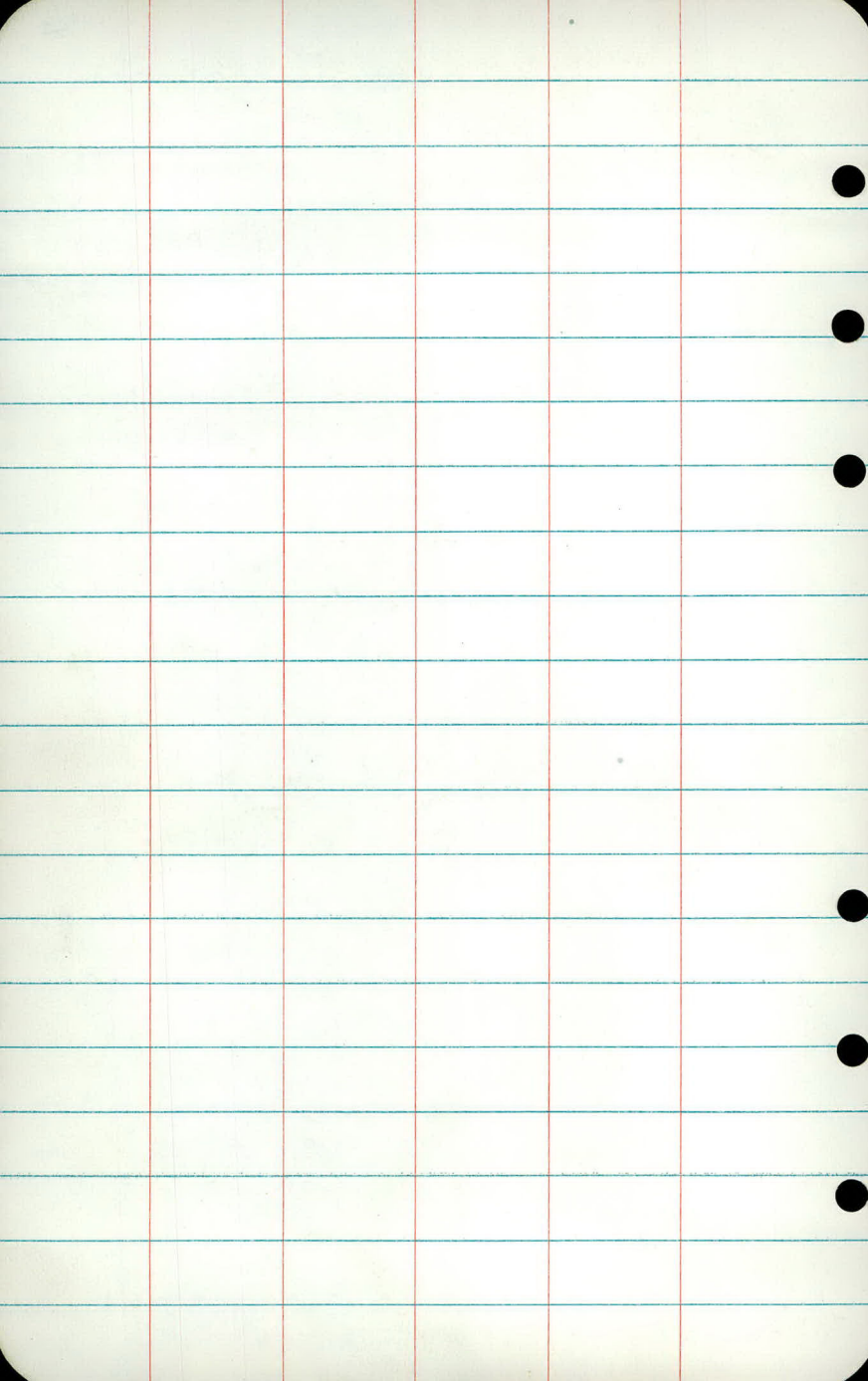
STORM

FL TO TOP = 5.35

ECCENTRIC CONE

BEEHIVE COVER

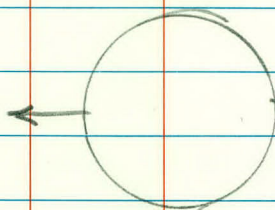




2-JUN-78

70+04 RT47

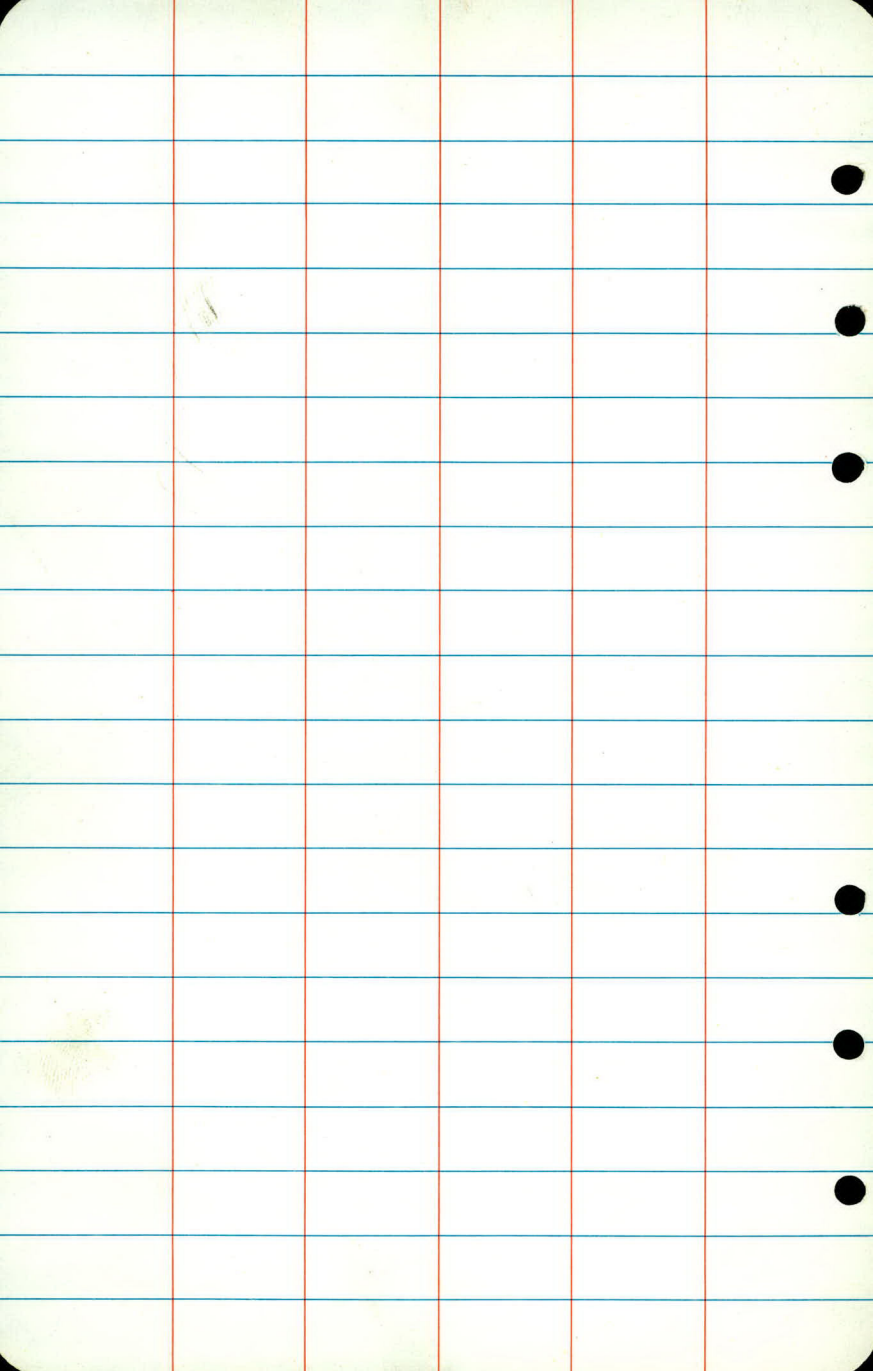
STORM DRAIN



CASTING BEEHIVE

INV TO TOP CASTING 5.79

NO RINGS

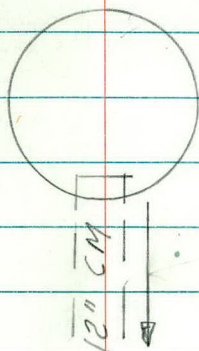


70+05

78'LT

CB

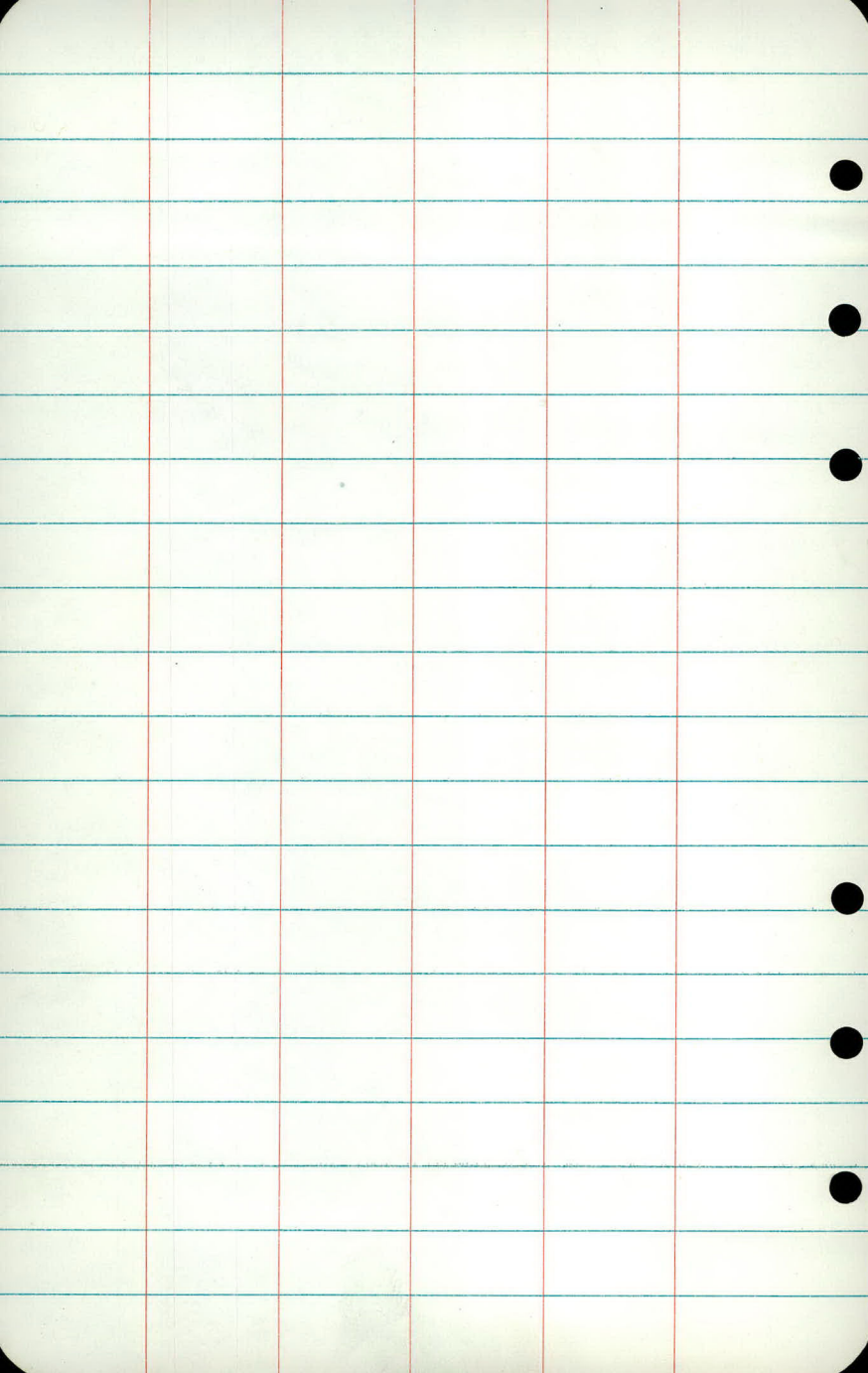
3A



FL TO TOP = 2.44

BLOCK

11" CASTING

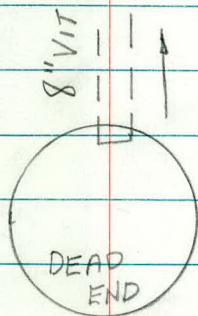


70+61

59'RT MH

4

SANITARY



FL TO TOP = 10.90

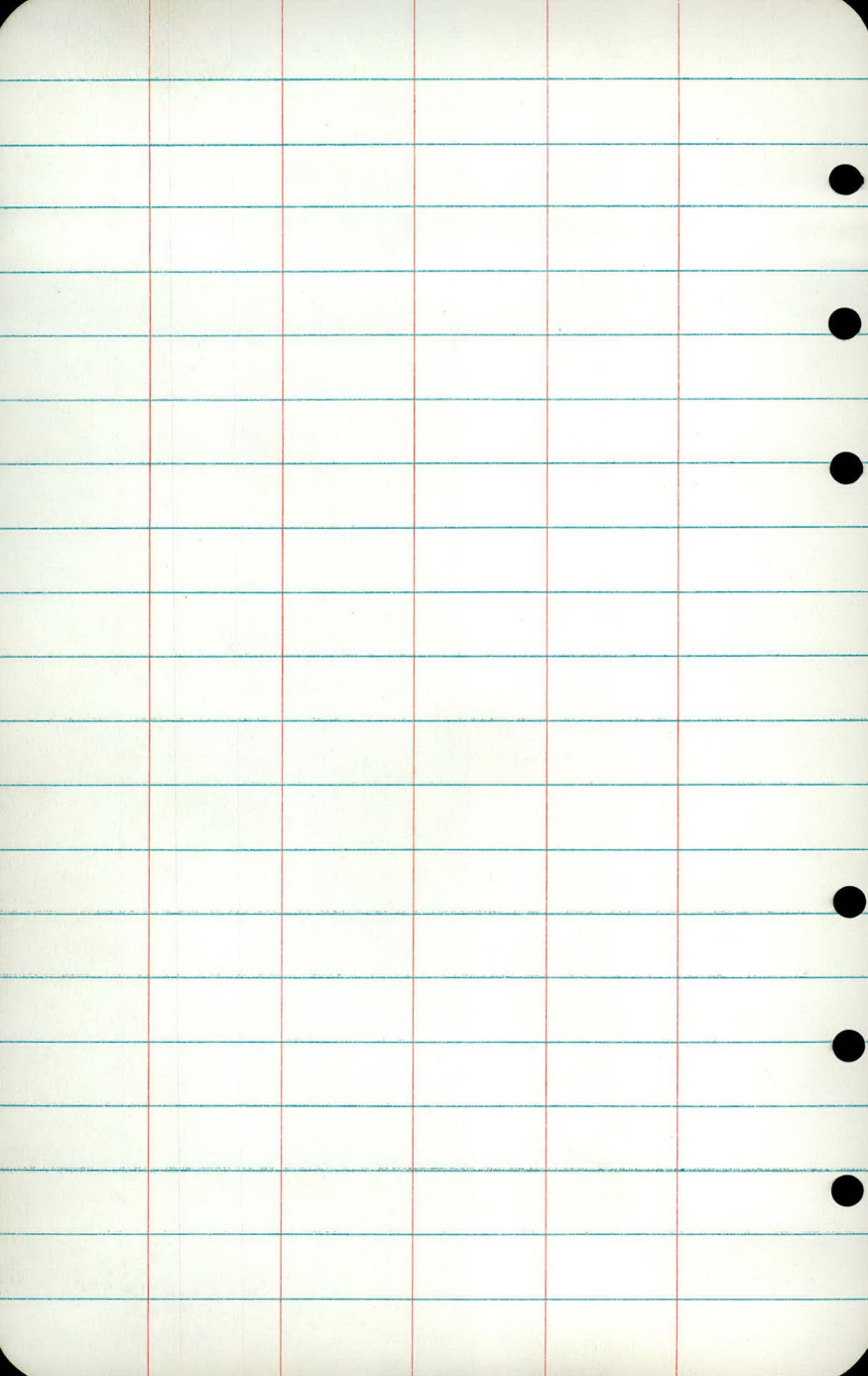
3.0 SECTION

1.5 SECTION

4.5 ECCENTRIC Cone

2 RINGS

11" CASTING

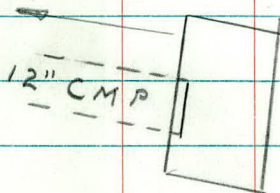


71+20

30' LT C.B.

4A

STORM

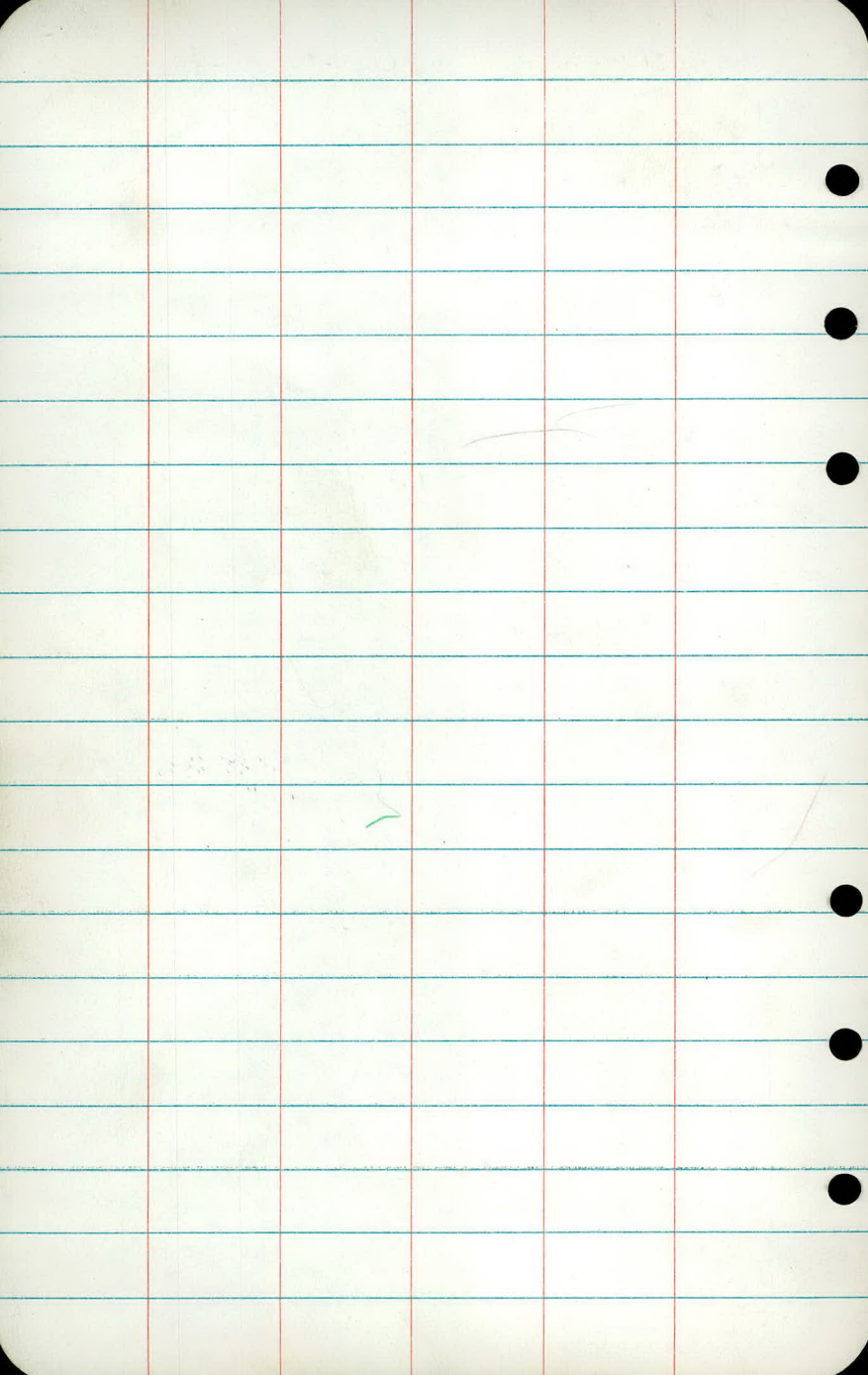


F.L. TO TOP 2.20'

CONC.

3" CASTING

NO RINGS

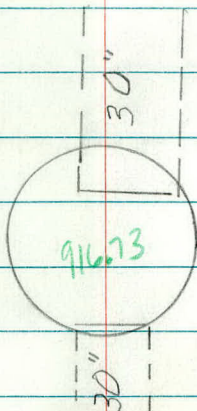


71+60

Rt 32'

CB

4B



$$\begin{array}{r} 925.38 \\ 916.73 \\ \hline \text{Inv} = 916.73 \end{array}$$

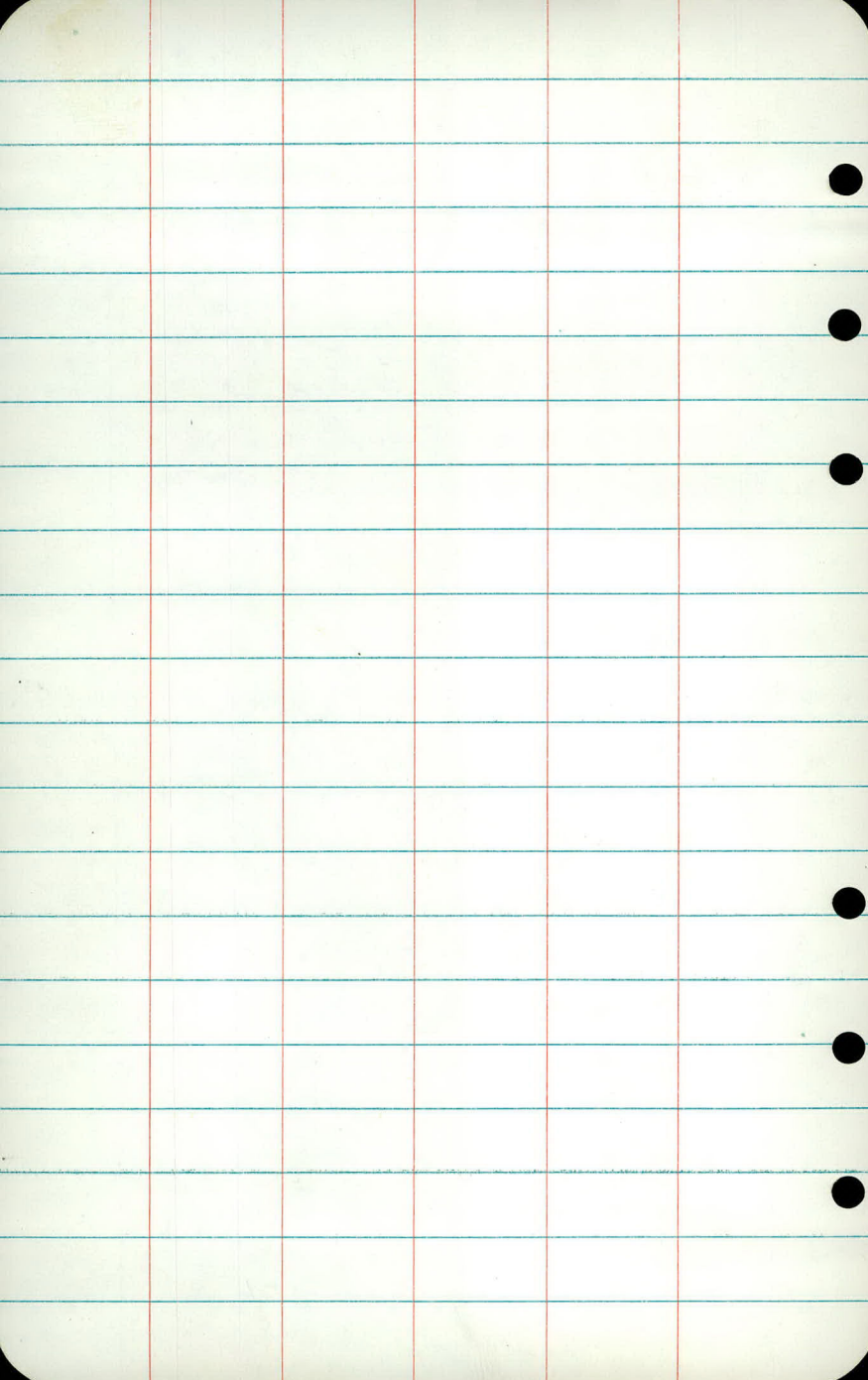
FL TO TOP = 8.64

H.S. Concentric Cone

2 rows 6" BLOCKS

11" CASTING

no rings

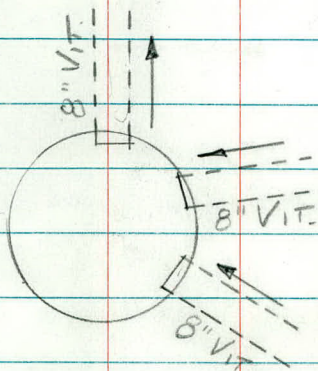


72+35

60' RT MH

5

Sanitary



F.L. TO TOP 13.05

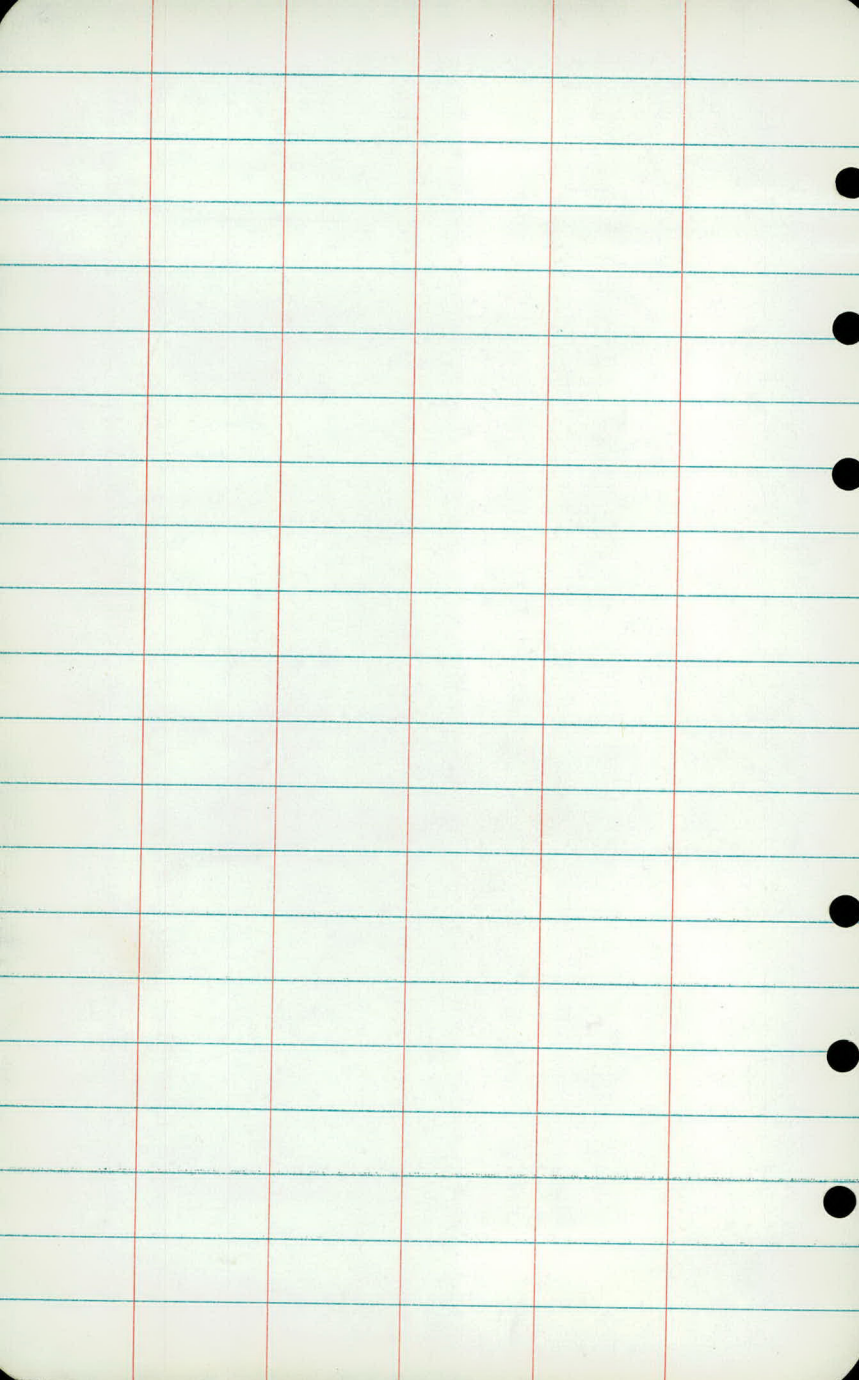
1.8 SECTION

4.0 SECTION

4.5 ECCENTRIC CONE

8 RINGS

11" CASTING



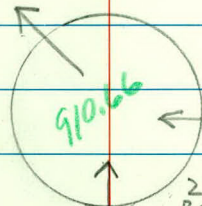
2-3 UN-78

72 + 52 RT 53'

MH STORM



36"
RCP



28"
RCP

28"
RCP

INV

8.44 - 913.45

CASTING 11"

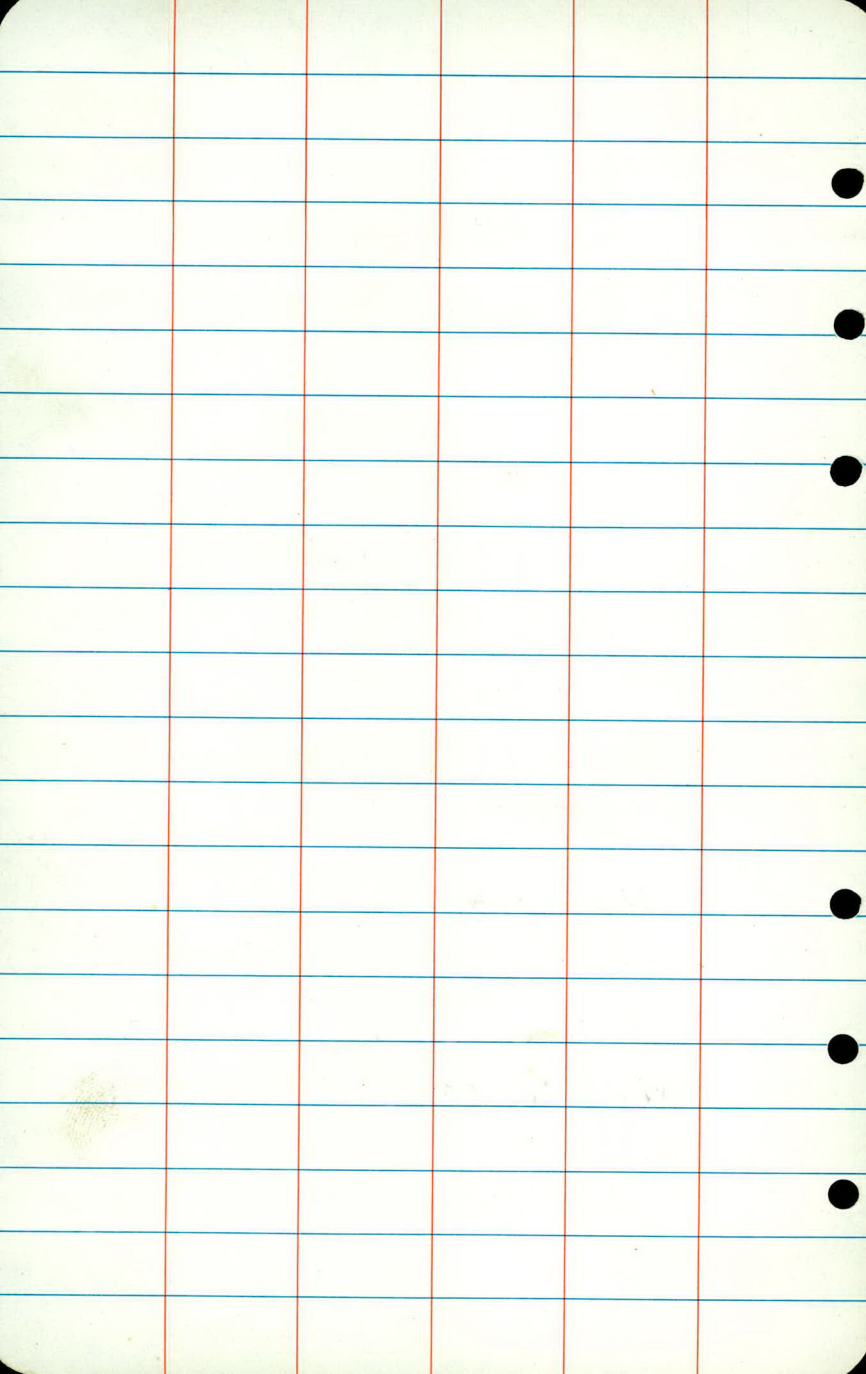
MIX. HAT

1-ROW BLOCK

1-6' SEC

M.H. INV 11.23

No RINGS

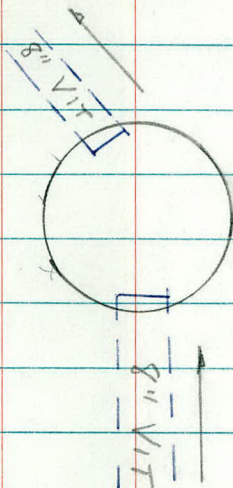


72462

60 RT MH

6

Sanitary



FL TO TOP = 11.39

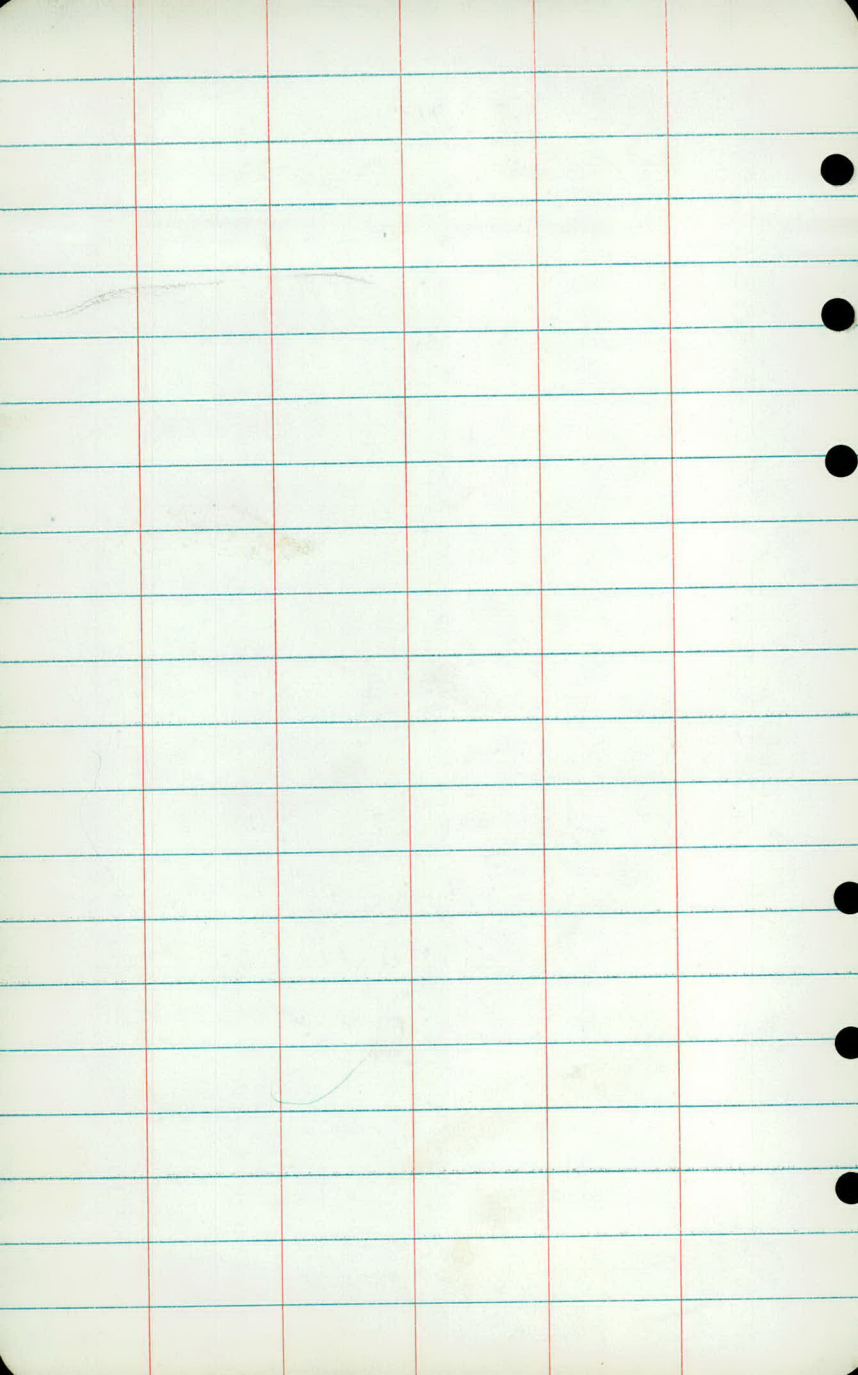
3.6 SECTION

1.4 SECTION

4.5 ECCENTRIC CONE

3 RINGS

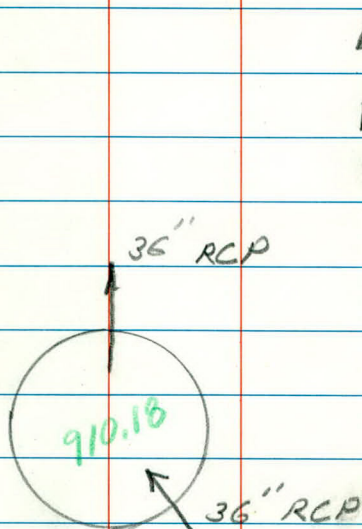
11\"/>



2-JUN-78

72+91 RT31

MH STORM



CASTING 11"

MIX. HAT

1-6' SEC

1-2.6' SEC

INV TO TOP CASTING 11.50

NO RINGS

1111

7-930

72-200

72-200

+100

✓

+100

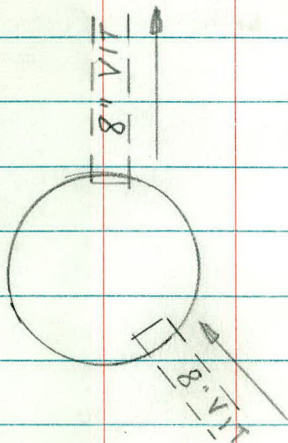
72 + 96

37' RT

6A

Sanitary

MH



FL TO TOP = 11.09

4' SECTION

4.5 ECCENTRIC CONE

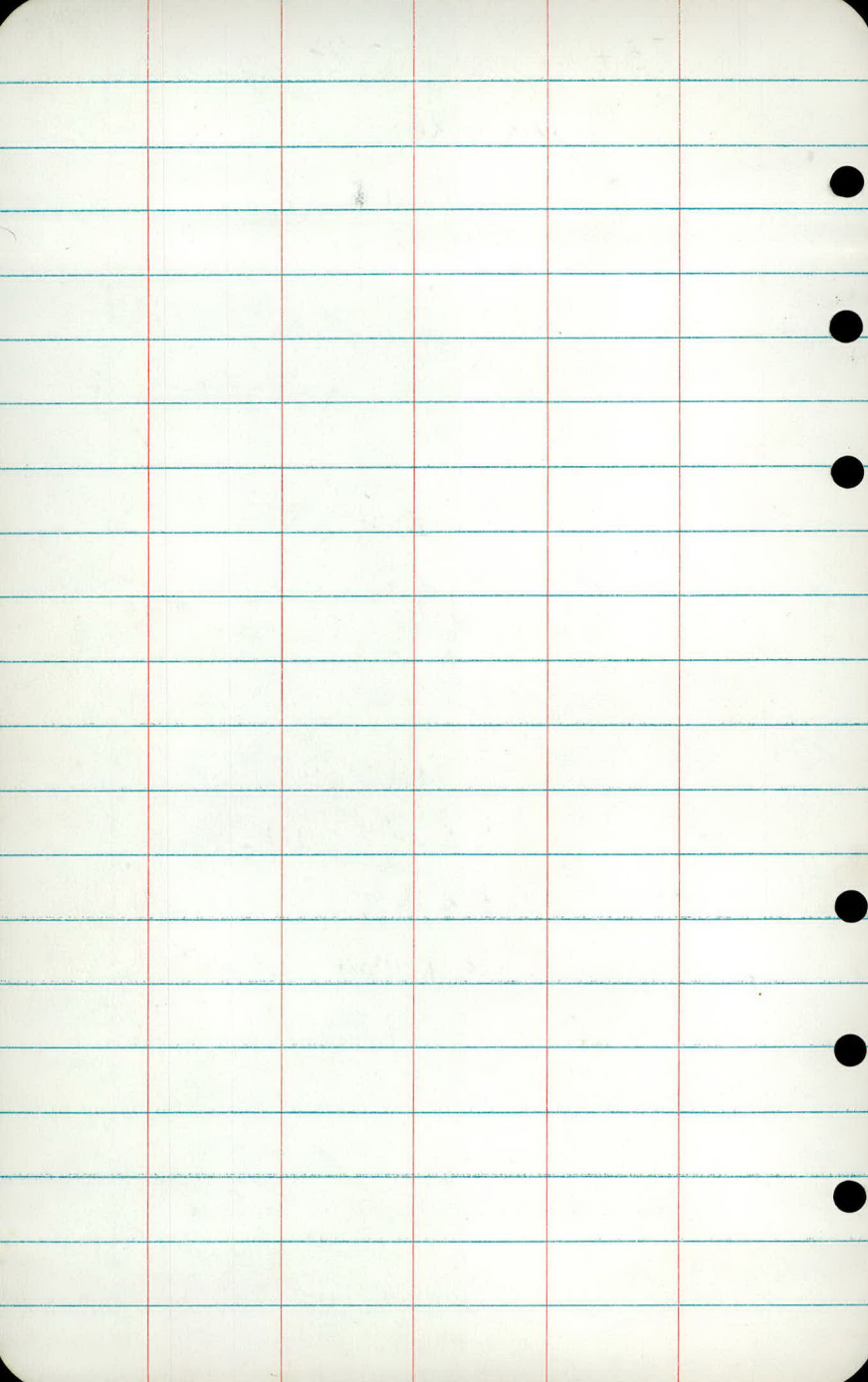
6 RINGS

11" CASTING

1.5
1
4
6.5

918.86
6.5
12.36

722.81
12.36
10.45
1
9.5

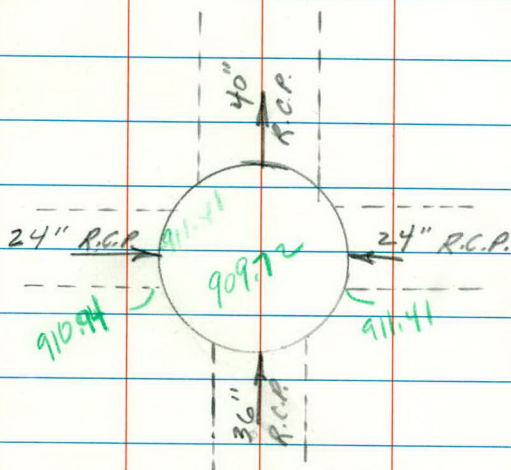


74+03

RT 32'

6-6-78
P.M.

MH. Storm



Mexican Hat

4 rows block

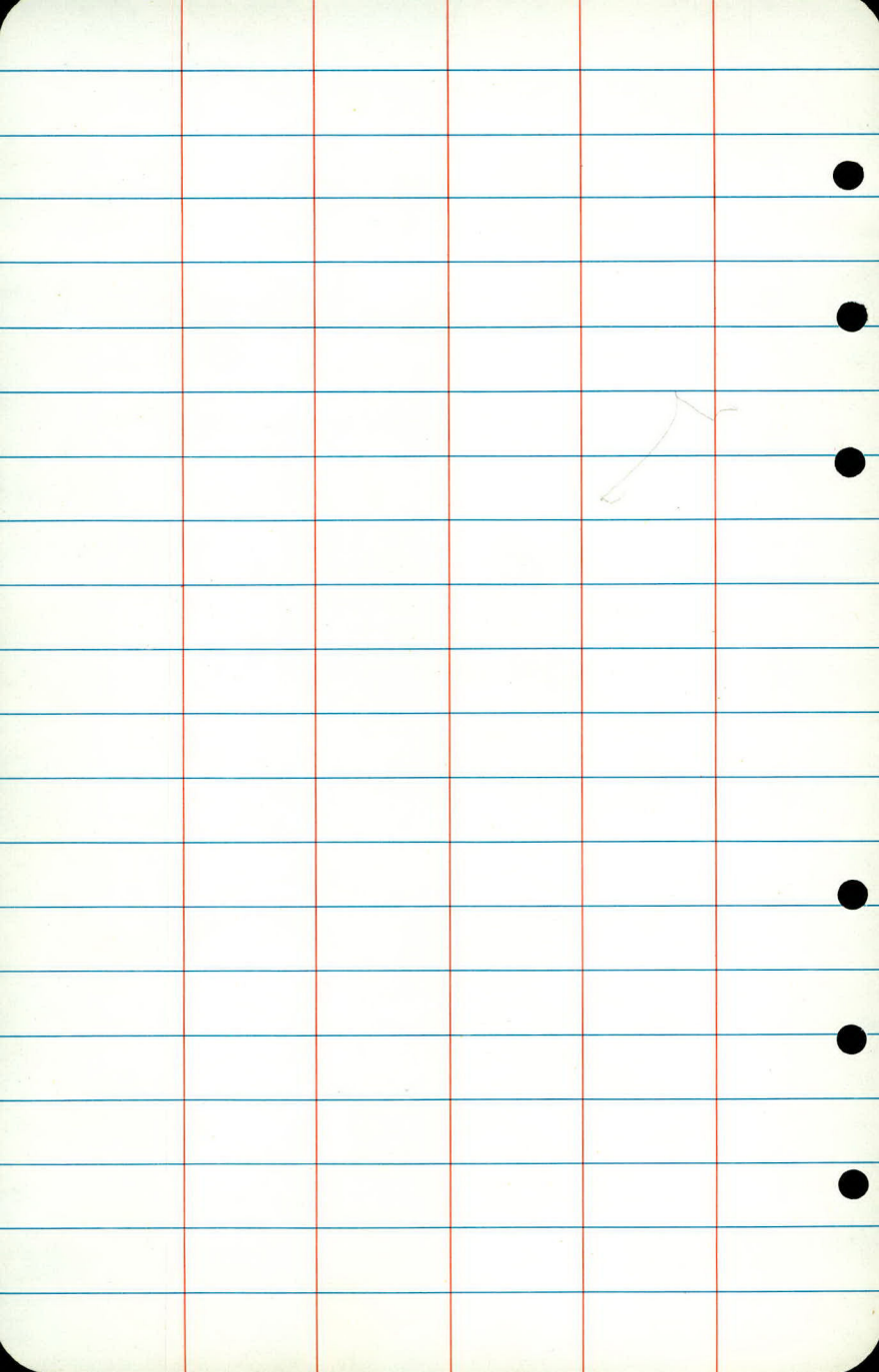
5.93 to E. Inv.

6.40 to W. Inv.

7.62 to Inv. M.H.

11" casting

No rings



75+35

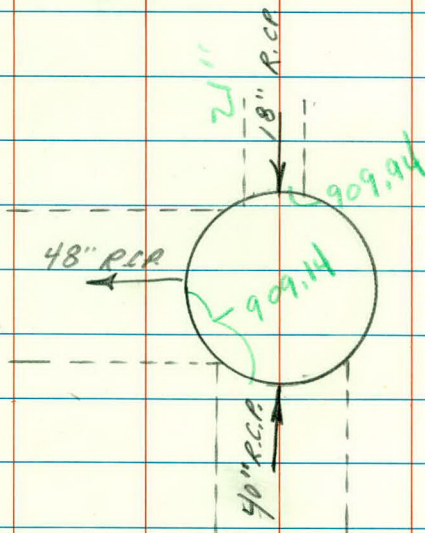
Pt. 35

6-6-78

P.M.

MH.

Storm



No rings

10.5 to inv.

9.7 to inv. N.

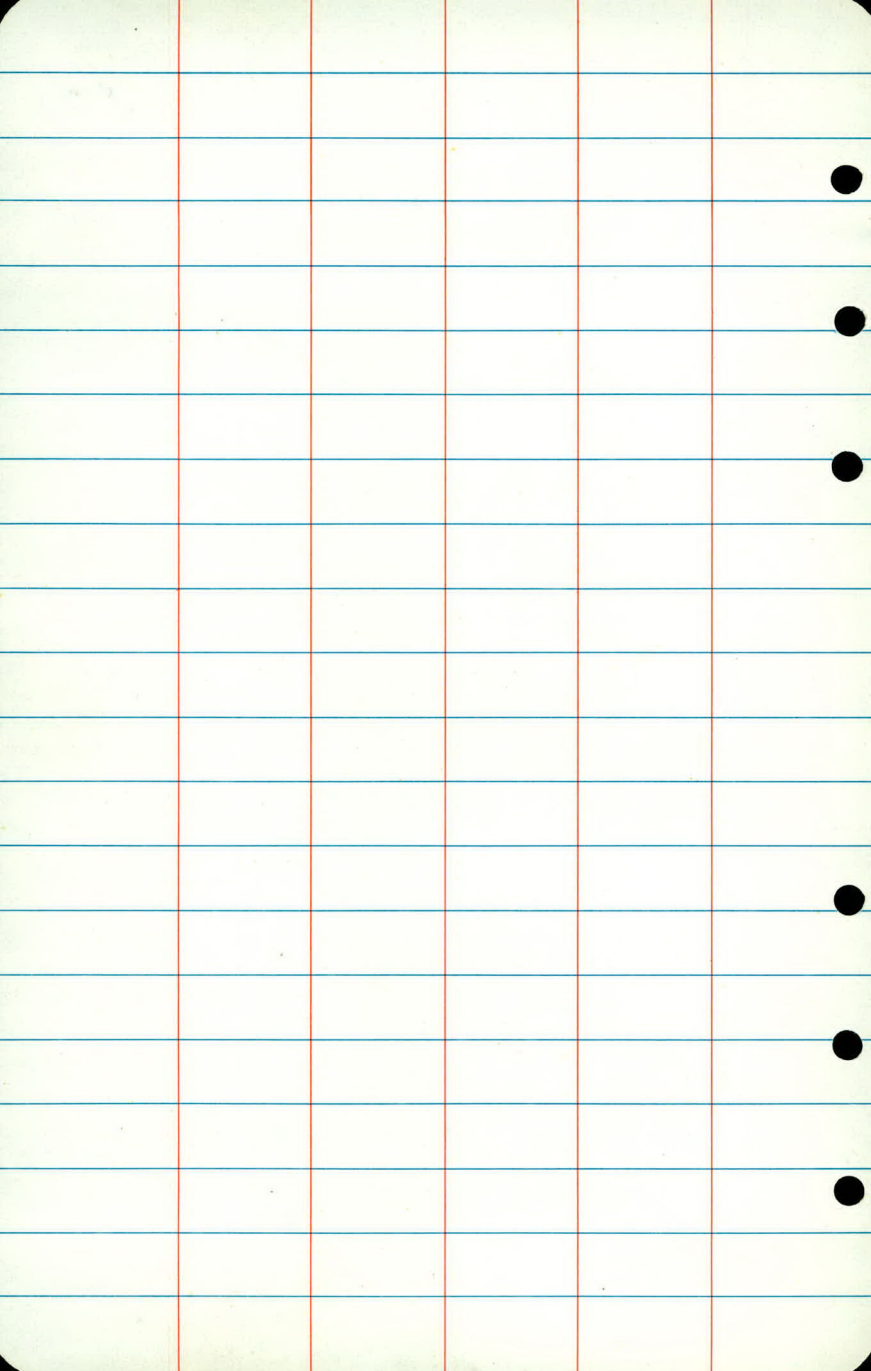
1- 18" precast section

1- 5' 10" " "

Mexican Hat

11" casting

MH steps

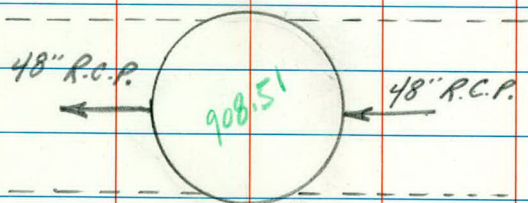


75+35 Lt. 20'

6-6-78

R.M.

M.H. Storm.



M.H. Steps

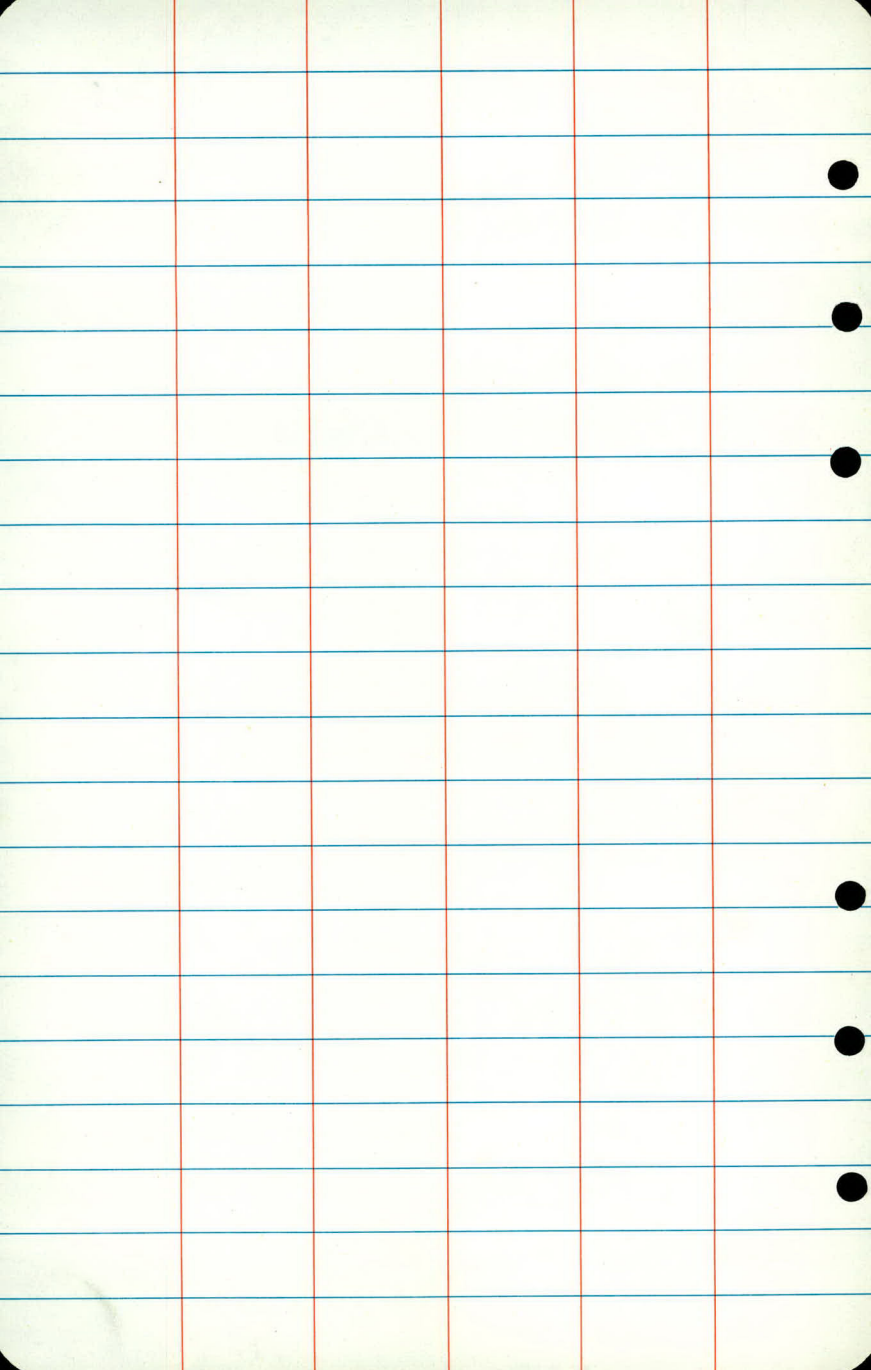
1-12" precast section

1-48" " "

12.2' to Inv. M.H.

8 rings

8" casting
catch basin grate

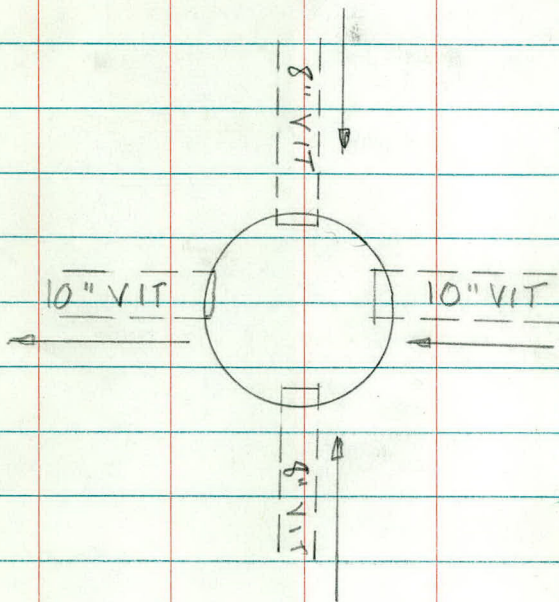


75+47

40' LT

MH

6B

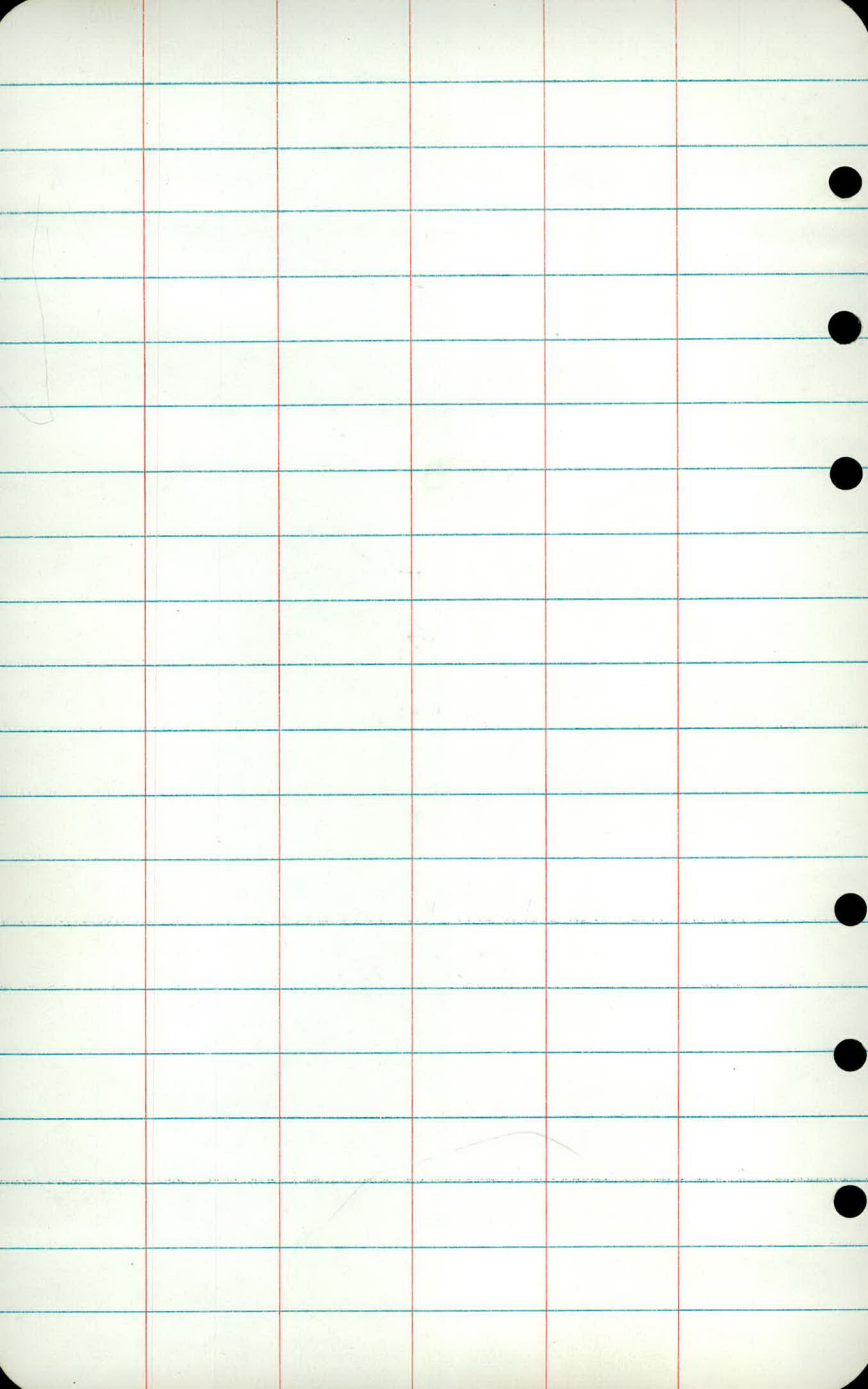


FL TO TOP = 8.35

11" Casting

No Adj. Rings

eccentric Cone



75+55

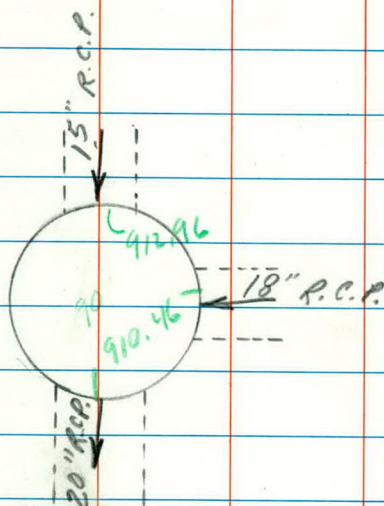
Pt. 32

6-6-78

R.M.

MH

Storm.



4 row block on base
 4- rings

1- 18" pre cast section

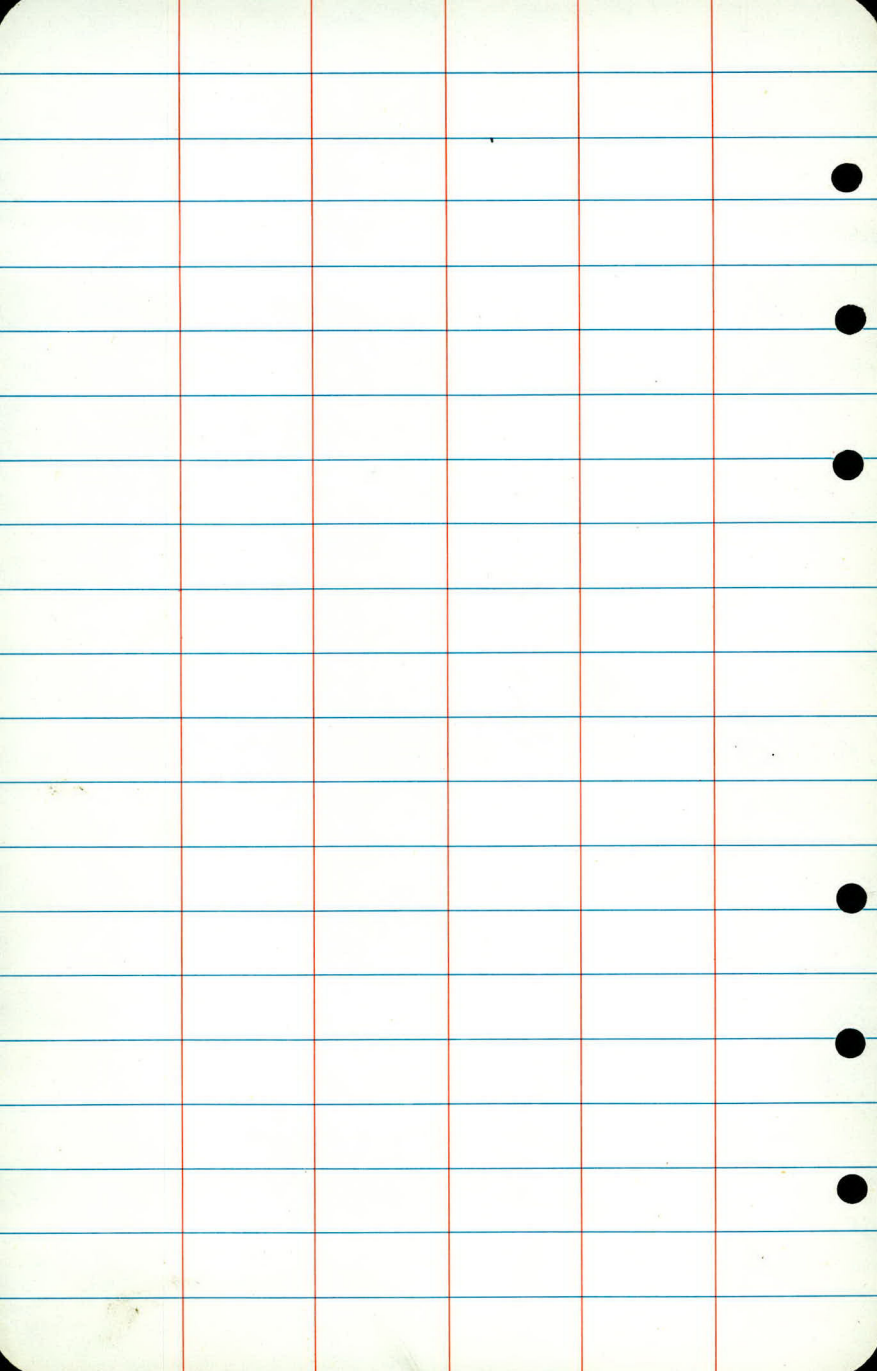
1- 42" " "

9.83' to inv. MH

7.33 to inv. N. pipe

11" Casting

Mexican Hat

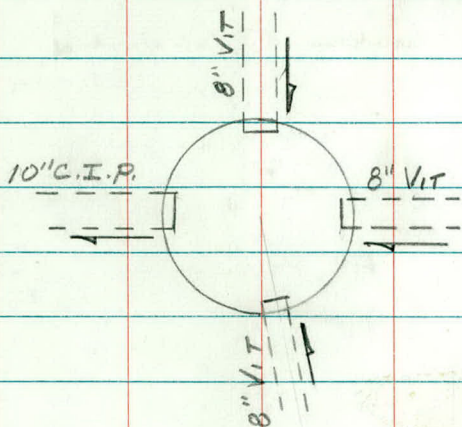


75+60

39' RT MH

7.

SANITARY



F.L. TO TOP 13.65

920.19

4.5' SECTION

C
919.2

2.7' SECTION

Sec
914.7

4.5' ELL. CONE

Rings
913.7

4 Rings

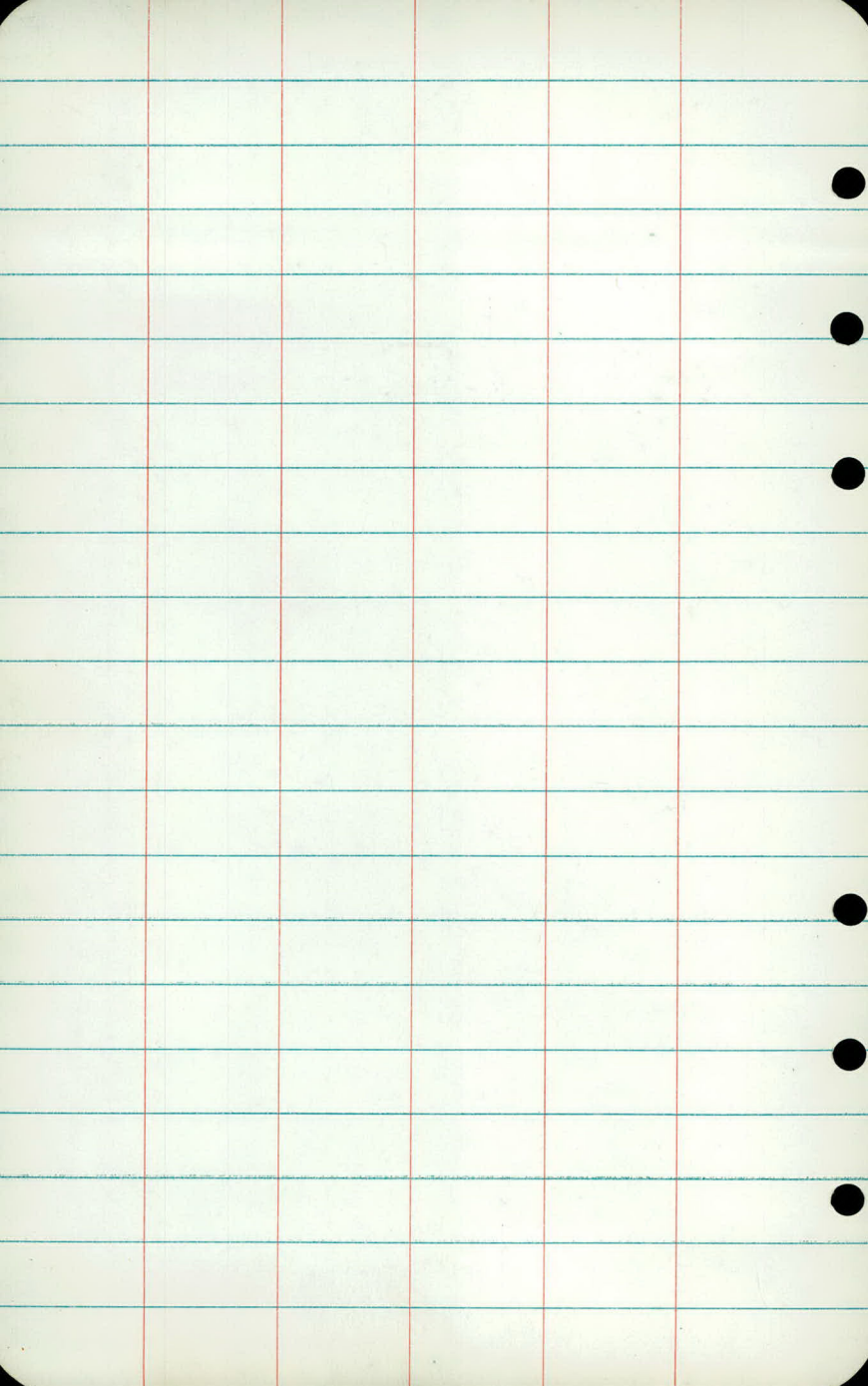
922.5

11" CASTING

913.7

8.8

- Cast - 1.0
78

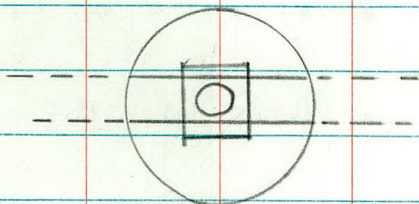


78+56

44' LT MH

8

WATER



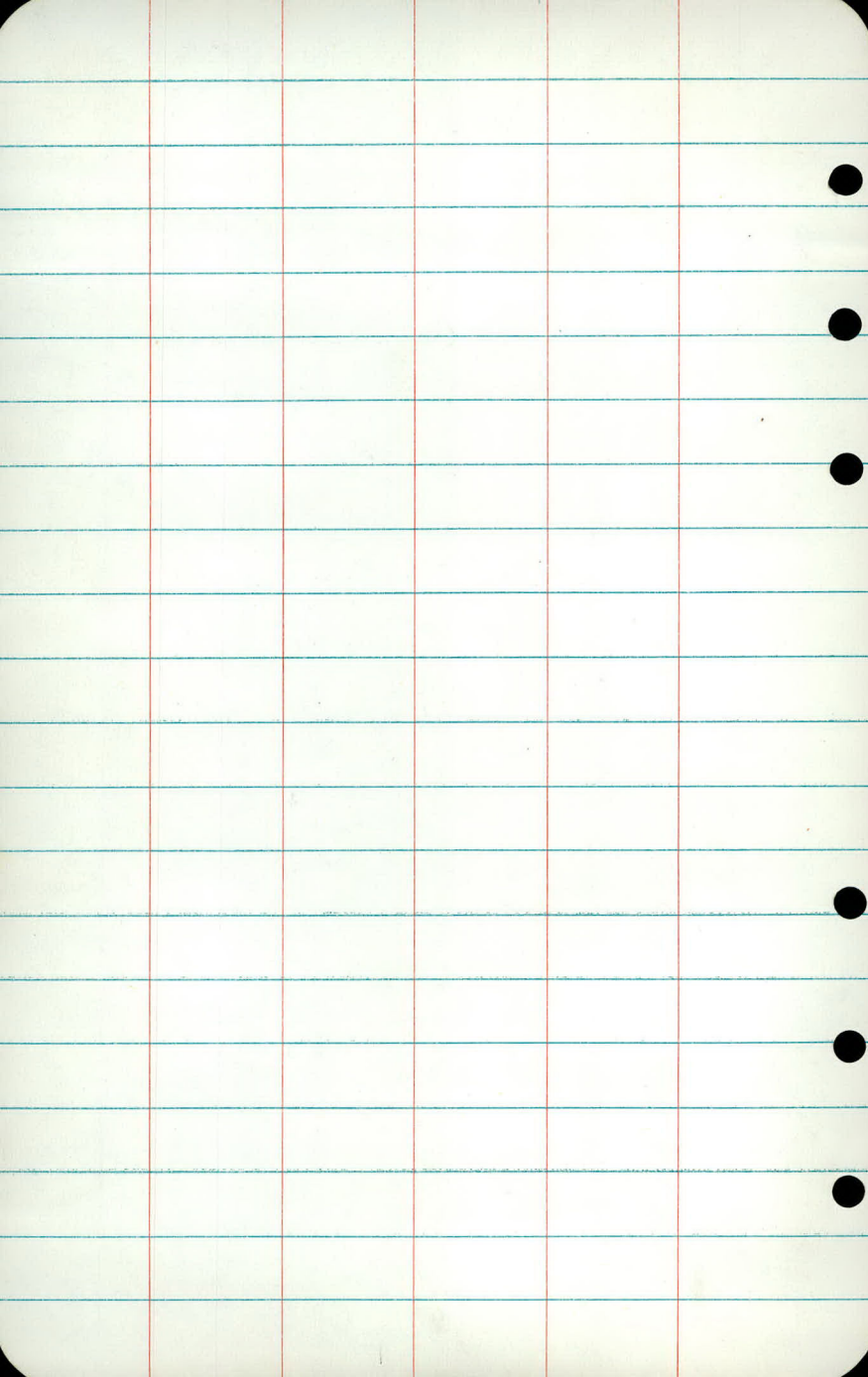
BOTTOM TO TOP 9'23

6' SECTION

0.5 MEXICAN HAT

8 RINGS

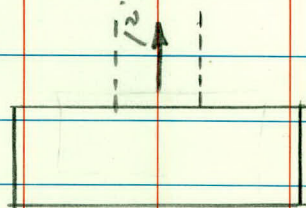
11" CASTINGS



7B+62 LT 74

6-6-78
R.m.

C.B. storm



catch basin (rect) top.

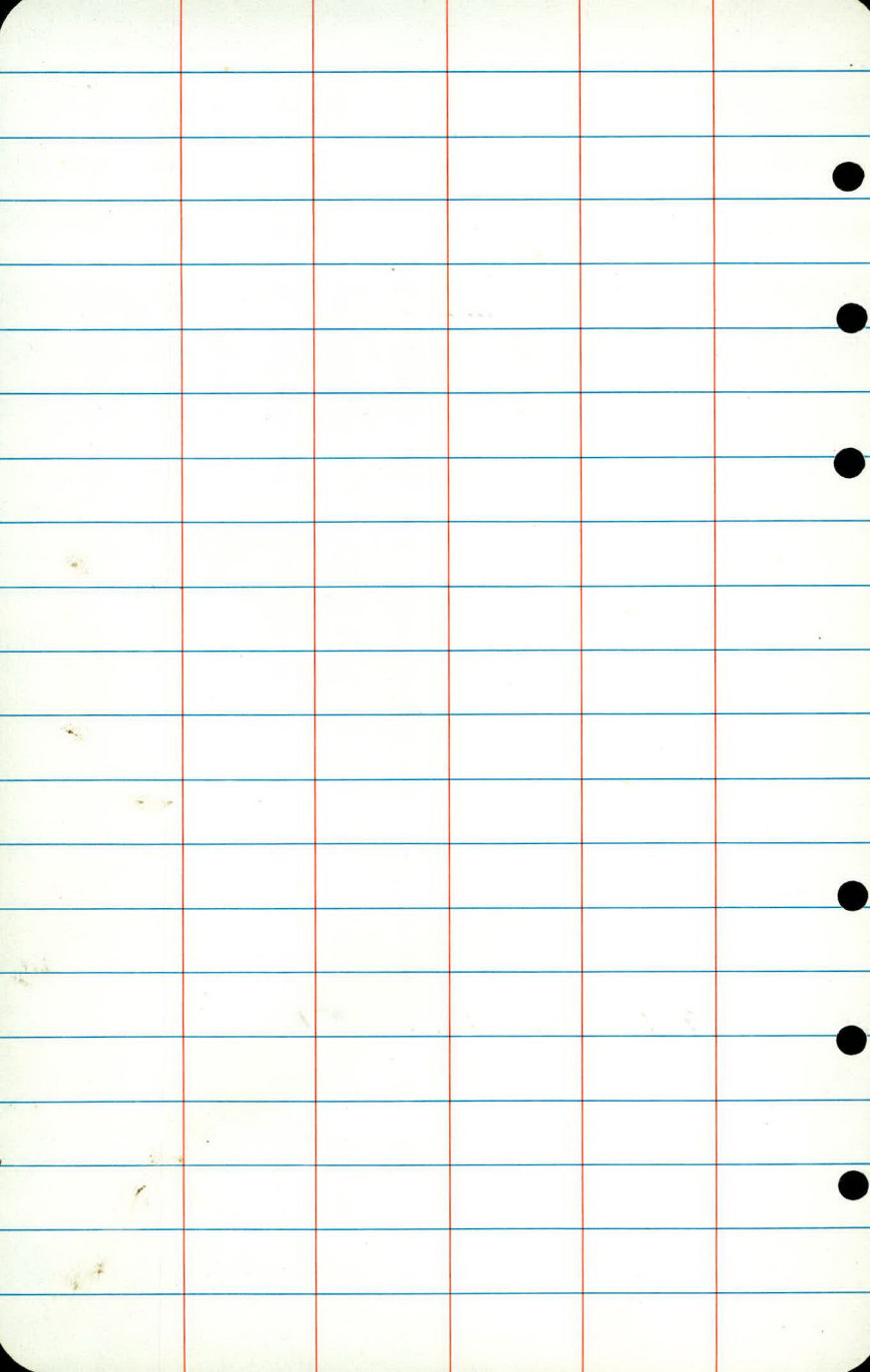
6" casting

6.17' to Inv. C.B.

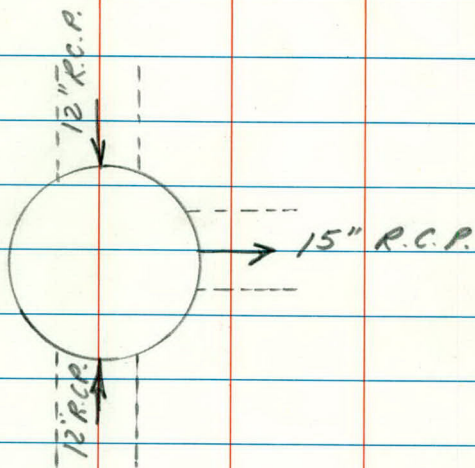
4' - 24" X 36" rectangle precast
section

1-8" block at bottom

2-brick on top of rect. section



78+65 74' LT. 6-6-78
MH. storm R.M.



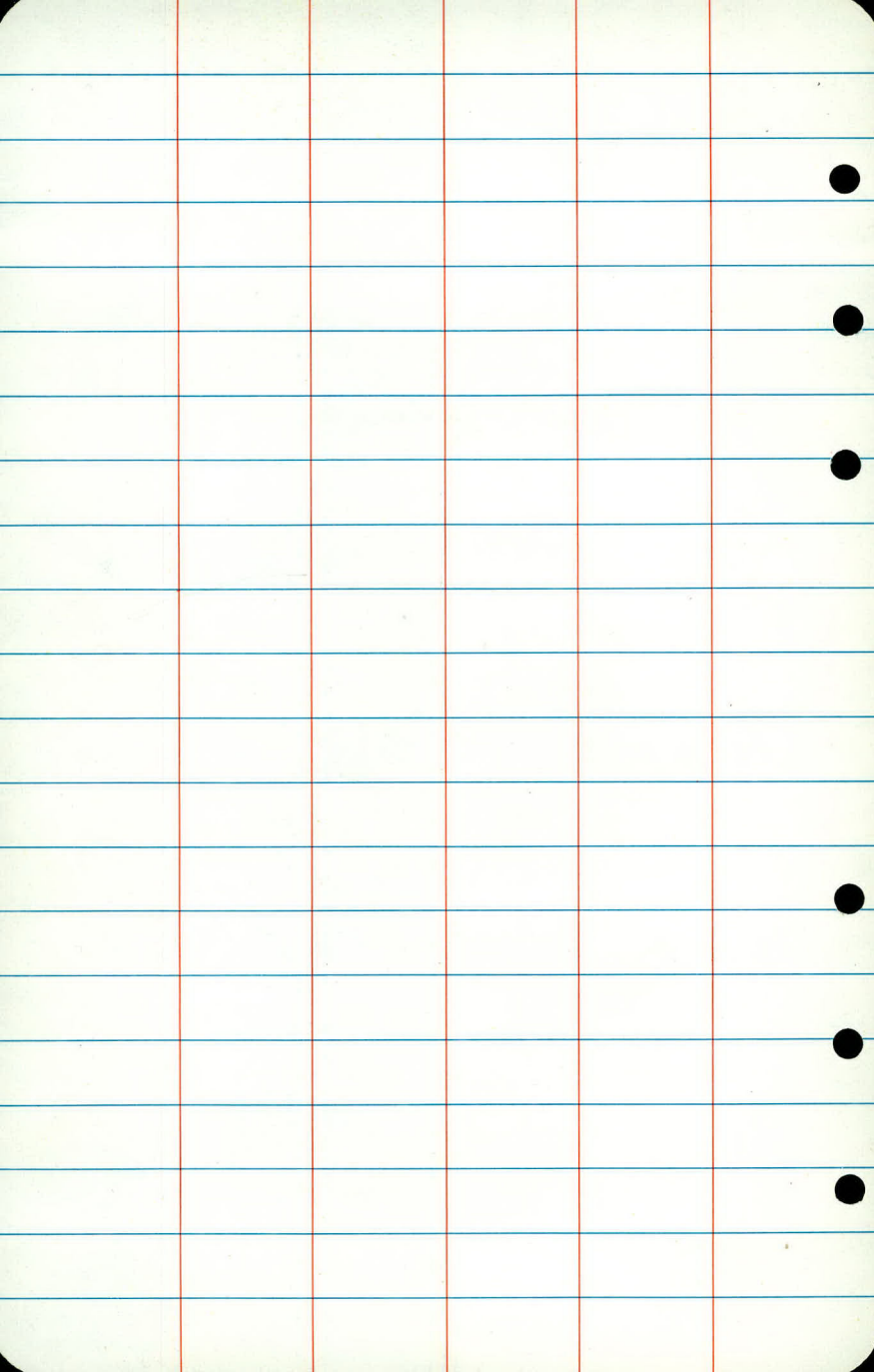
4'-9" pre cast section
Mexican Hat

11" casting

5 rings

7.45 to Inv. MH.

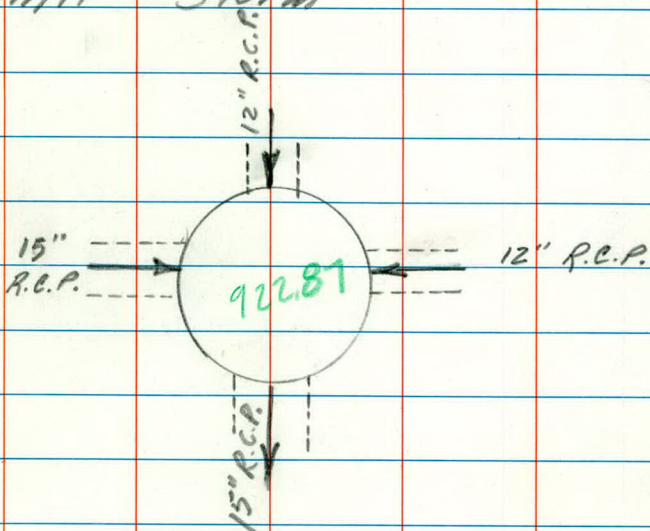
7.0 to Inv. pipe S.



78+65 RT 21

6-6-78
P.M.

MH Storm



1-2'-8" precast sections

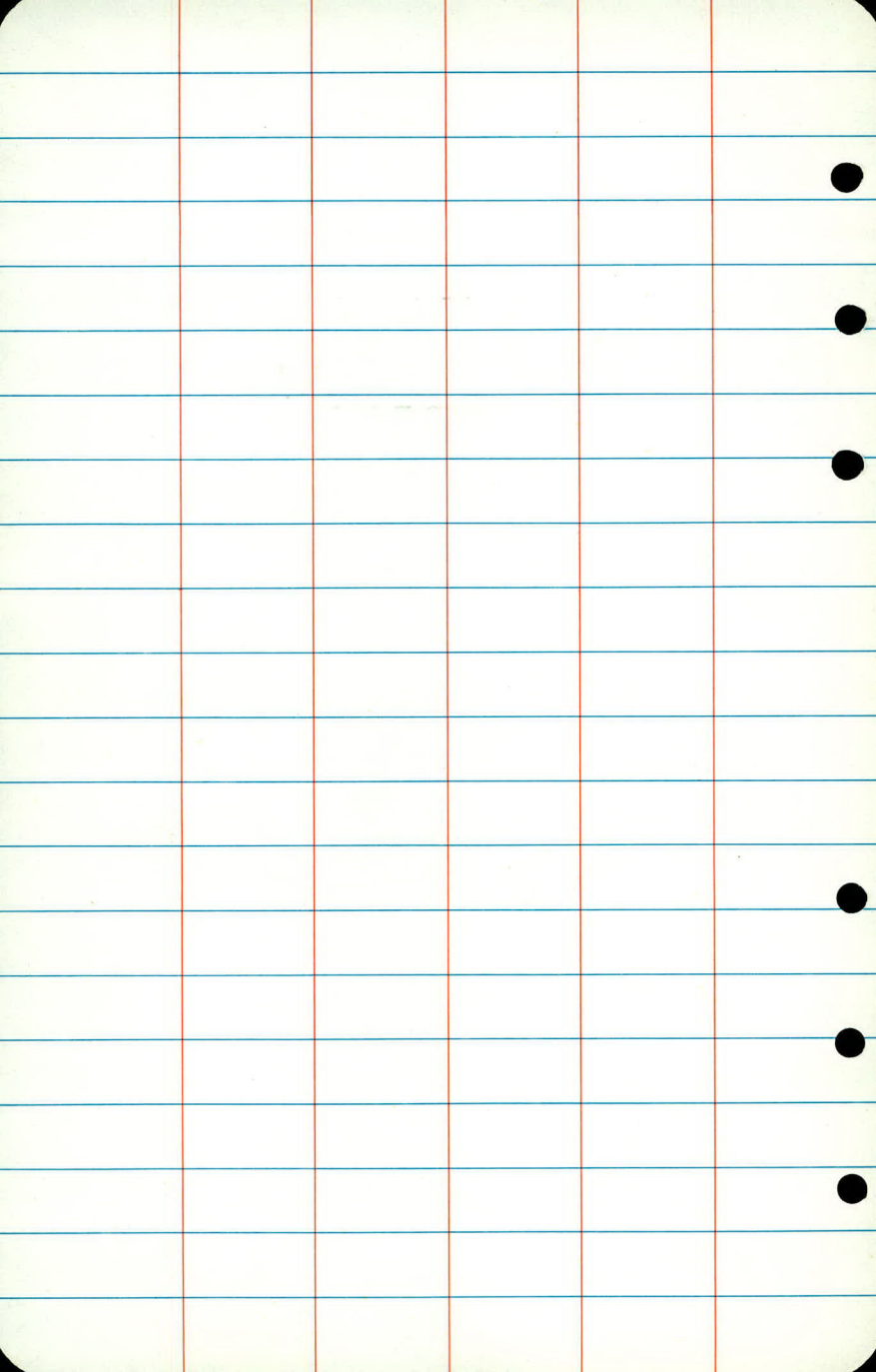
1-1'-9" " "

5 rings

11" casting

7.75 to Inv. MH.

Steps in MH.



78+65

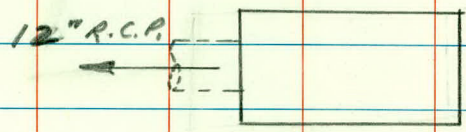
RT 73'

6-6-78

C.B.

Storm.

R.M.



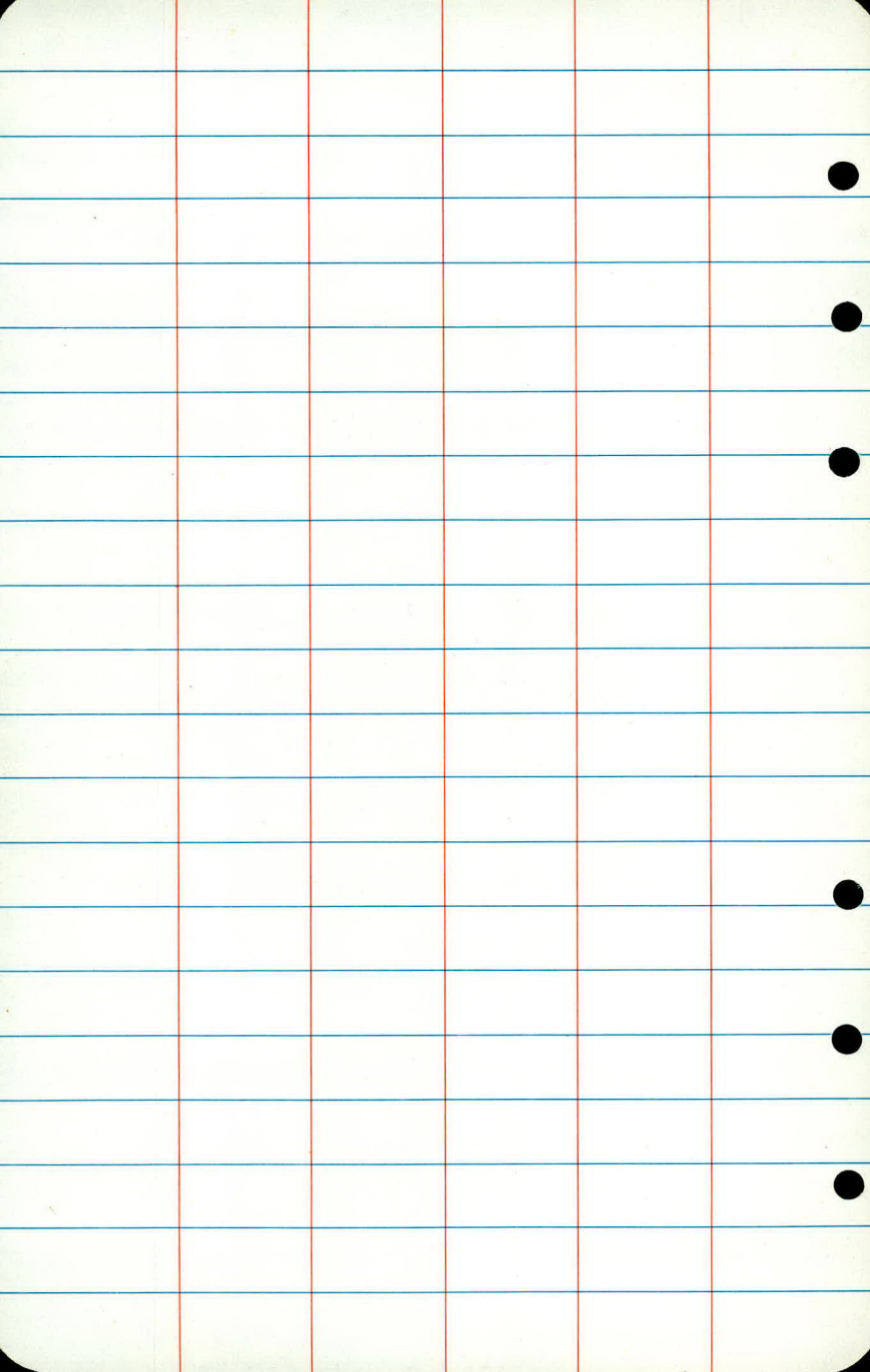
4 rows block

1-3' - 24" x 36" precast sect.

6" casting

1 row brick

6.96 to Inv. C.B.

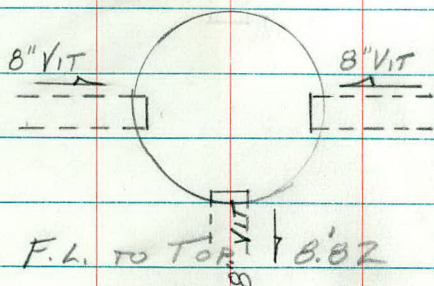


78+79

30' RT MH

9.

SANITARY



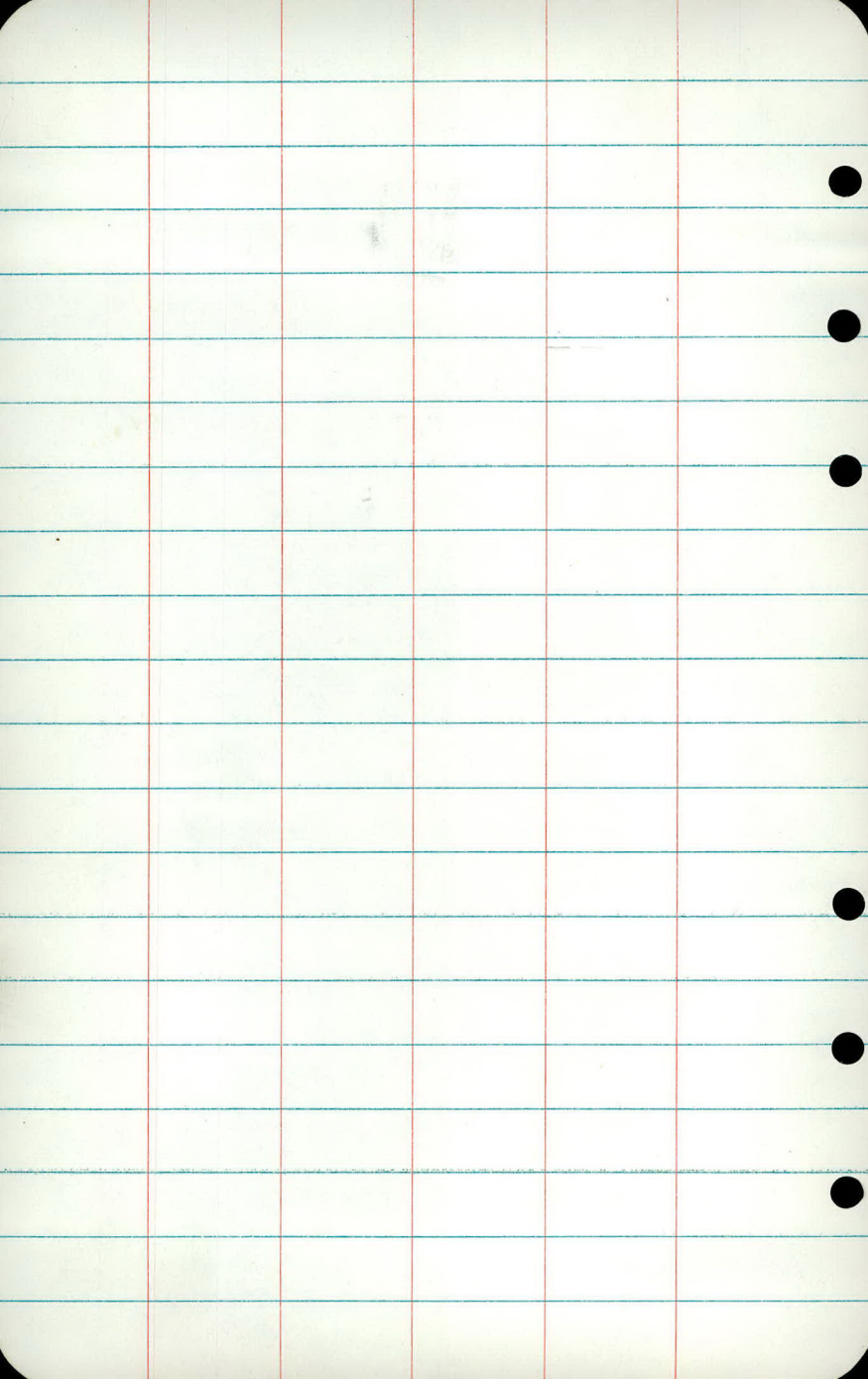
F.L. TO TOP 8.82

2.5 SECTION

4.5 ECC. CONE

3 RINGS

11" CASTINGS



78+97

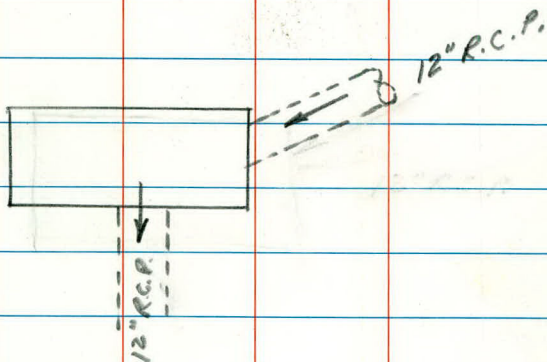
LT. 75'

6-6-78-

P.M.

C.B.

Storm



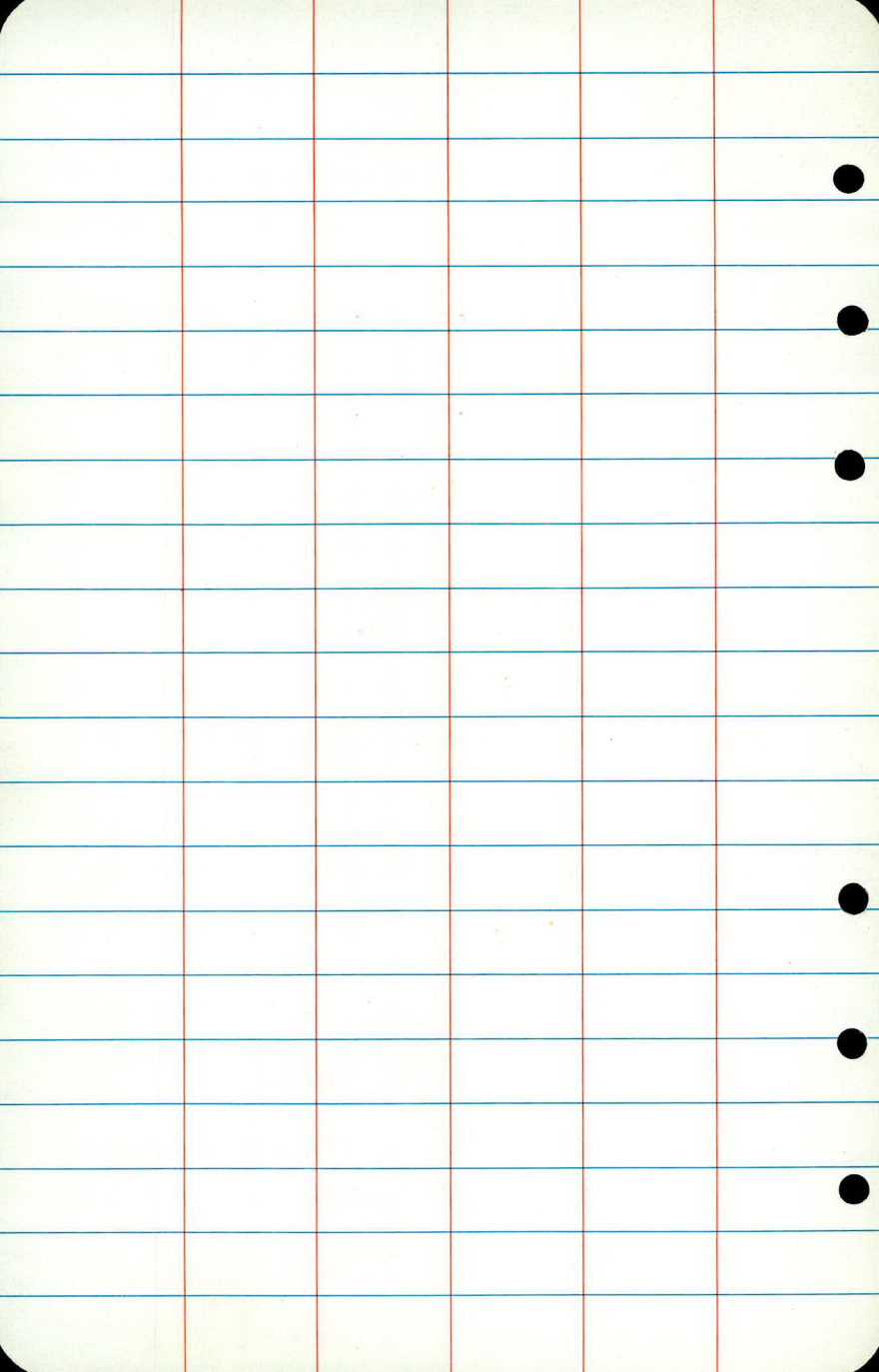
catch basin (rect) top
6" casting

4' - 24" x 36" rect. precast section

2- rows brick at bottom

4 rows " at top.

6.58' to Inv. C.B.

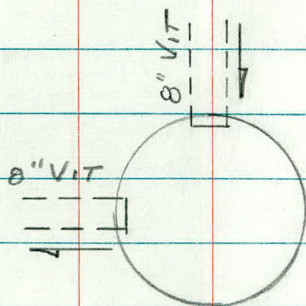


79+03

38' LT MH

10.

SANITARY



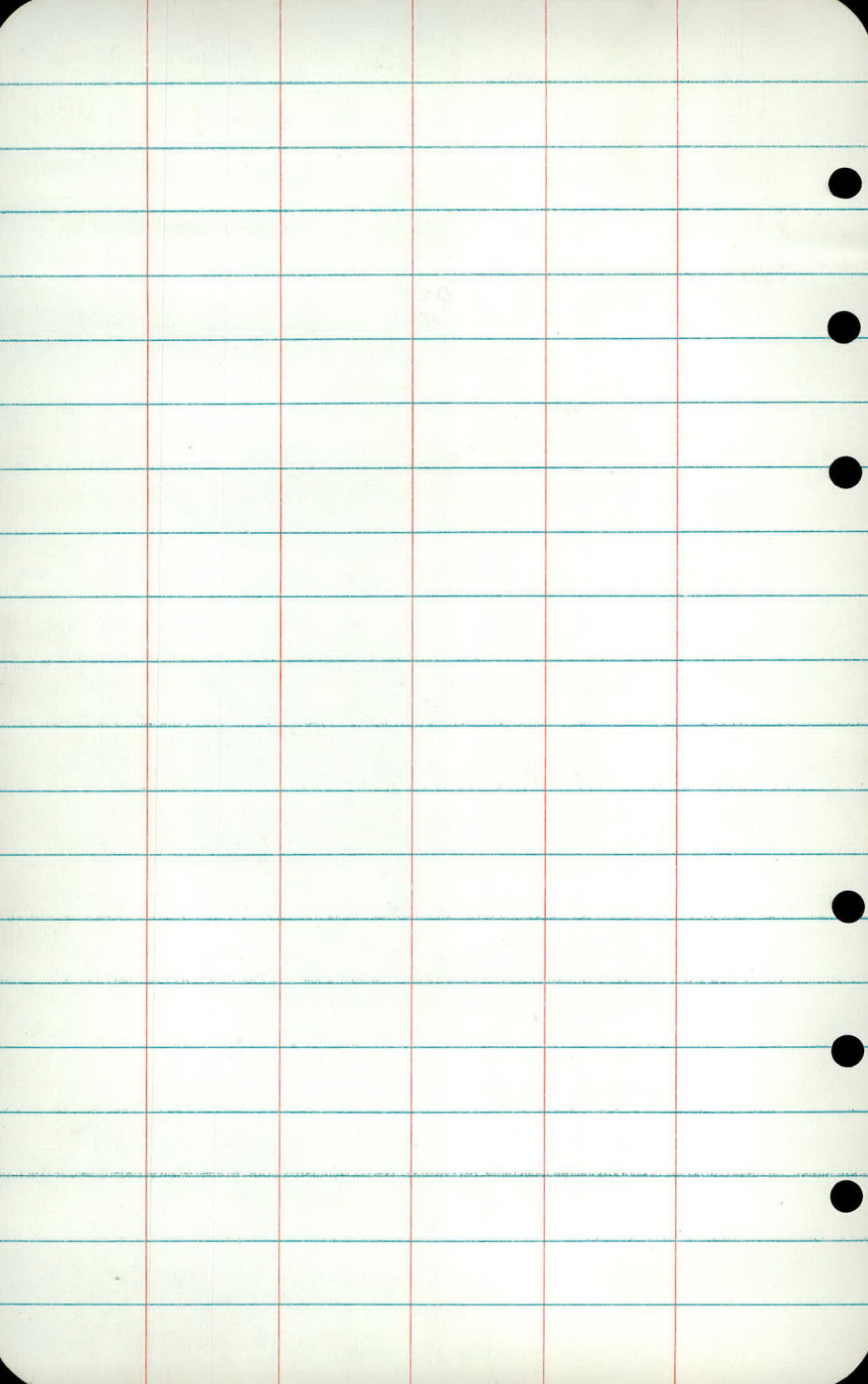
F.L. TO TOP 7.00

0.5 BLOCK CONST.

4.5 ECC. CONE

0.5 BLOCK CONST.

11" CASTING



79+13

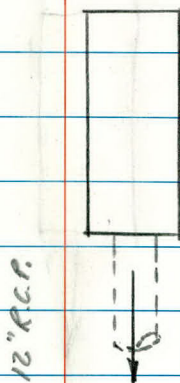
Rt. 24'

6-6-78

C.B.

Storm

P.M.



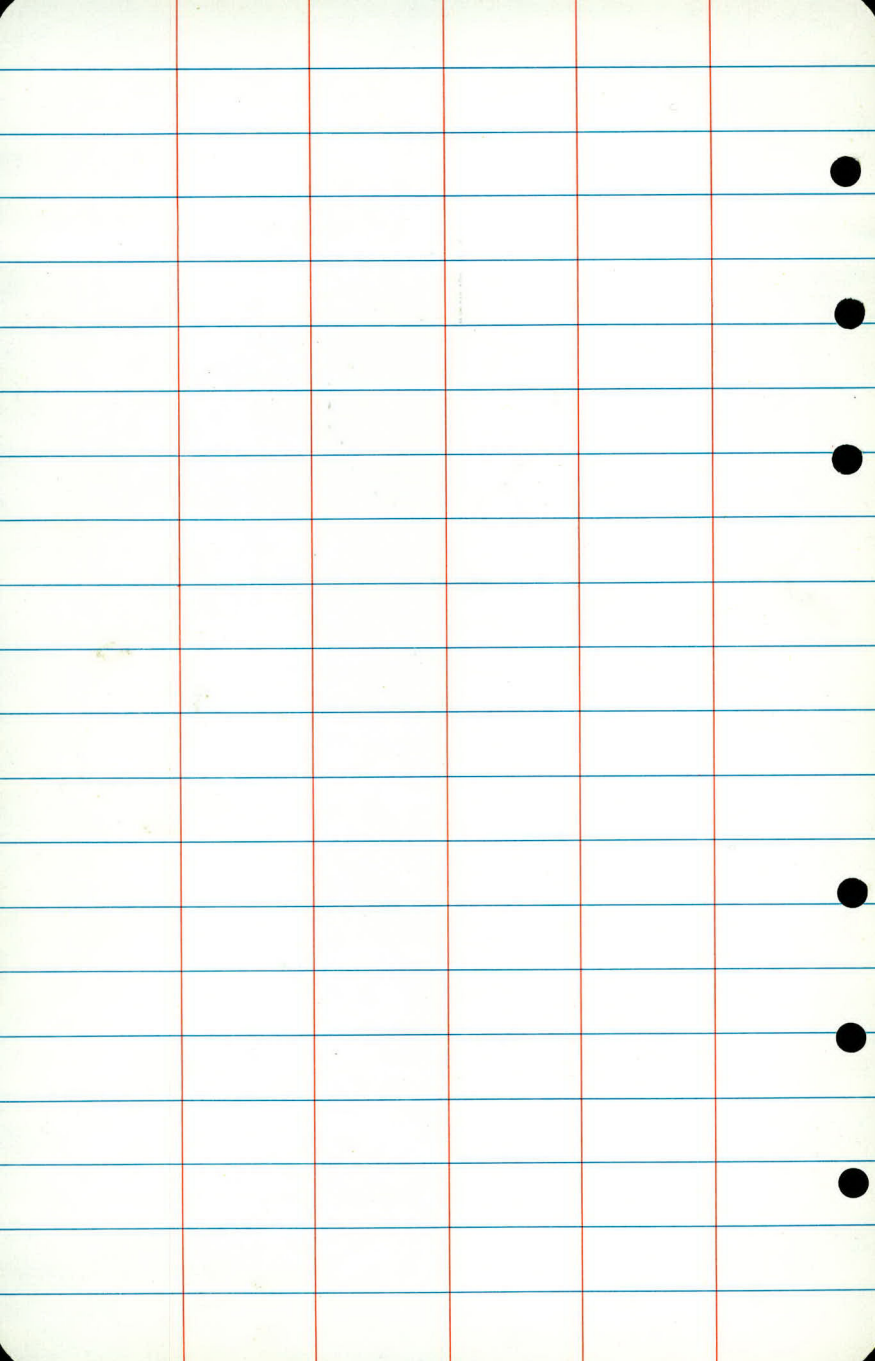
C.B. rect. top

4 rows 8" block

6" casting

36" - 24" x 36" precast section

6' to Inv. C.B.



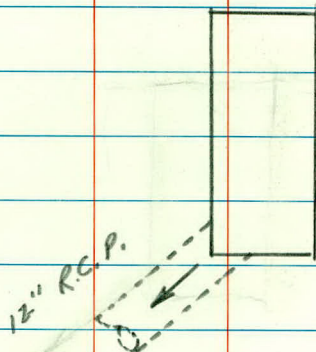
79+19 LT 25'

6-6-78

C.B.

Storm.

R.M.



6" casting

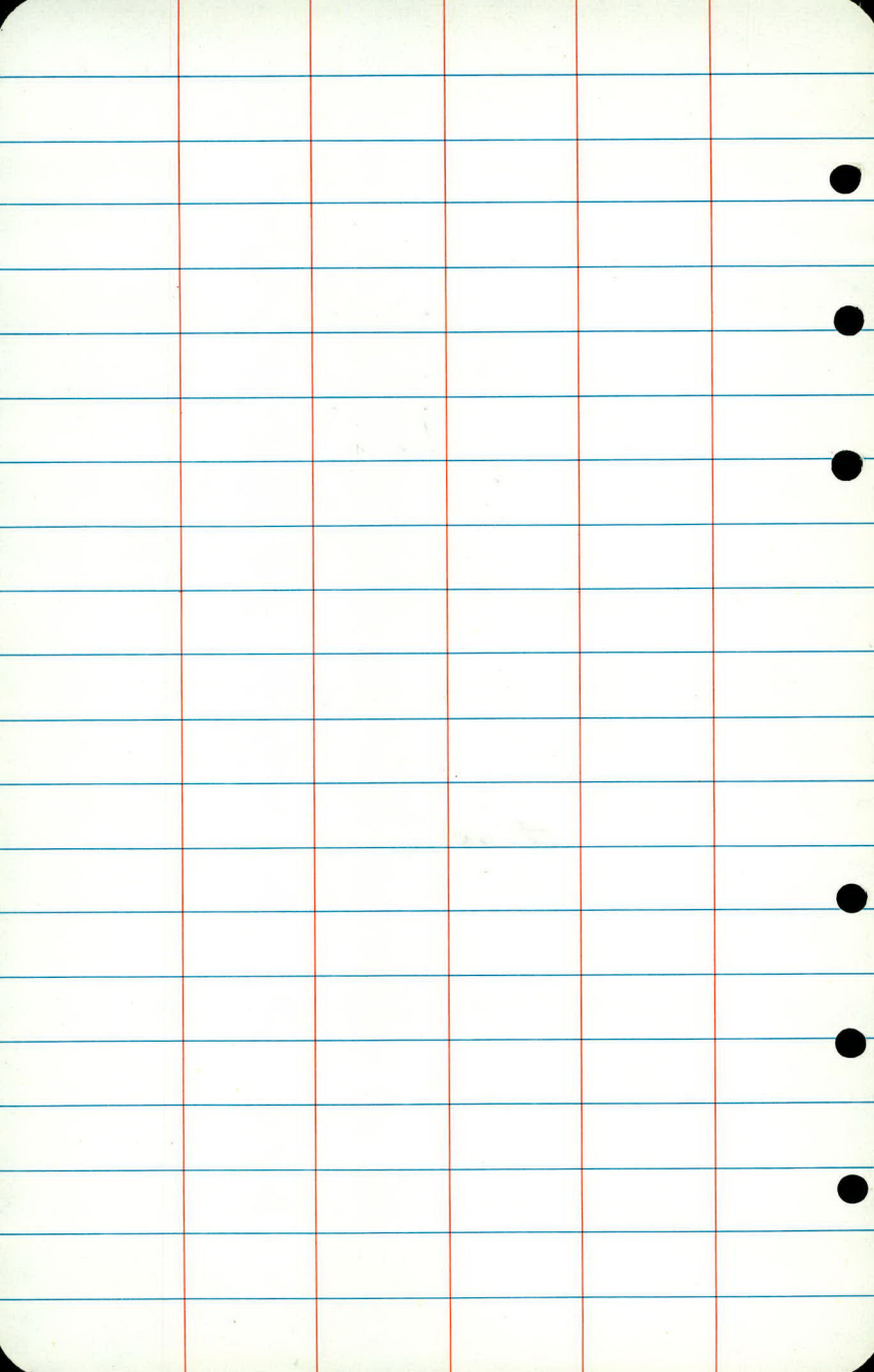
C.B. (rect.) top

1- 28" pre cast section 24"x36"

1- 8" block

2 rows brick

4.2' to Inv. C.B.

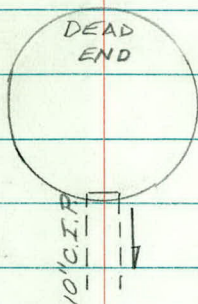


81+34

37'
~~44'~~ LT MH

11.

SANITARY



F.L. TO TOP 10.87

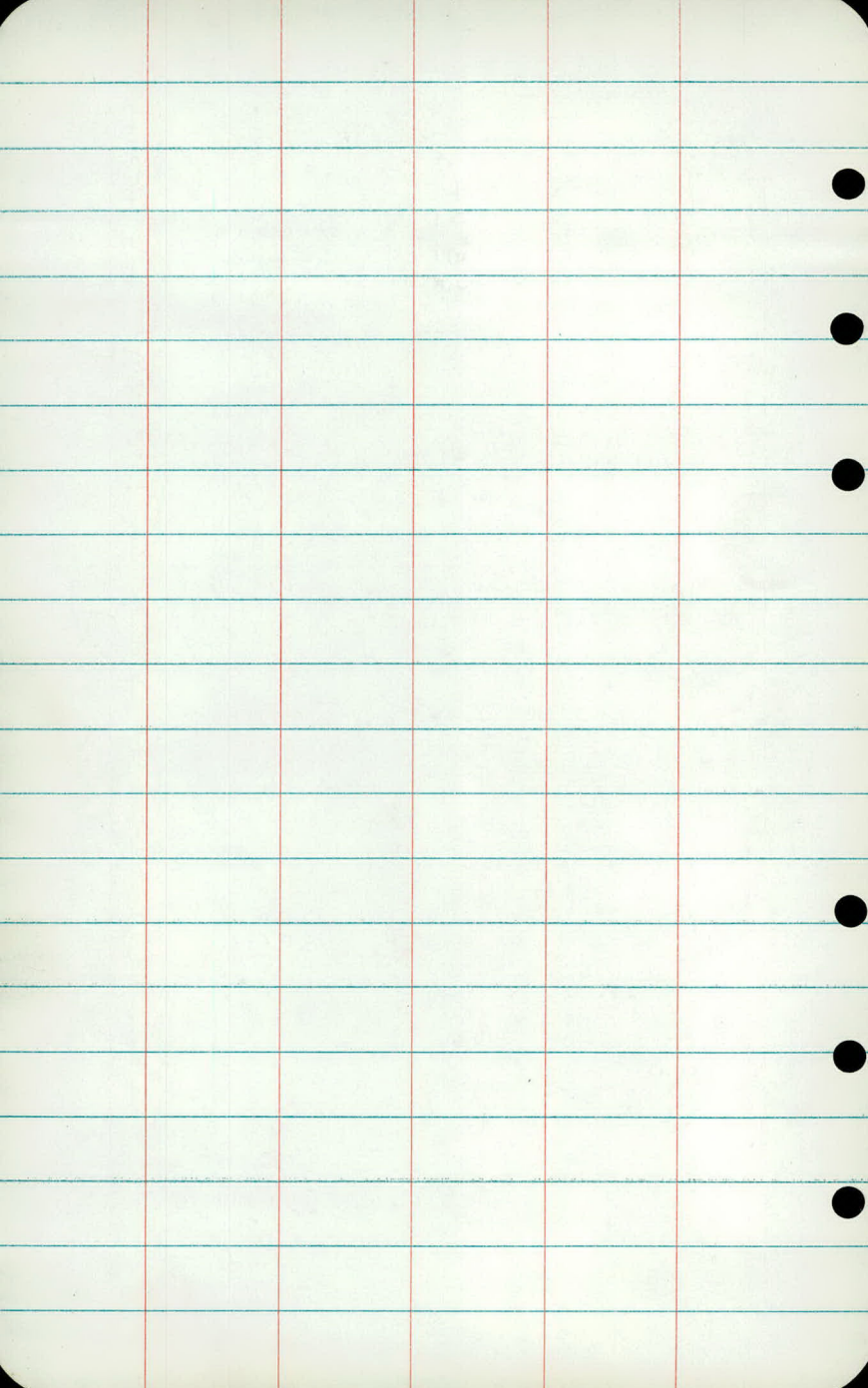
1.5 SECTION

2.3 SECTION

4.5 ECC CONE

1 RING

11" CASTING

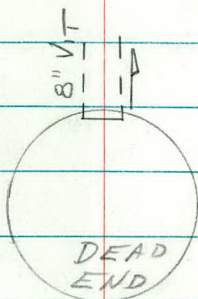


81453

36' RT MH

12

SANITARY



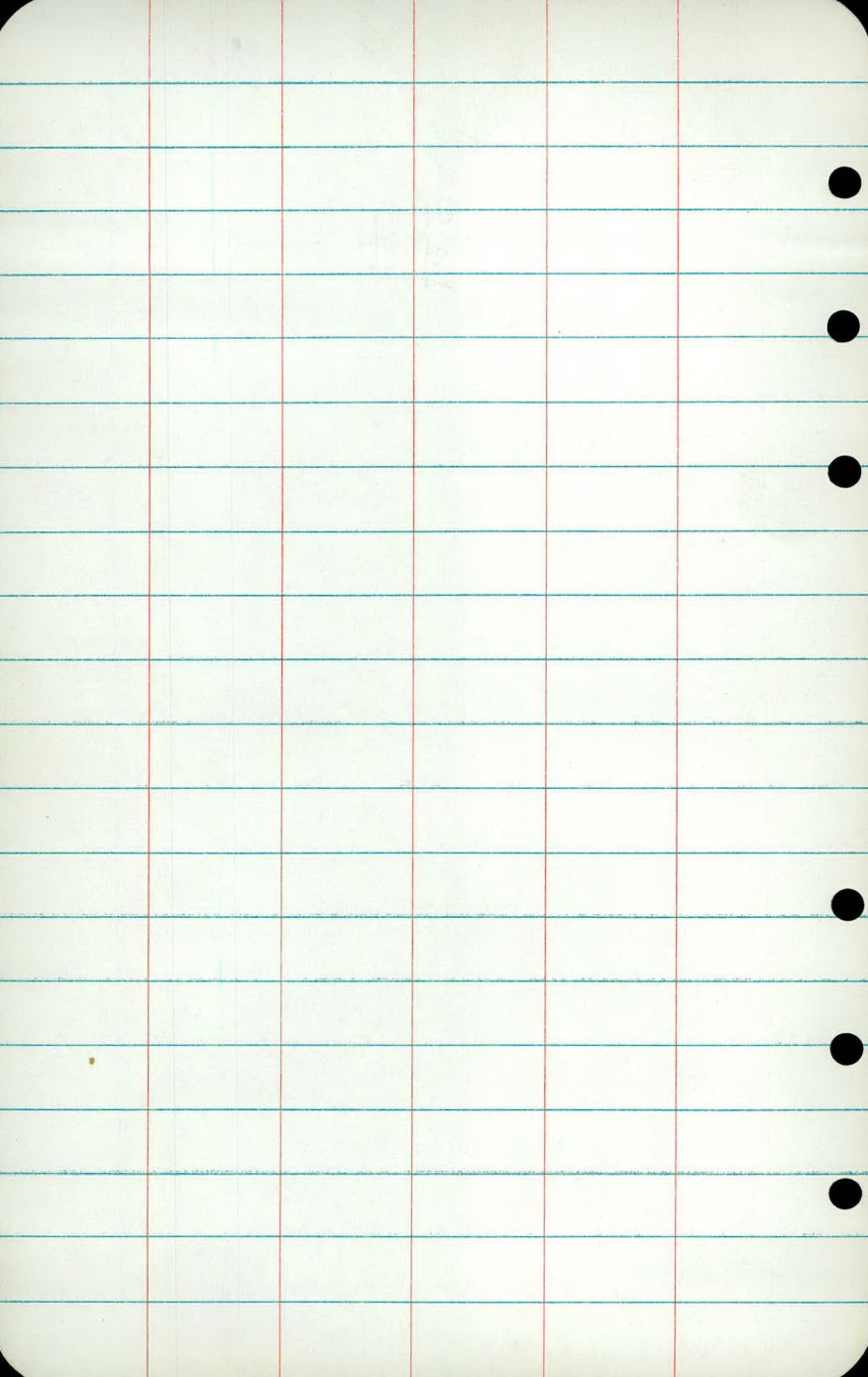
FL. TO TOP 9.37

3.3 SECTION

4.5 ELL CONE

1 RING

5" CASTING

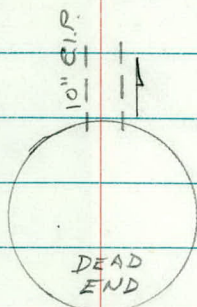


82+86

37' LT MH

13

SANITARY



F.L. TO TOP 10.73

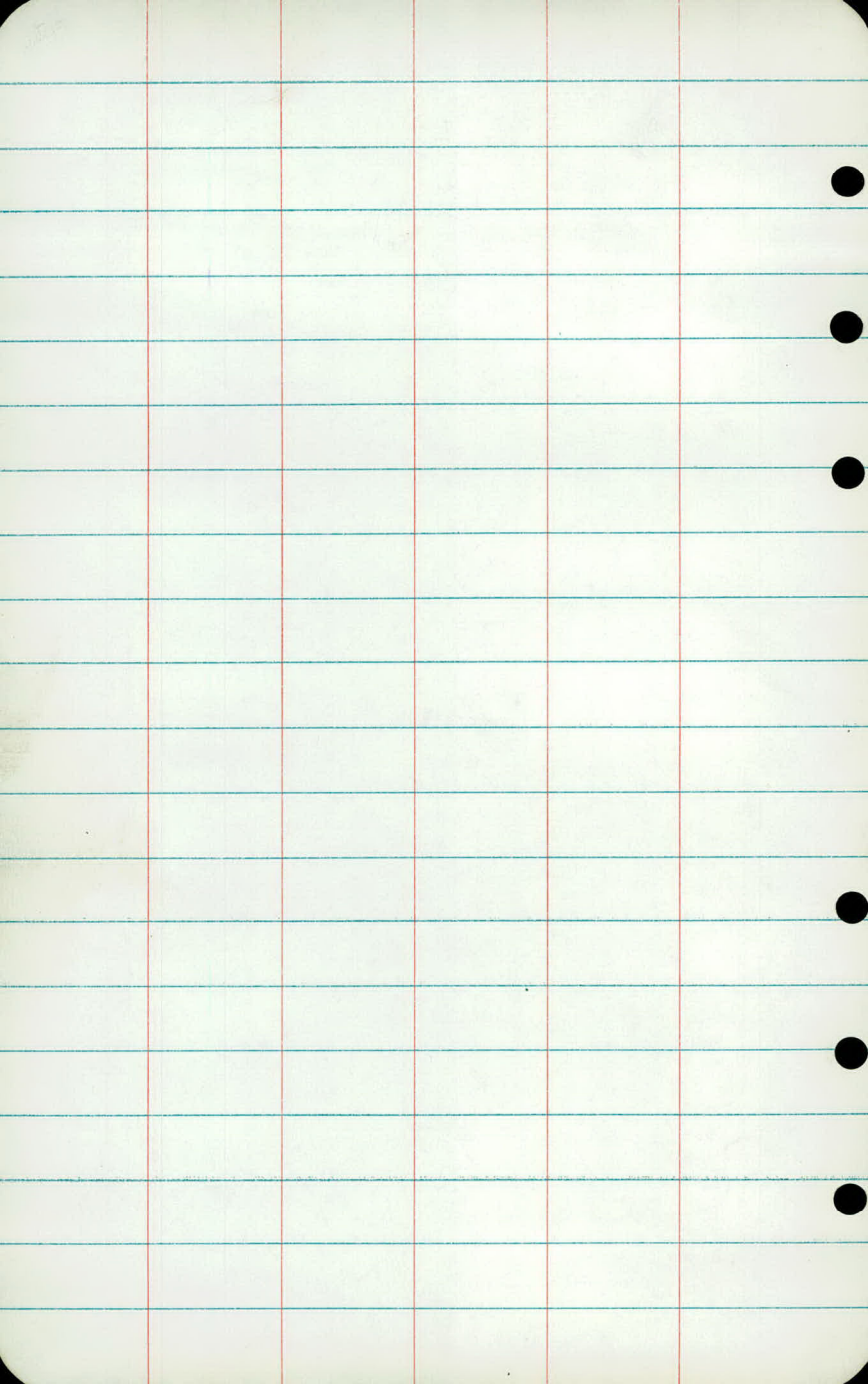
2.9 SECTION

1.4 SECTION

4.5 ELL. CONE

4 RINGS

11" CASTING



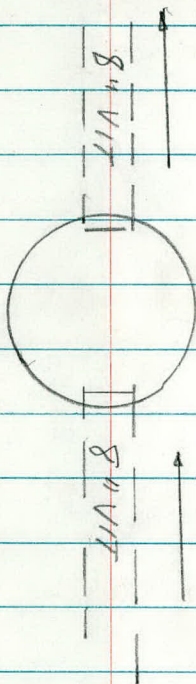
84+90

37' RT

MH

13A

Sanitary



FL TO TOP = 9.22

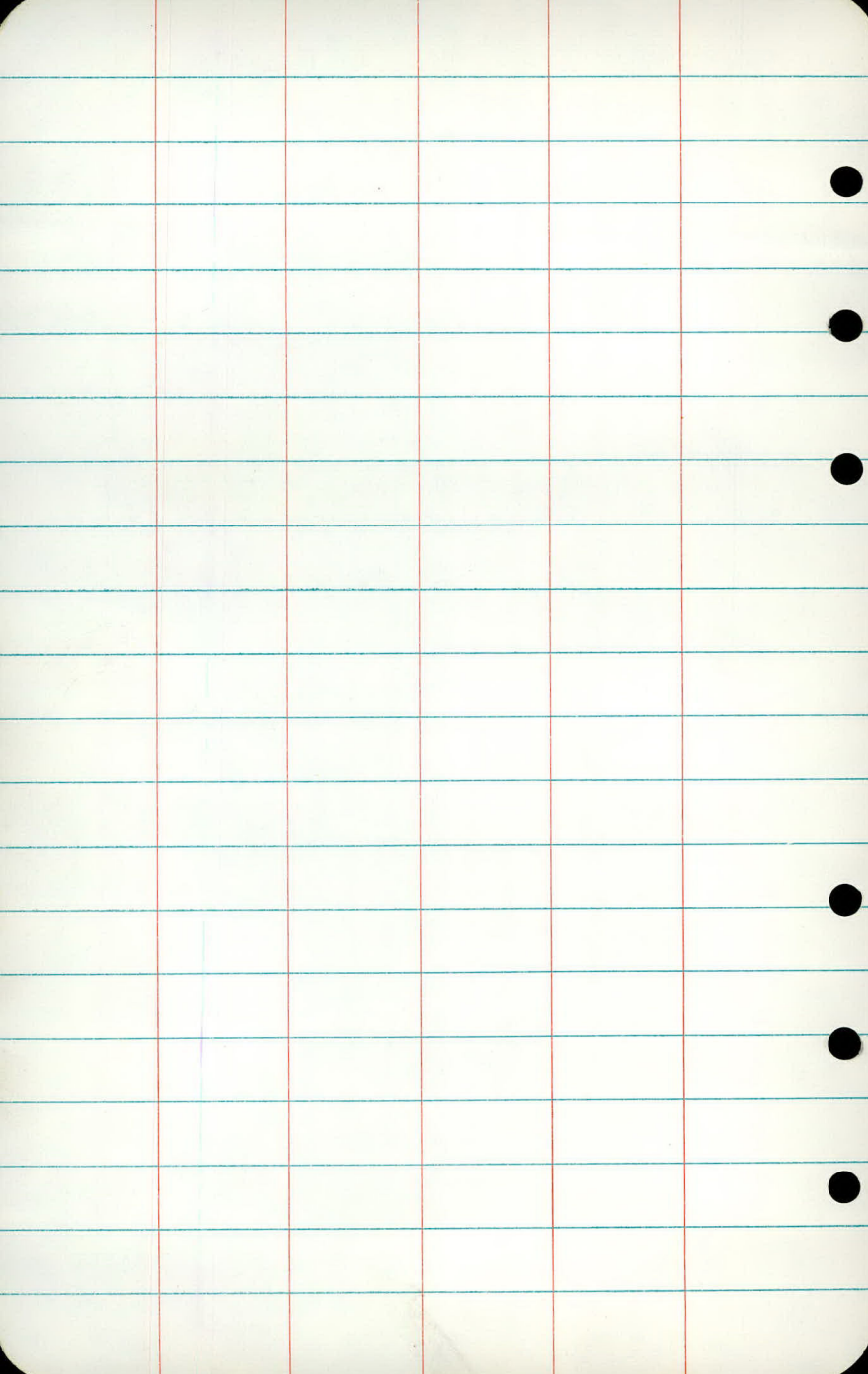
2'2 SECTION

1'8 SECTION

4'5 ECCENTRIC CONE

1 RING

11\"/>

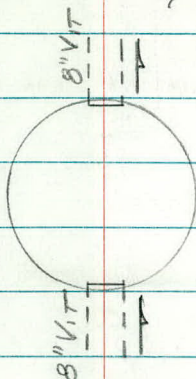


85+24

38' LT MH

14

SANITARY



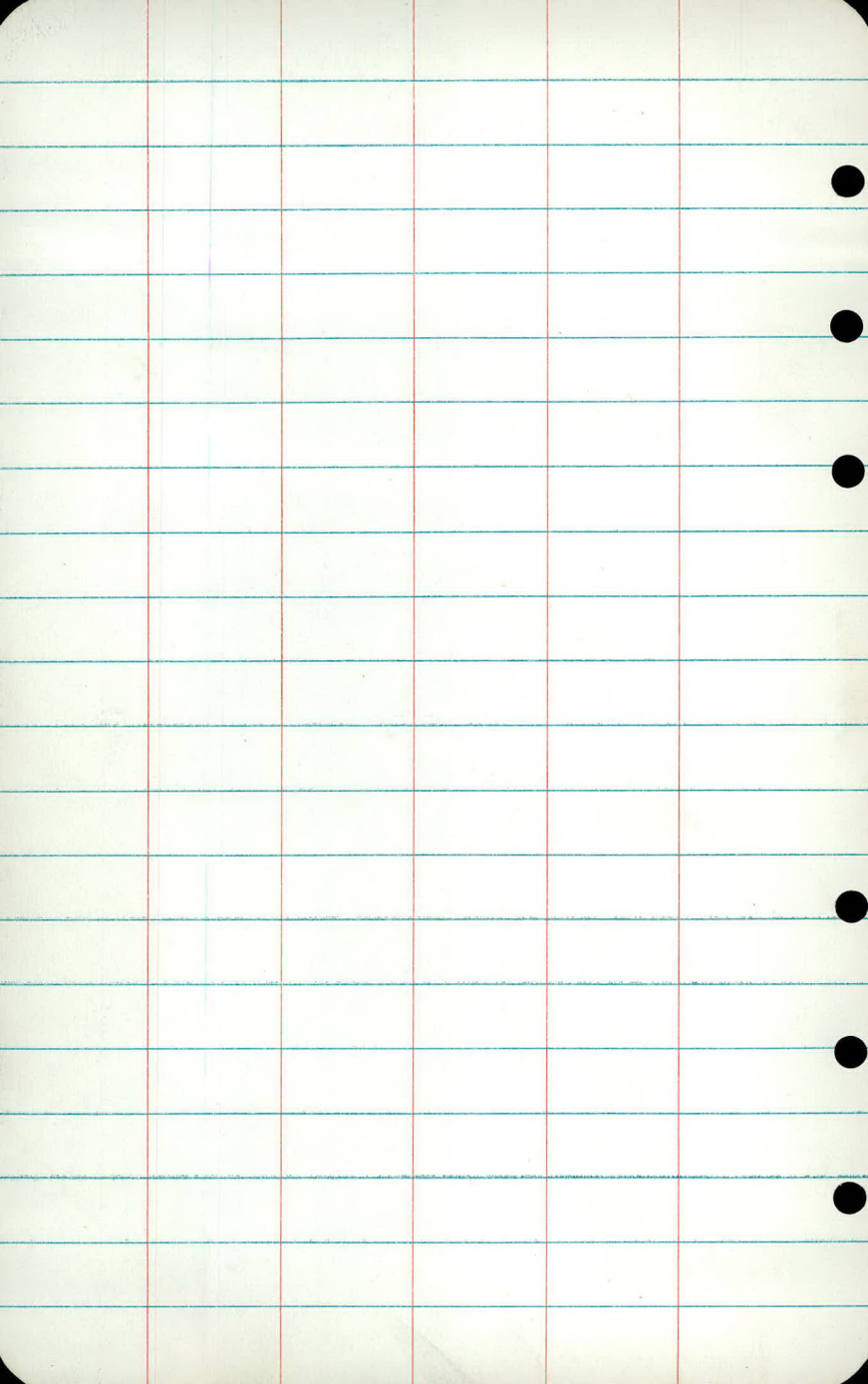
F. L. TO TOP 9.88

3'3 SECTION

4.5 ECL CONE

4 RINGS

11" CASTING

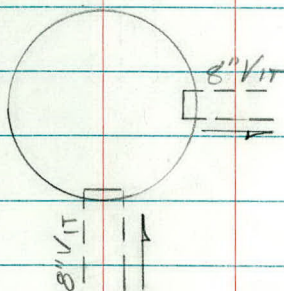


88+46

37'R7 MH

15

SANITARY



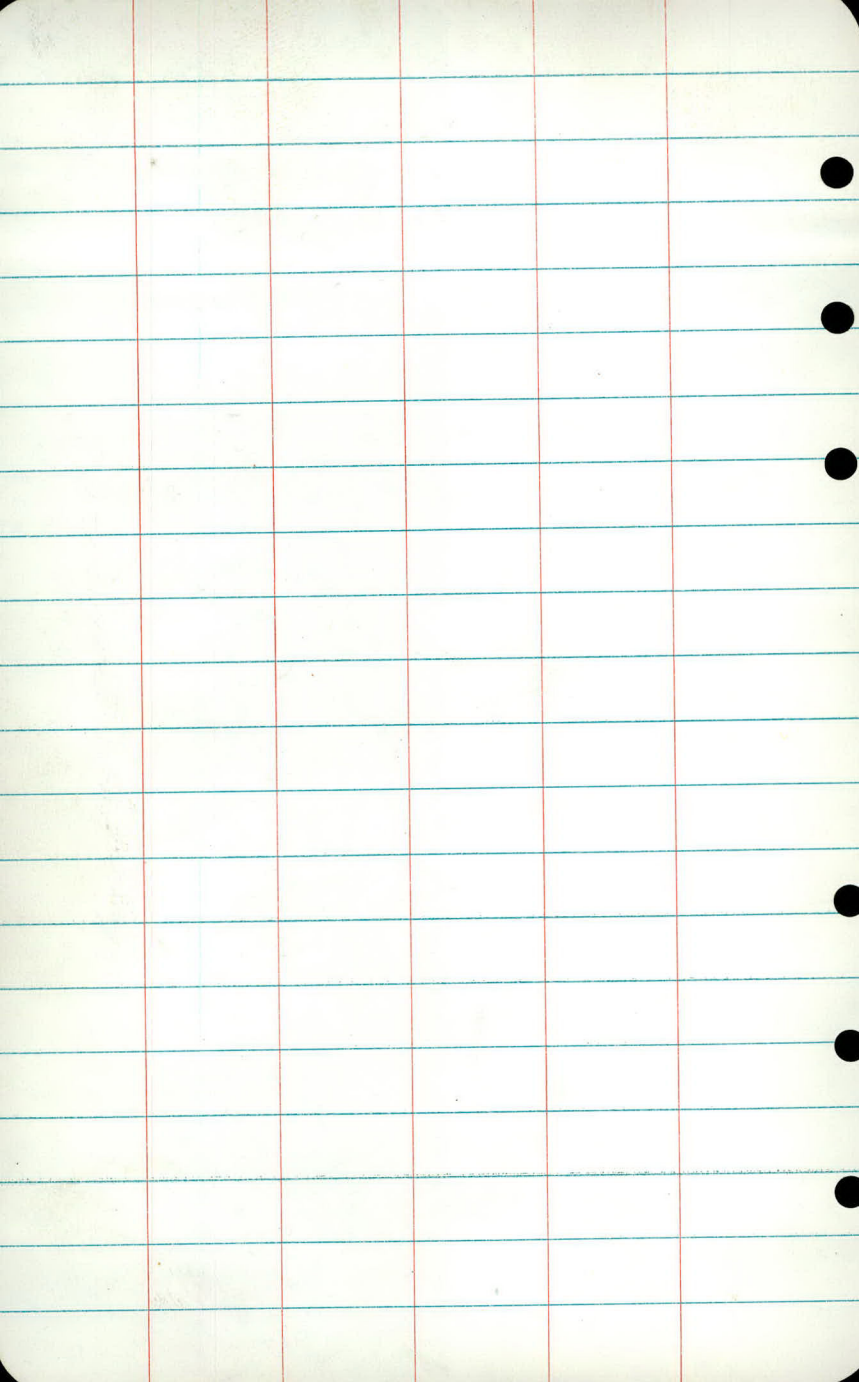
F.L. TO TOP 9.91

3.3 SECTION

4.5 ELL CONE

11" CASTING

NO RINGS

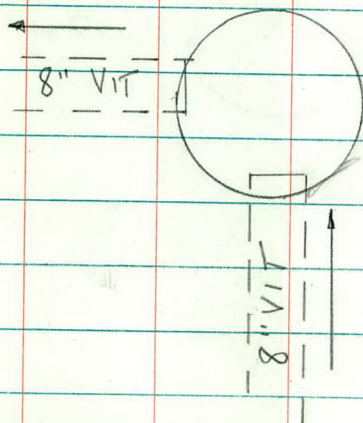


88+46

38' LT MH

15A

SANITARY



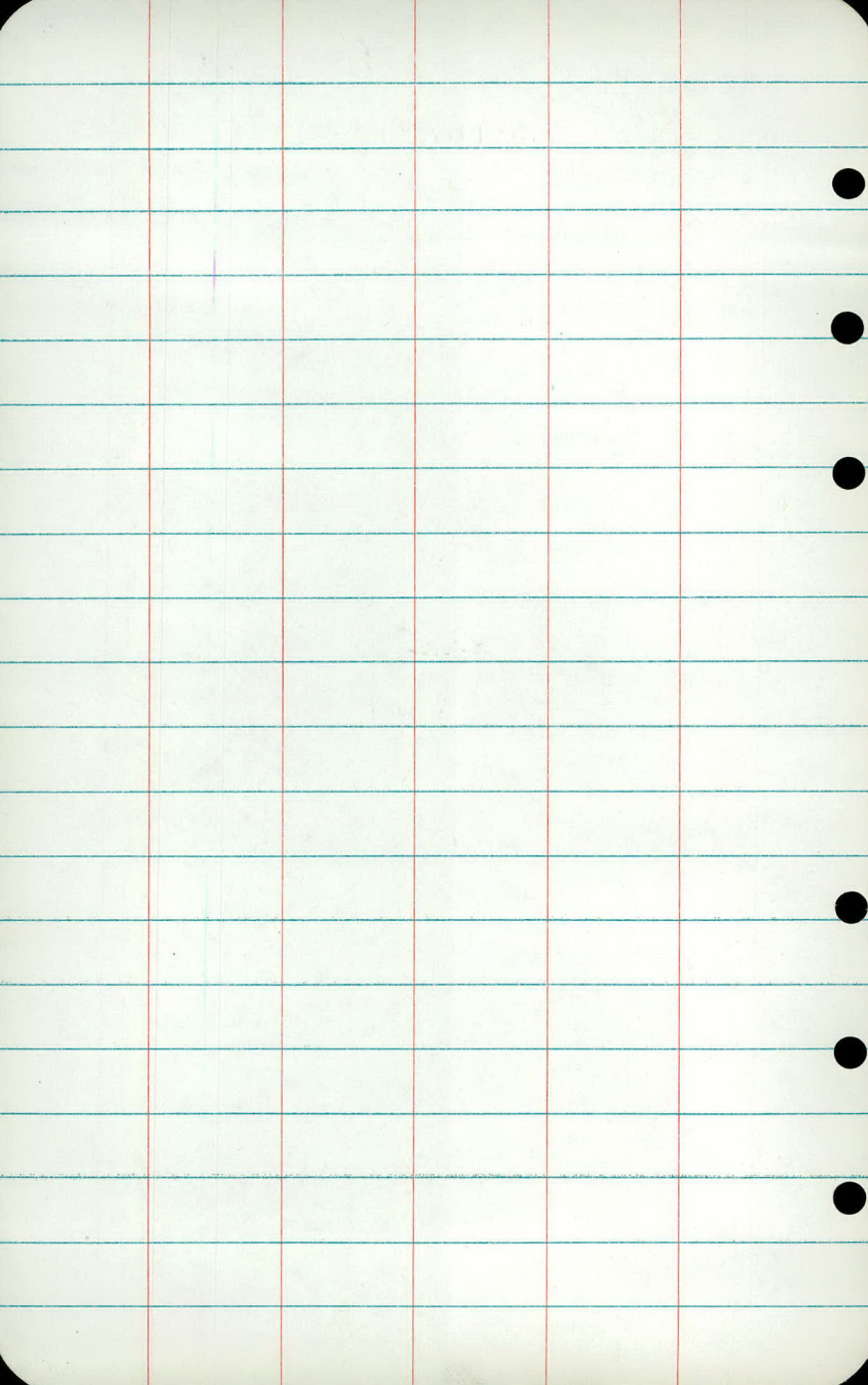
FL TO TOP = 9.00

2'0 SECTION

4'5 ECCENTRIC CONE

4 RINGS

11\"/>

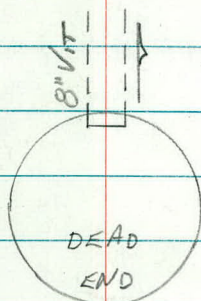


90+24

38'LT MH

16

SANITARY



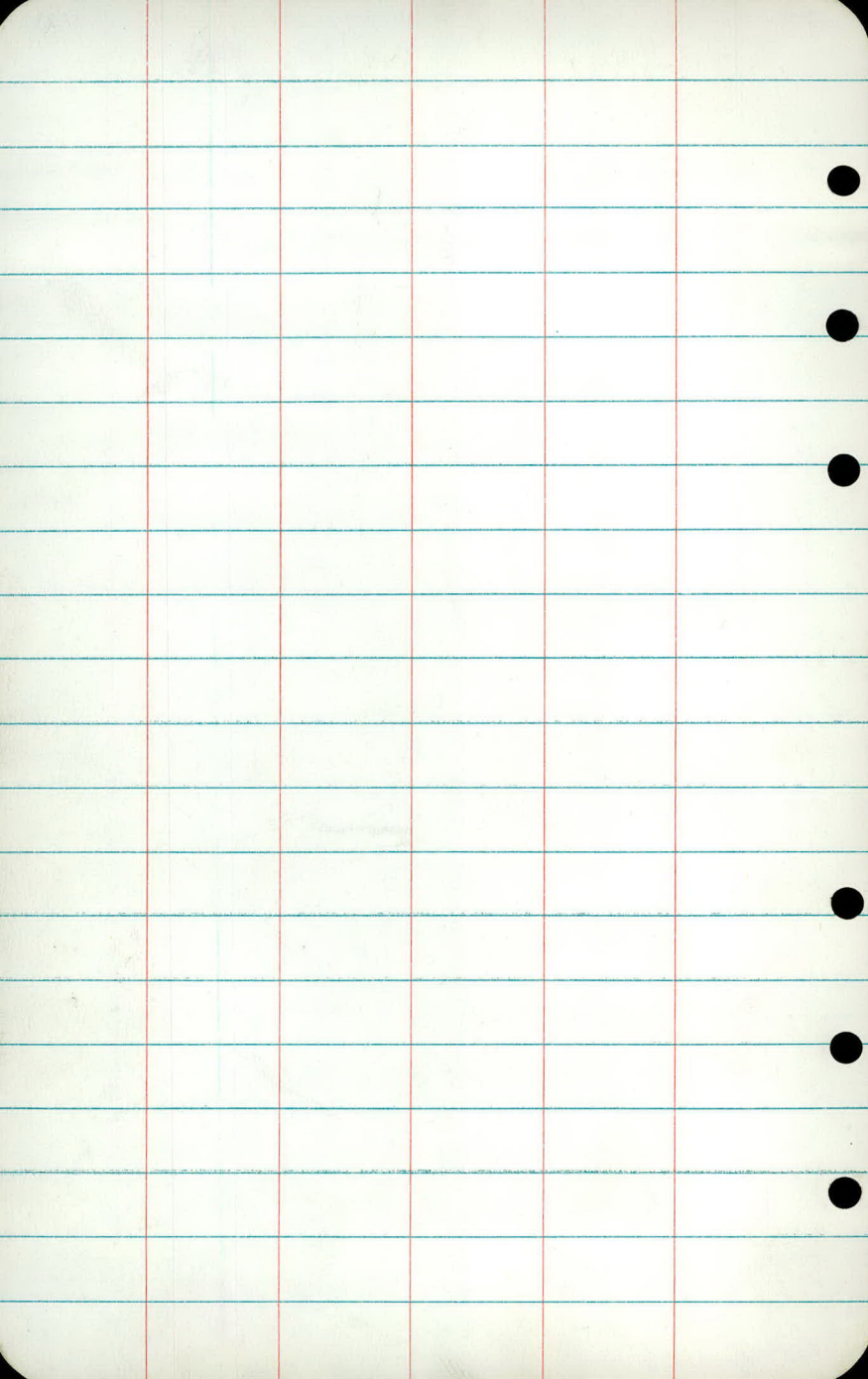
F.L. to Top 8'48

2'0 SECTION

4'5 ECL CONE

2 RINGS

11" CASTING



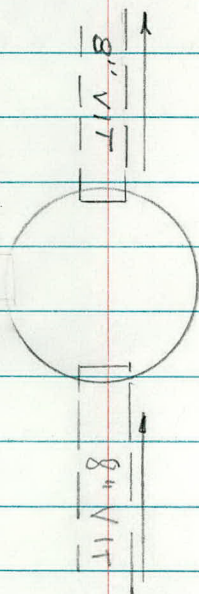
+15
91+20

37' LT

MN

16A

SANITARY



FL TO TOP = 9.56

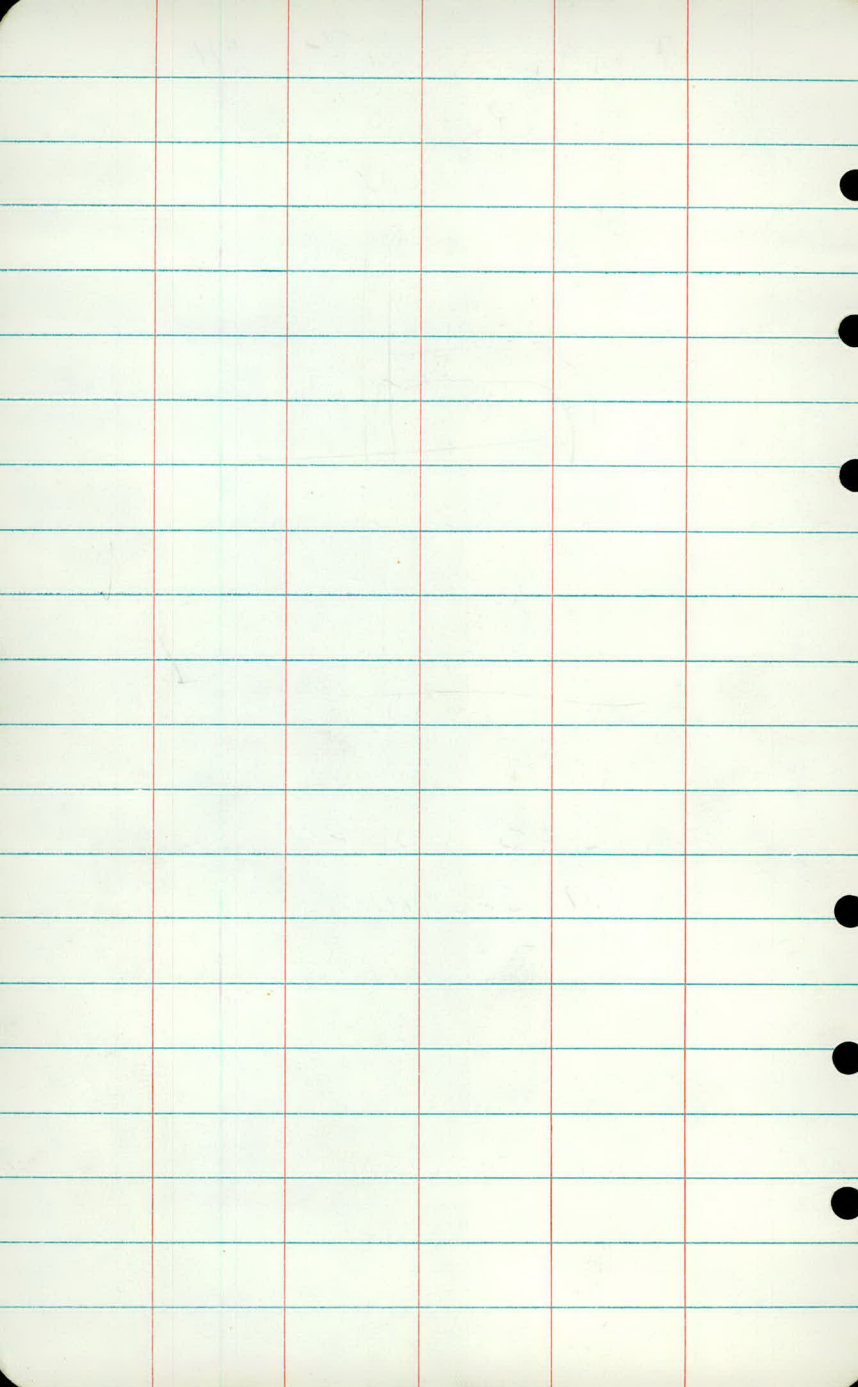
1.7 SECTION

4.5 CONCENTRIC CONE

5 RINGS

11" CASTING

1.4 SECTION

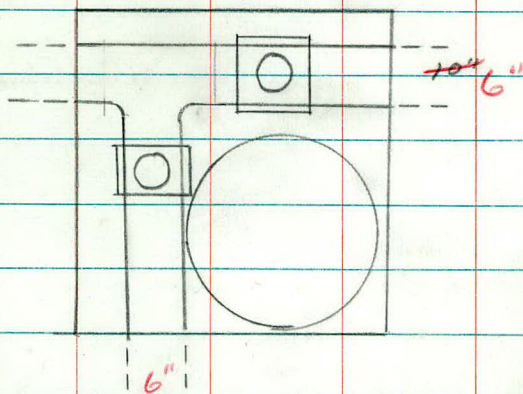


94+00

46' LT MH

17.

~~WATER~~ GAS RW 5-3-78



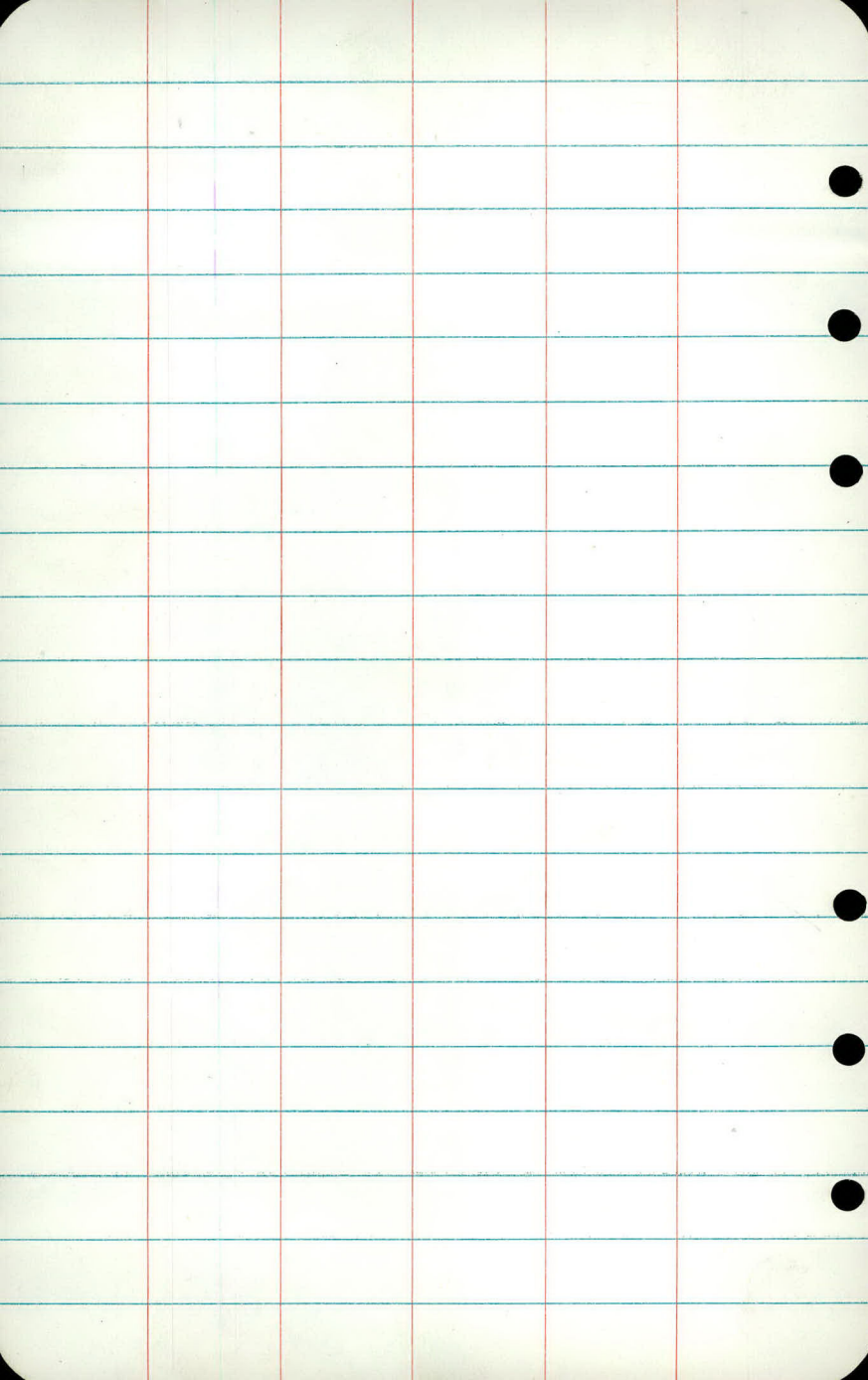
6' 33" ~~8"~~ BOTTOM TO TOP

BLOCK CONST.

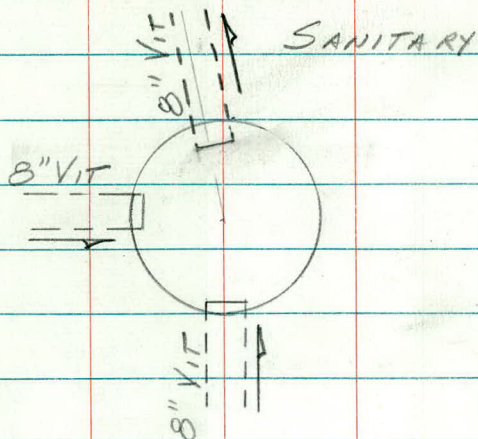
1' MEXICAN HAT

2 BRICK RINGS

11" CASTING



94+15 M.H. 38' L



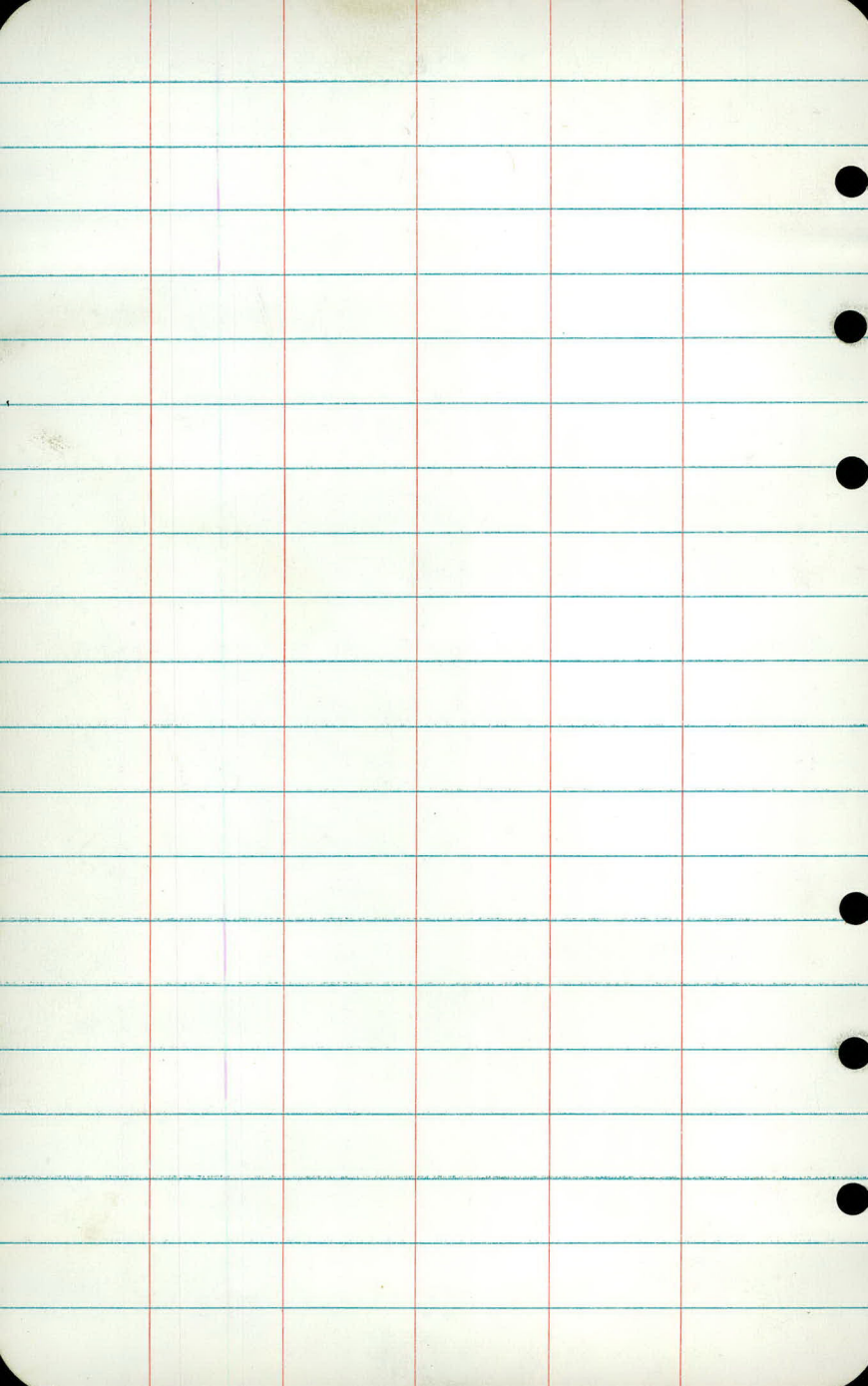
F.L. TO TOP 7'60

1.2 SECTION

4.5 ECL CONE

2 RINGS

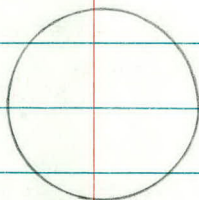
11" CASTING



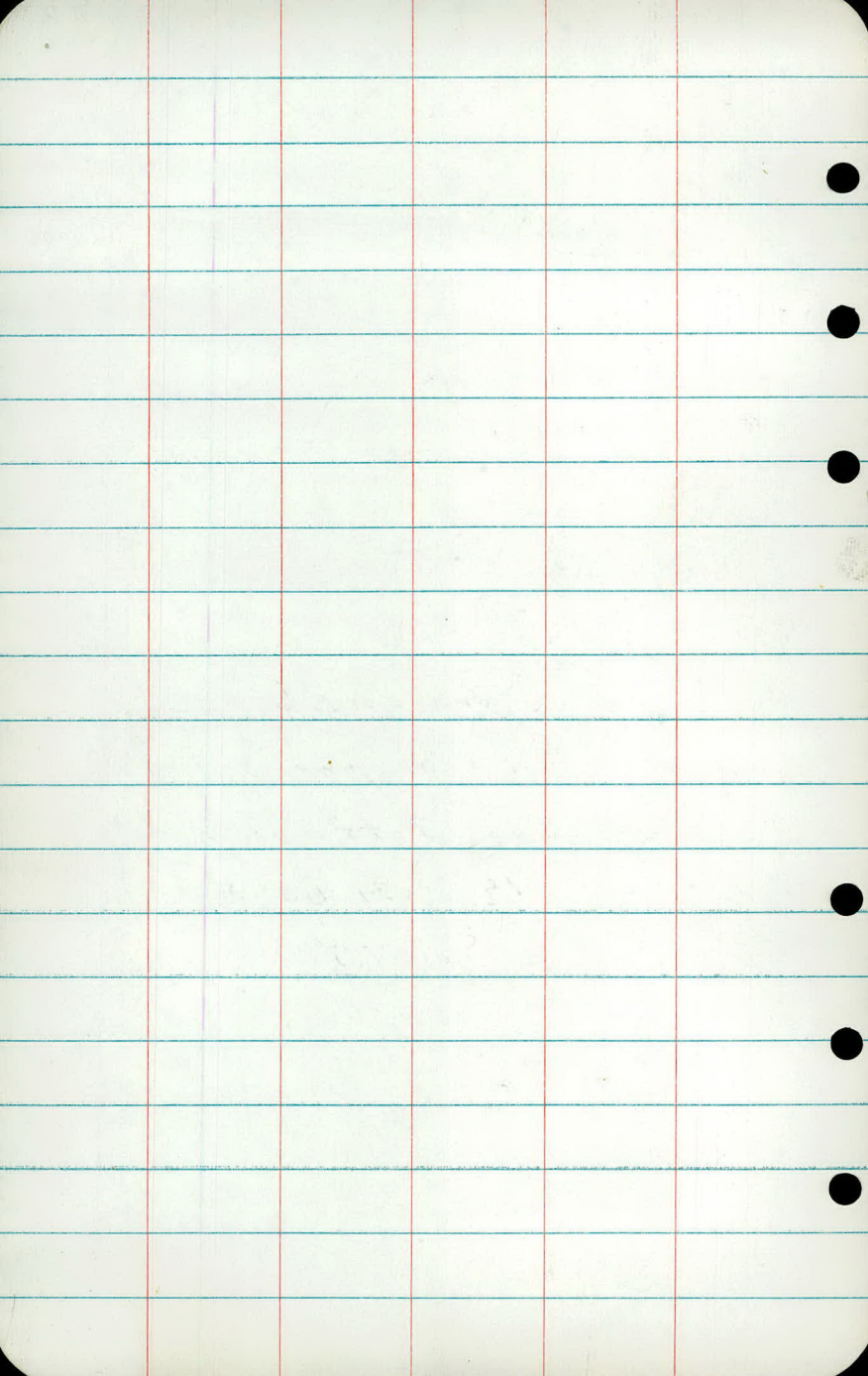
95+07

Rt 33' MH
Rt 30'-33'?

18A



Can not find. Must
be under blacktop
entrance to park down
approx. 3 ft. as per
as-builts. As-builts show
MH to be 67' Ely of
MH. at 95+08, 40' Lt..

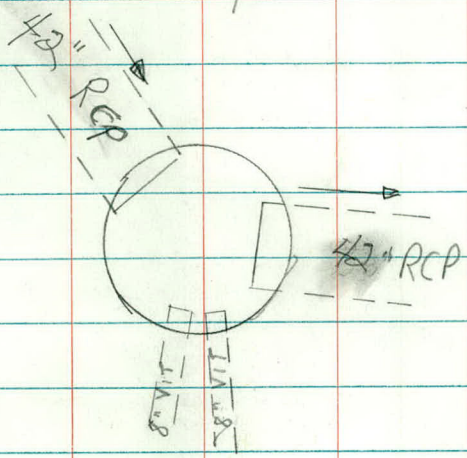


95+08

40' LT

MH

Sanitary



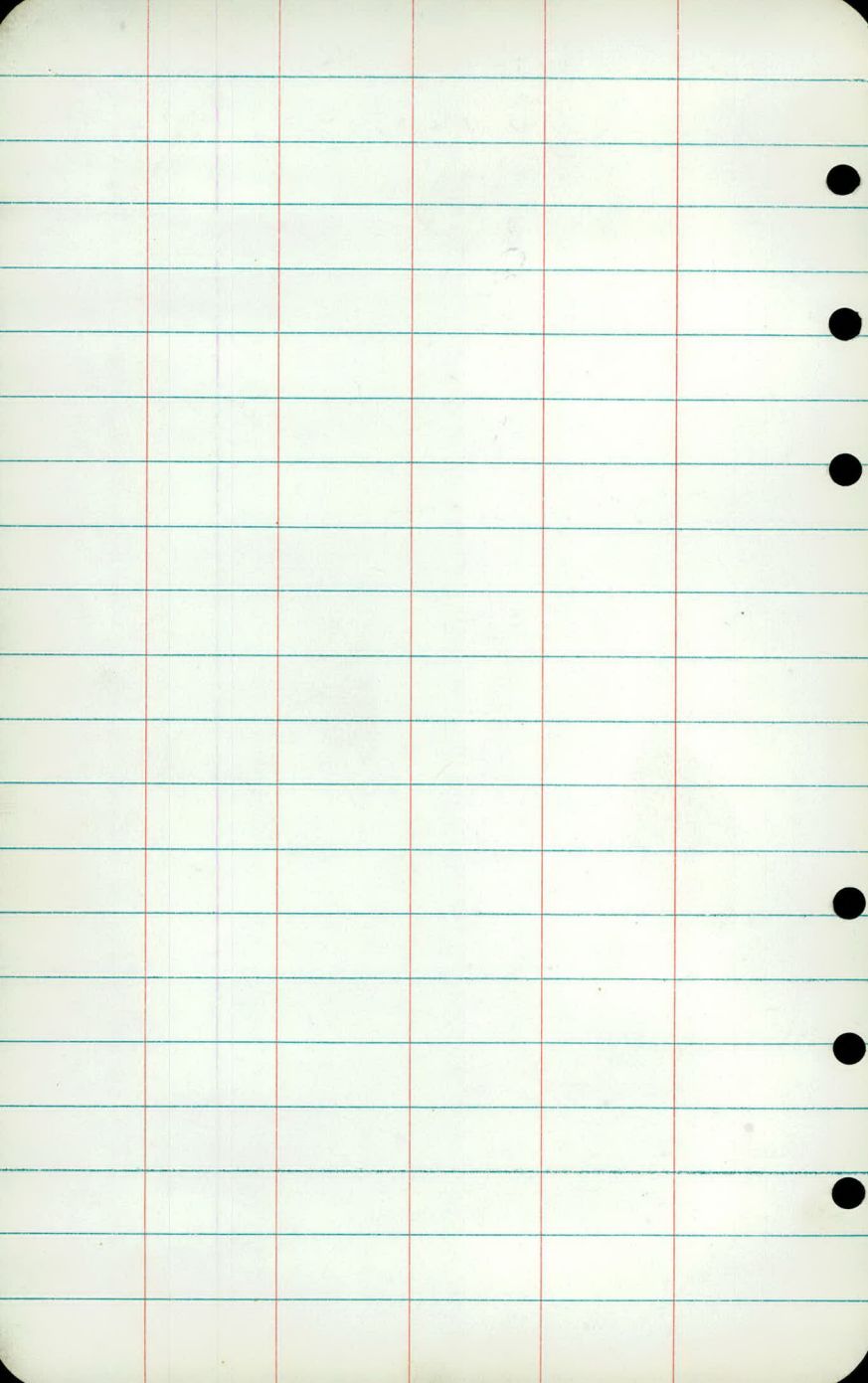
FL TO TOP = 15.15

4.5 SECTION

3.8 ECCENTRIC CONE

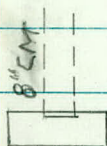
4.5 ECCENTRIC CONE

11" CASTING



96+50 S.D. 33' Pt

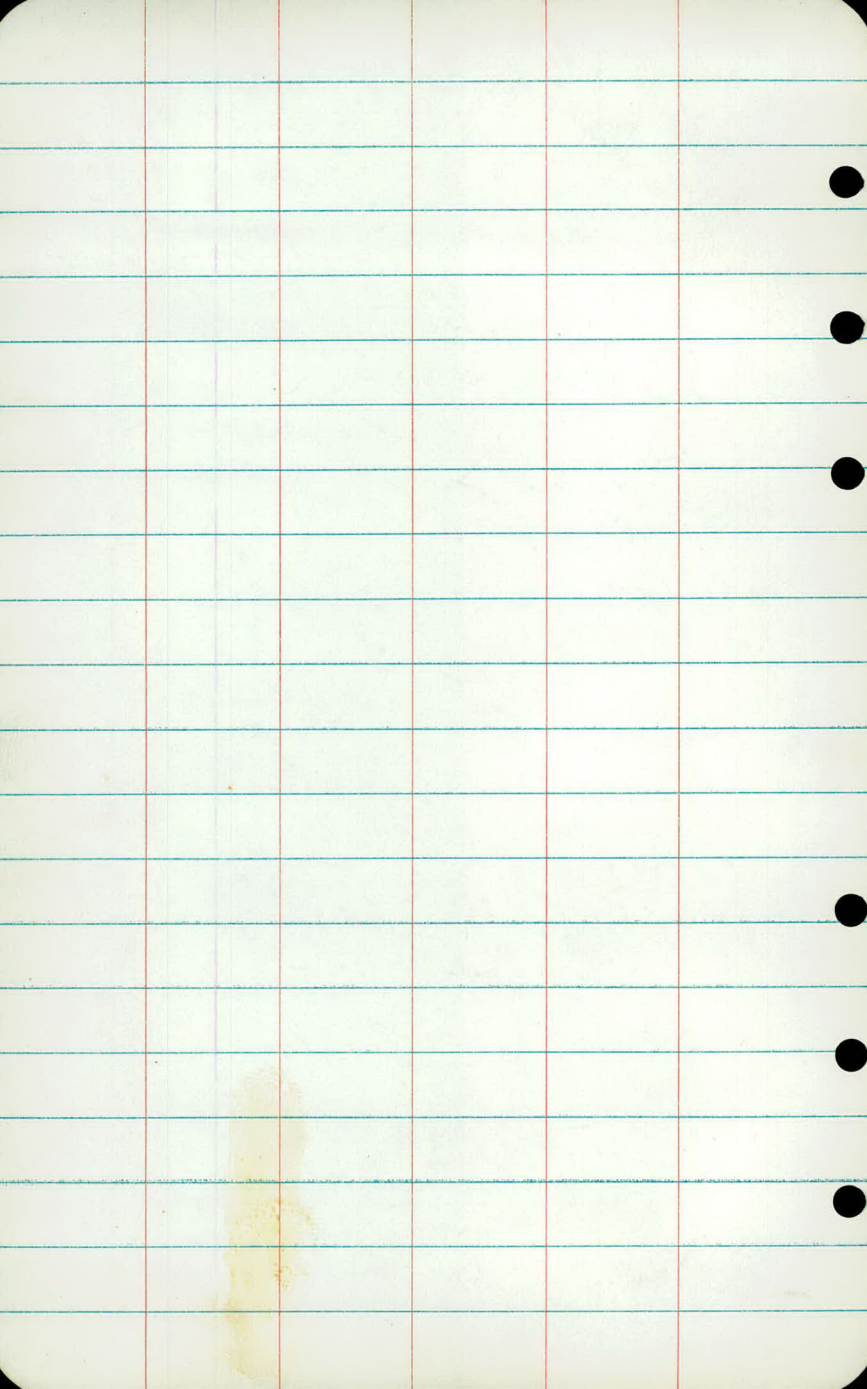
STORM



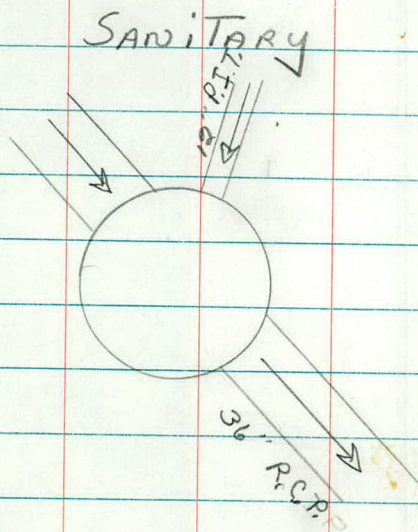
F.L. TO TOP 1.80

BRICK CONST.

3" CASTING



98+03 MH 54' LT



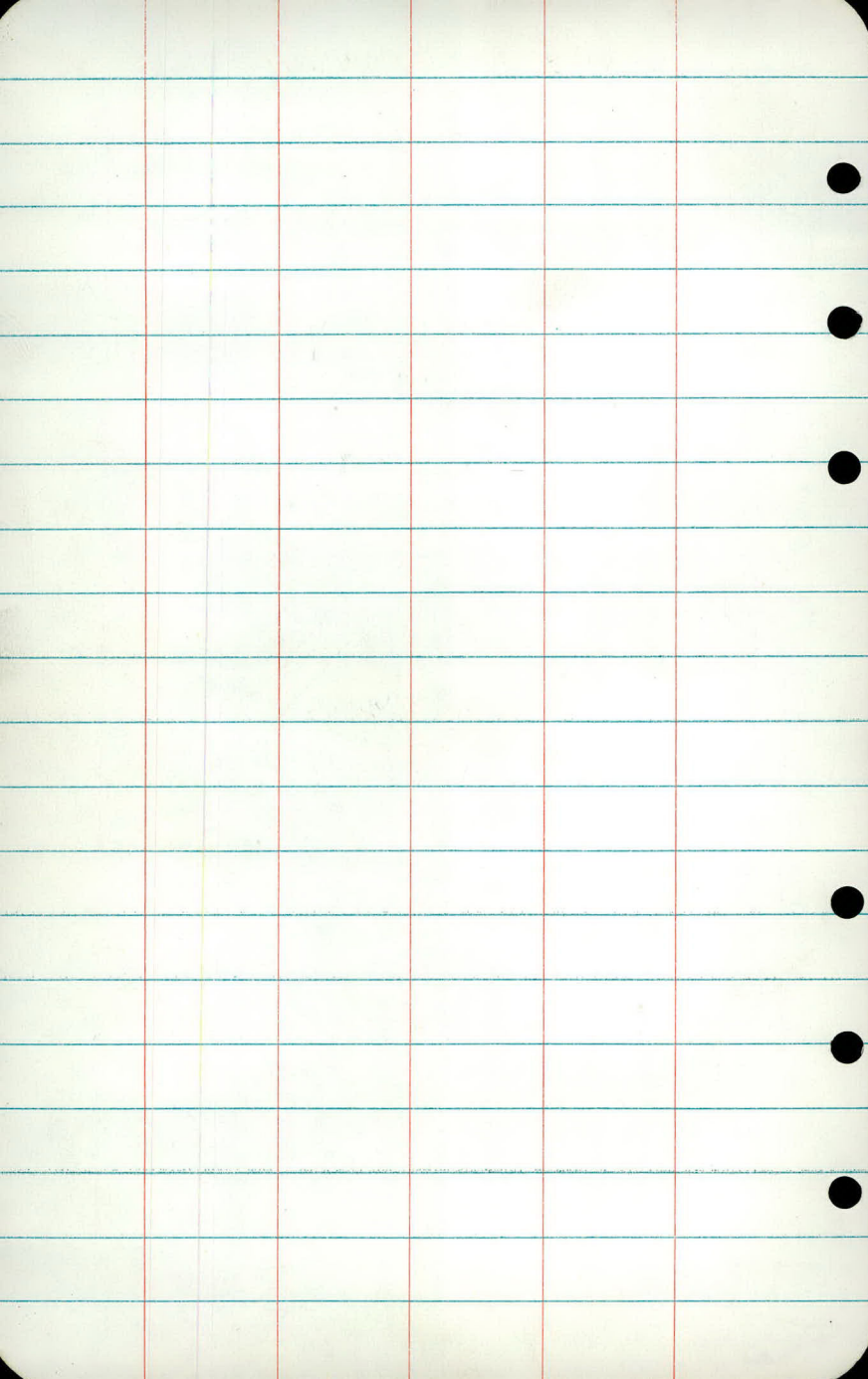
F.L. to Top 12.01

1.5 Section

4.5 ECC Cone

9 Rings

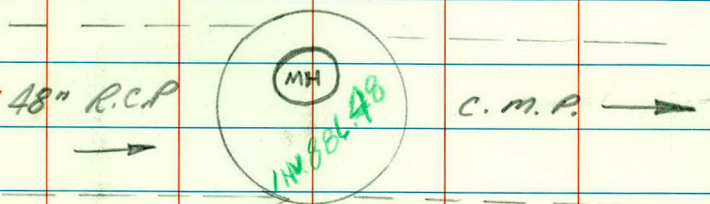
11" Casting



98+13 77 RT.

6-7-68
R.M.

M.H. Storm



Mexican Hat

8" M.H. Casting

Block construction

5.8' to Inv. M.H.

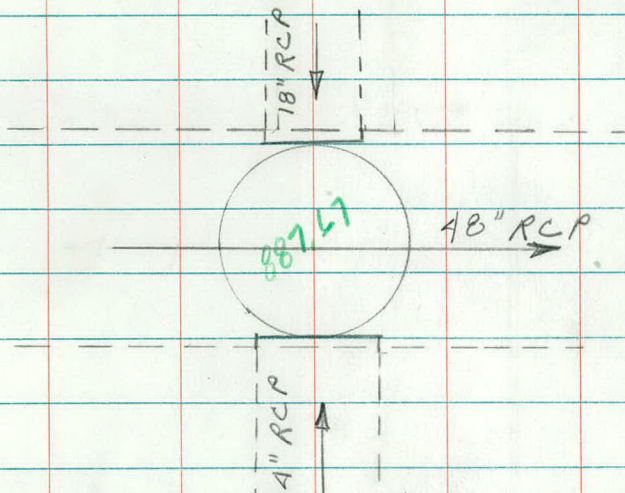
48" R.C.P. has flared end
section; joining of two
pipes is by block const.
to fit.

OBJECT

AZ

STADIA

90+13 M.H. 32' LT

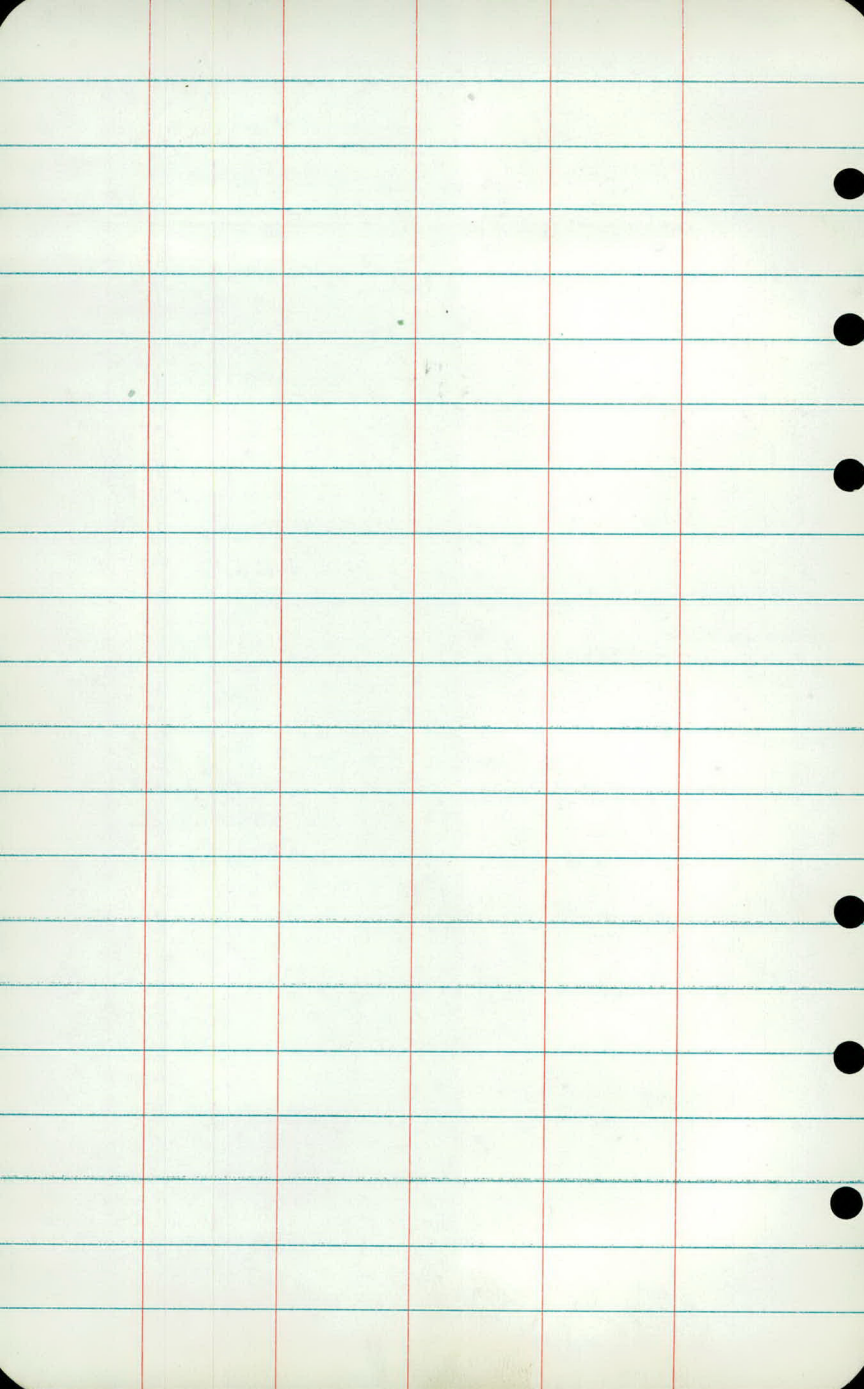


F.L. TO TOP 5.35

CONSTRUCTION:

48" RCP

11" CASTING

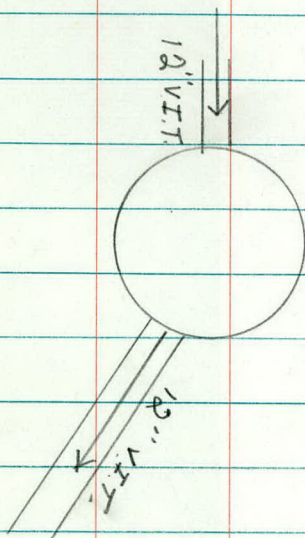


98+46

42' LT

MH

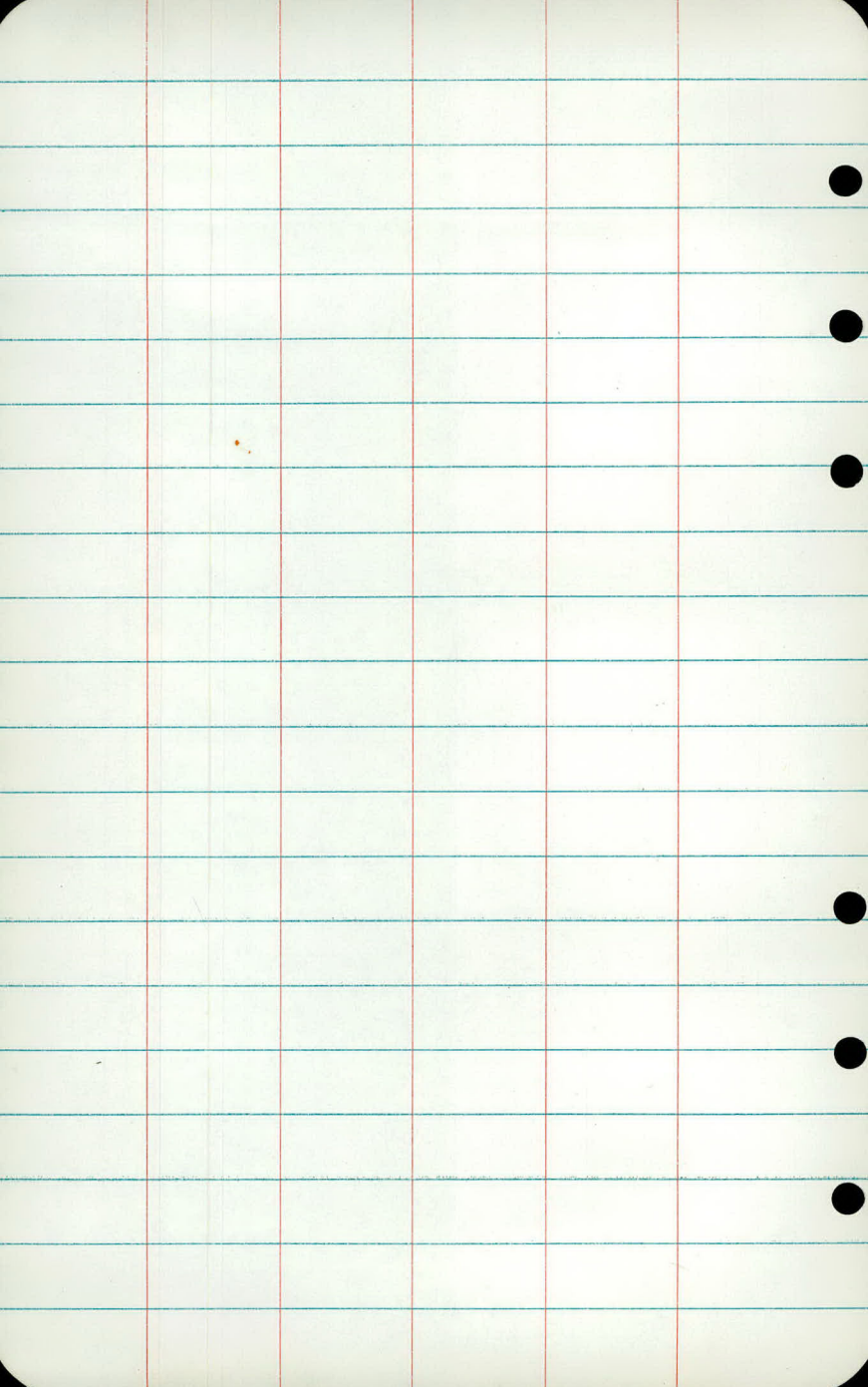
23



F. L. To Top 6' 80

4' 5 ECC Cone

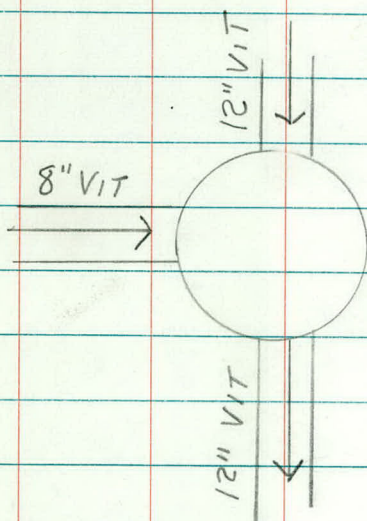
11' Casting



99+56

48' LT MH

24.



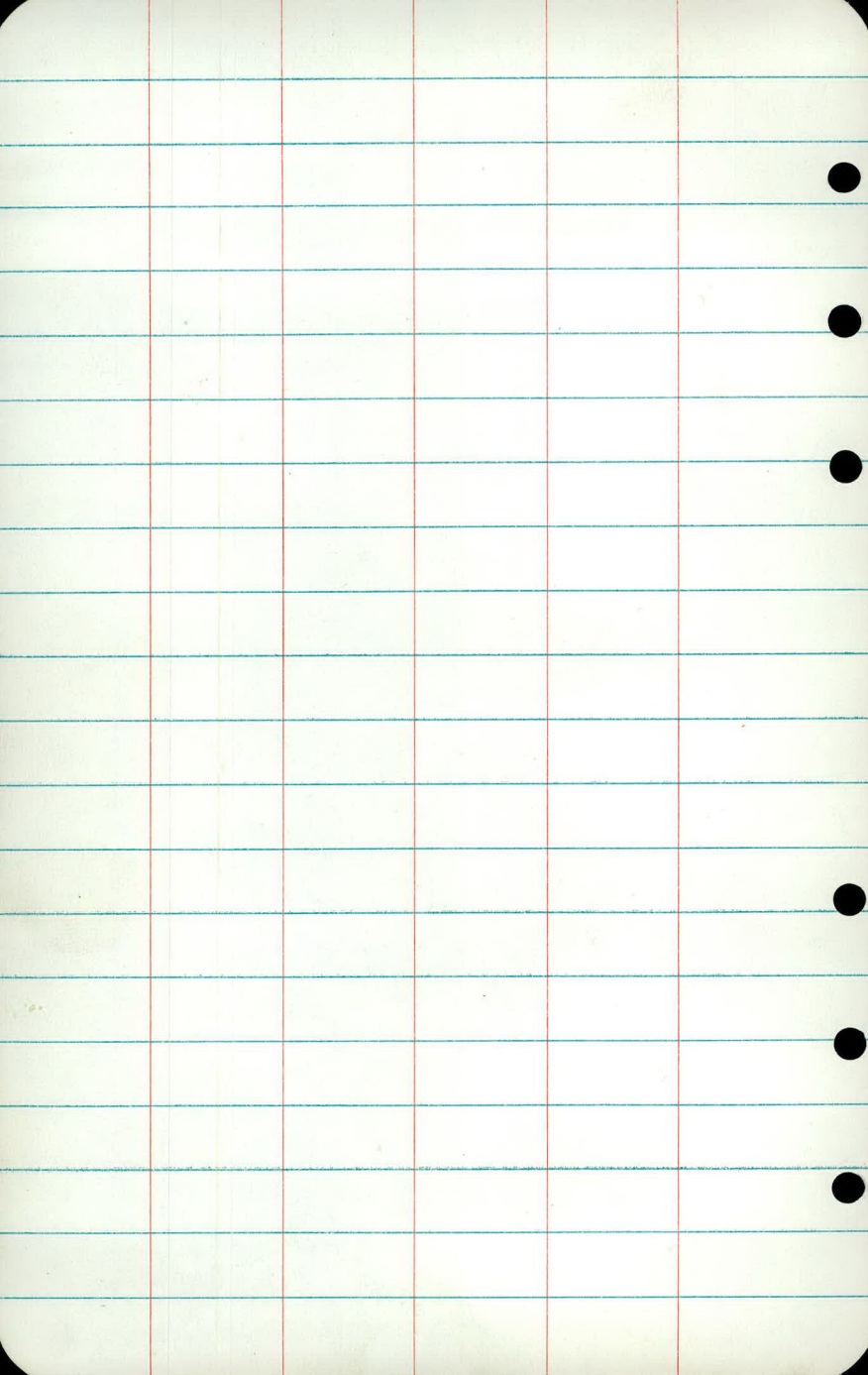
F.L. To Top 9.06

2.0 Section

4.5 ECC Cone

3 Rings

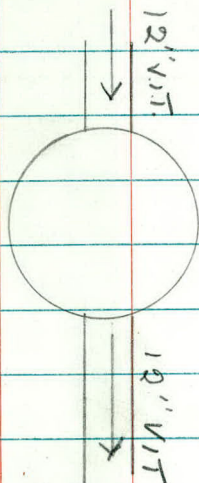
11 Casting



101 + 87
+ 83

43'
48' LT

25 A

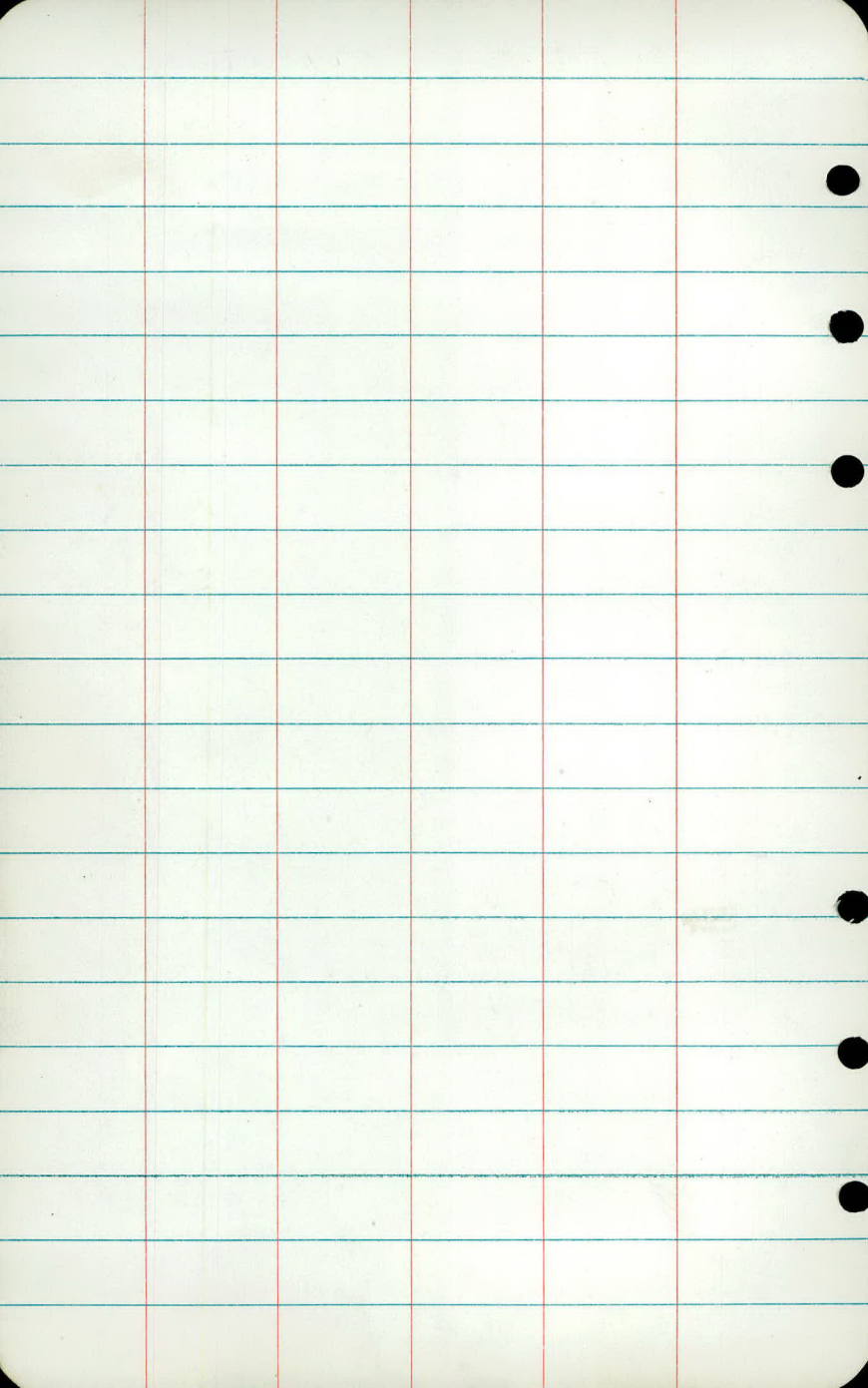


F.L. To Top 8.74

2'8 Section

4'5 ECC Cone

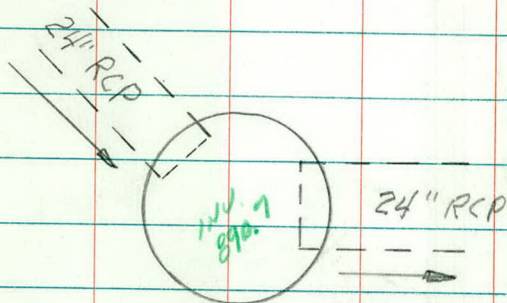
11" Casting



102456

31' LT MH

26.



FL TO TOP = 9.34

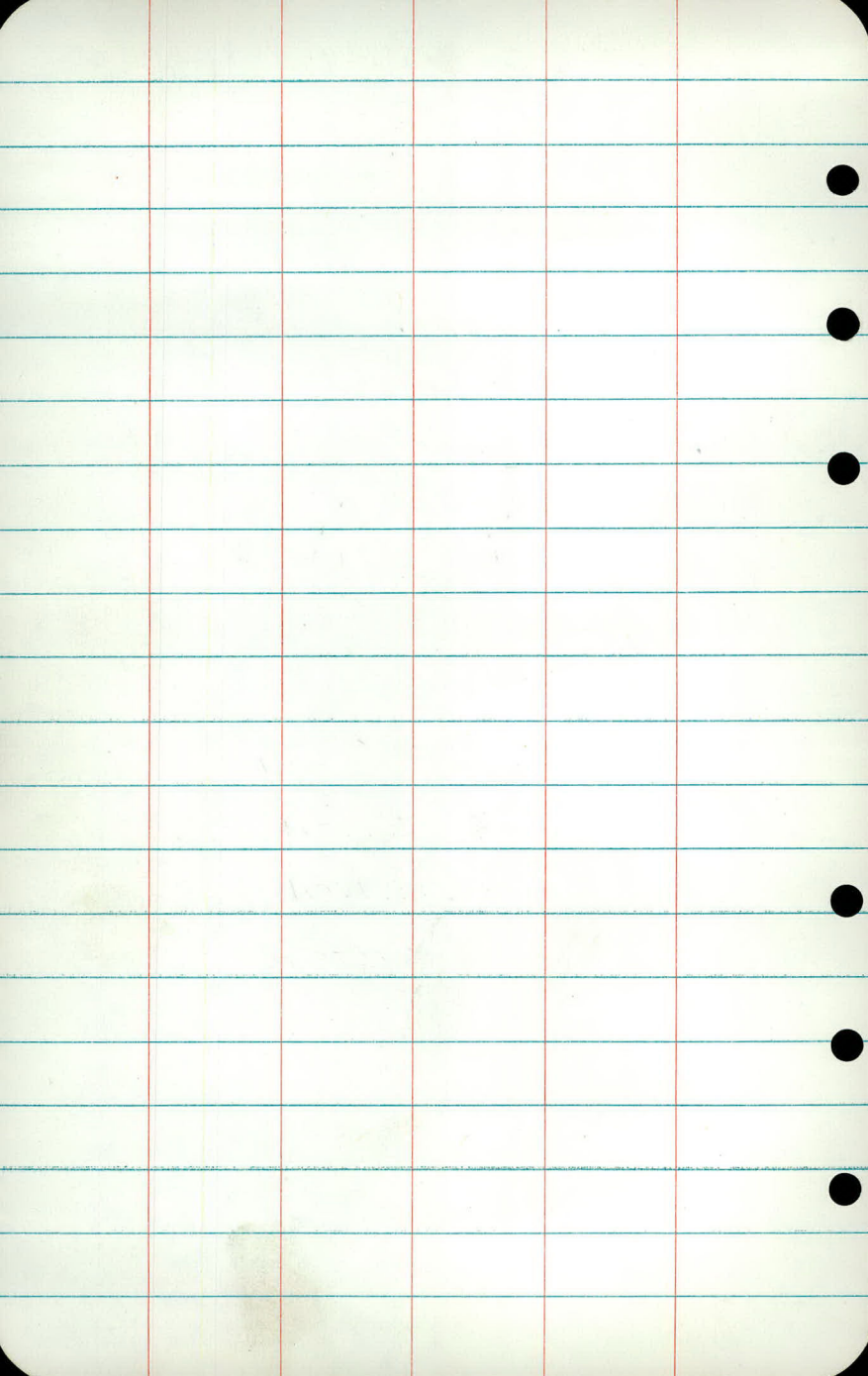
1.2 SECTION

2.2 SECTION

4.5 CONCENTRIC CONE

4 RINGS

9" CASTING



102+69

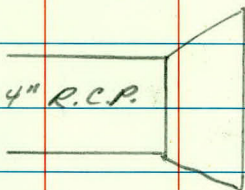
RT 92

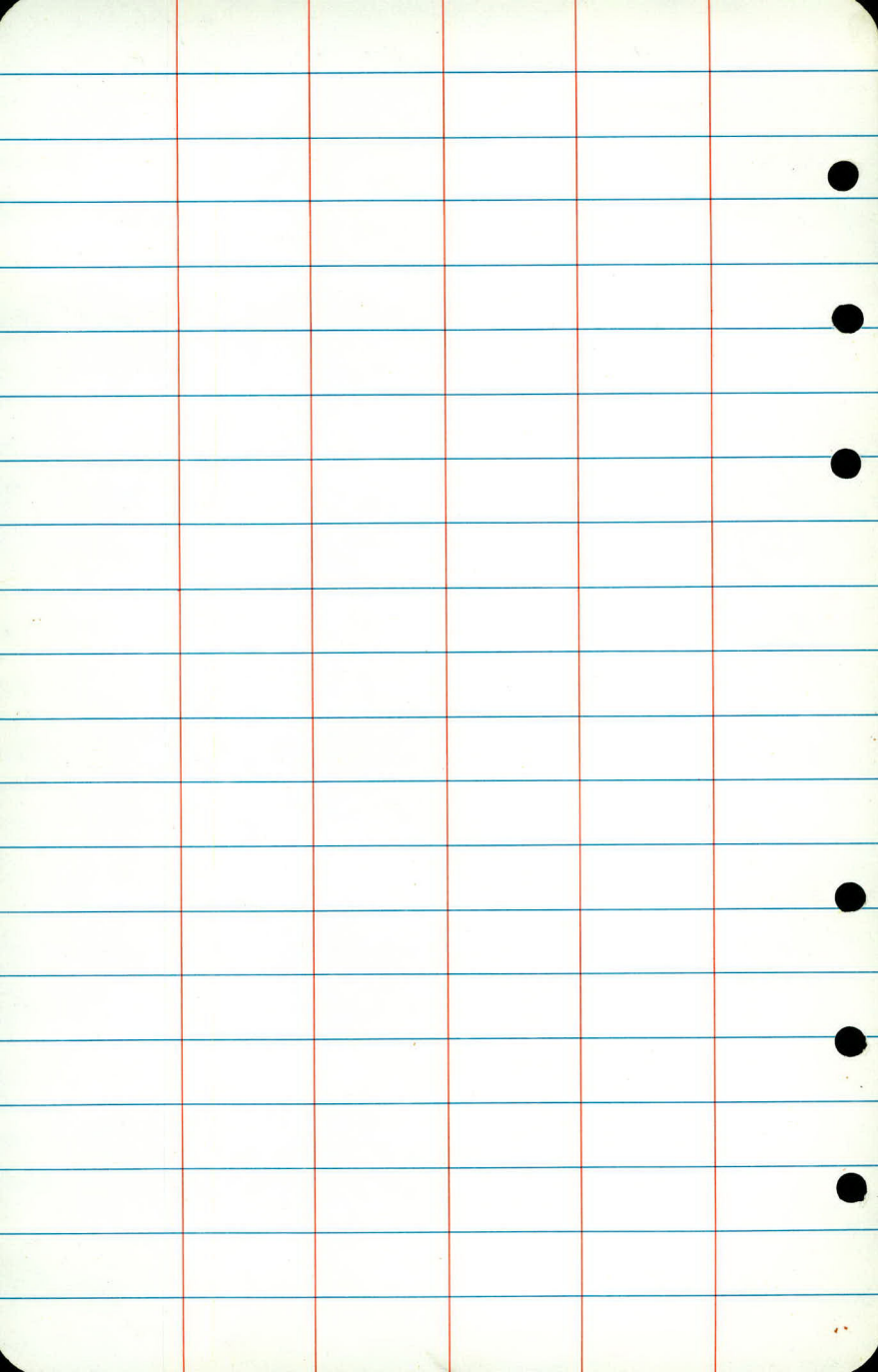
6-7-78
R.M

Apron

Storm

24" R.C.P.



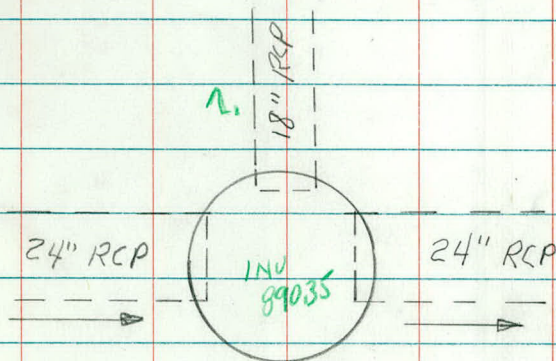


102+68

30' RT MH

27.

Storm



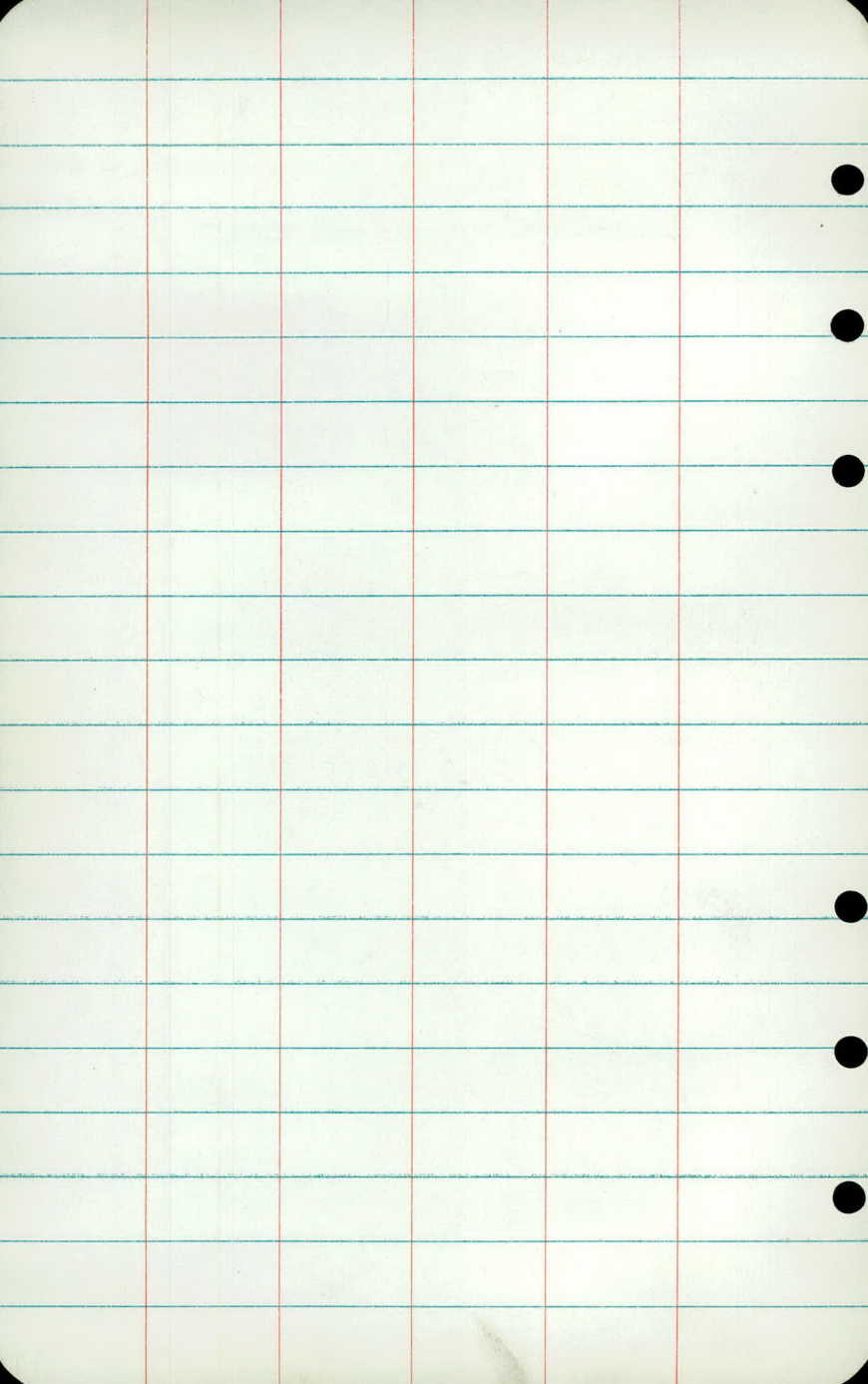
FL TO TOP = 10.00

1.2' SECTION

4.0' SECTION

4.5' CONCENTRIC CONE

9" CASTING

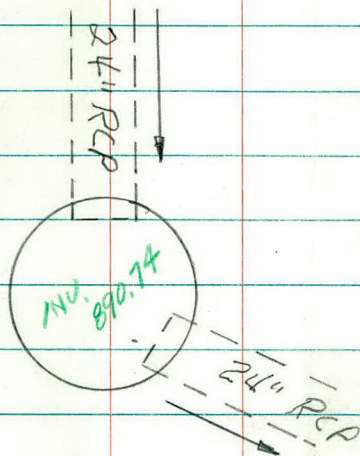


102475

51' LT SD

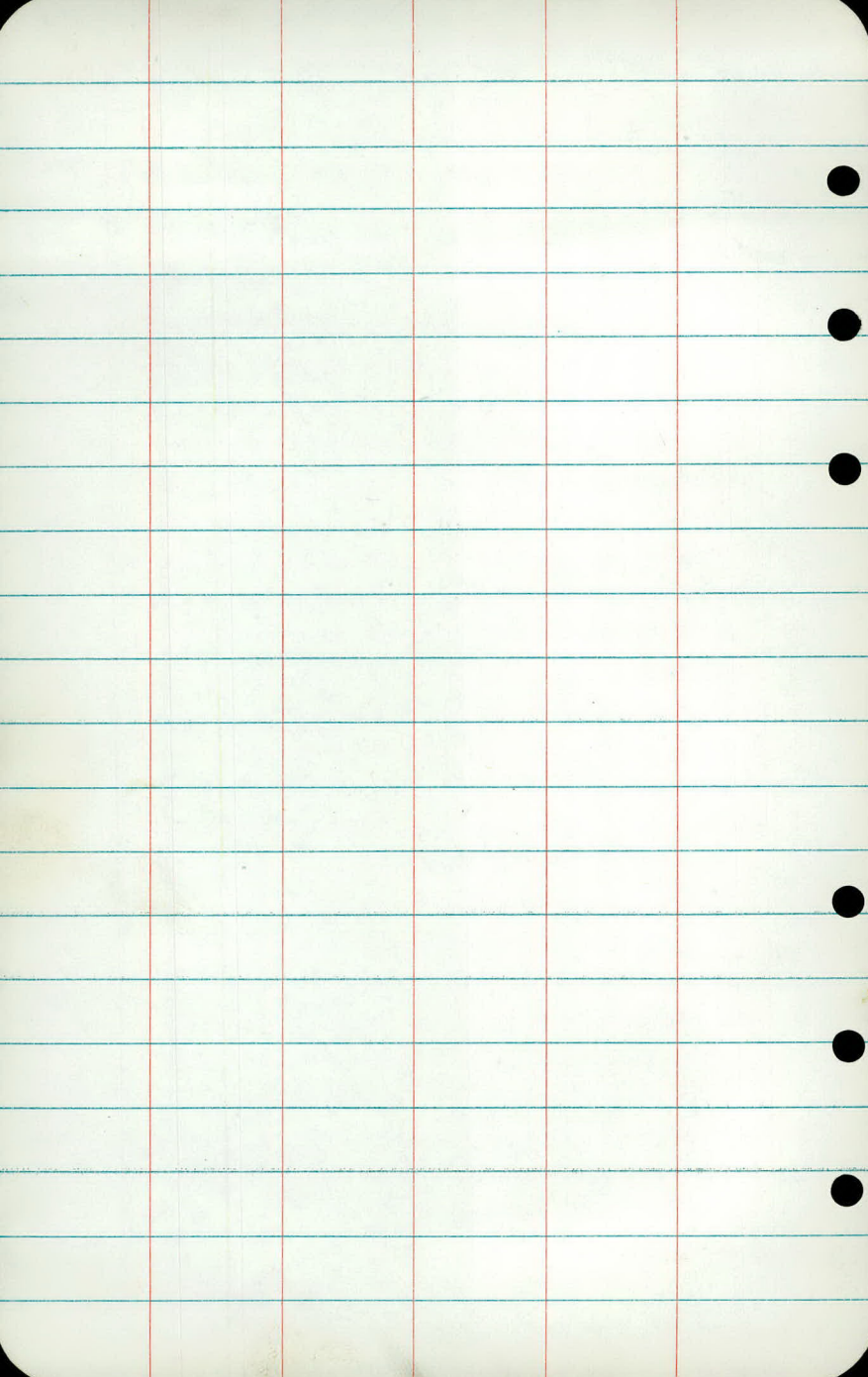
28.

BEEHIVE



FL TO TOP = 5.45

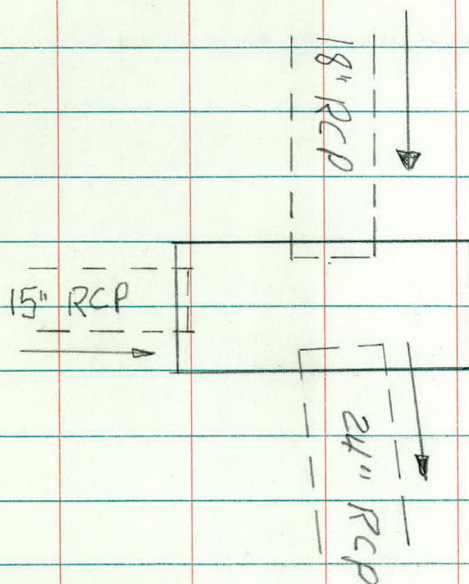
BLOCK



103+00

52' LT CB

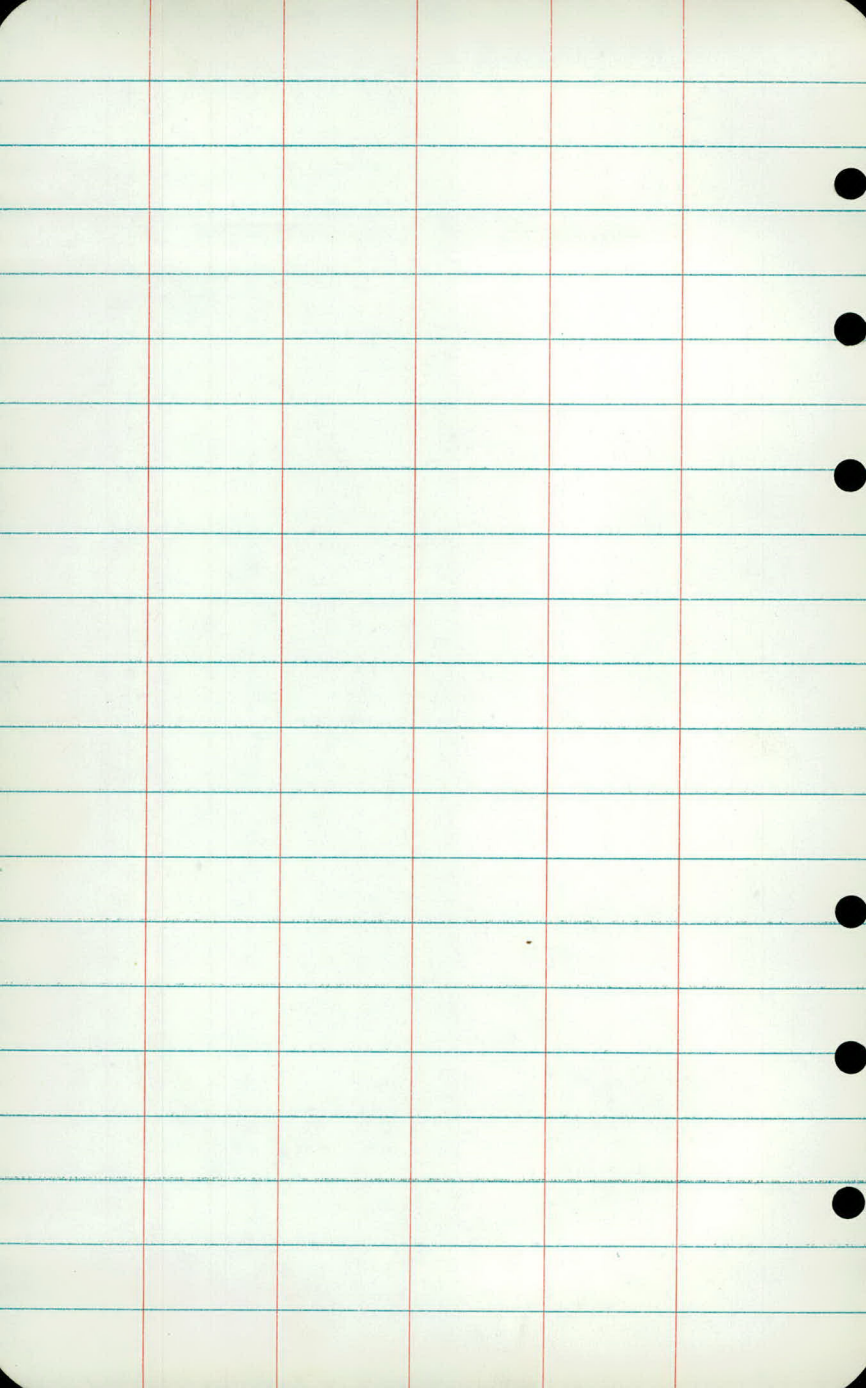
29.



FL TO TOP = 6.73

BLOCK

3" CASTING

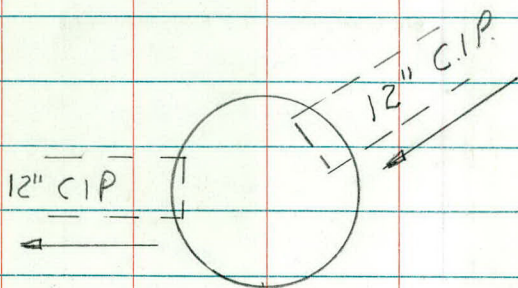


103+33

37' RT MH

30.

SANITARY



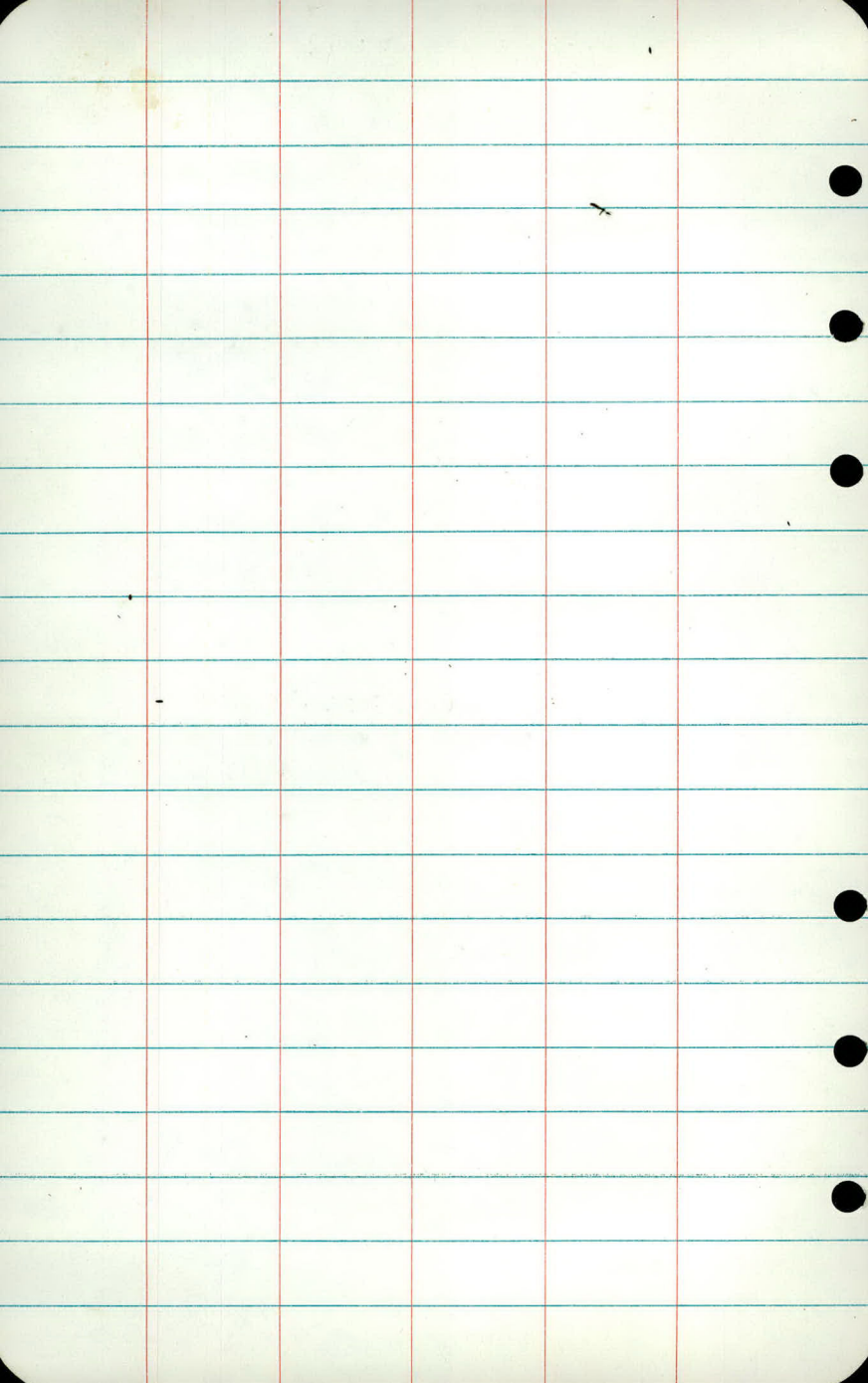
FL TO TOP = 13.24

5.0 SECTION

4.5 ECCENTRIC CONE

7 RINGS

9" CASTING



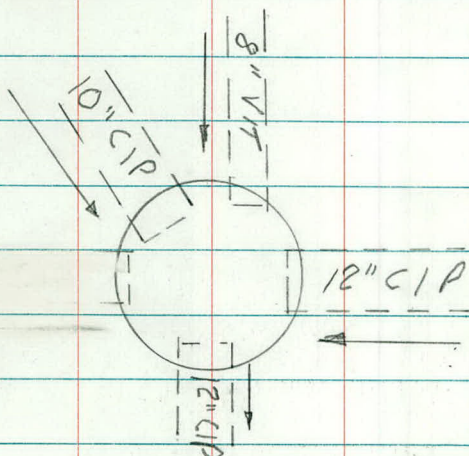
103428

42' LT

MH

31.

SANITARY



FL TO TOP = 13.65

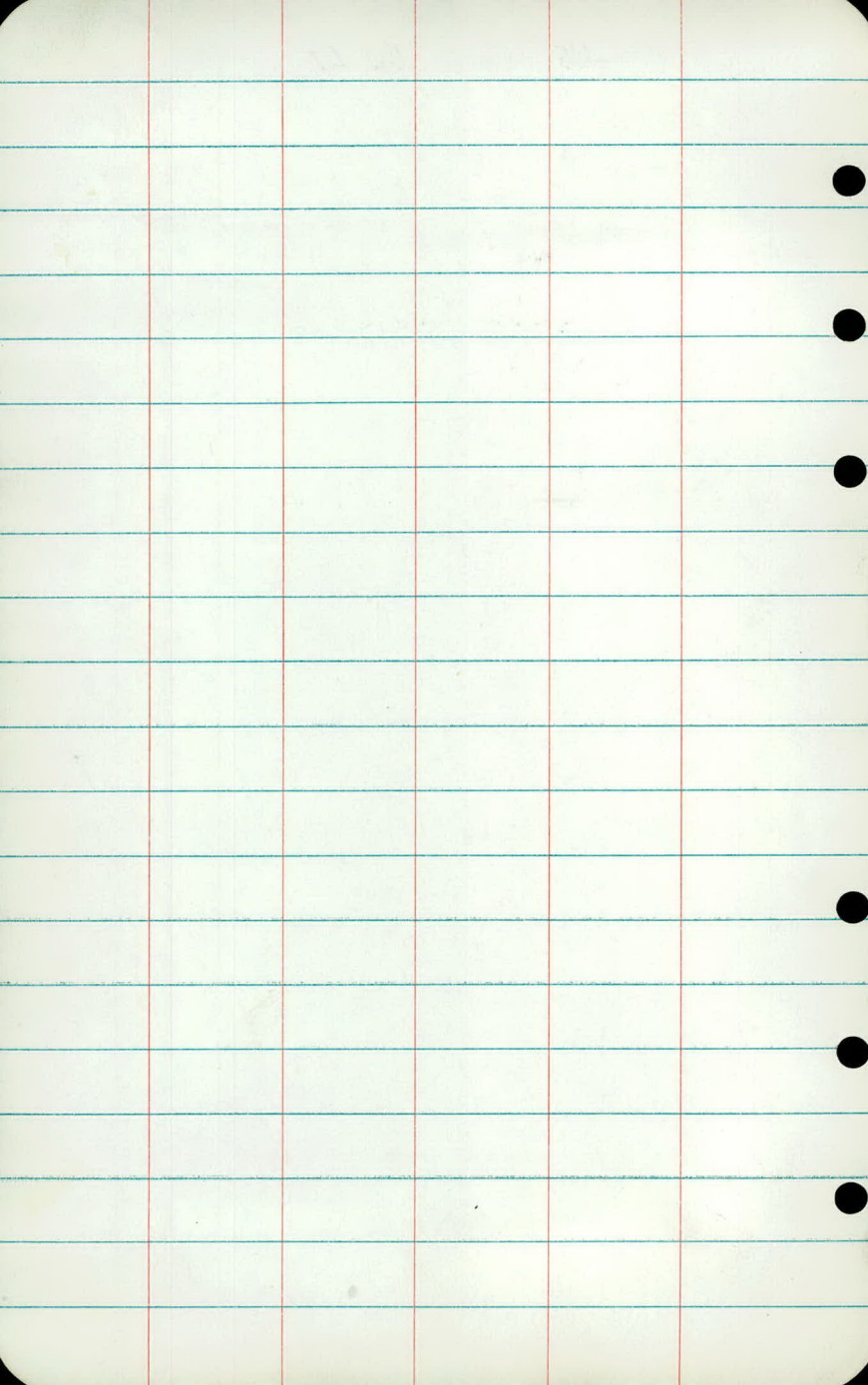
2'0 SECTION

5'4 SECTION

4.5 ECCENTRIC CONE

4 RINGS

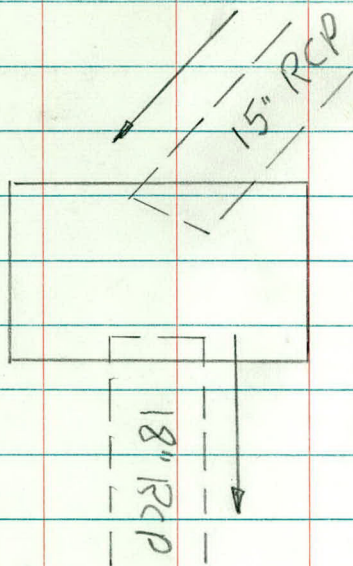
9" CASTING



103+48

52' LT CB

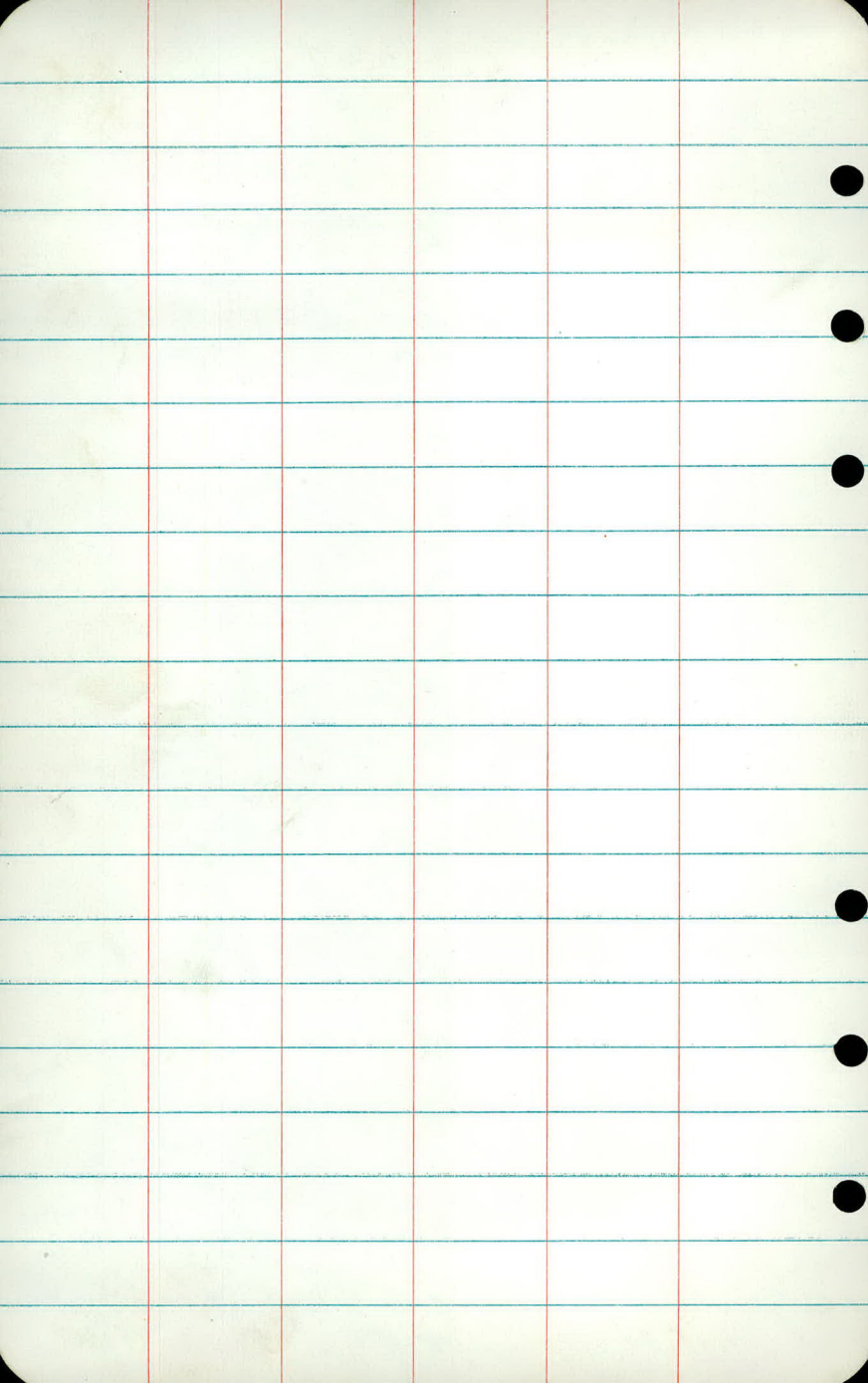
32.



FL TO TOP = 6.18

BLOCK

3" CASTING

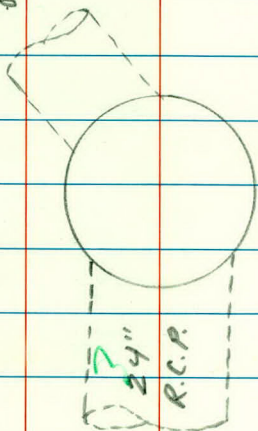


103+65 RT 36

6-7-78
Rm.

MH Storm

15"
R.C.P.



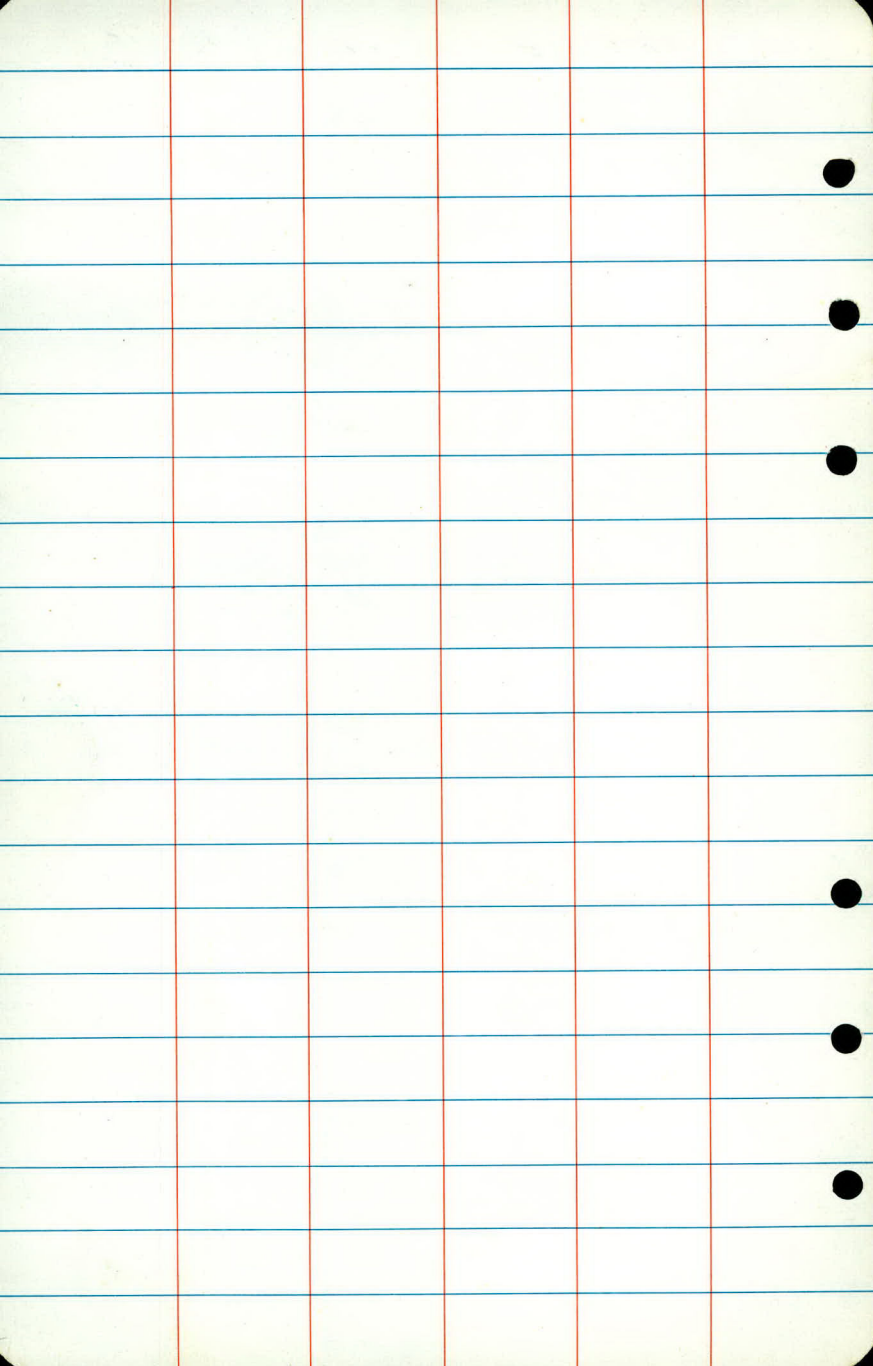
INV. 894.54

11" Casting

Block construction

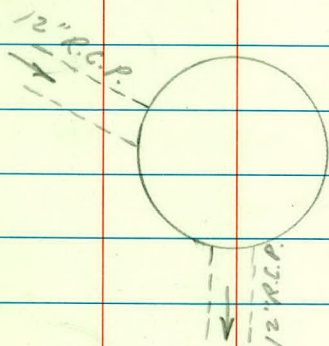
6.35 to Inv. MH

no rings



103+65 52' Lt.

MH Storm

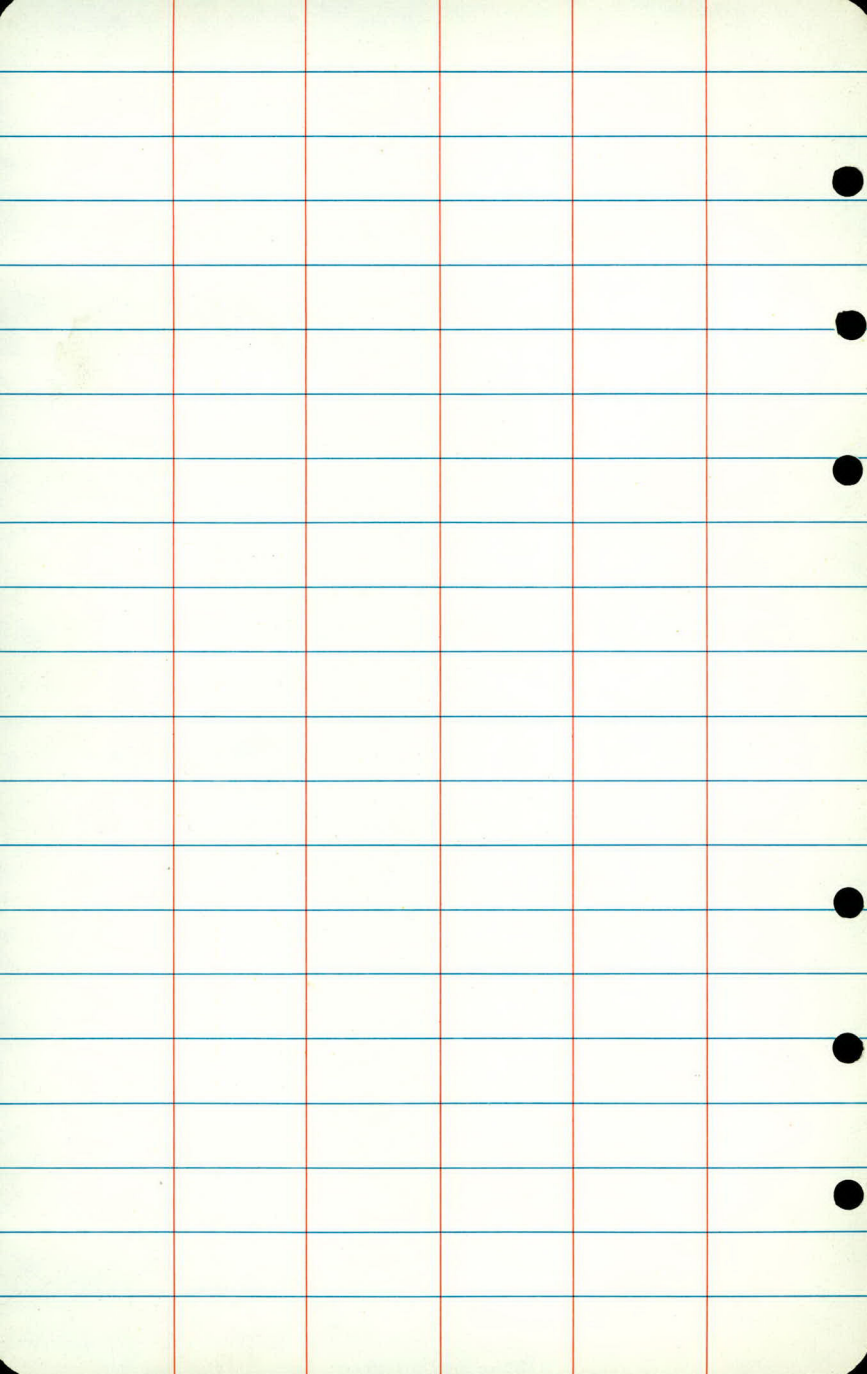


10" Casting (MH)

1 - cone section (concentric)

1 - course 8" block

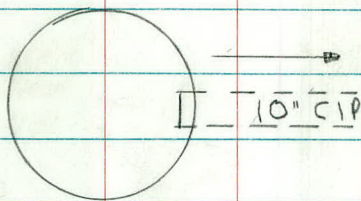
Top to Inv. = 6.0



103473

83'LT MH

33.



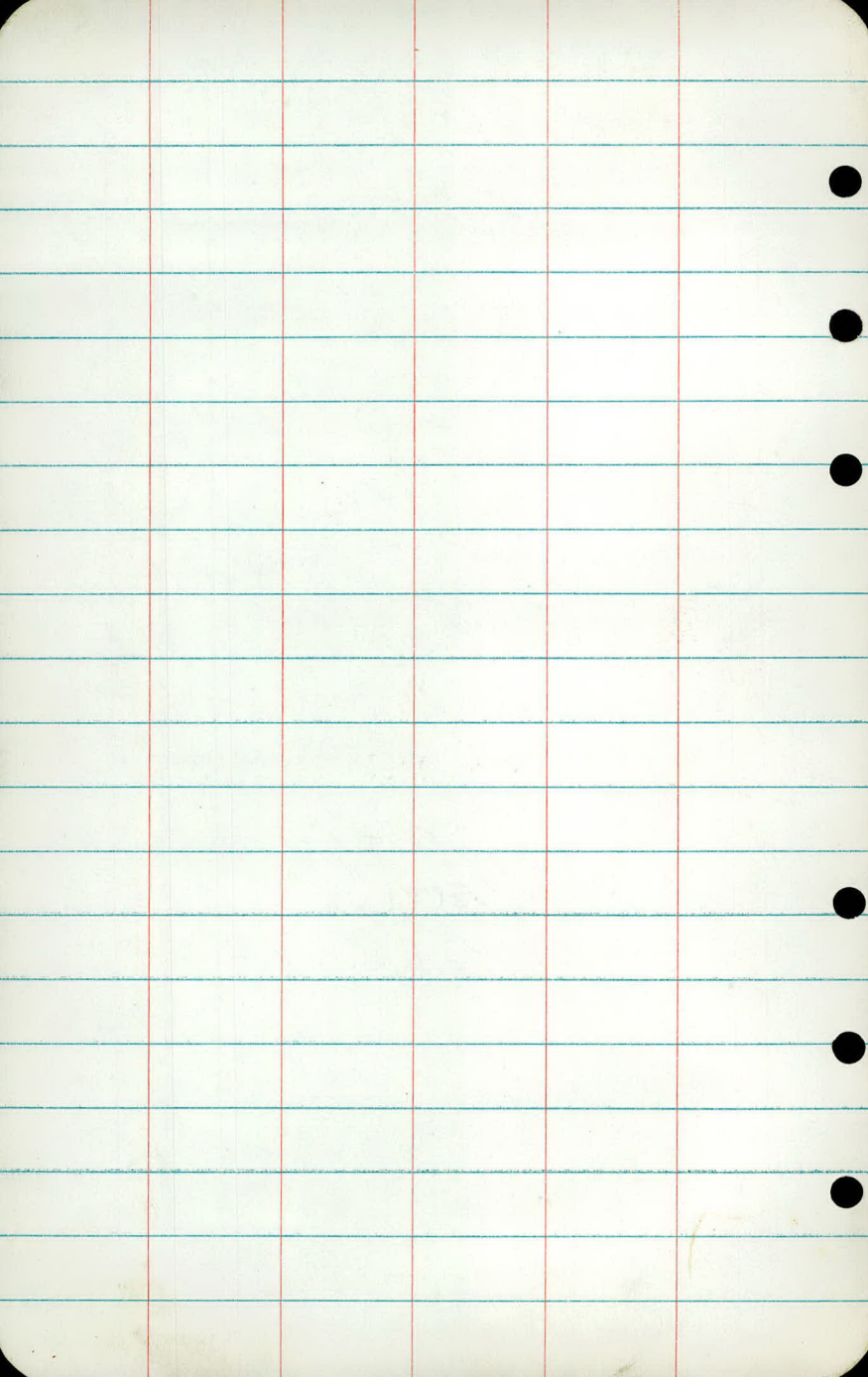
FL TO TOP = 14.10

3.8 SECTION

5.4 SECTION

4.0 ELLIPSICAL CONE

11" CASTING



103+81

24' RT

CB

32A

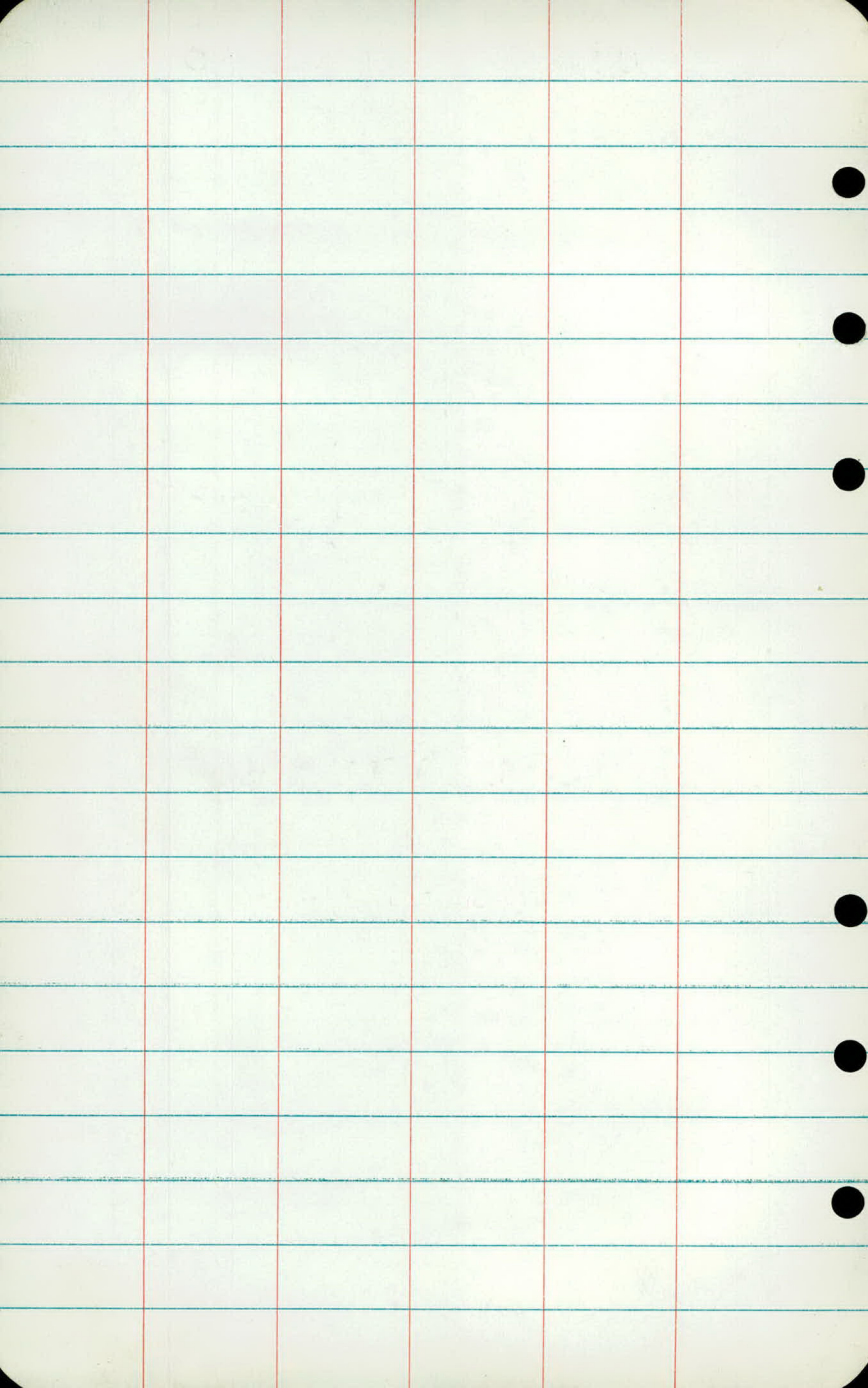


1HV. 896.99

TOP 850

FL TO TOP = 4.95

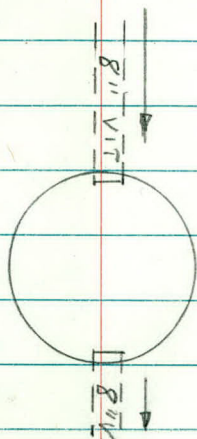
TOP 850



104+33

44' LT MH

34.



FL TO TOP = 12.26

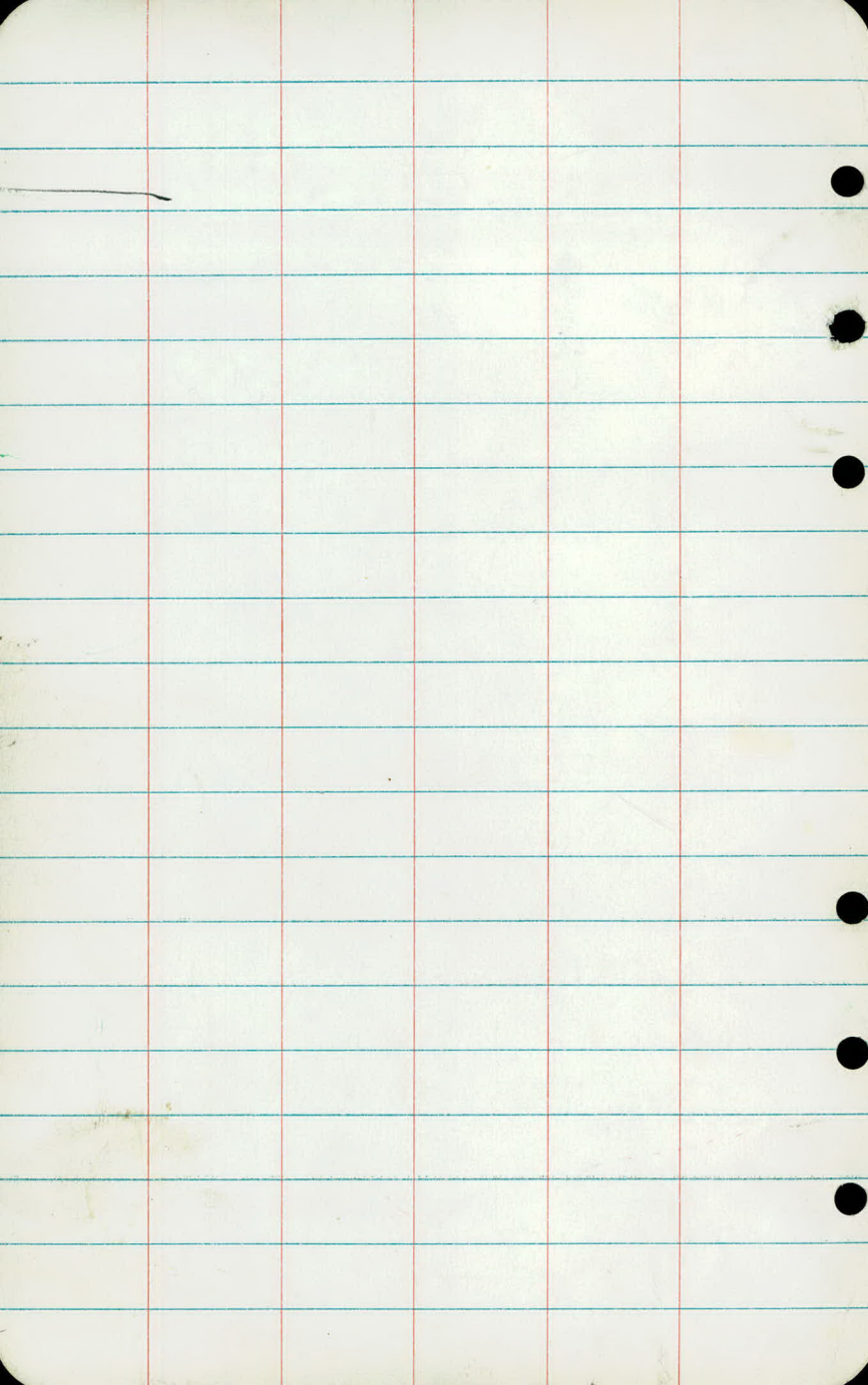
4'0 SECTION

1'4 SECTION

4.5 ELLIPTICAL CONE

5 RINGS

11" CASTING



LEXINGTON AVENUE

EXTRA STRUCTURE ELEVATIONS
(78+62 - 102+69)

CREW: R.M.

P.K.

P.D.

Cloudy & Rainy

6-7-78

LEXINGTON AVE.

STA.	+	H.I.	-	Elev.
B.M.	0.29	901.62		901.33

			9.34	892.28
--	--	--	------	--------

B.M.	3.94	936.29		932.35
------	------	--------	--	--------

			4.89	931.40
--	--	--	------	--------

			4.55	931.74
--	--	--	------	--------

			5.67	930.62
--	--	--	------	--------

			4.06	932.23
--	--	--	------	--------

			5.01	931.28
--	--	--	------	--------

			4.60	931.69
--	--	--	------	--------

			5.32	935.97
--	--	--	------	--------

			5.14	931.15
--	--	--	------	--------

			5.45	930.84
--	--	--	------	--------

B.M.				899.45
------	--	--	--	--------

				889.5
--	--	--	--	-------

party? _____ If yes, do you ever rent out? _____

ts in some manner which involves use of the

ate family? _____

e to see placed on the use of the lake? _____

e you fear might be enacted which would de=
f the lake? _____

the improvement of White Bear Lake? _____



Top Hyd N.W. Cor. Oakcrest

Top M.H. 98+13 44 RT.

Top Hyd SW. Cor. "B2"

Top C.B. 78+62 74' LT

Top M.H. 78+65 74' LT

" " 78+65 21' RT.

" C.B. 78+65 73' RT.

" M.H. 78+79 30' RT.

" C.B. 78+97 75' LT.

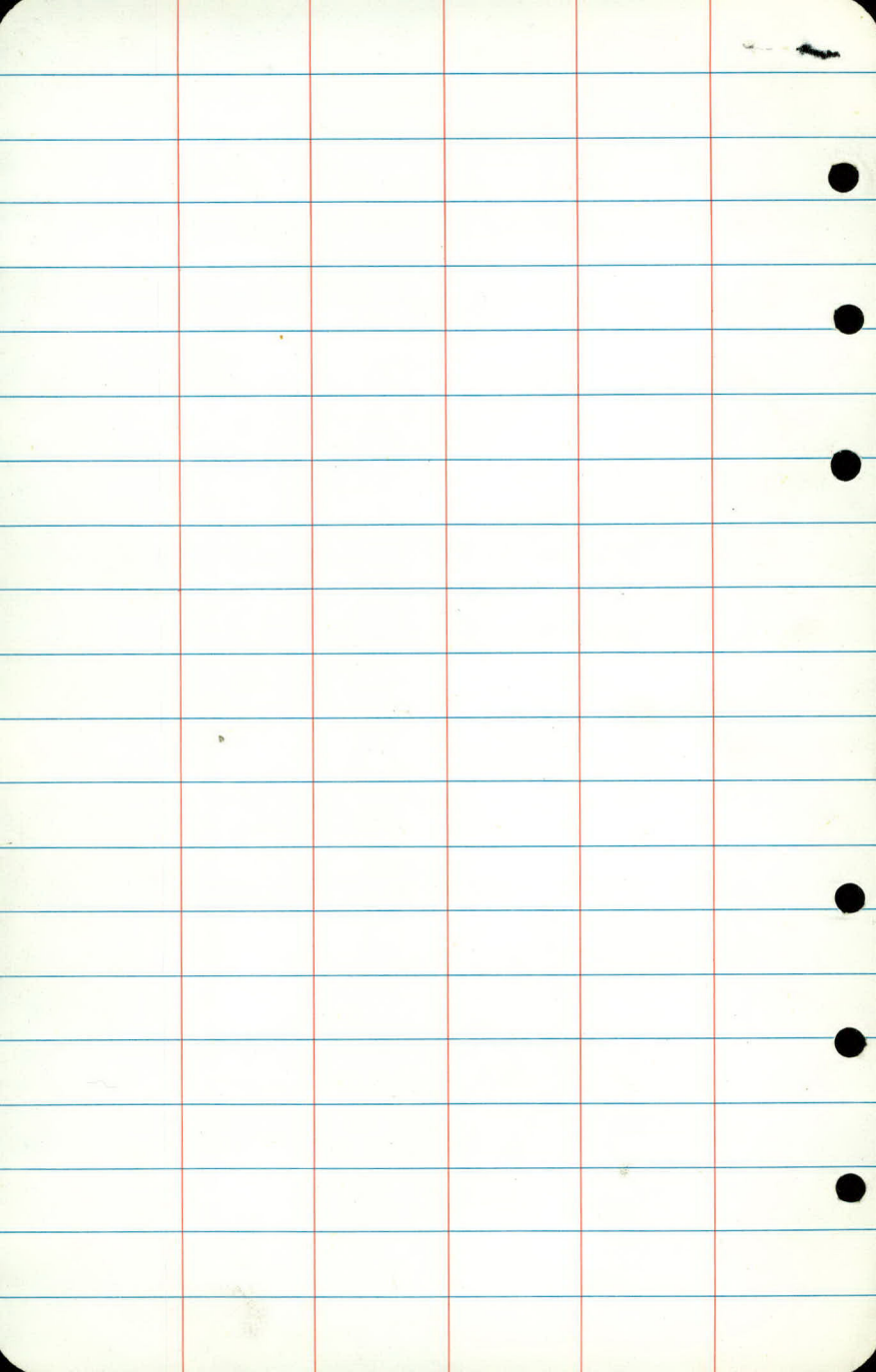
" C.B. 79+13 24' RT.

" C.B. 79+19 25' LT.

" M.H. 78+56 44 LT.

Top Hyd S. of R.R. Tracks

Inv. A.P. 102+69 RT 92



RG
LPD
DK

March 3, 1972
Clear -10°

M.H. Elevations

Lexington Ave.

62-651-03

Sta	+	π	-	Elev
BM	0.14	929.45		929.31
S.D.			4.07	925.38
MH			6.66	922.79
MH			9.96	919.49
MH			10.59	918.86
MH			14.71	914.74
BM			6.57	922.88 922.88
BM	5.88	938.23		932.35
MH			6.03	932.20
BM			5.88	932.35 932.35

Mar. 3, 1972

2

Remarks

Top Hyd Rt Sta 71+20

Sta 71+60 Rt 32'

Sta 72+35 Rt 60'

Sta 72+62 Rt 60'

Sta 72+96 Rt 37'

Sta 75+47 Lt 40'

Top Hyd. NE Cor. Grandview

Top Hyd SW Cor. B²

Sta 79+03 Lt 38'

Sta

+

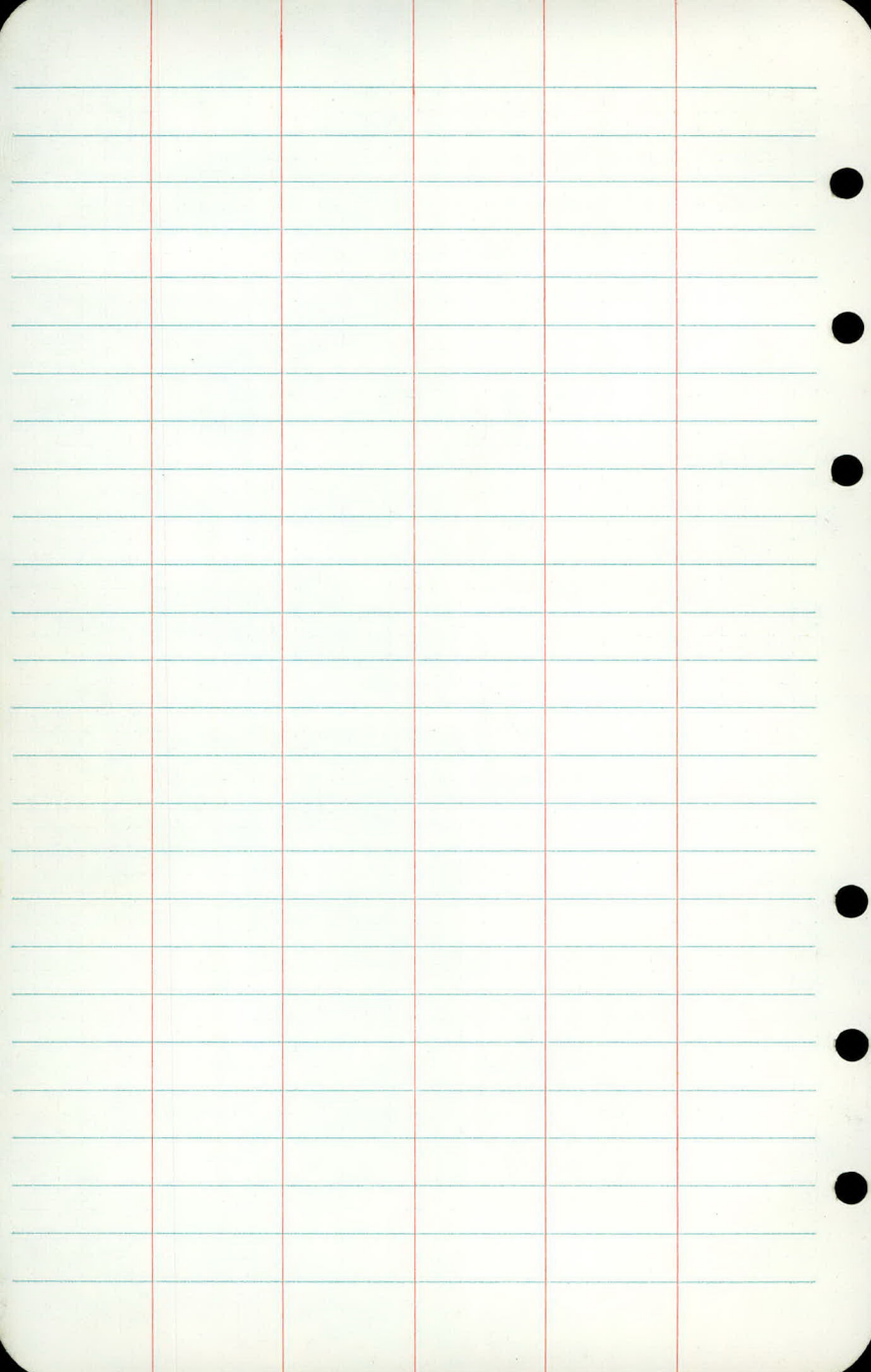
π

-

Elv.

Remarks

3



KP
DS
GA

6 MARCH 1972 1.
CLOUDY 20°

62-651-03 CTB

MH & CB ELEVATIONS

STA	+	-	π	-	ELEV
BM	2.46	936.53			934.07

			5.61	930.92	✓
--	--	--	------	--------	---

			5.73	930.80	✓
--	--	--	------	--------	---

BM	3.58	924.22			920.64
----	------	--------	--	--	--------

			5.44	918.78	✓
--	--	--	------	--------	---

			6.41	917.81	✓
--	--	--	------	--------	---

BM	6.80	908.13			901.33
----	------	--------	--	--	--------

			2.92	905.21	✓
--	--	--	------	--------	---

			8.97	899.16	
--	--	--	------	--------	--

BM	3.61	899.08			895.47
----	------	--------	--	--	--------

			6.37	892.71	✓
--	--	--	------	--------	---

			3.85	895.23	✓
--	--	--	------	--------	---

			3.88	895.20	
--	--	--	------	--------	--

LT

E

6 MAR. 1972

RT

2.

TOP HYDRANT N.W COR TRANSIT

TOP MH STA 84+90 37' RT

TOP MH STA 85+24 38' LT

TOP HYDRANT NW COR BROOKS

TOP MH STA 88+46 37' LT

TOP MH STA 88+46 37' RT

TOP HYDRANT NW COR OAKCREST

TOP MH STA 91+15 37' LT

TOP HYDRANT STA 94+35 40' RT

TOP HYDRANT STA 98+49 26' LT

TOP MH STA 98+46 48' LT

TOP MH STA 98+03 54' LT

TOP PK NAIL E STA 98+00

STA	+	π	-	ELEV.
BM	6.92	906.37		(899.45)

			11.04	95.33
--	--	--	-------	-------

			5.48	00.89
--	--	--	------	-------

			4.43	01.94
--	--	--	------	-------

			5.42	900.95
--	--	--	------	--------

9.55
14.5
11.04

BM	9.44	932.93		(923.49)
----	------	--------	--	----------

			3.54	29.39
--	--	--	------	-------

			4.57	928.36
--	--	--	------	--------

Lt

E

8 MAR. 1972

3.

Rt

TOP HYDRANT S. RR TRACKS AT CARD C

TOP MH 101+87 43' LT

TOP CB 103+65 36' RT

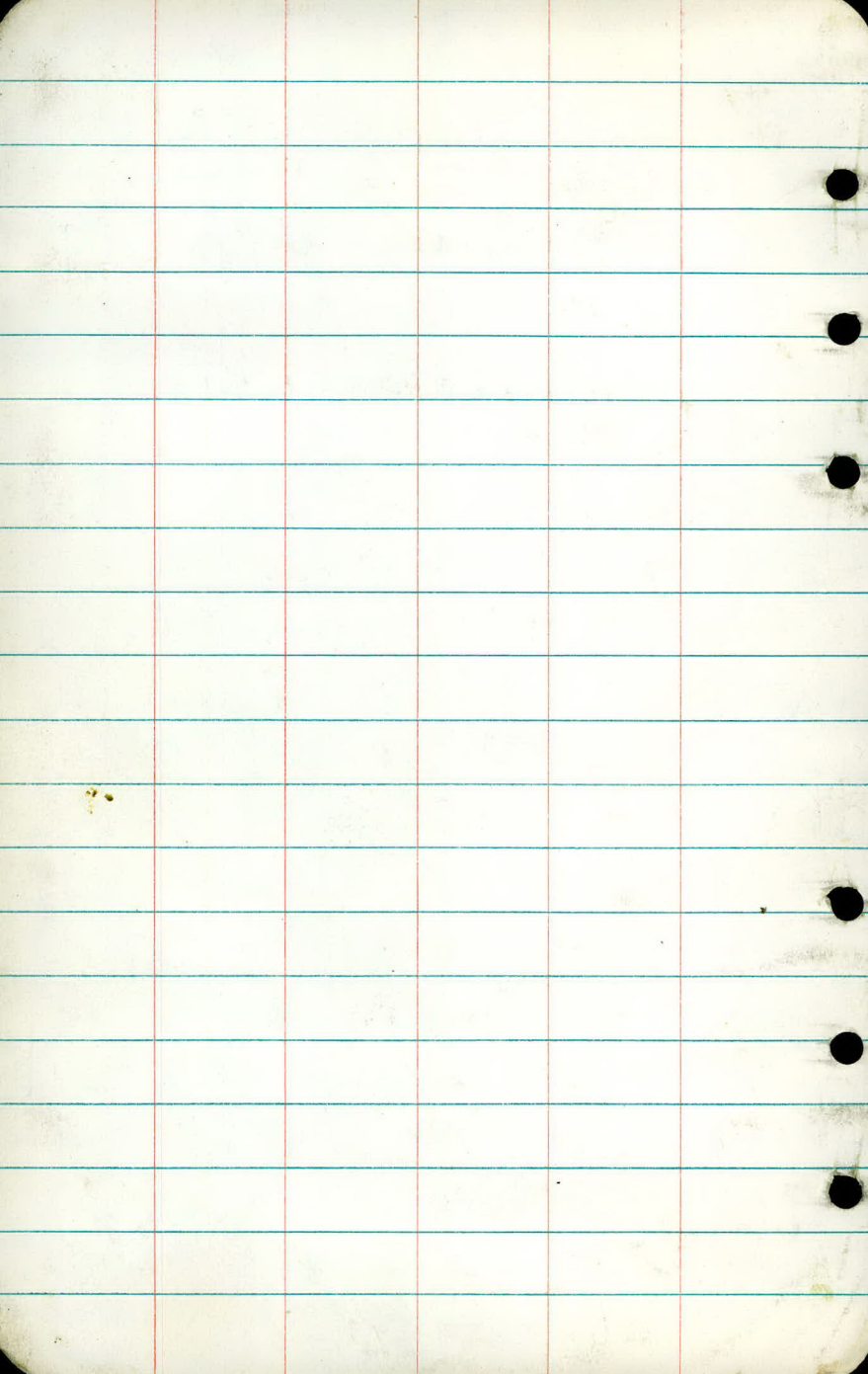
TOP CB 103+81 24' RT

TOP MH 103+33 37' RT

TOP HND LT STA 107+30

TOP MH 46' LT STA 108+44

TOP PK E STA 109+00



KP
DS
DK
PH

26 OCT 1971
CLOUDY 55°

1

X-SECTIONS

LEXINGTON AVE
STH 36 TO CO. RD. E.C.

X-SECTIONS

STA + π - ELEV.

BM 0.98 945.32

(944.34)

3.94 41.38

TP 2.33 943.75 3.90 941.42

2.58 41.17

3.57 40.18

5.46 38.29

8.22 35.53

TP 3.34 935.42 11.67 932.08

BM 2.01 931.32 6.11 929.31 (929.31)

3.20 28.12

7/172 $\neq$ 16' CONC. ENT (RT)

✓

2.77 927.47 6.62 924.70

KP
DK
DS
PH

LT

26 OCT. 1971
RT

2

TOP HYDRANT AT LAURIE.

TOP MEDIAN STA 64+00

TOP MEDIAN STA 65+00

TOP MEDIAN STA 66+00

TOP MEDIAN STA 67+00

TOP MEDIAN STA 68+00

TOP MEDIAN STA 69+00

TOP MEDIAN STA 70+00

TOP HYDRANT RT STA 71+20

TOP PK Φ STA 71+00

25.1	23.5	25.0	24.3	25.0	26.6	25.1	25.9	27.1	27.8
5.6	7.8	6.3	7.0	6.3	5.7	6.2	5.40	4.22	3.48
56	47	34	33	24		29	50	71	85
							conc.	conc.	conc.

25.9

5.4
75

29.0

234
106
GA

TOP PK Φ STA 72+00

STA	+	π	-	ELEV.
-----	---	-------	---	-------

		927.47		
--	--	--------	--	--

71+98				
-------	--	--	--	--

		5.76	21.71	
--	--	------	-------	--

72+00				
-------	--	--	--	--

✓				
---	--	--	--	--

107				
-----	--	--	--	--

✓				
---	--	--	--	--

+23				
-----	--	--	--	--

		6.83	20.64	
--	--	------	-------	--

KP
DK
DS
PH

LT

E

26 OCT. 1971

RT

3

FL S. END 18" CM 45.0 LT

23.5	23.2	23.5	24.2	24.7	24.3	23.7	24.3	26.5
4.0	4.3	4.0	3.3	2.8	3.2	3.8	3.2	2.0
70	47	35	22		23	31	39	56
FE								

24.4	26.5
1.1	1.0
100	74

23.4	23.0	23.4	24.0	24.5	24.0	23.9	24.0	24.4
4.1	4.5	4.1	3.5	3.0	3.5	3.7	3.5	2.7
70	51	35	22		23	30	42	57
FE								

21.9	22.3	23.5
5.6	5.2	4.0
100	75	61

FL N. END 18" CM 44' LT

STA + π - ELEV,

927.47

72+50

✓

+65

✓

+70

✓

KP
DK
DS
PH

LT

26 OCT 1911
RT 4

20.9 22.3 22.1 23.0 23.4 22.8 22.5 22.4 21.7
6.6 5.2 4.8 4.5 4.1 4.7 5.0 5.1 5.8
44 38 32 20 20 23 45 70

20.8 21.4 23.3 21.1
6.7 6.1 4.2 6.4
48 56 70 100
FE

20.5 20.6 22.4 22.5 23.1 22.4 22.2 22.0 21.1
7.0 6.9 5.1 5.0 4.4 5.1 5.3 5.5 6.4
48 45 35 19 21 36 52 67

21.9 23.2 20.8
5.6 4.3 6.7
60 70 100
FE

21.8 20.1 20.3 22.1 22.5 22.9 22.4 21.9 22.9 22.6
5.7 7.4 7.2 5.4 5.0 4.6 5.1 5.6 4.6 4.9
59 46 43 35 19 20 23 29 37

23.1
4.4
70

15.3 15.5 12.9 12.7 18.7
12.2 12.0 14.6 8.8
78 64 56 47

FL 30"
RCP

STA	+	π	-	ELEV
-----	---	-------	---	------

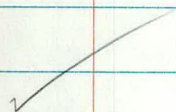
		927.43		
--	--	--------	--	--

TP	3.30	925.58	5.19	922.28
----	------	--------	------	--------

72+80			4.66	20.92
-------	--	--	------	-------

+92			11.79	13.79
-----	--	--	-------	-------

73+00				
-------	--	--	--	--



+50				
-----	--	--	--	--



KP
DK
DS
PH

LT

26 OCT. 1971
RT

5

TOP DK & STA 73+00

FL W.END 12" CM 24' RT

FL E.END 12" CM 51' RT

18.2 18.1 19.8 21.4 21.9 22.3 21.8 21.9 22.2 18.9
7.4 7.5 5.6 4.2 3.7 3.3 3.8 3.7 3.4 6.7
44 43 41 31 18 19 23 27 38

19.7 21.6 22.9
5.9 4.0 2.7
46 59 70

12.7 13.0 13.9
12.9 12.6 11.7
72 59 51

17.0 18.4 18.8 20.7 21.1 21.5 21.1 21.3 20.7 15.3
8.6 7.2 6.8 4.9 4.5 4.1 4.5 4.3 4.9 10.3
41 40 35 27 16 16 24 28 42

16.9 18.4 20.1 22.3
8.7 7.2 5.5 3.3
43 44 55 73

11.1 12.0 12.6
14.5 13.6 13.0
70 58 54

STA + π - ELEV.
925.58

74+00

✓

BM 2.07 924.95 2.70 922.88 (922.88)

74+50

✓

75+00

6

$$\begin{array}{r} 15.7 \\ 9.3 \\ \hline 50 \end{array}$$

$$\begin{array}{r} 19.6 \\ 6.0 \\ \hline 63 \end{array}$$

$$\begin{array}{r} 21.6 \\ 3.4 \\ \hline 10 \end{array}$$

$$\begin{array}{r} 11.9 \\ 13.1 \\ \hline 75 \end{array}$$

$$\begin{array}{r} 12.6 \\ 12.4 \\ \hline 50 \end{array}$$

STA	+	π	-	ELEV,
		924.95		
75+40				
✓				
+55				
✓				
+60			4.76	20.19
+68	=	±	GRAND VIEW RT	
TP	5.97	928.49	2.43	922.52

KP
DK
DS
PH

LT

26 RT

7

15.9 15.8 20.9 21.2 21.4 21.6 21.3 21.0 20.0 17.2 15.7
9.1 9.2 4.1 3.8 3.6 3.4 3.7 4.0 5.0 7.8 9.3
46 33 23 14 11 12 14 32 53 71

16.5 19.4 21.3
8.5 5.6 3.7
58 65 74
FE

14.0 13.8
11.0 11.2
100 86

16.5 14.3 21.0 21.2 21.6 21.8 21.5 21.2 20.5 19.5
8.5 8.7 4.0 3.8 3.4 3.2 3.5 3.8 4.5 5.5
48 31 22 14 11 12 14 31 51

19.4 21.7
5.6 3.3
60 73
FE

17.9 18.8
7.1 6.2
90 71

TOP MH 39' RT

21.9 19.6 17.5 17.2 21.0 21.4 21.8 22.0 21.7 20.2 19.2 17.9 16.6
3.1 5.4 7.5 7.8 4.0 3.6 3.2 3.0 3.3 4.8 5.8 7.1 8.4
73 60 45 29 20 14 11 13 42 66 100 169
FE

TOP PK 2 STA 76+00

STA	+	π	-	ELEV.
-----	---	-------	---	-------

		928.49		
--	--	--------	--	--

75+84				
-------	--	--	--	--

✓				
---	--	--	--	--

76+00				
-------	--	--	--	--

✓				
---	--	--	--	--

+50				
-----	--	--	--	--

✓				
---	--	--	--	--

LT

28 OCT 1971 8
RT

17.3	17.3	21.4	22.0	22.2	22.6	20.9	20.2	19.7
11.2	11.2	7.1	6.5	6.3	6.5	7.4	8.3	8.8
34	29	21	11		13	31	47	70

18.1	20.2	21.9	18.1
10.4	8.3	6.6	10.4
50	60	72	90
		FE	

17.3	17.8	21.5	21.7	22.3	22.5	22.3	21.3	18.2	17.3
11.2	10.7	7.0	6.8	6.2	5.9	7.2	10.3	11.2	
32	30	23	20	11	13	21	26	29	

17.3	19.3	22.1	15.4	16.4	16.1
11.2	9.2	6.4	13.1	12.1	12.4
35	52	70	70	56	47
		FE			

19.7	20.0	22.7	22.8	23.6	23.8	23.5	23.0	16.9	17.0
8.8	8.5	5.8	5.7	4.9	4.7	5.0	5.5	11.6	11.5
29	27	23	20	11	13	20	29	36	

18.6	18.2	19.8	20.8	23.1	14.3	15.9
9.9	10.3	8.7	7.7	5.4	14.2	12.6
31	33	34	49	66	70	53
				FE		

STA	+	π	-	ELEV.
		928.49		

77+00

✓

77+19

10.05

18.44

77+50

✓

+66 ± ENT LT (BT)

TP

8.90

934.22

3.17

925.32

LT

28 OCT. 1971

RT

9

21.6	24.1	24.5	25.1	25.3	25.0	24.6	18.3	18.5
6.9	4.4	4.0	3.4	3.2	3.5	3.9	10.2	10.0
30-35	26	20	11		13	19	30	45

22.4	24.4	24.4	17.6
6.1	4.1	4.1	10.9
36	44	62	70
FE			

FL S.END 12" CM 34' RT

25.2	24.3	26.4	26.9	27.0	24.7	26.3	22.9	22.6	22.6
3.3	4.16	2.1	1.6	1.5	1.8	2.2	5.6	5.9	5.9
32	23	19	11		13	20	33	45	60

FL 12" CM
S.END

25.5	25.5
3.0	3.0
47	58

23.6
4.9
80

26.4	26.5	27.1	27.4	27.5	27.3	26.8	23.9	24.0	23.6
2.1	2.0	1.4	1.1	1.0	1.2	1.7	4.6	4.5	4.9
60	46	25	11		13	20	32	40	60

TOP PK & STA 77+00

STA + π - ELEV.

934.22

77+73

✓

* +79 next page

78+00

✓

+14

7.82 26.40

+26

L7

28

Oct. 1971

RT

10

26.5 26.6 27.3 27.7 27.8 27.6 26.7 24.0 24.2
 7.7 7.6 6.9 6.5 6.4 6.6 7.5 10.2 10.0
 64 40 24 11 13 21 35 41

24.3 23.6
 9.9 10.6
 72 52

27.4 26.8 28.3 28.7 28.8 28.5 28.1 26.8 27.0
 6.8 7.4 5.9 5.5 5.4 5.7 6.1 7.4 7.2
 28 24 26 17 11 13 21 32 48

Ditch



29.3 30.2
 49 40
 40 65

27.5
 6.7
 66
 110

FL N. END 12" CM 25' RT

31.4 30.4 29.2 27.6 29.2 29.7 29.2 27.0 28.3 30.9 32.3
 2.6 3.8 5.0 6.6 5.0 4.5 5.0 7.18 5.9 3.4 1.9
 59 43 31 24-26 18 20 25 29 37 67
 Ditch FL S. END 12" CM 110

STA + π - ELEV.

934.22

* 77+79

✓

78+34

6.10 27.52

BM 1.85 934.20 1.85 932.37 932.35

+47

✓

KP
DS
PH

LT

F

28 OCT. 1971
CLOUDY R7
45°

11

27.2 26.5 27.3 27.9 28.0 27.7 27.2 25.2 26.4 29.4
7.0 8.66 6.9 6.3 6.2 6.5 7.0 9.0 9.8 9.8
27 23 19 11 13 20 29 35 40

FL N. END
12" CM

26.1 28.8
6.1 5.4
41 60

24.6 29.0
9.6 10.2
68 52

FL S. END 12" CM 26' LT

TOP HYDRANT S.W. COR CO. RD B2

32.7 32.0 30.7 30.4 30.1 30.3 29.8 30.1 33.0 32.5
1.5 2.2 3.5 3.8 4.1 3.9 4.4 4.1 1.2 1.4
66 48 40 26 25 28 33 44 62
TC G

32.8
1.4
70

STA + π - ELEV.
934.20

78+56

+63 = GUTTER LT ERT (S)

TP 7.36 939.14 2.42 931.78

+79 = $\neq$ CO. RD B²

✓

+97 = GUTTER LT (N)

LT

L

28 OCT. 1971

RT

12

31.7	30.8	30.8	30.4	30.5	30.4	30.9	31.4	32.1
2.5	3.35	3.4	3.8	3.7	3.8	3.3	2.8	2.1
62	44	36	35	33	42	59	74	
	MH	TC	G					

31.6	31.1	30.6	30.5	30.7	30.6	31.2	31.9	32.4
2.6	3.1	3.6	3.7	3.5	3.6	3.0	2.3	1.8
68	52	35	20	21	37	55	74	

TOP PK & STA 79+00

32.5	31.9	31.3	30.9	31.1	31.0	31.2	32.0	32.7
6.6	7.2	7.8	8.2	8.0	8.1	7.85	7.1	6.4
100	69	43	22	20	30	53	78	
					MH			

33.0	33.6	34.3	34.9	35.4	34.3	34.2	33.7	33.1
6.1	5.5	4.8	4.2	3.7	4.3	4.9	5.4	6.0
125	150	175	200	200	175	150	125	100

32.3	31.8	31.5	31.4	31.7
6.8	7.3	7.6	7.7	7.4
100	72	46	19	

STA	+	π	-	ELEV.
		939.14		

79+00 = GUTTER RT (N)

+12

+17

9.32 29.82

+32

+40 = $\frac{1}{2}$ ENT RT (DIRT)

+62

LT

28 OCT. 1971
RT

13

33.2 32.6 22.4 31.5 31.5 31.7 31.1 31.1 31.5 32.1
 5.9 6.5 6.7 7.6 7.6 7.36 8.0 8.0 7.6 7.0
 100 74 54 33 19 22 38 56 72

34.5 33.7 32.8 32.1 31.7 32.1 31.1 29.6 31.2 33.1 36.6
 4.6 5.4 6.3 7.0 7.4 7.0 8.0 9.45 7.9 6.0 2.5
 74 48 36 23 22 21 25 29 41 76
 TC G FL N END
 12" CM

FL N END 12" CM 25' LT

36.8 35.4 33.7 31.7 31.7 32.2 32.5 32.0 31.9 32.5 35.3 37.6
 2.3 3.7 5.4 7.4 7.4 6.9 6.6 7.1 7.2 6.6 3.8 1.5
 63 47 34 27 25 19 19 23 43 65 88

37.2 35.7 33.5 31.9 32.0 32.3 32.6 32.0 33.0 34.1 35.4
 1.9 3.4 5.2 7.2 7.1 6.8 6.5 7.1 6.1 5.0 3.7
 63 47 33 27 22 17 19 44 66 80

37.4 36.0 34.3 32.4 32.4 32.8 33.1 32.8 32.4 33.0 34.9 36.6
 1.7 3.1 4.8 6.7 6.7 6.3 6.0 6.3 6.7 6.1 4.2 2.5
 60 44 33 26 20 14 13 18 22 38 50

38.1
 1.0
 60

STA	+	π	-	ELEV.
-----	---	-------	---	-------

		939.14		
--	--	--------	--	--

79+96				
-------	--	--	--	--

		6.46		
--	--	------	--	--

			32.68	
--	--	--	-------	--

80+00				
-------	--	--	--	--

+16	ENT. LT (CONC.)			
-----	-----------------	--	--	--

+26				
-----	--	--	--	--

		6.26		
--	--	------	--	--

			32.88	
--	--	--	-------	--

+50				
-----	--	--	--	--

BM				
----	--	--	--	--

	3.20			
--	------	--	--	--

		940.98		
--	--	--------	--	--

			1.35	
--	--	--	------	--

				937.79
--	--	--	--	--------

				937.78
--	--	--	--	--------

LT

28 OCT. 1971

RT

14

FL S. END 12" CM 23' LT

37.9 36.9 35.3 33.9 33.6 33.7 33.5 33.1 33.8 35.9 38.4
 1.2 2.2 3.8 5.2 5.5 5.40 5.6 6.0 5.3 32 0.7
 75 64 44 29 12 13 20 22 39 59

37.2 35.3 34.6 34.2 33.8 33.9 33.7 33.4 33.9 36.9 38.8
 1.93 3.80 4.53 4.94 5.3 5.2 5.4 5.7 5.2 2.2 0.3
 71 50 43 31 12 13 21 22 45 61
 CONC. CONC. CONC. CONC.

FL N. END 12" CM 23' LT

* 38.2 36.7 34.7 33.4 34.3 34.3 34.3 34.1 33.9 34.5 37.7 39.1
 0.9 2.4 4.4 5.7 4.8 4.8 4.8 5.0 5.2 4.6 1.4 0.0
 61 44 30 23 19 12 13 20 22 44 56

TOP HYDRANT AT SEXTANT

STA + π - ELEV

940.98

80+70

✓

+79

✓

+91 = ~~ENT~~ RT (BT)

✓

KP
DS
LPO
PH

LT

E

29 OCT. 1971
CLOUDY RT
36°

15

34.4 38.5 34.4 34.4 34.6 34.4 34.3 36.0 34.9
6.4 7.5 6.6 6.4 6.4 6.6 6.7 5.0 3.1
27 22 18 11 13 21 34 48

37.0 38.3 38.1
4.0 2.7 2.3
42 58 67

39.2
1.8
70

36.5 34.7 33.7 34.5 34.6 34.7 34.5 34.7 35.6 36.5
4.5 6.3 7.3 6.5 6.4 6.3 6.5 6.3 5.4 4.5
38 28 23 18 11 13 22 39 56

38.1 38.5
2.9 2.5
54 71

37.3
3.7
73

34.8 33.9 34.6 34.7 34.8 34.7 35.6 37.0 37.6
6.2 7.1 6.4 6.3 6.2 6.3 5.4 4.0 3.4
28 23 18 11 13 27 43 62

36.9 38.2 38.2
4.1 2.8 2.8
40 56 67

38.2
2.8
78

STA + π - ELEV

940.98

81+00

✓

+34

4.20 36.78

+50

✓

+53

4.32 36.66

+59 = $\pm$ ENT RT (BT)

LT

29 Oct. 1971
RT

16

35.0 34.1 34.6 34.8 34.8 34.8 35.1 36.5 38.0

6.0 6.9 6.4 6.2 6.2 6.2 5.9 4.5 3.0
27 23 19 11 13 22 35 58

37.0 38.1 38.5 38.8

4.0 2.9 2.5 2.2
39 54 67 78

TOP MH 37' LT

36.6 34.9 34.0 35.1 34.9 35.0 34.9 35.1 36.1 38.3
4.4 6.1 7.0 5.9 6.1 6.0 6.1 5.9 4.3 2.7

35 27 22 17 11 13 24 37 53

38.1 38.8 39.1

2.9 2.2 1.9
50 68 72

TOP MH 36' RT

38.5 38.1 36.6 34.7 34.1 34.9 34.8 35.0 34.9 36.1 37.9 38.9

2.5 2.9 4.4 6.3 6.9 6.1 6.2 6.0 6.1 4.9 3.1 2.1
69 52 38 27 22 17 11 13 31 49 65

STA	+	π	-	ELEV.
		940.98		

82+00 = GUTTER LT (S)

+13 = ϕ SEXTANT (LT)

✓

+25 = GUTTER LT (N)

+50

TP 8.11 941.19 1.90 933.08

LT

29 OCT. 1971

RT

17

^{35.2} 5.8 80 ^{34.9} 6.1 54 ^{34.8} 6.2 28 ^{34.9} 6.2 11 ^{35.0} 6.0 ^{34.9} 6.1 14 ^{35.1} 5.9 23 ^{36.8} 4.2 32 ^{38.3} 2.7 49 ^{38.7} 2. 68

^{35.9} 5.1 125 ^{35.6} 5.4 100 ^{35.1} 5.9 62 ^{34.9} 6.1 38 ^{34.9} 6.2 11 ^{35.0} 6.0 14 ^{34.9} 6.1 23 ^{35.1} 5.9 34 ^{36.1} 4.4 50 ^{38.4} 2.6 70 ^{38.6} 2.4

^{36.0} 5.0 150 ^{36.1} 4.9 175 ^{36.2} 4.8 200

^{35.1} 5.9 84 ^{34.7} 6.3 58 ^{34.5} 6.5 32 ^{34.8} 6.2 11 ^{34.9} 6.1 ^{34.9} 6.2 14 ^{35.4} 5.6 31 ^{36.6} 4.4 40 ^{38.0} 3.0 56 ^{38.5} 2.5 76

^{37.6} 3.4 47 ^{35.9} 5.1 31 ^{33.6} 7.4 25 ^{34.4} 6.6 19 ^{34.6} 6.4 13 ^{34.8} 6.2 ^{34.6} 6.4 14 ^{35.3} 5.7 29 ^{37.0} 4.0 45 ^{38.2} 2.8 65

^{38.4} 2.6 74

TOP PK & STA 84 400

STA + π - ELEV

941.19

82+69 = $\angle$ ENT RT (BT)

✓

+86

410 37.09

83+00

✓

+41

LT

29 OCT. 1971 18
RT

38.8 36.6 33.4 34.1 34.5 34.6 34.5 34.5 36.0 37.3
2.4 4.6 7.8 7.1 6.7 6.6 6.7 6.7 5.2 3.69
58 33 25 21 14 13 23 36 49
✓ CONC.

39.2
2.0
74

39.8 38.6
1.37 2.55
93 69
GA CONC.

TOP MH 37' LT

38.6 36.1 33.1 33.7 34.1 34.3 34.0 34.3 36.7 38.3 39.6
2.6 5.1 8.1 7.5 7.1 6.9 7.2 6.9 4.5 2.9 1.6
50 33 25 21 14 13 24 40 60 85
✓

39.8
1.4
76

39.4 38.9 37.9 32.7 33.6 33.6 33.7 33.6 33.7 35.1 36.6 37.6 38.1
1.8 2.3 3.3 8.5 7.6 7.6 7.5 7.6 7.5 6.1 4.6 3.6 2.5
77 66 44 25 20 14 13 24 30 41 49 81
✓

STA + π - ELEV.

941.19

83+51 = $\angle$ ENT RT (GRAVEL)

✓

+65

✓

84+00

✓

LT

29 OCT. 1971

PT

19

39.2 38.6 35.8 32.7 30.5 33.5 33.7 33.4 33.1 34.7 36.5 37.5
2.0 2.6 5.4 8.5 7.7 7.7 7.5 7.8 7.5 6.5 4.7 3.
59 51 34 25 18 14 13 26 41 67 90

39.4

1.8
75

38.6 35.6 32.6 33.3 33.3 33.5 33.2 32.0 35.3 38.1 38.3
2.6 5.6 8.6 7.9 7.9 7.7 8.0 8.2 5.9 3.1 2.9
52 34 25 19 14 13 22 35 53 75

39.1

2.1
75

38.5 35.1 32.1 32.7 32.9 33.1 32.7 32.2 36.1 38.3 38.6
2.7 6.1 9.1 8.5 8.3 8.1 8.5 9.0 5.1 2.9 2.6
53 34 25 20 14 13 21 32 51 89
40

39.4

1.8
64

39.4

1.8
63

STA + π - ELEV.
941.19

84+37

✓

+65

✓

+77 = Φ ENT RT (BT)

✓

LT

29 OCT. 1971
R_T

20

30.6 34.7 31.7 32.1 32.4 32.6 32.2 31.9 35.6 31.4 31.4
 2.4 6.5 9.5 9.1 8.8 8.6 9.0 9.4 5.6 3.8 3.1
 55 34 25 21 14 0 13 23 34 54 77

39.4 39.5
 1.8 1.7
 67 80

36.5 33.4 31.0 31.0 31.9 32.0 31.7 31.4 32.4 32.6
 4.7 7.8 10.2 9.4 9.3 9.2 9.5 9.8 9.0 8.6
 49 35 25 19 14 ✓ 13 22 49 76

30.7 39.4
 2.5 1.8
 63 73

30.4 35.1 32.7 30.6 31.6 31.7 31.5 31.3 31.9 32.5
 2.8 6.1 8.5 10.6 9.6 9.5 9.7 9.9 9.3 8.7
 67 49 34 25 14 13 25 55 87
 GA

39.4
 1.8
 80

STA + K - ELEV.

941.19

85400

✓

-403

11.47 29.72

+11 GUTTER LT (S) ENT RT BT

+24 = 2 TRANSIT LT.

✓

BM 1.24 935.31 7.14 934.05 (934.07)

LT

29 OCT 1971
RT

21

31.3	30.1	30.9	31.0	31.2	31.0	30.9	29.20
9.9	11.1	10.3	10.2	10.0	10.2	10.3	11.99
31	25	20	14		13	23	24
							FL 15" CM

31.8	32.7
9.4	8.5
52	72

32.4	31.5
8.8	9.7
75	44

FL S. END 15" CM 24" LT

32.1	31.7	30.9	30.8	31.0	30.8	30.9	31.5	32.9
9.1	9.5	10.3	10.4	10.2	10.4	10.3	9.7	8.3
78	65	41	14		13	29	53	83

33.3	32.1	30.83	30.5	30.7	30.5	30.6	31.2	32.6
7.9	9.1	10.36	10.7	10.5	10.7	10.6	10.0	8.6
100	73	38	14		13	28	51	75

34.6	35.7
6.6	5.5
125	150

TOP HYDRANT NW Cor. Transit

STA + π - ELEV

935.31

85+28

6.42 28.89

+38 = GUTTER LT (N)

✓

+42

7.16 28.15

+50

86+00

TP 7.34 932.21 10.44 924.87

LT

29 OCT. 1971

RT

22

FL N. END 15' CM 25' RT

32.4	31.4	30.3	30.1	30.3	30.1	29.1	30.1	30.8
2.9	3.9	5.0	5.2	5.0	5.2	6.2	5.2	4.5
84	64	39	13	13	13	22	29	53

32.6
2.7
76

FL N. END 15" CM 24' LT

32.2	30.5	28.9	29.8	30.0	29.7	28.7	29.7	29.8	30.0
3.1	4.8	6.4	5.5	5.3	5.6	6.6	5.6	5.5	3.0
70	42	20	13	13	13	21	28	44	78

31.6	29.3	26.8	28.4	28.5	28.3	27.0	27.6	28.8	31.5
3.7	6.0	8.5	6.9	6.8	7.0	8.3	7.7	6.5	3.8
69	41	19	13	13	13	24	26	47	70

TOP PK & STA 87 +00

STA

+

π

-

ELEV.

932.21

$$86+31 = \cancel{f} \text{ ENT. RT. (BT)}$$

+50



$$87+00 = \cancel{f} \text{ ENT. LT. (BT)}$$



+50

LT

29 Oct 1977

RT

23

31.1	29.9	28.2	26.2	26.8	27.4	27.5	27.2	26.3	26.3	26.6
1.1	2.3	4.0	6.0	5.4	4.8	4.7	5.0	5.9	5.9	5.6
73	60	48	20	17	11	✓	13	28	55	87
										GA

31.0	29.8	26.8	25.7	26.2	26.8	26.8	26.5	25.7	25.0	25.7	25.5
1.2	3.4	5.4	6.5	6.0	5.4	5.4	5.7	6.5	7.2	6.5	6.7
71	49	32	20	17	11	✓	13	24	28	32	58

25.9

6.3

87

26.5	25.8	24.6	23.9	24.6	24.9	24.5	23.8	23.0	23.6
5.7	6.4	7.6	8.3	7.6	7.3	7.7	8.4	9.2	8.6
87	53	28	19	14	✓	13	24	28	32
GA									

22.1	22.8	24.0
10.1	9.4	8.2
82	61	48

24.9	23.8	22.7	22.0	22.6	22.9	22.5	21.8	21.1	21.5	21.5
7.3	4.4	9.5	10.2	9.6	9.3	9.7	10.4	11.1	10.7	10.7
66	55	38	23	13	✓	13	22	27	31	41

20.6

11.6

20.7

11.5

13

STA + π - ELEV.

932.21

BM 2.94 923.58 11.59 920.62 (920.64)

88+00

+22

7.41 16.17

+33 = GUTTER Lt & Rt (S)

+46 $\neq$ BROOKS Lt & Rt

+61 = GUTTER Lt & Rt (N)

LT

E

29 OCT. 1971

RT

24

TOP HYDRANT NW COR. BROOKS

✓

23.1	21.7	20.8	20.4	20.1	20.9	20.3	19.7	19.1	20.3	20.2	19.1
0.5	1.9	2.8	3.2	2.9	2.7	3.3	3.9	4.5	3.3	3.4	4.2
74	59	40	23	13	✓	15	24	27	29	38	70

FL S. END 15" CM 27' RT

✓

19.3	19.0	19.1	19.4	19.5	19.1	18.3	17.1	16.0
4.3	4.6	4.5	4.2	4.1	4.5	5.3	6.5	7.6
78	54	28	13	✓	13	30	53	78

✓

19.6	19.3	19.2	18.9	18.8	19.0	18.6	17.3	16.5	15.3	14.8	13.8
4.0	4.3	4.4	4.7	4.8	4.6	5.0	5.75	7.1	8.3	8.8	9.8
150	100	79	48	13	✓	13	37	60	87	100	150

MH

✓

18.8	18.4	18.2	18.4	18.1	17.3	17.2	15.2
4.8	5.2	5.4	5.2	5.5	6.3	7.4	8.4
73	43	13	✓	13	32	57	81

STA + π - ELEV.

923.58

88+70

9.66 913.88

TP 6.53 919.30 10.81 912.77

89+00

✓

+50

✓

LT

29 OCT. 1971
RT 25

FL 15" CM 33' RT N. END

TOP PK & STA 90+00

18.1	15.8	15.5	15.5	16.5	16.8	16.4	15.8	11.3	11.1
1.2	3.5	3.8	3.8	2.8	2.5	2.9	3.5	8.0	8.2
68	45	37	26	14	✓ 13	21	27	30	

18.5
0.8
90

14.5 14.5 09.3 09.8
4.8 4.8 10.0 9.5
64 51 41 31

16.6	15.1	13.4	13.1	14.6	14.8	14.4	13.8	06.5	06.5
2.7	4.2	5.9	6.2	4.7	4.5	4.9	5.5	12.8	12.8
75	50	38	25	14	✓ 13	20	29	40	

12.9 12.4
6.4 6.9
73 50

STA	+	π	-	ELEV.
-----	---	-------	---	-------

		919.30		
--	--	--------	--	--

90+00				
-------	--	--	--	--

✓				
---	--	--	--	--

+24				
-----	--	--	--	--

		9.09	10.21	
--	--	------	-------	--

TP	1.32	910.06	10.56	908.74
----	------	--------	-------	--------

90+50				
-------	--	--	--	--

✓				
---	--	--	--	--

LT

29 OCT 1971

RT

26

14.3	13.3	10.6	11.2	12.4	12.8	12.5	11.9	03.4	03.2
5.0	6.0	8.7	8.1	6.9	6.5	6.8	7.4	15.9	16.1
74	52	35	23	14	✓	13	21	35	47

11.0	10.5
8.3	8.8
78	60

TOP MH 38' LT

TOP PK 5 STA 91+00

09.3	08.3	09.6	10.4	10.9	10.4	09.9	00.5
0.8	1.8	0.5	10.3	10.8	10.3	0.2	9.6
44	32	22	14	✓	14	20	37

02.8
1.3
75

04.6	03.7	00.0
5.5	6.4	10.1
78	57	52

STA + π - ELEV.

910.06

91+00

✓

91+50

✓

92+00

✓

TP 2.75 904.05 8.76 901.30

RP
DS
DK
PH

LT

NOV 1971
CLOUDY
45°

RT

27

06.1	06.8	07.4	08.4	08.8	08.6	01.9	03.4	98.0
3.4	3.3	2.7	1.7	1.3	1.5	2.2	6.7	12.1
36	29	22	14		13	20	27	35

06.6	06.1	04.6
3.5	4.0	5.5
43	66	81

97.4	97.5
12.7	12.6
70	50

04.0	04.8	04.4	05.6	06.4	06.8	06.5	05.8	01.3	97.5
6.1	5.3	5.7	4.5	3.7	3.3	3.6	4.3	8.8	12.6
68	49	28	23	14		13	20	27	34

03.0
7.1
84

97.1	97.3
13.0	12.8
70	45

02.1	01.8	02.6	03.9	04.6	04.9	04.6	04.0	98.7	98.2
8.0	8.3	7.5	6.2	5.5	5.2	5.5	6.1	11.4	11.9
70	50	25	21	14		13	19	29	55

01.7
8.4
88

97.5
12.6
75

TOP PK to STA 93 +00

STA	+	π	-	ELEV.
-----	---	-------	---	-------

STA	+	π	-	ELEV.
-----	---	-------	---	-------

904.05

STA	+	π	-	ELEV.
-----	---	-------	---	-------

92+50

STA	+	π	-	ELEV.
-----	---	-------	---	-------

✓

STA	+	π	-	ELEV.
-----	---	-------	---	-------

93+00

STA	+	π	-	ELEV.
-----	---	-------	---	-------

✓

STA	+	π	-	ELEV.
-----	---	-------	---	-------

93+50

STA	+	π	-	ELEV.
-----	---	-------	---	-------

✓

LT

1 NOV. 1971
RT

28

3.0 1.9 1.2 2.2 2.8 2.0 2.8 1.9 897.1 897.2

1.1 2.2 2.9 1.9 1.3 1.1 1.3 2.2 7.0 6.9

54 42 25 21 14 13 22 27 48

3.6

0.5
75

897.4

6.7
75

3.6 899.9 899.8 0.7 1.2 1.3 1.1 0.3 898.2 897.2

0.5 4.3 4.3 3.4 2.9 2.8 3.0 3.8 5.9 6.9

52 29 24 21 14 13 18 26 39

4.1

0.0
75897.6
6.7
75897.3
6.8
50

1.3 898.6 898.6 899.2 899.8 899.9 899.3 898.4 897.2 896.7

2.8 5.5 5.5 4.9 4.3 4.2 4.8 5.7 6.9 7.4

40 27 24 21 13 13 26 44 55

3.9

0.2
57

4.1

0.0
65
110897.2
6.9
75896.8
7.3
60

STA + π - ELEV.

904.05

93+94

7.26

94+00 = GUTTER LT (S)

+14 = ~~E~~ OAKCREST & EXIT (RT) BT

✓

+31 = GUTTER LT (N)

+36

8.41

BM 0.63 901.96 2.74 901.31 901.33

LT

RT

NOV. 1971

29

FL S. END 18" ARCH CM 25' LT

898.8	898.7	898.1	899.2	898.5	897.9	897.2	897.3
4.3	5.4	6.0	5.9	5.6	6.2	6.9	6.8
75	46	23	13	13	34	67	
	MH						

1.5	0.5	899.7	898.5	897.9	897.0	897.5	897.2	897.4	897.9
2.6	3.6	4.4	5.6	6.2	6.1	6.6	6.9	6.7	6.2
100	80	60	36	13	13	31	52	75	

8
3
0.3
150

0.0	898.6	897.3	897.8	897.5	897.1	896.9	897.2	897.7
4.1	5.5	6.8	6.7	6.6	7.0	7.2	6.9	6.4
75	50	24	13	13	31	44	80	

FL N. END 18" ARCH CM 26' LT

TOP HYDRANT NW COR OAKCREST

STA + π - ELEV.

901.96

94+50

✓

+92 $\angle$ ENT RT (BT)

↓

95+00

↓

LT

1 NOV. 1977

RT

30

897.3	896.5	896.5	896.9	896.9	896.6	896.4	896.7	897.6
4.7	6.5	5.5	5.1	5.1	5.4	5.6	5.3	4.4
31	24-26	19	12		13	28	33	57

DITCH

897.5	898.1	900.0
4.5	3.3	2.0
38	45	60

898.0
4.0
80

897.3	897.1	895.0	895.5	896.1	896.6	895.6	895.3	895.3	894.7
4.7	4.9	7.0	6.5	5.9	6.0	6.4	6.7	6.7	7.3
38	34	23-25	19	12		12	31	56	85

DITCH

899.5	900.7	901.4
2.5	1.3	0.6
46	55	66

Ho

896.7	894.8	895.0	895.4	895.8	895.8	895.4	895.0	894.9	894.5
5.3	7.2	7.0	6.6	6.2	6.2	6.6	7.0	7.1	7.5
35	28	24-26	20	12		12	29	68	90

898.0	899.3	900.3	1.4
4.0	2.7	1.7	0.6
40	47	52	65

Ho

STA	+	π	-	ELEV.
-----	---	---	---	-------

		901.96		
--	--	--------	--	--

95+08				
-------	--	--	--	--

			387	898.09
--	--	--	-----	--------

+41				
-----	--	--	--	--

✓				
---	--	--	--	--

+69				
-----	--	--	--	--

✓				
---	--	--	--	--

+96				
-----	--	--	--	--

		9.66		
--	--	------	--	--

LT

- E 1 NOV. 1971

R7

31

TOP MH 40' LT

896.3	893.9	893.9	894.6	895.0	894.9	894.5	894.2	893.9	894.3
5.1	8.1	8.1	7.4	7.0	7.1	7.5	7.8	8.1	7.7
47	32	23	21	12		12	20	40	50

898.1	899.0	898.7
3.9	3.0	3.3
55	65	75

894.3
7.7
75

893.3	893.2	893.2	894.0	894.4	894.5	894.1	893.5	892.9	893.1	893.4
8.7	8.8	8.8	8.0	7.6	7.5	7.9	8.5	9.1	8.3	8.6
50	37	25	22	12		12	23	37	56	75

894.5
7.5
77

FL S. END 15" CM 28' LT

STA	+	Δ	-	ELEV.
-----	---	---	---	-------

		961.96		
--	--	--------	--	--

96400				
-------	--	--	--	--

+11	=	ENT LT (DIRT)		
-----	---	---------------	--	--

+20				
-----	--	--	--	--

		9.98		
--	--	------	--	--

+50				
-----	--	--	--	--

✓				
---	--	--	--	--

TP				
----	--	--	--	--

6.05				
------	--	--	--	--

900.68				
--------	--	--	--	--

7.33				
------	--	--	--	--

894.63				
--------	--	--	--	--

LT

1 NOV.

RT

32

^{894.3} 7.7 70
^{894.1} 7.9 54
^{893.9} 8.1 35
^{894.0} 8.0 23
^{894.0} 8.0 12
^{894.2} 7.8 12
^{893.7} 8.3 12
^{893.2} 8.8 21
^{892.4} 9.6 31
^{892.6} 9.4 48
^{892.9} 9.1 63

^{894.9} 7.1 74
^{894.5} 7.5 57
^{894.0} 8.0 38
^{894.0} 8.0 23
^{894.0} 8.0 12
^{894.1} 7.9 12
^{893.6} 8.4 22
^{893.1} 8.9 22
^{892.2} 9.8 33
^{892.3} 9.7 50
^{892.6} 9.4 63

FL N. END 15" CM 30' LT

^{892.8} 9.2 34
^{892.5} 9.5 29
^{893.7} 8.3 26
^{894.1} 7.9 20
^{894.3} 7.7 12
^{894.2} 7.8 12
^{893.7} 8.3 12
^{892.9} 9.1 21
^{891.3} 10.66 33
^{892.0} 10.0 50
^{892.1} 9.9 65

^{893.9} 8.1 37
^{894.7} 7.3 47
^{895.7} 6.3 70

TOP PK & STA 97+00

STA + π - ELEV.

900.68

96+65



+84 $\neq$ ENT. LT (BT)

97+00

+05



KIP
DS
DK
PH

LT

2 NOV. 1971
CLOUDY RT
450

33

891.8	894.5	894.3	894.4	894.4	893.7	893.0	891.7	892.1
8.89	6.2	6.4	6.3	6.3	7.0	7.7	9.0	8.6
30	30	20	12		14	22	35	70

FL 15"
SM
S. END

894.7	895.8	896.9
6.0	4.9	4.3
43	63	75

896.7	895.4	894.6	894.6	894.6	893.9	893.0	892.4	892.2
4.0	5.3	6.1	6.1	6.1	6.8	7.7	8.3	8.5
70	46	26	12		14	22	38	75

897.9	897.0	895.0	894.4	894.6	894.6	894.0	893.1	892.3	892.3
2.8	3.7	5.7	6.3	6.1	6.1	6.7	7.6	8.4	8.4
76	62	38	21	12		14	23	35	75

894.0	891.6	894.0	894.6	894.7	894.0	893.2	892.2	892.1
6.7	9.08	6.7	6.1	6.0	6.7	7.5	8.5	8.6
38	30	24	12		14	22	35	75

FL 15"
N END

896.0	898.1
4.7	2.6
46	75

STA

+

π

-

ELEV

900.68

97+50



+75



98+00



LT

L

2 NOV. 1971

RT

34

894.1 890.4 894.0 9.8 895.0 894.3 893.5 892.3 892.1
 6.6 10.3 6.7 5.9 5.7 6.4 7.2 8.4 8.6
 37 28-30 21 13 14 22 36 75

DITCH
 896.8 898.4
 3.9 2.3
 53 75

890.7 892.5 894.3 894.9 895.1 894.5 893.9 892.3 892.2
 10.02 8.2 6.4 5.8 5.6 6.2 6.8 8.4 8.5
 30 30 20 13 14 21 41 75

FL SEND
 15" ROP APRON

893.7 896.8 898.5
 7.0 3.9 2.2
 35 51 75

895.3 894.2 894.4 895.0 895.2 894.6 894.3 893.9 892.9 892.1
 5.4 6.5 6.3 5.7 5.5 6.1 6.4 6.8 7.8 8.5
 45 36 22 14 14 22 30 35 50

895.5 898.2
 5.2 2.5
 50 68

892.3
 8.4
 75

STA + T - ELEV.

900.68

98+13 @ Rose Pl. LT.

✓

+37

✓

+68

✓

LT

2 NOV, 1971

RT

35

894.9	893.0	894.4	894.9	895.2	894.6	894.2	892.4	892.2
5.8	7.66	6.3	5.8	5.5	6.1	6.5	8.3	8.5
46	32	22	14	14	27	50	75	

MH

896.8

3.9

70

890.4	892.6	894.0	895.0	895.3	894.8	894.4	892.2	892.3
10.34	8.1	6.7	5.7	5.4	5.9	6.3	8.5	8.4
34	34	24	14	14	23	58	75	

FL. N. END

15" RCP
APRON

892.8

7.9

38

893.4

6.3

75

893.2	891.9	893.7	895.1	895.4	894.9	894.7	892.5	892.5
7.5	8.85	7.0	5.6	5.3	5.8	6.0	8.2	8.2
34	31	31	14	14	23	47	75	

FL. S. END
12" CM

893.6

7.1

60

893.8

6.9

75

STA + π - ELEV.

900.68

98+89 = ∇ ENT LT (BT)

99+00

+07



+46



LT

E

2 NOV. 1971

RT

36

899.2	894.1	894.7	895.2	895.5	895.0	894.8	892.8	892.5
6.5	6.6	6.0	5.5	5.2	5.7	5.9	7.9	8.2
75	47	32	14	14	24	43	75	



894.3	894.2	894.3	894.6	895.2	895.5	895.1	894.8	893.0	892.7
6.4	6.5	6.4	6.1	5.5	5.2	5.6	5.9	7.7	8.0
75	68	50	30	14	14	23	38	75	



894.4	892.4	894.5	895.2	895.6	895.1	894.8	893.2	892.7
6.3	8.26	6.2	5.5	5.1	5.6	5.9	7.5	8.0
34	30	26	14	14	23	36	75	



FL NEND
12" CM

894.1	894.5
6.6	6.2
54	70



894.9	895.1	892.7	894.7	895.4	895.7	895.3	894.7	893.4	892.6
5.8	5.6	7.98	6.0	5.3	5.0	5.4	6.0	7.3	8.1
50	37	32	28	14	14	24	37	75	



FL 15" CM

895.0
5.7
70

STA + π - ELEV

900.68

99+56

5.56 895.12

+69 = $\angle$ ENT LT (BT)

BM

5.22 895.46 (895.47)

TP

7.22 903.15 4.80 895.88 (895.93)

99+86



LT

E

2 Nov. 1971

RT

37

$$\begin{array}{r} 7.94 \\ 1.65 \\ \hline 9.59 \end{array}$$

TOP MH 48' LT

895.5	895.4	895.5	895.5	895.7	895.4	899.8	893.2	892.8
5.2	5.3	5.2	5.2	5.0	5.3	5.9	7.5	7.9
75	50	32	14	14	23	40	75	

TOP HYDRANT AT ROSE PLACE
E STA 100+00

893.6	895.3	895.3	895.7	895.9	895.4	895.0	893.7	893.1
9.59	7.9	7.9	7.5	7.3	7.6	8.2	9.5	10.1
33	33	27	14	14	24	35	75	

FL 12" CM

895.5	895.7
7.7	7.5
54	75

STA + K - ELEV.

90315

100+00

+50

101+00

+44

7.42

+61

± ENT LT (DIRT)

+77

6.80

BM

3.69

899.46

899.45

LT

2 NOV 1971

RT

38

895.8	894.1	895.2	895.1	896.0	895.9	894.1	893.9	893.1
7.4	9.1	8.0	7.5	7.2	7.4	8.1	9.3	10.1
65	32	24	13	14	24	34	75	

896.3	895.0	894.3	895.1	896.1	896.2	895.9	895.2	893.9	893.1
6.9	8.2	8.9	7.5	7.1	7.0	7.3	8.0	9.3	9.5
71	37	33	22	13	14	22	41	75	

895.8	894.1	894.6	895.9	896.4	896.9	896.4	895.8	894.2	893.6
7.4	8.5	8.6	7.3	6.8	6.3	6.8	7.4	9.0	9.6
75	46	33	21	13	14	23	48	75	

FL 12" CM 33' LT S. END

897.4	897.2	897.1	898.0	897.6	7.2	894.1	894.1
5.8	6.0	5.5	5.2	5.6	6.0	8.5	9.1
75	26	12	14	23	48	75	

FL N END 12" CM 33' LT

TOP HYDRANT S. RR TRACKS

STA + π - ELEV.

BM 4.98 900.45

895.47

TP 4.52 895.93

BM 6.82 906.27 1.00 899.45 899.45

102+00

+30 = S. RAIL

+35 = N. RAIL

+44

+56

TP 3.02 906.48 2.81 903.46

LT

£ 3 NOV. 1971

RT

39

TOP HYD. AT ROSE PLACE

PK £ STA 100+00

TOP HYDRANT S. RR TRACKS

897.6	897.3	898.1	898.6	898.9	898.7	898.2	895.3	895.0
8.7	9.0	8.2	7.7	7.4	7.6	8.1	11.0	11.3
75	50	26	12	14	23	55	75	

900.4	899.4	899.6	899.5	899.3	899.0	899.6
5.89	6.39	6.72	6.81	7.01	7.26	7.69
100	50	25	14	50	100	

900.4	899.9	899.6	899.5	899.1	899.0	898.6
5.90	6.41	6.68	6.82	7.15	7.25	7.67
100	50	25	25	50	100	

898.7	898.8	899.8	899.8	899.2	898.4	897.3
7.6	7.5	6.5	6.5	7.1	7.9	9.0
100	51	14	22	50	75	

896.9	896.3	899.3	900.0	899.9	900.2	899.5	899.8	895.0
9.4	9.0	7.0	6.23	6.4	6.1	6.8	6.5	11.3
75	50	38	31	20	24	35	70	

£ STA 104+00

STA + - ELEV.

906.48

102+68

6.13 900.35

+75

+91

103+00 = GUTTER LT & RT.

+22 = ~~E~~ CO. RDC

✓

LT

E

3 NOV. 1971

RT

40

TOP MH30-RT

896.5	896.2	900.2	900.3	899.9	900.5	900.1	900.5	900.7	895.4	894.1
10.0	10.29	6.3	6.15	6.61	6.0	6.35	6.00	5.8	11.1	11.5
75	51	37	24	24		24	24	35	53	75
	SD		TC	G		G	TC			

900.2	900.5	900.5	900.1	900.7	900.4	900.9	901.4	901.1
6.3	6.0	5.95	6.41	5.8	6.09	5.70	5.1	5.4
75	45	27	27		30	30	55	75
		TC	G		G	TC		

900.1	900.2	900.4	899.5	900.8	900.7	901.1	900.5	901.0
5.83	6.30	6.05	6.98	5.7	5.79	5.35	5.98	5.52
75	75	52	52		46	46	75	75
6	G	TC	FL		G	TC	G	TC

901.3	901.0	900.8	900.9	901.2	901.1	901.0	900.6	900.2
5.2	5.5	5.7	5.7	5.3	5.4	5.5	5.9	6.3
150	100	75	24		24	50	100	150

STA + X - ELEV.

906.48

103+28

5.80 900.68

+33

5.60 900.88

+48 = GUTTER LINE LT & RT

+73

+89 ± ENT RT (BT)

104+00

X+33

TP 10.13 913.59 3.02 903.46

LT

E

3 NOV, 1971

RT

41

TOP MH43' LT

TOP MH 37' RT

901.2	900.7	901.1	900.3	901.2	901.8	901.3	900.6	901.2	900.5	901.0
5.34	5.80	5.40	6.22	5.3	4.7	5.2	5.86	5.38	5.95	5.46
75	75	TC	52	24	24	24	49	49	75	75
TC	G		FL				G	TC	G	TC

902.2	902.6	902.4	901.9	902.5	901.7	902.4	902.5	901.8
4.32	3.9	4.09	4.56	4.0	4.78	4.08	4.0	4.7
73	54	24	24	24	24	24	50	75
MH		TC	G		FL	TC		

902.9	903.4	903.0	902.5	903.0	902.4	903.1	902.6
3.6	3.1	3.52	4.01	3.5	3.96	3.4	3.9
80	65	24	24	24	24	45	75
		TC	G		G		

903.2	904.2	904.0	903.4	902.9	903.5	902.9	903.4	904.5	904.1	903.0
3.3	2.3	2.5	3.13	3.60	3.0	3.59	3.06	2.0	2.4	3.5
80	57	35	24	24	24	24	24	36	51	61
			TC	G		G	TC			

STA 104400

STA + π - ELEV

913.59

104+50

+64 $\neq$ ENT RT (BT)

+79

105+00

* +23

4.90 908.69

* +23

4.91 908.68

BM

3.35 910.24 (910.20)

LT

3 NOV 1971
RT

42

1.0 2.2 2.1 5.3 5.3 5.0 5.3 5.9 7.0 6.9
6.2 5.4 5.5 7.82 8.29 8.0 8.34 7.84 6.6 6.7
75 58 46 24 24 24 24 26 46
TC G G TC 40

9.0 8.8 6.9 5.9 6.3 6.0 6.1 5.3 4.5
4.6 4.8 7.22 7.70 7.3 7.60 7.5 8.3 9.1
75 49 24 24 24 38 60 74
TC G

10.4 10.3 9.5 7.2 6.7 7.0 6.6 7.1 8.0 8.1 6.2
3.2 3.3 5.1 6.42 6.91 6.6 7.03 6.54 5.0 5.5 7.4
75 55 41 24 24 24 24 38 50 75
TC G TC

13.2 11.9 10.8 9.4 8.2 7.8 9.1 7.6 9.1 9.0 9.2 6.4
0.4 1.7 2.8 4.2 5.40 5.84 5.5 5.97 5.48 4.6 5.4 6.8
75 60 54 42 24 24 24 24 30 48 75
TC G TC

FL CB 24' RT

FL CB 24' LT

TOP HYD 27' LT 104+50

STA	+	π	-	ELEV.
BM	6.66	906.15		(899.49)
TP	10.41	913.93	2.63	903.52
BM	7.12	917.41	3.64	910.29 (910.20)
TP	10.58	925.03	2.96	914.45
			1.42	923.61 (923.49)

BM	5.07	900.54		(895.47)
	6.88	906. ³³ 37	1.09	899.45 (899.49)
	11.60	915. ⁰⁸ 12	2.85	903. ⁴⁸ 52
			4.83	910. ²⁵ 29 (910.20)
	9.54	923. ⁹⁴ 98	0.68	914. ⁴⁰ 44
	11.63	935. ¹⁸ 21	0.39	923. ⁵⁵ 58 (923.49)
	8.00	940. ⁴¹ 44	2.77	932. ⁴¹ 44
BM			1.44	939.00 (938.92)
				938.97

LT

£

3 NOV 1971
RT

43

TOP HYDRANT S. OF RR TRACKS

TOP PK £ STA 104+00

TOP HYDRANT AT 27' LT STA 104+50

TOP PK £ STA 106+00

TOP HYDRANT LT STA 107+30

TOP HYDRANT AT ROSE PLACE

TOP HYDRANT S. OF RR TRACKS

PK £ STA 104+00

TOP HYDRANT 27' LT STA 104+50

PK £ STA 106+00

TOP HYDRANT LT STA 107+30

PK £ STA 110+00

TOP HYDRANT SW COR WOODHILL DR.

STA + π - ELEV

BM 13.37 923.57

910.20

*104+33

16.98 906.59

*105+23

+50

LT

4 NOV. 1971
E SUNNY RT
400

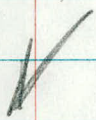
44

TOP HYDRANT 27' LT 104+50

TOP MH 44' LT



11.2	10.1	9.3	8.1	9.3	8.6	9.3	10.2
12.4	13.5	14.29	14.93	14.3	15.01	14.31	13.4
39	31	24 TC	24 FL		24 G	24 TC	33



16.2	16.2
7.4	7.4
48	75

7.9	9.4
15.7	14.2
56	47

17.0	12.2	11.0	11.1	11.2	10.8	11.2	10.3
6.6	11.4	12.6	12.5	12.4	12.8	12.4	13.3
40	29	22	11		24	29	41



18.8	18.1
4.8	4.9
61	75

09.8
13.8
60

STA + π - ELEV.

923.57

✓
105+92 = ~~E~~ ENT RT (DIRT)

✓
106+00

✓
106 SAME AS 106+00 (LT)

✓

LEXINGTON AVE.

X-SECTIONS
(72+00 - 75+00)REVISED
X-SECTIONS
72+00 - 75+00

Sunny 65°

Crew: R.M.

6-8-78

P.K.

P.D.

T.P.

STA

+

Δ

-

ELEV

929.31

72+00

✓

+07

+26

LT

C

RT

2 of 6

TOP HYD RT STA. 71+20

$$\begin{array}{r} 21.9 \\ \hline 45 \\ \hline 24.3 \\ \hline 22 \end{array} \quad 924.6 \quad \begin{array}{r} 24.3 \\ \hline 23 \end{array} \quad \begin{array}{r} 23.8 \\ \hline 31.6 \end{array} \quad \begin{array}{r} 25.5 \\ \hline 56 \end{array}$$

Trav.
Apron
15" C.M.C.

$$\begin{array}{r} 23.6 \\ \hline 70 \end{array}$$

$$\begin{array}{r} 923.4 \\ \hline 71 \end{array}$$

$$\begin{array}{r} 924.0 \\ \hline 21 \end{array}$$

$$924.4$$

$$\begin{array}{r} 924.1 \\ \hline 22 \end{array}$$

$$\begin{array}{r} 923.5 \\ \hline 32 \end{array}$$

$$\begin{array}{r} 924.0 \\ \hline 47 \end{array}$$

$$\begin{array}{r} 925.1 \\ \hline 80 \end{array}$$

$$\begin{array}{r} 920.59 \\ \hline 45 \end{array}$$

N. end 15" C.M.C.

STA

+

Λ

-

ELEV

121.23

✓

+50

✓

+65

✓

LT

C

RT

3 of 6

$$923.3 \quad \frac{922.9}{21}$$

$$\frac{22.5}{25}$$

$$\frac{22.1}{50}$$

$$\frac{920.8}{75}$$

$$\frac{22.4}{33}$$

$$\frac{22.4}{19}$$

$$922.9$$

$$\frac{22.5}{21}$$

$$\frac{22.6}{30}$$

$$\frac{21.1}{46}$$

$$\frac{20.2}{44}$$

$$\frac{23.1}{70}$$

$$\frac{20.3}{100}$$

$$\frac{19.7}{71}$$

$$\frac{19.2}{59}$$

+

π

-

ELEV

72+70

✓

73+00

✓

+50

✓

LT

E

RT

4 of 6

922.8

$$\frac{22.3}{22}$$

$$\frac{22.0}{26}$$

$$\frac{22.3}{31}$$

$$\frac{19.6}{72}$$

$$\frac{19.3}{58}$$

$$\frac{20.0}{50}$$

$$\frac{20.3}{100}$$

$$\frac{21.4}{30}$$

$$\frac{21.8}{16}$$

922.3

$$\frac{21.7}{19}$$

$$\frac{21.5}{25}$$

$$\frac{21.2}{48}$$

$$\frac{19.1}{48}$$

$$\frac{22.8}{71}$$

$$\frac{19.6}{100}$$

$$\frac{19.8}{77}$$

$$\frac{15.2}{59}$$

$$\frac{20.6}{26}$$

$$\frac{21.1}{16}$$

921.5

$$\frac{21.0}{16}$$

$$\frac{21.0}{22}$$

$$\frac{15.5}{39}$$

$$\frac{18.3}{40}$$

$$\frac{22.2}{74}$$

$$\frac{18.5}{85}$$

$$\frac{13.7}{62}$$

$$\frac{13.2}{52}$$

$$\frac{18.3}{100}$$

STA

+

π

-

ELEV

74+00

✓

+50

✓

75+00

✓

LT

E

RT

5 of 6

$$\frac{20.3}{22}$$

$$\frac{20.5}{15}$$

921.0

$$\frac{20.6}{14}$$

$$\frac{20.4}{22}$$

$$\frac{15.1}{43}$$

$$\frac{16.1}{35}$$

$$\frac{15.6}{46}$$

↓

↓

$$\frac{12.8}{67}$$

$$\frac{12.3}{50}$$

$$\frac{21.7}{74}$$

$$\frac{16.9}{81}$$

$$\frac{17.1}{100}$$

$$\frac{20.2}{20}$$

$$\frac{20.7}{12}$$

921.1

$$\frac{20.6}{11}$$

$$\frac{20.0}{20}$$

$$\frac{14.4}{38}$$

$$\frac{15.1}{35}$$

$$\frac{16.3}{49}$$

↓

$$\frac{16.8}{82}$$

$$\frac{11.7}{62}$$

$$\frac{21.7}{75}$$

$$\frac{20.7}{21}$$

$$\frac{21.0}{12}$$

921.2

$$\frac{20.8}{12}$$

$$\frac{20.3}{22}$$

$$\frac{13.8}{41}$$

$$\frac{15.7}{34}$$

$$\frac{15.9}{50}$$

↓

$$\frac{15.8}{100}$$

$$\frac{15.4}{79}$$

$$\frac{12.3}{67}$$

$$\frac{21.4}{74}$$

STA

+

不

www.elsevier.com/locate/jmb

ELEV

B M

922.85 922.88

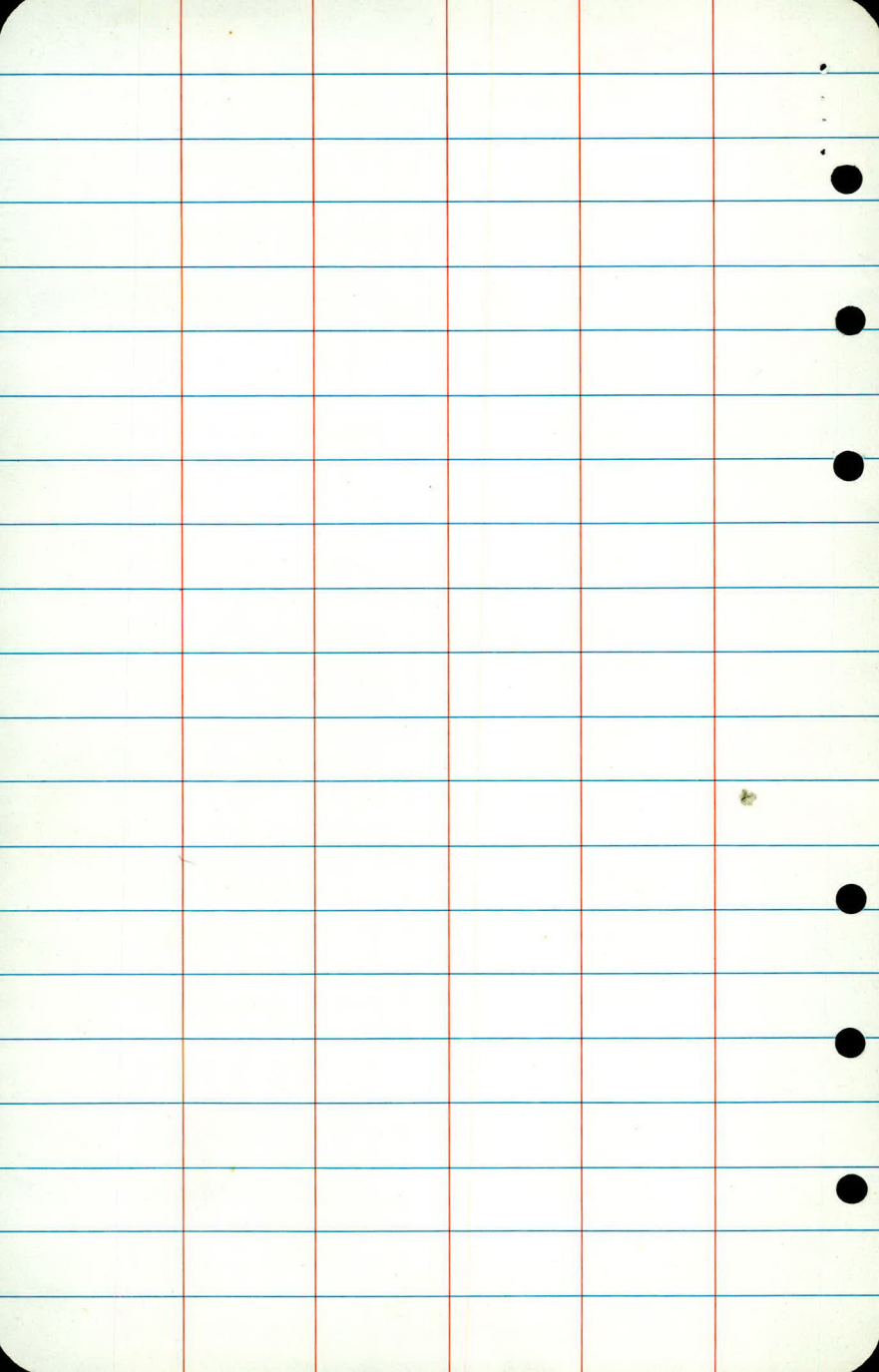
LT

¢

RT

6 of 6

TOP HYD. N.E. COR. GRANDVIEW



X-SECTIONS RT.
LEXINGTON AVE
(96+11 - 102+00)

CREW: R.M

6-12-78

P.K

Sunny

P.D

T.P.

X-SECT. EXTEND
RIGHT
CAL + 100 - 102+00

901.33

T.P.

894.47

96+11

+50

+84

97+00

+50

98+00

+68

99+00

RT.

100

150

2 of 3

Top Hyd. N.W. Cor. Oakcrest

892.4

92.4

91.6

91.9

91.9

91.9

92.2

91.9

91.9

91.9

92.3

92.3

92.5

92.4

92.7

92.3

99+46

100+00

+50

T.P.

893.28

101+00

+61

102+00

£ Bike Path

899.40 899.45

RT

100

150

3 of 3

92.7

92.7

93.2

92.9

93.3

92.9

93.3

92.8

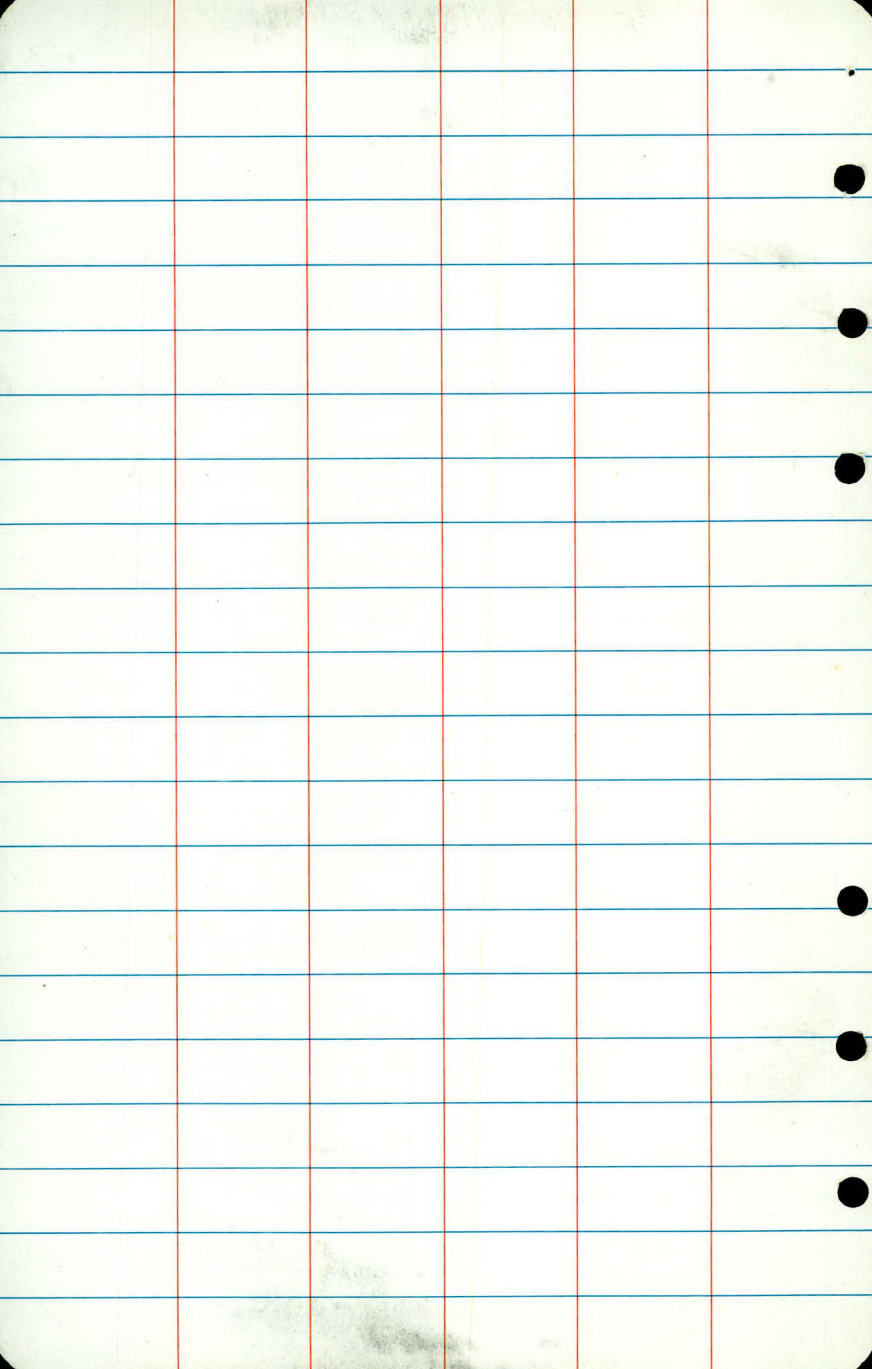
93.7

93.2

94.6

93.9

Top Hyd S. R.R. Tracks



ML
MR
SE

MAY 23, 79

CLOUDY 47°

ENTRANCE PROFILE GRADES

HO # 2062 + 2096 LEXINGTON AVE

+

K

-

ELEV

3.95

958.30

954.35

41+68

ENT RT (2062 So)

42+67

ENT RT (2062 No)

42+89

ENT RT (2096 So)

43+90

ENT RT (2096 No)

B.M.

2.16

956.14

956.15

LT

E

RT

✓ 53.71	✓ 53.5	✓ 53.1	✓ 52.7	
4.53	4.8	5.2	5.6	5.4
	12	25	48	67

✓ 54.41	✓	✓	✓	✓	✓
	54.1	54.0	54.3	54.3	54.2
3.89	4.2	4.3	4.0	4.0	4.1
	12	21	43	50	71

✓ 54.60	✓ 54.3	✓ 54.3	55.8		
				56.2	56.9
3.70	4.0	4.0	2.5	2.1	1.4
	12	18	46	58	83

✓ 54.61	✓ 54.3	✓ 54.1	✓ 55.7	✓ 56.2	✓ 57.0
3.69	4.0	4.2	2.6	2.1	1.3
	12	19	42	50	67

