

OFFICE OF COUNTY ENGINEER
RAMSEY COUNTY, MINN.

PLAN Survey

LEXINGTON AVENUE

From LARPENTEUR To S.T.H. 36
AVENUE

Road Acc't. No. 51

Date Filed _____

File _____

ML
MR

MAY 18, 79

PROFILE GRADE

ENTRANCE TO NORTH STAR BANK

LEXINGTON AVE

STA	+	π	-	ELEV
	294	951.57		948.63

13+44

2

944.82
6.75
24

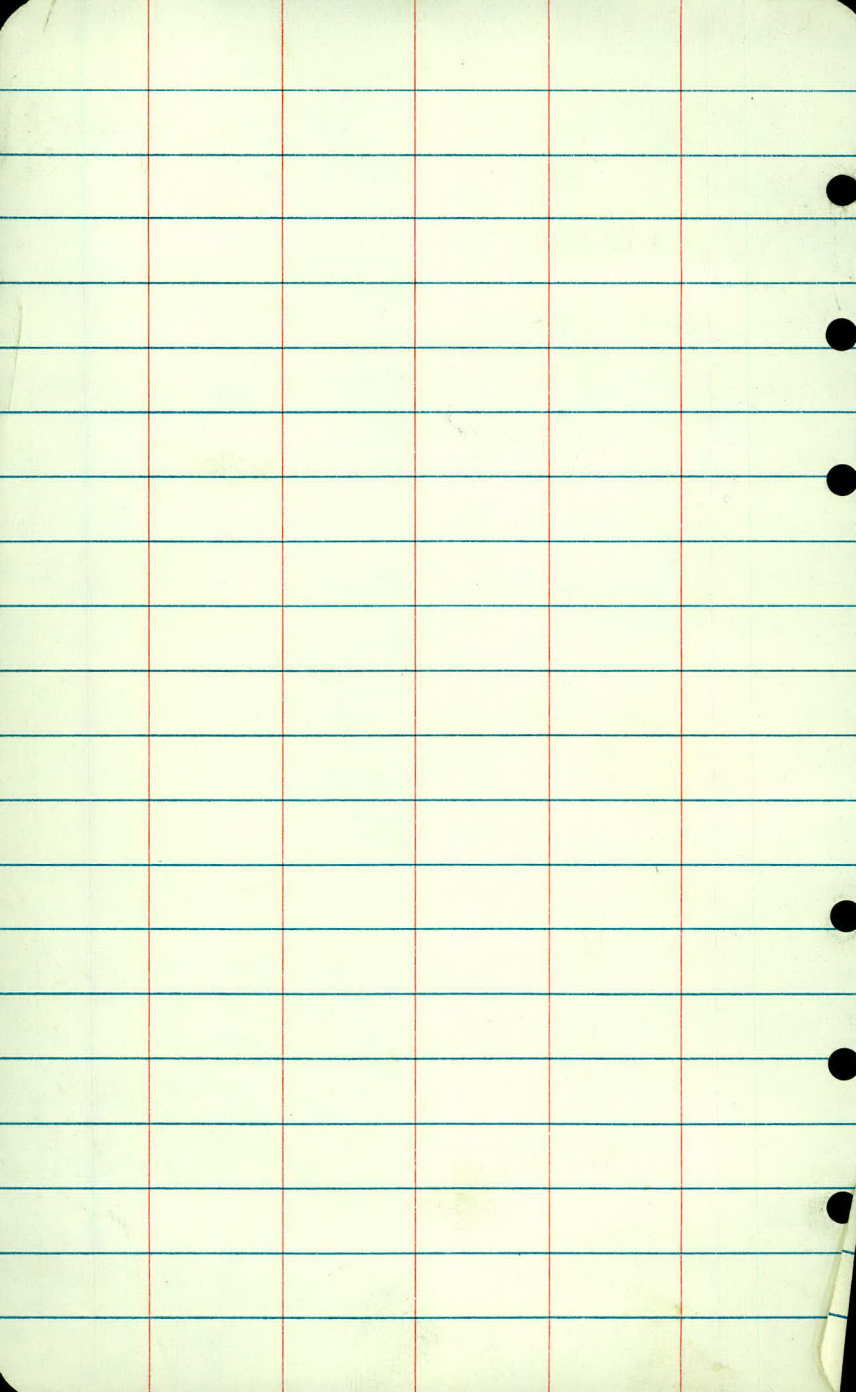
945.33
6.74
34

945.98
5.59
44

946.72
4.85
54

947.40
4.17
64

947.82
3.75
74



Lexington Ave.

2

Alinement

Alinement

Larp to Roselawn

pages 2-8

Sta.

Pt.

 ΔLT ΔRt

Defl.

18

17

16

0+00

12'

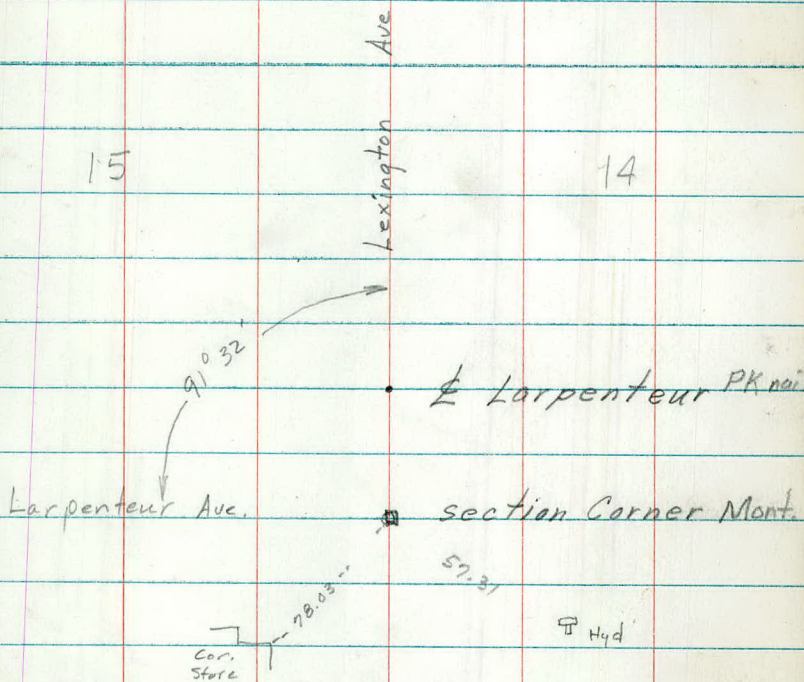
0+00

FK
HP
RG
DK

March 24, 1971

3

SE 1/4 Cor Sec 15, 29, 23



Sta

Pt

Δ LT

Δ RT

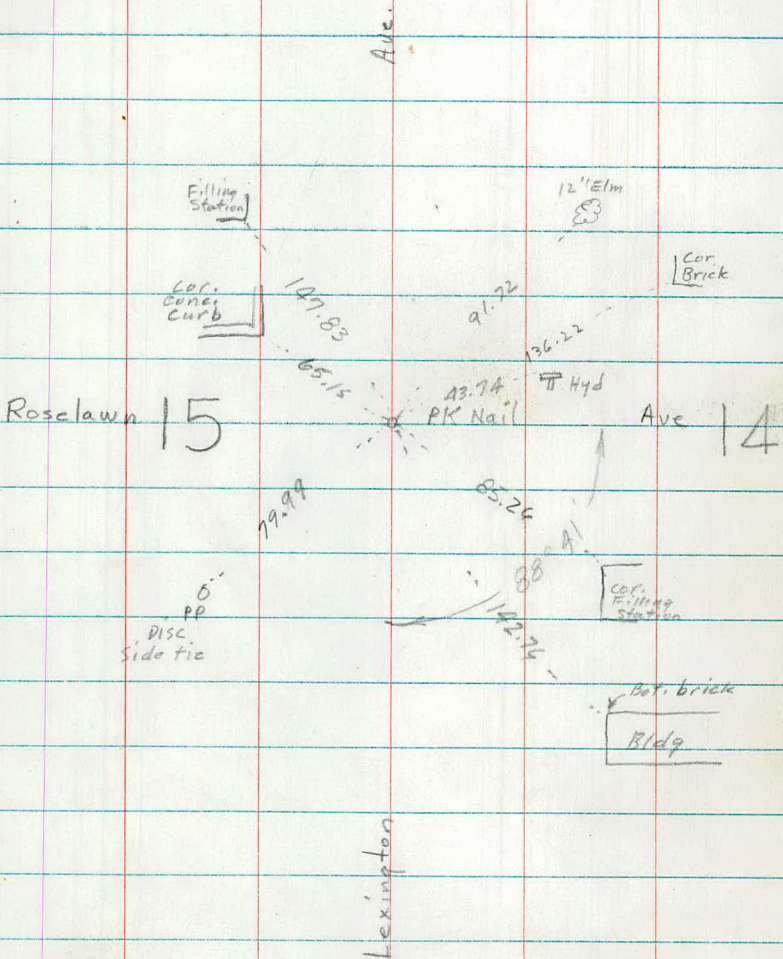
Defl.

26+27.94 P.I.

March 24, 1971

4

E 1/4 Sec 15, 29, 23



Sta

Pt

ΔL

ΔR

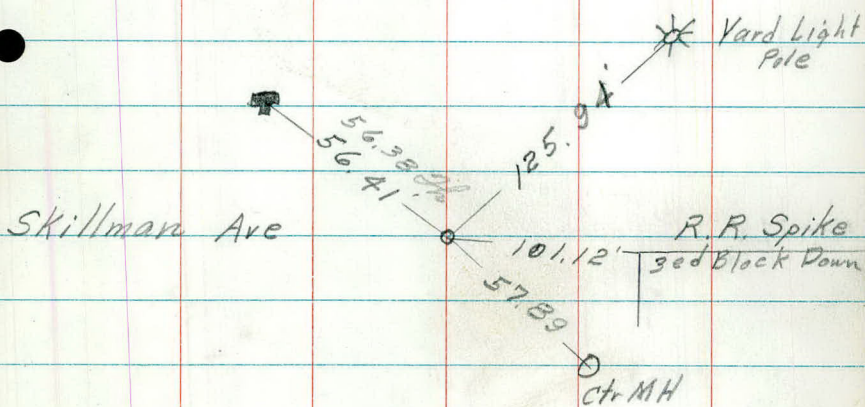
Defl.

221-2393

39+40.94 P.O.T.

March 24, 1971

5



105 (66)
(98)

Sections 10-11-14+15
F/g 8

2140

Br. Cone.
Base



93.66'

Ave.

Co. Rd

"B"

51.82'

Hyd.

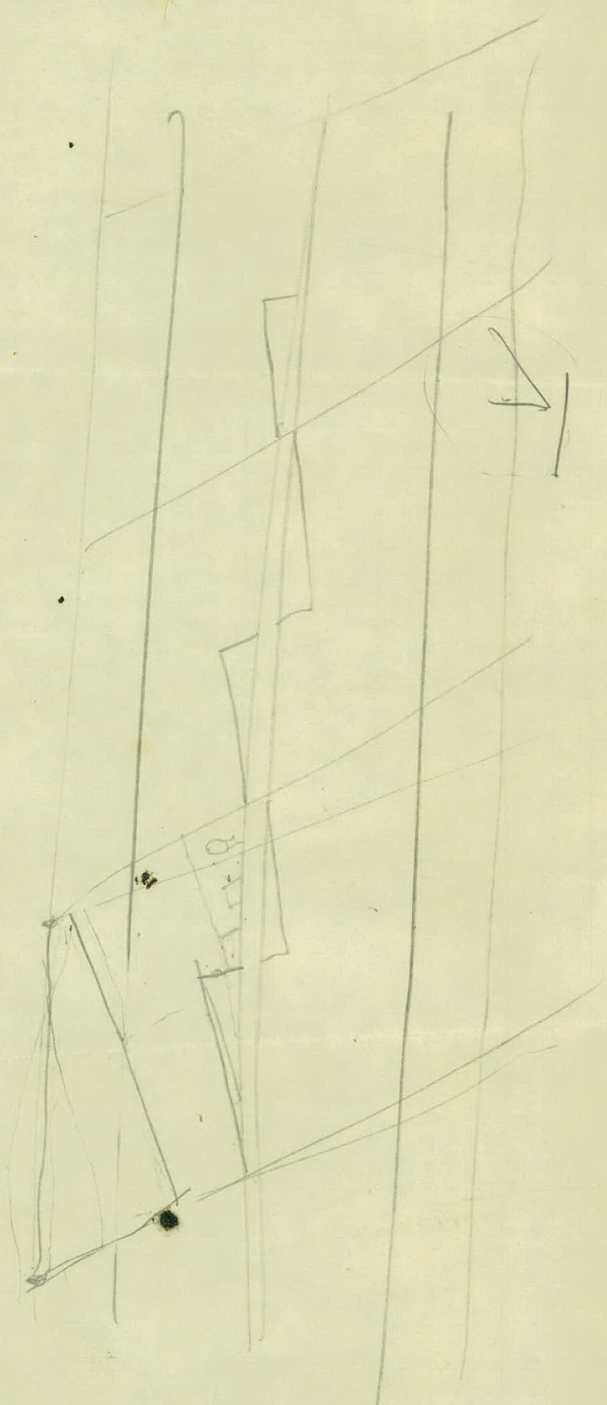


68.51'



Lexington

McMenamy
4236
Lexington



March 24, 1971

6

Section Corner to Sections

10-11-14 & 15

(NE $\frac{1}{4}$ Cor. Sec. 15, 29, 23)

78+80.23

10

11

72+11.12

S.E. Corner
Steel Plate of Sign

S. 1/2 - Corner Bottom
Cast Iron Base

52+54.23
State

Co Rd

2+00 "B" "B" Bent Nail

S.W. Corner
Flood Light

Hyp.

15

14

Note: Sum of Angles = $359^{\circ}58'$

Sta

Pt.

$\Delta L +$

$\Delta R +$

Defl.

78+79.50

P.I.

E 1/4 Cor Sec 10, 29, 23

7

Ave.

90° 10'

Disc PP
O

91° 48'

T.P.
O Disc

40.67

52.21

Co. Rd

10

68.9

3" Maple
No tie Nails
or disc.

Hyd.

44.84

105.13

7th Brick
from Top

SW
Cor Ho.

88° 10'

11

B²

89° 52'

Lexington
2624.75 R

Sta

Pt.

ΔL

ΔR

Defl.

NE 1/4 Cor Sec 10, 29, 23

8

Ave

3

2

Cor. Ho.
Fndn.

45.57



66.80

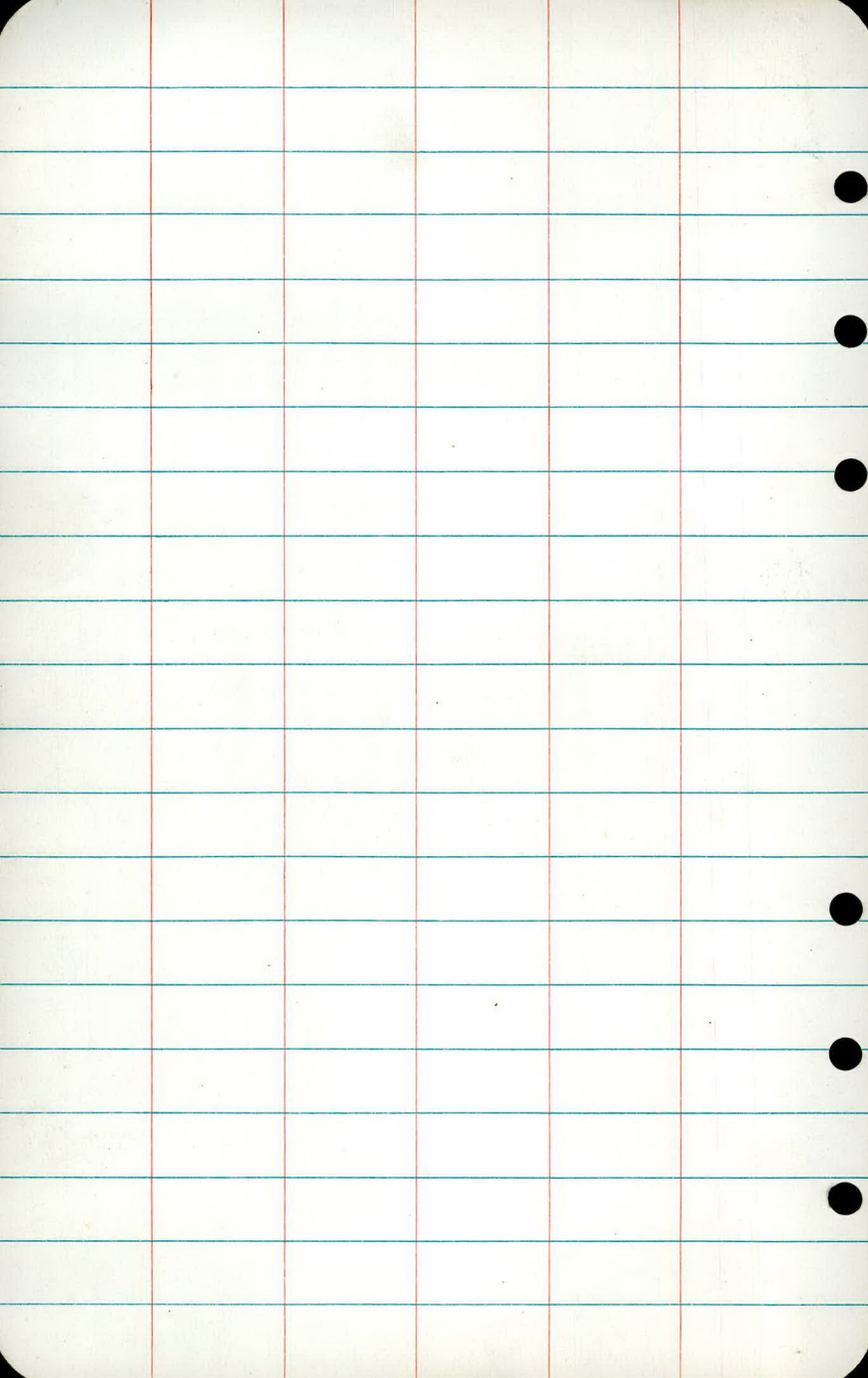
12" O.
91° 09'

89° 05'

10

11

Lexington



KP
WS
DS
GA
DK

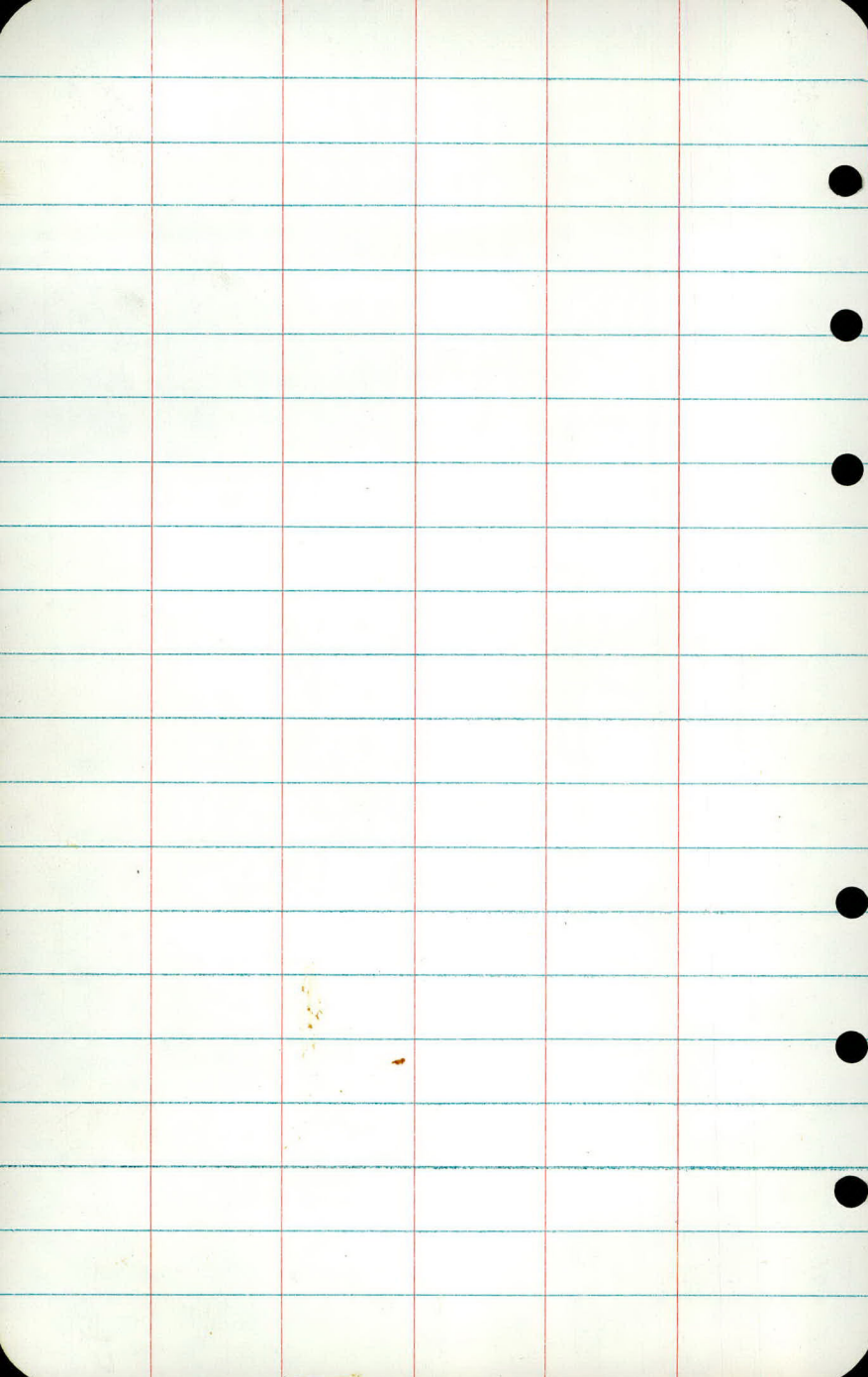
LT

31 MAR 1971
CLOUDY
40° RT

0°40'0

Co. RD "B"

LEXINGTON AVE



KP
WS
DS
GA
DK

LT

31 MAR. 1971
cloudy
40° RT

$0^{\circ}38'22.5''$



ROSELAWN AVE

$2^{\circ}33'30''$
4

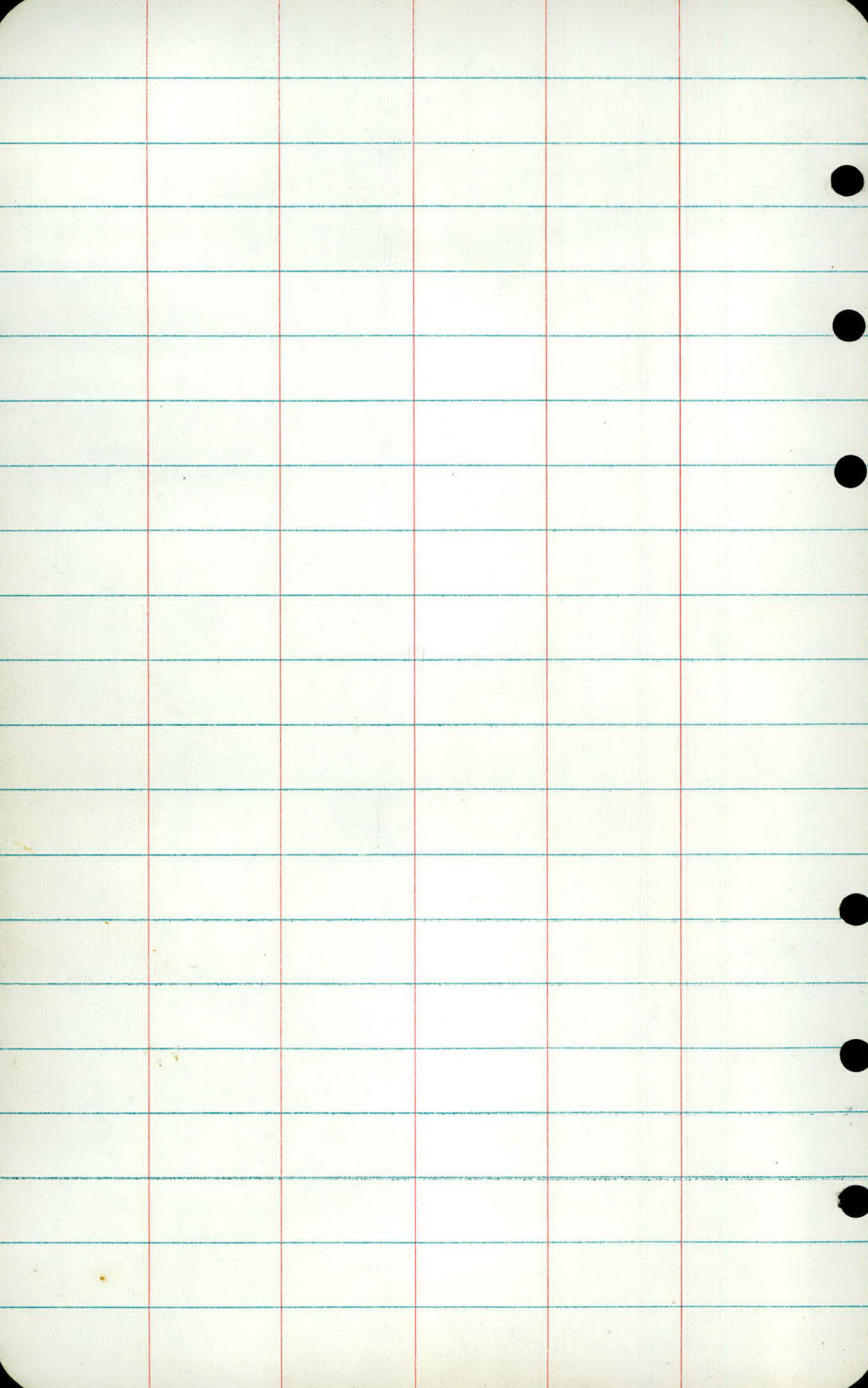
$0^{\circ}38'22.5''$

4 | 153 - 90

$\frac{12}{33}$ $\frac{9}{10}$
 $\frac{8}{20}$

AVE

LEXINGTON



62-651-01 C.T.B.

TOPOGRAPHY

LT

L

RT

✓ +16 TEL

39

✓ +72 LITE

35

✓ +06 Begin Conc. Curb +34 PP

33

29

✓ +06 Conc

28-33

Curb

Curb

23

23

2

✓ +82 E Bit Ent (46')

✓ +88 Cor Conc

33

✓ +69 Cor Conc

66

✓ +53 Cor Conc

29

+51.5 30' BIT ENT

✓ +48 Cor Conc

33

✓ +42 PP

27

✓ +32 Pump Island

End Conc. 53-57

✓ +05 curb

33

Conc.

Curb

Curb

Begin Conc Curb

23

23

✓ +95

33

✓ +95 Pump IS

53-57

✓ +89 PP

28

✓ +91

TEL Booth

34

✓ +72 E Bit Ent (31')

✓ +48 ST. SIGN

36

+58 END Conc

✓ +46 Conc Curb

33

+38 SEM SIGN

34

✓ +49 Mont

29

✓ +47 Cor Bit

35

+44 Sem Sign

31

0

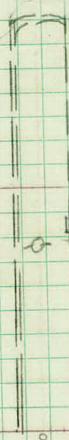
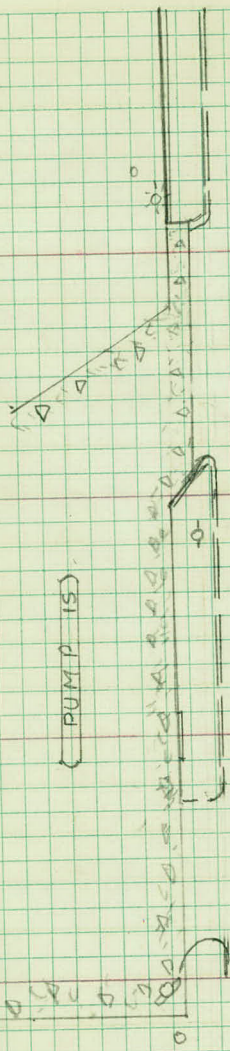
LT

£

RT

6

BIT.
PARKING LOT



5

LT

£

RT

✓ +97 LITE

45 + 97 LITE
35

✓ +80 £ 30' BIT ENT

✓ +32 £ 28' BIT ENT

4

✓ +85 £ 28' BIT ENT

✓ +95 Conc Cor
77✓ +82 PP
29✓ +67 LITE
36✓ +74 Conc Cor
33

+56 PP

49

✓ +41 £ 28' BIT ENT

✓ +25 LITE
35✓ +25 END CONC. COR
33✓ +25 Bush
333 ✓ END HEDGE
33✓ +65 Begin Hedge
33✓ +65 Bush
37✓ +63 Bush
31✓ +63 SIGN
36

✓ +72 £ 30' ENT

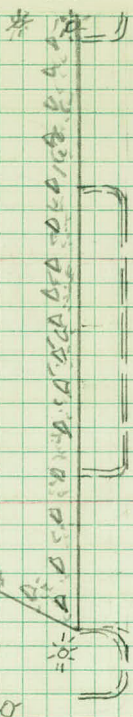
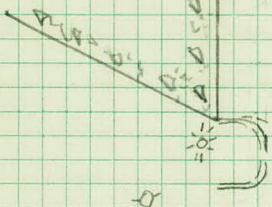
1972

LT

2

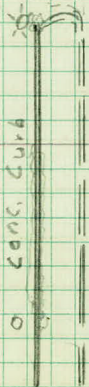
RT

C



BIT. PARKING LOT

2.5 x 5.5
5.5 x 5.5



0 Conc. Curb

LT

E

RT

$$\checkmark +33 \frac{PP}{30}$$

7

$$\checkmark +02 \frac{Hyd}{41} +06 \frac{Cor PKg Lot (BT)}{39}$$

 $\checkmark +94 \text{ } \frac{9' \text{ Bit sidewalk}}{24-60}$

$$\checkmark +98 \frac{PP}{30}$$

$$\checkmark +44 \frac{Cor Conc \& ER}{33}$$

6

$$\checkmark +00 \frac{Conc}{33}$$

 $+63 \text{ } \frac{E \text{ Ent (32' Bit)}}{47}$

$$\checkmark +51 \frac{Edge Conc.}{47}$$

$$\checkmark +34 \frac{PP}{30} +42 \frac{Cor Conc + BR}{32}$$

$$\checkmark +08 \text{ Conc Cor } 33$$

$$\checkmark +29 \frac{GB}{26}$$

$$\checkmark +12 \text{ } \frac{E \text{ Ent 25' (Bit)}}{26}$$

5

LT

E

RT

1972 d

Bit. Sidewalk

Bit,
Parking
Lot.

DIONNE AVE.

Bit. Sidewalk

10

LT

F

RT

$$\checkmark +87 \frac{PP}{29}$$

$$\checkmark +73 \frac{Sign \ 2\frac{1}{2} \times 4 \ Base}{42}$$

$$\checkmark +54 \text{ Ent } 26' \text{ Bit}$$

9

$$\checkmark +84 \frac{L^+ \text{ pole } 2 \times 2 \ Base}{36}$$

$$\checkmark +51 \frac{Sign \ 2\frac{1}{2} \times 6 \ Base}{43}$$

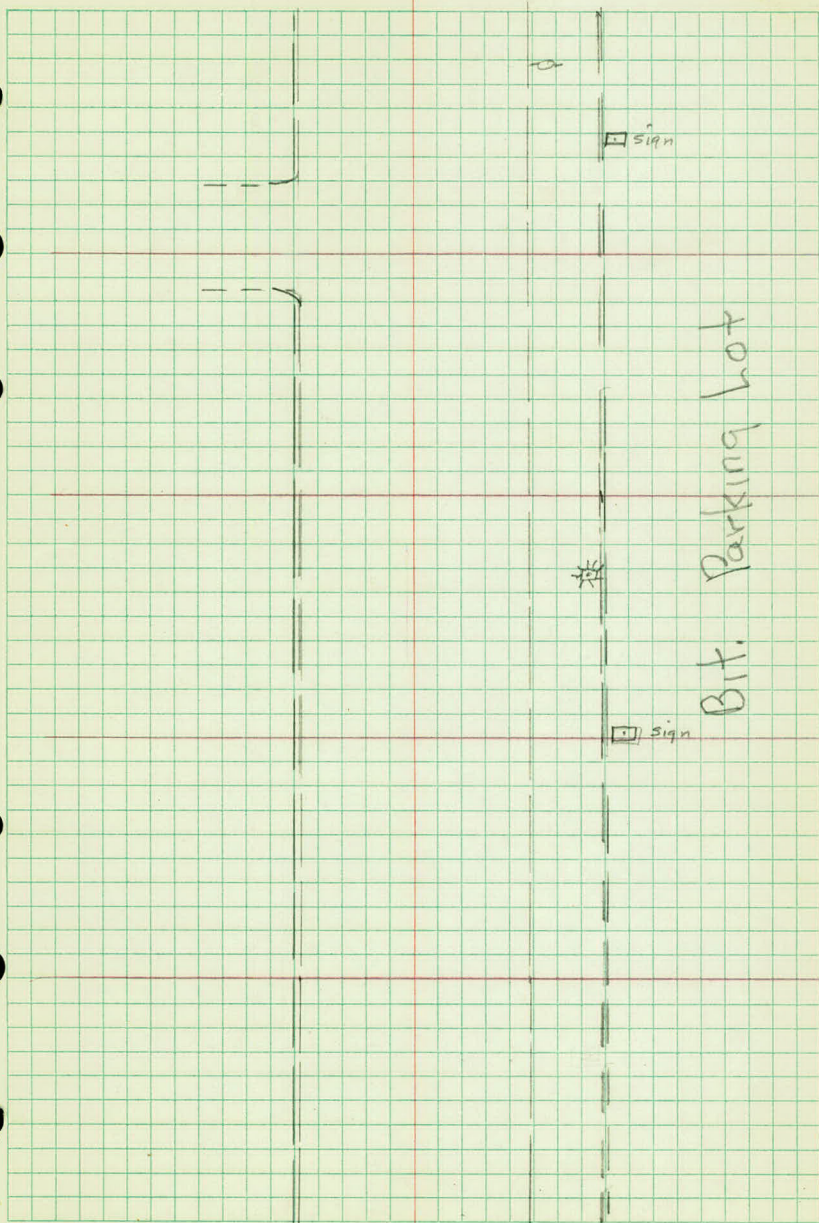
8

LT

\$

1972
RT

e



LT

E

RT

$$\checkmark \quad +45 \quad \begin{array}{r} 12'' \text{ Maple} \\ 33 \end{array}$$

$$\checkmark \quad +32 \text{ \& 17' Ent (Bit)}$$

$$\checkmark \quad +15 \quad \begin{array}{r} 24'' \text{ Maple} \\ 49 \end{array}$$

12

$$\checkmark \quad +44 \quad \begin{array}{r} \text{Pkg Lot} \\ 43 \end{array}$$

$$\checkmark \quad +28 \text{ \& Bit Ent 30'}$$

$$\checkmark \quad +10 \quad \begin{array}{r} \text{Pkg Lot 2 pt} \\ 34 \end{array}$$

$$11 \quad \checkmark \quad +00 \quad \begin{array}{r} \text{Cor Pkg Lot} \\ 57 \end{array}$$

$$\checkmark \quad +65 \quad \begin{array}{r} \text{Cor Pkg Lot} \\ 37 \end{array}$$

10

LT

£

RT

1972
f

Bit. Parking Lot

ROMA AVE.

Bit.
Parking
Lot

15

$$+88 \begin{array}{r} 10'' \text{ BE} \\ \hline 54 \end{array} \quad \begin{array}{r} \text{(dead)} \\ 20'' \text{ BE} \\ \hline 69 \end{array}$$

$$+81 \begin{array}{r} 10'' \text{ Pine} \\ \hline 49 \\ 8'' \text{ Pine} \\ \hline 52 \end{array}$$

$$\checkmark +66 \begin{array}{r} 18'' \text{ Elm} \\ \hline 69 \end{array} \quad \checkmark +67 \begin{array}{r} 24'' \text{ BE} \\ \hline 52 \end{array}$$

$$\checkmark +41 \begin{array}{r} 20'' \text{ Elm} \\ \hline 51 \end{array}$$

$$\checkmark +100 \begin{array}{r} (12' \text{ tall stump}) \\ 36'' \text{ BE} \\ \hline 51 \end{array}$$

$$\checkmark +19 \begin{array}{r} 12'' \text{ Pine} \\ \hline 52 \end{array}$$

$$14 \quad \checkmark +98 \begin{array}{r} \text{dead } 36'' \text{ BE (tall stump)} \\ \hline 51 \end{array}$$

$$\checkmark +70 \begin{array}{r} 12'' \text{ Pine} \\ \hline 52 \end{array}$$

$$\checkmark +57 \begin{array}{r} 10'' \text{ Apple} \\ \hline 57 \end{array}$$

$$\checkmark +08 \text{ Garden Ave} \quad \checkmark +25 \text{ Bit. Ent (26')}$$

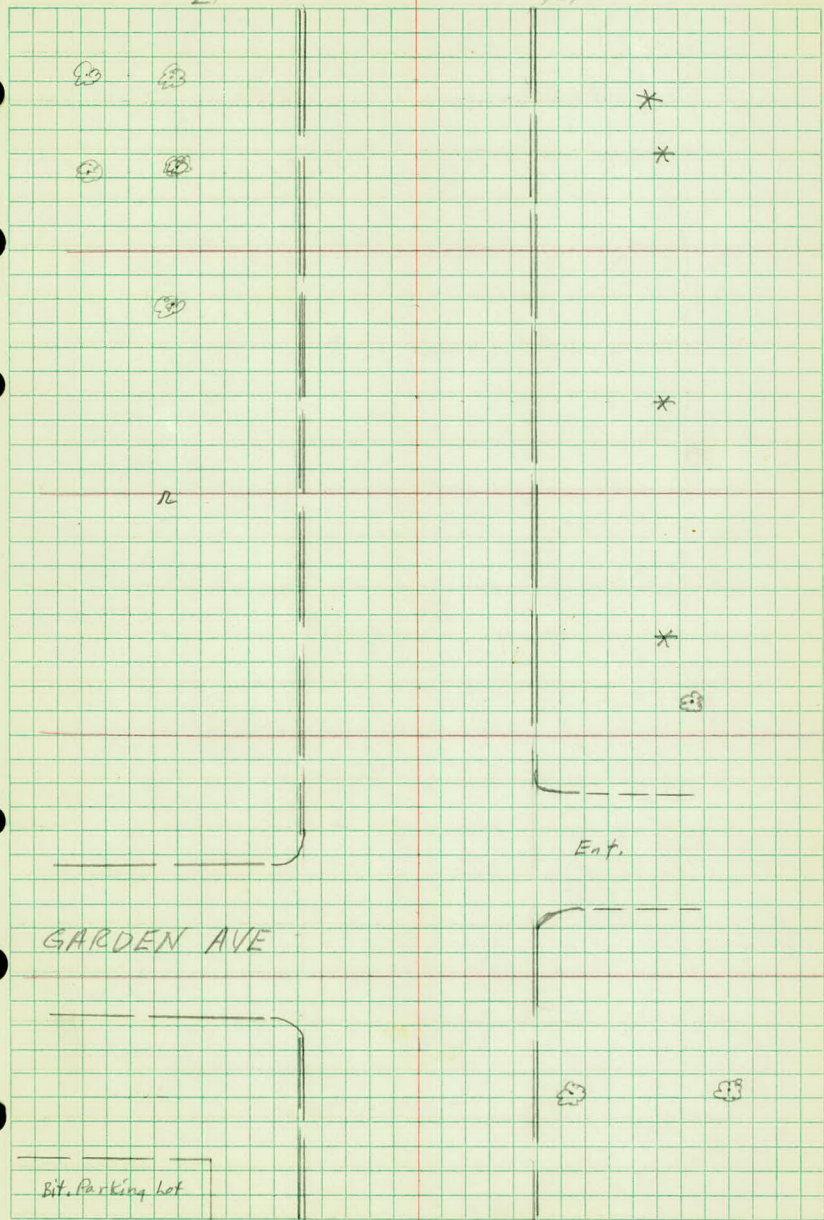
13

$$\checkmark +63 \begin{array}{r} \text{cor. Rky Lot} \\ \hline 43 \end{array}$$

$$\checkmark +76 \begin{array}{r} 14'' \text{ Maple} \\ \hline 32 \end{array} \quad \checkmark +77 \begin{array}{r} 14'' \text{ Maple} \\ \hline 65 \end{array}$$

Lt

Rt



GARDEN AVE

Ent.

Bit. Parking Lot

✓ +40 $\frac{10'' \text{ Poplar}}{36}$ ✓ +43 $\frac{3'' \text{ Maple}}{53}$

✓ +31 $\frac{1'' \text{ Maple}}{46}$

✓ +23 $\frac{1'' \text{ Maple}}{51}$ ✓ +11 $\frac{4'' \text{ Maple}}{36}$

17 ✓ +09 $\frac{8'' \text{ Pine}}{50}$

✓ +00 $\frac{36'' \text{ Elm}}{37}$ ✓ +09 $\frac{36'' \text{ Elm}}{49}$

✓ +61 $\frac{12'' \text{ Elm}}{49}$

+59 E Ruggles St +

+41 E Ruggles St.

✓ +12 $\frac{14'' \text{ Elm}}{47}$ ✓ +14 $\frac{\text{End Carb}}{25}$

16

✓ +93 $\frac{6'' \text{ Maple}}{57}$

✓ +77 $\frac{34'' \text{ Elm}}{55}$

✓ +67 $\frac{5'' \text{ maple}}{48}$

✓ +33 $\frac{T.P.}{31}$

✓ +32 $\frac{\text{Twin 4'' Maple}}{50}$

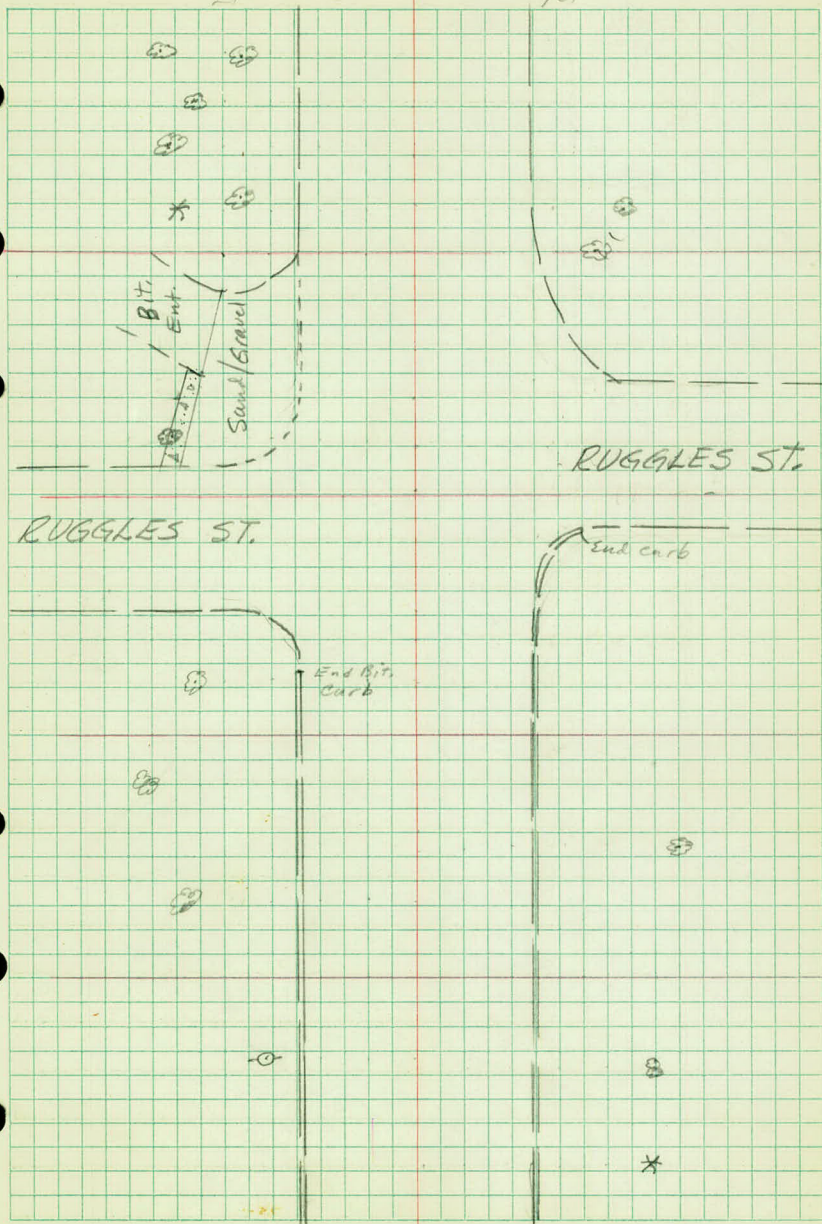
✓ +12 $\frac{8'' \text{ Pine}}{49}$

15

1972 h

24

RF



20

$$\checkmark +90 \quad \frac{12'' \text{ Elm}}{49}$$

$$\checkmark +77 \text{ } \frac{1}{2} (\pm) \text{ Summer St}$$

$$\checkmark +74 \text{ } \frac{1}{2} 12' \text{ Ent (crushed Rock)}$$

$$\checkmark +58 \quad \frac{\text{wall}}{49} \quad +61 \quad \frac{\text{wall}}{21}$$

$$\checkmark +49 \text{ } \frac{1}{2} 10' \text{ Bit. Ent.}$$

$$\checkmark +43 \quad \frac{12'' \text{ Ash}}{49}$$

$$\checkmark +36 \quad \frac{\text{wall}}{22} \quad \checkmark +43 \quad \frac{\text{wall}}{51}$$

$$\checkmark +25 \quad \frac{24'' \text{ BE}}{53}$$

$$\checkmark +16 \quad \frac{6'' \text{ Ash}}{57}$$

$$\checkmark +07 \quad \frac{36'' \text{ BE}}{52}$$

19

$$\checkmark +62 \quad \frac{8'' \text{ Pine}}{57}$$

$$\checkmark +63 \quad \frac{\text{stump}}{41}$$

$$\checkmark +46 \quad \frac{10'' \text{ Birch}}{56}$$

$$\checkmark +26 \quad \frac{6'' \text{ Pine}}{55}$$

$$\checkmark +22 \quad \frac{36'' \text{ Elm}}{41}$$

$$18 \quad \checkmark +04 \quad \frac{14'' \text{ Poplar}}{37} \quad \checkmark +09 \quad \frac{6'' \text{ Pine}}{52}$$

$$\checkmark +90 \text{ } \frac{1}{2} 11' \text{ Bit. Ent.}$$

$$\checkmark +77 \quad \frac{8'' \text{ Pine}}{46}$$

$$\checkmark +73 \quad \frac{\text{Hedge}}{42+} \quad \checkmark +74 \quad \frac{38'' \text{ Elm}}{39}$$

$$\checkmark +60 \quad \frac{8'' \text{ Maple}}{40} \quad \checkmark +74$$

$$\frac{18'' \text{ Poplar}}{37}$$

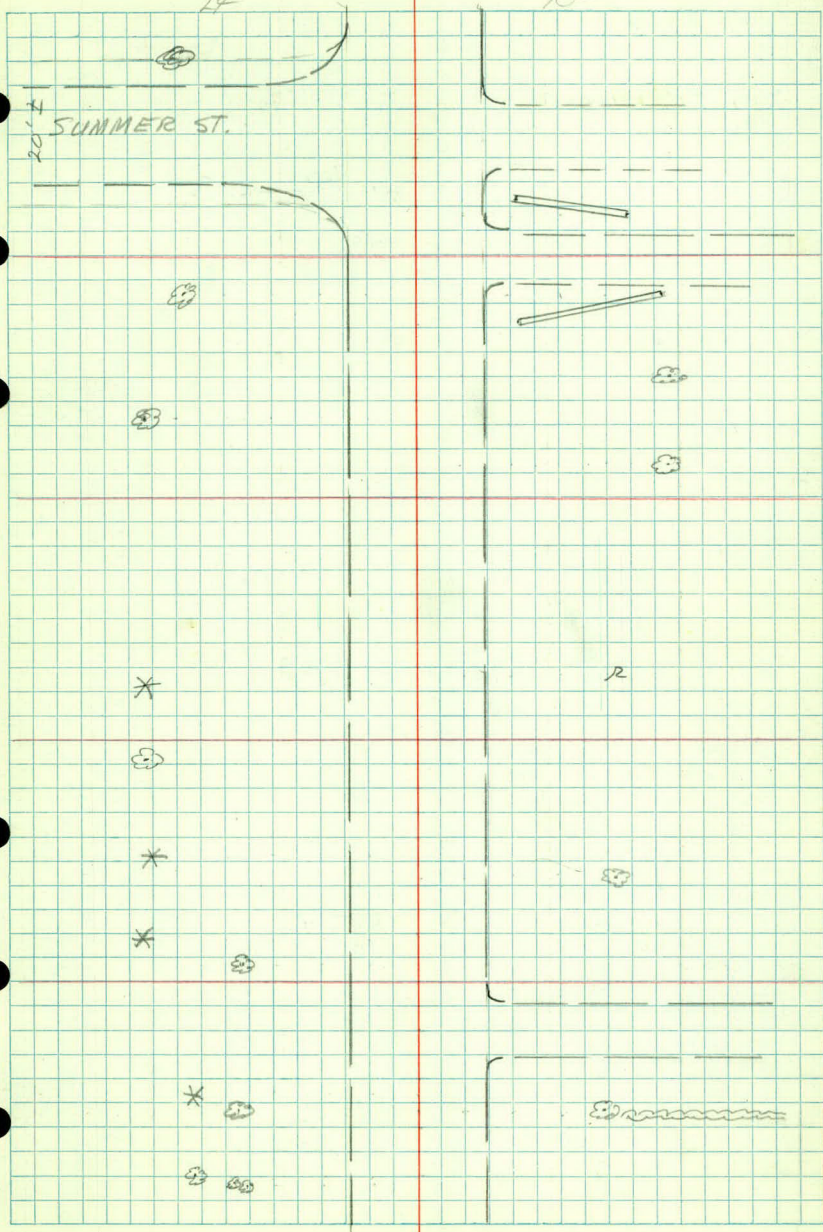
$$\checkmark +58 \quad \frac{\text{Two } 10'' \text{ Pop}}{34}$$

1972.
i

LH

Rt

20' x
SUMMER ST.



✓ +29 & 15' Bit. Ent

✓ +28 $\frac{27'' Elm}{52}$

✓ +22 & 10' Ent (Rock)

✓ +11 $\frac{Tw. 14'' Pine}{54}$

22

✓ +43 $\frac{12'' Elm}{52}$

21

✓ +00 $\frac{wall}{22-32}$ ✓ +06 $\frac{20'' Maple}{51}$

+95 & 10' Ent (gravel)

✓ +69 $\frac{4'' Birch}{52}$

✓ +44 $\frac{8'' Pine}{57}$

✓ +77 $\frac{18'' Ash}{49}$ ✓ +80 $\frac{wall}{22-32}$

✓ +68 $\frac{wall (Block)}{24+}$

+49 $\frac{14'' Elm}{54}$

✓ +21 & Ent (s/g) 10'

✓ +20 $\frac{40'' Maple}{39}$

20

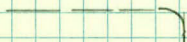
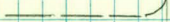
Lt

Rt



ED

x



25

✓ +96 $\frac{\text{Cor. Conc}}{52} + 70$

+58 & 35' Conc Ent.

✓ +47 $\frac{\text{Cor. Conc. Ent}}{1 \cancel{4} + 33}$ RT = +33 ✓ +42 $\frac{12" \text{ Maple}}{50}$ ✓ +43 $\frac{\text{Sign}}{34}$

✓ +49 cor curb +50 $\frac{\text{Barrier}}{52}$ ✓ +35 Beg Bit. Ent.

✓ +47 $\frac{\text{Barrier}^{33}}{40}$ ✓ +45 $\frac{\text{Conc Wall}}{35}$ ✓ +26 & 12' Sand Ent.

✓ +13 & 40' Bit. Ent.

24

✓ +02 ± & Autumn St ✓ +04 & 17' Bit. Ent.

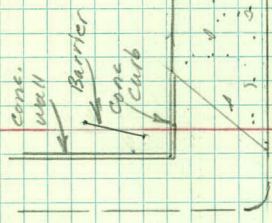
23

1972

K

RT

2 2 4



B.Y. Ent.

B



AUTUMN ST.

✓ Flag Pole
+42 37

✓ PP
+46 28

✓ +16 Cor. Conc.
50
✓ BR ✓ ER
27 +09 15 +09 27

✓ +13 14" E/m
39

✓ Cor Conc ✓ Sign
+92 50 +95 & 24' Conc Ent RT = +84 +83 39
BR ✓ ER ref. pt. 21'

✓ +77 15 +84 27
✓ +72 Sign +88 Light
53 53

✓ +50 14" E/m 20" E/m
39 150 78
✓ +43 ± Cor. Pkg Lot
45

+28 & Roselawn

26
✓ +96 Cor Conc curb 33+ (Revolving) Sign ✓ Light Pole
✓ +85 Cor. Conc. 33 ✓ +87 40
✓ +68 Cor. Conc 15
✓ +65 & 35' Conc. Ent.
✓ +53 Cor. Conc. 15

✓ +40 Cor. Conc
36-52

✓ +33 Cor Conc. 33
✓ +19 Light Pole 34

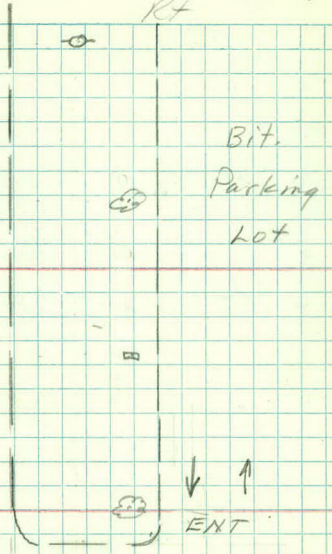
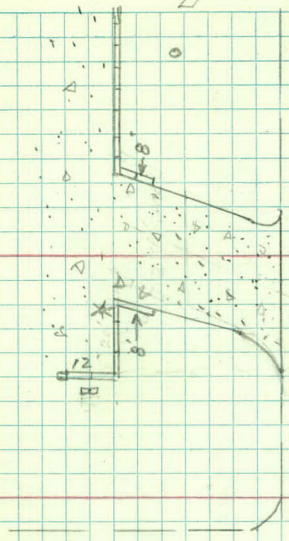
25

1972

1

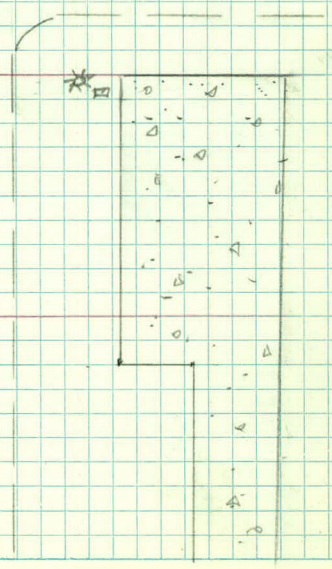
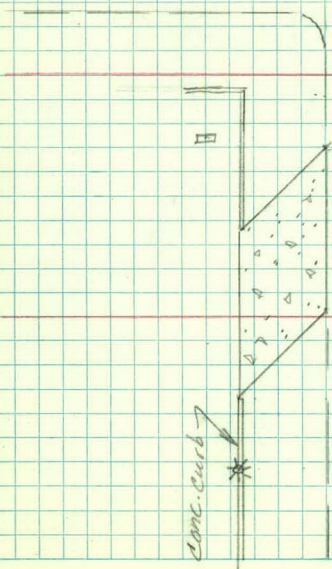
Lt

Rt



ROSELAWN

AVE



30

$$+89 \quad \frac{26'' \text{ Elm}}{47}$$

$$\checkmark +53 \quad \frac{2'' \text{ Pine}}{40} \quad \frac{12'' \text{ Birch}}{59} \quad 46$$

$$\checkmark +64 \text{ \& 9' Crushed Rock Ent}$$

$$\checkmark +52 \quad \frac{18'' \text{ Elm}}{40}$$

$$\checkmark +45 \quad \frac{2'' \text{ Pine}}{40} \quad \checkmark +41 \quad \frac{2'' \text{ Pine}}{40} \quad \checkmark +48 \quad \frac{1'' \text{ Pine}}{40} \quad \checkmark +44 \quad \frac{\text{Bit Curb}}{20+}$$

$$\checkmark +36 \text{ \& Bit Ent (15')}$$

$$\checkmark +13 \quad \frac{3'' \text{ Pine}}{40} \quad \checkmark +17 \quad \frac{4'' \text{ Pine}}{40}$$

$$\checkmark +13 \quad \frac{24'' \text{ Elm}}{40}$$

29

$$\checkmark +78 \quad \frac{4'' \text{ Pine}}{45}$$

$$\checkmark +72 \quad \frac{\text{Cor Pkg Lot}}{45} \quad \checkmark +74 \quad \frac{20'' \text{ Elm}}{38}$$

$$\checkmark +69 \quad \frac{2'' \text{ Pine}}{40}$$

$$\checkmark +41 \text{ \& Bit Ent (19')}$$

$$\text{Cor Bit Pkg Lot}$$

$$\checkmark +25 \quad 45$$

$$\checkmark +51 \quad \frac{\text{Pkg Lot}}{45}$$

$$\checkmark +41 \text{ \& Bit Ent (20')}$$

$$\checkmark +25 \quad \frac{\text{Beg Wood Fence}}{50+}$$

$$\checkmark +25 \quad \frac{\text{Cor Conc}}{50} \quad \checkmark +25 \quad \frac{\text{End Curb}}{50}$$

$$\checkmark +31 \quad \frac{\text{Bit Curb}}{20-39}$$

$$\checkmark +02 \quad \frac{\text{Light}}{53}$$

$$\checkmark +12 \quad \frac{\text{Bit curb corner \& Pkg Lot}}{39}$$

$$\checkmark +06 \quad \frac{\text{BR}}{27} \quad \checkmark +12 \quad \frac{\text{ER}}{15}$$

$$\checkmark +05 \quad \frac{\text{Cor Bit Pkg Lot}}{45}$$

$$\checkmark +99 \quad \frac{\text{Cor Conc Ent}}{50}$$

$$\checkmark +93 \quad \frac{18'' \text{ Elm}}{39}$$

$$\checkmark +83 \quad \frac{\text{POR}}{23}$$

$$\checkmark +80 \quad \frac{\text{BR Conc Ent}}{15}$$

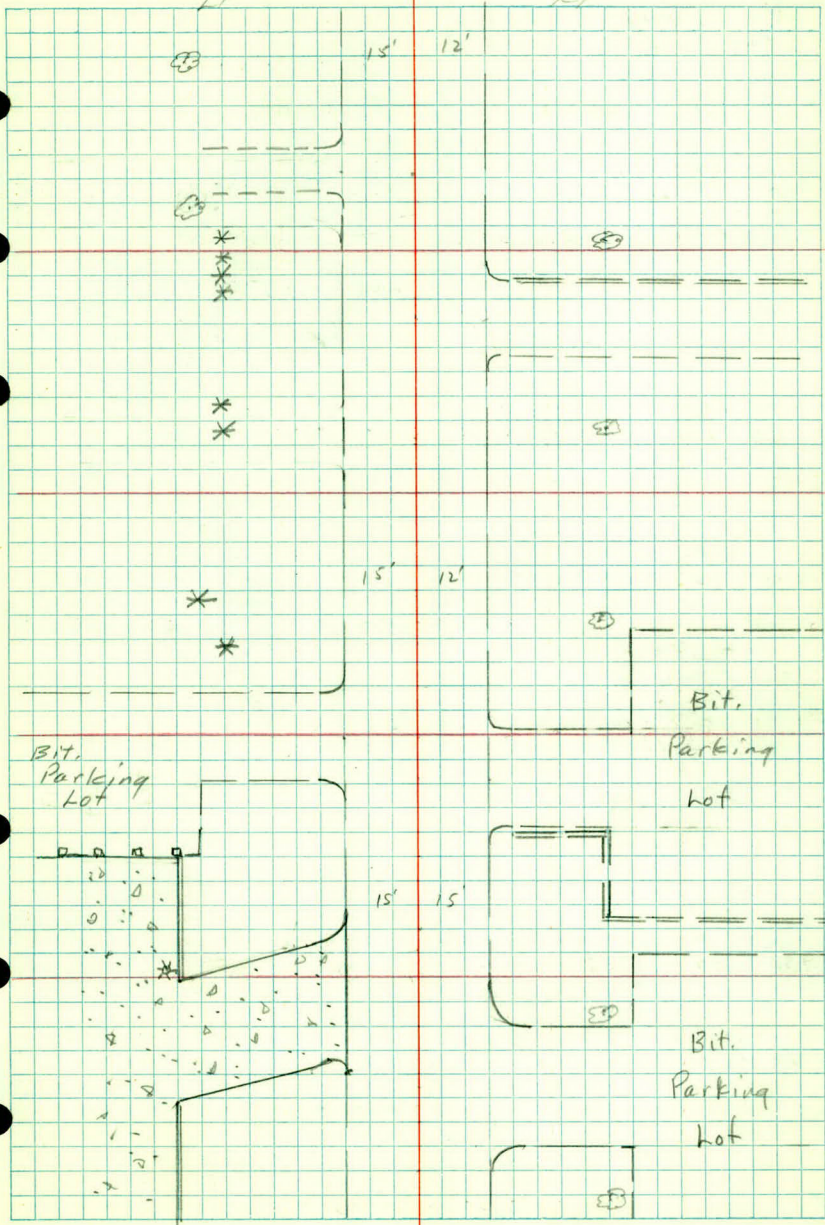
$$\checkmark +77 \text{ \& Bit Ent (25')}$$

$$\checkmark +74 \quad \frac{\text{Cor Conc Ent}}{50}$$

$$\checkmark +53 \quad \frac{24'' \text{ Elm}}{40}$$

Lt

Rt



✓ +47 $\frac{2'' \text{ Pine}}{44}$

✓ +40 $\frac{\text{stump}}{38}$

✓ +29 $\frac{\text{E } 10' \text{ Ent (Sand \& Gravel)}}{24'' \text{ Maple}}$

✓ +16 $\frac{46}{46}$

32

+09 $\frac{36'' \text{ Elm}}{39}$

✓ +95 $\frac{\text{E } 10' \text{ Ent. (Sand \& Gravel)}}{24'' \text{ Elm}}$
(Abandoned) +83 $\frac{39}{39}$

✓ +69 $\frac{\text{Bush}}{40}$

✓ +52 $\frac{7 \text{ Bushes}}{38-48}$ to +62

✓ +35 $\frac{4'' \text{ Pine}}{34}$

✓ +11 $\frac{\text{E Ryan Ave}}{24'' \text{ Elm}}$

✓ +16 $\frac{36'' \text{ Elm}}{40}$

31 ✓ +05 $\frac{\text{E } 8' \text{ Dolomite Ent}}{\text{End hedge}}$
✓ +99 $\frac{33}{24'' \text{ Elm}}$ +93 $\frac{47}{47}$

✓ +50 $\frac{24'' \text{ Elm}}{47}$

✓ +32 $\frac{24'' \text{ Elm}}{47}$ ✓ +36 $\frac{\text{Bog. hedge}}{33}$

✓ +38 $\frac{\text{E Conc Ent (16')}}{22'}$

30

Lt

Rt

*

R

③

③

Sand,
Gravel

seeded Area

③

④ Bush

④ 7 Bushes

④

*

④

RYAN AVE.

④

④

15' 12'

35

$$\begin{array}{r} \checkmark \quad 24'' \text{ Elm} \\ +93 \quad 36 \end{array} \quad \begin{array}{r} \text{End Fe} \\ +97 \quad 32 \end{array}$$

✓ +84 ♀ Ent (10')
Poor Condition

$$\checkmark \quad 28'' \text{ BE} \\ +74 \quad 40$$

$$\checkmark \quad 26'' \text{ Elm} \quad \checkmark \quad \text{Bay Fe} \\ +65 \quad 37 \quad +64 \quad 32$$

✓ +55 ♀ Bit Ent (9')

$$\checkmark \quad 26'' \text{ Elm} \quad \checkmark \quad \text{End Fe} \\ +44 \quad 37 \quad +48 \quad 32$$

$$\checkmark \quad 6'' \text{ Pine} \quad \checkmark \quad 8'' \text{ Pine}$$

$$\checkmark \quad 28 \quad 36 \quad +35 \quad 39 \quad \checkmark \quad \text{Corr Wood Fe}$$

$$\checkmark \quad 23 \quad 40 \quad \checkmark \quad \text{Hedge} \quad +24 \quad 32-41$$

$$\checkmark \quad 4'' \text{ Pine} \\ +22 \quad 38$$

✓ +09 ♀ Bit Ent. (19')

✓ +14 ♀ Bit Ent (14')

34

$$\checkmark \quad 2'' \text{ Pine} \\ +90 \quad 38$$

$$\checkmark \quad 36'' \text{ Elm} \quad \checkmark \quad 6'' \text{ Pine} \\ +94 \quad 38 \quad +98 \quad 51$$

$$\checkmark \quad 6'' \text{ Pine} \\ +82 \quad 54$$

$$\checkmark \quad \text{Bush} \quad \checkmark \quad \text{Bush} \\ +41 \quad 40 \quad +48 \quad 40$$

$$\checkmark \quad 20'' \text{ Elm} \\ +35 \quad 38$$

$$\checkmark \quad \text{Bush} \quad \checkmark \quad \text{Bush} \\ +23 \quad 40 \quad +30 \quad 40$$

$$\checkmark \quad \text{Bush} \quad \checkmark \quad 24'' \text{ Maple} \\ +00 \quad 40 \quad +07 \quad 38$$

33

$$\checkmark \quad \text{Bush} \quad \checkmark \quad \text{Bush} \\ +94 \quad 40 \quad +82 \quad 35$$

$$\checkmark \quad 24'' \text{ Elm} \quad \checkmark \quad \text{Fe} \\ +70 \quad 38 \quad +84 \quad 33+$$

+85 ♀ Ryan Ave

14

Rt

Mud, Sand & Gravel



3' wood Fence
2 board



- Bush
- Bush
- Bush
- Bush

- Bush
- Bush

Bush

RYAN AVE



✓ 32" Elm

+39 40

✓ +30 & 9' 5 1/2' Ent

✓ 40" Elm

+32 34

✓ Begin Hedge

+17 34

✓ 40" Elm

+10 34

✓ Stump

+86 33

37

✓ 36" Elm
+50 40

✓ 36" Elm

+42 36

✓ +12 & Shryer Ave

✓ +28 & Shryer

✓ End Fe & Cor

+12 32-36

✓ 36" Cott

+06 30

✓ 10" Pine

+97 43

36

✓ Tw. 12" Pop.

+84 54

✓ 20" Elm

+41 36

✓ 34" BE

+15 40

✓ 30" BE

35

✓ +00 40

✓ Begin Fe

+13 32

✓ +06 & Bit Ent (7')

14

RL

30'

SHRYER AVE.

SHRYER AVE.

20'

302

3' Wood Fence
2 beards

12 12

40

$$\begin{array}{r} \checkmark \\ +91 \quad \frac{18'' \text{ Elm}}{40} \end{array}$$

$$\begin{array}{r} \checkmark \\ +74 \quad \frac{\text{Bush}}{42} \\ \checkmark \\ +61 \quad \frac{26'' \text{ Elm}}{46} \end{array}$$

+41 & Skillman Ave.

$$\checkmark +74 \quad \frac{\text{Bush}}{30}$$

$$\checkmark +69 \quad \frac{14'' \text{ Elm}}{34}$$

$$\checkmark +39 \quad \frac{18'' \text{ Elm}}{30}$$

$$\checkmark +11 \quad \frac{\text{Fe Cor}}{34} + \checkmark +06 \quad \frac{\text{Tw. 8'' Apple}}{55}$$

$$\begin{array}{r} \checkmark \\ 39 \quad +00 \quad \frac{\text{Tri 10'' Apple}}{44} \\ \checkmark \\ +94 \quad \frac{12'' \text{ Apple}}{54} \end{array}$$

$$\checkmark +07 \quad \frac{\text{Stump}}{30}$$

+97 & 10's/6 Ent

$$\checkmark +87 \quad \frac{28'' \text{ Maple}}{30}$$

$$\checkmark +68 \quad \frac{48'' \text{ Elm}}{40}$$

$$\checkmark +65 \quad \frac{36'' \text{ Maple}}{34}$$

$$\checkmark +41 \quad \frac{36'' \text{ Elm}}{33}$$

$$\checkmark +16 \quad \frac{18'' \text{ Elm}}{41}$$

+27 & Bit Ent. (2')

38

$$\checkmark +97 \quad \frac{\text{Tri 10'' Elm}}{40}$$

$$\checkmark +97 \quad \frac{36'' \text{ Elm}}{53}$$

$$\checkmark +82 \quad \frac{\text{Bush}}{37} + \checkmark +87 \quad \frac{4'' \text{ Birch}}{52}$$

$$\checkmark +80 \quad \frac{\text{End Hedge}}{34}$$

$$\checkmark +80 \quad \frac{\text{Fe Cor}}{34}$$

$$\checkmark +75 \quad \frac{36'' \text{ Elm}}{34}$$

$$\checkmark +68 \quad \frac{36'' \text{ Elm}}{40}$$

$$\checkmark +66 \quad \frac{\text{Beg Hedge}}{34}$$

$$\checkmark +58 \text{ & Bit Ent (12')} + \checkmark +51 \quad \frac{\text{End Hedge}}{34}$$

1972

B

14

Et

Bush ES

→ Bush

90 SKILLMAN AVE

4' cyclone
Fence

Bush &

6.

$$\checkmark +41 \overset{\text{stump}}{\underline{34}}$$

$$\checkmark +36 \text{ Bit Ent (16')} \\ \checkmark \text{ Conc at 33'} \quad \checkmark 20'' \text{ Elm} \\ +21 \overset{2'' \text{ Pine}}{\underline{36}} \quad +21 \underline{40}$$

$$\checkmark +07 \text{ Bit Ent (16')}$$

42

$$\checkmark +86 \overset{\text{hedge}}{\underline{35}} \quad \checkmark +96 \overset{\text{hedge}}{\underline{42}}$$

$$\checkmark +66 \text{ Ent. (10' sand)}$$

$$\checkmark +31 \overset{24'' \text{ Elm}}{\underline{40}}$$

$$\checkmark +15 \overset{\text{stump}}{\underline{35}} \\ \checkmark +03 \overset{8'' \text{ Pine}}{\underline{35}}$$

$$41 \quad \checkmark +01 \overset{\text{stump}}{\underline{40}}$$

$$\checkmark +84 \text{ Conc Ent (14')} \quad \checkmark +95 \overset{\text{Bush}}{\underline{40}}$$

$$\checkmark +84 \overset{33''}{\text{Bit Ent (14')}} \\ 12-33$$

$$\checkmark +90 \text{ Bit Ent (12')}$$

$$\checkmark +79 \overset{36'' \text{ Elm}}{\underline{34}}$$

$$\checkmark +60 \overset{\text{Tw } 1'' \text{ Pines}}{\underline{44}} \quad \checkmark +70 \overset{12'' \text{ Elm}}{\underline{40}} \\ \checkmark +45 \overset{12'' \text{ Elm}}{\underline{40}}$$

$$\checkmark +34 \overset{2' \text{ conc drive}}{\underline{33}} \quad \checkmark +40 \overset{14'' \text{ Elm}}{\underline{34}}$$

$$\checkmark +29 \overset{2' \text{ conc drive}}{\underline{33}}$$

$$\checkmark +21 \overset{\text{Bush}}{\underline{34}}$$

$$\checkmark +00 \overset{30'' \text{ Elm}}{\underline{34}}$$

$$\checkmark +19 \overset{14'' \text{ Elm}}{\underline{40}}$$

40

1972 r

Lt

Rt

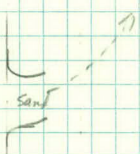


5X

Bit



2



8



8 2 Bush



8

**

8

8

2

*

Bit.

8



S Bush

45

$$\begin{array}{r} \checkmark \quad 30'' \text{ Elm} \\ +72 \quad 34 \\ \hline \checkmark \quad \text{hedge} \\ +63 \quad 50 \end{array}$$

+36 & Parker Ave

✓ +17 & Bit Ent (10')
conc at 33'

$$\checkmark \quad 36'' \text{ Elm} \\ +02 \quad 34$$

44

$$\checkmark \quad 26'' \text{ Elm} \\ +93 \quad 39$$

✓ +93 & 10' Limestone Ent.

✓ +76 & Bit Ent (11')
conc. at 33'

$$\checkmark \quad 26'' \text{ Elm} \\ +63 \quad 34$$

$$\checkmark \quad 20'' \text{ Elm} \\ +59 \quad 40$$

$$\checkmark \quad 4'' \text{ Pine} \\ +27 \quad 50$$

$$\checkmark \quad 24'' \text{ Maple} \\ +12 \quad 40$$

$$\checkmark \quad 6'' \text{ Pine} \\ +06 \quad 47$$

$$\checkmark \quad 24'' \text{ Elm} \\ +15 \quad 36$$

✓ +95 & 10' Rock Ent.
gray limestone

$$\checkmark \quad 18'' \text{ Elm} \\ +81 \quad 34$$

$$\checkmark \quad 26'' \text{ Elm} \\ +63 \quad 40$$

$$\checkmark \quad 8'' \text{ Pine} \\ +65 \quad 51$$

✓ +60 & Bit Ent (10')
Poor Condition

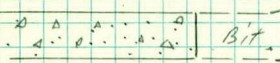
$$\checkmark \quad 6'' \text{ Pine} \\ +50 \quad 36$$

1972 S

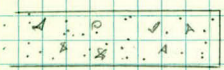
Lt

Rt

PARKER AVE



Bit



Bit

*

*

*

*

*

*

*

*

*

*

*

$$\checkmark \quad \begin{array}{r} 22'' \text{ Ash} \\ +44 \quad \underline{38} \end{array}$$

$$\checkmark \quad \begin{array}{r} 24'' \text{ Ash} \\ +18 \quad \underline{37} \end{array}$$

$$47 \quad \checkmark \quad \begin{array}{r} \text{Fe} \\ +02 \quad \underline{33} \end{array}$$

$$\checkmark \quad \begin{array}{r} \text{stump} \\ +77 \quad \underline{35} \end{array}$$

$$\checkmark \quad \begin{array}{r} \text{Fe Cor} \\ +31 \quad \underline{34+} \end{array}$$

$$\checkmark \quad \begin{array}{r} 18'' \text{ Elm} \\ +11 \quad \underline{34} \end{array}$$

$$\checkmark \quad \begin{array}{r} 18'' \text{ Elm} \\ +84 \quad \underline{34} \end{array}$$

$$\checkmark \quad \begin{array}{r} 20'' \text{ Elm} \\ +71 \quad \underline{34} \end{array}$$

$$\checkmark \quad \begin{array}{r} 20'' \text{ Elm} \\ +58 \quad \underline{34} \end{array}$$

$$\checkmark \quad \begin{array}{r} 36'' \text{ Elm} \\ +34 \quad \underline{34} \end{array}$$

46

+98 E Eldridge Ave.

$$\checkmark \quad \begin{array}{r} 30'' \text{ Elm} \\ +92 \quad \underline{34} \end{array}$$

$$\checkmark \quad \begin{array}{r} 10'' \text{ Elm} \\ +78 \quad \underline{51} \end{array}$$

$$\checkmark \quad \begin{array}{r} 6'' \text{ Pine} \\ +52 \quad \underline{40} \end{array}$$

$$\checkmark \quad \begin{array}{r} 34'' \text{ Elm} \\ +52 \quad \underline{34} \end{array}$$

$$\checkmark \quad \begin{array}{r} \text{stump} \\ +42 \quad \underline{43} \end{array}$$

$$\checkmark \quad \begin{array}{r} 30'' \text{ Elm} \\ +13 \quad \underline{34} \end{array}$$

45

1972 +

Lt

Rt

3

11

12

6 Cyclone Fe. →

ELDRIDGE AVE

*

28

6

4

8

28

3

8

12

6

50

✓ +96 Bit Ent (25')

✓ +83 End curb
67

✓ +68 cor Bit curb
67

+24 E Burke Ave.

49

+52 24" Elm
34

+31 28" Elm
34

48 +100 Fe - 33'

✓ +91 10" Plum
56

✓ +91 28" Maple
34

✓ +80 8" Pine ✓ +80 10" Pine
46 38

+51 36" Elm
34

1972 u

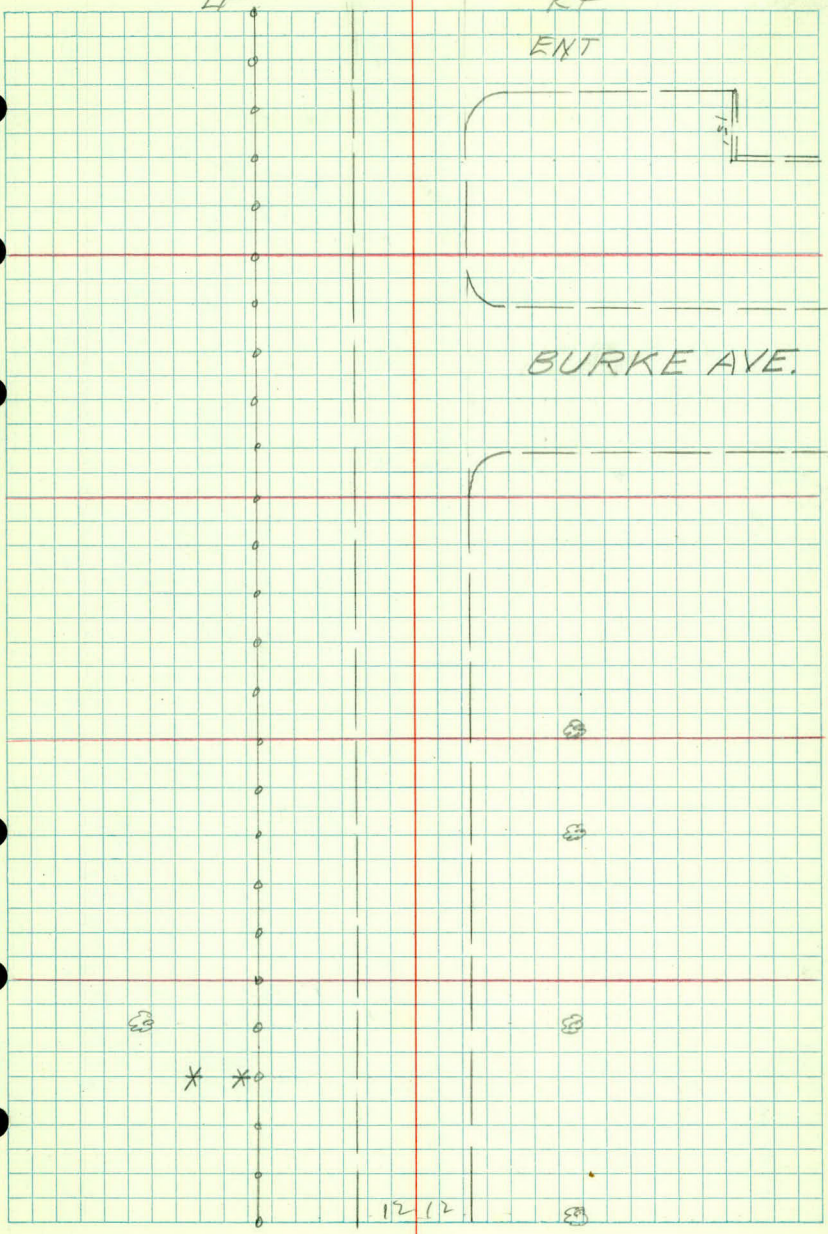
Lt

Rt

ENT

BURKE AVE.

12 12



✓ Fe Cor 18" Elm
+10 38+ +14 46

✓ Beg B618C46 Fe Cor
+06 24 +06 35

✓ End. S' S.W. Light
+16 28-33 +20 34

✓ Beg B618C46 Sign
+09 28 +12 41

52

✓ End Wall Beg 6' cyclone Fe
+96 33 +95 35 +88 2 Conc Ent (25')

✓ 18" Elm
+73 46

✓ Light
+64 35

✓ Bush
+69 41

✓ 36" Elm Bush
+44 46 +48 41

+43 2 Conc Ent (25')

✓ 26" Elm
+30 2 S' S.W. +22 46

✓ Beg. S' Conc. S.W. Light
+22 28-33' +25 34

✓ 26" Elm
+02 46

✓ conc. slab 2' cyclone Fe
+22 34+ +22 38+

51

✓ 20" Elm
+82 46

✓ +95 2 Bit Ent (25')

✓ End curb
+82 67

✓ 26" Elm
+70 34

✓ Quad 4" Birch
+65 34

✓ 34" Elm
+60 46

✓ 24" Elm
+44 34

✓ End Fe Beg. 2' store wall
+30 33 +30 34

✓ PP
+30 28

✓ 18" Ash
+26 34

50

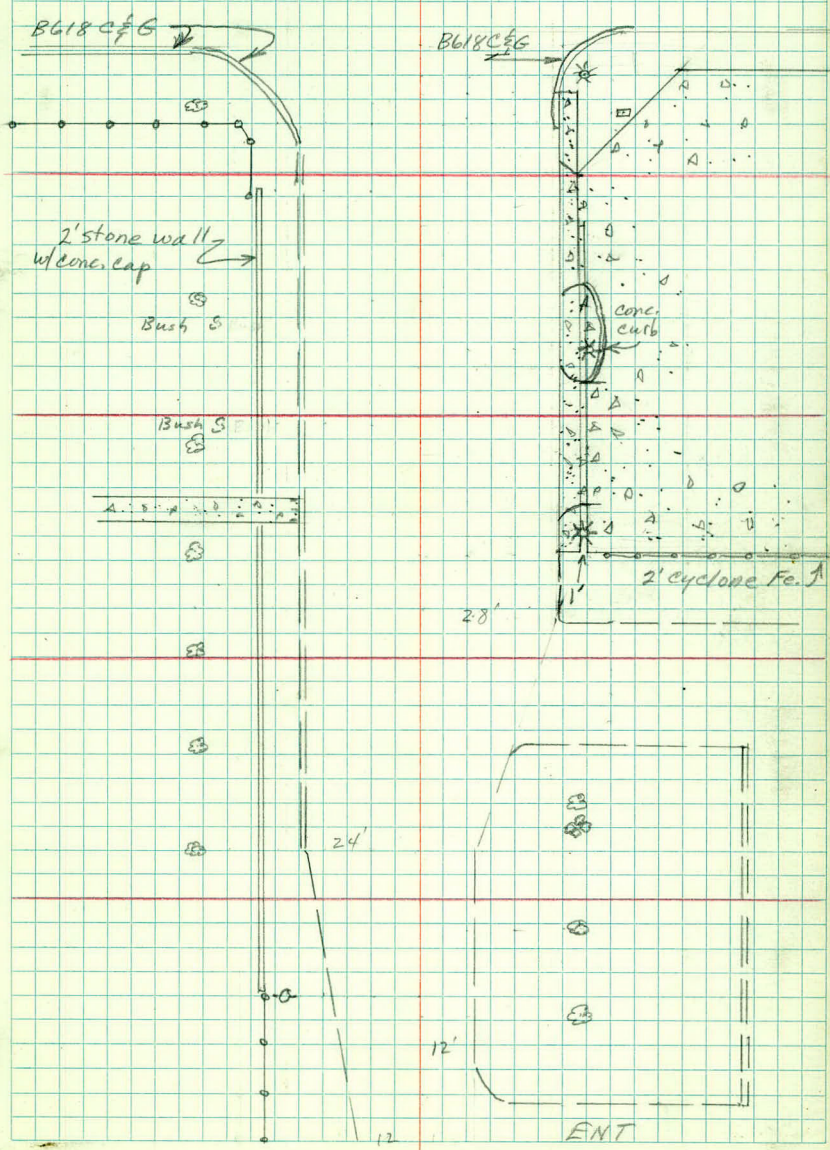
✓ Beg Bit curb
+08 67

1972
w

Lt

Rt

CO. RD "B"



55

✓ telephone
 +76 $\frac{\text{on pole}}{33}$

✓ +37 £ Bit Ent. (26')

54

✓ +00 £ Bit Ent. (23')

✓ +78 $\frac{\text{light}}{37}$

53

✓ +97 $\frac{\text{Corr. Bit Pkg Lot}}{33}$ ✓ $\frac{\text{Sign}}{42}$ +95
 ✓ +97 $\frac{\text{Bush}}{36}$

1972

w

LT

 RT

ENT.

9

ENT.

Bit.

Parking

EXT Lot

CS = sign
Bush

B618 C±G

CORD "B"

$$\begin{array}{r} \checkmark \quad 12'' \text{ Oak} \\ +43 \quad 42 \\ \hline \end{array} \quad \begin{array}{r} \checkmark \quad \text{Tw. } 36'' \text{ Oak} \\ +41 \quad 32 \\ \hline \end{array}$$

$$\checkmark +46 \quad \frac{4'' \text{ Oak}}{40}$$

$$\checkmark +34 \quad \frac{12'' \text{ Pine}}{40}$$

$$57. \quad \checkmark +04 \quad \frac{18'' \text{ Apple}}{52} \quad \checkmark +04 \quad \frac{18'' \text{ Apple}}{40}$$

$$\checkmark +91 \quad \frac{12'' \text{ Pine}}{38}$$

$$\checkmark +62 \quad \frac{12'' \text{ Pine}}{40}$$

$$\checkmark +84 \text{ \& Conc Sidewalk (5')} \\ 26+$$

$$\checkmark +60 \quad \frac{12'' \text{ Pine}}{36}$$

$$\checkmark +48 \quad \frac{12'' \text{ Pine}}{38}$$

$$\checkmark +54 \quad \frac{8'' \text{ Pine}}{36} \quad \checkmark +59 \quad \frac{8'' \text{ Pine}}{46}$$

56

$$\checkmark +80 \quad \frac{10'' \text{ Pine}}{61}$$

+74 \& Sandhurst

$$+52 \text{ \& Bit Ent (21')}$$

$$\checkmark +47 \quad \frac{24'' \text{ Elm}}{50}$$

$$\checkmark +37 \quad \frac{\text{cor Rkg Lot}}{34} \quad \checkmark +40 \quad \frac{1'' \text{ Willows}}{37; 41; 45; 50}$$

$$\checkmark +36 \quad \frac{\text{Light}}{33} \quad \checkmark +37 \quad \frac{\text{wall (Black)}}{34+}$$

$$\checkmark +19 \text{ \& Bit Ent (26')}$$

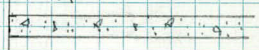
$$55 \quad \checkmark +04 \text{ \& Bit Ent (26')}$$

1972

x

Lt

Rt



SANDHURST AVE.



ENT.

60

✓
+89 $\frac{8'' \text{Oak}}{29}$
✓ +79 $\frac{8'' \text{Oak}}{33}$

✓ +38 $\frac{20'' \text{Elm}}{36}$

✓ +12 $\frac{\text{Beg. Hedge (Lilacs)}}{40}$
✓ +12 $\frac{12'' \text{Oak}}{33}$ ✓ Beg Fe
✓ +12 33 +12 34+

+14 & LAURIE AVE

59

✓ +02 & Bit Ent (9')

✓ +87 $\frac{1'' \text{cedar}}{37}$ ✓ +88 $\frac{8'' \text{Apple}}{55}$

✓ +62 $\frac{8'' \text{Elm}}{45}$

✓ +20 $\frac{\text{Tw } 48'' \text{Cott.}}{32}$

✓ +33 $\frac{\text{Bit Curb}}{33+}$ ✓ +37 $\frac{1'' \text{cedar}}{37}$

✓ +20 & Bit Ent (25')

58

✓ +71 $\frac{30'' \text{Oak}}{32}$

1972

4

Lt

Rt

LAURIE AVE.

3' wood Fe.
3 boards

*

* Bit curb 2

✓ +44 ♀ Sherren Ave

✓ 30" BE
+37 42

✓
+11 30" Cott.
48

✓ +09 ER
20
✓ 28" Oak
+02 38

✓ +85 BR
47

✓ +70 ♀ Sherren Ave

✓ +56 ER
68

+38 18" Elm
53

✓ +37 12" Elm
36

✓ End lilachedge
+37 45

✓ +16 BR
22

✓ 24" Elm
+18 37

✓ +91 ♀ 8' Ent (sand)
conc. at 50'

✓ 38" Oak
+72 32

✓ +54 8" Elm
41

✓ +32 8" Oak
33

✓ +49 10" Elm
40

✓ +05 6" Oak
42

✓ +03 4" Elm
40

✓ +09 24" Elm
29

60

62

61

1972

2

LT

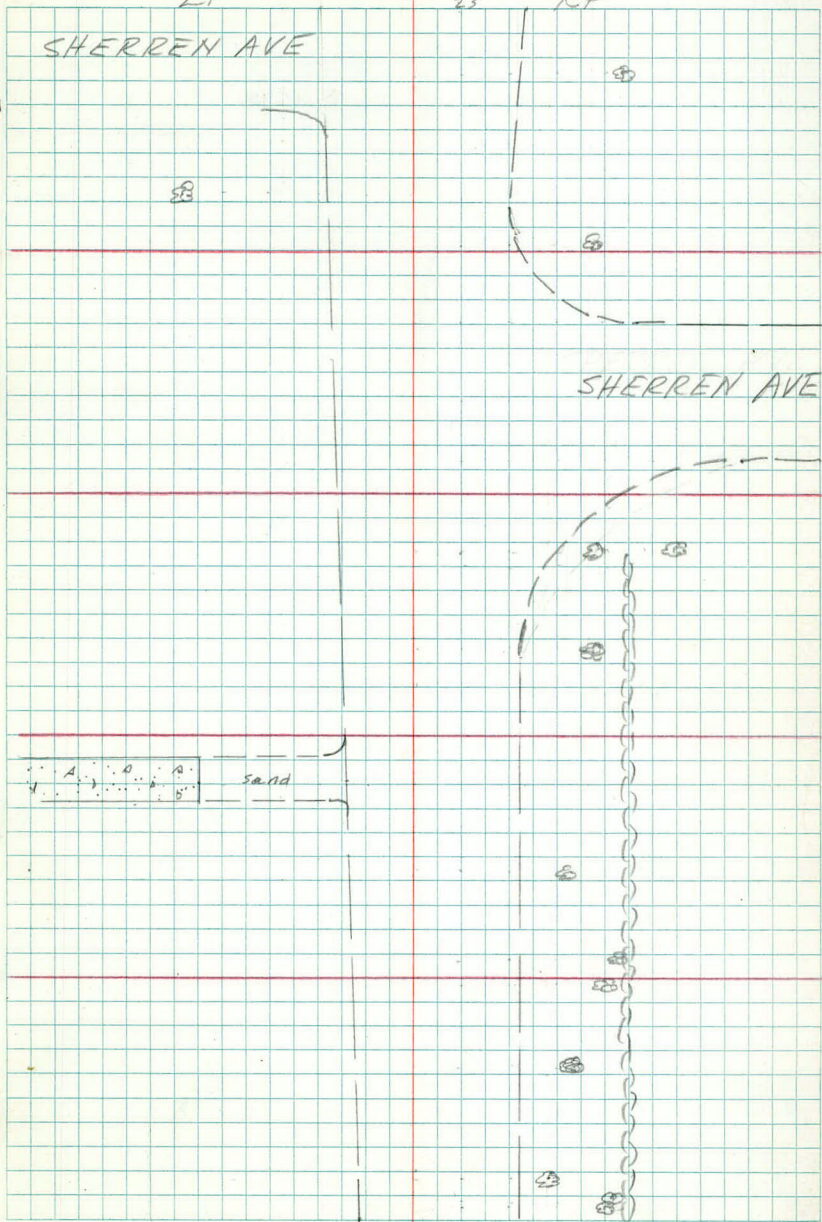
23

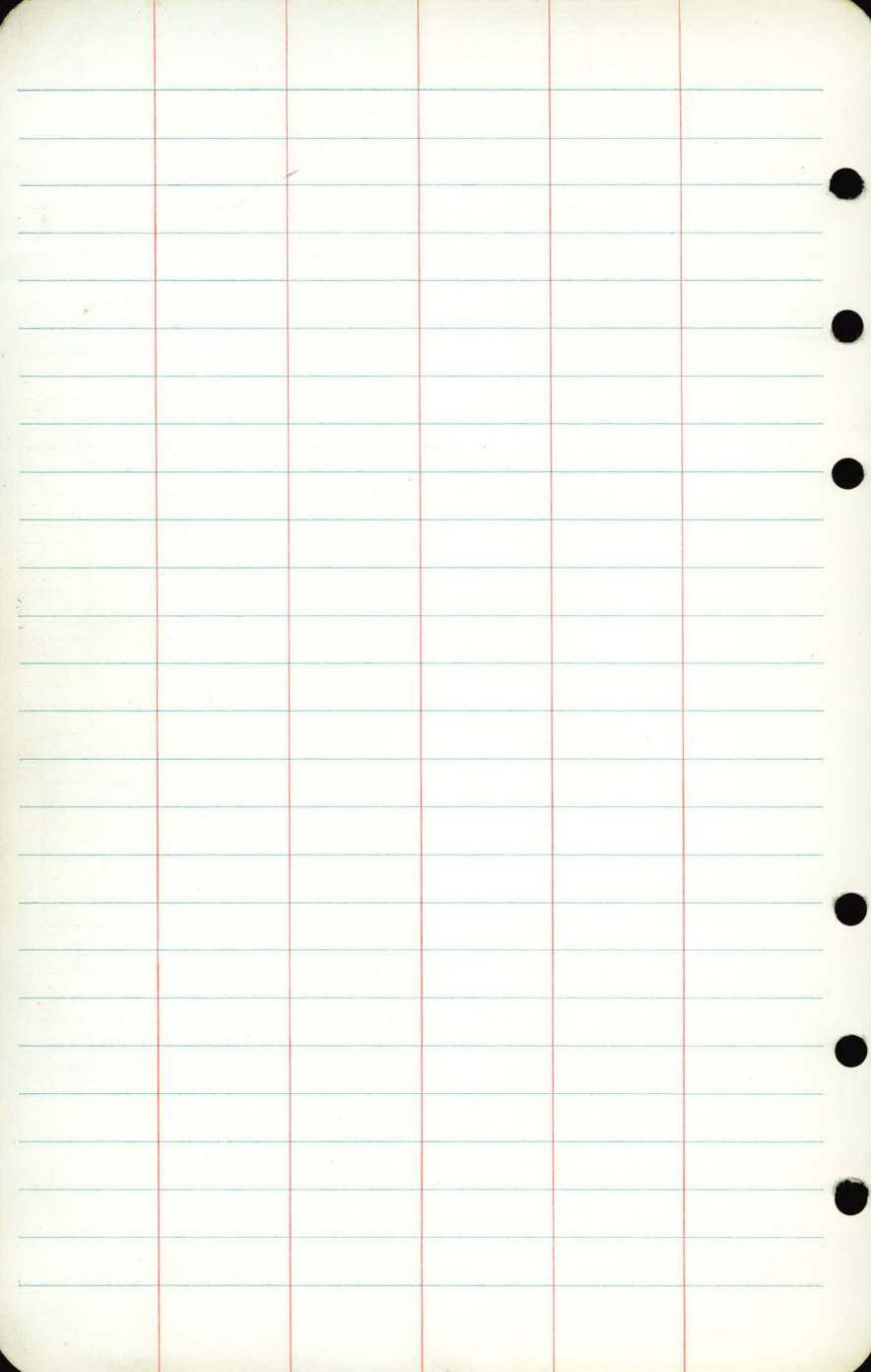
RT

SHERREN AVE

SHERREN AVE

A . . . D . . . A . . . sand





ML
DS

MARCH 6, 78
SUNNY 25°

ADDITIONAL
TOPOGRAPHY LEXINGTON AVE
CARPENTIER TO HWY 36

ADDITIONAL
TOPOG.

Lt

\$

Rt

+50

✓

+29 COR. PARKING LOT
53

+17 ER
53

+10 CURB
38-45

+10 END SIDE
33-38

5+00

+97 & DRIVE.

+89 END SIDE
71-76

+84 CURB
38-

+71 NO E BLDG
76

+64 LIGHT
48

+50 FOS
30

+50 SIDE
38

+50 SIDE
33-38

+50

+44 F.P.
42

+45 SIDE
38

+40 SIDE

44-99

+34 & 12' SIDE
38-76

+13 LIGHT
48

+100 SAE. BLDG
76

+100 SIDE
71-76

A+00

+88 & DRIVE.

+99 CURB
38-7

+77 CURB
38-51

+70 CR
60

+65 ER
60

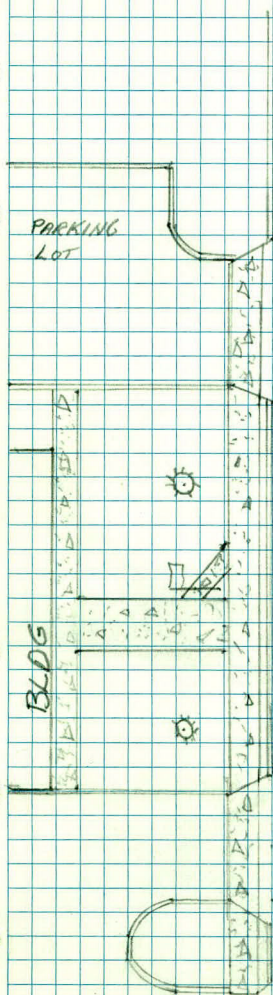
+50 SIDE +58 CURB +58 BLDG SIDE.
30 38-50 33-38

3+50

LT

£

RT



LT

\$

RT

26+00

+83 ARV
40

+79 CURB
61

(77) COR. PARKING LOT
59

+65 NAIL
44

+78 BUSH
37

+63 SIGN + 61 ER
64 59

+55 CURB
48-53

+50

42E DRIVE

+29 CURB
48

+29 BR
48

+23 ER
54

+16 2" MAPLE
39

+12 ASP
37

+12 END SIDE
71

+10 1 CEDAR
48

+09 SIDE
71

+04 NE COR BLDG
71

25+00

+99 CURB
53

+00 STEP
66-71

+99 WOOD FENCE
53-64

+88 2" MAPLE
39

+79 WOOD FENCE
53-64

+79 CURB
64-71

+53 2" MAPLE
41

+68 SEC COR BLDG
71

+64 WOOD FENCE
87

+50

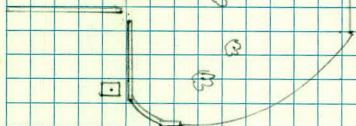
+98 WOOD FENCE
54-87

24+00

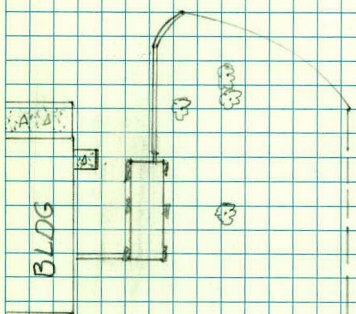
LT

&

RT



B.T.
PARKING
Lot



BLDG

2

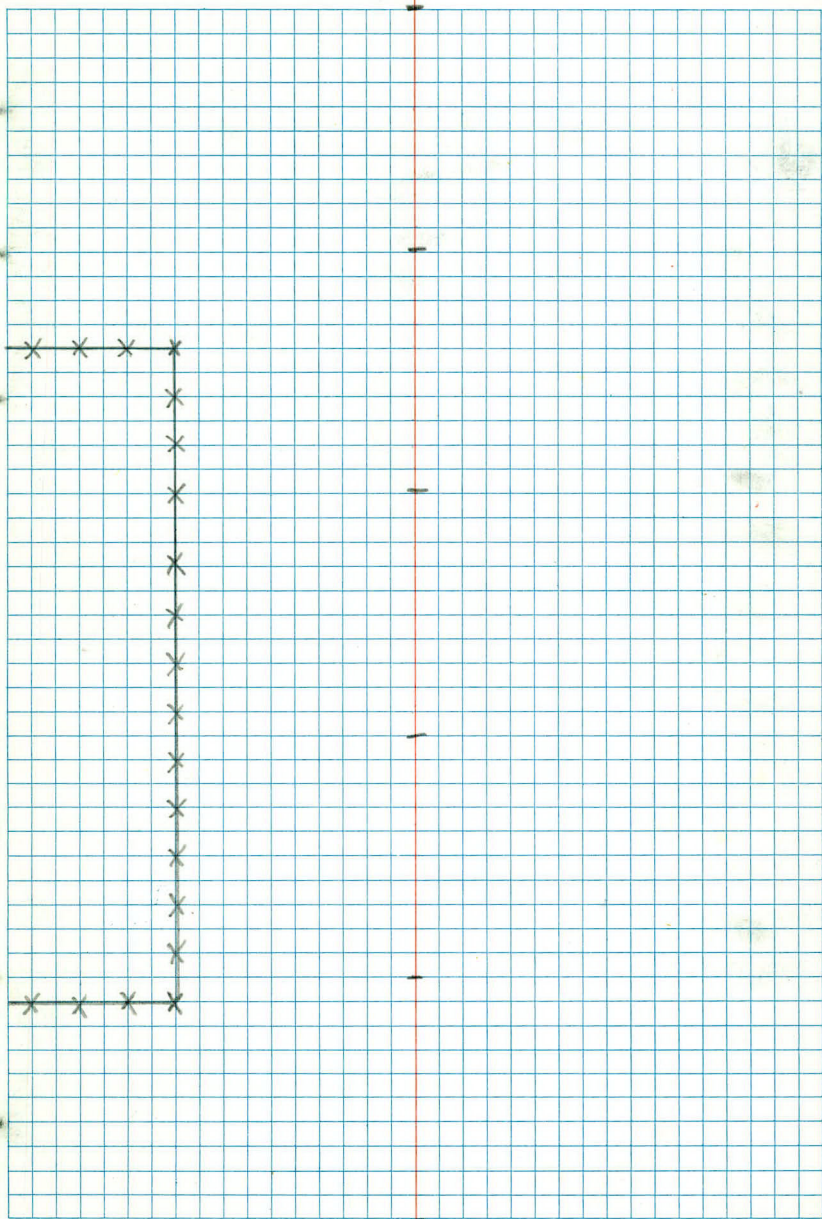
+79 ENO 4' CYCLONE FEN.
50

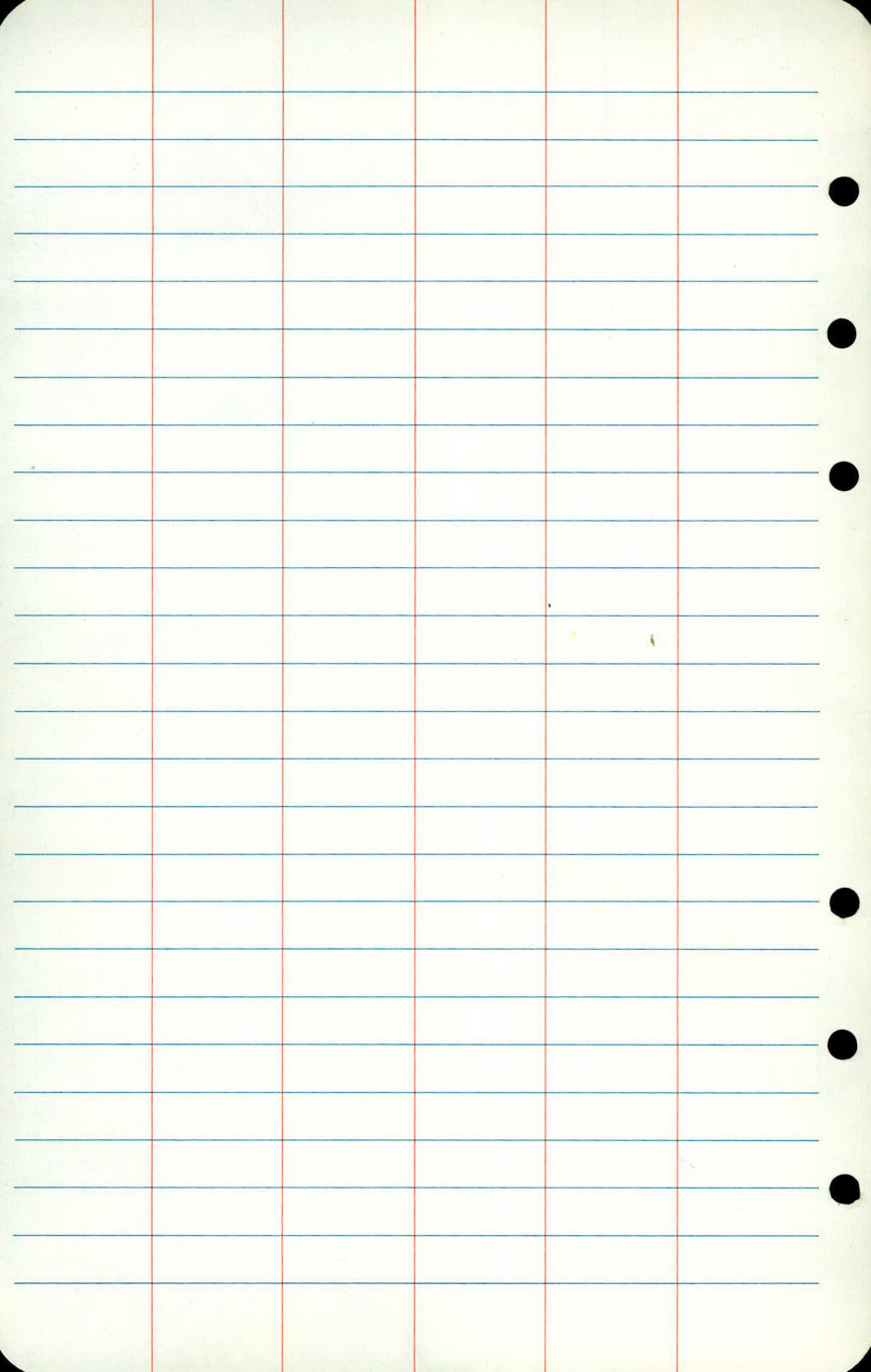
+50

60+00

+45 4' CYCLONE FEN.
50

59+00





62-651-01

BLDG

LOCATION

±

MEASUREMENTS

HARP. TO Hwy 36

10 PAGES

PK
LPD
RR
GM

Sept 16, 17, 20, 21, 1971

$$\begin{array}{r} \checkmark \quad 12+10 \quad \underline{\text{NE COR Bldg}} \\ \quad \quad \quad 101 \end{array}$$

$$\checkmark \quad 6+31 \quad \underline{\text{N END ISLAND}} \quad 2$$

$$\checkmark \quad 6+30 \quad \underline{\text{N END ISLAND}} \quad 3$$

$$\checkmark \quad 6+20 \quad \underline{\text{S END ISLAND}} \quad 3$$

$$\checkmark \quad 6+17 \quad \underline{\text{S END ISLAND}} \quad 2$$

$$\checkmark \quad 6+00 \quad \underline{\text{NW COR STATION}} \quad 119$$

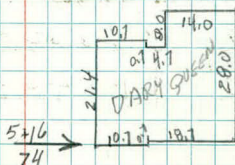
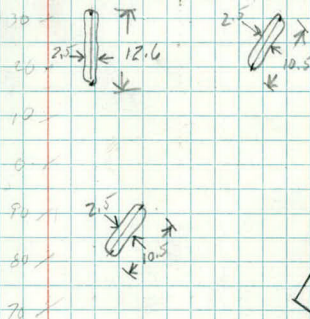
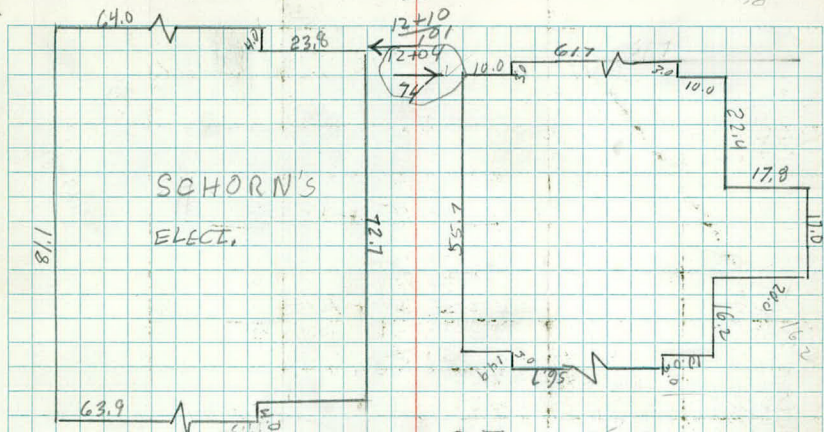
$$\checkmark \quad +91 \quad \underline{\text{N END ISLAND}} \quad 1$$

$$\checkmark \quad +83 \quad \underline{\text{S END ISLAND}} \quad 1$$

$$\checkmark \quad +72 \quad \underline{\text{SW COR Bldg}} \quad 702$$

$$\checkmark \quad 5+16 \quad \underline{\text{SW COR Bldg}} \quad 74$$

17.8



NORTH STAR BANK LOCATION

15 + 93 BANK
128

+ 76 BANK
97

+ 57 BANK
88

✓ + 38 BANK
84

+ 25 BANK
86

+ 00 BANK
96

14 + 93 BANK
101

STADIA LOCATION TRANSECT ② 14+00 ⑤ 33' EAST

0° 00' = STA 15+00 ⑤ 33' EAST All $\frac{1}{2}$ s to Right

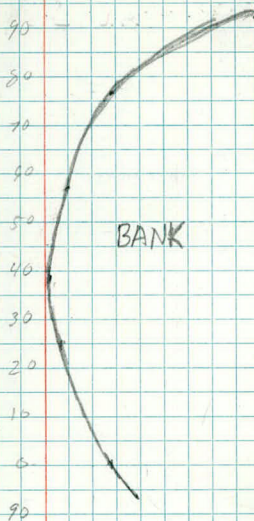
$\frac{1}{2}$	DISTANCE	OBJECT	$\frac{1}{2}$	DIST.	OBJ.
0° 00'	100'	15+00 ⑤ 33' EAST	51° 45'	152'	BANK
34° 57'	115'	BANK	52° 04'	171'	"
37° 06'	134'	"	28° 13'	123'	"
35° 07'	139'	"	21° 25'	140'	"
47° 46'	157'	"	19° 18'	160'	"

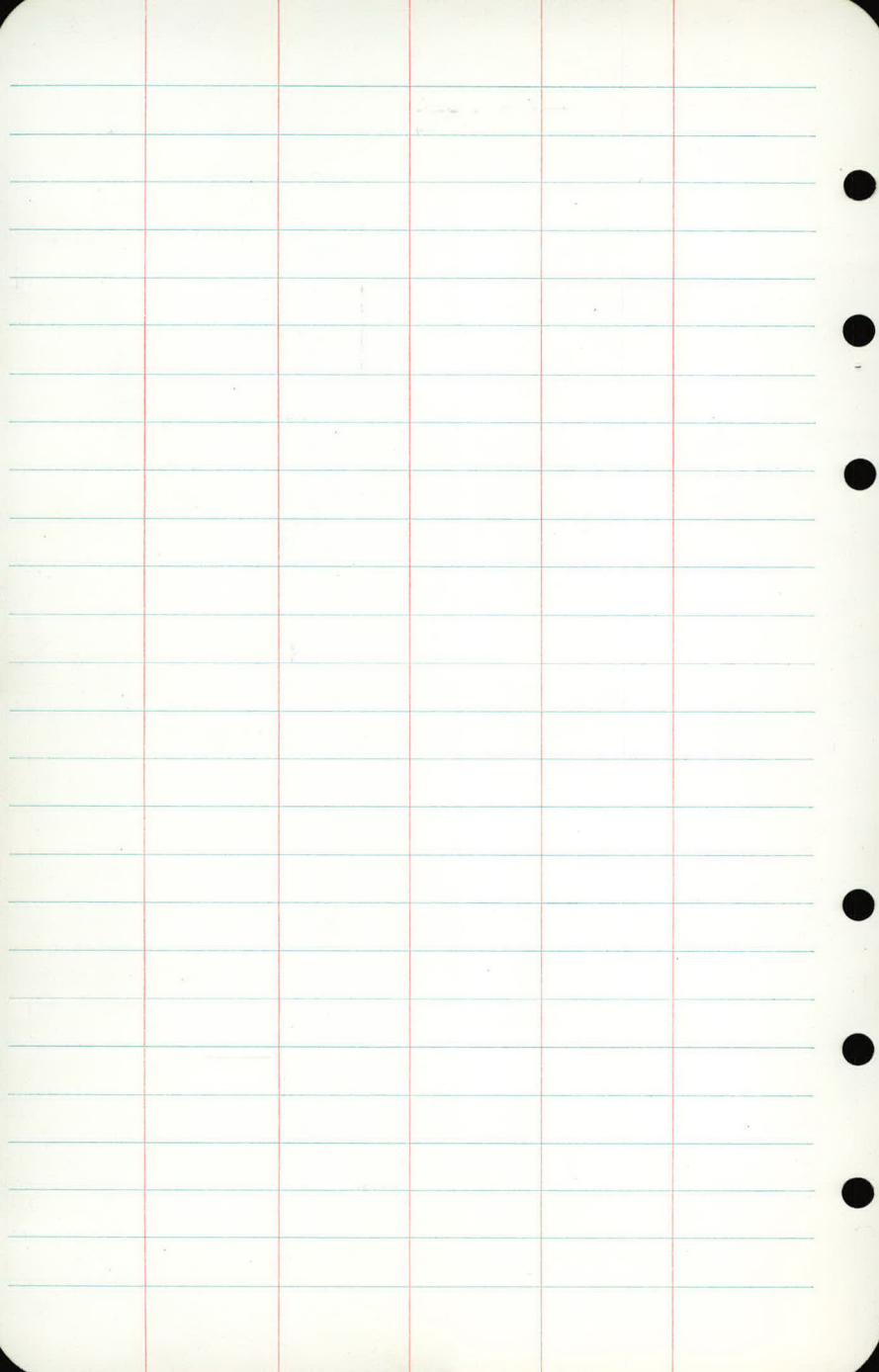
Lt

£

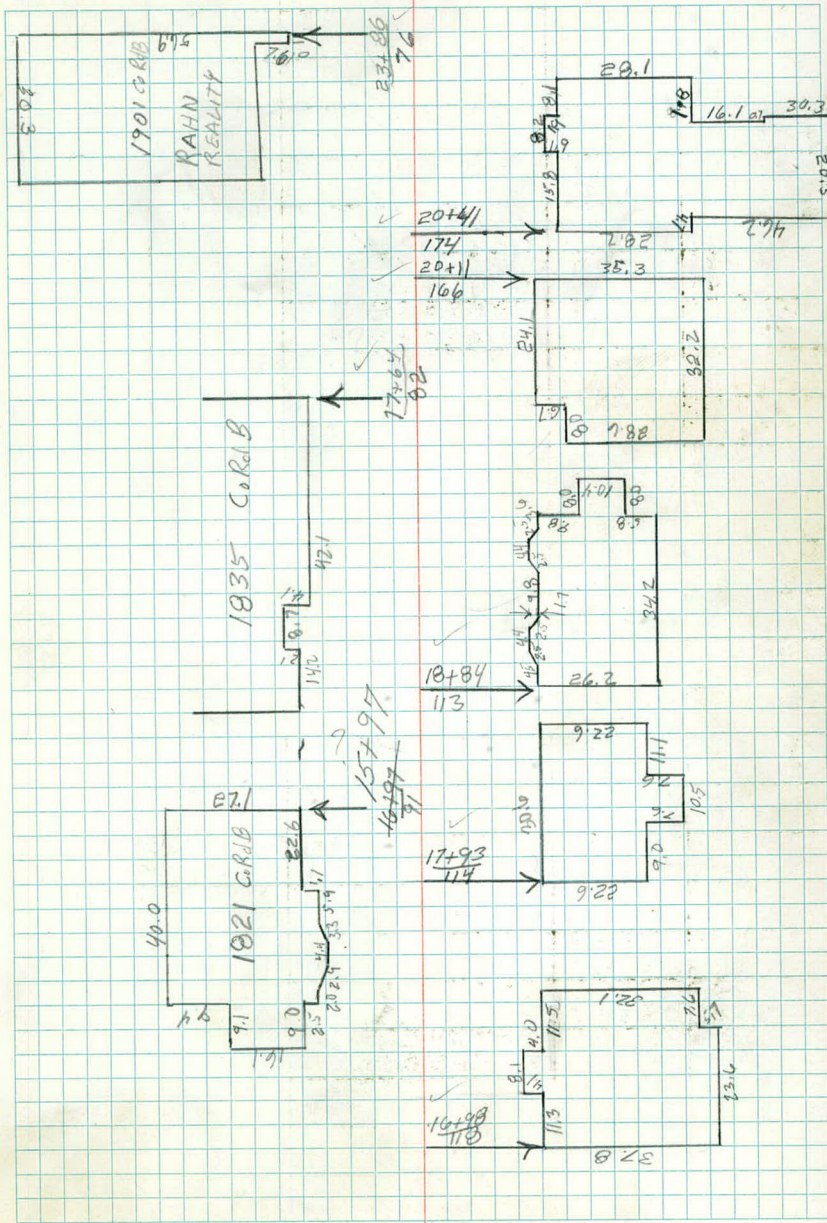
Rt

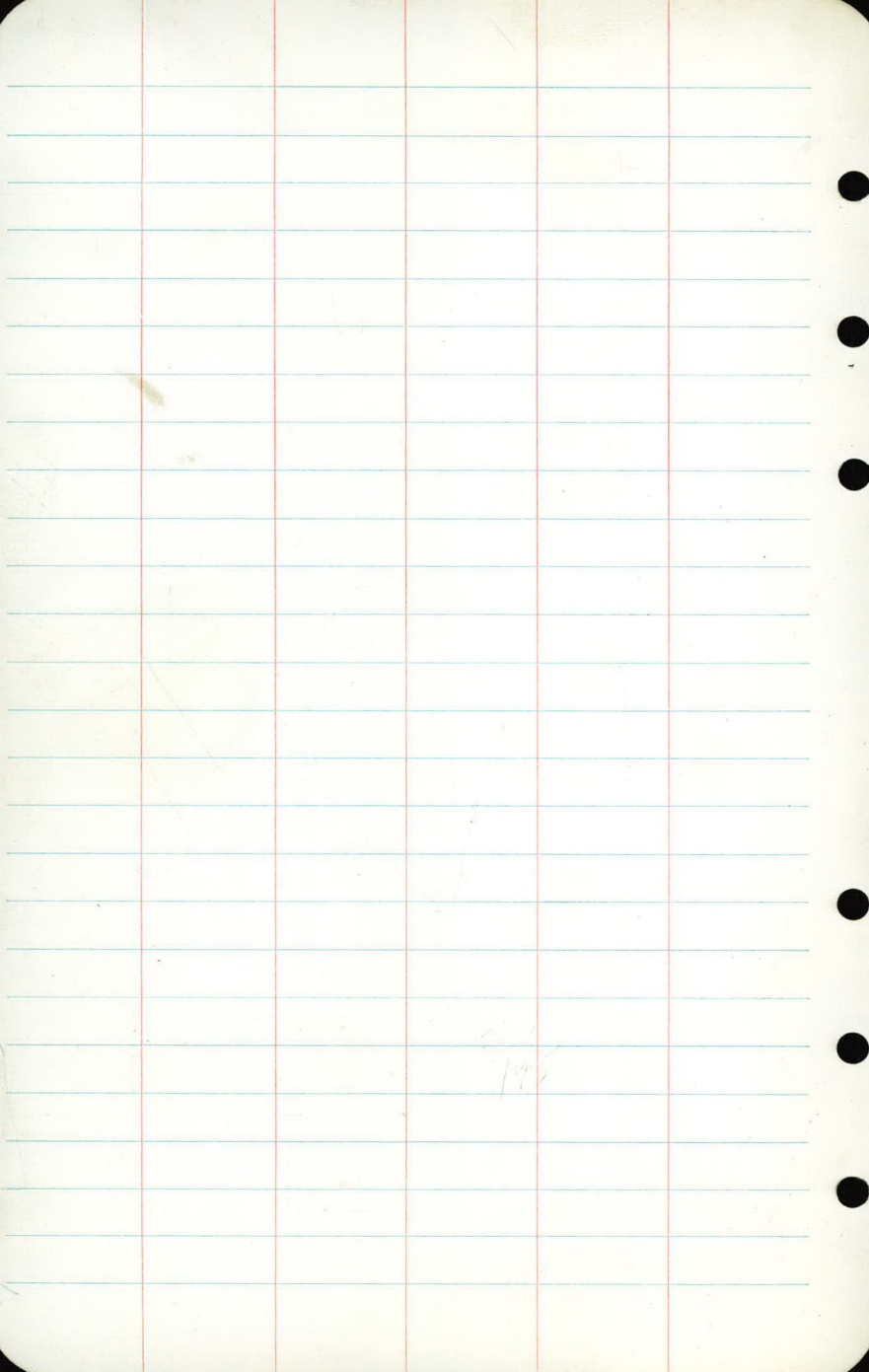
3





4





Lt

28+03

46.0

Rt 5

109

0.1

0.9

72.9

1943 CORRB

67.8

74.8

25.1

24.6

72.9

28+17
27+03
114

27+03

66.0

25+90

16.3

9.0

10.0

7.0

10.0

27+88

9.3

12.0

6.0

9.8

5.3

56.0

34.2

27.2

9.0

14.7

27.3

14.2

24.1

6.8

24+70

75

11.7

13.4

12.0

22+00

195

13.3

8.0

15.3

10.5

4.4

8.5

10.5

7.5

7.8

30.1

9.1

25+28

94

26

7.6

11.5

11.5

11.5

11.5

11.5

11.5

11.5

11.5

11.5

11.5

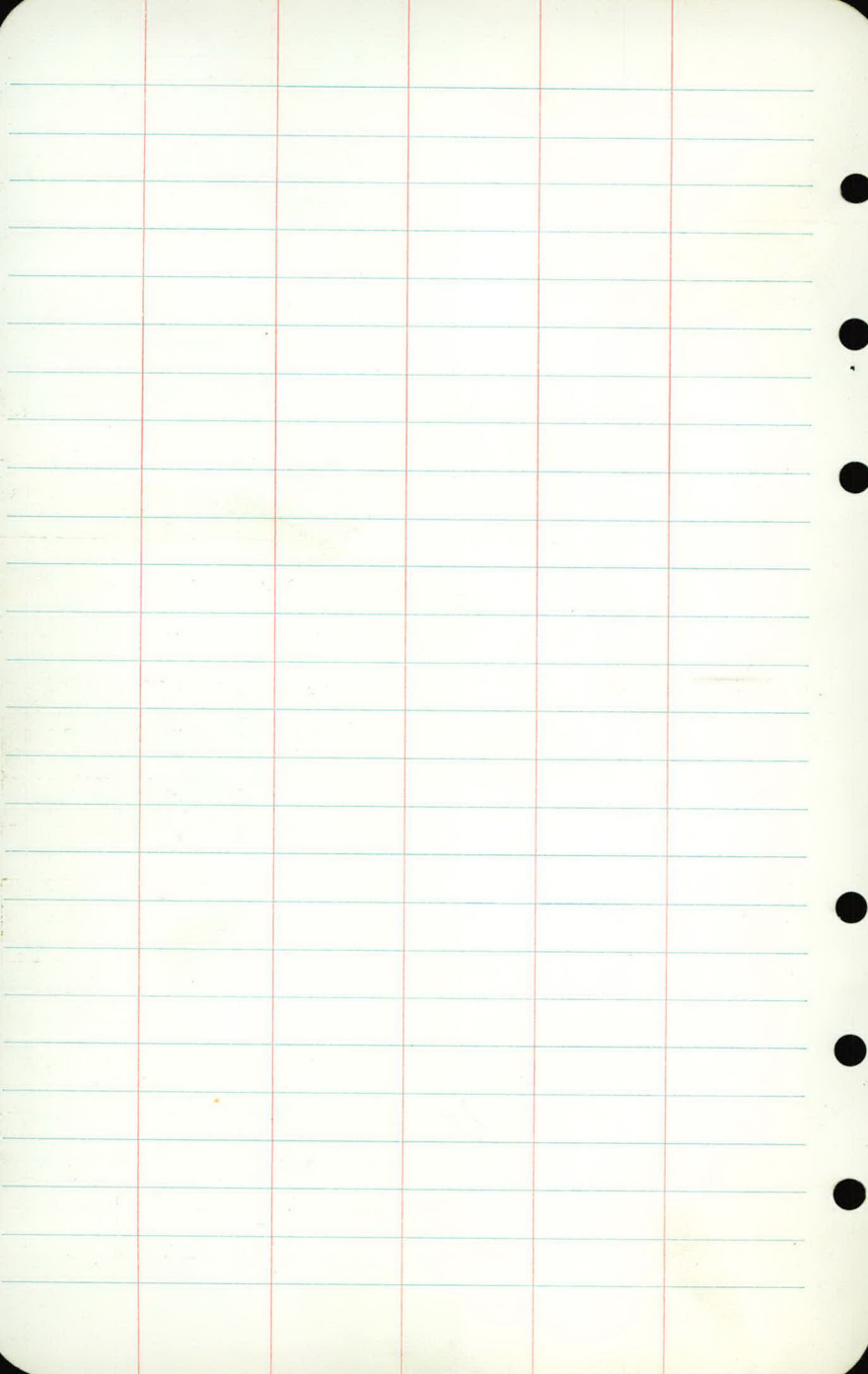
11.5

42.4

1909 CORRB
N GAS

42.4

68.2

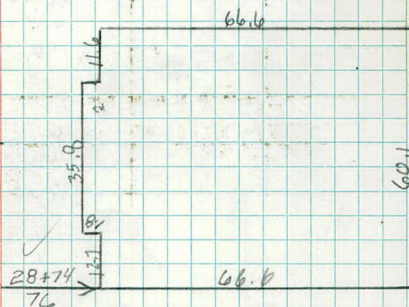
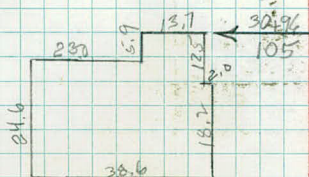
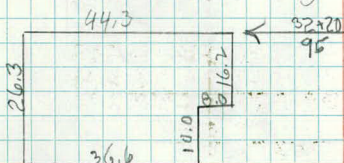
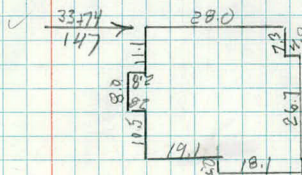
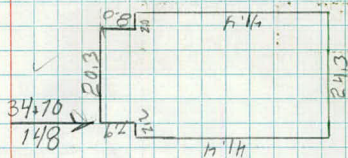
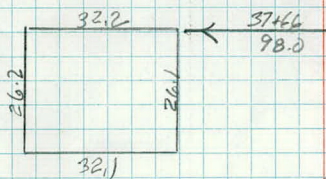


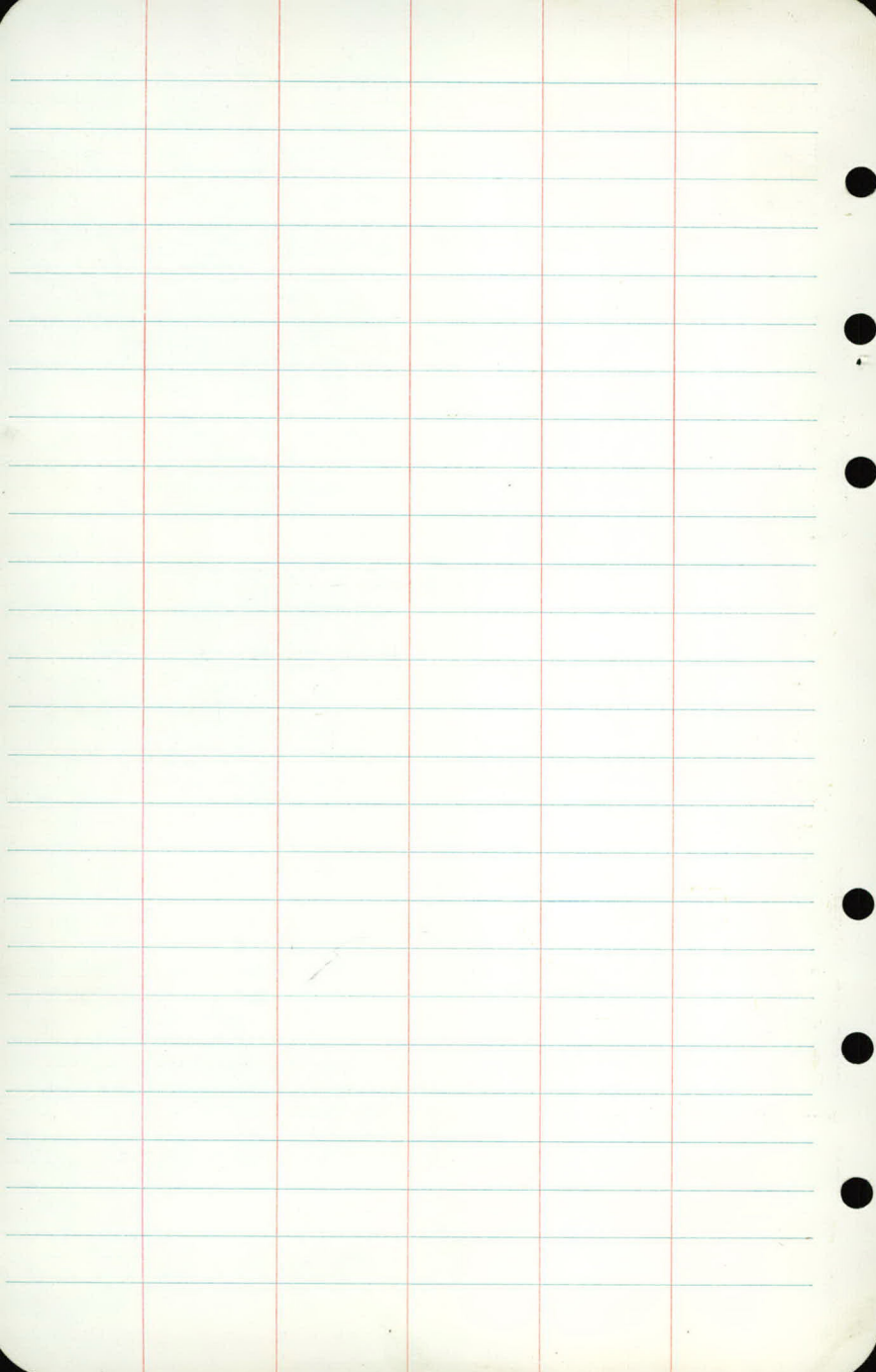
Lt

C

Rt

C



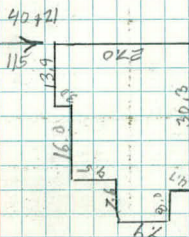
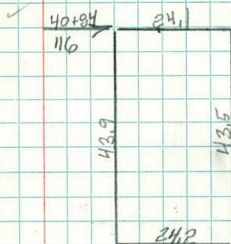
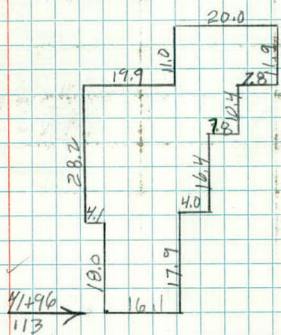


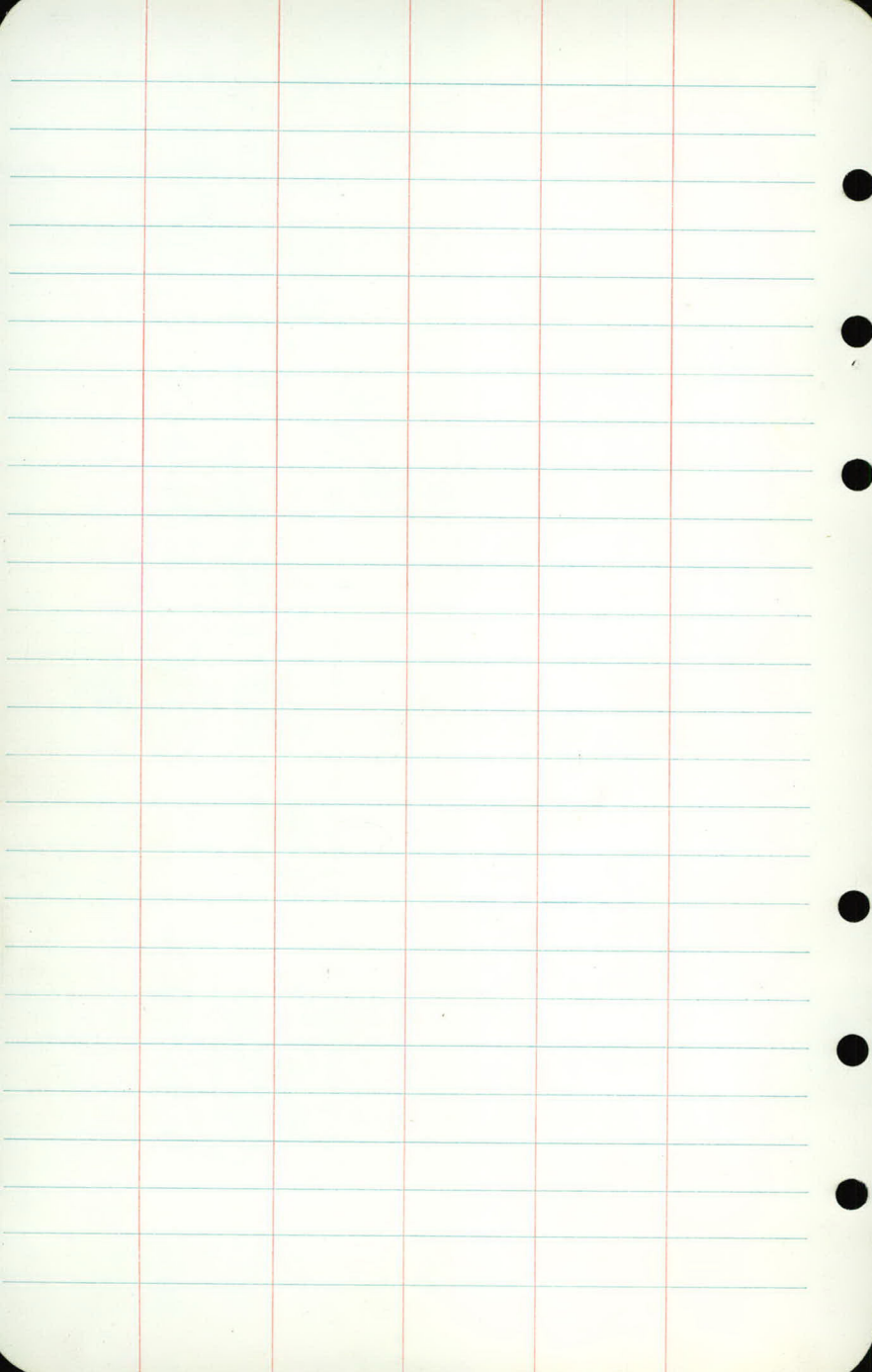
Lt

E

Rt

7



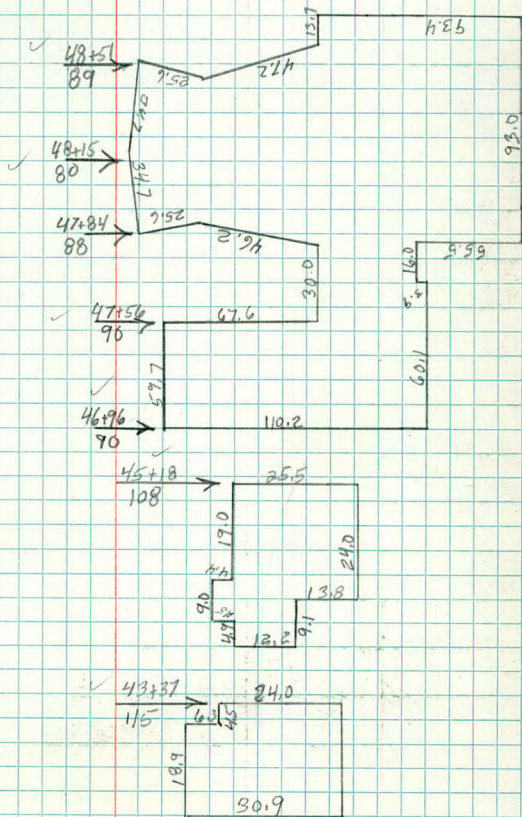


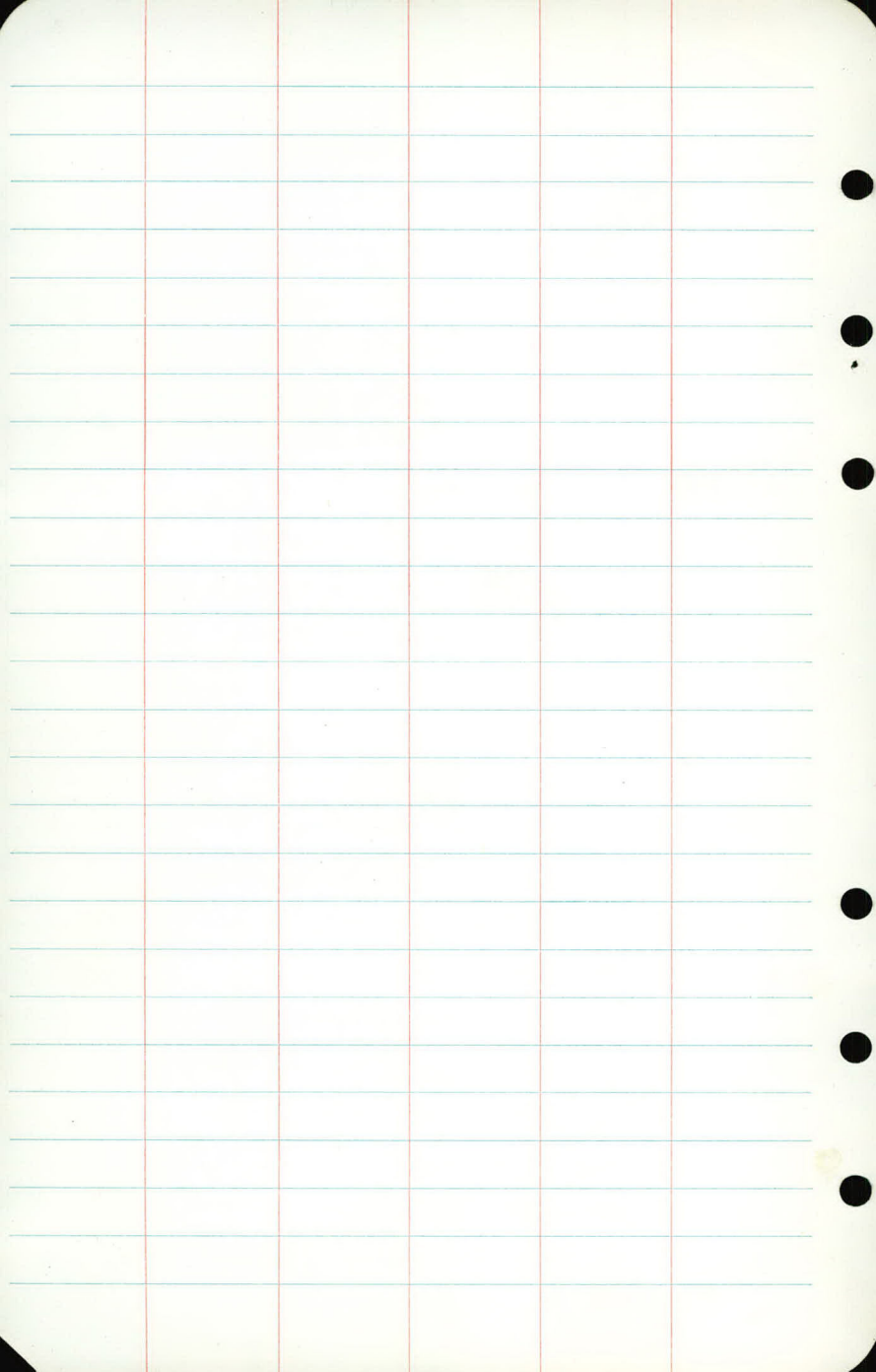
77

8

Rt

8



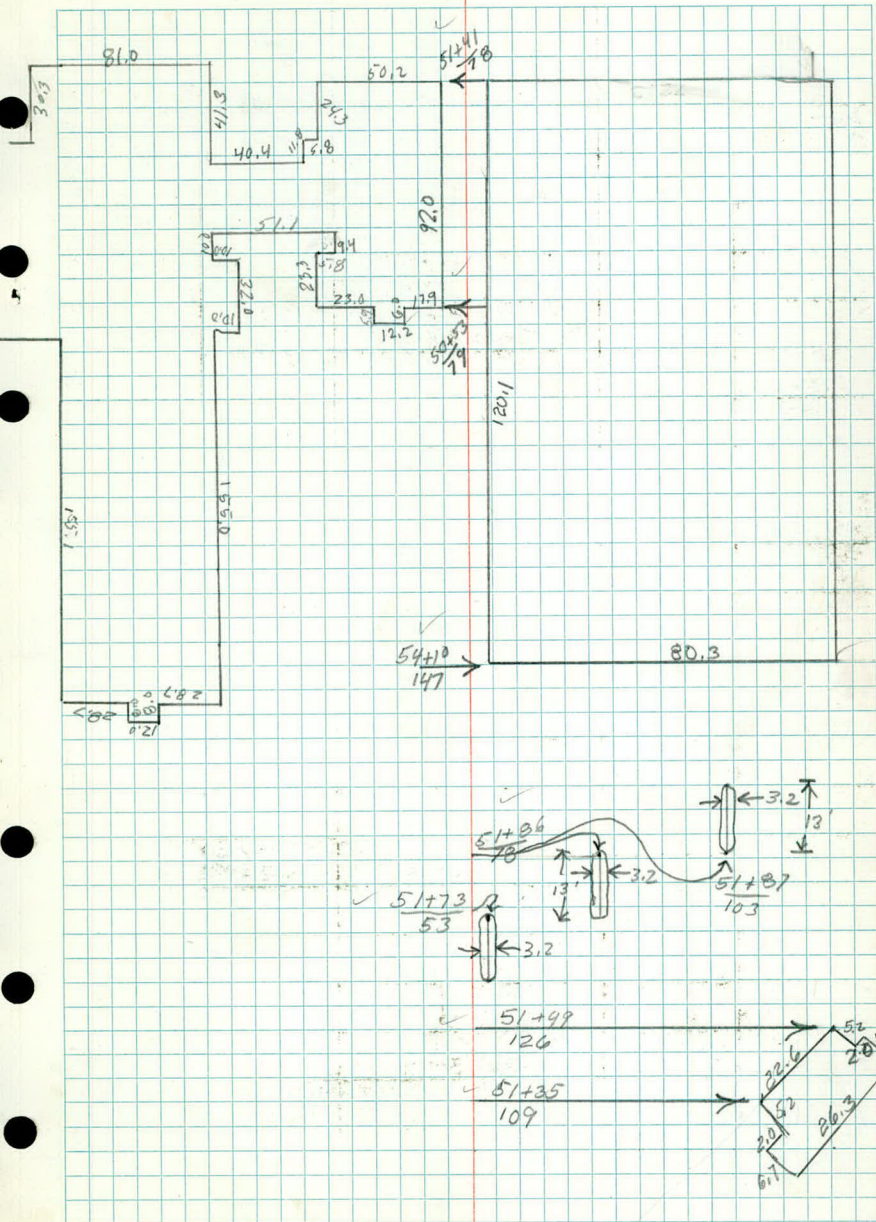


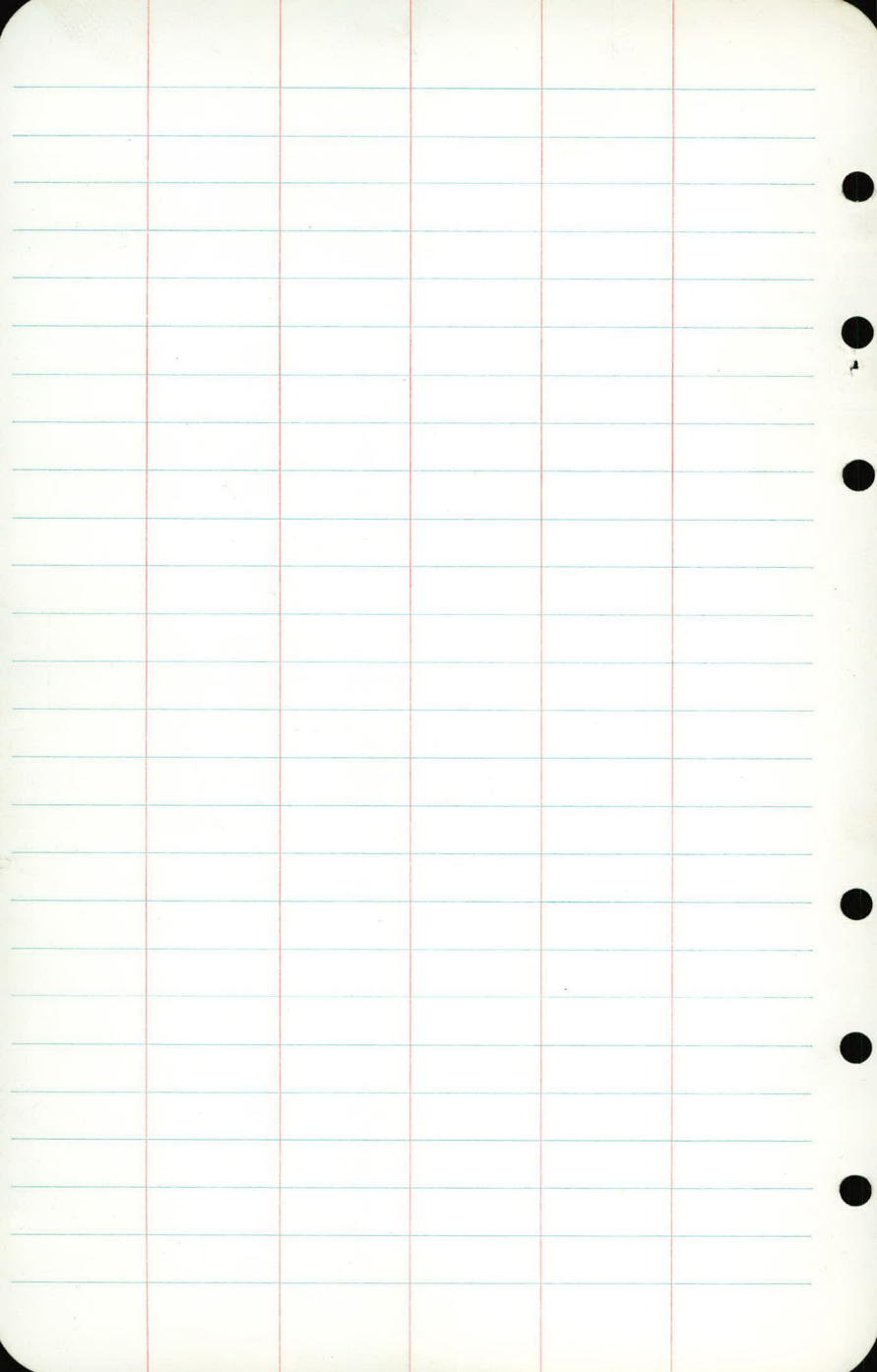
LT

E

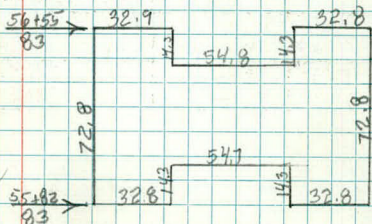
RT

9





18



19.7 BANK
95433

+73 BANK
24000

+57 BANK
55112

+38 BANK
51433

+ BANK
53433

+ BANK
50433

+ BANK
50

KP
LPD
DK

9 APRIL 1971 1.
Sunny 50°

LEXINGTON AVE
LARPENTEUR to STH#36

tree location

+50

LT

E

RT

+41 18" ELM ✓
52

+19 12" Pine ✓
52

14+00

+00 36" BE ✓
51

✓ +70 12" PINE ✓
52

✓ +57 10" APPLE ✓
57

+50

13+00

✓ +77 14" M ✓
65

✓ +76 14" M ✓
32

+50

✓ +45 12" M ✓
33

✓ +15 24" MAPLE ✓
49

12+00

✓ +04 NW COR BLDG
71

LT

19 APRIL 1971 2.

RT



17+00

LT

$$\begin{array}{r} 36'' \text{ ELM RT} \\ 37 \\ +98 \text{ SWCORHO} \\ \hline 118 \end{array}$$

+50

$$\begin{array}{r} +61 \text{ 12'' ELM} \\ 49 \\ \hline \end{array} \times$$

$$\begin{array}{r} +13 \text{ 12'' ELM} \\ 47 \\ \hline \end{array} \times$$

16+00

+97 NECORHO

$$\begin{array}{r} +93 \text{ 6'' M} \\ 56 \\ \hline \end{array} \times$$

$$\begin{array}{r} +77 \text{ 34'' ELM} \\ 55 \\ \hline \end{array} \times$$

+50

$$\begin{array}{r} +68 \text{ 6'' M} \\ 48 \\ \hline \end{array} \checkmark$$

$$\begin{array}{r} +32 \text{ 2-4'' M} \\ 50 \\ \hline \end{array} \checkmark$$

$$\begin{array}{r} +12 \text{ 8'' PINE} \\ 49 \\ \hline \end{array} \checkmark$$

15+00

$$\begin{array}{r} +88 \text{ 10'' BE} \\ 54 \\ \hline \end{array} \checkmark$$

$$\begin{array}{r} +81 \text{ 10'' PINE} \\ 49 \\ \hline \end{array} \checkmark$$

$$\begin{array}{r} +68 \text{ 24'' BE} \\ 52 \\ \hline \end{array} \checkmark$$

$$\begin{array}{r} +70 \text{ 8'' PINE} \\ 52 \\ \hline \end{array} \checkmark$$

4+50

LT

9 APRIL 1971

3.

RT



+50

LT

E

RT

+43

12" ASH
49

+43 WALL ✓

51 +36 WALL
22

+16 6" ASH ✓

+25 24" BE
53

+04 NE COR HO
88

57

+07 36" BE
52

19+00

+04 SW COR HO
113

+62 8" PINE ✓

57

+63 STP ✓
41

+50

+46 10" Birch
56

+26 6" PINE
55

+09 6" PINE

56 +04 1/4" POP
37

+22 36" ELM
41

18+00

+64 NE COR HO
82

+77 8" PINE ✓

+93 SW COR HO

114

+60 8" M ✓
46

+46 +74 18" POP
37

+74 38" ELM
39

+58 10" TW 130R
36

+73 HEDGE
42-E ✓

+50

+10

+40 10" POP
36

+43 3" M
53

+23 1" M
51

+31 1" M
46

+11 4" M
36

+09 8" PINE
50

+09 36" ELM ✓
44

+00 36" ELM ✓
37

17+00

LT

9 APRIL 1971 4.

E

RT

8.



HEDGE



22+00

LT

E

RT

+50

+43 12" ELM
52+06 20" M ✓
51

21+00

+826 N E Cor Ho
85+80 WALL
22-32+99 WALL
22-32+68 WALL
24-E+69 4" Birch ✓
56+77 18" ASH ✓
49

+50

+44 8" Pine ✓
57+49 14" ELM ✓
54+41 SW Cor 110
174

20+00

+20 40" M ✓ +11 NW Cor House
39 166+90 12" ELM ✓
49+61 WALL ✓
21+58 WALL ✓
49

19+50

LT

£

9 APRIL 1971

5.

RT



BLOCK WALL



+50

LT +50 Barrier ✓
52

R+

+47 Barrier ✓
40

+45 CONC WALL ✓
35

+42 12" M ✓

+43 5/6 N 50
34

24+00

+86 NE COR AHN Redity
78

+55 NW COR APT
106

+50

23+00

+86 NW COR APT
106

+50

+36 NE COR HO
87

+28 27" ELM ✓
52

+11 14" TWIN PINE ✓
54

+00 NW COR HO
195

22+00

9 APRIL 1971

6.

—

④

④

*

27+00

LT

F

RT

+88 LITE, +92 Cor Conc 50 ✓+82 Cor Conc 53
24+77 Cor Conc 15 ✓+72 SIGN 55 ✓+83 SIGN 39 ✓

+50

+50 14" ELM 39 ✓

26+00

Cor Conc

35

+96 SIGN 33 ✓+98 LP 28 ✓+87 SIGN 40 ✓
32+83 NEND. Island 5327
20+80 NW Cor GAS STATION 70

+50

+63 NEND island 53+26 NE Cor GAS STATION 61+26 NEND Island 76+25 NEND Island 55+19 LITE 34+30 Cor Conc 33+39 Cor Conc 35+09 Cor Conc 33

25+00

+70 SW COR Ho 75

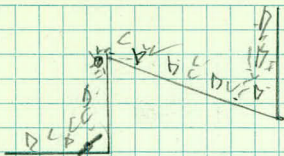
24+50

LT

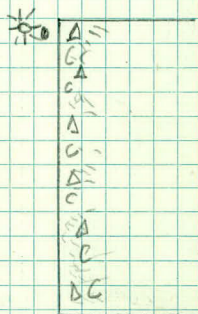
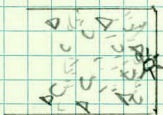
9 APRIL 1971

RT

7.



REVOLVING



+50

✓LT
+48 11" Pine
40

E

R_T

+45 2" Pine ✓
40
+47 2" Pine ✓
40

+33 4" Pine ✓
40
+17 4" Pine ✓
40

+13 3" Pine ✓
40

+39 NE CORAPE
83

+13 24" ELM ✓
40

29+00

+78 4" Pine ✓
40
+89 2" Pine ✓
40

+71 SE CORAPE
83

+74 20" ELM ✓
38

+50

+74 SW COR Bldg
76

+12 Conc. Cor. ✓
15

+06 Conc. ✓
27

+02 LITE ✓

+03 NW COR Bldg
109

28+00

+99 Conc. Cor. ✓
53

+88 NE COR Bldg
93

+93 18" ELM ✓
39

+80 Conc. Cor. ✓
15-23

+74 Conc. Cor. ✓
50

+57 N Side 156nd
66

+53 24" ELM ✓
40

+50

+42 FLAG POLE ✓
37

+41 N Side 156nd
67

+46 PP ✓
28

+16 Conc. Cor. ✓
50

+09 Conc. Cor. ✓
15 & 27

+13 14" ELM ✓
39

27+00

+03 SW COR Bldg
114

LT

~~4~~

4 APRIL 1971

RT

8,

X

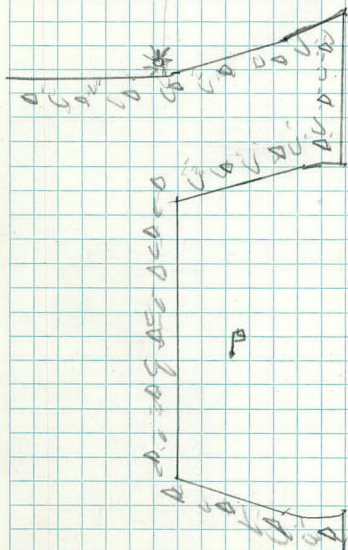
*
*

8

*

*

8



8

8

8

32+00

LT

E

RT

✓
+83 24" ELM
39

✓
+69 Bush
40

✓
+62 Bushes
38
+52 ✓ Bushes
38

+50

✓
+16 36" ELM
40

✓
+35 4" Pine
34

31+00

+99 END HEDGE

+19 NW COR HO
105

33

✓
+93 24" ELM
47

+51 NW COR HO
80

+50

✓
24" ELM
47

✓
+36 Begin hedge
33
+32 24" ELM
47

30+00

✓
+89 26" ELM
47

✓
+61 12" Birch
40

✓
+53 2" Pine
40

✓
+52 18" ELM
40

29+50

LT

9 APRIL 1971

RT

9.



Bushes



HERE



+50

LT

L

RT

+48 FE
32

+44 26" ELM +24 FE
37 32-41

+22 4" Pine
38

+28 6" Pine +35 8" Pine
36 39
+23 6" Pine +25 HEDGE
40 41-E

34+00

+90 2" Pine
38

+74 NW COR HO +98 6" Pine
147 51
+94 36" ELM +82 6" Pine
38 54

+50

+49 SE COR HO
96

+41 BUSH +48 Bush
40 40
+35 20" ELM
38
+30 BUSH +23 Bush
40 40
+07 24" M
40

33+00

+00? BUSH +82 Bush
40 35
+70 24" ELM +84 FE
38 33-E

+50

+47 2" Pine
44

+16 24" M +20 NE COR HO
46 95

+40 STP +36 NW COR HO
38 149

+09 36" ELM
39

32+00

LT

9 APRIL 1971

10.

RT

3' WOOD
2 BOARDS



X

X

X

X

X



X

π



14
33

13
33
44

37+00

LT

Z

RT

+50

$$\begin{array}{r} \checkmark \\ 36" \text{ELM} \\ \hline 40 \end{array}$$

$$\begin{array}{r} \checkmark \\ +86 \text{ STP} \\ \hline 33 \end{array}$$

36+00

$$\begin{array}{r} \checkmark \\ +84 \text{ TW } 12" \text{ROP} \\ \hline 54 \end{array}$$

$$\begin{array}{r} \checkmark \\ +42 \text{ 36" ELM} \\ \hline 36 \end{array}$$

$$\begin{array}{r} \checkmark \\ +46 \text{ 36" CPTT} \\ \hline 36 \end{array}$$

$$\begin{array}{r} +12 \text{ FE} \\ \hline 32-36 \end{array}$$

$$\begin{array}{r} \text{FE} \\ \hline 32 \end{array}$$

$$\begin{array}{r} \checkmark \\ +97 \text{ 10" Pms} \\ \hline 43 \end{array}$$

+50

$$\begin{array}{r} \checkmark \\ +15 \text{ 34" BE} \\ \hline 40 \end{array}$$

$$\begin{array}{r} \checkmark \\ +41 \text{ 20" ELM} \\ \hline 36 \end{array}$$

$$\begin{array}{r} \text{FE} \\ \hline 32 \end{array}$$

$$\begin{array}{r} +13 \text{ FE} \\ \hline 32 \end{array}$$

35+00

$$\begin{array}{r} \checkmark \\ 30" \text{BE} \\ \hline 40 \end{array}$$

$$\begin{array}{r} +96 \text{ SECOR HO} \\ \hline 97 \end{array}$$

$$\begin{array}{r} +97 \text{ FE} \\ \hline 32 \end{array}$$

$$\begin{array}{r} +70 \text{ SW COR HO} \\ \hline 148 \end{array}$$

$$\begin{array}{r} \checkmark \\ +76 \text{ 28" BE} \\ \hline 40 \end{array}$$

$$\begin{array}{r} \checkmark \\ +93 \text{ 24" ELM} \\ \hline 36 \end{array}$$

$$\begin{array}{r} \checkmark \\ +65 \text{ 26" ELM} \\ \hline 37 \end{array}$$

$$\begin{array}{r} +64 \text{ FE} \\ \hline 32 \end{array}$$

34+50

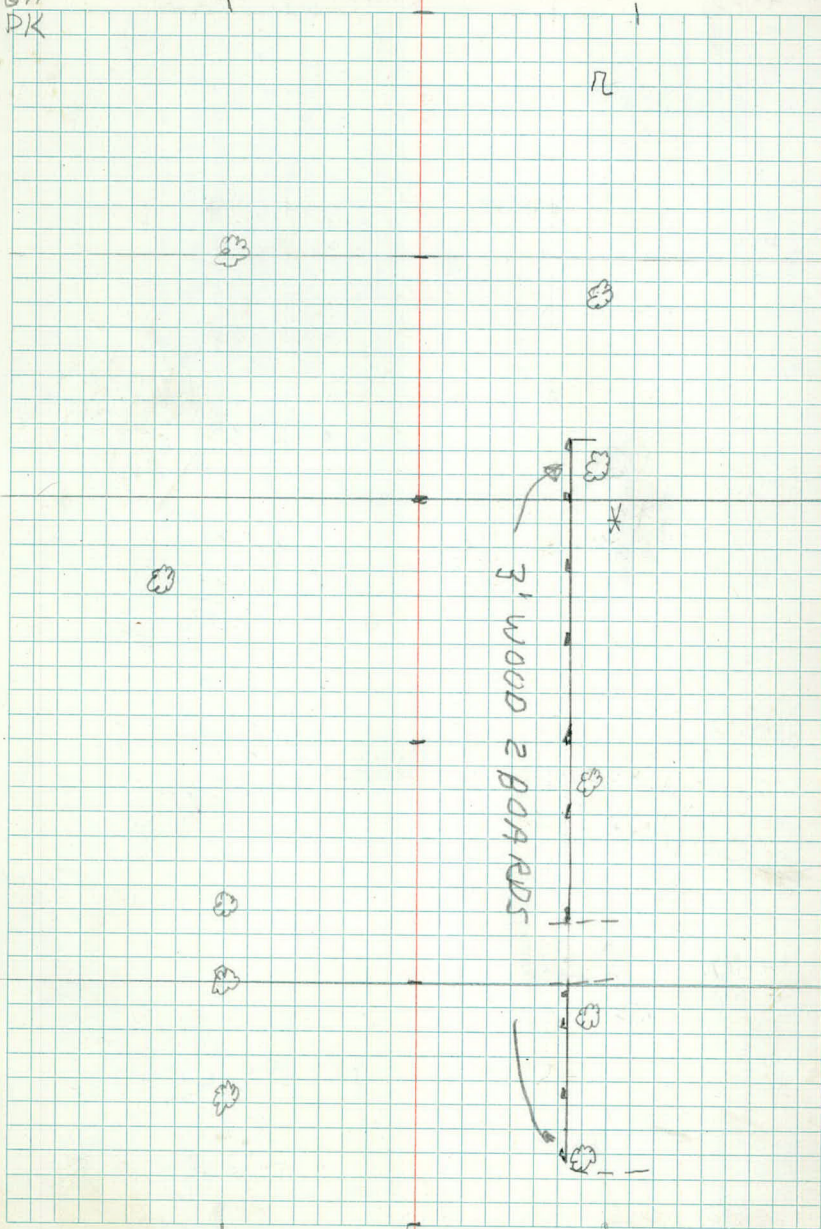
KP
LPD
GA
DK

16 APR 12 1971
Sunny 55°

11.

12

3' WOOD 2 BOARDS



+50

LT

£

R_T

+106 8" TW APPLE

55

+11 FE Cor

34-W

39+00

Triple 10" APPLE

44

+94 12" APPLE

+89 NE Cor Ho

109

54

+68 48" ELM

40

+50

FE

34

+16 18" ELM

41

+38 NW Cor Ho

102

+39 18" ELM

30

+07 57P

30

+87 28" M

30

+65 16" M

34

+34 NW Cor Ho

108

+41 36" ELM

33

38+00

FE

34

+97 36" ELM

33

+97 Trip 10" ELM

40

+75 36" ELM

34

+80 End hedge

34

+87 4" Birch

52

+82 Bush

37

+68 36" ELM

40

+51 END HEDGE

34

+67 NW Cor Ho

107

+50

+80 FE Cor

34-W

+66 NE Cor Ho

98

+32 40" ELM

34

+39 32" ELM

40

+17 Begin hedge

34

+10 40" ELM

34

+11 NW Cor Ho

106

37+00

42+00

LT

£100 STP
34

RT

+96 Hedge ✓
42

+96 SW COR HO
113

+86 HEDGE ✓
35

+50

+31 24" ELM ✓

+15 STP ✓
35

40

+28 NE COR HO +03 8" Pine 83
90 35 23

+01 STP
40

41+00

+95 Bush ✓
40

+84 NW COR HO
116

+70 12" ELM ✓

+79 36" ELM
34

+60 2-1" Pine 40

+50 44 ✓

+45 12" ELM ✓
40

+40 14" ELM
34

+44 NE COR HO
90

+19 14" ELM ✓
40

+21 NW COR HO
115

+21 Bush ✓
34

+00 30" ELM
34

+74 Bush ✓
30

+91 18" ELM ✓
40

+74 Bush ✓
42

+61 26" ELM
46

+69 14" ELM ✓
34

39+50

12 APRIL 1971 13.

LT

~~E~~

RT



+50

44+00

+87 NE con Ho
90 + 93 26" ELM
39

+59 20" ELM
40

+50

+27 4" Pine
50
+ 12 24" M
40

+06 6" Pine
47

43+00

+02 NE con Ho
90
33
51

+

+63 26" ELM
40

+50 6" Pine
36

+21 2" Pine
36

+21 20" ELM
40

+10 NE con Ho
96

42+00

+02 36" ELM
34

+63 26" ELM
34

82
33

+37 NE con Ho
115

+15 24" ELM
36

+81 18" ELM
34

+65 8" Pine
51

+41 STP
34

12 APRIL 1971

14.

LT

£

RT

47+00

FE
33

+96 SW cor church & dy
90 ✓

+77 STP
35 ✓

+71 20" ELM
34 ✓

+84 18" ELM
34 ✓

+58 20" ELM
34 ✓

+50

+31 FE cor
34-W

+34 36" ELM
34 ✓

46+00

+78 10" ELM
51 ✓

+92 30" ELM
34 ✓

+50

+52 6" Pine
40 ✓

+52 34" ELM
34 ✓

+42 STP
43 ✓

+37 NE cor Ho
93

+13 30" ELM
34 ✓

+18 NW cor Ho
108

45+00

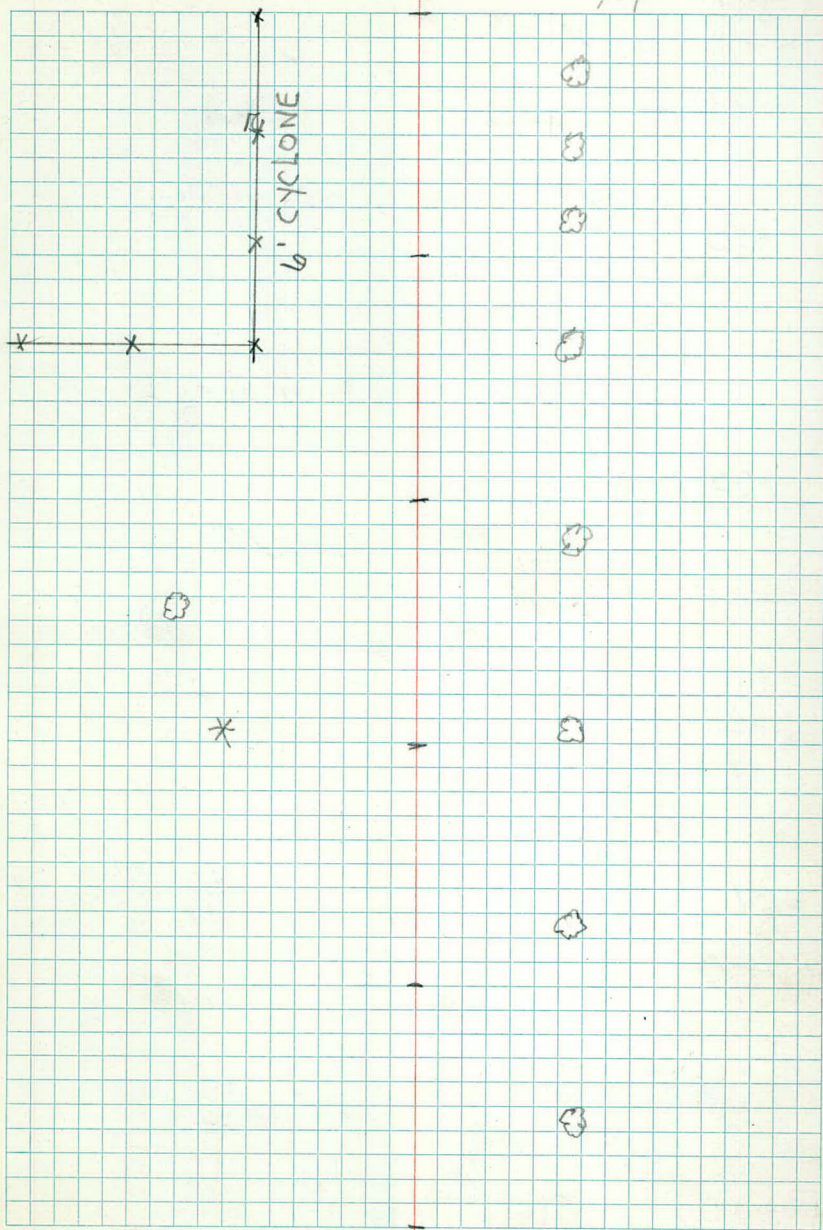
+71 NE cor House
91

+72 30" ELM
34 ✓

44+50

+63 HEDGE
50-E

LT 12 APRIL 1971 15. RT



+50

FE
33

E

+9 400

+50

✓
+52 24" ELM
34

+51 NWCOA Church
89

✓
+31 28" ELM
34

47 55
33 33
+15 ETR Church
80

+8 400

✓
+91 10" PLUM
56

+80 10" Pine
38

✓
+80 8" Pine
46

+50

✓
+91 28" M
34

+84 SWCO Church
88

✓
+57 36" ELM
34

+56 NWCOA Church
90

✓
+44 22" Ash
38

+18 24" Ash
37

✓
+11 18" ELM
34

+7 400

12 APRIL 1971 16.

6' CYCLONE



52+00

LT

L

SW

RT

+95 FE
35+96 END WALL +73 18" ELM
33 46+69 BUSH
41

+50

+45 NE COR School
78+48 Bush
41+44 36" ELM
+30 E 5' SW 46+22 26" ELM
4651+00 +02 26" ELM WALL
46 34+82 20" ELM
46+60 34" ELM
46

+50

+30 PP +30 WALL
28 33+30 END FE
33

50+00

49+50

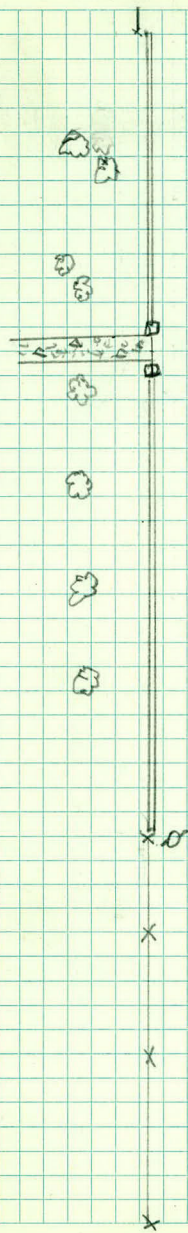
28-33

+87 S END ISLAND #1
103+86 N. END ISLAND #2
78+73 N. END ISLAND #3
53+64 LITE
35+49 NW COR Bldg
126+35 SW COR Bldg
109
+22 SW
28-33+25 LITE
34+22 FE
38-E+79 NW COR Bldg
136
+70 26" ELM
34+45 4'-4" Birch
34+44 24" ELM
34+26 18" Ash
34

12 APRIL 1971 17,
Rt

LT

E



A
B
C
D
E
F
G
H
I
J
K
L
M
N
O
P
Q
R
S
T
U
V
W
X
Y
Z

CLARK

2' CYCLONE



+50

LT

~~L~~

RT

+05 ~~NE~~ ^{cor}
80 Burger chef

+10 SW cor Store
147

54+00

+78 LITE
33

+50

53+00

+95 SIGN
42

+97 Bush
36

+50

+10 FE
38-W +14 18" ELM
46

+06 FE
35

52+00

+20 LITE
34

+12 SIGN
41

+16 SW
28-33

LT

E

12 APRIL 1971 18.

RT

✱

✱



57+00

Σ

✓
+62 12" Pine
+68 Necor Ho 40
64
+50

✓
+48 12" Pine
38

✓
+91 12" Pine
38
+60 ✓ 12" Pine
36
+59 8" Pine
46
+54 ✓ 8" Pine
36

+55 NW cor Apt
83

56+00

✓
+80 10" Pine
61

+82 SW cor Apt
83

+50

✓
+47 24" ELM
50

+40 1" Willows
37-41-45-50
+37 WALL
34-E
+36 LITE
33 ✓

55+00

+76 TEL
33

54+50

12 APRIL 1971 19.

*

*

*

*

B

BLOCK WALL

+50

✱

✓

+38 20' ELM
36

40
32

✓

✓ +12 Begon hedge
+12 FE

+12 12" OAK 34-E 40

33

+94 Nuc cor 1/2 79

+88 8" APPLE

+87 1" Cedar
37

37

✓
+62 8" ELM
45

+50

+49 NE cor 40
103

✓
+20 48" TW COR
32

✓
+37 1" CEDAR
37

58+00

✓
+85 NW cor Apt 2
84

+71 30" OAK
32

+50

✓
+46 4" OAK
40

✓
+41 36" TW OAK
32

+43 12" OAK

✓
+34 12" Pine
40

+44 18" APPLE
52

+44 18" APPLE
40

57+00

✓
+11 SW cor Apt
83

12 APRIL 1971 20.



3 WOOD PE
3 BOARDS



62+00

LT

\$

RT

+50

$$+38 \begin{array}{r} 18" \text{ ELM} \\ 55 \end{array} + 37 \text{ END HEDGE}$$

$$+37 \begin{array}{r} 12" \text{ ELM} \\ 36 \end{array}$$

45

$$+18 \begin{array}{r} 24" \text{ ELM} \\ 37 \end{array}$$

61+00

$$+98 \begin{array}{r} \text{SECOR HO} \\ 103 \end{array}$$

$$+72 \begin{array}{r} 38" \text{ OAK} \\ 32 \end{array}$$

$$+94 \begin{array}{r} \text{NW COR HO} \\ 124 \end{array}$$

$$+54 \begin{array}{r} 8" \text{ ELM} \\ 41 \end{array}$$

$$+51 \begin{array}{r} \text{NE COR HO} \\ 101 \end{array}$$

+50

$$+49 \begin{array}{r} 10" \text{ ELM} \\ 40 \end{array}$$

$$+32 \begin{array}{r} 8" \text{ OAK} \\ 33 \end{array}$$

$$+09 \begin{array}{r} 24" \text{ ELM} \\ 29 \end{array}$$

$$+05 \begin{array}{r} 6" \text{ OAK} \\ 42 \end{array}$$

$$+03 \begin{array}{r} 4" \text{ ELM} \\ 40 \end{array}$$

42

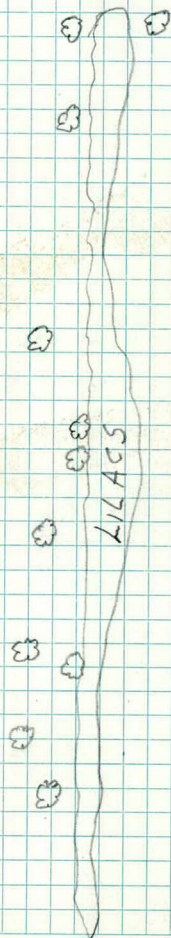
60+00

$$+89 \begin{array}{r} 8" \text{ OAK} \\ 29 \end{array}$$

$$+79 \begin{array}{r} 8" \text{ OAK} \\ 33 \end{array}$$

59+50

12 APRIL 1977, 21.



64+50

2

64+00

+74 hedge
50-70

+59 24" ELM
50

+50

+23 24" ELM
45

63+00

+04 6" ASH
42

+83 1 1/2" GCS
46

+51 1 1/2" GCS
45

+50

+51 36" M
48

+11 30" COTT
48

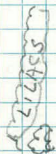
+37 30" BE
42

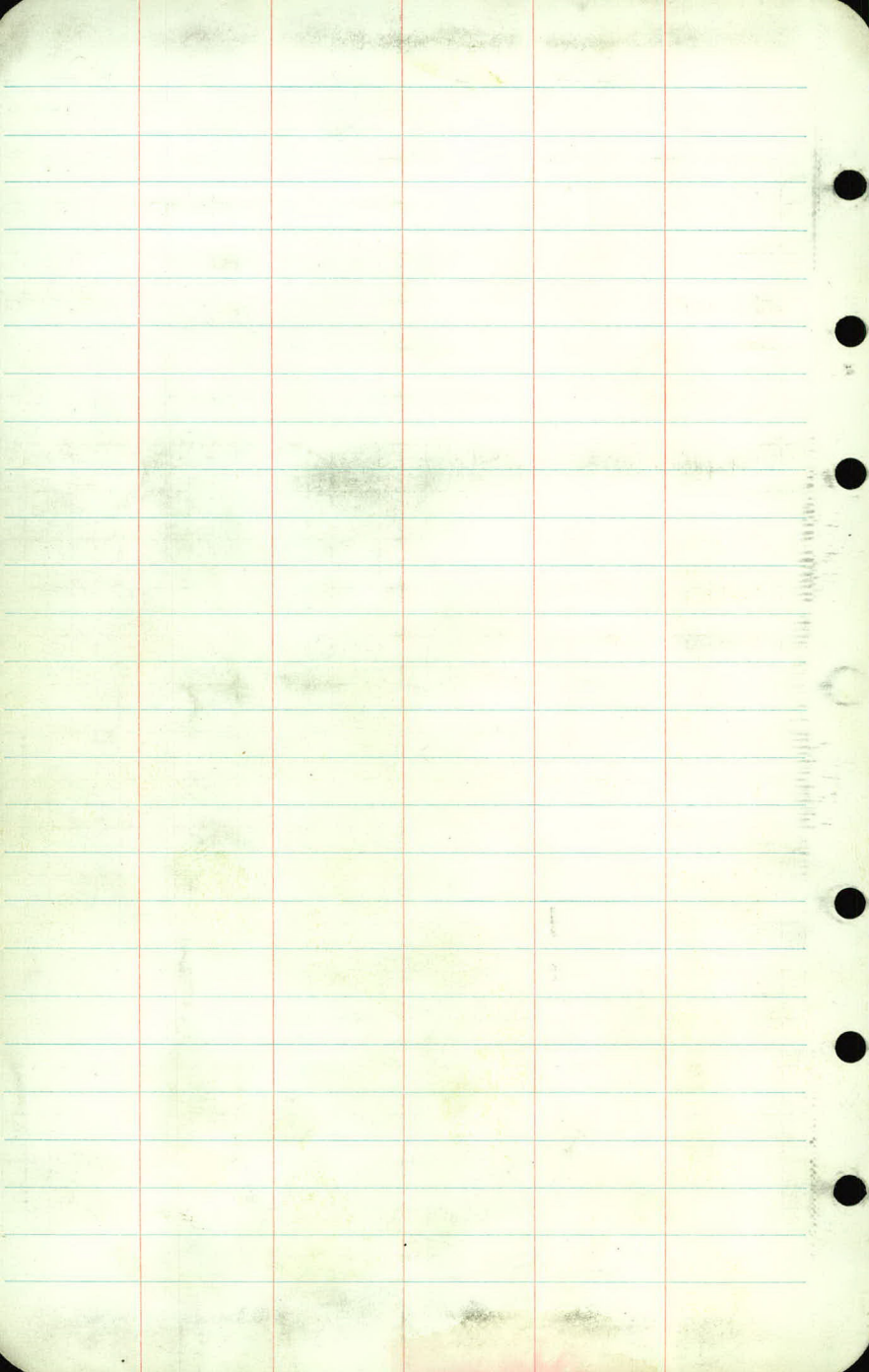
62+00

+62 28" DAK
38

12 APRIL 1971 22.

HEDGE





KP
WS
DS
GA
DK

31 MAR, 1971 1.
CLOUDY 40°

LEXINGTON AVE.

51 TURNBACK

LARPEUR AVE TO STH #36

CB'S & MH'S

+50

+32 $\frac{MH}{16}$

2+00

+50

1+00

+50

+35 $\frac{MH}{38}$

0+00

LT

2

31 MAR. 71

2.

RT

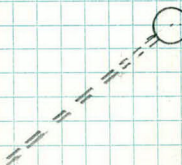
TELEPHONE M.H.

2



BOTTOM TO TOP = 7.0'
 HIGHEST CABLE
 TO TOP = 3.3'
 10" CASTING
 BRICK CONSTRUCTION
 3.5' WIDE
 6.0' LONG

1



W.S.O
 FL TO TOP = 6.60
 VALVE TO TOP = 3.30
 CASTING = 11"
 ONE RING
 ONE 1' SECTION
 ONE 45' CONCENTRIC
 COVE

6" MAIN TO SW

5+100

+50

4

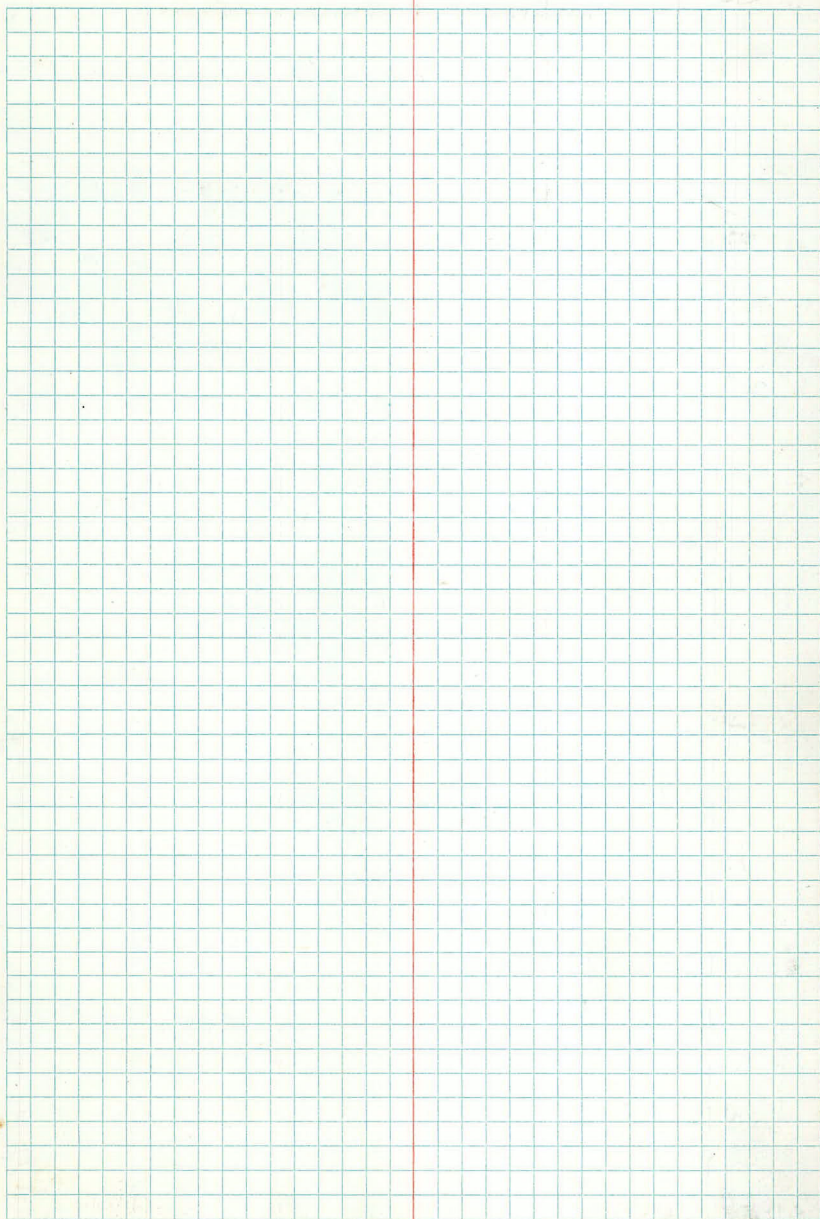
+50

3

2+50

31 MAR. 71

3



+50

+12 $\frac{MH}{34}$

+07 $\frac{CB}{23}$

+07 $\frac{SD}{34}$

7

+77 $\frac{MH}{48}$

+77 $\frac{MH}{49}$

+50

+44 $\frac{CB}{23}$

6

+88 $\frac{MH}{30}$

+88 $\frac{SD}{25}$

+50

+28 $\frac{SD}{25}$

5 +00

STORM SEWER

FL TO TOP = 3.5
11" CASTING
M/A BLOCKS
ELEVATION
932.88

STORM SEWER
FL TO TOP = 3.7
9" CASTING
BRICK CONST
15' C.N.P TO EAST

SANITARY SEWER
FL TO TOP = 15.7
11" CASTING
BOTTOM TO TOP
5' SECTION
1.5' SECTION
3.0' SECTION
4.0' CONE
2 RINGS
CONES FROM
N/E
RUNS TO
SOUTH

STORM SEWER
#15 FL TO TOP 3.9
9" CASTING
BRICK CONST
24" R.C.P TO SW

12" x 24" C.M.P.
24" R.C.P.
STORM SEWER
FL TO TOP = 3.5
11" CASTING
BRICK CONST.

SANITARY S.
FL TO TOP = 13.7
11" CASTING
BOTTOM TO TOP
4.5' SECTION
3.0' SECTION
4.5' CONE
2 RINGS
CONES FROM N/E
RUNS TO WEST
ELEVATION OF
933.42

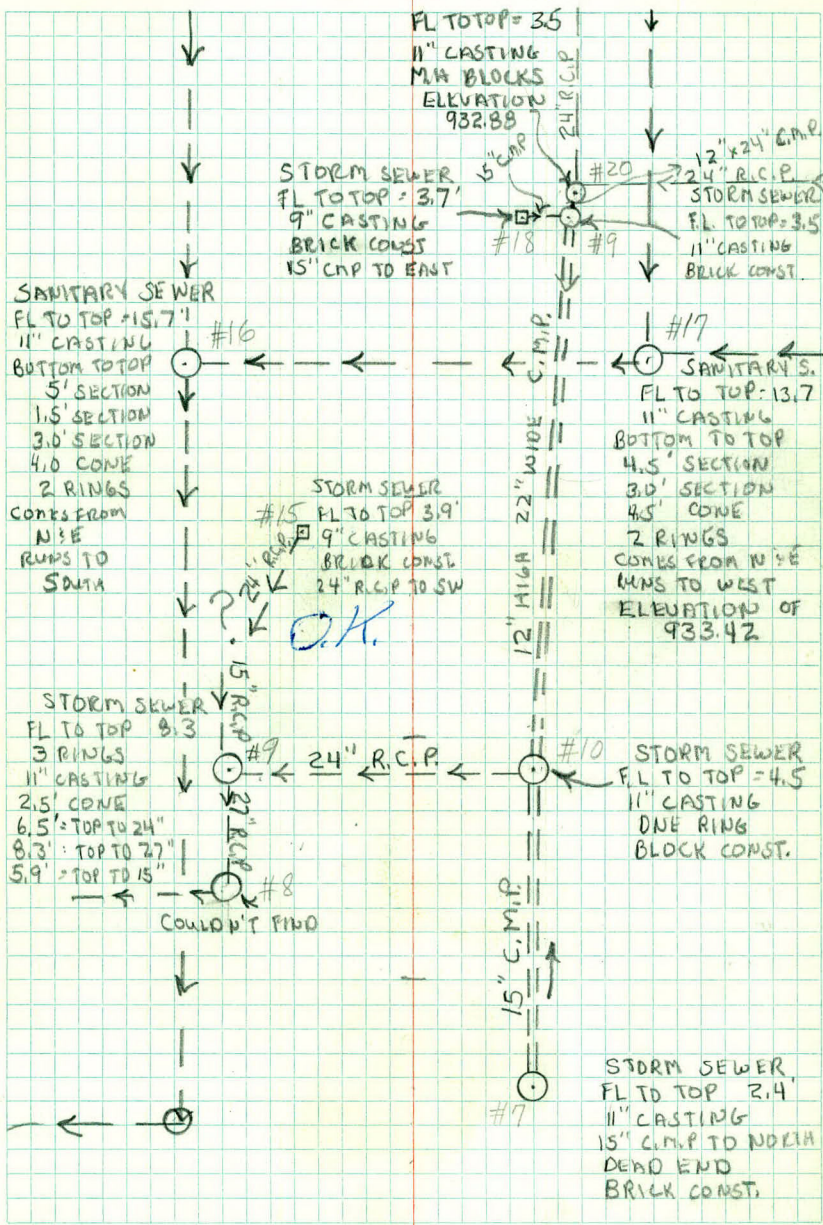
STORM SEWER
FL TO TOP 8.3
3 RINGS
11" CASTING
2.5' CONE
6.5' TO TOP TO 24"
8.3' TO TOP TO 27"
5.9' TO TOP TO 15"

STORM SEWER
FL TO TOP = 4.5
11" CASTING
ONE RING
BLOCK CONST.

STORM SEWER
FL TO TOP 2.4
11" CASTING
15" C.M.P TO NORTH
DEAD END
BRICK CONST.

COULDN'T FIND

O.K.



10

+50

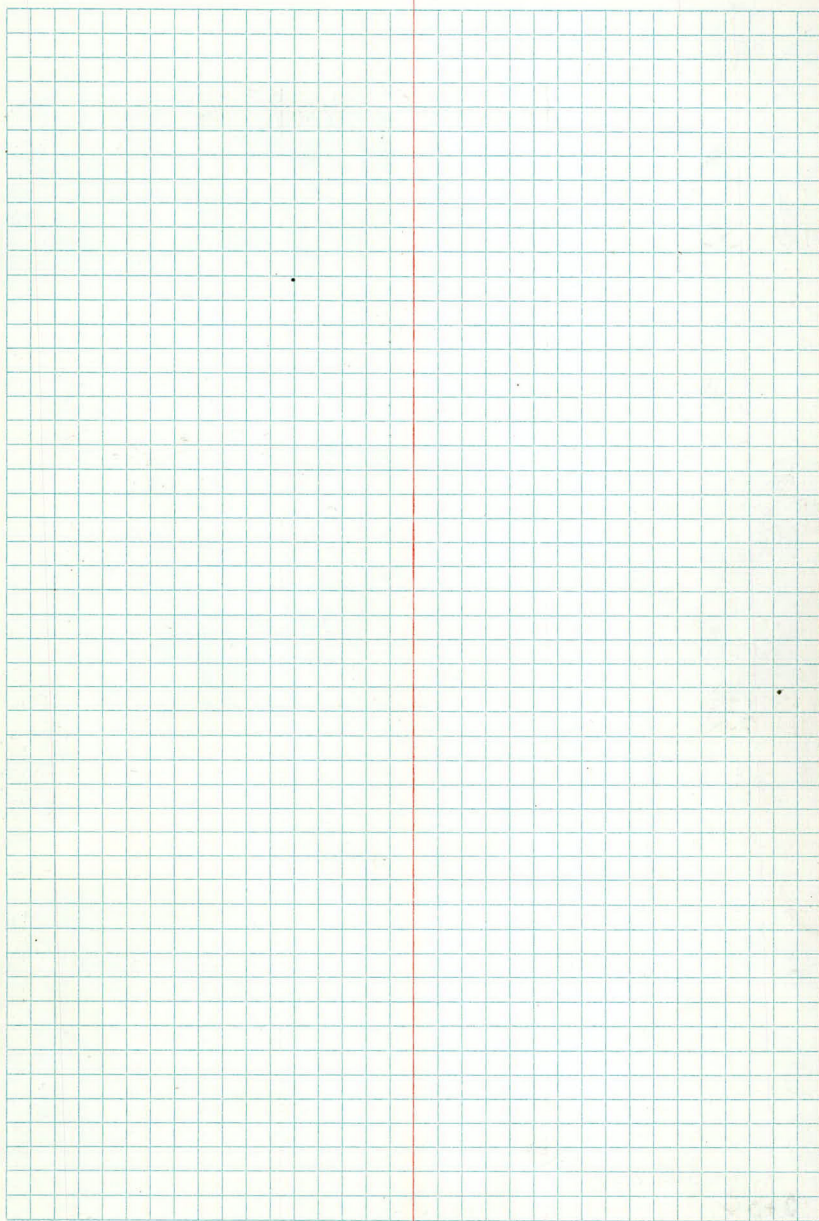
9

+50

8

7+50

31 MAR 1971 5



+50

+30 $\frac{MH}{47}$

12

+50

+17 $\frac{CB}{24}$

+03 $\frac{MH}{47}$

11

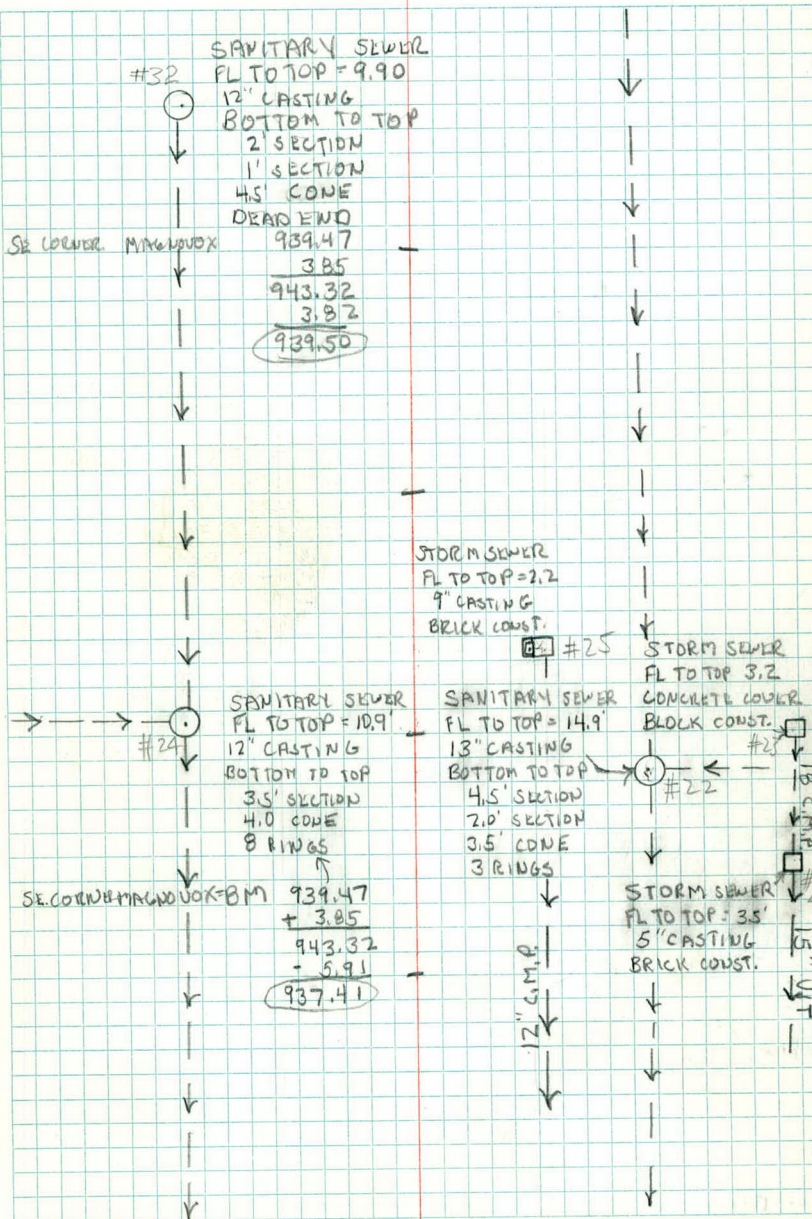
+00 $\frac{SD}{137}$

+93 $\frac{MH}{48}$

+72 $\frac{SD}{135}$

+50

10+00



15+00

£

+50

14+00

+50

13+00

•
+91 $\frac{MH}{30}$

•
+89 $\frac{MH}{17}$

•
+89 $\frac{MH}{41}$

12+50

WATER MAIN
FL TO TOP 8.34
BOTTOM TO TOP
1.6' SEC
1.1' SEC

4.3' CONCRETE CONE #3A
4 RINGS
11" CASTING

NW 1/4 BELL
FL TO TOP 5.51
11" CASTING
2 ROWS BRICK RING

#35

Sanitary SEWER
FL TO TOP 9.20
BOTTOM TO TOP
3' SECTION
5.3' ELLIPTICAL CO
11" CASTING

#36

+50

17+00

+73 $\frac{CB}{46}$

+50

+41 $\frac{M.H.}{84}$

+41 $\frac{CB}{45}$

16+00

+97 $\frac{CB}{23}$

+98 $\frac{CB}{23}$

+50

+06 $\frac{M.H.}{38}$

15+00

SAN. SEWER
 FL TO TOP 9.33'
 BOT. TO TOP
 3.2' SEC.
 4.3' ECC CONE
 4 RINGS
 11" CASTING

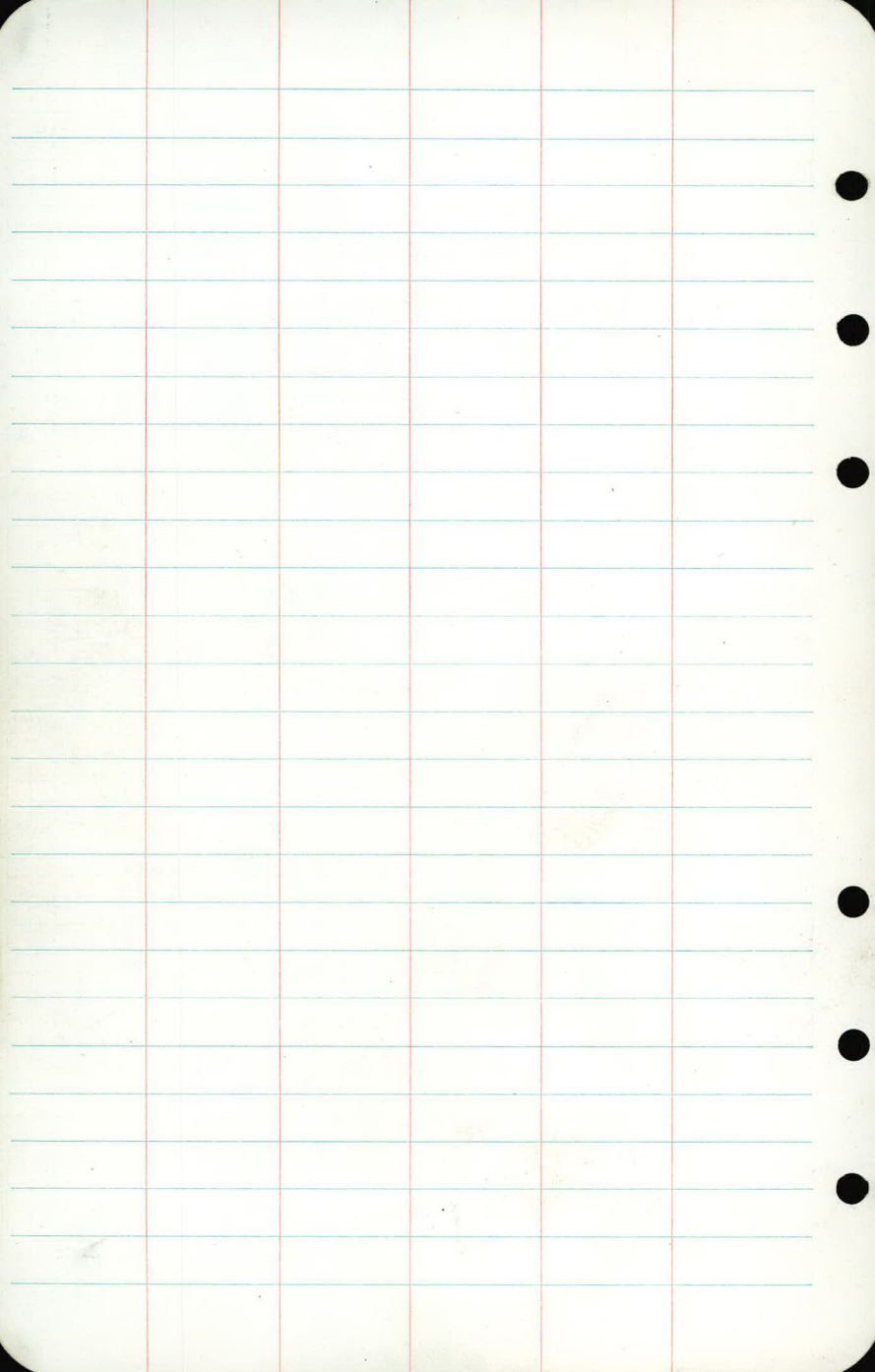
CATCH BASIN
 FL TO TOP 5.88'
 BOTTOM TO TOP #43
 3' POURED CONC
 6" MEX. HAT
 3 RINGS
 11" CASTING

#46
 CATCH BASIN
 FL TO TOP 3.68'
 BOT TO TOP
 2.1' P. CONC.
 3 RINGS
 11" CASTING

#45
 CATCH BASIN
 FL TO TOP 4.4'
 BOT TO TOP
 1.8' P. CONC.
 6" MEX. HAT
 5 RINGS
 11" CASTING

#44
 CATCH BASIN
 FLOOR TO TOP 5.02'
 BOTTOM TO TOP
 2' POURED CONC
 10 RINGS
 11" CASTING

#42
 SANITARY SEWER
 FL TO TOP 9.73'
 BOTTOM TO TOP
 3.3' SECTION
 4.4' ECC CONC
 3 RINGS
 11" CASTING



MH 38' RT 0+35
W.S.O.

FL TO TOP = 6.60

VALVE TO TOP = 3.30

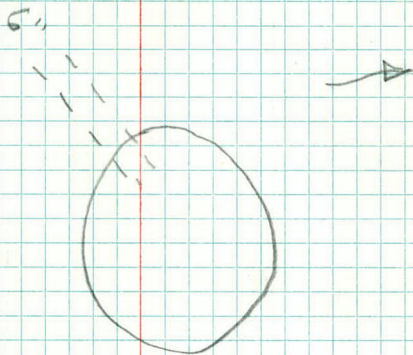
CASTING = 11"

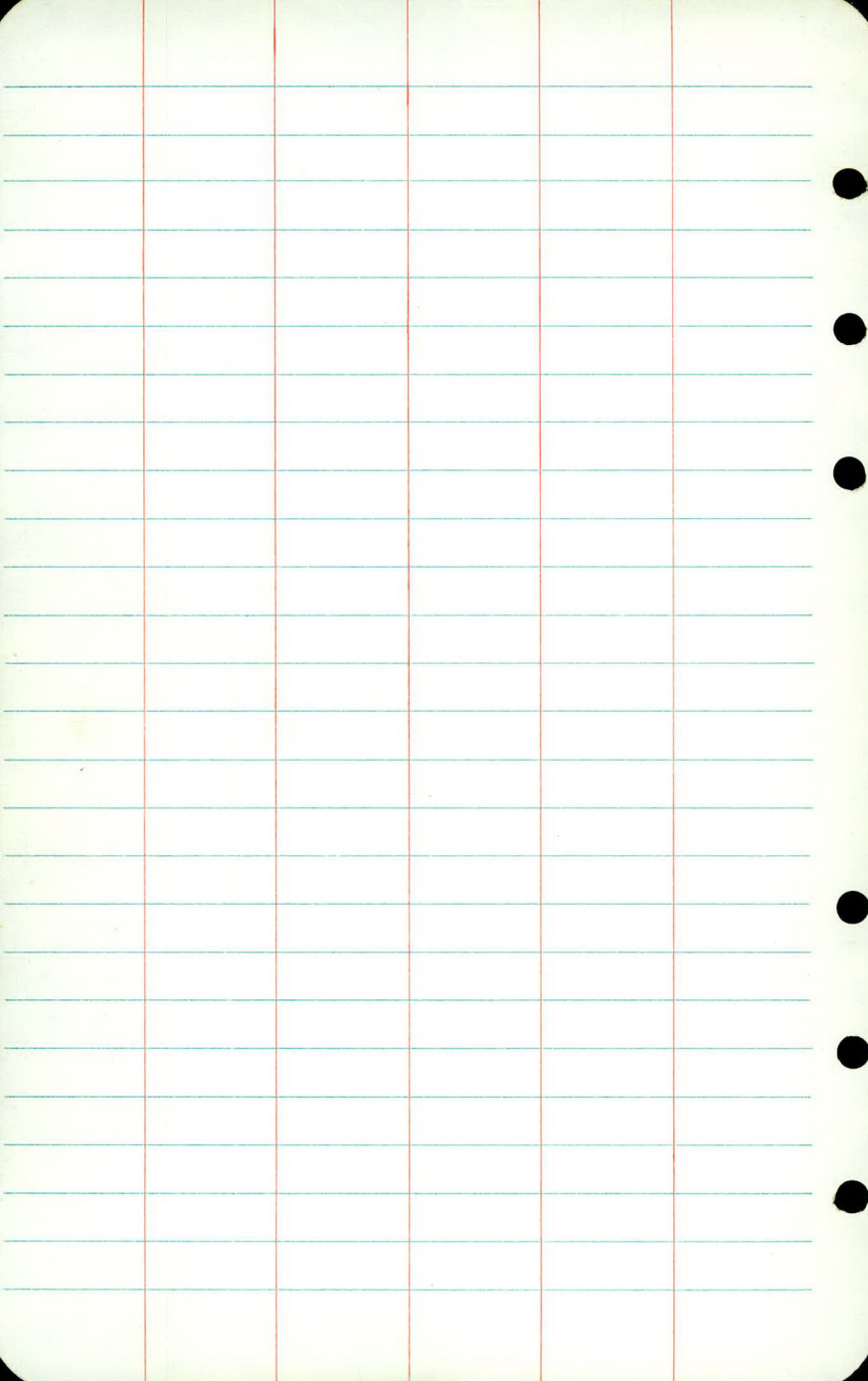
1 ring

1 - concentric cone

1 - 1' section

6" main. from SW.





2+32 16' RT (TEL.)^{3.}

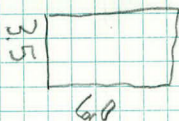
FL TO TOP = 7.0

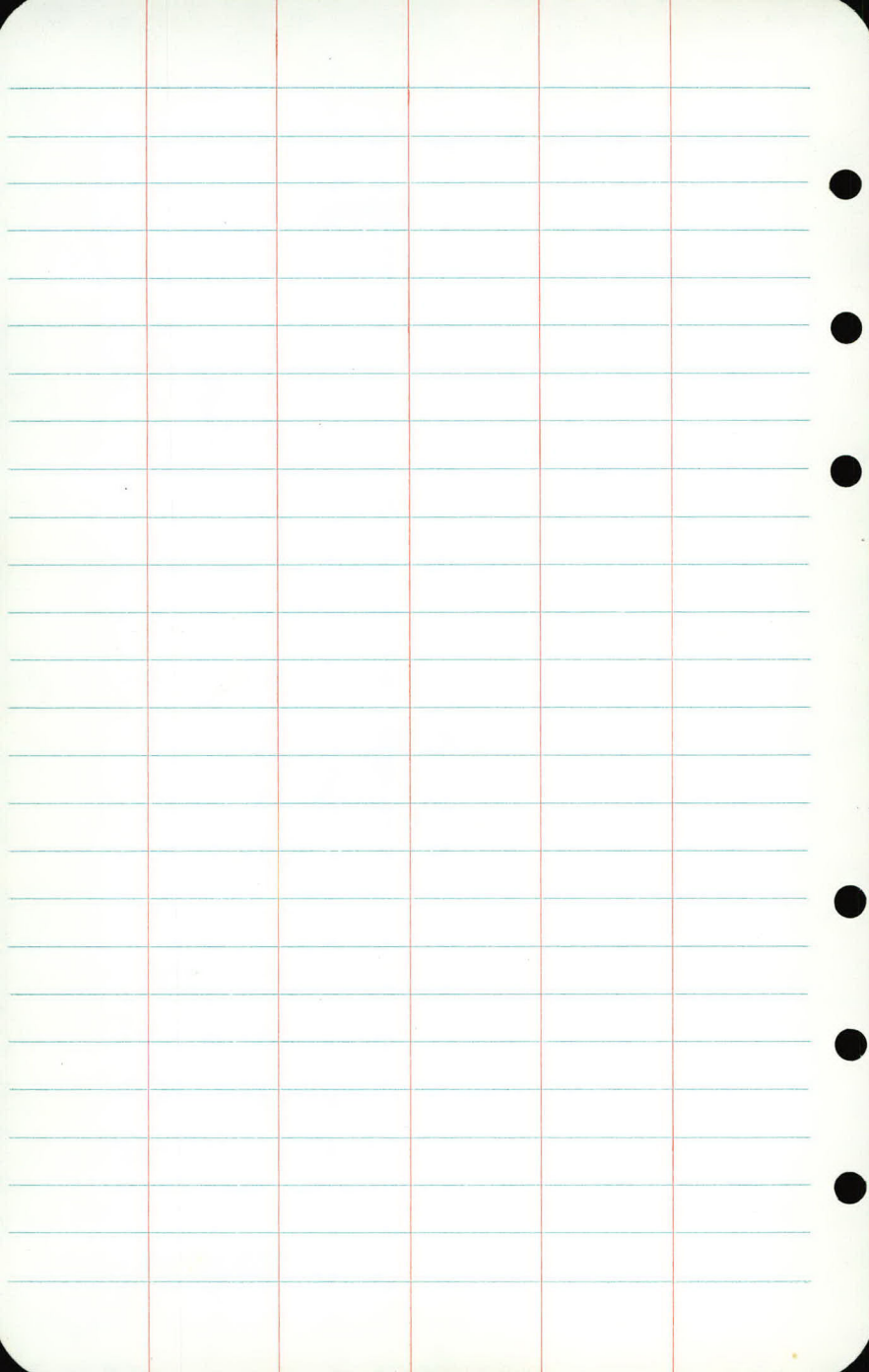
N to S
E

CABLE = 3.3

10" CASTING

BRICK





31 MAR 1971

4.

SD 5+28 25' RT

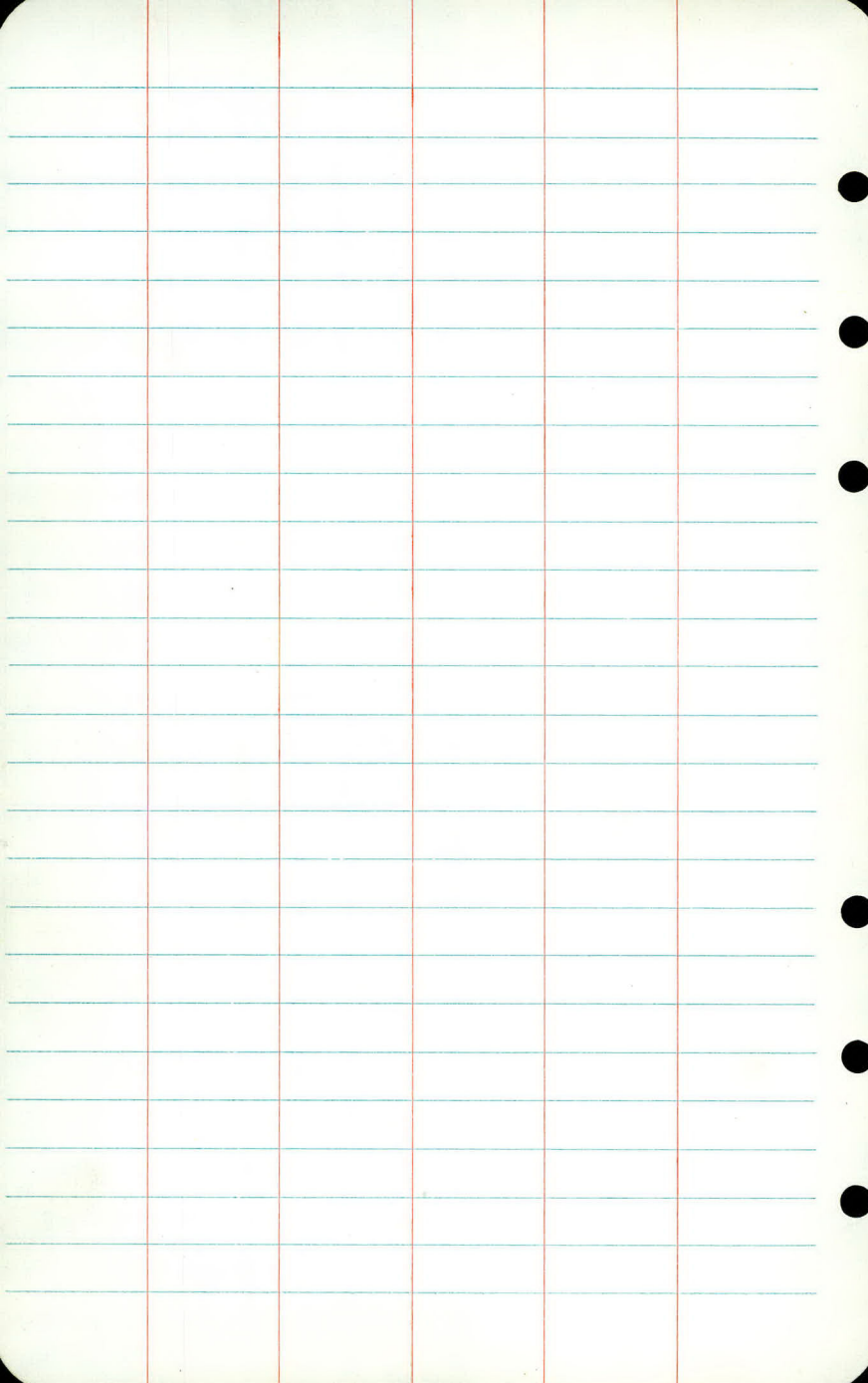
FL TO TOP = 2.4

11" CASTING

DEAD END

15" CM TO North





31 MAR 1971

SD 5+88 25' RT

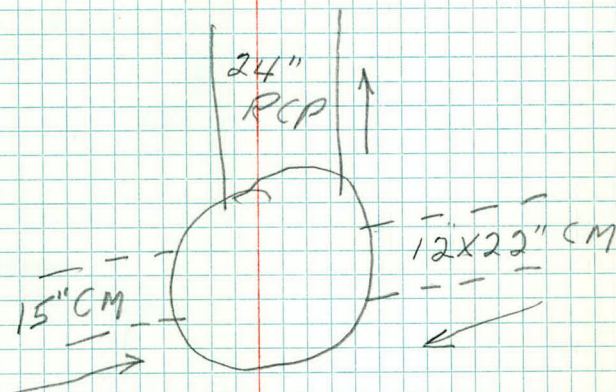
FL TO TOP = 4.5

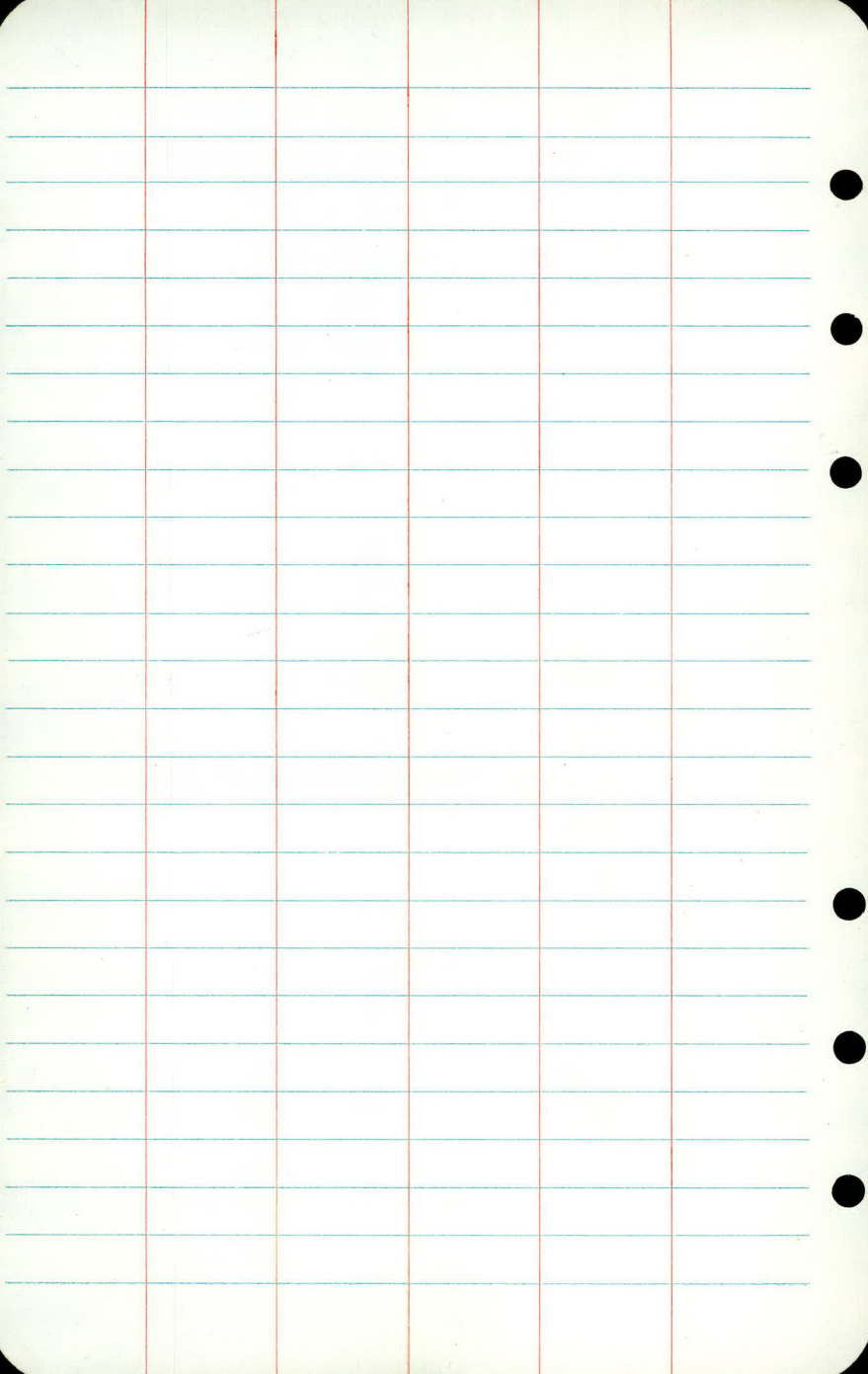
11" CASTING

1 - ring

BLOCK

Z →





MH 5+88

38' LT

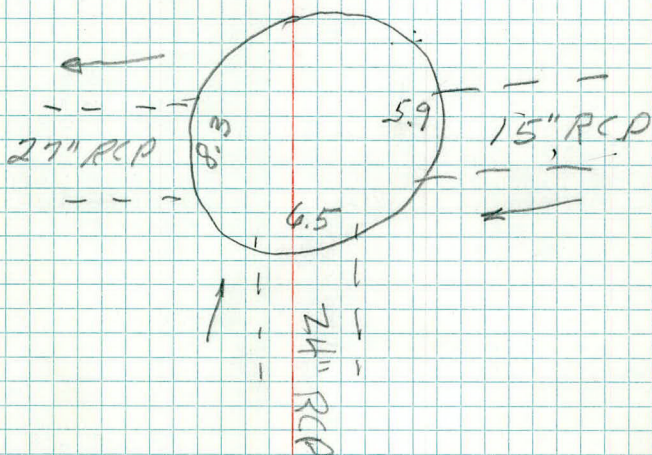
FL TO TOP 8.5

FL

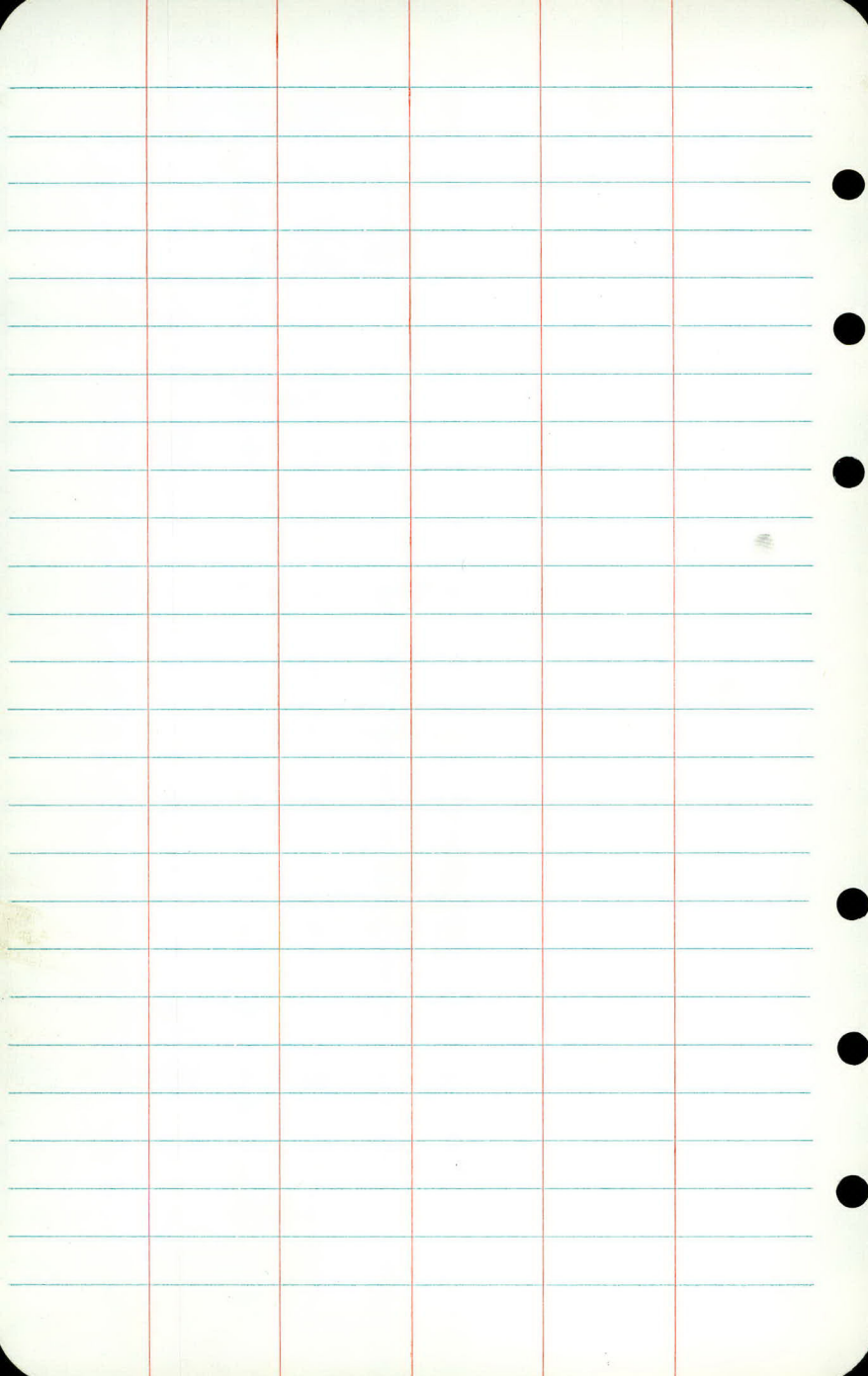
11" CASTING

3- rings

2.5 Cone



→



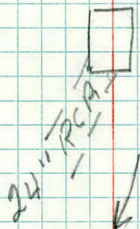
C B 6444

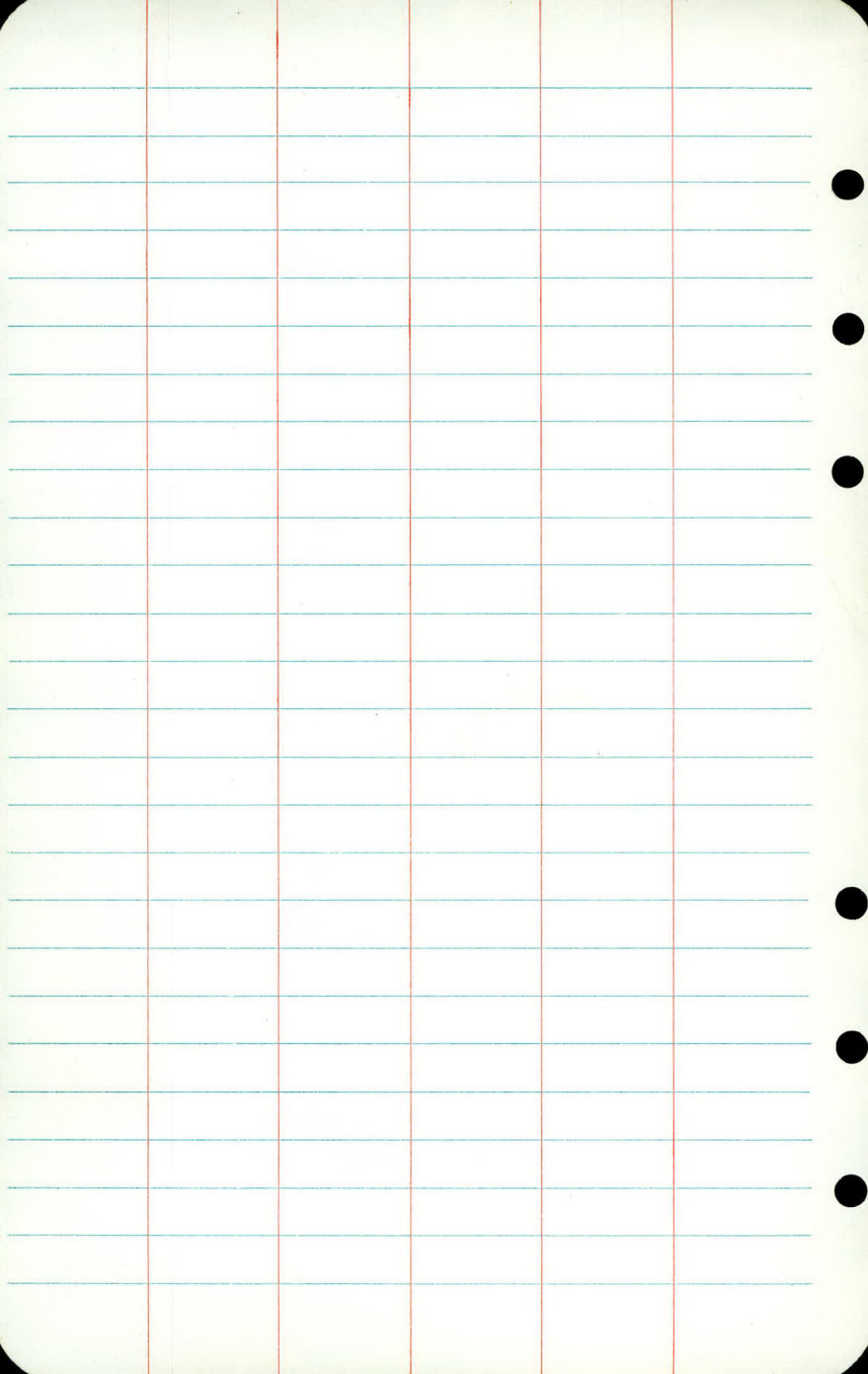
23' LT

FL TO TOP = 3.9

9" CASTING

BRICK





6+77 MH 48' LT

SANITARY

FL TO TOP = 15.7

11" CASTING

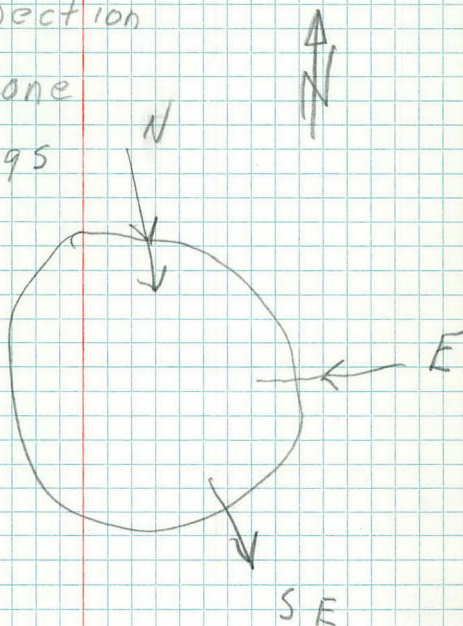
5' Section

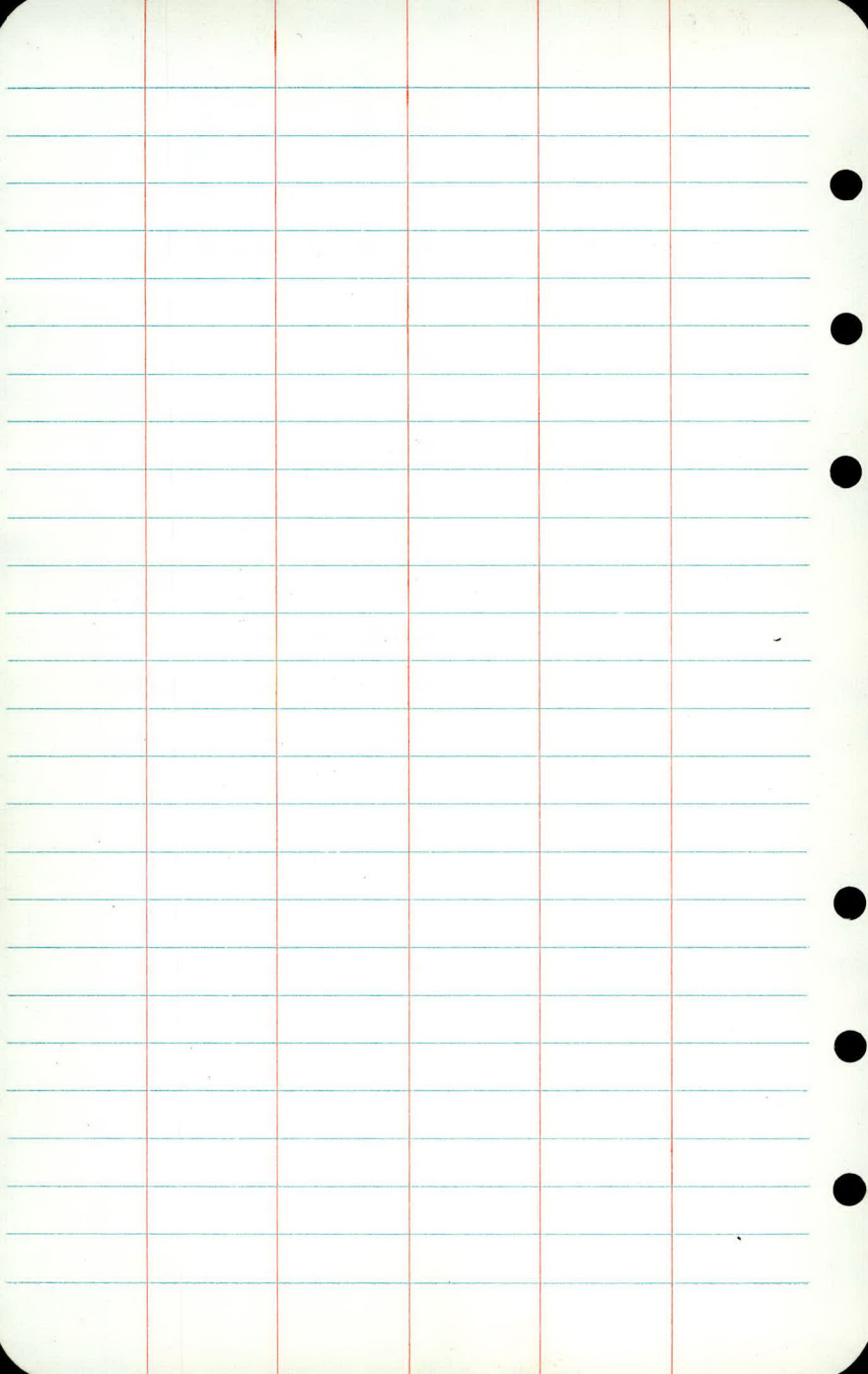
1.5' Section

3.0' Section

4.0' Cone

2 - rings





ELEV. 933.42

31 MAR 1971

MH 6+77 490' RT

SAN.

FL TO TOP = 13.7

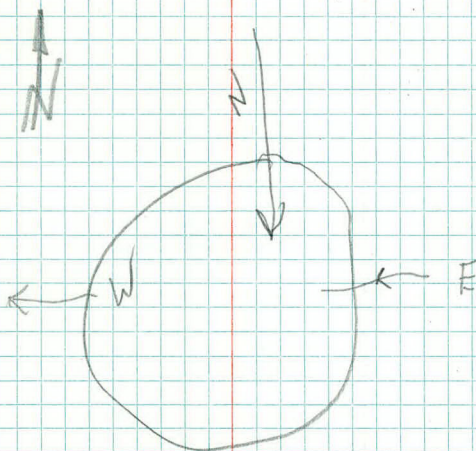
2 rings

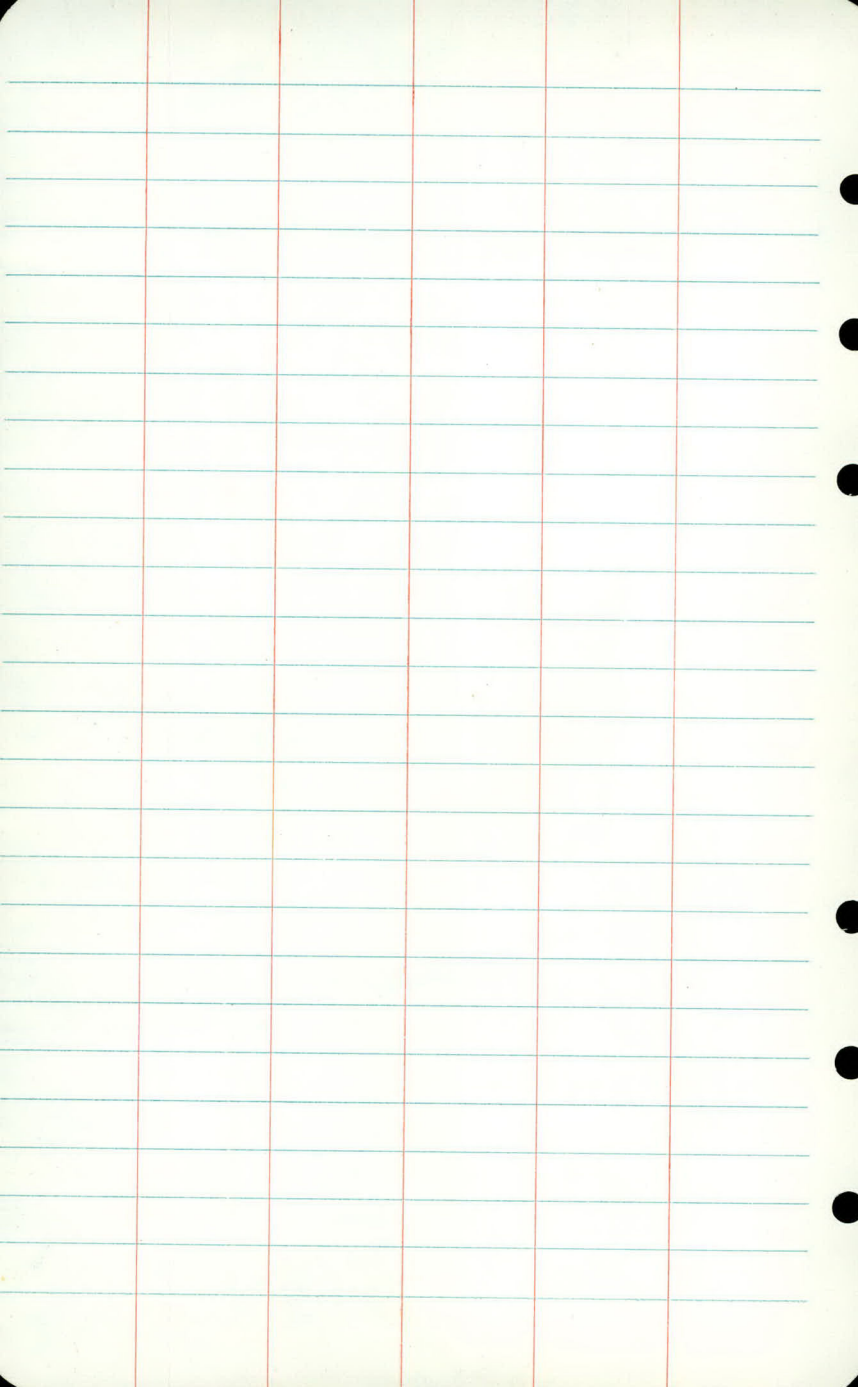
4.5 Section

3.0 Section

4.5 cone (concentric)

11" CASTING



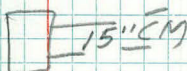
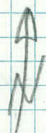


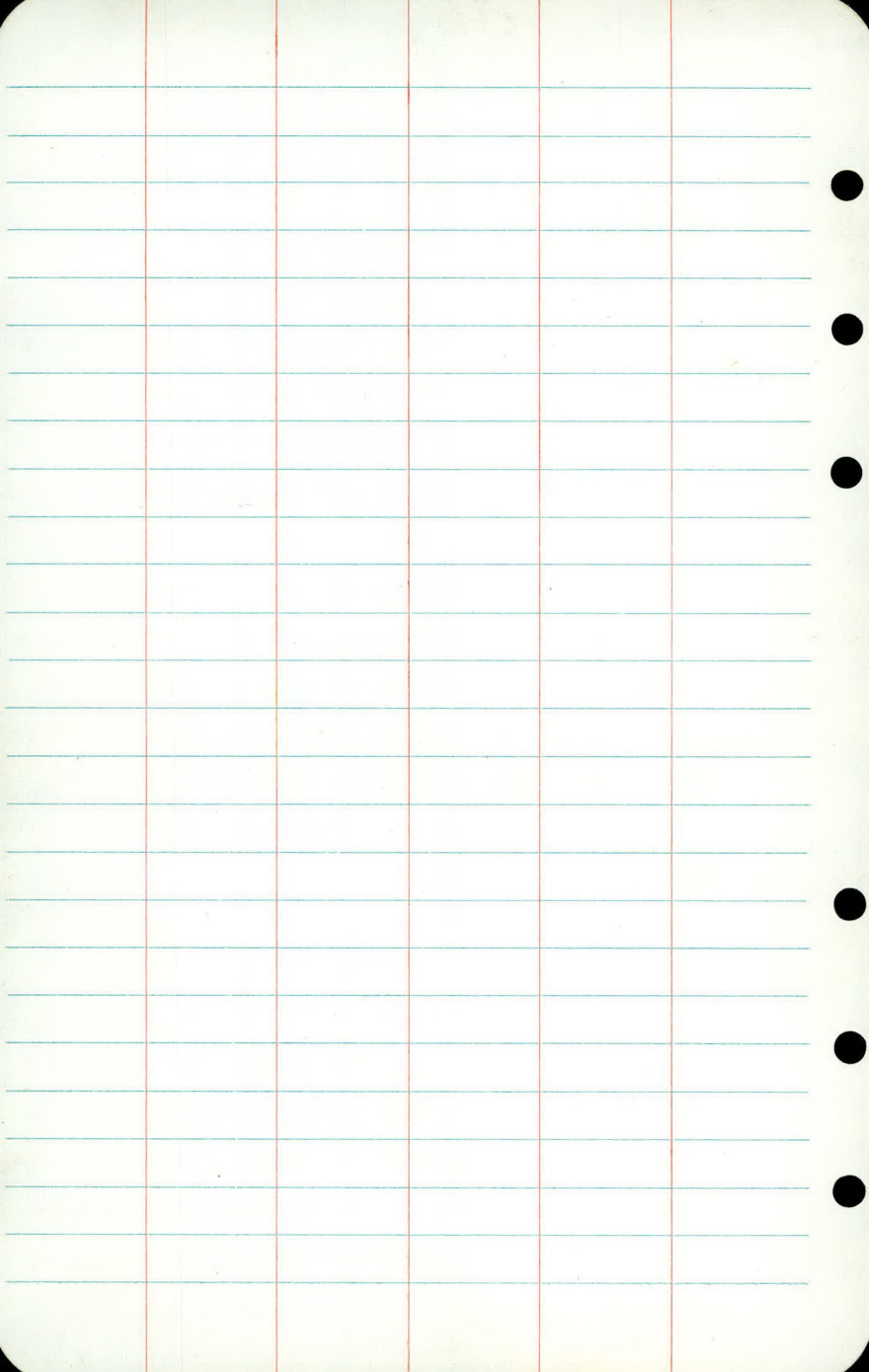
SD 31 MAR 1971
CB 7 + 07 23' RT

FL TO TOP = 3.7

9" CASTING

BRICK





31 MAR

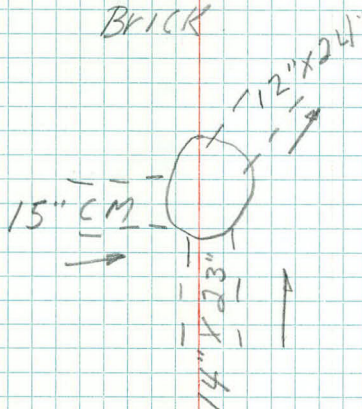
SD 7+07 34' RT

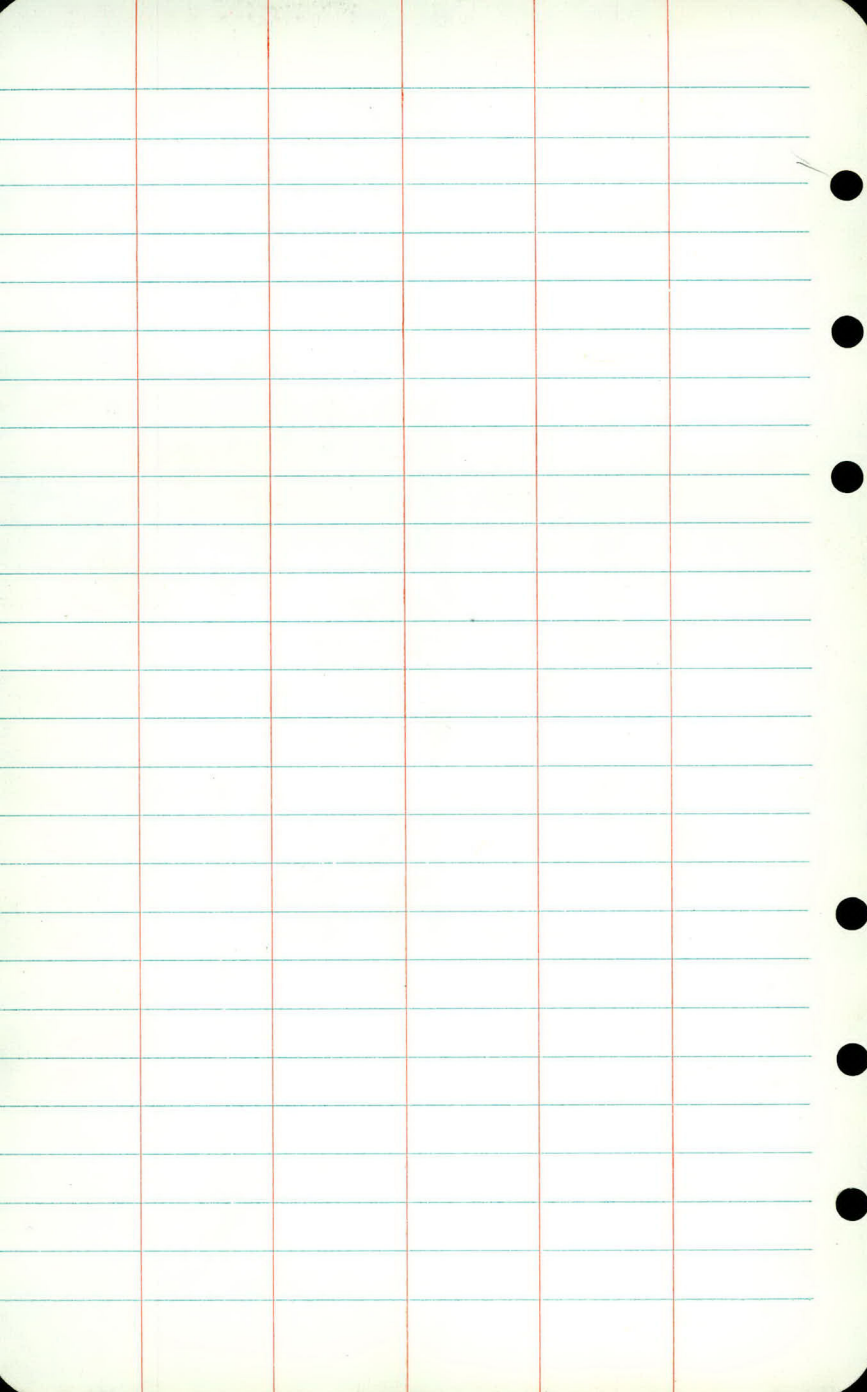
FL TO TOP 3.5

11" CASTING

BRICK

A
N





ELEV.

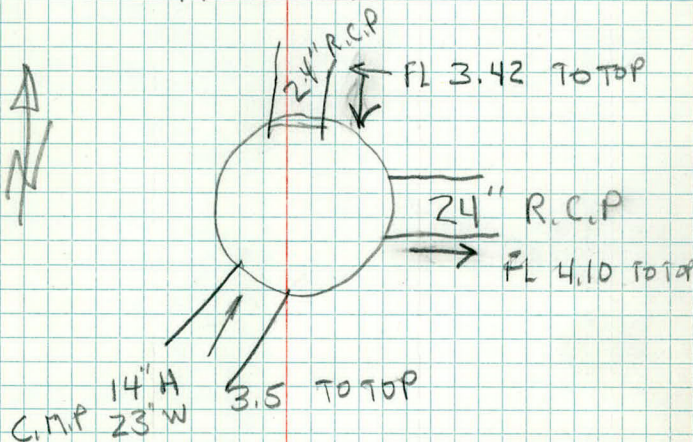
~~927.21~~ 932.88

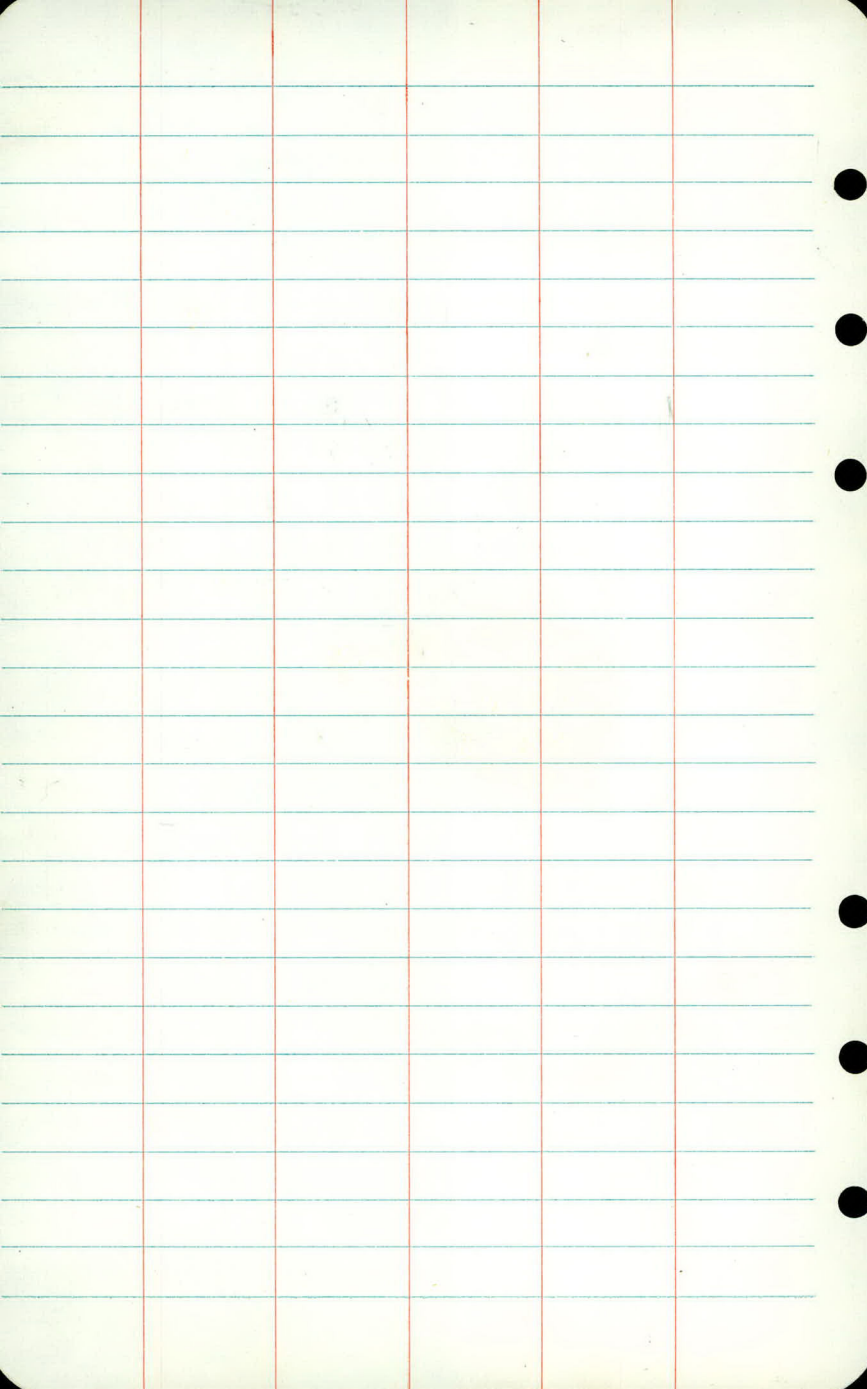
M/H 7+12 36' RT

FL TO TOP = 35

11" CASTING

M.H. → BLOCKS





SD 10+72

31 MAR 1971

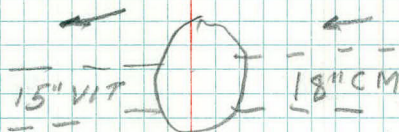
135' RT

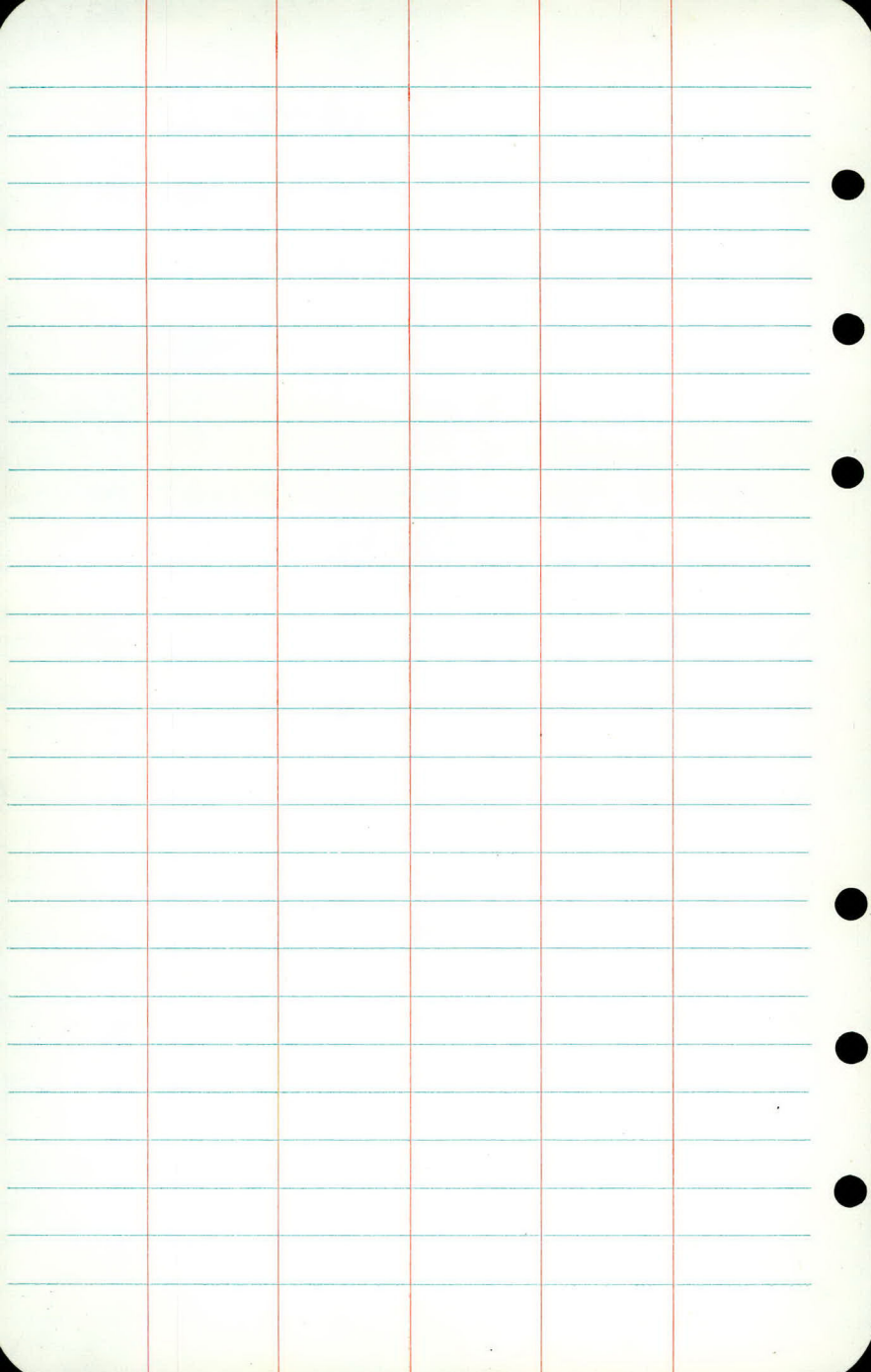
FL TO TOP = 3.5

5" CASTING

BRICK

→



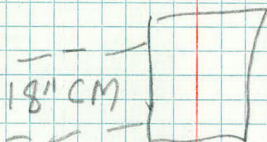


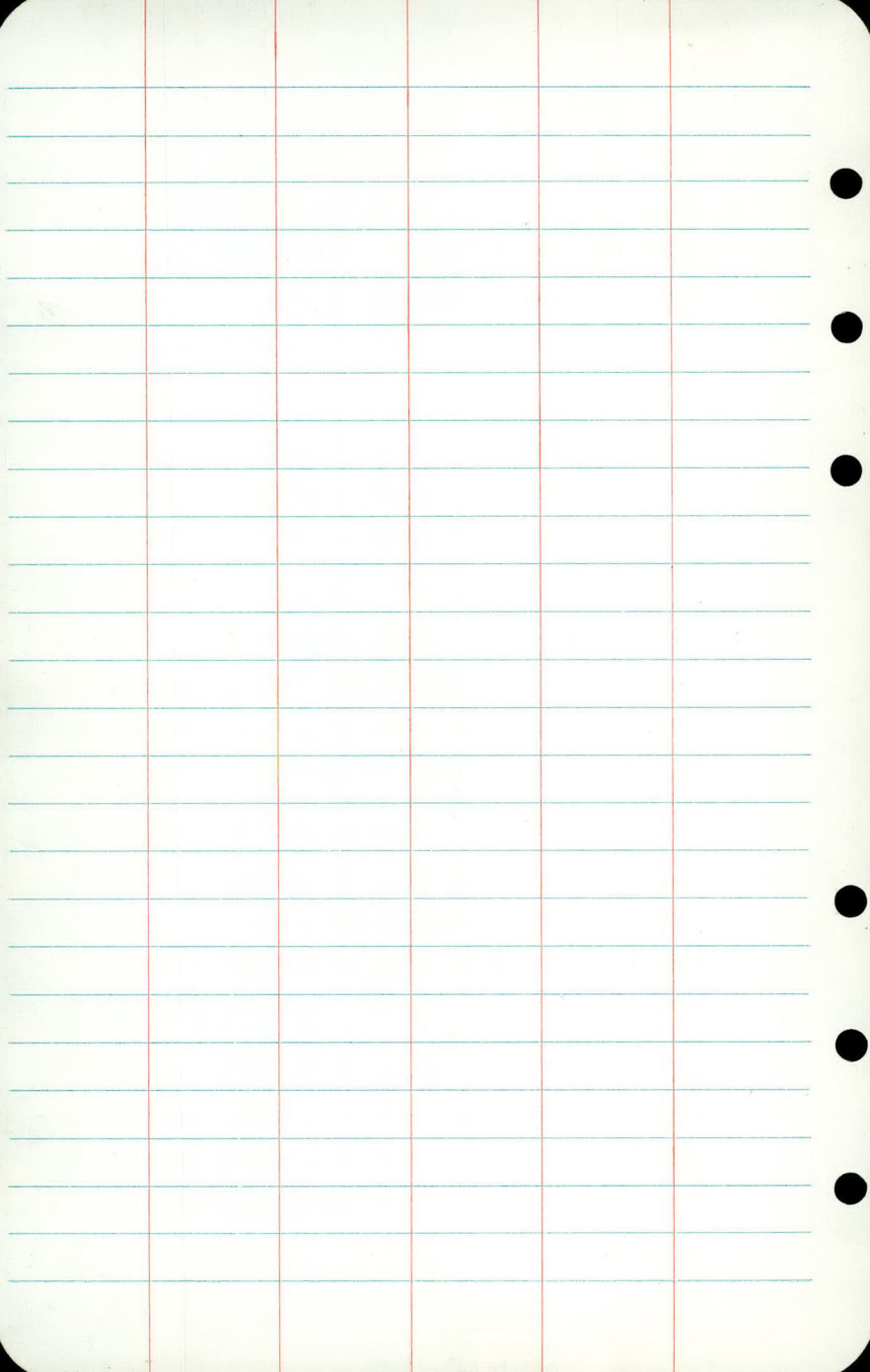
31 MAR 1971

CB 11400 137' RT

FL TO TOP = 3.2

BLOCK





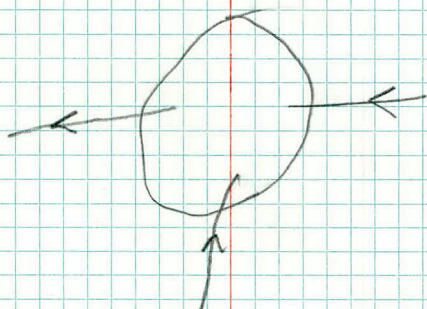
31 MAR 1971

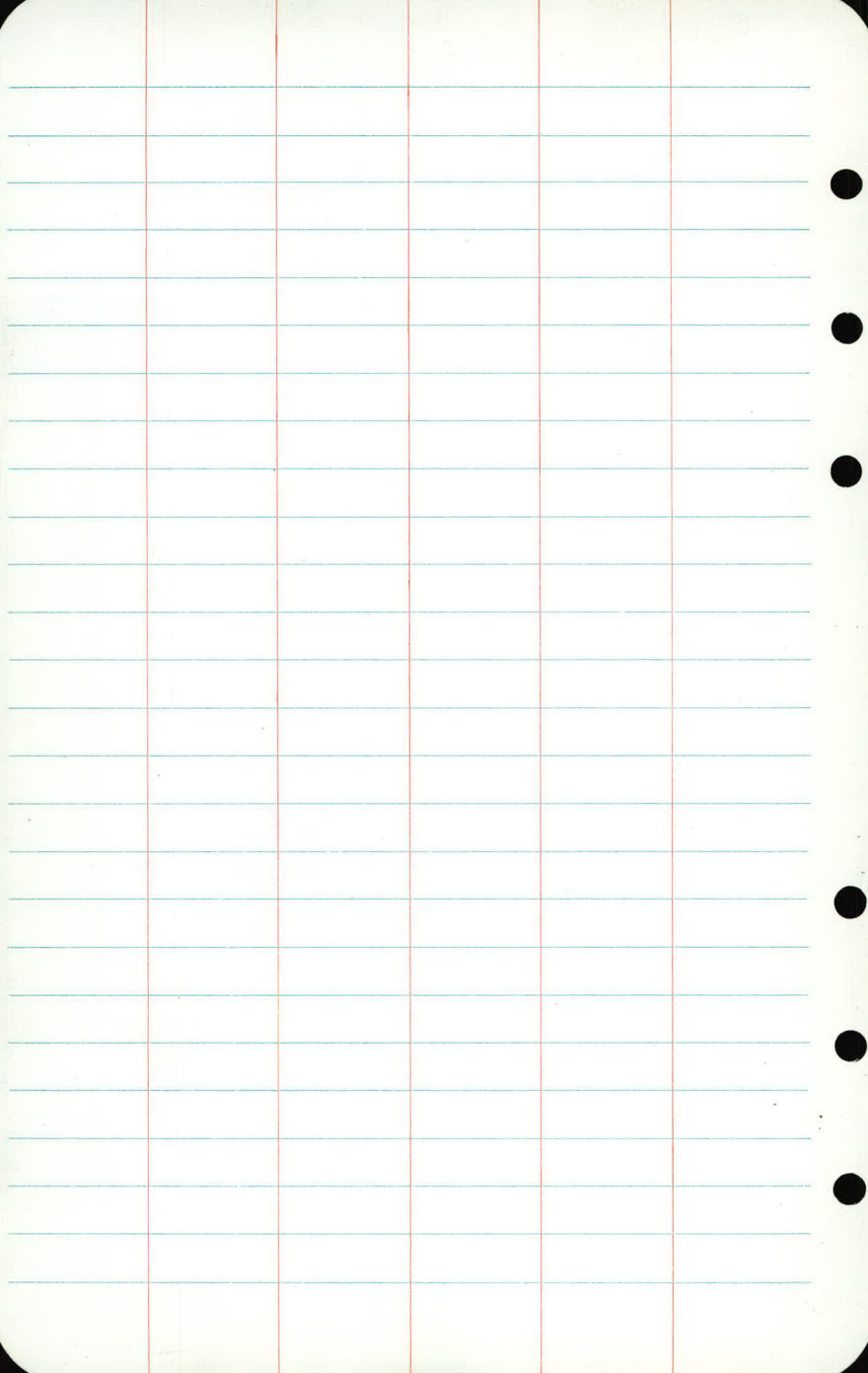
MH 10493 48' RT
Sanitary

FL TO TOP = 14.9
13" CASTING
3 rings

4.5' section
2.0' section
3.5' Con. Cone

Z →





ELEV. 937.41

31 MAR 1971

MH 11+03

47' LT

Sanitary

→ Z →

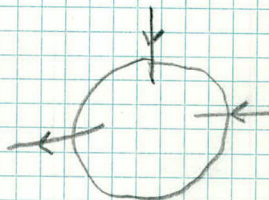
FL TO TOP = 10.85

3.5 Section

4.0 Cone

8 rings

12" Casting



BM = 939.47

MAGNOVOX S.E. Con

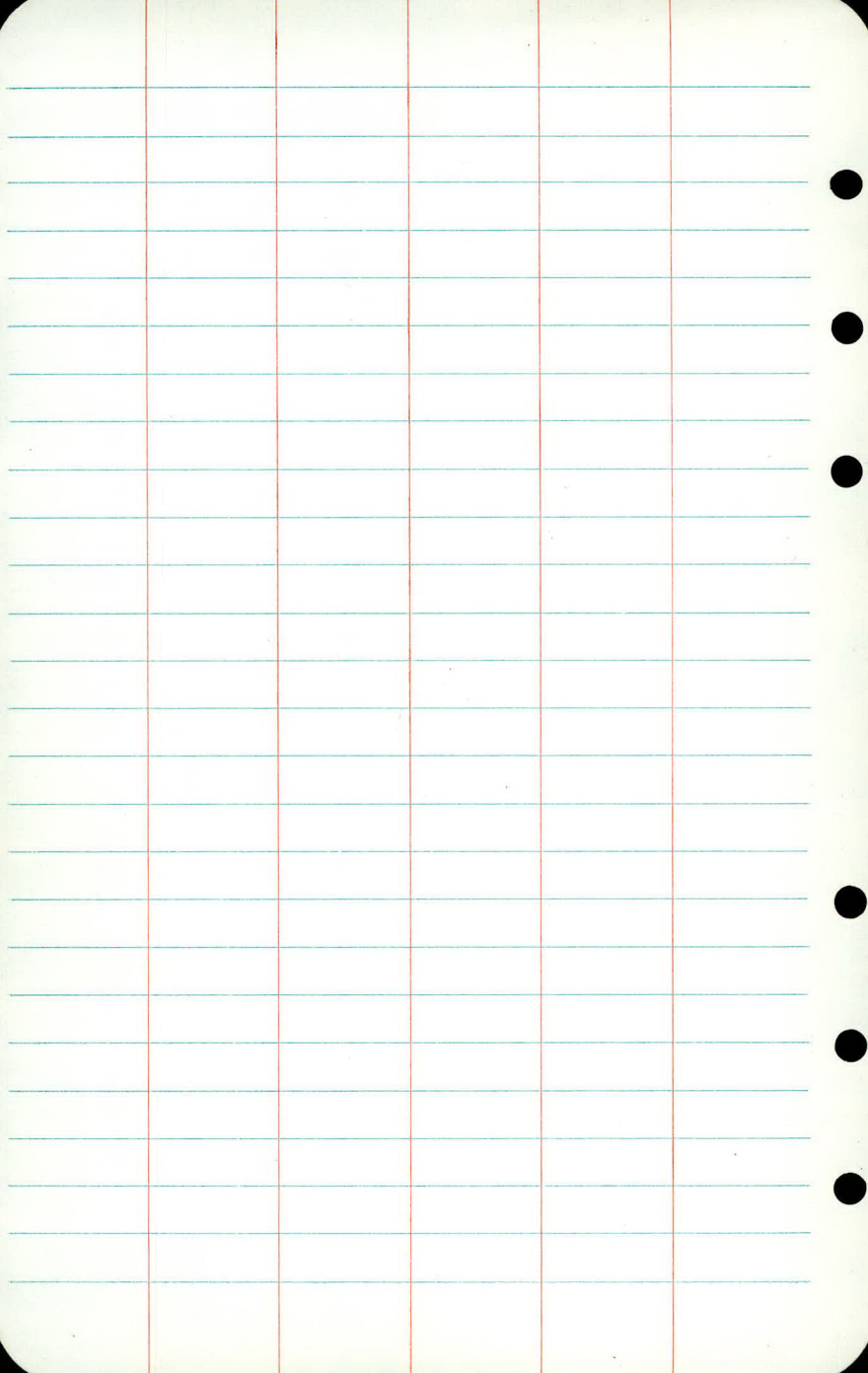
3.85

943.32
3.82

939.50

943.32
5.91

937.41

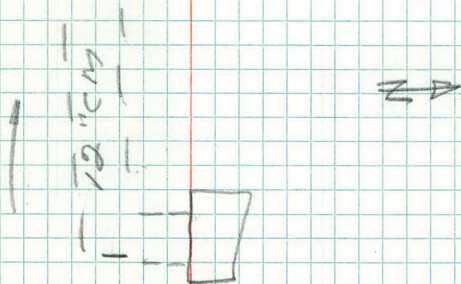


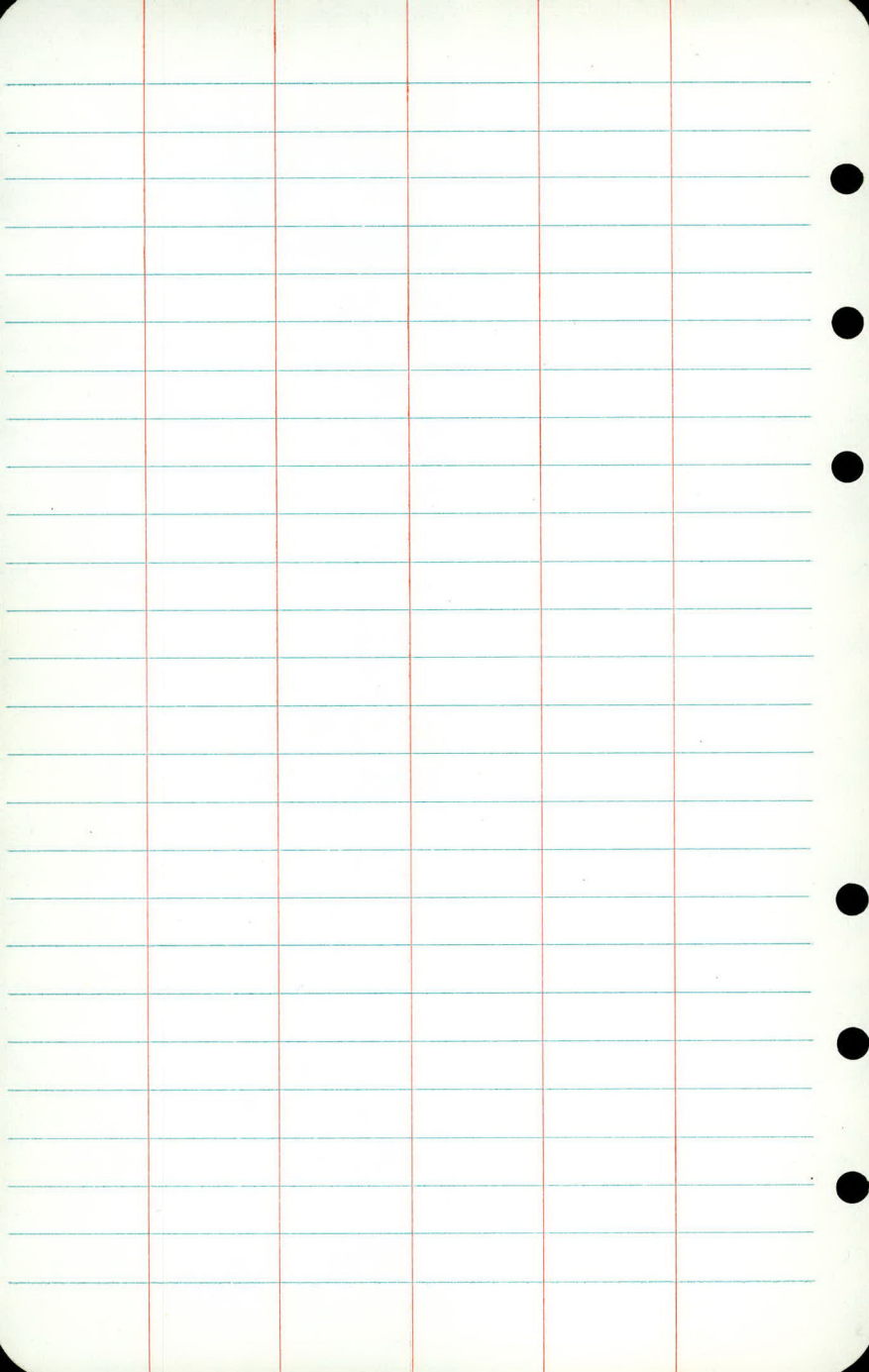
CB 11+17 24'RT

BRICK

FL TO TOP = 2.2

9" casting





31 MAR 1971

ELEV. 939.50 / MH 12+30 47' LT

FL TO TOP = 9.90

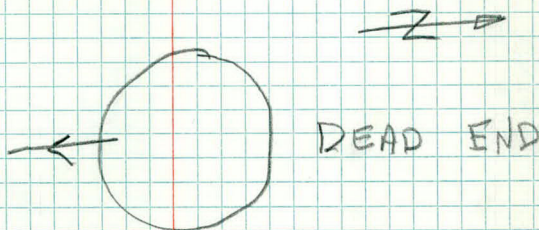
3 rings

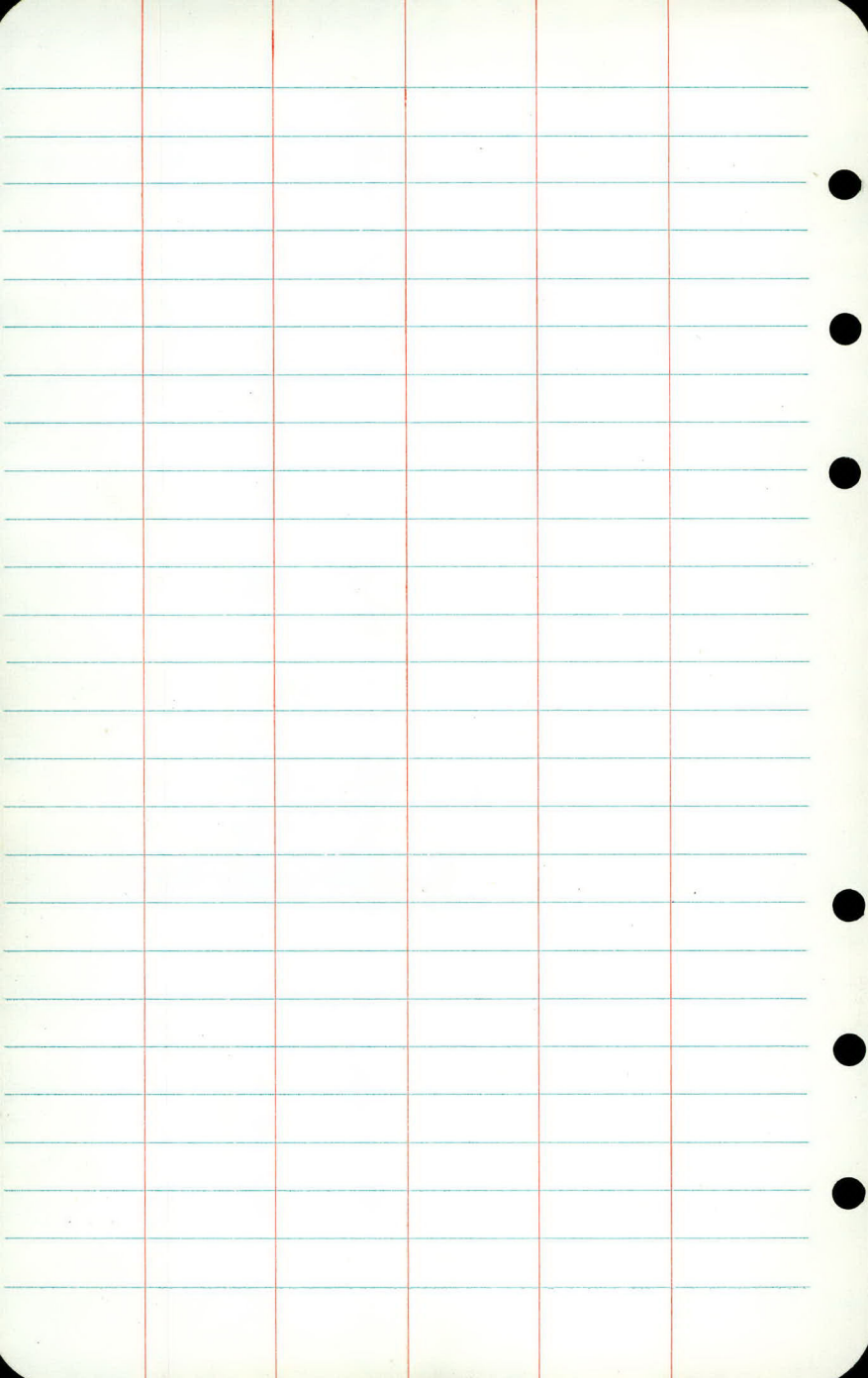
12" CASTING

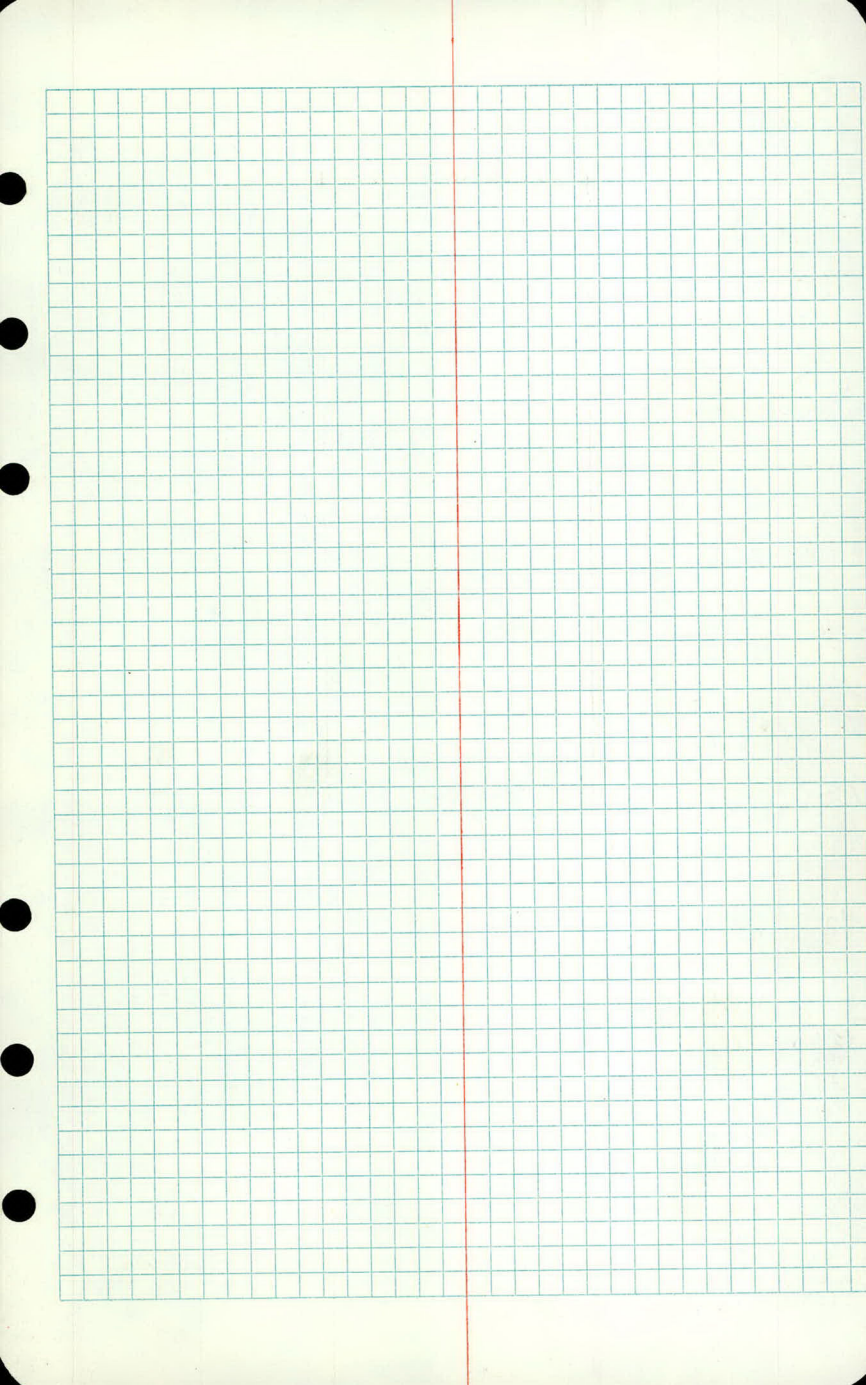
2' Section

1' Section

4.5' Con Cone







16+00

+50

15

+50

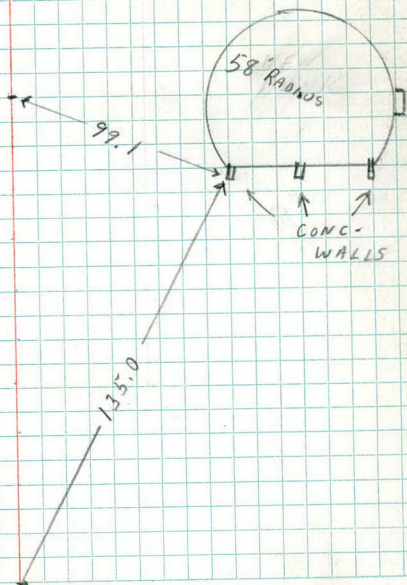
14+00

GA
DS
DK

APR 3, 1971

£

CENTER OF BANK IS
110' FROM LEX. PROP. LINE
AND 89' FROM RUGGLES
PROPERTY LINE



2

54+00

+04

N.E. COR BURGER CHEF

79.5

+54

S.E. COR BURGER CHEF

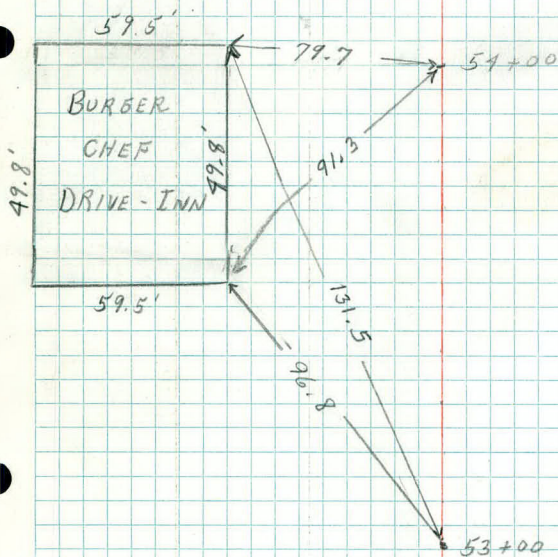
79.5

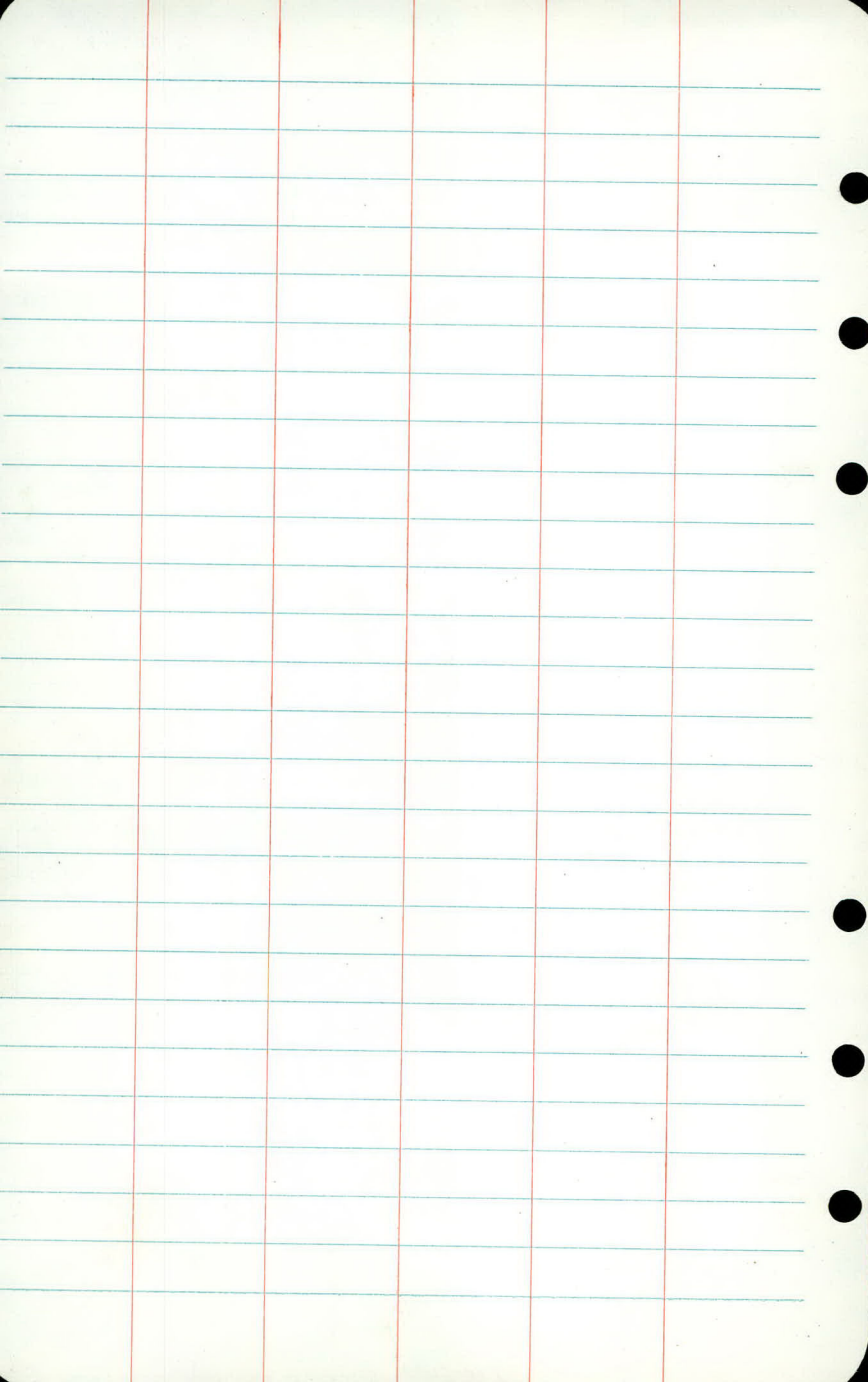
53+00

GA
DS
DK

Apr 5, 1971
SUNNY 60°

E





8 APRIL 1971
Sunny 60°

BURGER CHEF

51 TURNBACK

+37 END 5' WK.

+33 END PR LOT ✓

⁵⁸
+03 & 26' DR ✓

53+00

+50

+38 & DR.

+08 ✓ COR. PR LOT

⁵⁸
+03 SIDE WK 5'

54+00 N.E. COR BLK.
⁵⁰
80

✓ SIDE WK 5'
+53 50-75

+50

✓ PR LOT

S.E. COR BLK
80 +48 ⁵⁸ SIDE WK 5'
+48 50-80

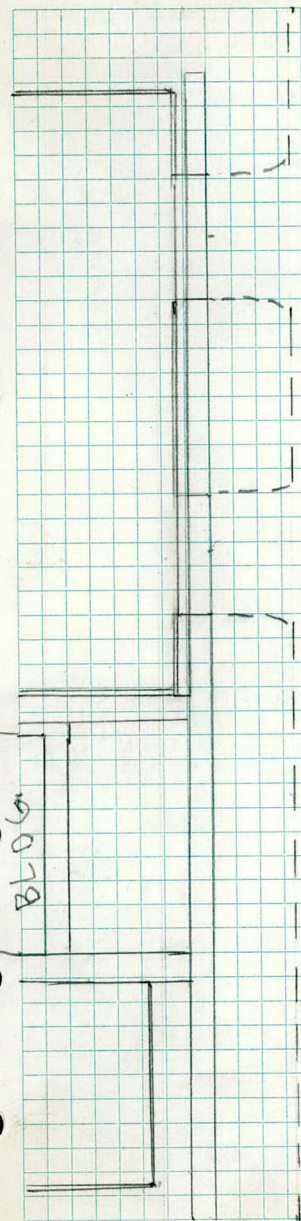
✓
+07 COR RH LOT
58

53+00

2

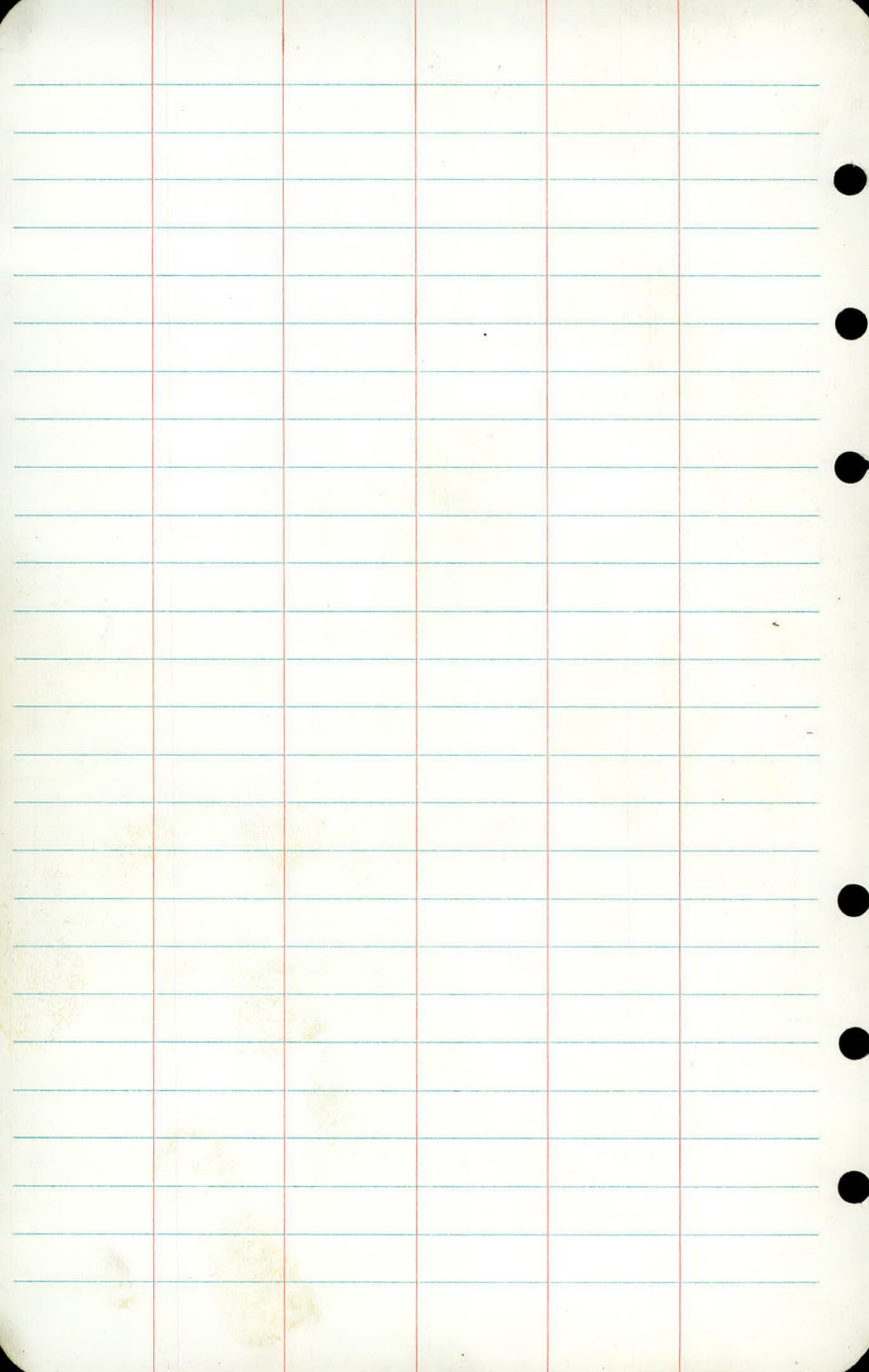
LT

8 APRIL 1971
RT



BLOG

2



5 APRIL 1911
SUNNY 46°

1

LEXINGTON AVE.

51 TURNBACK

TOPOGRAPHY

31

55

✓ 111
105 / 10

Ms.

2

+ 89 CB

60

1

1

End 12" CM

4254.6

CH 10

0.131

27	✓
4/19	5 0

48

411 FF

50 - was y

 $64 + 00$

Med

2

POR

5D

37

42

+75 FE

48-EAST

475POR

27

+50

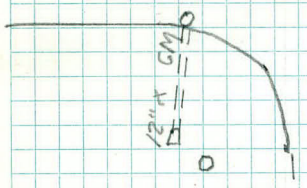
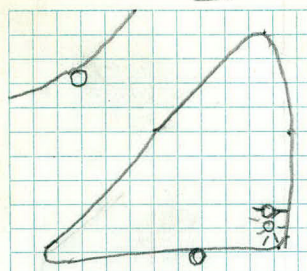
3+00

5 APRIL 1971 2,

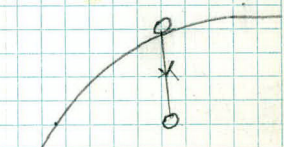
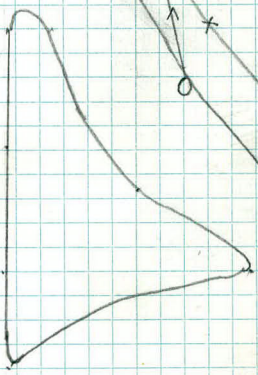
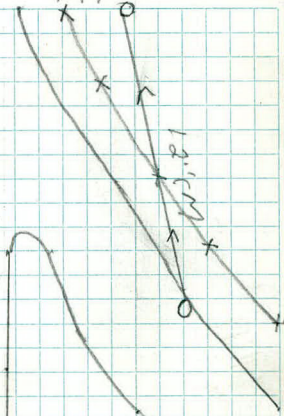
LT

E

Rt



7 pines
x x x x x
x x x x x
x x x x x



x x x x x

68+00

£

+50

67+00

+80 Curb	+80 End Fe	+80 Bridge	+80 Begin Bridge
27	35	28	28
			+78 End Fe
			36
			464 CB
			26

+50

+40 PP
31

Curb	FE
27	38

+30 FE
39

+30 ER
27

+32 LP
37

66+00

✓
FE
45

✓
Curb
31

✓
Med
2

✓
Med
2

✓
Curb
27

✓
FE
42

✓
+89 SD
58

✓
+89 Fe
50

+89 Curb
35

✓
+76 ER
27

65+50

✓
Fe
41

✓
Curb
59

✓
PBR
31

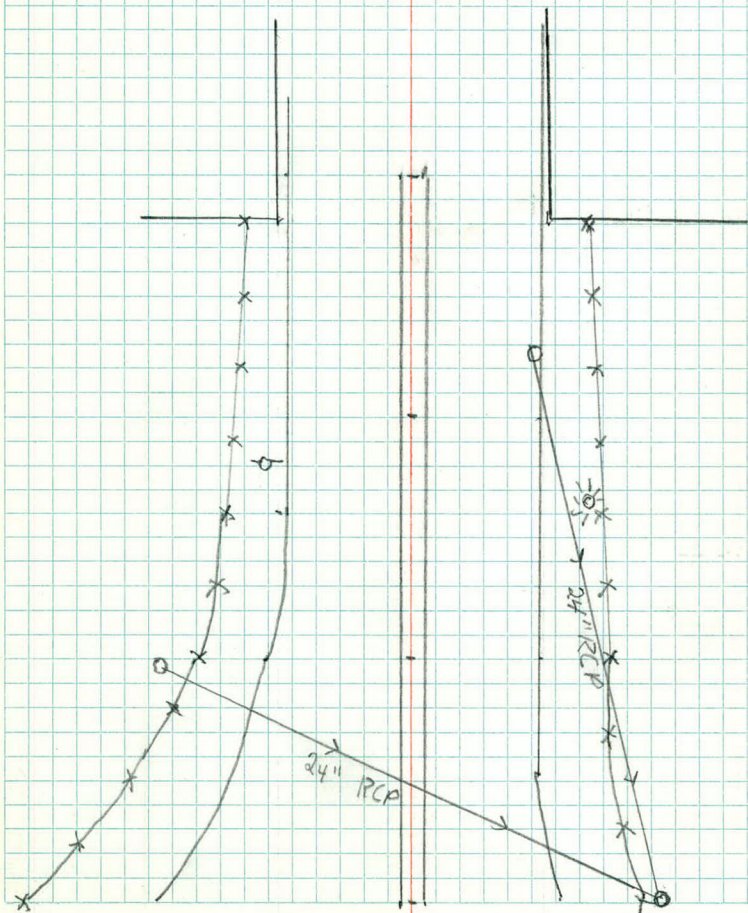
✓
Fe
47

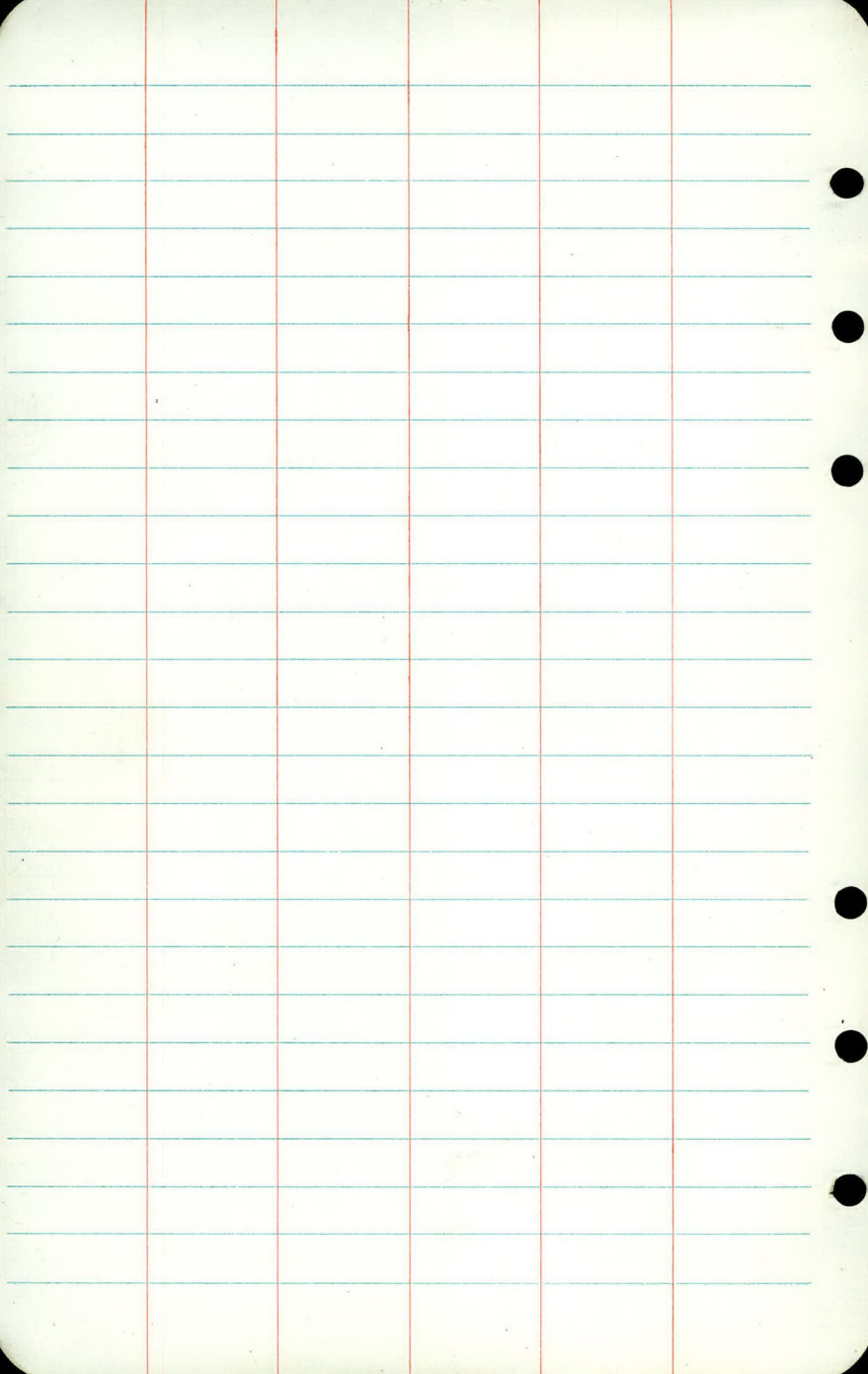
✓
SD
52

LT

5 APRIL 1971 3.

RT





FK
LPD
DK

April 29, 1971

Lexington Ave. 51CTB

at "B"

WALL

6.00
3.73
4.27
4.48
2.20

A Pillars
152.0 L.F. Wall
162.0 L.F. Footing

2.09' 2.08'

0.30

2.70
1.95 x 1.95

Cap
1.68

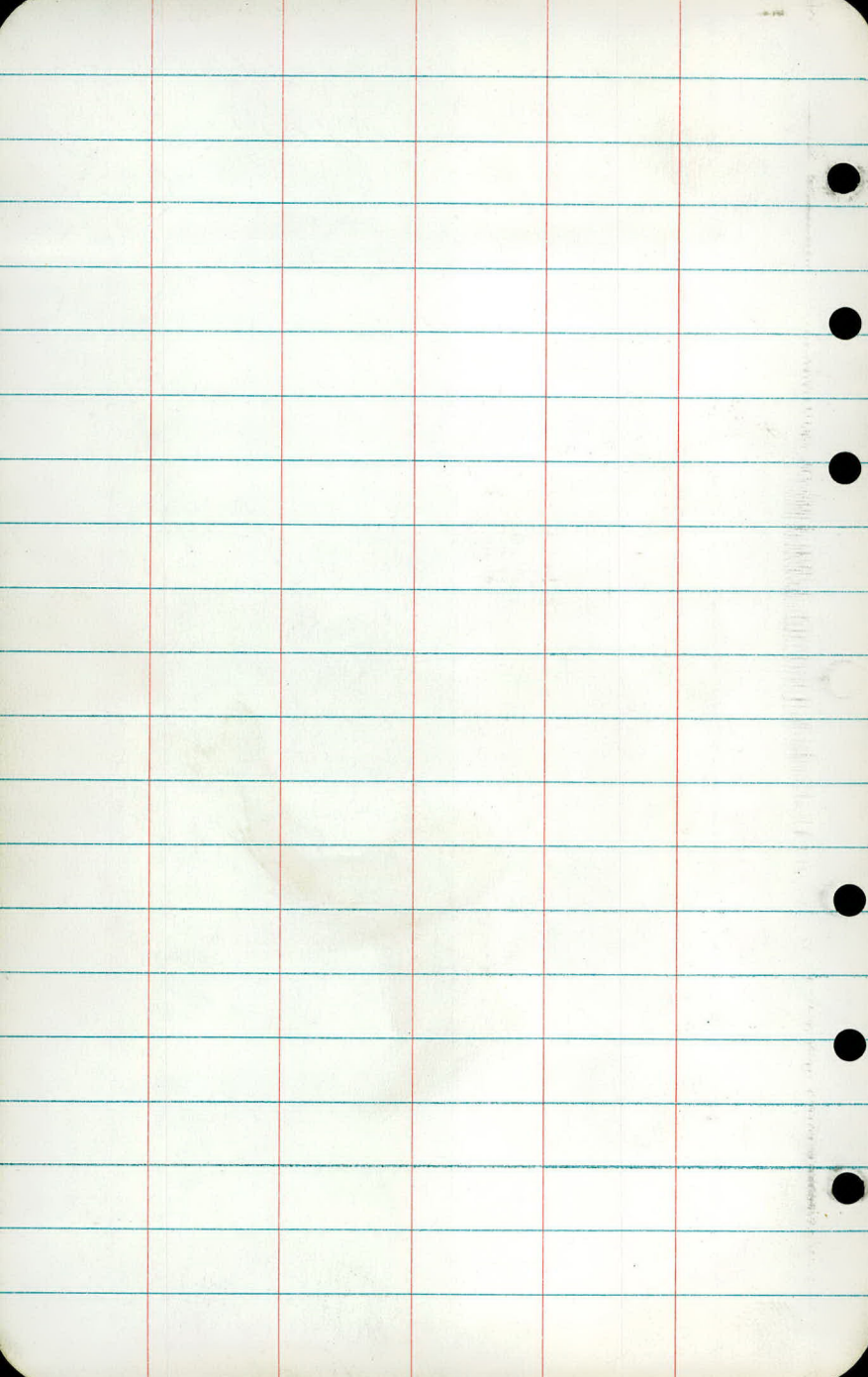
Cap
29.4 + 122.6 = 152.0
2.27

Footing = Wall width + 8" x 8" thick

1.55 + 0.67 x 0.67 =
length x 2.22 x 0.67 =

0.30

1.55
width
Wall



ML
CM
RC
MR

OCT 23, 79
PARTLY CLOUDY 45°

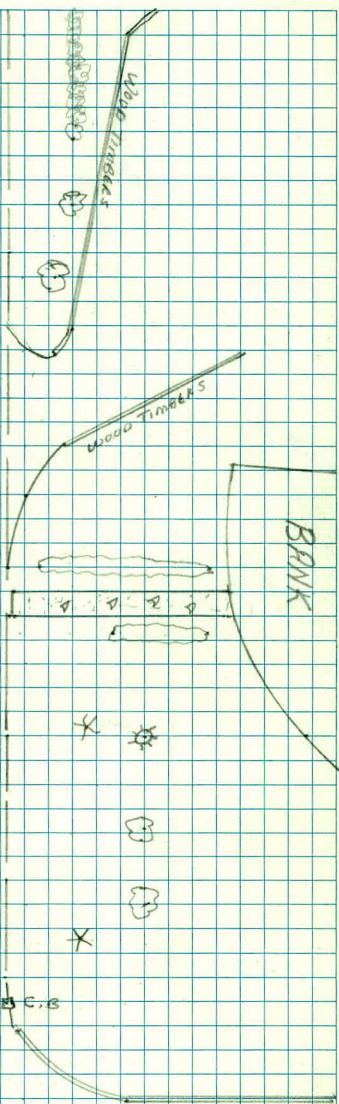
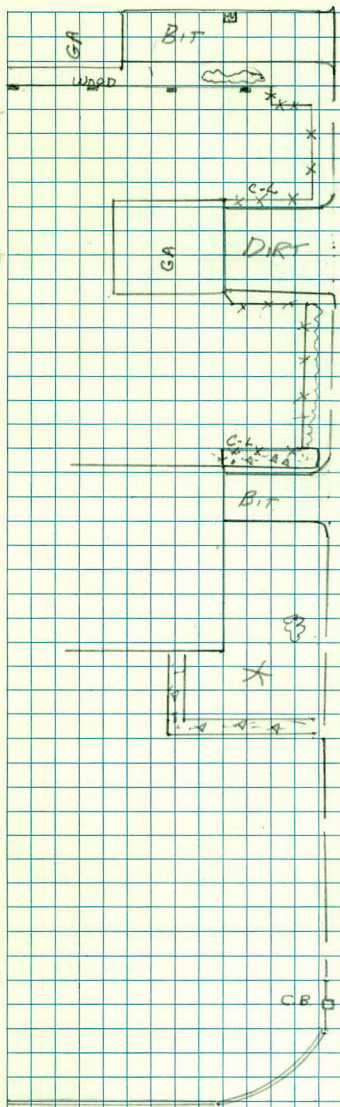
TOPOGRAPHY
RUGGLES ST

48 S.W.	45 E DR (BIT) 12'		
38	37 SW COR GAR		
35 FE (WOOD)	36 ROW SCHRUBS		
30	32-44		
32 COR FE	18 PD	44 COR DR	
30	22-30	42	
12 COR FE	12 SE COR GAR		
22-40	40	10 BUSH	24 BEG SCHRUBS
	102 E DR (BIT)	30	
2+00	17	100 BIT	100 DR
	93 SW COR GARAGE	17	34
90 COR FE	40		95 36 EL 19
23-38	90 END BUSH		26
	22	24 BR	17
60 COR FE	60 BEG BUSH	30	
24-40	23	79 POR	79 BEG WOOD CURB
56 BEG FE	50 3' S.W.	26	
40	20-40	60 POR	60 BEG WOOD CURB
	40	27	27
50	50 E BIT 10'	57 COR	50 POR
		63	20
		35	41
	22 8" BIRCH	35 ROW SCHRUBS	30 S.W.
	24	23-37	18-63
18 SW COR NO	14 12" PINE	27 M.H.	25 S.W.
40	33		18-63
	103 S.W.		22 ROW SCHRUBS
	21-51		38-59
1+00	101 S.W.	100 FLOOD	100 2" PINE
	21-51	45	33
	100 BIT	100 BIT	100 BANK
	19	16	79
			81 14" ELM
			45
			65 14" ELM
			45
		57 2" PINE	
		31	
50	50 BIT	50 BIT	
	18	16	
	49 ER	49 ER	
	18	16	
45 C.B.		44 C.B.	
17		16	
END			
38 CURB		38 END C+G	
17		17	
0+00	24 BR	24 BR	
	41	41	

Lt

E

Rt



LEXINGTON

STA

LT

E

RT

3+00

+05 SE COR NO #1045

67

815

BIT

+30 NE COR NO #1072

70

+99 TRI. BIRCH

47

18

16

+94 NW COR NO #1072

70

+72 S.W.

58

+72 SW COR NO #1045

67

+84 ROW PINES(?)

31-75

+60 SE COR GAR.

+64 2" PINE

53

+70 4" PINE

32

+55 SW

25-38

+63 BUSH

25

+61 END SCRUBS

29

+53 2 1/2" ELM

26

2+50

+54 ROW SCRUBS

25-38

#1072

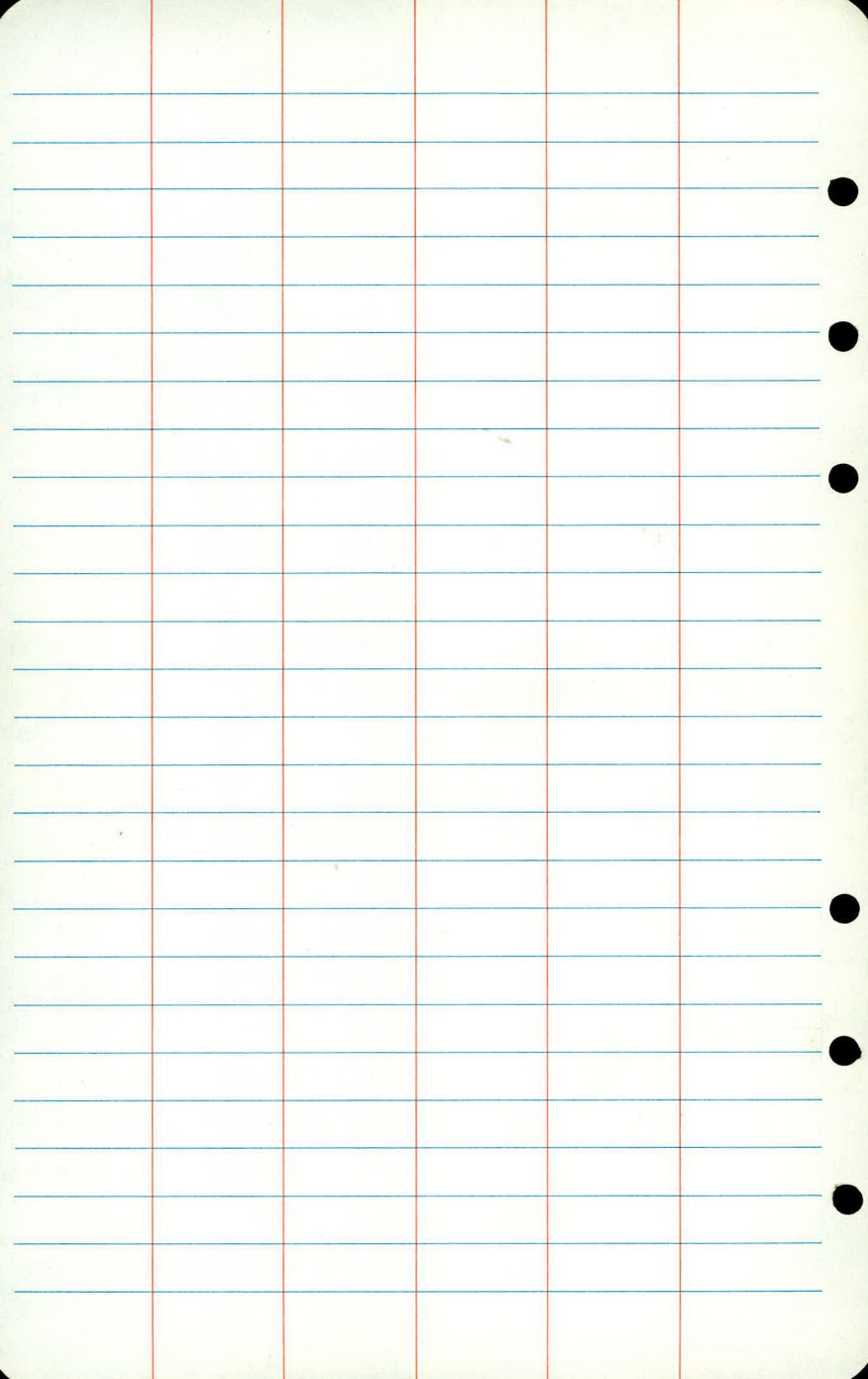
* * * * *

*
G

G

#1045

GA



ML
CM
RE
MR

Oct 18, 79
Cloudy 48° 1

X SECTION

RUGGLES AVE

0+00 = 16+56 E LEXINGTON AVE

STA

950.65

0+24

0+44

CATCH BASIN LT + RT

0+50

0+75

1+00

+25

KENNER ROD

LT

E

RT

2

Top 140 NW Cor RUGGLES & LEXINGTON

46.88 47.06 47.42
42 42
BR BR

48.36 48.66 48.34
17 17
C.B. C.B.

49.9 48.9 48.85 49.18 49.07 49.2 52.3 BS.
27 27 16 17 19 42.3
GUTTER GUTTER 36

51.8 50.3 50.09 50.77 50.29 50.5 51.2
30 18 16 17 18 36
GUTTER GUTTER

51.60 51.5 51.22 52.01 51.37 51.5 53.1
20 19 18 17 19 35
CONC GUTTER GUTTER
S.W.

53.4 52.3 52.10 52.86 52.31 52.43 52.95
25 19 17 17 19 34
GUTTER GUTTER CONC
S.W. S.W.

STA

1+27

M.4. £

52.85

+50

£ ENT LT (BROKEN CONC)

+69

£ DRIVE (BIT) RT

+75

2+00

£ DRIVE (DIRT) LT

+25

LENKER ROD

LT

4

RT

3

53.67	52.86	53.36	53.00	52.90	53.6
39	17		17	22	36
GARAGE	GUTTER		GUTTER		
SLRB					

53.71	53.30	53.30	53.62
	18	32	50

53.39	53.83	53.39	53.40
15	17	33	
GUTTER	GUTTER	BIT	

54.40	53.51	54.26	53.90	54.0	53.73
37	17		17	20	43
SLRB	GUTTER		GUTTER		BIT
					DR

54.3	53.75	54.36	53.90	54.13	53.82
21	17		18	20	40
C.L.	GUTTER		GUTTER		BIT
FEN					DR

4.26

STA

2+42 R DRIVE (BIT) LT

+50

3+00

+50

4+00

+50

LT

2

RT

4

54.46	54.19	53.90	54.33	53.89	54.00	54.00
60	19	17		16	19	30
CONC		GUTTER		GUTTER		
SLAB						

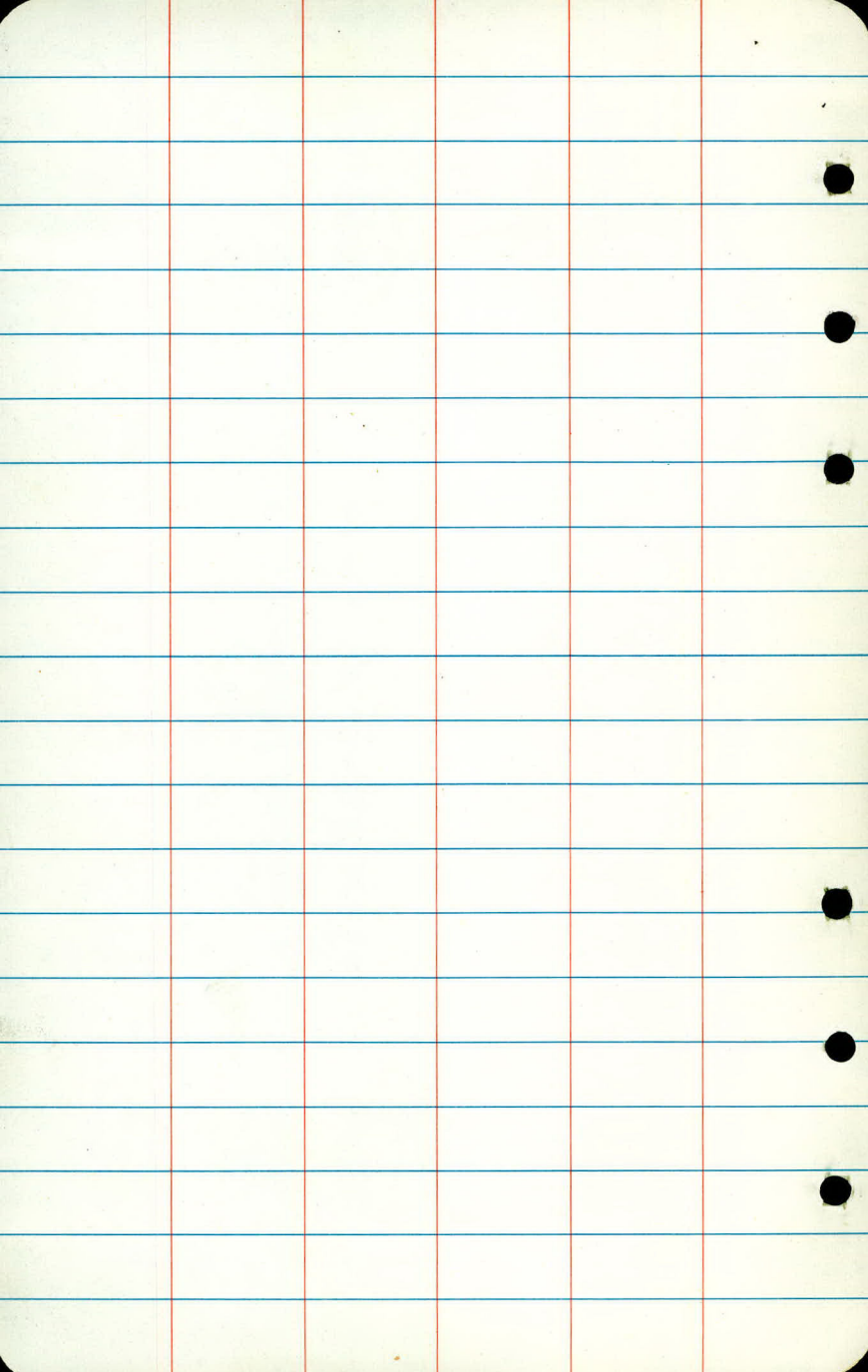
54.35

54.39

54.56

54.36

54.22



STRUCTURAL DATA TYPE

STORM	ELECTRIC	WATER	
SANITARY ☒	TELEPHONE	OTHER	
STATION	LEFT	RIGHT	SIZE
1+27	£		11" INCH CASTING

TYPE OF CONST.	COMMENTS
BLOCK	ECCEN.
BRICK	
SECTIONAL ☒	

ADJUSTING RINGS	TYPE	NO.	DEPTH	COMMENTS
BLOCK				
BRICK				
CONC. RINGS	3			

DEPTH FROM BOTTOM OF M.H. TO TOP OF CASTING DISTANCE FROM HIGHEST FLOW LINE TO TOP OF CASTING ETC. INV.	<table border="1" style="width: 100%; border-collapse: collapse;"> <tr> <td style="width: 40%; text-align: center;">9.08</td> <td style="width: 60%;">ELEV.</td> </tr> <tr> <td style="text-align: center;">8.60</td> <td></td> </tr> <tr><td> </td><td> </td></tr> <tr><td> </td><td> </td></tr> <tr><td> </td><td> </td></tr> <tr><td> </td><td> </td></tr> </table> 4' 2 1/2'	9.08	ELEV.	8.60									
9.08	ELEV.												
8.60													
SIZES OF ALL PIPES AND DIRECTION OF FLOW													
DESIGN ELEVATION - TOP FINAL ELEVATION DIFFERENCES ADJUST RECONSTRUCT	<table border="1" style="width: 100%; border-collapse: collapse;"> <tr> <td style="width: 40%; text-align: center;">952.85</td> <td style="width: 60%;"></td> </tr> <tr><td> </td><td> </td></tr> <tr><td> </td><td> </td></tr> </table>	952.85											
952.85													

KP
DS
WS

23 MAR 1971
Sunny 20°

LEXINGTON AVE.

Larpenteur Ave to S.T.H. #36

Bench Levels

STA + π - ELEV.

BM 4.80 945.81 941.00

BM 1.17 946.53 0.45 945.36

BM 4.99 946.49 4.99 941.54 941.50

2.15 941.37 7.27 939.22

3.81 937.56

TP 5.73 941.64 5.46 935.91

10.13 949.52 2.25 939.39

8.14 956.77 0.89 948.63

1.72 952.29 6.20 950.57

2.85 947.91 7.23 945.06

2.75 948.53 2.13 945.78

BM 1.17 947.36 947.42

BM 4.81 945.82 941.01

BM 0.44 945.38

BM 2.92 944.48 4.26 941.56

BM 2.13 939.79 6.82 937.66

BM 5.51 941.52 3.78 936.01

BM 2.05 939.47

23 MAR 1971

DESCRIPTION

TOP HYDRANT SW COR LARP. & OXFORD

TOP HYDRANT S.E. COR LARP & LEX.

ROSEVILLE BENCH N.E. COR LARP & LEX.

S.E. COR. Lite Pedestal (Garden Center)

TOP HYDRANT ACROSS FROM DAIRY QUEEN

TOP HYDRANT N.E. COR DIONE

S.E. COR. LOWER STEP MAGNA VOX

TOP HYDRANT NW COR GARDEN

TOP HYDRANT N.W. COR RUGGLES

TOP HYDRANT NW COR SUMMER

TOP HYDRANT N.W. COR AUTUMN

TOP HYDRANT N.E. COR ROSELAWN AVE.

Top Hyd S.W. Corner Larpenteur & Oxford

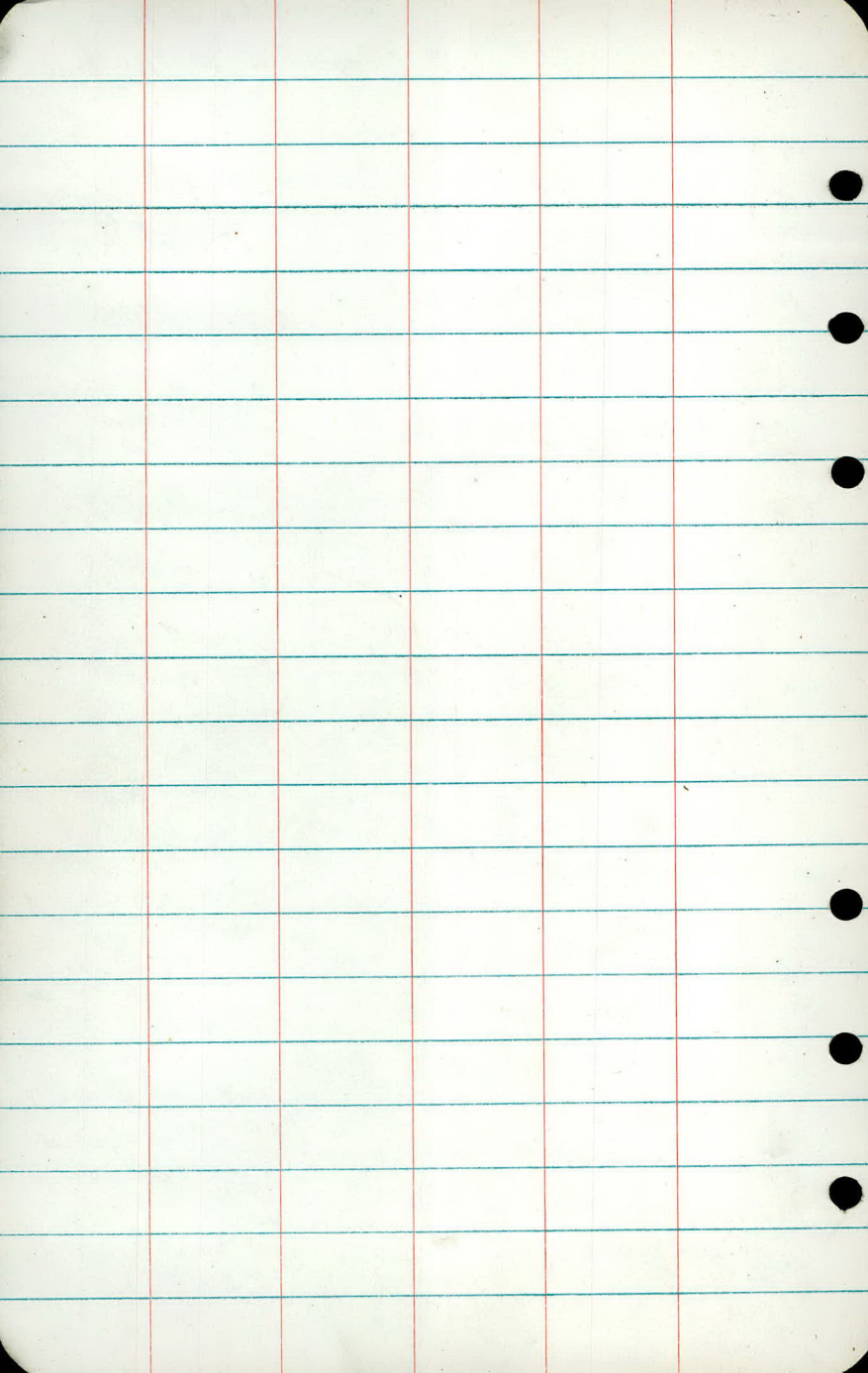
Top Hyd SE Corner Larpenteur & Lexington

Roseville B.M. NE Corner Larpenteur & Lex.

Top Hyd across from Dairy Queen

Top Hyd NE Corner Dionne St & Lex

Top S.E. Corner Walk



PA
WS
GA
DS

March 25, 1971
Cloudy 18°

X-1

X-Sections

Sta + π - Elev.

BM 1.22 946.58

(945.36)

0+00 ϕ Larpenieur

✓

0+26 Edge Traveled Lanes

✓

+35 Gutter East & West

✓

March 25, 1971

Lt

E

Rt

X-2

Top Hyd S.E. Corner Lexington & Carpenter

41.22	41.48	41.17	41.39	41.19	41.48	41.26
5.36	5.10	5.41	5.19	5.41	5.10	5.32
50	34	25		25	34	50

40.81	40.36	40.81	40.86	41.03
5.77	6.22	5.77	5.72	5.55
25	100	100	82	70

40.13	40.44	40.82	41.07	41.25	41.10	40.76	40.53
6.45	6.14	5.76	5.51	5.33	5.48	5.82	6.05
80	60	40	20		21	40	60

39.75	40.22	40.40
6.83	6.36	6.18
100	100	80

40.33	40.69	41.00	41.21	40.95	40.61	40.44
6.25	5.90	5.58	5.37	5.63	5.97	6.14
60	40	20		20	38	59

39.97	39.61	40.04	40.24
6.61	6.97	6.54	6.34
80	100	100	79

Sta + x

946.58

0+46 N R-W Line Larp

✓

1+00

✓

TP 3.07 944.58 5.07 941.51 Rock

+45

✓

£ March 25, 1971

41.37

40.86

40.93

41.18

40.82

40.76

X-3

41.20

5.21

5.72

5.65

5.40

5.76

5.87

5.38

24

24

20

20

26

27

C

G

G

C

41.57

41.62

41.17

41.2

41.4

5.01

4.96

5.41

5.4

5.2

37

43

60

60

47

Conc

41.37

41.46

41.26

40.74

41.23

40.64

41.14

41.1

5.21

5.12

5.32

5.84

5.35

5.94

5.44

5.5

47

33

C

G

G

C

34

23

23

41.34

41.80

40.7

40.9

5.24

Par. P/L

4.78

5.9

5.7

53

53

60

42

41.04

41.25

40.93

40.39

40.91

40.33

40.8

40.4

3.54

3.33

3.65

4.19

3.67

4.25

3.8

4.2

54

33

C

G

G

35

60

Conc

23

23

40.93

3.65

60

Sta + π - Elev

944.58

2 in Ent Lt

S TTC₀

+32 MH 16' Rt 4.93 939.65

3

+43 2 Ent Lt

4

5

BM 1.80 939.44 6.94 937.64

937.56

+28

2

x4

37.5	38.4	38.8	39.30	39.77	40.43	39.84	40.28	40.3	40.0
71 62 58	5 28	4 81	4 15	4 74	4 30	4 34	60		
85 60 48	33	23		G	C	34	60		
						23			

37.4	37.7	38.2	39.03	38.52	39.08	38.59	39.09	39.1	39.0
72 6.9 6.4	5.55	6.06	5.50	5.99	5.49	5.5	5.6		
60 50 37	C	G		G	C	35	60		
		23			23				

36.7	37.1	37.6	37.76	38.39	37.92	38.5	38.6	38.4
7.9	7.5	7.0	6.82	6.19	6.66	6.1	6.0	6.2
100 75	50	23			G	C	34	60
							23	

37.10	37.00	37.06	37.06	36.68	37.22	36.66	37.2	37.2	37.2
748 758 752	752	790	7.36	7.92	7.4	7.4	7.4		
60 54 35	C	G		G	C	33	60		
		24				23			

35.04	35.28	35.14	34.64	35.26	34.56	34.7	35.8	35.8
954 9.30 9.44	9.94	9.32	10.02	9.9	9.2	8.8		
60 49	C	G	G	33	47	60		
Top Hand Lt.		24		24				

34.9	34.8	34.6	34.1	34.8	34.2	34.7	33.83	34.8
4.5	4.6	4.8	5.3	4.6	5.2	4.7	5.6	4.6
60 47	C	G		G	C	25	38	
		24			23	50		

35.6
38
60

Sta + π - Elev

939.44

5 + 88

✓

6

+44

+55 Gutter Line

+77 MH A8' Lt 4.66 934.78

+88 Gutter Line

Mar: h 25, 1971

Lt

PT X-5

34.58	33.7	34.4	34.4	33.7	34.4	33.7	33.30	34.28	34.5	35.60
486	61	51	51	57	51	57	614	516	49	384
(38	36	32	24	24		23	25	35	60	61
MH			C	G			SD			PLUG 15.

33.6
5.8
60

33.8	33.8	34.5	34.2	33.6	34.3	33.8	34.3	34.29	34.69	34.86
56	56	49	52	58	51	56	51	515	475	458
60	36	31	C	G		24	25	32	53	60
			24					Conc		

33.6	33.5	34.0	34.0	33.28	34.3	33.6	34.1	34.15	34.40
58	59	54	54	616	51	58	53	5.29	5.04
60	33	28	24	23		24	24	34	60
			CB		G	C	Conc.		

33.6	33.5	34.1	34.3	33.6	34.2	33.6	33.6	33.8	33.8	33.9
5.8	5.9	5.3	5.1	5.8	5.2	5.8	5.8	5.6	5.6	5.7
60	34	30	C	G		24	40	60	100	150
			23						33.1	33.6

34.3	33.6	34.2	34.1	33.6	34.4	33.6	33.3	33.7	33.5	33.5
51	58	52	53	58	5.0	58	6.1	6.1	5.9	5.9
60	42	30	C	G		24	42	60	100	150
			23							

32.6
6.82
SD
200

Sta	+	x	-	Elev.
-----	---	---	---	-------

939.44

7

+07	CB 23' RT	5.83	933.61
-----	-----------	------	--------

+07	SD 34' RT	6.64	932.50
-----	-----------	------	--------

8

BM

3.43 936.01

935.91

TOP Hyd

NE Gr Dionne

TD	6.83	942.49	3.78	935.66
----	------	--------	------	--------

9

36.61

3.09

39.09

5.67

33.42

6.21

27.21

+72 Gutter Line

10 +93	MH 48' RT	5.48	937.01
--------	-----------	------	--------

March 25, 1971

X-6

^{3A.5} 49	^{3A.2} 52	^{3A.2} 52	^{3A.6} 58	^{3A.5} 49	^{3A.7} 57	^{3A.3} 51	^{3A.7} 57	^{3A.3} 61	^{3A.2} 62
60	36	C	G		G	C	C	G	60
		23			23		53		

^{35.A} 40	^{35.2} 42	^{33.6} 58	^{34.1} 53	^{3A.8} 46	^{3A.1} 53	^{3A.6} 48	^{3A.5} 49	^{3A.8} 56
60	34	C	G		G	C	35	60
		23			23			

Top SW Cor base Earls Pizza Sign

^{35.7} 6.8	^{35.A} 71	^{3A.8} 77	^{35.9} 6.6	^{35.A} 71	^{3A.8} 77	^{35.A} 71	^{3A.7} 78	^{35.2} 73	^{3A.9} 76	^{3A.5} 8.0
60	48	42	32	C	G		G	C	38	60
			24				24			

^{36.2} 6.3	^{35.A} 6.6	^{35.6} 6.9	^{36.8} 5.7	^{36.8} 5.7	^{36.2} 6.3	^{36.8} 5.7	^{36.3} 6.2	^{36.8} 5.7	^{36.3} 6.2	^{35.6} 6.9
60	53	45	35	C	G		G	C	38	60
			24				24			

^{36.5} 6.0	^{36.0} 6.5	^{38.0} 4.5	^{38.2} 4.3	^{37.7} 4.8	^{38.3} 4.2	^{37.6} 4.9	^{36.7} 5.8	^{36.7} 5.8	^{36.3} 6.2
60	45	33	C	G		24	45	60	82
			24						

^{3A.7} 78	^{35.1} 74	^{35.5} 70
135	120	110
SD		

Sta + π - Elev.

942.49

11+00 Gutter Line

v

T.P.

+17

+50

12

BM 9.80 949.27 3.02 939.47

939.39

+60

0.54

48.73

March 25, 1971

11.

RT

x-7

37.9	37.8	38.4	38.8	38.3	38.9	38.2	37.7	36.9	36.0
46	47	41	37	42	3.6	4.3	48	56	6.5
60	43	31	C	G		24	37	60	93
			24						

34.5	35.1	35.5
8.02	24	2.0
CB	137	120
137		

37.8	38.0	38.7	39.3	38.33	39.1	38.9	38.8
47	45	3.8	3.2	4.16	3.4	3.6	3.7
60	40	24		CB	C	42	60
				24			

38.2	38.6	40.2	39.7	40.2	39.8	40.3	40.5	41.2	41.7
43	39	23	2.8	2.3	2.7	2.2	2.2	1.4	0.8
60	39	C	G		G	C	38	53	71
		24			24				

38.8	39.2	41.2	41.6	41.0	41.7	41.15	41.7	41.5	41.9
3.7	3.3	1.3	0.9	1.5	0.8	1.4	0.8	1.0	0.6
60	43	33	C	G		G	C	36	60
			24			24			

39.9	40.2	42.8	43.1	42.7	43.3	42.9	43.5	43.2	43.2
9.4	9.1	6.5	6.2	6.6	6.0	6.4	5.8	6.1	6.1
60	42	34	C	G		G	C	37	60
			23			24			

Part 1

Sta + π - Elev.

949.27

2+74

+89

13 Lower st Lt slightly

+31

+44

BM 7.92 956.60 0.54 948.73 (948.68)

March 25, 1971

LT

RT X-8

AA ⁰	AA ⁰	A3.6	A3.1	A3.7	A3.4	A3.9	A3.8	A3.9
53	53	57	62	56	59	54	55	54
60	42	C	G		G	C	37	60
		23			24			

AA ⁰	A3.7	A3.6	A3.7	AA ²	A3.7.5	A3.7	AA ³	AA ^{2.8}	AA ³
53	56	58	56	51	5.52	56	50	4994	60
100	60	45	23		17	5	C	41	60
					MH	24		MH	

AA.7	AA.6	AA.4	AA ⁰	AA.1	AA.5	AA.1	AA.6	A5.2	A5.4
46	47	49	53	52	48	52	47	41	39
150	100	60	43	24		G	C	36	60
						24		curb	

AA.5	AA.4	AA.4	AA.9	A5.3	AA.9	A5.4	AA ⁰	A7.3	A7.9	A7.1
48	49	49	44	40	44	39	33	20	14	16
100	60	43	24		G	C	29	36	51	60
					24					

A8.2	A6.8	A5.7	A5.2	A5.6	A5.3	A5.8	A6.4	A7.8
1.1	2.5	3.6	4.1	3.7	4.0	3.5	2.9	1.5
43	33	C	G		G	C	28	36
		24			23			

A8.0
1.3
60

A8.4
0.9
60

A8.3
1.0
51

Top Hyd NW Corner Garden

Sta	+	π	-	Elev
-----	---	-------	---	------

956.60

14+00

+50

15

+06	MH 38' R	5.15	951.45
-----	----------	------	--------

+50

+97	CB 23' L	8.79	947.81
-----	----------	------	--------

+98	CB 23' R	8.44	948.16
-----	----------	------	--------

16

BM	3.72	954.35	5.97	950.63
----	------	--------	------	--------

95.10
3.52

+26

FX
WS
DS

March 25, 1971
March 26, 1971

LT

BT X-9

50.0	50.1	48.1	47.1	46.6	47.0	46.6	47.1	47.9	49.6	50.5
66	62	79	95	10.0	96	10.0	95	87	70	61
60	43	32	C	G		G	C	30	34	46
			23			24				Under Cons

51.9	51.7	49.5	47.8	47.2	48.0	47.6	49.0	50.6	51.5
47	49	71	8.8	94	86	9.0	76	60	5.1
60	41	32	C	G		24	34	46	60
			23						

52.7	51.5	49.0	48.1	47.9	48.1	48.0	48.5	49.2	51.3
39	52	76	82	87	8.2	8.6	8.1	74	5.3
60	40	29	C	G		G	C	29	37
			24			24			Under Const

51.0	50.3	48.6	48.1	48.8	48.2	48.7	49.2	52.6	53.0
56	63	80	85	78	8.4	79	74	4.0	30
60	38	C	G		G	C	30	43	60
			24		24				

50.6	50.0	49.4	48.1	47.9	48.8	48.2	48.6	49.0	53.1	53.9
6.0	66	72	82	8.7	7.8	8.4	8.0	76	35	2.7
60	39	33	C	G		G	C	28	43	55
			23			24				Const

Top Hyd N.W. Corner Ruggles + Lexington

45.8	47.0	47.5	48.0	48.7	48.1	48.9	49.8	53.3	53.8
8.6	24	6.9	6.4	5.7	6.0	5.5	4.6	1.1	0.6
100	60	43	25		G	C	35	49	60
					24				

Sta	+	X	-	Elev.
-----	---	---	---	-------

		954.35		
--	--	--------	--	--

16+41		E West		
-------	--	--------	--	--

+52		E East		
-----	--	--------	--	--

+73				
-----	--	--	--	--

17				
----	--	--	--	--

+46				
-----	--	--	--	--

TP	2.80	949.60	7.55	946.80
----	------	--------	------	--------

Scaffolding
Spike in
PP

March 26, 1971

LT

♀

RT X-10

45.9	46.50	47.1	47.4	47.8	48.5	48.2	48.40	49.8	51.9
8.5	7.85	7.3	7.0	6.6	5.9	6.2	5.95	4.6	2.5
100	84	60	50	28		25	45	60	100
MH						CB			

45.7	46.7	47.2	47.7	48.4	48.2	49.7	52.1	52.70
8.7	7.7	7.2	6.7	6.0	6.2	4.7	2.3	1.65
100	60	50	28		25	60	100	128
MH?								

0.1 1.1
200 150

47.6	47.63	47.8	48.2	48.0	48.33	49.4	51.3
6.8	6.72	6.6	6.2	6.4	6.02	5.0	3.1
60	40	18		25	46	60	100
walk				CB			

47.49	47.4	46.7	47.8	47.9	47.7	47.5	49.4	51.1
6.86	7.0	7.7	6.6	6.5	6.7	6.9	5.0	3.3
80	60	32	14		15	28	37	60
Apron								

46.5	44.5	44.6	46.6	47.1	47.2	42.9	46.9	45.7	47.1
7.9	9.9	9.8	7.8	7.3	7.2	7.5	7.5	8.7	7.3
52	40	30	21	14		15	21	28	34

46.8

7.6
60

48.7

5.7
60

Sta	+	π	-	Elev.
-----	---	-------	---	-------

		949.60		
--	--	--------	--	--

18+00				
-------	--	--	--	--

17+97	S.D. 32' Lt	6.88	942.72	
-------	-------------	------	--------	--

✓				
---	--	--	--	--

18+27				
-------	--	--	--	--

+38				
-----	--	--	--	--

+64				
-----	--	--	--	--

19	Ent Lt.			
----	---------	--	--	--

March 26, 1971

11

2

RT x-11

44.0	43.8	43.0	45.8	46.1	46.2	46.1	45.9	44.9	45.7
56	58	66	38	35	34	35	37	47	36
60	53	31	20	14		14	21	26	31

46.4
3.2
60

44.1	43.7	43.1	43.1	45.2	45.6	45.9	45.7	45.4	44.1	45.3	45.9
55	59	65	65	44	40	37	39	42	55	43	37
60	56	38	29	20	14		13	20	26	34	60

44.2	43.8	43.1	43.3	45.1	45.5	45.7	45.5	45.2	43.3	42.6	42.9
54	58	65	63	45	41	39	41	44	63	70	67
60	50	35	27	20	14		13	20	28	45	60

44.2	43.9	43.2	43.7	44.9	45.2	45.4	45.0	44.7	42.6	42.3	42.6
54	57	64	59	47	44	42	46	49	70	73	70
60	50	34	25	20	14		13	19	27	43	60

44.67	44.41	44.5	44.3	44.6	44.9	44.6	44.3	42.1	41.9	42.4
49	51	51	53	50	47	50	53	75	77	72
60	50	32	25	14		13	19	28	44	60

conc

Sta + π - Elev

949.60

19+28

+47 Ent Rt.

+61 Good For Gutter Left.

+67 MH 92' Lt 7.25 942.35

+82 Ent Rt Gutter Lt.

20

+19 MH 51' Rt 8.31 941.29

+27

T.P. 200 947.11 4.49 945.11

March 26, 1971

Lt

£

RT x-12

44.4	43.6	42.67	43.6	44.2	44.6	44.4	44.6	40.74	41.6	41.9	42.1
5.2	6.0	6.93	5.74	5.4	5.0	5.2	5.0	8.86	8.0	7.7	7.5
60	45	38	22	15	✓	13	19	27	32	44	60
		SD	MH					SD			

43.7	43.9	43.4	43.8	44.1	44.4	44.3	44.3	44.4	43.9	43.7
5.9	5.7	6.2	5.8	5.5	5.2	5.3	5.3	5.2	5.7	5.9
60	49	35	26	15	✓	13	24	38	48	60

42.2	42.8	43.16	44.1	44.3	44.1	44.1	44.3	44.4	42.2
7.4	6.8	6.44	5.5	5.3	5.5	5.5	5.5	5.3	2.2
100	60	38	14	✓	13	21	35	43	60
		MH							

42.1	42.5	43.0	43.8	44.1	43.9	43.8	43.4	43.6
7.5	7.1	6.6	5.8	5.5	5.7	5.8	6.2	6.0
100	60	34	14	✓	13	37	60	100

43.10	42.9	43.2	43.6	44.0	43.8	43.6	41.5	41.4	41.5
6.50	6.7	6.4	6.0	5.6	5.8	6.0	8.1	8.2	8.1
63	49	24	14	✓	13	18	25	44	60
Conc									

43.35	43.01	42.9	43.4	43.8	43.6	43.4	41.3	41.3	41.2
6.25	6.53	6.7	6.2	5.8	6.0	6.2	8.3	8.3	8.4
60	49	26	14	✓	13	20	27	45	60
Conc	Ent								

Top Hyd NW Corner Summer St.

Sta	+	π	-	Elev.
-----	---	-------	---	-------

947.11

20 + 40

✓

21

+23

BM	2.70	948.54	1.27	945.84	NWG Top of Antenna
----	------	--------	------	--------	-----------------------

+53

22

✓

± March 26, 1971

Lt.

Rt x-13

40.6	40.9	42.9	43.4	43.7	43.6	43.3	41.0	41.3	41.3
65	62	42	37	34	35	38	61	58	5.8
40	29	20	14	✓	13	19	28	40	60

42.4	43.5
47	36
53	64
walk	

42.1	41.8	40.4	42.6	43.1	43.4	43.3	43.0	42.0	42.0	41.6
50	53	67	4.3	40	3.7	38	41	51	51	5.5
60	49	30	19	14	✓	13	22	34	53	60

40.5	40.4	39.7	38.29	42.6	43.1	43.3	43.2	42.9	40.68	41.4	41.6
66	6.7	7.4	8.82	4.5	4.0	3.8	39	42	6.43	5.7	5.5
60	49	35	26	19	13	✓	13	20	27	34	60
x-Culvert										S.D.	

42.5	42.1	40.6	40.5	42.6	42.9	43.2	43.1	42.7	41.3	41.7	41.8
6.0	6.4	7.9	8.0	5.9	5.6	5.3	5.4	5.8	7.2	6.8	6.7
60	41	32	27	18	13	✓	13	21	26	44	60

42.5	41.1	41.2	42.6	43.0	43.2	43.1	42.9	41.3	42.4	42.0
6.0	7.4	7.3	5.9	5.5	5.3	5.4	5.6	7.2	6.1	6.5
43	32	27	20	14	✓	12	20	26	41	60

→ 43.0
5.5
60

Sta + π - Elev.

948.54

22+21 Ent Rt & Lt

+67

+84 Gather Lt

23 Aprox 2 Autumn Ent Rt

+14

+62

March 26, 1971

Lt.

BT

X-14

43.21

42.92

42.8

43.1

43.2

43.1

43.4

43.3

5.33 5.62 5.7 5.4 5.3 5.4 5.1 5.2

65 49 28 13 13 33 60

Conc

42.4

42.7

42.6

43.1

43.2

43.1

43.2

41.7

42.0

43.0

6.1 5.8 5.9 5.4 5.3 5.4 5.3 6.8 5.9 5.5

60 36 22 14 13 23 29 34 60

41.4

41.8

41.9

42.4

43.1

43.3

43.2

42.7

42.8

43.3

7.1 6.7 6.6 6.1 5.4 5.2 5.3 5.8 5.7 5.2

100 60 50 29 13 13 27 43 60

41.21

42.1

42.4

42.8

43.2

43.2

43.3

43.0

43.1

43.3

6.8 6.83 6.4 6.1 5.7 5.3 5.3 5.2 5.5 5.4 5.2

100 96 60 41 24 14 13 27 43 60

MH

41.3

41.7

41.9

42.3

43.2

43.3

43.3

43.0

43.1

43.4

7.2 6.8 6.6 6.0 5.3 5.2 5.2 5.5 5.4 5.1

100 60 45 27 15 13 26 40 60

44.59

44.4

43.7

42.9

42.8

43.3

43.5

43.5

43.2

42.5

43.69

43.5

3.95 4.1 4.8 5.6 5.7 5.2 5.0 5.0 5.3 6.0 4.85 5.0

60 45 38 23 14 13 22 34 46 60

Bldg

MH

Sta + π - Elev

948.54

24+00

E_h + L_t

+42

7
15

+73

25

BM 2.06 949.48 1.12 947.42 (947.42)

+40

+65

March 26, 1971

LT

RT

X-15

43.9	43.8	43.2	43.0	43.3	43.5	43.3	43.5	43.2	43.1
46	47	53	55	52	50	50	50	53	48
60	56	41	25	14	✓	12	20	31	60

43.5	42.9	41.98	43.2	43.6	43.5	43.4	42.33	43.4	42.8
50	56	65.6	53	49	50	51	62	51	57
60	35	26	14	✓	13	21	26	36	60
		50					50		

44.2	43.64	43.48	43.5	43.7	43.5	43.2	43.7	43.6
43	490	506	50	48	50	53	48	49
60	33	14	14	✓	13	24	44	60
		Conc						

44.4	43.8	43.8	43.6	43.7	43.5	43.3	43.9	44.28
41	47	47	49	48	50	52	46	426
60	34	31	14	✓	12	22	33	51

Top Hyd NE Corner Roseawn 4 Lex

Conc

44.5	44.1	44.1	43.7	43.8	43.7	43.7	44.18	44.37	44.51
50	54	54	58	57	57	58	530	511	491
60	33	29	13	✓	12	23	35	50	60
							Conc		

44.4	44.01	43.45	43.58	43.9	43.8	43.7	44.16	44.5	45.5
51	547	603	590	56	57	58	532	50	40
60	33	26	13	✓	11	22	35	50	60
		Conc					Conc		

Sta

949.48

26+00

✓

+07

Gutter East

+14

✓

BM

2.06 947.42 947.42

± March 26, 1971

LT

RT

X-16

43.0

42.66

43.5

43.7

43.9

43.9

43.9

44.49

44.68

44.16

6.5 682 60 5.8 5.6 5.6 5.6 4.99 4.80 5.32

35 34 23 13 ✓ 11 G C C G

SD

22

35

43.70

43.5

5.78

60

39

60

conc

44.26

44.26

522

5.22

60

51

43.2

43.5

43.7

43.8

43.9

43.93

43.99

44.0

44.1

44.1

6.3 60 5.8 5.7 5.6 5.55 5.49 5.5 5.4 5.4

60 42 31 13 ✓ 19 26 33 50 60

conc

MH

MH

42.87

43.05

43.38

43.7

43.9

43.9

44.0

43.9

44.1

44.1

44.1

66 6.43 610 5.8 5.6 5.6 5.5 5.6 5.4 5.4 5.4

69 60 41 31 13 ✓ 12 25 43 60 100

conc

42.3

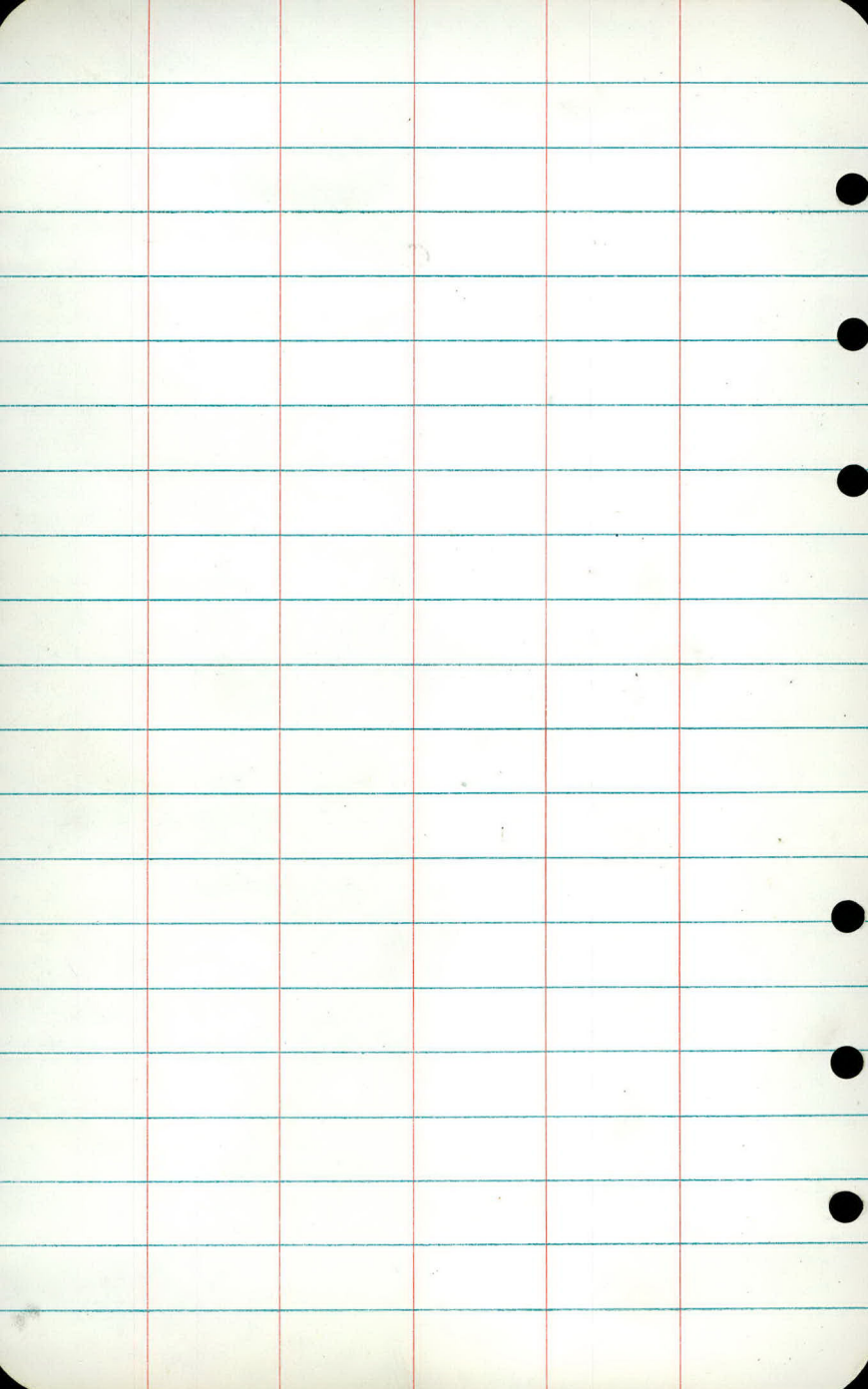
7.2

100

5.5

183

Top Hyd NE Corner Roselawn & Lex.



KP
RG
LPD
DK

25 MARCH 1971

Sunny 25°

X-17

LEXINGTON AVE
51 TURNBACK

X - SECTIONS

Roselawn Ave to Co. Rd. "B"

~~Sta 26+39.94 to Sta~~
Sta 26+27.94

STA + π - ELEV.

BM 1.87 949.29

947.42

^{27.94}
26 + ~~37.94~~ = $\pm$ ROSELAWN

✓

36
+ ~~48~~

5.30 943.99

42
+ ~~54~~ = N. GUTTER

✓

62
+ ~~74~~

5.80 943.49

LT

25 MAR. 1971

RT

x-18

TOP HYDRANT N.E. Cor. ROSELAWN

A3.2	A3.38	A3.54	A3.9	A3.9	A3.9	A3.9	A4.1	A4.1
6.1	5.91	5.8	5.4	5.4	5.4	5.4	5.2	5.2
58	39	39	14	✓	20	40	65	94
MH								
A2.8	A2.5						A4.0	
6.5	6.8						5.3	
83	100						100	

TOP MH 54' RT

A2.5	A2.88	A3.3	A3.9	A3.9	A4.0	A4.0	A4.1	A4.1
6.8	6.41	6.0	5.4	5.4	5.3	5.3	5.2	5.2
74	54	34	14	✓	14	22	50	75
MH								
A2.2							A3.9	
7.1							5.4	
100							100	

TOP DRAIN 28' LT

STA	+	π	-	ELEV.
-----	---	-------	---	-------

STA	+	π	-	ELEV.
-----	---	-------	---	-------

949.29

STA	+	π	-	ELEV.
-----	---	-------	---	-------

27+00

STA	+	π	-	ELEV.
-----	---	-------	---	-------

✓

STA	+	π	-	ELEV.
-----	---	-------	---	-------

28+00

STA	+	π	-	ELEV.
-----	---	-------	---	-------

✓

STA	+	π	-	ELEV.
-----	---	-------	---	-------

+11

STA	+	π	-	ELEV.
-----	---	-------	---	-------

5.44 943.85

STA	+	π	-	ELEV.
-----	---	-------	---	-------

+17

STA	+	π	-	ELEV.
-----	---	-------	---	-------

6.71 942.58

LT

Z

25 MAR 1971

RT

x19

AA.25

AA.37

AA.26

AA.01

AA.2

AA.1

AA.7

AA.0

AA.5

5.04

4.92

5.03

5.28

5.1

5.2

5.6

5.3

4.8

100

68

38

14

✓

12

29

44

64

conc

conc.

conc.

conc.

AA.5.2

4.1

100

AA.5.0

AA.6

AA.14

AA.16

AA.5

AA.2

AA.8

AA.2

AA.5

4.3

4.7

5.15

5.13

4.8

5.1

5.5

7.1

5.8

75

55

34

14

✓

13

22

29

38

conc.

conc.

AA.9

AA.3

4.4

5.0

100

65

TOP MH 21.5' LT

TOP DRAIN 29' LT

STA + π - ELEV.

949.29

29+00

✓

+22

7.38

941.91

BM 3.87 951.03 2.18 947.11 947.16

+57

✓

LT

E

25 MAR. 1971

RT

X-208

✓

A2.6	A2.6	A3.9	A4.5	A4.8	A4.6	A4.4	A4.4	A4.4
6.7	6.7	5.4	4.8	4.5	4.7	4.9	6.9	6.9
32	28	21	14	✓	12	20	25	29

A3.7	A4.4	A5.51	A5.8	A5.53	A5.6	A5.0	A2.8
5.6	4.9	3.78	3.5	3.6	3.7	4.3	6.5
37	54	74	84	74	56	44	30
		SW	BLDG.	BLDG.			

TOP DRAIN 28' LT

TOP HYDRANT SOUTH OF RYAN

✓

A3.8	A3.2	A4.5	A4.9	A5.1	A4.9	A4.8	A3.2	A3.6
7.2	7.8	6.5	6.1	5.9	6.1	6.2	7.8	7.4
39	34	22	14	✓	12	19	25	33

AA.1	AA.1	AA.0
6.9	6.9	7.0
61	80	100

AA.4	AA.7	AA.3
6.6	6.3	6.7
100	75	52

STA	+	π	-	ELEV.
-----	---	-------	---	-------

		951.03		
--	--	--------	--	--

30+00				
-------	--	--	--	--

✓				
---	--	--	--	--

+ 10				
------	--	--	--	--

		8.52	942.51	
--	--	------	--------	--

+ 23				
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		8.75	942.28	
--	--	------	--------	--

31+00				
-------	--	--	--	--

LT

E

25 MAR 1971

RT

X-21

✓

A ^{2.1}	A ^{3.3}	A ^{5.0}	A ^{5.2}	A ^{5.5}	A ^{5.3}	A ^{5.1}	A ^{3.9}	A ^{3.8}
8.3	7.7	6.0	5.8	5.5	5.7	5.9	7.1	7.2
38	27	19	14	✓	12	19	22	26

A ^{2.9}	A ^{2.5}	A ^{2.3}	A ^{5.9}	A ^{6.2}	A ^{5.7}	A ^{5.2}
8.1	8.5	8.7	5.1	4.8	5.3	5.8
51	75	100	80	60	49	32
			40.			

TOP MH52' LT

TOP DRAIN 32' LT

✓

A ^{5.1}	A ^{5.6}	A ^{5.0}	A ^{3.9}	A ^{6.1}	A ^{6.0}	A ^{5.7}	A ^{5.1}	A ^{5.1}
5.6	5.5	5.4	5.1	4.9	5.0	5.3	5.6	5.9
75	46	23	12	✓	12	28	49	72

A^{5.0}
6.0
100

STA + π - ELEV.

951.03

31+09

5.55 945.48

BM 1.45 951.96 0.51 950.52 (950.51)

+ 49

✓

32+00

✓

LT

E

25 MAR. 1971

RT

X-22

TOP MH 49' RT

TOP H/D. NW COR RYAN

A ^{5.0}	A ^{4.2} A	A ^{6.1}	A ^{6.3}	A ^{6.0}	A ^{6.2}	A ^{5.9}	A ^{4.2} 3	A ^{5.1}
6.4	7.72	5.9	5.7	5.4	5.8	6.1	7.73	6.9
33	28	18	14	✓	12	19	24	30
	SD						SD	

A ^{5.8}	A ^{6.0}
6.2	6.0
50	75

A ^{5.3}	A ^{5.4}
6.7	6.6
75	50

A ^{5.8}	A ^{5.6}	A ^{6.3}	A ^{6.1}	A ^{7.0}	A ^{6.1}	A ^{6.9}	A ^{6.1}	A ^{6.4}
6.2	6.4	5.7	5.3	5.0	5.3	5.1	5.6	5.6
35	28	19	12		12	19	32	47

A ^{6.0}	A ^{6.5}
6.0	5.5
53	75

A ^{6.5}
5.5
75

STA	+	π	-	ELEV.
-----	---	-------	---	-------

		951.96		
--	--	--------	--	--

32+69				
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		6.15	945.81	
--	--	------	--------	--

+76				
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		4.99	946.97	
--	--	------	--------	--

+76				
-----	--	--	--	--

		5.54	946.42	
--	--	------	--------	--

+83	=	$\neq$	RYAN	
-----	---	--------	------	--

✓				
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+85				
-----	--	--	--	--

		5.09	946.87	
--	--	------	--------	--

33+00				
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X-23

$\lambda^{7.5}$	$\lambda^{7.3}$	$\lambda^{6.8^3}$	$\lambda^{6.9}$	$\lambda^{7.4}$	$\lambda^{7.1}$	$\lambda^{7.3}$	$\lambda^{7.0}$	$\lambda^{6.2}$	λ^A	$\lambda^{6.8}$	$\lambda^{7.0}$
4.5	4.7	6.13	5.4	4.6	4.3	4.7	5.0	5.8	5.6	5.2	5.0
100	77	57 SD	36	12	✓	14	20	27	36	50	75

STA	+	π	-	ELEV.
-----	---	-------	---	-------

		951.96		
--	--	--------	--	--

33+22				
-------	--	--	--	--

		5.49	946.47	
--	--	------	--------	--

+27				
-----	--	--	--	--

		6.11	945.85	
--	--	------	--------	--

+27				
-----	--	--	--	--

		6.74	945.22	
--	--	------	--------	--

TP				
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	5.55	953.80	3.71	948.25
--	------	--------	------	--------

34+00				
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+46				
-----	--	--	--	--

LT

25 MAR. 1971

RT

X-24

TOP MH 32' LT

TOP DRAIN 28' LT

TOP DRAIN 23' RT

± STA 34+00

48.8	48.5	47.9	48.1	48.2	47.9	48.0	47.6	47.7	48.2
5.0	5.3	5.9	5.7	5.6	5.9	5.8	6.2	6.1	5.6
75	45	24	12	✓	13	18	33	47	75

48.4	48.3	47.6	47.4	48.1	48.4	48.6	48.4	48.5	48.8	49.6	49.7	49.9
5.4	5.5	6.2	6.4	5.7	5.4	5.2	5.4	5.3	5.0	4.2	4.1	3.9
75	57	38	25	18	12	✓	12	20	31	38	57	75

STA + π - ELEV.

953.80

34+50

35+00

+97

36+06

4.52 949.28

36+06

4.58 949.22

+13

£ SHRYER

ICG
LPD
DK

LT

March 26, 1971
cloudy 33° RT

X-25

17.3 17.2 16.9 17.2 16.73
6.6 6.6 6.9 6.6 7.07 5.9 5.3 5.2
75 52 43 29 22 19 12

DUPL.
Sta 30+46 RT

19.4 19.0 18.9 18.8 18.9 18.9 18.7 18.6 19.0 19.6 19.9
4.4 4.8 4.9 5.0 4.9 4.9 5.1 5.2 4.8 4.2 3.9
75 60 35 17 11 12 21 26 50 75

19.3 19.1 18.69 19.2 19.3 19.5 19.3 19.1 18.6 19.1 19.3 19.0 19.7
4.5 4.7 5.1 4.6 4.3 4.3 4.5 4.7 5.2 4.1 3.3 3.8 4.1
75 68 49 28 12 13 21 27 32 56 61 75

MH 21' LT.

MH 49' LT.

19.5 19.4 19.2 19.43 19.6 19.6 19.4 19.1 19.2 19.5 19.7
4.3 4.4 4.6 4.37 4.2 4.2 4.4 4.7 4.6 4.3 4.1
100 75 50 30 16 13 23 36 52 75

STA + π - ELEV

953.80

36+28

T.P. 2.32 954.41 1.71 952.09 (925.10)

36+53

37+00

+33

T.P. 5.23 956.21 3.43 950.98

38+00

LT E RT A-26

18.9	AB.50	AB.1	A9.0	A9.4	A9.7	A9.5	A9.5	A9.8	A9.7A
49	530	5.1	4.8	4.2	4.1	4.3	4.3	4.0	4.01
75	50	32	28	12	✓	13	30	58	72

TOP HYD. N.W. COR. SHRYER

46.2	AB.0	AB.0	AB.89	AB.72	A9.4	A9.7	50.0	A9.7	A9.2	A9.77	AB.1	A9.5	A9.7	A9.9
6.2	6.4	6.4	7.52	5.69	5.0	4.7	4.4	4.7	5.2	6.64	5.3	4.9	4.74	5.5
75	55	38	27	21	17	13	✓	13	20	25	37	45	52	75

AB.6	AB.9	AB.9	AB.0	AB.8	50.2	50.3	50.1	50.0	AB.6	AB.5	AB.9	AB.8
6.8	6.5	6.5	6.4	4.6	4.2	4.1	4.3	4.4	5.8	5.1	4.5	4.6
75	48	33	25	18	11	✓	13	18	26	38	52	75

AB.5	AB.6	AB.7	50.1	50.4	50.3	50.4	50.1	AB.6	AB.7	AB.1	AB.8
4.9	4.8	4.7	4.3	4.0	3.9	4.0	4.3	5.8	5.7	5.3	4.6
75	53	32	20	11	✓	13	20	27	35	54	75

STA 38 + 00 E

50.1	50.3	50.0	AB.6	50.6	50.9	51.0	50.8	50.4	AB.0	AB.3	AB.1	AB.0
5.8	5.9	6.2	6.6	5.6	5.3	5.2	5.4	5.8	7.2	6.9	7.1	7.2
75	50	33	21	18	11	✓	13	21	26	36	54	75

STA	+	Δ	-	ELEV.
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		956.21		
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38+55				
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+50				
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	8.20	948.01		
--	------	--------	--	--

39+00				
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+25				
-----	--	--	--	--

LT

✓

RT

x-27

5 ^{0.8}	5 ^{1.1}	5 ^{1.1}	5 ^{1.1}	5 ^{1.1}	5 ^{1.1}	5 ^{1.1}	5 ^{1.1}	5 ^{1.1}	5 ^{1.1}	5 ^{1.1}	5 ^{1.1}	5 ^{1.1}	5 ^{1.1}	5 ^{1.1}
5.4	5.8	5.8	5.1	5.1	9.8	5.1	5.3	6.5	6.7	6.4				
50	33	21	18	10		14	19	23	32	37				

5^{1.0}
5.2
75

5^{1.2} 5^{1.7}
8.0 7.5
75 51

MA RT. 71

✓

5 ^{0.7}	5 ^{0.7}	5 ^{0.7}	5 ^{0.7}	5 ^{0.7}	5 ^{0.7}	5 ^{0.7}	5 ^{0.7}	5 ^{0.7}	5 ^{0.7}	5 ^{0.7}	5 ^{0.7}	5 ^{0.7}	5 ^{0.7}	5 ^{0.7}
5.5	5.5	5.7	4.6	4.7	4.5	4.7	5.0	5.3	5.9	5.2				
50	33	24	16	10		13	20	36	53					

5^{1.0}
5.2
75
51.00
CB

5^{1.4} 5^{1.7}
WALL
4.8 6.5
75
51.3

5 ^{1.3}	5 ^{1.4}	5 ^{1.7}	5 ^{1.7}	5 ^{1.7}	5 ^{1.7}	5 ^{1.7}	5 ^{1.7}	5 ^{1.7}	5 ^{1.7}	5 ^{1.7}	5 ^{1.7}	5 ^{1.7}	5 ^{1.7}	5 ^{1.7}
5.21	4.9	4.8	4.5	4.3	4.5	4.7	5.4	5.1	4.9					
43	35	21	10		14	21	26	28	42					

5^{1.6} 5^{1.7}
4.6 4.7
60 75

5^{1.7} 5^{1.7}
4.5 4.7
75 59

STA + π - ELEV

956.2¹~~0~~

39 + 41

~~E~~ SKILLMAN

+ 57

B.M. 3.65 958.00 1.87 954.3⁴~~3~~ 954.35

+ 81

7.66 948.55

+ 81

8.11 948.10

LT



RT

A-28

5 ^{1.1}	5 ^{1.6}	5 ^{1.54}	5 ^{1.8}	5 ^{2.0}	5 ^{1.8}	5 ^{1.6}	5 ^{1.7}	5 ^{1.2}
4.5	4.6	4.67	4.4	4.2	4.4	4.6	5.5	5.0
75	50	35	9	1	14	20	25	32

5^{1.8}
4.4
100

5^{1.5} 5^{1.3} 5^{1.0}
4.7 4.9 5.2
102 70 46

5 ^{0.78}	5 ^{1.2}	5 ^{1.44}	5 ^{1.9}	5 ^{2.1}	5 ^{1.9}	5 ^{1.6}	5 ^{1.7}	5 ^{1.8}
CB		MH						
5.43	5.0	4.77	4.3	4.1	4.3	4.6	5.5	5.4
45	33	22	10		13	19	25	31

5^{1.2} 5^{1.2}
5.0 5.0
61 75

5^{1.8} 5^{1.7}
5.4 5.5
75 60

TOP HYD. N.W. COR. SKILLMAN

DRAIN LT. 39'

DRAIN RT. 25'

STA	+	π	-	ELEV
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		958.00		
--	--	--------	--	--

40+00				
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41+00				
-------	--	--	--	--

+ 87				
------	--	--	--	--

		4.56	953.44	
--	--	------	--------	--

42+00				
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LT

E

RT

x-29

5 ^{1.2}	5 ^{1.2}	5 ^{2.1}	5 ^{2.3}	5 ^{2.4}	5 ^{2.1}	5 ^{1.8}	5 ^{0.5}
6.8	6.8	5.9	5.7	5.6	5.9	6.2	7.5
26	22	17	9	✓	13	20	25

5 ^{1.9}	5 ^{2.5}	5 ^{3.0}	5 ^{1.2}	5 ^{1.1}	5 ^{1.4}	5 ^{1.0}	
6.1	5.5	5.0	6.8	6.9	6.6	7.0	
31	50	75	✓	75	56	36	32

5 ^{3.4}	5 ^{2.6}	5 ^{2.8}	5 ^{3.0}	5 ^{3.2}	5 ^{3.0}	5 ^{3.5}	5 ^{2.9}	5 ^{1.3}
4.6	5.4	5.2	5.0	4.8	5.0	5.5	6.1	6.7
35	24	18	9	13	21	31	55	

5 ^{3.99}	5 ^{4.5}	5 ^{5.3}
CONC.	CONC.	
4.01	3.35	2.7
48	62	75

5 ^{1.1}
6.9
75

MH LT. 27'

5 ^{1.2}	5 ^{1.2}	5 ^{1.9}	5 ^{3.8}	5 ^{3.9}	5 ^{3.7}	5 ^{3.5}	5 ^{2.4}	5 ^{1.2}
2.8	3.8	4.1	4.2	4.1	4.3	4.5	5.6	4.8
51	28	15	9	14	20	24	28	

5 ^{1.6}	5 ^{4.0}	5 ^{4.5}	5 ^{4.6}
2.2	4.0	4.5	4.6
75	100	68	43

STA	+	T	-	ELEV
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		958.00		
--	--	--------	--	--

42+11			4.62	953.38
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43+00				
-------	--	--	--	--

T.P.	3.71	959.78	1.93	956.07
------	------	--------	------	--------

43+50				
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LT

E

RT

X-30

M+ RT. 47'



5 ^{4.6}	5 ^{4.2}	5 ^{4.4}	5 ^{4.3}	5 ^{4.5}	5 ^{4.3}	5 ^{4.5}	5 ^{4.1}	5 ^{4.1}
3.4	3.8	3.6	3.7	3.5	3.7	3.5	3.9	3.3
30	24	20	10		12	20	23	27



5 ^{4.4}	5 ^{5.1}	5 ^{6.1}
2.6	2.3	1.9
51	57	75

5 ^{4.5}	5 ^{4.3}	5 ^{4.8}
0.5	0.7	2.2
10	53	34

TOP HYD. N.E. COR. PARKER ST.



5 ^{3.8}	5 ^{4.1}	5 ^{4.3}	5 ^{4.6}	5 ^{4.4}	5 ^{3.9}	5 ^{5.1}	5 ^{4.3}
6.0	5.1	5.5	5.2	5.4	5.9	4.7	2.5
24	18	11		13	22	28	45



5 ^{5.4}	5 ^{5.9}
4.4	3.9
38	60

5 ^{4.1}
1.7
60

STA	+	π	-	ELEV
-----	---	-------	---	------

		959.78		
--	--	--------	--	--

43+78				
-------	--	--	--	--

✓				
---	--	--	--	--

44+00				
-------	--	--	--	--

✓				
---	--	--	--	--

+05				
-----	--	--	--	--

		6.43	953.35	
--	--	------	--------	--

+17				
-----	--	--	--	--

+31				
-----	--	--	--	--

		1140		
--	--	------	--	--

		5.00	954.78	
--	--	------	--------	--

	LT		RT	X-31
5.1.5	5.1.6	5.1.3	5.1.5	5.1.2
CONC	5.2	5.5	5.3	6.0
4.63	23	11	13	24
32				27
5.1.3	5.1.3		5.1.7	5.1.9
CONC	CONC		3.1	2.9
4.45	4.15		60	56
46	60			
				5.1.0
				3.8
				38

5.1.9	5.1.9	5.1.4	5.1.3	5.1.4	5.1.2	5.1.7	5.1.3
5.9	5.9	5.4	5.5	5.4	5.6	6.1	5.5
45	24	17	11	13	20	27	
5.1.3					5.1.7	5.1.7	5.1.3
5.5					4.1	4.4	4.5
60					60	51	38

1714 RT 20

5.1.0	5.1.2	5.1.1	5.1.3	5.1.2	5.1.1	5.1.6
5.8	5.6	5.7	5.5	5.6	5.7	5.2
26	16	10		13	29	5.1
CONC	5.1.2	5.1.0			5.1.0	5.1.0
5.52	5.50	5.38			4.2	5.0
33	44	60			120	60

1714 RT 52

STA	+	π	-	ELEV
-----	---	-------	---	------

		959.78		
--	--	--------	--	--

44+34				
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✓				
---	--	--	--	--

+46				
-----	--	--	--	--

	1/42			
--	------	--	--	--

		5.43	954.35	
--	--	------	--------	--

+52				
-----	--	--	--	--

✓				
---	--	--	--	--

T.P	2.93	956.51	6.20	953.58
-----	------	--------	------	--------

44+52				
-------	--	--	--	--

		2.92	956.86	
--	--	------	--------	--

LT

~~E~~

RT

X-32

5A.1
6.7
26

5A.1
5.7
17

5A.1
5.7
11

5A.1
5.7
✓

5A.0
5.8
12

5A.2
5.6
28

5A.9
4.9
60

5A.0
5.8
30

5A.7
5.1
60

5A.3
4.5
100

MH

5A.3
4.48
91

MH RT 35

5A.6
7.2
26

5A.0
5.8
17

5A.0
5.8
11

5A.1
5.7
✓

5A.9
5.9
12

5A.0
5.8
27

5A.3
5.5
39

5A.8
6.0
35

5A.6
5.2
60

5A.4
7.4
110

5A.6
5.2
57

PK. STA 45+00

MH RT 44

STA	+	Δ	-	ELEV
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		956.51		
--	--	--------	--	--

44+88				
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		4.47	952.04	
--	--	------	--------	--

45+00				
-------	--	--	--	--

✓				
---	--	--	--	--

+50				
-----	--	--	--	--

✓				
---	--	--	--	--

+59				
-----	--	--	--	--

		5.72	950.79	
--	--	------	--------	--

LT

E

RT

X-33

Lt 10

HH RT 27

52.3

4.2

25

53.3

3.2

18

53.3

3.0

11

53.6

2.9

53.4

3.1

12

53.4

3.1

17

52.4

4.1

21

53.4

3.1
34

54.2

2.3
60

55.2

1.3
60

54.6

1.9
48

53.4

3.1
29

51.2

5.3

25

52.3

4.2

19

52.7

3.8

11

53.0

3.5

52.7

3.8

13

52.3

4.2

20

51.1

4.8

23

52.4

4.1

34

53.7

2.8

60

53.6

2.9

60

52.9

3.6

31

S.D. LT 22

STA

+

π

-

ELEV.

956.51

45+81

✓

46+00

✓

+13

✓

LT

RT

X-34

~~51.6~~

4.9

44

~~52.0~~

4.5

26

~~52.3~~

4.2

12

~~52.6~~

3.9

~~52.4~~

4.1

14

~~51.9~~

4.6

18

~~51.3~~

5.2

23

~~51.6~~

4.9

60

~~51.7~~

4.8

100

~~51.7~~

4.8

60

~~51.7~~

4.8

34

~~51.8~~

4.7

60

~~51.8~~

4.7

48

~~52.0~~

4.5

12

~~52.3~~

4.2

~~52.1~~

4.4

13

~~51.7~~

4.8

18

~~51.0~~

5.5

23

~~51.4~~

5.1

36

~~51.8~~

4.7

100

~~51.6~~

4.9

60

~~51.4~~

5.0

60

~~51.4~~

5.0

31

~~51.9~~

4.6

12

~~52.1~~

4.4

~~51.9~~

4.6

13

~~51.6~~

4.9

17

~~50.9~~

5.6

23

~~51.5~~

5.0

34

~~51.7~~

4.8

100

~~51.6~~

4.9

60

STA	+	π	-	ELEV
-----	---	-------	---	------

		956.51		
--	--	--------	--	--

46+50				
-------	--	--	--	--

✓				
---	--	--	--	--

47+00				
-------	--	--	--	--

✓				
---	--	--	--	--

+50				
-----	--	--	--	--

48+00				
-------	--	--	--	--

LT

X

RT

X-35

50.2

51.1

51.4

51.6

51.4

51.3

50.6

6.3

5.4

5.1

4.9

5.1

5.3

5.9

23

20

13

✓

12

17

23

51.0

51.1

51.3

51.3

5.5

5.4

5.2

5.2

33

60

60

35

FE

50.3

50.8

51.0

50.7

50.5

49.5

6.2

6.2

5.7

5.5

5.8

6.0

7.0

34

21

13

✓

14

20

27

50.0

49.7

50.20
MH

50.2

6.5

6.8

6.31

6.3

60

60

52

38

49.3

FE 49.8

49.6

50.0

50.4

50.1

49.7

47.8

47.9

7.2

7.7

6.9

6.5

6.1

6.4

6.8

8.7

8.6

60

34

22

13

✓

14

20

28

60

48.6

49.5

49.8

49.5

49.1

47.4

FE

49.0

7.0

6.7

7.0

7.4

9.1

7.9

7.5

7.0

6.7

7.0

7.4

9.1

34

22

12

✓

14

20

30

48.8

47.8

47.7

7.7

8.7

8.8

60

60

42

STA	+	π	-	ELEV
-----	---	-------	---	------

		956.51		
--	--	--------	--	--

TP	3.95	953.78	6.68	949.83
----	------	--------	------	--------

48+50

✓

+97

7.37 949.14

49+10

+34

7.19 949.32

+34

9.27 947.24

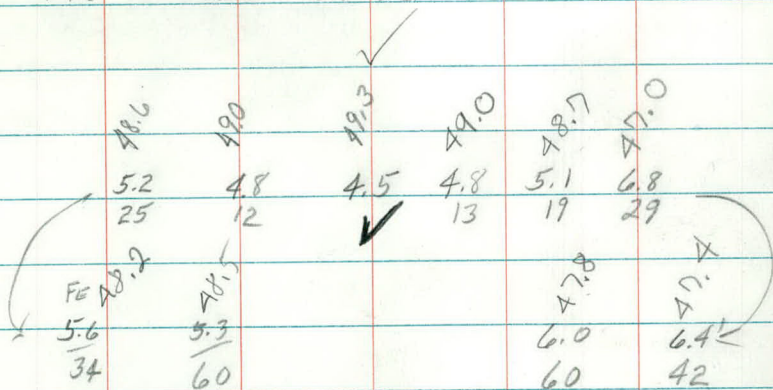
LT

4

RT

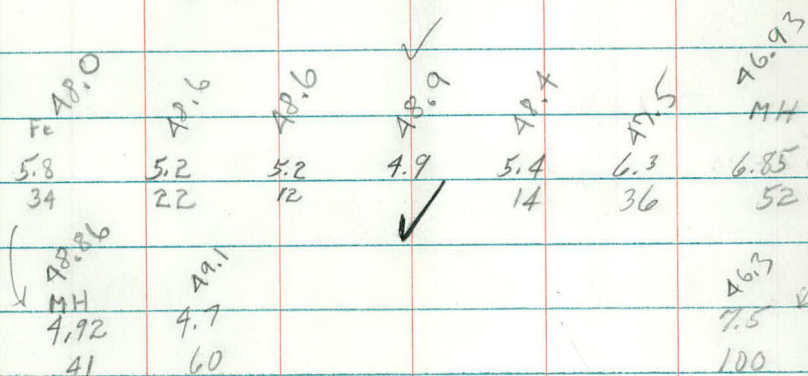
X-36

PK STA. 48+00



S. DRAIN

RT 45



S. DRAIN

RT 23

S. DRAIN

RT 44

STA	+	π	-	ELEV
-----	---	-------	---	------

		953.78		
--	--	--------	--	--

49+48				
-------	--	--	--	--

✓				
---	--	--	--	--

+57				
-----	--	--	--	--

✓				
---	--	--	--	--

50+00				
-------	--	--	--	--

LT

~~2~~

RT

x-37

~~48.4~~~~48.4~~~~48.6~~~~48.3~~~~47.8~~~~45.7~~

5.4

5.4

5.2

5.5

6.0

8.1

25

10

14

20

30

49.1

49.8

49.9

✓

45.3

45.2

4.7

4.0

3.9

8.5

8.6

34

47

60

60

48

~~48.4~~~~48.4~~~~48.6~~~~48.3~~~~48.0~~~~46.0~~

5.4

5.4

5.2

5.5

5.8

7.8

26

10

13

20

28

49.1

49.8

49.9

✓

48.4

48.4

45.8

4.7

4.0

3.9

5.4

5.4

8.0

34

47

60

80

60

48

48.7

48.5

48.3

48.5

48.2

48.2

48.7

5.1

5.3

5.5

5.3

5.6

5.6

5.1

33

23

13

12

23

45

49.0

✓

48.9

4.8

4.9

60

60

STA	+	π	-	ELEV
-----	---	-------	---	------

		953.78		
--	--	--------	--	--

50+50				
-------	--	--	--	--

✓				
---	--	--	--	--

51+00				
-------	--	--	--	--

+50				
-----	--	--	--	--

✓				
---	--	--	--	--

T.P.	4.60	953.01	5.37	948.41
------	------	--------	------	--------

BM	1.60	952.92	1.70	951.31	951.32
----	------	--------	------	--------	--------

LT

E/

RT

X-38

48.7
5.1
29

48.2
5.6
25

48.3
5.5
14

48.4
5.4
✓

48.3
5.5
13

48.9
P.BOX
4.89
29

48.8
4.0
50

48.8
5.0
33

49.6
4.2
60

49.4
4.4
60

49.7
4.1
60

49.0
4.8
34

48.6
CURB
5.2
27

48.0
5.8
27

48.4
5.4
✓

48.2
5.6
20

48.6
5.2
35

49.0
4.8
60

49.7
4.1
60

49.1
4.7
33

48.6
CURB
5.2
26

48.0
5.8
26

48.3
5.5
✓

48.3
5.5
25

48.58
S.W.
5.20
28

48.72
CONC
5.06
34

49.10
CONC
4.68
60

49.04
CONC
4.74
54

PK STA 51+00

TOP HYD SW COR CO RD "B"

STA + π - ELEV.
952.92

52+00

✓
+06

5.19 947.73

+12

5.05 947.87

+29 = GUTTER LT

✓

KP
WS
DS
GA
DK

LT

✓

30 MAR 1971

RT

X-39

49.1	48.6	48.3	47.8	48.3	48.1	48.4	48.5A	48.72
3.8	4.3	4.6	5.1	4.6	4.8	4.5	4.38	4.20
60	35	27	26	✓	24	27	34	55
		TC	G				conc.	conc

48.75
4.17
60
conc

TOP CB 26' LT

TOP CB 26' RT

47.37	47.39	47.34	48.3	47.93	47.79	48.14
5.55	5.53	5.58	4.6	5.19	5.13	4.78
60	44	41	✓	34	37	38
	CB	conc.			G	TC

47.19
5.73
100

48.42
4.50
60
TC

48.41
4.51
55
TC

STA + π - ELEV.

952.92

62+33 = GUTTER RT

+55 $\notin$ Co. RD B

✓

+71

5.21 947.71

+76 = GUTTER RT

✓

LT

E

30 MAR 1971

RT

x-40

7.3 ^x	7.38	7.34 ^x	7.2	7.70	7.5 ^x	7.66	7.87
5.58	5.44	5.58	4.7	5.22	5.38	5.26	5.09
100	60	42	✓	38	48	60	100
conc	conc	conc,	✓		CB		

7.63	7.76	7.78	7.1	7.0	7.0	7.0	7.1
5.29	5.16	5.14	4.8	4.9	4.9	4.9	4.8
100	60	43	✓	32	48	60	100
conc	conc	conc,	✓				

7.46	7.23	7.1	7.4
5.46	5.69	3.8	4.5
150	200	200	150
conc	conc,		

TOP MH 33' LT

7.47	7.52	7.1	7.72	7.45	7.61
5.45	5.40	4.8	5.20	5.47	5.31
60	43	✓	25	44	60
conc	conc,	✓	MH	CB	

7.76
5.16
100

STA	+	π	-	ELEV.
-----	---	-------	---	-------

		952.92		
--	--	--------	--	--

2+81		GUTTER	LT	
------	--	--------	----	--

✓

+96				
-----	--	--	--	--

		5.48	947.44	
--	--	------	--------	--

+99				
-----	--	--	--	--

		5.41	947.51	
--	--	------	--------	--

53+00				
-------	--	--	--	--

✓

30 MAR 1971

LT

E

RT

x-41

x7.21	x7.40	x7.38	x7.48	x8.2	x7.49	x7.99	x7.99
5.71	5.52	5.54	5.44	4.7	5.43	4.93	4.93
100	60	51	43	✓	35	36	46
conc.	conc.	CB	conc		G	TC	Pull BOX

x8.1
4.8
60

TOP CB 27' LT

TOP CB 26' RT

x8.16	x8.12	x8.01	x7.32	x8.1	x7.54	x8.02	x8.8	x8.9
4.76	4.71	4.91	5.60	4.8	5.38	4.90	4.1	4.0
50	46	27	26	✓	24	27	38	52
SW	SW	TC	G		G	TC		

x8.2
4.7
60

x8.9
4.0
60

STA	+	π	-	ELEV.
-----	---	-------	---	-------

		952.92		
--	--	--------	--	--

54+00				
-------	--	--	--	--

TP	3.96	953.27	3.61	949.31
----	------	--------	------	--------

BM				
----	--	--	--	--

		2.62	950.65	950.66
--	--	------	--------	--------

55+00				
-------	--	--	--	--

+40				
-----	--	--	--	--

		6.51	946.41	
--	--	------	--------	--

+43				
-----	--	--	--	--

		6.40	946.52	
--	--	------	--------	--

30 MAR 1971

LT

E

RT

x42

48.46	48.47	48.3	47.9	48.1	47.7	48.1	48.5
4.46	4.45	4.6	5.0	4.8	5.2	4.8	4.4
50	46	29	23	✓	26	43	60
	SW						

TOP ROCK 51' LT 54+00

TOP HYD. N.W. COR. SANDHURST

48.32	48.11	47.5	48.0	47.3	47.7	48.1
4.95	5.16	5.8	5.3	6.0	5.6	5.2
60	47	22	✓	20	32	60
	conc.					

SD 22' LT

MH 26' RT

STA	+	π	-	ELEV.
		7		
		953.2X		

55 + 58 = GUTTER LT (S)

✓

+63

5.93 947.34

+69

6.55 946.72

+71 = $\neq$ SANDHURST LT

+89 = GUTTER LT (N)

X-43

✓	✓	✓	✓	✓	✓	✓	✓	✓	
27.5	27.52	27.8	27.7	27.5	27.6	26.9	27.4	27.6	
5.8	5.75	5.5	5.6	5.8	5.7	6.4	5.9	5.7	
150	118	60	44	16	✓	24	29	60	
	MH				✓				
27.3	27.4	27.1	26.99	27.4	27.5	27.0	27.3	27.1	27.3
6.0	5.9	6.2	6.28	5.9	5.8	6.3	6.0	6.2	6.0
200	100	60	54	14	✓	21	28	37	60
			CB						

STA + Δ - ELEV.

953.27

56+00

BM 0.22 950.88 2.62 950.65 (950.66)

57+00

✓

58+00

✓

LT

30 MAR 1971

RT

x-44

7.9	8.1	7.4	6.9	7.1	7.5	7.1	6.9	6.9	7.4
5.4	5.2	5.9	6.4	6.2	5.8	6.2	6.4	6.4	5.9
60	58	33	26	14	✓	18	24	33	60

TOP HYD. NW COR SAND TURST

5.7	4.9	5.6	6.0	6.3	5.9	5.8	6.4
5.7	6.0	5.3	4.9	4.6	5.0	5.1	4.5
33	26	21	13	✓	16	22	60

5.7	5.5
5.6	5.4
50	60

4.3	3.8	3.1	4.3	4.5	4.8	4.4	4.1	4.6	5.3
6.8	7.1	7.8	6.6	6.4	6.1	6.5	6.8	6.3	5.6
37	31	25	19	12	✓	16	24	31	60

4.3
6.6
60

STA

+

K

-

ELEV

950.88

58+14

7.00 / 943.88

+22

7.25 943.63

+30

✓

+33

59+00

✓

LT

E

30 MAR 1971

RT

x-45

MH---24' RT

S.D---28' RT

x 4.0	x 3.9	x 3.8	x 4.0	x 4.3	x 4.0	x 4.2	x 4.2	x 4.1
6.9	7.0	7.1	6.9	6.6	6.9	6.7	7.0	6.8
60	29	21	12		16	24	34	47

x 4.1
6.8
60

x 4.0	x 3.9	x 3.8	x 4.0	x 4.3	x 4.0	x 4.0	x 3.3	x 3.0
6.9	7.0	7.1	6.9	6.6	6.9	6.9	7.6	7.9
60	29	21	12		15	26	32	60

x 4.0	9.0-7.7	x 1.8	x 2.8	x 3.2	x 2.8	x 3.1	x 2.5
9.9	10.11	9.1	8.1	7.7	8.1	7.8	8.4
60	53	31	11		16	30	60
	CB						

10.0
100

STA + T - ELEV.

950.88

59+16 GUTTER LT. & LAURIE RD-LT

+30 GUTTER LT.

✓

3M 0.80 945.14 6.54 944.34 (944.34)

60+00

✓

LT

E

30 MAR 1971

R7

x-46

$\Delta 1.06$	$\Delta 1.3$	$\Delta 1.8$	$\Delta 2.6$	$\Delta 3.0$	$\Delta 2.6$	$\Delta 2.8$	$\Delta 3.5$	$\Delta 3.7$
9.82	9.6	9.1	8.3	7.9	8.3	8.1	17.4	11.6
100	60	38	12	✓	16	27	42	60

$\Delta 0.8$	$\Delta 0.77$	$\Delta 1.3$	$\Delta 2.5$	$\Delta 2.8$	$\Delta 2.3$	$\Delta 2.2$	$\Delta 3.0$	$\Delta 3.8$
10.1	10.1	9.6	8.4	8.1	8.6	8.7	11.9	12.5
60	54	35	12	✓	16	26	40	60
	CB							

$\Delta 0.8$	$\Delta 0.7$
10.1	10.2
100	150

TOP HYD. NW CORNER LAURIE

$\Delta 1.0$	$\Delta 3.3$	$\Delta 3.5$	$\Delta 1.5$	$\Delta 1.4$	$\Delta 1.7$	$\Delta 1.2$	$\Delta 1.0$	$\Delta 3.8$	$\Delta 3.0$
4.1	5.8	5.6	3.6	3.7	3.4	3.9	4.1	7.3	8.1
38	30	25	21	12		16	25	36	60

$\Delta 1.9$
3.2
50
FE

STA

+

π

-

ELEV.

945.14

60+84

61

+48

✓

+58

GUTTER RT.

✓

LT

30 MAR 1971

RT x-47

x0.71	x0.70	x0.5	x0.6	x0.9	x0.4	x0.0	x3.9	x2.1
4.43	4.44	4.6	4.5	4.2	4.7	5.1	11.2	12.0
60	53	34	14	17	27	42	60	
COND ENT.	COND ENT.							

x0.9	x0.6	x0.4	x0.5	x0.8	x0.3	x0.1	x3.9	x2.7
4.2	4.5	4.7	4.6	4.3	4.8	5.0	11.2	12.4
60	52	28	13	17	28	43	60	

x0.7	x0.7	x0.4	x0.4	x0.8	x0.2	x3.8	x3.7	x3.9
4.4	4.4	4.7	4.7	4.3	4.9	6.3	10.4	11.2
60	47	32	17	19	37	53	60	

A
 3.5
 11.7
 100

x0.5	x0.3	x0.2	x0.5	x0.8	x0.2	x3.9	x3.6	x5.6
4.6	4.8	4.9	4.6	4.3	4.9	6.2	8.5	9.5
60	50	38	17	18	34	60	100	82

5.1
 10.0
 100

STA	+	π	-	ELEV.
-----	---	---	---	-------

		945.14		
--	--	--------	--	--

61+70	±	SHERREN		
-------	---	---------	--	--

✓				
---	--	--	--	--

+75				
-----	--	--	--	--

		4.74		
--	--	------	--	--

			940.40	
--	--	--	--------	--

+80				
-----	--	--	--	--

		GUTTER RT		
--	--	-----------	--	--

62				
----	--	--	--	--

✓				
---	--	--	--	--

LT

30 MHR 1971

RT

x-48

x0.3	x0.5	x0.5	x0.7	x0.2	39.86	37.6	36.8
4.8	4.6	4.6	4.4	4.9	5.28	7.5	8.3
60	31	19		21	27	50	60

5.2	5.8
9.9	9.3
100	80

MH 24' LT

x0.3	x0.5	x0.5	x0.7	x0.3	38.5	36.8	35.4
4.8	4.6	4.6	4.4	4.8	6.6	8.3	9.7
60	32	17		19	40	60	100

x0.3	x0.5	x0.4	x0.7	x0.3	x0.0	39.5	36.7
4.8	4.6	4.7	4.4	4.8	5.1	5.6	8.4
60	32	18		19	26	38	45

36.0
9.1
60

STA	+	π	-	ELEV.
-----	---	-------	---	-------

STA	+	π	-	ELEV.
		945.14		

STA	+	π	-	ELEV.
62+27				

STA	+	π	-	ELEV.
				GUTTER LT.

STA	+	π	-	ELEV.
+39				

STA	+	π	-	ELEV.
		4.89		940.25

STA	+	π	-	ELEV.
+45				

STA	+	π	-	ELEV.
+59				

STA	+	π	-	ELEV.
				GUTTER LT.

STA	+	π	-	ELEV.
+74				

STA	+	π	-	ELEV.
+87				

LT

30 MAR 1971

RT

X-49

39.5	39.7	39.61	40.2	40.5	40.8	40.6	40.2	37.2	36.8
5.6	5.4	5.53	4.9	4.6	4.3	4.5	4.9	7.9	8.3
100	60	35 CB	39	19		19	34	48	60

M.H 33' LT.

39.7	39.9	40.10	40.2	40.5	40.8	40.5	40.2	37.2	37.2
5.4	5.2	5.04	4.9	4.6	4.3	4.6	4.9	7.7	7.9
100	75	55	40	19		20	38	50	60

M.H.

39.4	39.5	39.56	40.0	40.5	40.8	40.5	40.0	37.1	36.8
5.7	5.6	5.58	5.1	4.6	4.3	4.6	5.1	8.0	8.3
100	75	55	37	21		21	39	52	60

CB

40.6	40.6	41.0	40.2	40.6	40.8	40.4	40.1	37.6
4.5	4.5	4.1	4.9	4.5	4.3	4.7	5.0	7.5
60	50	39	35	19		23	46	60

42.3	42.2	40.5	40.6	40.8	40.5	40.5	40.6
2.8	2.9	4.6	4.5	4.3	4.6	4.6	4.5
60	50	38	20		21	47	60

STA + π - ELEV.

945.14

63+00

+50 = End Median

+80

✓

64+00

✓

+21

LT

30 MAR 1971

RT

x-50

$\times 2.5$ $\times 2.3$ $\times 0.4$ $\times 0.4$ $\times 0.9$ $\times 0.5$ $\times 0.6$ $\times 0.8$
 2.6 2.8 4.7 4.7 4.2 4.6 4.5 4.3
 60 51 40 23 22 43 60

$\times 3.8$ $\times 0.4$ $\times 0.5$ $\times 1.06$ $\times 1.41$ $\times 1.08$ $\times 0.11$ $\times 0.20$ $\times 0.1$
 6.3 4.7 4.6 4.08 3.73 4.06 5.03 4.94 6.0
 38 32 25 2 2 29 29 40

$\times 3.0$
 2.1
 60

$\times 0.6$
 4.5
 60

$\times 3.1$ $\times 0.3$ $\times 0.5$ $\times 0.9$ $\times 1.40$ $\times 1.03$ $\times 0.4$ $\times 0.94$ $\times 0.94$ $\times 0.7$
 6.0 4.8 4.6 4.2 3.74 4.11 4.7 5.30 5.15 5.9
 38 31 29 2 2 22 38 38 53

$\times 3.2$ $\times 3.3$
 1.9 1.8
 51 60

$\times 7.93$
 7.21
 64
 50

$\times 3.5$ $\times 0.2$ $\times 0.5$ $\times 0.6$ $\times 1.02$ $\times 1.40$ $\times 1.02$ $\times 0.5$ $\times 0.0$ $\times 0.40$
 6.6 4.9 4.6 4.5 4.12 3.74 4.12 4.6 5.1 5.65
 40 32 25 21 2 2 23 43 60
 CB

$\times 3.2$ $\times 3.3$
 1.9 1.8
 53 60

STA	+	Δ	-	ELEV.
-----	---	----------	---	-------

		945.14		
--	--	--------	--	--

64+50				
-------	--	--	--	--

+75				
-----	--	--	--	--

		4.82	940.32	
--	--	------	--------	--

		6.02	939.12	
--	--	------	--------	--

				939.11
--	--	--	--	--------

30 MAR. 71

LT

£

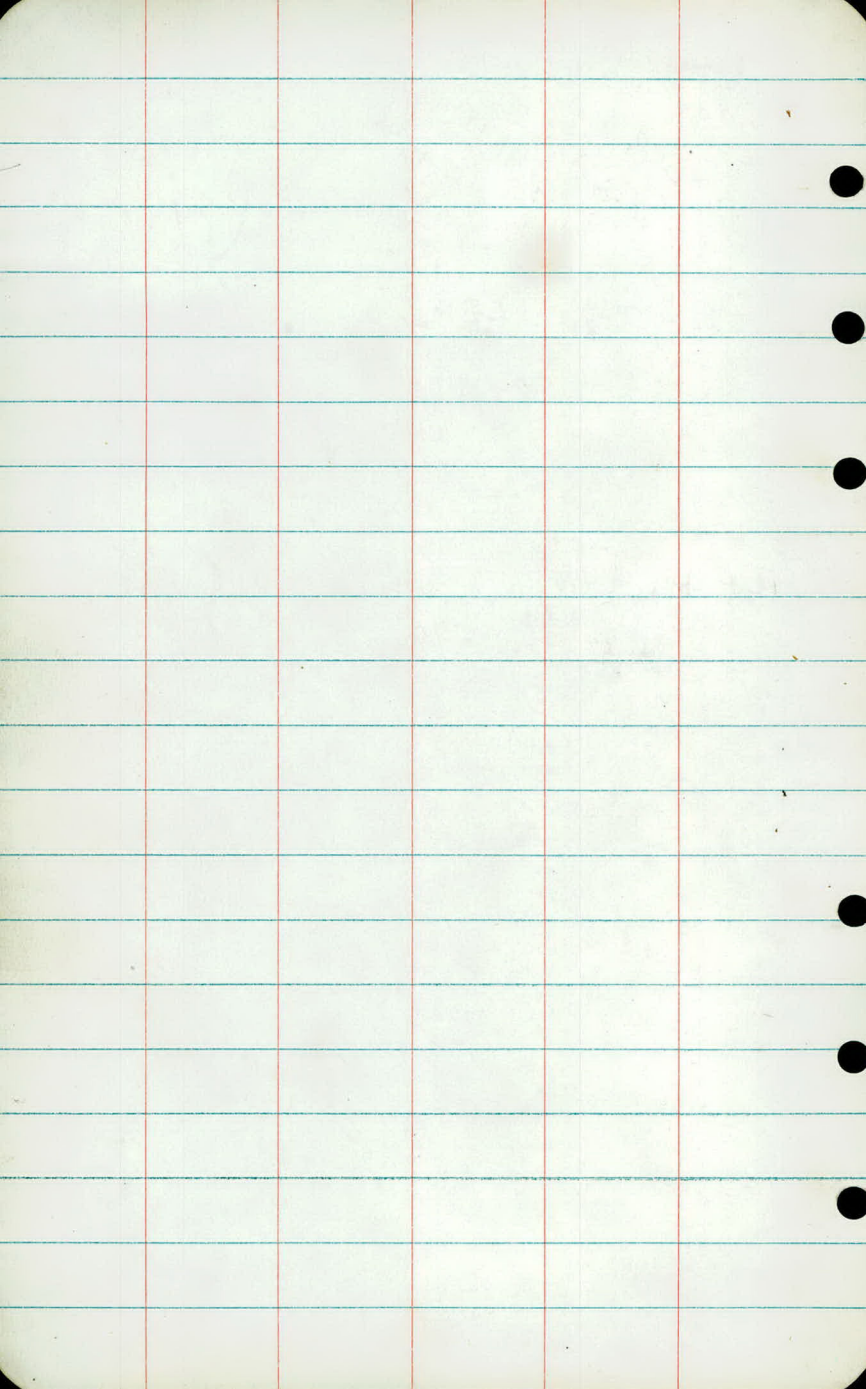
RT

X-51

57.03	39.9	40.5	41.18	41.48	41.24	39.53	41.00	40.9
8.11	5.2	4.6	3.96	3.66	3.90	5.61	4.14	4.2
50	38	25	2		2	27	27	60
SD							TOP CURB	

CB 48' RT
50'

TOP HYD. NE CORNER SHERREN ST.



MH & CB Elevations

C.B.'s
M.H.'s

Sta + π - Elev

B.M. 3.66 948.77 945.11

M.H. #43 4.34 944.43

M.H. #45 6.68 942.09

FP. CLOSE 2.53 946.24

B.M. 1.52 946.63 945.11

M.H. #55 5.56 941.07

CLOSE 3.52 943.11

B.M. 2.31 948.15 945.84

M.H. #60 5.53 942.62

CLOSE 4.65 943.50

B.M. +1.15 948.57 947.42

M.H. #76 5.08 943.49

CLOSE 4.43 944.14

HYD N.W. COR. SUMMER ST

STA 17+⁹⁷90 LT ²¹35' ±

STA 18+45 RT 50'

STA 18+00 ±

HYD N.W. COR. ~~AUTUMN~~ SUMMER

STA 21+30 RT 30'

STA 22+00 ±

HYD N.W. COR. AUTUMN

STA 23+40

STA 24

HYD N.E. COR. ROSELAWN 26

STA 26+75 LT

STA 27+00 ±

	+	π	-	
B.M.	2.98	950.14		947.16
M.H.	#82		7.19	942.95
M.H.	#89		6.91	943.23
M.H.	#93		5.12	945.02
C.B.			5.68	944.26
close			5.32	944.83

B.M.	1.44	953.54		952.10
M.H.	#93		8.57	944.97
M.H.	#103B		7.72	945.82
M.H.			6.90	946.64
Close			4.02	949.32 ✓

B.M.	2.25	956.60		954.35
M.H.	#129		6.20	950.40
CLOSE			3.55	953.05

HyD Sta 29+70

Sta 29+20 $\pm$

30+20 $\pm$

31+50 $\pm$

31+50 $\pm$

Sta 29+00 $\pm$

HyD NW CORNER SNRYER

Sta 31+50 $\pm$ LT 30

33+25 $\pm$ LT 30

34+50 $\pm$ LT 30

Sta 36+00 $\pm$

HyD NW CORNER SKILLMAN

39+80 $\pm$ LT.

41+00 $\pm$

+

K

-

B.M.	0.81	956.88	956.07
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C.B.		6.13	950.75
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M.H.	#150	5.01	951.87
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C.B.	#151	7.02	949.86
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CLOSE		4.64	952.24
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B.M.	1.99	946.33	944.34
------	------	--------	--------

M.H.	#197	2.96	943.37
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close		3.15	943.18
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HYD N.E. CORNER PARKER

Sta 45+70[±] LT

Sta 46+00[±] LT

Sta 46+50[±] LT.

Sta 46+00 ϕ

N.W. CORNER LAURIE

Sta 58+22[±] LT 23

Sta 59+00

$$STA + \pi - ELEV.$$

62-651-01

Sta	+	π	-	Elev.
BM	1.64	939.28		937.64
5+24	MH	475' Lt	5.78	933.50
5+00	E		4.11	935.17 935.26
BM	0.28	948.96		948.68
13+28	MH	25' Lt	4.37	944.59
12+90	MH	Lt 34'	5.67	943.29
13+00	E		4.61	944.35
BM	2.78	948.62		945.84
23+34	MH	20' Lt	5.91	942.71 ✓
23+38	CB	27' Rt	7.24	941.38 ✓
28+10	MH	21' Lt	4.73	943.89 ✓
28+17	CB	29' Lt	6.09	942.53 ✓
28+09	CB	25' Rt	7.25	941.33 ✓
BM			1.19	947.43 947.42

FK
LPD
KG
DK

April 19, 1971
Cloudy 70

5

Top Hyd by Sta 5+00⁺

Top Hyd NW Corner Garden

Top Hyd NW Corner

Top Hyd NE Corner Roselawn & Lexington

BM 4.09 956.19 952.10

36+31 MH 17' RT 6.78

39+13 MH 50' RT 5.12

BM 1.83 954.36 954.35

BM 2.18 958.25 956.07

45+91 MH 23' LT 6.35 951.90

46+38 SD 22' LT 8.30

46+00 £ 6.00 952.25

BM 2.65 946.99 944.34

58+09 Apron 23' LT 4.57

58+22 MH 21' LT 3.64

59+08 MH 55' LT 5.75

59+09 MH 24' LT 4.85 942.14

59+00 £ 3.83 943.16 ✓

61+71 MH 26' RT 7.20