

OFFICE OF COUNTY ENGINEER
RAMSEY COUNTY, MINN.

PLAN Survey

CLEVELAND AVE.

From C. Rd. "C" To C. Rd. "D"

Road Acc't. No. 46

Date Filed _____ File 13-45

R.G
LPD
DS
J.A.

April 15, 1976.
P.C. 70°

1

ALINEMENT OF

CLEVELAND AVE

FROM

Co Rd "C" to Co Rd "D"

105+16.05 POT 0°20'

R.G.
LPD
J.A.
D.S.

April 15, 1976
P.C. 70°

2

RLS side tie

⊥

42.82

N.E. Cor "C2"

⊥ Top Hyd.

Co. Rd.

⊥

41.99

"C2"

C.I. Mont

40.77

39.57

⊥

RLS side Tie

⊥

RLS side Tie

Co. Rd.

⊥

"C"

C.I. MONT.

Sta	Point	DLT	ARt	Defl
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(160+60.40) R				
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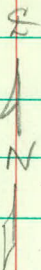
^M 160+59.93 POT				
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			1°04'	
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RG
LPD
JA
DS

Apr. 15, 1976
P.C. 75'

3



Top Hyd.

N.W. COR



57.27'

90°06'

90°06'

CO 122



"D"

C.E. Mont

90°58'

88°50'

90.27'

62.24'

3 NAILS
P.P.



Top Hyd
S.E. COR



DIETZEN NO. 384-B

GA
RJ

4-15-76
CLOUDY 66°
1

CLEVELAND AVE.

FROM

CO. RD "C" TO CO. RD. "D"

BENCH LEVELS

STA	+	∇	-	ELEV
BM	1.22	923.19		921.97
TP	3.65 2.96 2.27	919.43	7.24 6.72 6.19	916.47
TP	1.01 0.05 —	916.93	3.08 2.55 2.02	916.88
TP	2.98 1.56 ^s 0.15	913.96 ^s	5.57 4.53 3.49	912.40
TP	5.12 4.34 3.56	913.38 ^s	6.07 4.92 3.77	909.04 ^s
TP	3.09 2.01 ^s 0.94	911.67 ^s	4.53 3.72 ^s 2.92	909.66
TP	6.91 6.16 ^s 5.42	915.41	3.84 2.43 1.02	909.24 ^s
TP	3.58 2.45 1.31 ^s	908.64	10.47 9.22 7.97	906.19
TP	5.28 4.27 ^s 3.27	910.33 ^s	3.73 ^s 2.58 1.42	906.06

GA
RJ

4-15-76
CLOY 66°

DESCRIPTION

By Railroad tracks

ROSEVILLE B.M. #173

200' SO. "C" on SE cor

NE NUT OF Signal base SW cor Co Rd C

HYD. (TOP NUT) AT AMOCA STATION 200' NO. Co Rd C

TOP NUT HYD IN FRONT OF CUMMINS

TOP NUT HYD AT ENT TO DOHRN TRANS. CO.

TOP NUT HYD SO. ENT. TO MIDWEST TRANS. CO.

TOP NUT HYD IN FRONT OF AMERICAN
SO. ENT

TOP NUT HYD AT NO. ENT TO AMERICAN

TOP NUT HYD NE COR CO. RD C²

STA	+	K	-	ELEV
		910.33 ^s		
TP	4.50 ^s 3.50 ^s 2.50 ^s	910.38	4.48 ^s 3.46 2.43	906.87 ^s
TP	5.22 ^s 4.09 2.96	912.57	2.84 ^s 1.90 0.95 ^s	908.48
TP	4.60 3.49 2.38	914.01 ^s	3.03 2.04 ^s 1.06	910.52 ^s
TP	3.74 2.76 ^s 1.79	912.14	5.72 4.64 3.56	909.37 ^s
TP	8.00 ^s 6.76 5.52	916.46 ^s	3.47 2.43 ^s 1.40	909.70 ^s
TP	2.85 2.39 ^s 1.94	917.81	2.06 1.05 0.04 ^s	915.41 ^s
TP	6.75 5.98 ^s 5.22 ^s	920.74 ^s	3.60 ^s 3.05 2.49	914.76
TP	3.56 2.56 1.56	921.00	3.28 ^s 2.30 ^s 1.33	918.44
TP	3.50 2.91 ^s 2.33	917.67 ^s	6.97 6.24 5.51	914.76

GA
RJ

4-15-76
CLOUDY 66
3

DESCRIPTION

TOP NUT HYD. 500' NO OF C² EAST SIDE

TOP NUT HYD AT 50. ENT. TO DATA GRAPH INC

TOP NUT HYD AT HOUSE NO. 2996

TOP NUT HYD 125' / NO OF H₀ # 3010

TOP NUT HYD IN FRONT OF H₀ # 3060

TOP NUT HYD AT H₀ # 3090

NE COR BOTTOM STEP H₀ # 3095

TOP NUT HYD NW COR COR D

NE COR BOTTOM STEP H₀ # 3095

STA	+	K	-	ELEV	
TP	2.18 ^s 1.18 ^s 0.18	916.60	2.71 ^s 2.26 1.80	915.41 ^s	
TP	3.47 2.42 1.36 ^s	912.12	8.14 6.90 5.65	909.70	909.70 ^s
TP	6.01 ^s 4.84 ^s 3.67 ^s	914.22 ^s	3.69 2.74 1.79	909.38	
TP	2.74 ^s 1.70 ^s 0.67	912.24 ^s	4.67 3.68 ^s 2.70	910.54	
TP	3.12 ^s 2.02 ^s 0.92 ^s	910.52	4.81 3.75 2.69	908.49 ^s	
TP	4.59 ^s 3.54 ^s 2.50	910.44	4.47 ^s 3.62 ^s 2.77	906.89 ^s	
TP	2.10	908.18	5.35 4.36 3.37	906.08	
TP	3.07	909.26	1.99	906.19	
TP	2.32 ^s	911.54 ^s	0.04	909.22	

GA.
RJ

4-15-76
cloudy 75°
4

DESCRIPTION

TOP NUT ^{HYD} AT Ho # 3090

TOP NUT ^{HYD} AT Ho # 3060

TOP NUT HYD AT 125' No OF Ho # 3010

TOP NUT HYD AT Ho # 2996

TOP NUT HYD AT SO. ENT. TO DATA GRAPH INC

TOP NUT HYD 500' No OF C² EAST SIDE

TOP NUT HYD NE COR CO. RD C²

TOP NUT HYD AT NO. ENT TO AMERICAN

TOP NUT HYD AT SO. ENT TO AMERICAN

STA	+	π	-	ELEV.
		911.54 ^s		
TP	1.75	911.38 ^s	1.91	909.63 ^s
TP	3.86	912.87	2.37 ^s	909.01
T.P	4.97	917.36 ^s	0.48 ^s	912.39 ^s
T.P	3.21	920.10 ^s	0.47	916.89 ^s
T.P	5.99	922.47	3.62 ^s	916.48
Bm			0.49	921.98

TOP HYD SQ. ENT TO MIDWEST

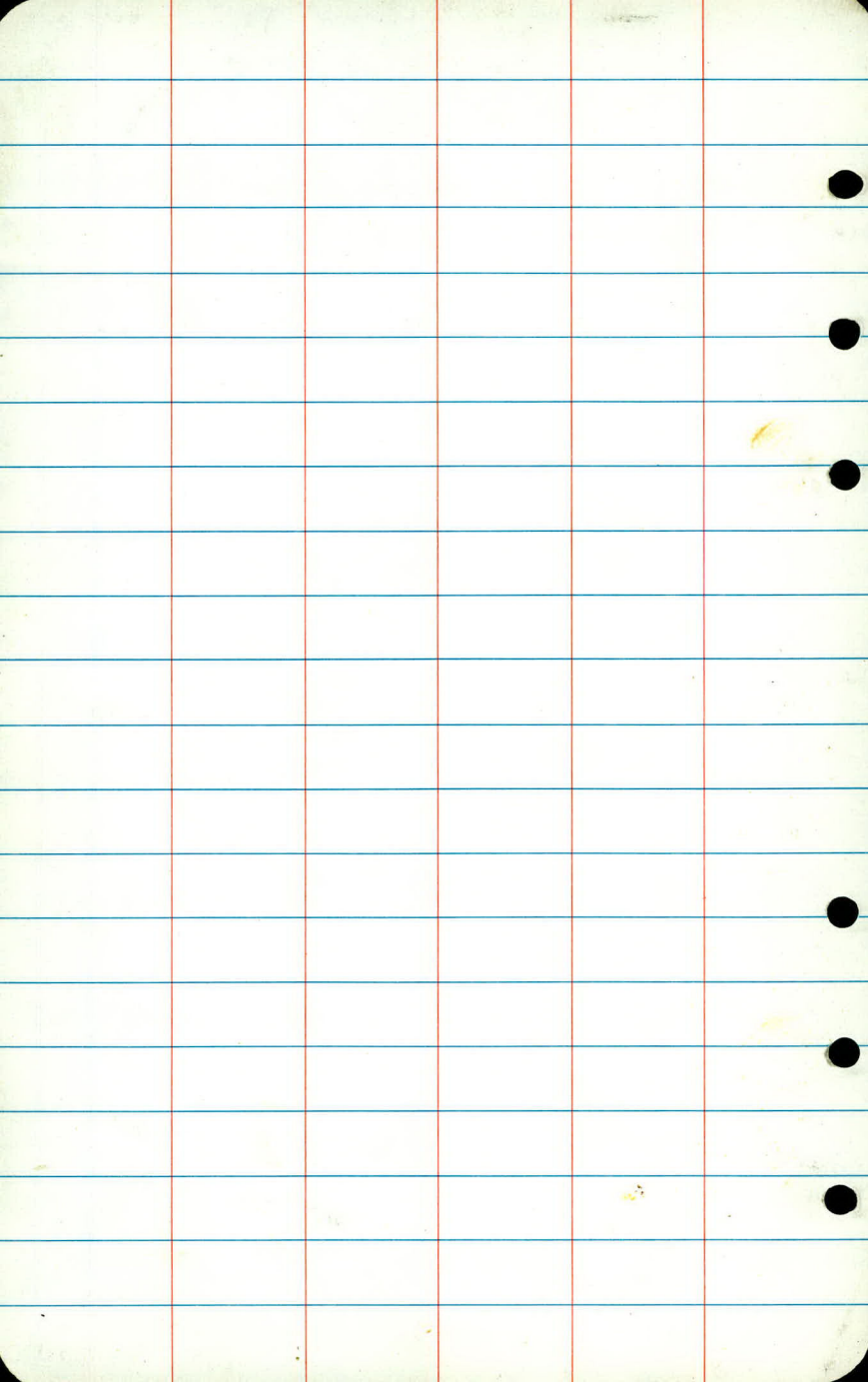
TOP HYD AT DOBBS TRAWS. CO.

TOP HYD IN FRONT OF CUMMINS

TOP HYD AT AMOCO STATION 200' N CO. RD "C"

NE OUT OF SIGNAL BASE SW CORNER "C"

ROSEVILLE B.M. [#]173



TOPOGRAPHY
CLEVELAND
AVE

CO. RD "C"
TO
CO. RD "D"

+50

LT.

E

RT

+24 $\frac{PP}{31}$ +19 $\frac{2" PIPE}{76}$ +32 $\frac{ERAD}{63}$ +08 $\frac{BG RAD}{41}$ +21 $\frac{P.O.R.}{46}$

108

FE RD
42 25MED
8-14CURB
41+89 $\frac{4" MAPLE}{75}$ +60 $\frac{MED}{12-18}$ +69 $\frac{ERAD}{41}$ +59 $\frac{PP}{79}$ +52 $\frac{P.O.R.}{50}$

+50

FE RD
42 25+46 $\frac{BG RAD: 82 CONC CURB}{68-79}$ +16 $\frac{ERAD}{68}$ +14 $\frac{86 CONC CURB}{80}$ +02 $\frac{FLUX PIPE}{86}$ +12 $\frac{P.O.R.}{53}$

107

FE RD
42 25MED
12-18P.O.R.
42W.S.O.
81+91 $\frac{86 RAD}{41}$ +75 $\frac{ERAD}{41}$ +72 $\frac{AND}{75}$ +54 $\frac{E CONC CURB}{26}$ +58 $\frac{P.O.R.}{50}$ +50 $\frac{FE 5' CHAIN LINK}{42}$ +53 $\frac{CONC CURB}{82}$ +53 $\frac{BG RAD}{64}$

106

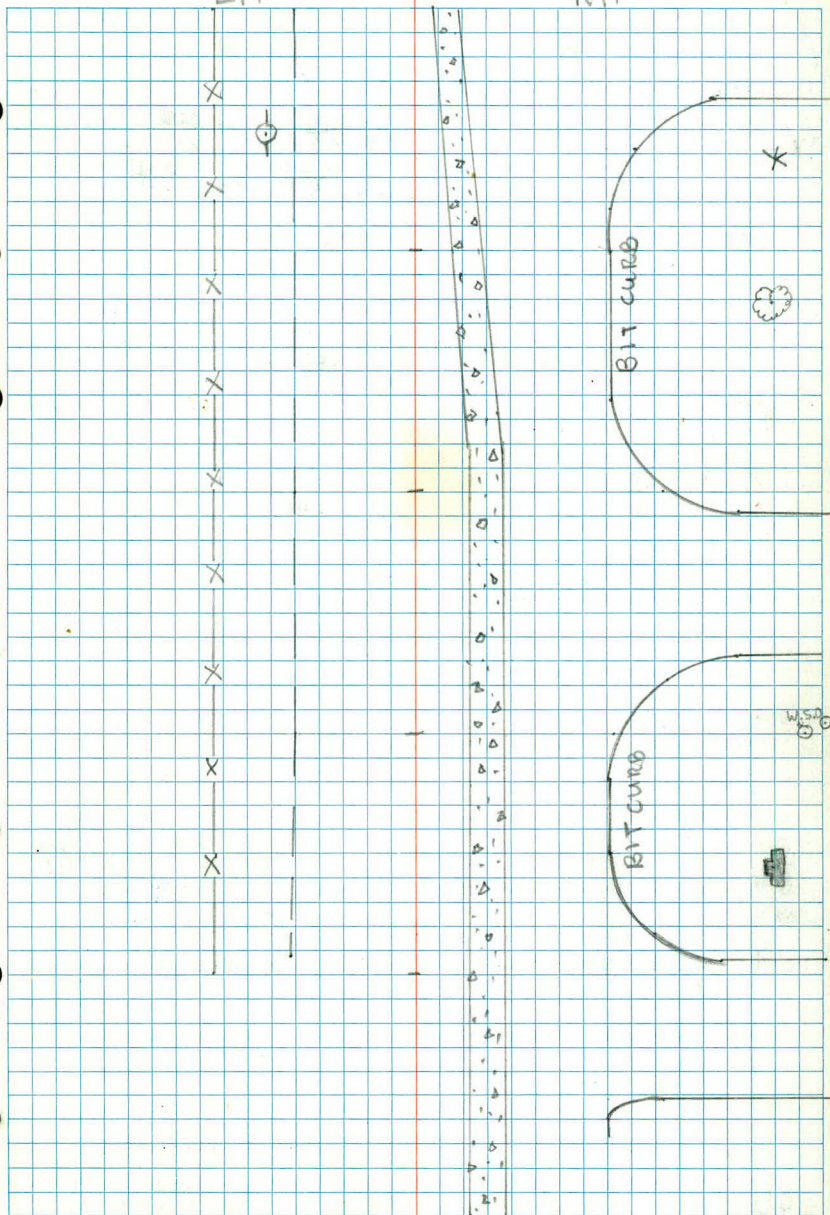
MED
12-18+24 $\frac{E CONC CURB}{52}$ +24 $\frac{BG BIT CURB}{52-82}$ +20 $\frac{CONC CURB}{41}$

W.S
G.A
B.J

19 APRIL 76 2
SUNNY: 61°
RT.

LT.

E



111

LT

+95 CB 96 ✓

E

RT

+93 ^{CB} 63 +95 ^{ERAD} 85 +95 ^{B6 CONC PAGE} 85 ✓+98 ^{B6 RAD} 40 ✓+83 ^{42" CONC SPWD} 77 ✓+81 ^{B6 CONC CHRS} 33 ✓+89 ^{CHRS} 48 ✓+67 ^{EMED (NOSE)} 2.5 ✓+74 ^{P.O.R} 37 +74+67 ✓ ^{12" CMP APPRO}+76 ^{12" CMP APPRO} 96 ✓+57 ^{MH} 30 ✓+63 ^{B6 RAD} 28 ^{E FE 5} 43 ^{CRAINLINK}+52 ^{W.S.O} 52 ✓+52 ^{HYD} 49 ✓

+50

+27 RD 25 ✓+32 ^{BELL TEL BOX} 58 ✓+03 ^{LP} 31 ✓

110

FE RD 42 25MED ¹ MED ⁵

RD BITCHUB 40

+50

FE 42

RD 25

MED 1

MED 5

+24 ^{P.O.R} 48+43 ^{ERAD} 40+10 ^{MH} 36+20 ^{B6 RAD} 62-100+

109

FE 42

RD 25

MED 1

MED 5

+77 ^{B6 RAD} 41+82 ^{BUSHES (5)} 71+83 ^{MED} 0-6+72 ^{ERAD} 41+66 ^{15 APPRO} 65+64 ^{P.O.R} 45+66 ^{SURFACE DRAIN} 43+61 ^{B6 RAD} 60+61 ^{B6 BIT} 60-100+

108 +50

+88 ^{P.O.R} 45+93 ^{ERAD} 57-100+

W.S
G.A
B.T

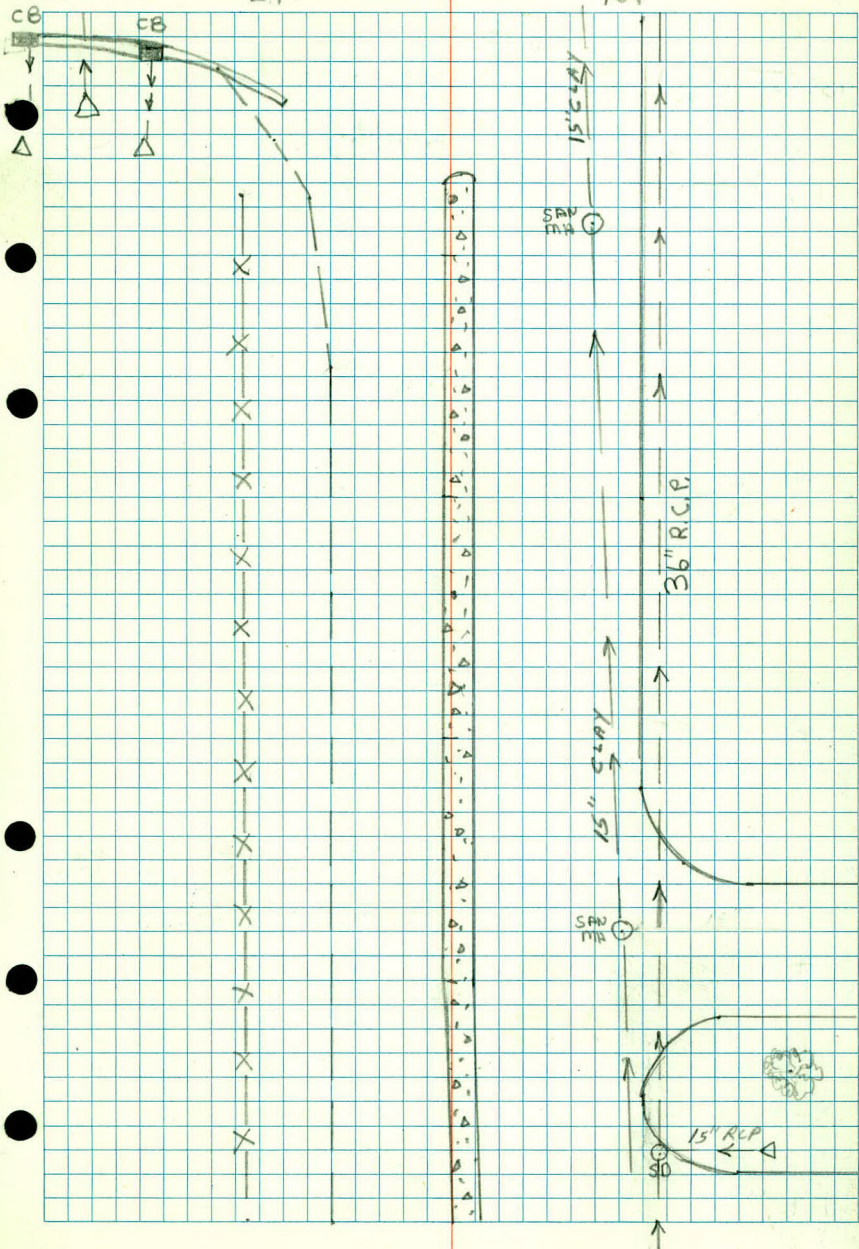
LT

L

19 APRIL 76
SUNNY 62°

3

RT



+50	RD LT 12	Swamp 37 PP +44 25 ✓	RT BIT CURB 27
+35	$\frac{6''}{39}$ 4"	+36 $\frac{8''}{39}$	
+23	$\frac{38}{39}$ ✓		SW CORN BIT SPILLWAY +44 52-92
+07	TW 9" 39 ✓		
113	RD Swamp 12 40	BIT CURB 32	FE 5' CHAIN LINK 92 ✓
+99	$\frac{3-4''}{37}$ ✓		
+85	$\frac{5''}{37}$ ✓		+87 $\frac{FE}{92}$ ✓
+76	$\frac{4'' \text{ ELM}}{42}$ ✓	+77 $\frac{8''}{39}$ ✓	+87 $\frac{NW CORN BLOD}{89}$ ✓
+50			+75 $\frac{CURB}{34}$ ✓
+40	$\frac{MA}{14}$ ✓	+45 $\frac{SWAMP}{44}$ ✓	+65 $\frac{MA}{22}$ ✓
+20	$\frac{E RAD}{12}$	+16 $\frac{PP}{26}$ ✓	+56 $\frac{E RAD}{36}$ ✓
			+43 $\frac{P.O.R.}{41}$ ✓
			+35 $\frac{BG RAD}{55}$ ✓
			+37 $\frac{SW CORNER BLOD}{90}$ ✓
112	+100 $\frac{SWAMP}{61}$ +72 $\frac{5'' \text{ CMP}}{100}$ ✓	+76 $\frac{P.O.R.}{22}$ ✓	+00 $\frac{P.O.R.}{15}$ ✓
+64	$\frac{EXP. CARB}{32}$ ✓	+67 $\frac{ARC RAD}{40}$ ✓	+63 $\frac{36'' \text{ ARCH}}{76}$ ✓
+59	$\frac{GRD POST}{53}$ ✓	+63 $\frac{CONC CURB}{42}$ ✓	+81 $\frac{TELE BOX}{48}$ ✓
+55	$\frac{GRD POST}{87}$ ✓	+54 $\frac{CONC CURB}{55}$ ✓	+81 $\frac{PP}{78}$ ✓
+52	$\frac{CB}{100}$ ✓	+51 $\frac{CONC SLAB i CURB}{88}$ ✓	+79 $\frac{BG RAD}{39}$ ✓
+50	+69 $\frac{CORNER SWAMP}{63}$ ✓		+77 $\frac{BIT CURB}{39}$ ✓
			+75 $\frac{15' \text{ CONC APPROX}}{56}$ ✓
			+70 $\frac{ER}{39}$ ✓
			+74 $\frac{CB (SD)}{42}$ ✓
			+74 $\frac{BIT CHAD}{44}$ ✓
			+54 $\frac{P.O.R.}{45}$ ✓
			+92 $\frac{P.O.R.}{48}$ ✓
			+98 $\frac{E RAD}{59}$ ✓
			+47 $\frac{BG RAD}{59}$ ✓
+34	$\frac{CONC SLAB i CURB}{85}$		
+24	$\frac{MED. ROAD}{40}$	+29 $\frac{CONC CURB}{55}$	
+18	$\frac{CONC. SLAB}{85}$ ✓	+20 $\frac{CONC CURB}{38}$ ✓	+20 $\frac{ER}{63}$ ✓
111			+12 $\frac{P.O.R.}{45}$ ✓

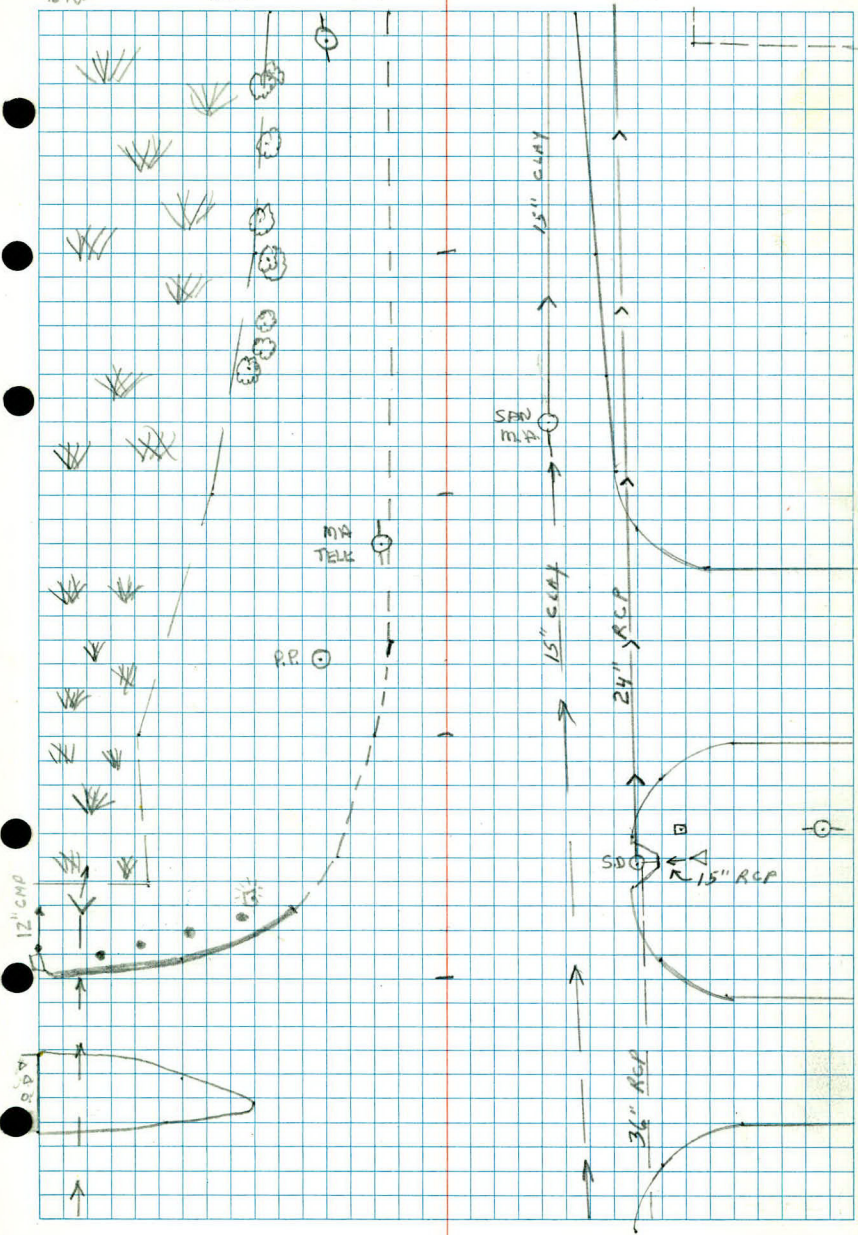
W.S
G.P
R.D
R.W

LT

±

RT

4-20-76
CLEAR 53° 4



116 Swamp ^{LT} RD ✓ RD ✓ RT

45 12 12

+60 W.S.O ✓

49

+59 HYD ✓ +61 ERAO ✓

47 12

+50 Swamp ✓

+43 PP ✓ ⁴⁴ 2-4" willow

26 45 40

+31 4-7" willow ✓

34

+29 2-4" willow ✓

39

+47 P.O.R ✓

15

+34 P.O.R ✓ +34 24" CMP ✓

27 36

+32 B6 RAD ✓

42

115 Swamp ✓ RD ✓

34 12

+87 P.O.R ✓ +91 P.O.R ✓ +95 ERAO ✓

30 35 51

+76 E BIT CURB ✓ +89 24" CMP ✓

22 36

+60 BIT CURB ✓

17

+50 Swamp ✓

32

DISCH (3') ✓

36

+33 E CORNER ✓

92

+30 24" CMP ^{BURIED} ✓ +26 24" CMP ✓

33 33

114 Swamp ✓ RD ✓ BIT CURB ✓ 6' BITCH FF ✓

35 12 26 36 92

+60 24" CORNER ✓ +65 CORN BIT SPILLWAY

43 52-92

113 +50 RD ✓ SWAMP ✓ BIT CURB +54 BIT SPILLWAY ✓

12 37 27 45-52-92

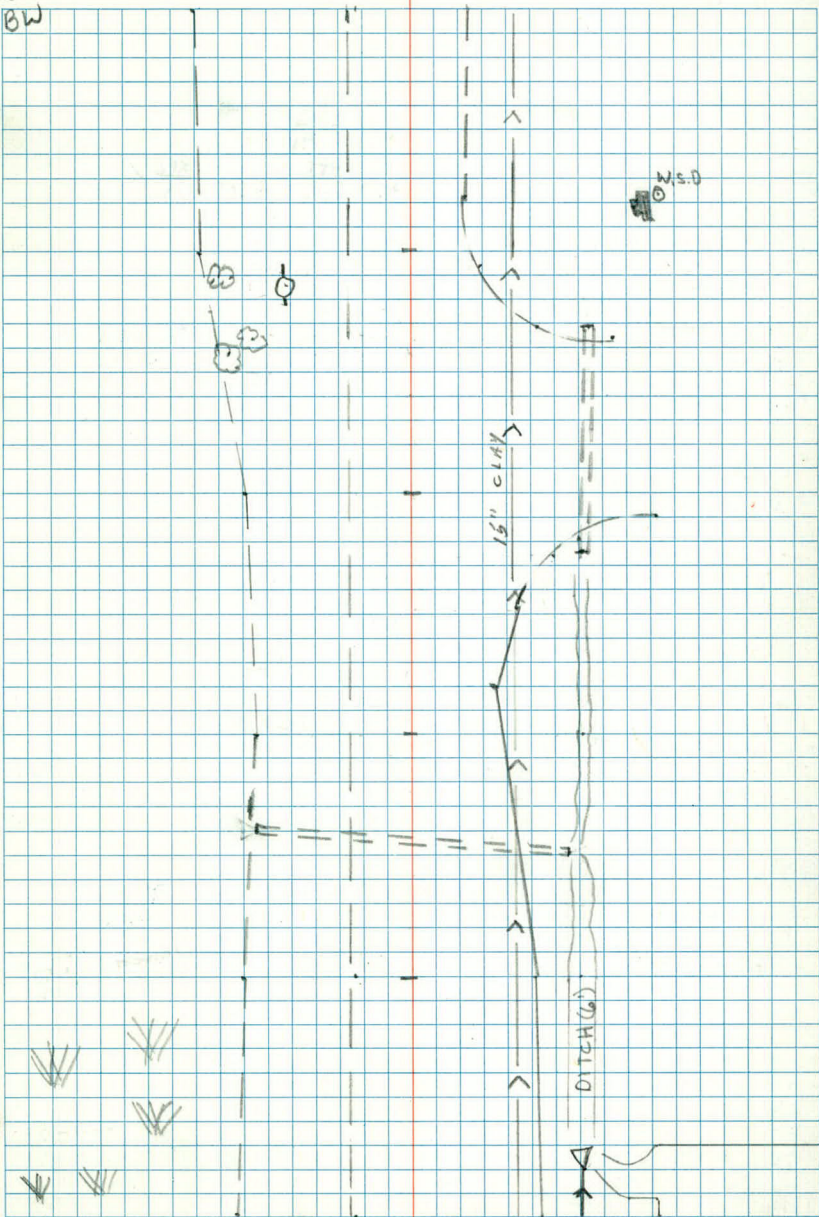
W.S
G.A
B.J
BW

LT

E

RT

4-20-16
CLEAR 34° S



+50

LT

RD
12

E

RT

BIT
66+30 $\frac{\text{BIT}}{46}$ ✓+40 $\frac{\text{BIT}}{55}$ ✓+10 $\frac{\text{BIT}}{33}$ ✓+20 $\frac{\text{BIT}}{38}$ ✓

118

LAKE ✓
100RD ✓
12RD ✓
29+67 $\frac{\text{POR}}{29}$ ✓+78 $\frac{\text{ERAO}}{25}$ ✓+66 $\frac{24 \text{ CMP}}{34}$ ✓+65 $\frac{\text{B6RAO}}{39}$ ✓

+50

+44 $\frac{\text{PP}}{27}$ ✓+16 $\frac{24 \text{ CMP}}{35}$ ✓+22 $\frac{\text{ERAO}}{42}$ ✓+15 $\frac{\text{POR}}{22}$ ✓

117

TILE
 $\frac{\text{M3}}{28}$ ✓RD ✓
12RD ✓
12B6RAO ✓
12+67 $\frac{\text{MM}}{22}$ ✓+54 $\frac{\text{END SWAMP}}{45}$ ✓

+50

116 ✓

SWAMP
45 ✓RD ✓
12RD ✓
12

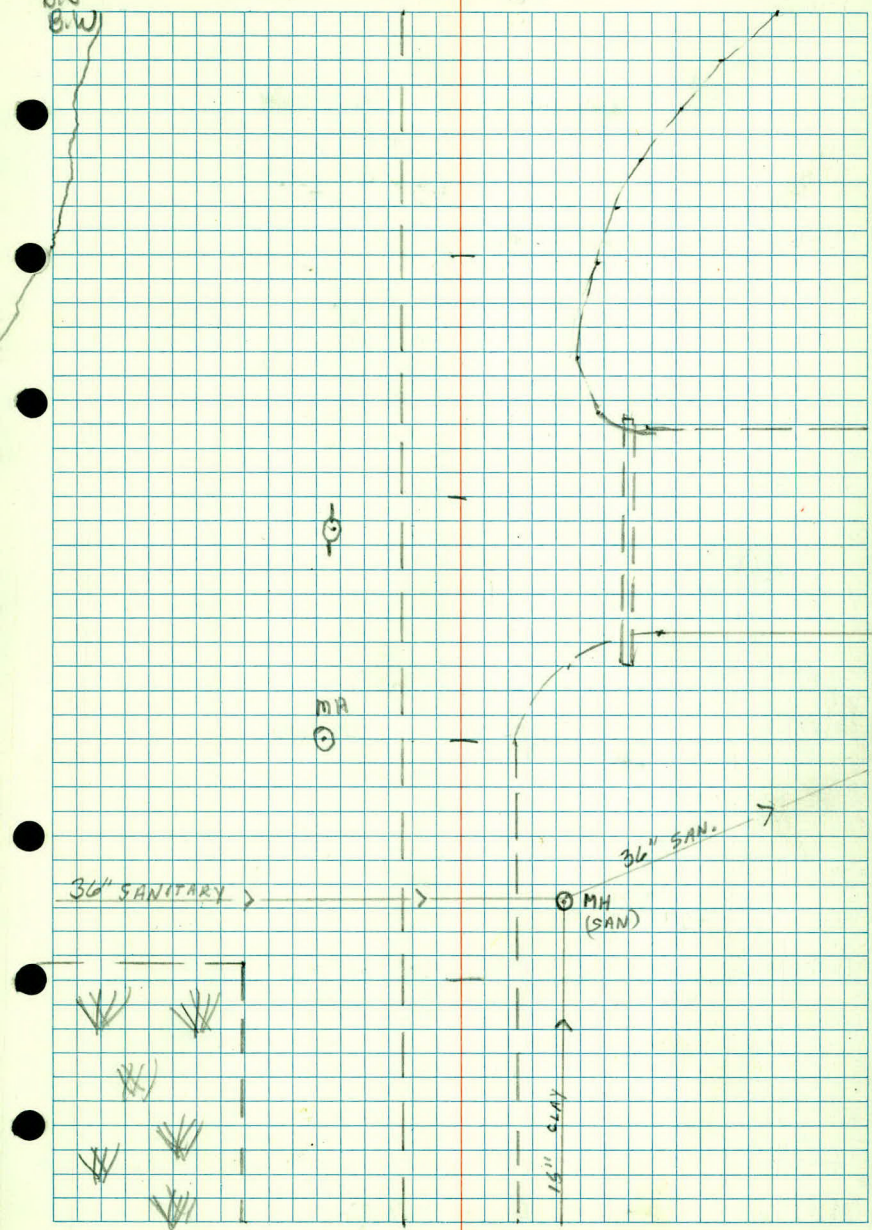
W.S
G.A
B.T
B.W

LT

2

RT

4-20-76
CLEAN: 60° 6



121 Swamp LT
59

RD E RD RT
12 12

+91 Swamp ✓
55

+57 CORRECT LOT ✓
67

+50

+42 Swamp ✓
40

120 SWAMP ✓
45

RD ✓ RD ✓
12 12

PARKING LOT ✓
67

+50

+45 BP ✓
26

+42 11" Elm ✓
40

H²O ✓
59

PARKING LOT ✓
67

+18 Tw 7" ✓
46

+10 2" ✓
44

+13 8" ✓
43

+17 6" ✓
44

+05 13" ✓
50

+07 2" ✓
44

+09 7" ✓
37

+00 SW CORN PARKING LOT ✓
57

119 Lake Swamp ✓
71

RD ✓
12

RD ✓
12

+86 ELM ✓
12

+69 R.O.R. ✓
22

+70 BLT ✓
59

+68 M¹⁴ ✓
14

+62 BLT ✓
44

+65 H¹⁴ ✓
45

+65 BLT ✓
51

118+50

RD ✓
12

+60 BLT ✓
85

+60 BLT ✓
29-40

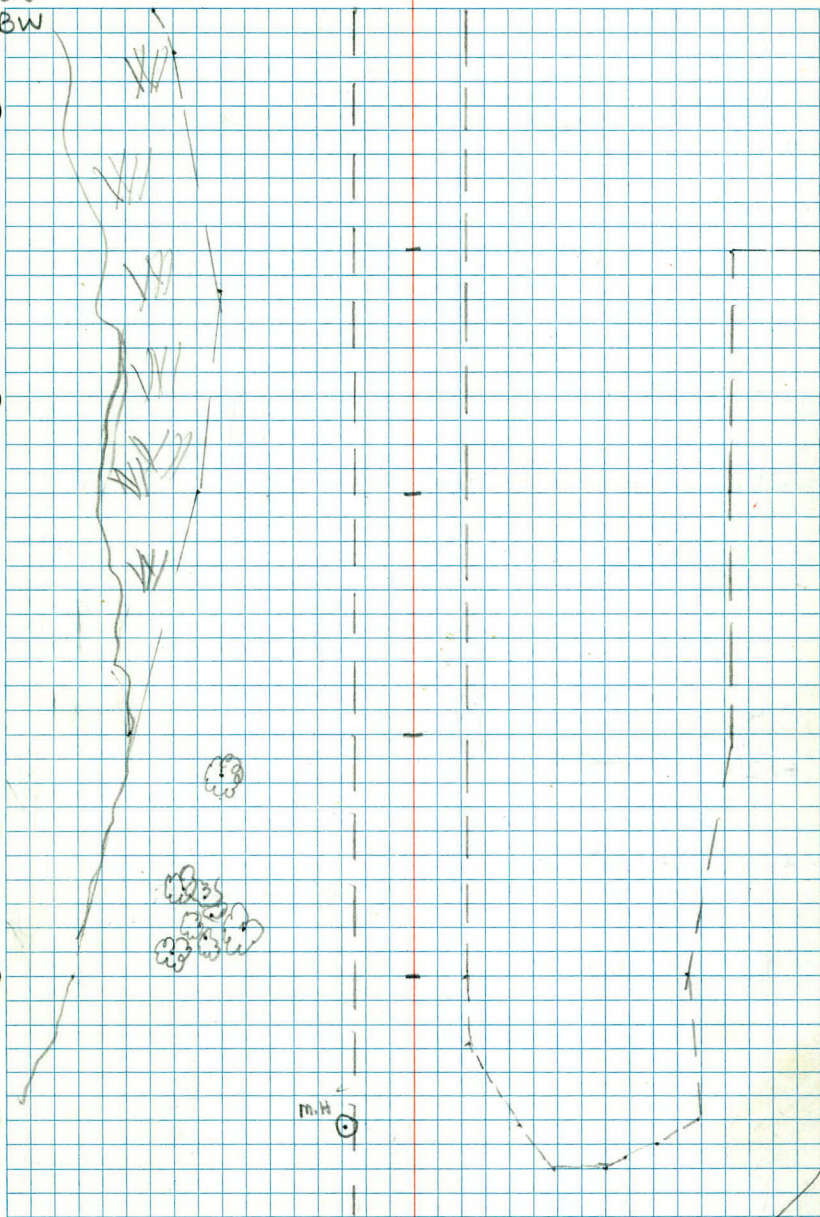
W.S
G.A
B.J
BW

LT

E

RT

4-20-76 →
CLW 11.63



+50

LT

FE ✓ RD ✓
41 13

RT

+47 $\frac{RD}{12}$ +28 $\frac{RP}{27}$ ✓

123

FE ✓ RD ✓ RD ✓
41 13 12+84 $\frac{BIT}{12-22}$ ✓172 $\frac{33" DAK}{59}$ ✓+81 $\frac{SE COR 7' FE}{41}$ ✓+64 $\frac{24" DAK}{47}$ ✓+60 $\frac{E RRD}{22}$ ✓

+50

+48 $\frac{P.O.R.}{26}$ ✓+36 $\frac{12' DIRT ENT}{}$ ✓+34 $\frac{P.O.R.}{36}$ ✓

+28

+28 $\frac{BL RRD}{50}$ ✓

122

+82 $\frac{BELL TALK BUREAU CABLE POST}{32}$ ✓ RD 13+85 $\frac{E RRD}{55}$ ✓+73 $\frac{SWAMP}{97}$ ✓+76 $\frac{P.O.R.}{33}$ ✓+64 $\frac{P.O.R.}{23}$ ✓

+50

SWAMP
84 ✓+46 $\frac{RP}{27}$ ✓+48 $\frac{BL RRD}{21}$ ✓+28 $\frac{MSO}{54}$ ✓

121

SWAMP
59 ✓RD ✓
12-19

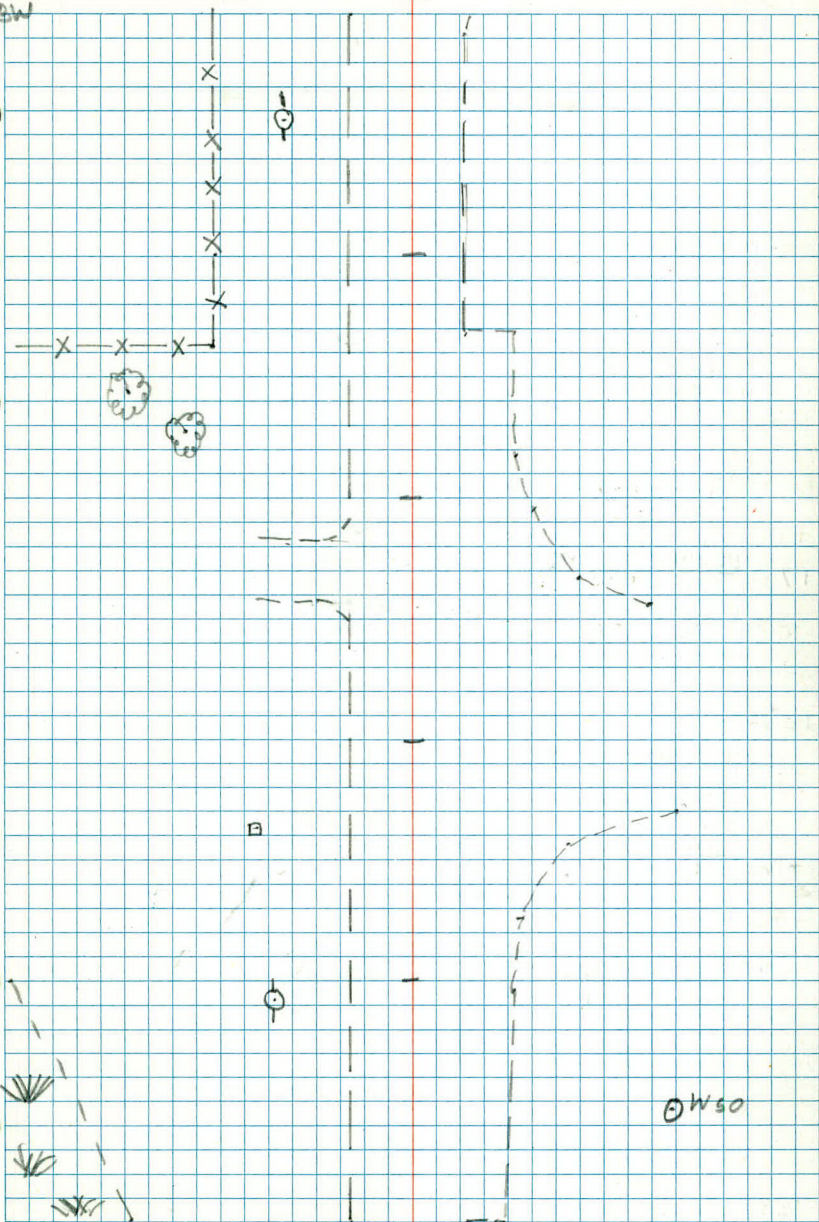
W.S
G.A
B.J
B.W

4-21-76
CLOUDY, 48° 8

LT

☉

RT



126

FE LT
41 ✓RD ✓
13

E

RT

+53 $\frac{ER}{35-100+}$ ✓

+50

+39 $\frac{BIT}{12}$ B6 RAD ✓+48 $\frac{BIT P.D.R.}{23}$ ✓+28 $\frac{BIT SPILLWAY (6' WIND)}{32-}$ ✓+06 $\frac{PP}{28}$ 125 $\frac{FE}{41}$ ✓ E RAD ✓AD ✓
12+92 $\frac{24" CMP}{35}$ ✓ 12+76 $\frac{B6 RAD}{37}$ ✓ +82 $\frac{P.D.R.}{26}$ ✓+70 $\frac{FE CORN}{80}$ ✓ +76 $\frac{FE CORNER}{41}$ ✓

+50

+44 $\frac{BIT}{12-80}$ ✓+25 $\frac{FE CORN}{41}$ ✓ +29 $\frac{FE CORN}{80}$ ✓+16 $\frac{P.D.R.}{24}$ ✓ +25 $\frac{E RAD}{39}$ ✓+02 $\frac{B6 RAD}{13}$ ✓ +17 $\frac{24" CMP}{36}$ ✓124 FE ✓ RD ✓
41 13+58 $\frac{BIT}{25}$ ✓ +59 $\frac{RAD}{43}$ ✓

123+50

FE ✓
41RD ✓
13

W.C.S.
B.A.D.
E

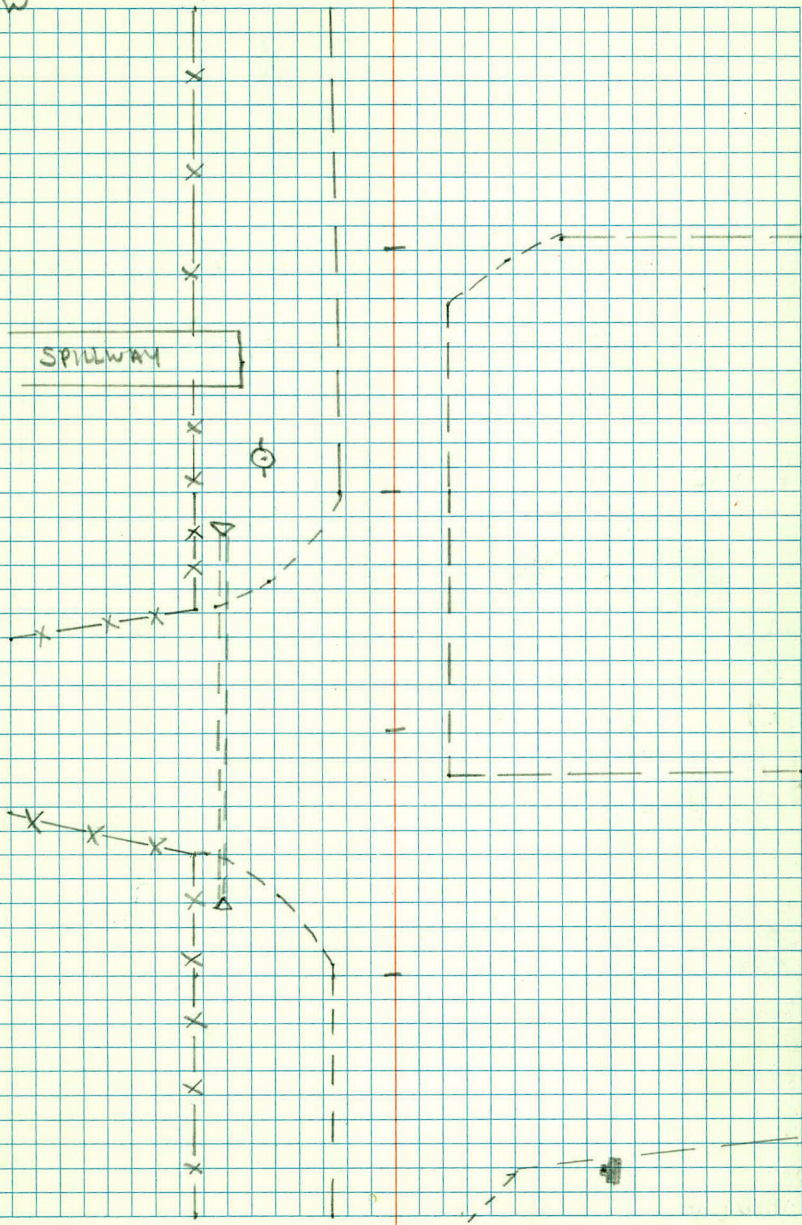
4-21-76
cloudy 48°

LT

C

RT

SPILLWAY



+50

LT

C

RT

+28 $\frac{6' \text{ BIT SPILLWAY}}{34-75+}$ ✓
 +23 $\frac{PP}{29}$ ✓

128

FE ✓
41RD ✓
12RD ✓
12FE ✓
51

+50

+39 $\frac{BIT}{12-51+}$ ✓ +43 $\frac{H4D}{43}$ ✓

+28 $\frac{5' \text{ BIT SPILLWAY}}{33-75+}$ ✓

+23 $\frac{PP \text{ FE}}{51}$ ✓

127

FE ✓
41RD ✓
13

+82 $\frac{FE-END}{51}$ ✓

+55 $\frac{PP}{29}$ ✓

+50

+49 $\frac{COR \text{ FE N:E}}{51}$ ✓

+29 $\frac{6' \text{ WIDE SPILLWAY}}{33-75+}$ ✓

126+00

FE
41RD
13

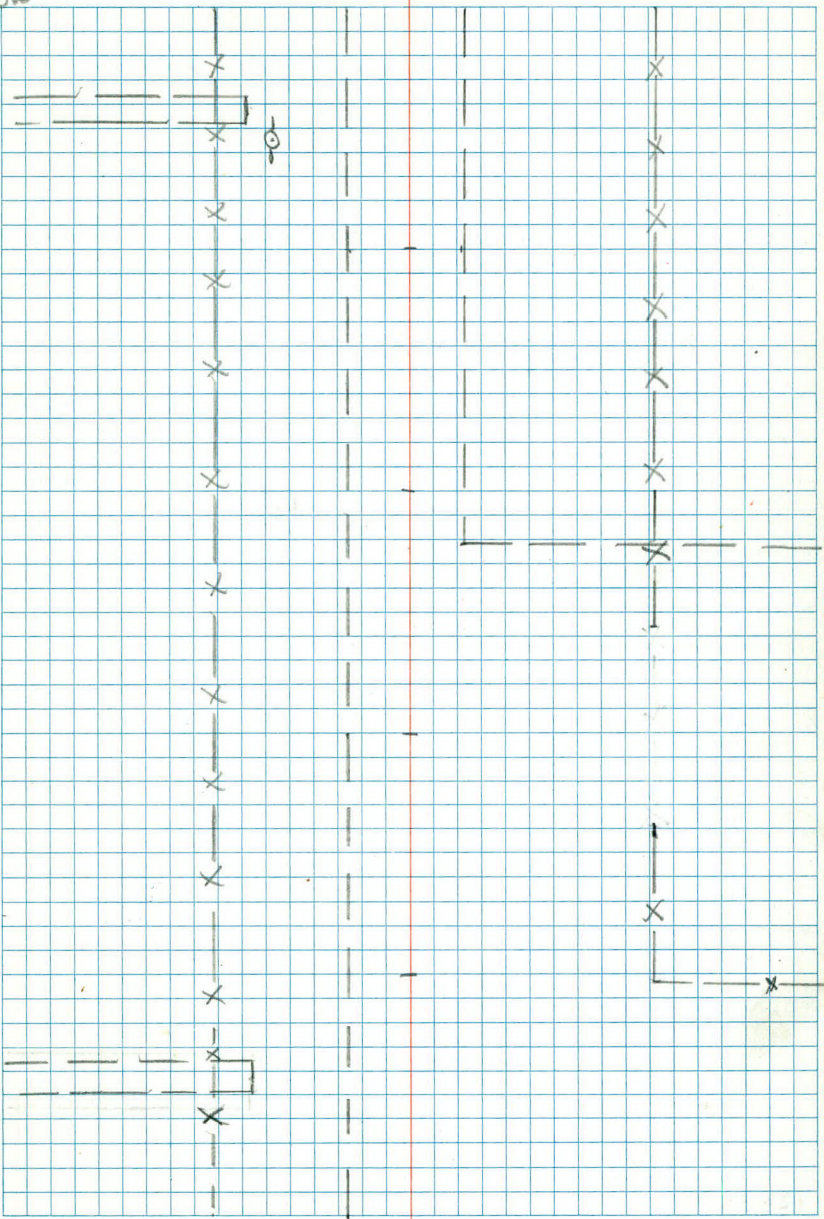
4

4-21-76
CLEAR 62°

15

LT

RT



131

LT

FE

41 ✓

RD

13 ✓

C

RD

12 ✓

RT

FE

51 ✓

+50

+30 $\frac{6' \text{ BIT SPILLWAY}}{34-75+}$ +25 $\frac{15'' \text{ cmp}}{35}$ ✓+21 $\frac{06 \text{ FE}}{51}$ ✓+01 $\frac{\text{END FE}}{51}$ ✓+11 $\frac{20' \text{ DIRECT}}{51}$

130

+94 $\frac{15'' \text{ cmp}}{35}$ ✓+82 $\frac{PP}{29}$ ✓

+50

+48 $\frac{\text{FE COR TO EAST FRONT}}{51}$ ✓+28 $\frac{6' \text{ BIT SPILLWAY}}{34-75+}$ ✓

129

FE ✓ RD ✓
41 12RD ✓
12FE ✓
51

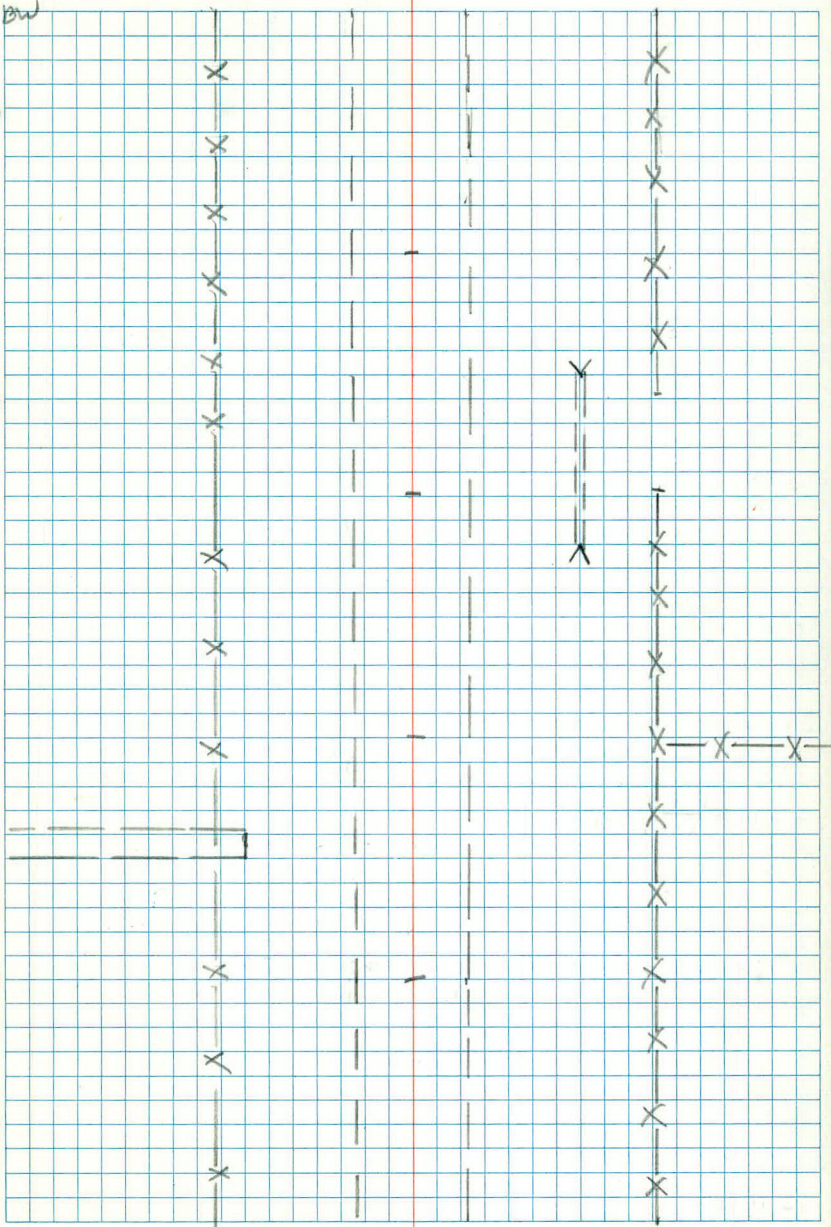
128+50

WS
GA
BT
BW

LT

E

RT. 4-21-76
CLEM:W 11



+50

LT

€

RT

RD
12 ✓

RD
12 ✓

133

RD
12 ✓

RD
12 ✓

+66 6" MABLE ✓
42
+61 4" MABLE ✓
45

+50

132

ERAD ✓
12

RD ✓
12

+83 RP ✓
30

+77 24" CMP ✓
48 +82 POR ✓
20

+95 ERAD ✓
12

+89 WSD ✓
28 +89 WSD ✓
25

+67 BL RAD ✓
49 +73 POR ✓
33

+81 POR ✓
19 +83 MA ✓
23

+50

+65 BL RAD ✓
44 +73 POR ✓
27

+35 POR ✓
29

+40 ER ✓
41

+25 RP ✓
31

+25 24" CMP ✓
48

+25 GUIDE PILE ✓
70

+36 CAS SHUTOFF ✓
49 59

+19 MA ✓
14

+11 BL RAD ✓
13

+25 POR ✓
19

+22 MA ✓
22

+26 RP ✓
28

+31 POR ✓
22

+40 ERAD ✓
41

+07 MA ✓
18

+08 FECOR ✓
41

+19 FECOR ✓
61

+06 COR FE TDEAST ✓
51

+16 BL RAD ✓
12

131+00

FE ✓
41 RD ✓
13

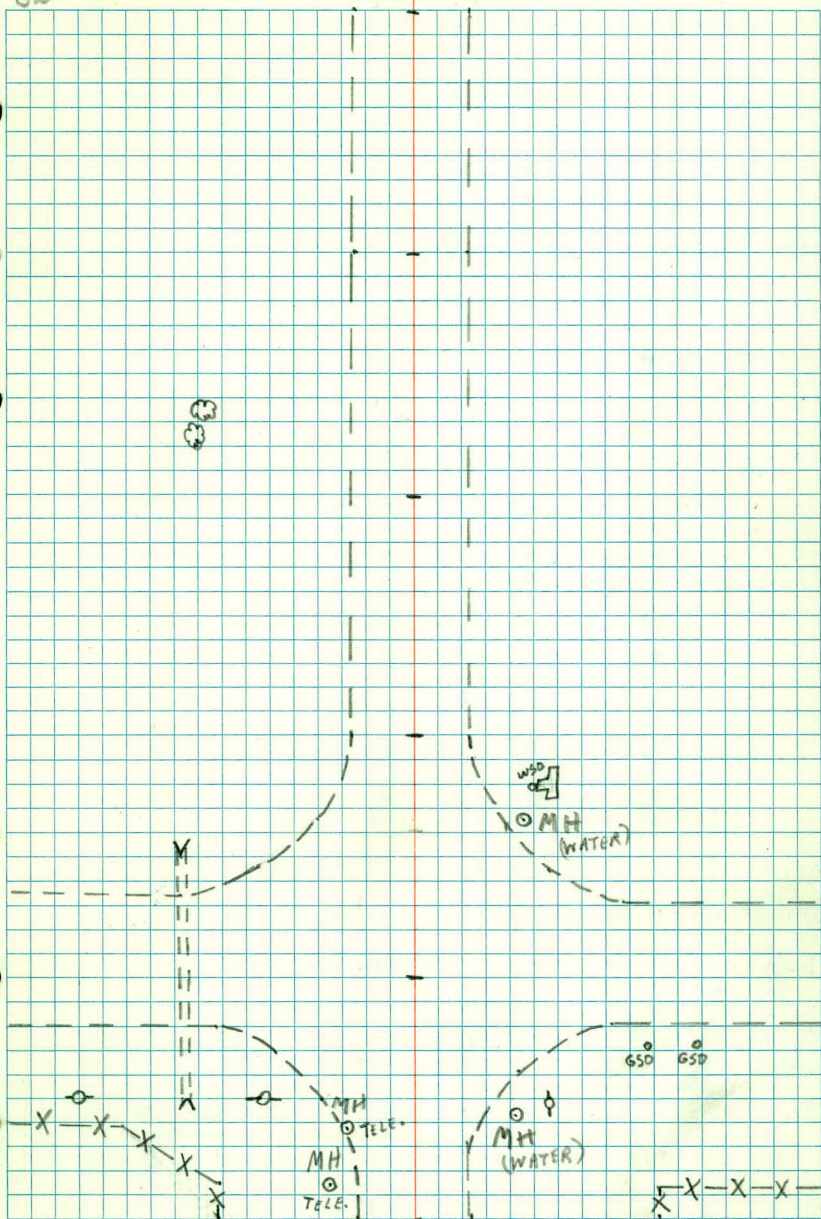
RD ✓
12 FE ✓
51

W.S
GPA
BJ
BW

LT

Q

RT 4-21-76
CLEAR: 64° 12



136

LT

RD ✓
12RD ✓
12+90 $\frac{W.S.O.}{25}$ ✓+89 $\frac{HND}{28}$ ✓Swamp ✓
35+68 $\frac{18" \text{ CMP}}{23}$ ✓+53 $\frac{10' \text{ ROCK WT}}{10}$ ✓+63 $\frac{TP}{26}$ ✓

+50

+36 $\frac{18" \text{ CMP}}{23}$ ✓

135

RD ✓
12RD ✓
12Swamp ✓
66

+50

+61 $\frac{6' \text{ ELM}}{32}$ ✓+59 $\frac{4' \text{ ELM}}{38}$ ✓

134

RD ✓
12RD ✓
12

133 +50

RD ✓
12RD ✓
12

W.S
C.V.A
B.T
BW

LT

Q

RT

4-21-16
CLW 04 61°
13

DIRT

W40

33

+50

LT

RD RD ✓
12 12

RT
DITCH ✓
27-33

138

+69 ^{min} 22 ✓

+99 ^{18" R.C.P.} 24 ✓

RD RD ✓
12 12
+99

^{18" R.C.P.} 30 ✓

+50

1

IP ✓
27

137

RD RD ✓
12 12

SWAMP DITCH ✓
32-38

+50

+12 ^{24" C.M.P.} 24 ✓

+12 ^{24" C.M.P.} 38 ✓
+12 ^{TW ELM} 35 ✓

136

RD RD
12 12

SWAMP-DITCH
34-40

W/S
G/A
B/J
B/W

LT

E

RT

4-25-16
cloudy 61° 14

8" clay



6" clay

MH

8" stub

φ



141

LT

20" ELM RD ✓
46 11RD ✓
13BIT ✓
13-2018" ✓
43+18 $\frac{5" \text{ PINE}}{36}$ ✓+85 $\frac{6" \text{ APPLE}}{45}$ ✓ +90 $\frac{10" \text{ ELM}}{33}$ ✓+73 $\frac{6" \text{ APPLE}}{44}$ ✓+61 $\frac{9" \text{ ELM}}{58}$ ✓ +70 $\frac{4" \text{ PINE}}{59}$ ✓+50 +53 $\frac{4" \text{ PINE}}{58}$ ✓ +56 $\frac{20" \text{ ELM}}{44}$ ✓+79 $\frac{\text{WOOD SIGN}}{55-69}$ ✓ +80 $\frac{14" \text{ ELM}}{43}$ ✓+65 $\frac{20" \text{ ELM}}{42}$ ✓+34 $\frac{9" \text{ ELM}}{55}$ ✓ +49 $\frac{\text{PP}}{27}$ ✓+32 $\frac{9" \text{ ELM}}{69}$ ✓+15 $\frac{15" \text{ ELM}}{36}$ ✓+05 $\frac{14" \text{ ELM}}{34}$ ✓

140

+93 $\frac{\text{E10 ROCKY}}{36}$ ✓ +80 $\frac{10" \text{ SPRUCE}}{36}$ ✓ RD ✓ 12 RD ✓ 12+80 $\frac{6" \text{ SPRUCE}}{33}$ ✓ +76 $\frac{8" \text{ SPRUCE}}{32}$ ✓+67 $\frac{3" \text{ ASH}}{45}$ ✓+53 $\frac{5" \text{ ASH}}{44}$ ✓+67 $\frac{\text{HYD}}{26}$ ✓ +67 $\frac{\text{P.O.P.}}{19}$ ✓ +78 $\frac{\text{ERRAD}}{12}$ ✓+57 $\frac{\text{W.S.O.}}{19}$ ✓ +65 $\frac{\text{ERRAD}}{28}$ ✓ +65 $\frac{\text{BIT}}{64}$ ✓

+50

+43 $\frac{12" \text{ SPRUCE}}{33}$ ✓+39 $\frac{10" \text{ SPRUCE}}{33}$ ✓ +40 $\frac{10" \text{ SPRUCE}}{36}$ ✓+37 $\frac{\text{ERRAD}}{28-48}$ ✓+34 $\frac{\text{P.A.R.}}{20}$ ✓ 5'x6' +35 $\frac{\text{PP}}{26}$ ✓+28 $\frac{\text{CONC STRUCTURE 24 R.C.P.}}{30}$ ✓+26 $\frac{\text{ERRAD}}{12}$ ✓ +25 $\frac{\text{BIT LOT}}{67}$ ✓

139

+90 $\frac{3" \text{ SPRUCE}}{35}$ ✓ +91 $\frac{3" \text{ SPRUCE}}{32}$ ✓ +97 $\frac{3" \text{ ASH}}{35}$ ✓+85 $\frac{6" \text{ ASH}}{49}$ ✓

138+50

RD RD ✓ ✓
12 12DITCH
27-33

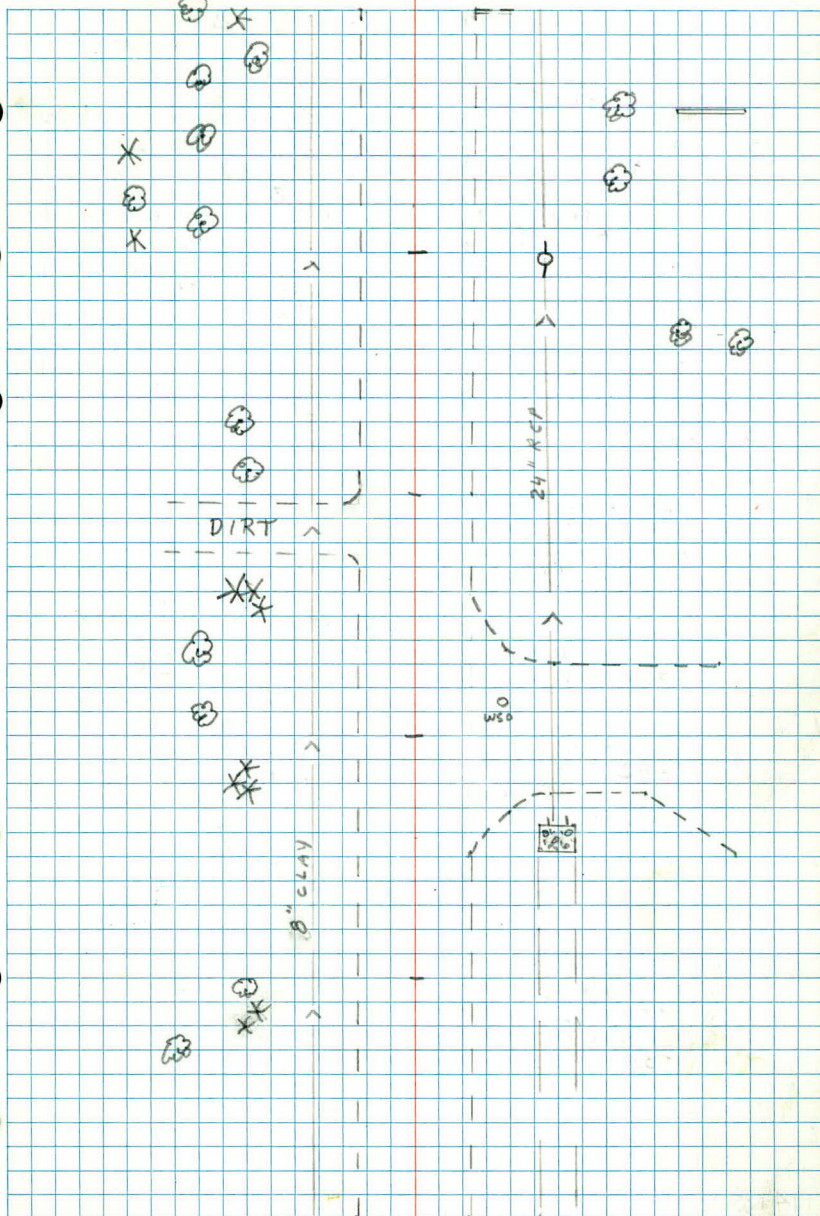
W.S.
B.J.
B.W

LT



RT

4-22-76
Cloudy 60°
15



LT

C

RT

+50

+50 PP ✓
28

+43 £10' DIRT ENT ✓

+41 $\frac{26'' \text{ OAK}}{71}$ ✓+43 $\frac{30'' \text{ OAK}}{81}$ ✓+24 NE COR HO ✓
 $\frac{103}{+26}$ 30" tree ✓
 $\frac{81}{+26}$ +33 $\frac{20'' \text{ Maple}}{40}$ ✓

143

+04 SE COR HO ✓
 $\frac{103}{11}$ Rd ✓Rd ✓
13+89 $\frac{40'' \text{ Maple}}{40}$ ✓+89 $\frac{\text{WSD}}{32}$ ✓+26 NW COR HO ✓
 $\frac{85}{85}$ +95 SW COR HO ✓
 $\frac{85}{85}$

+78 £ 10' dirt ENT ✓

+66 TW 28" COTT ✓
 $\frac{66}{66}$ +61 $\frac{\text{PP}}{28}$ ✓

+50

+38 $\frac{\text{Lilac}}{35}$ ✓+51 $\frac{\text{Lilac}}{34}$ ✓+28 $\frac{30'' \text{ Box E}}{63}$ ✓+28 NE COR HO ✓
 $\frac{99}{99}$ +40 NW COR HO ✓
 $\frac{89}{89}$ SW COR HO ✓
 $\frac{84}{84}$ +08 SE COR HO ✓
 $\frac{99}{99}$ +11 $\frac{24'' \text{ ELM}}{54}$ ✓+04 $\frac{\text{Box E}}{76}$ ✓+26 $\frac{\text{Box E}}{55}$ ✓+05 $\frac{\text{Lilac}}{34}$ ✓

142

+03 RD RD ✓
RD RD ✓
+92 £10' DIRT 11 14

+88 £16' DIRT ✓

+76 $\frac{10'' \text{ ASH}}{34}$ ✓+77 COR HEDGE ✓
 $\frac{34}{34}$ +74 $\frac{\text{PP}}{28}$ ✓+70 $\frac{\text{ER}}{13}$ ✓

+50

+41 B. HEDGE ✓
 $\frac{32}{32}$
£12' DIRT ✓
+32 $\frac{\text{MH}}{22}$ ✓+54 $\frac{\text{POR}}{23}$ ✓+54 $\frac{\text{STP}}{38}$ ✓+47 $\frac{\text{BR}}{45}$ ✓+24 $\frac{6'' \text{ ELM}}{55}$ ✓+22 $\frac{\text{ER}}{34}$ ✓
 $\frac{18'' \text{ PINE}}{18'' \text{ PINE}}$ +13 $\frac{80}{80}$ ✓+17 $\frac{27'' \text{ PINE}}{67}$ ✓

141

+12 £12' DIRT ✓

RD RD B.t ✓
11 13 12-20+05 $\frac{20'' \text{ PINE}}{69}$ ✓+07 $\frac{\text{POR}}{22}$ ✓

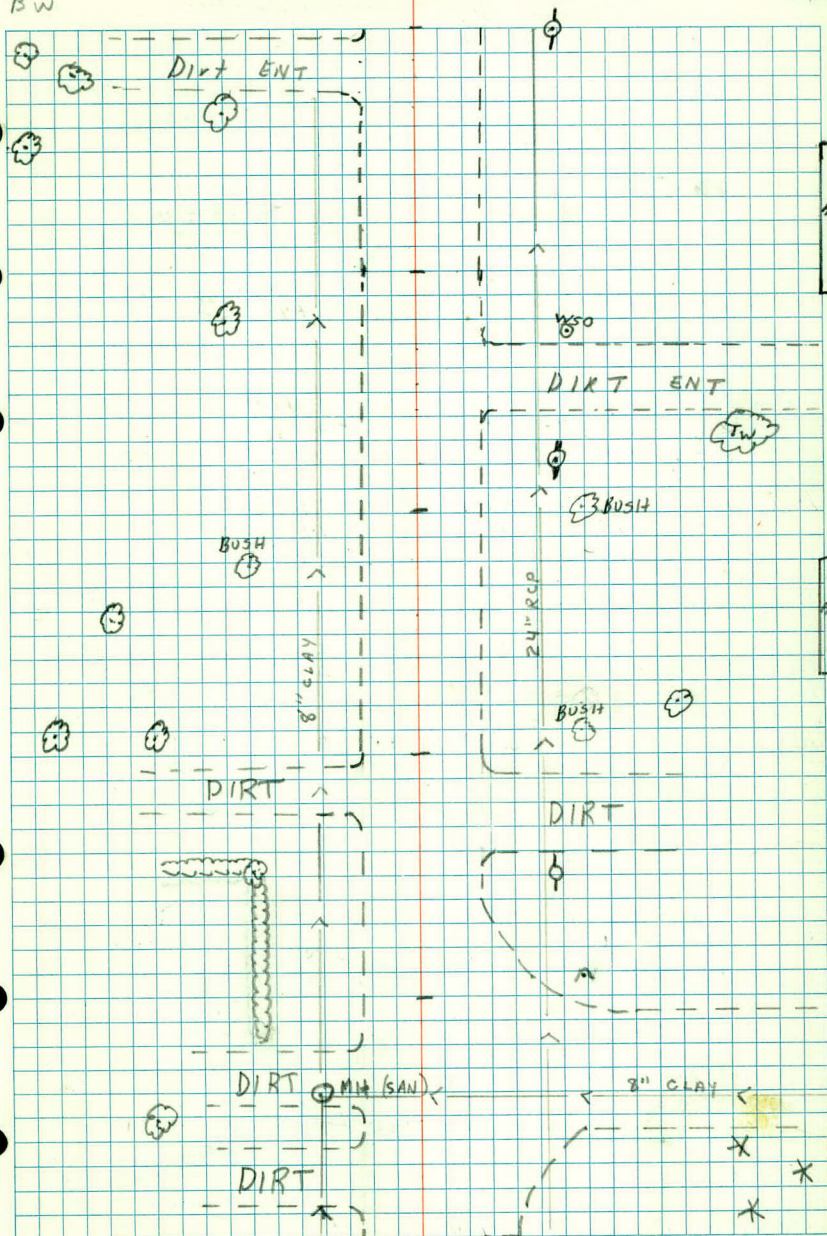
WS
BJ
BW

LT

E

RT

16



LT

E

RT

146

Fe ✓
43Rd ✓
11Rd ✓
14+88 $\frac{PP}{30}$ ✓+83 $\frac{24" ELM}{76}$ ✓+80 $\frac{12" OAK}{54}$ ✓+73 $\frac{15" OAK}{78}$ ✓+83 $\frac{12" ELM}{42}$ ✓+83 $\frac{BUSH}{66}$ ✓+60 $\frac{15" OAK}{63}$ ✓+70 $\frac{14' Gravel}{ENT}$ ✓+60 $\frac{Tw-30" Cott}{52}$ ✓

+50

+50 $\frac{4" ELM}{44}$ ✓+49 $\frac{Stump}{30}$ ✓+21 $\frac{3" Ash}{42}$ ✓+12 $\frac{WSO}{32}$ ✓+11 $\frac{20" OAK}{71}$ ✓+23 $\frac{7" Maple}{65}$

145

Fe ✓
40Rd ✓
11Rd ✓
14+95 $\frac{8" PINE}{45}$ +76 $\frac{22" OAK}{47}$ ✓+71 $\frac{Tw-15" ELM}{42}$ ✓+74 $\frac{C-2 Fe}{31-83}$ ✓

+50

+62 $\frac{20" OAK}{44}$ ✓+71 $\frac{4" ELM}{46}$ ✓+52 $\frac{PP}{30}$ ✓+70 $\frac{15" ELM}{50}$ ✓+45 $\frac{18" OAK}{50}$ ✓+40 $\frac{12' DWT ENT}{ENT}$ ✓+27 $\frac{3-5" ELMs}{43}$ ✓+24 $\frac{4" Maple}{40}$ +20 $\frac{bc Fe}{40}$ ✓+10 $\frac{BUSH}{40}$ ✓+18 $\frac{Flag Pole}{53}$ ✓+11 $\frac{13' dnt ENT}{Gate \& END Fe}$ +10 $\frac{NW COR Ho}{85}$ ✓

144

+07 $\frac{40 Rd}{11}$ ✓+80 $\frac{HYD}{29}$ ✓+77 $\frac{4" Birch}{68}$ ✓+78 $\frac{2" Maple}{42}$ ✓+86 $\frac{B-1" ELMs}{36}$ +67 $\frac{14' Gravel}{ENT}$ ✓+82 $\frac{SW COR Ho}{84}$ ✓+55 $\frac{36" COTT}{70}$ ✓+64 $\frac{PP}{37}$ +63 $\frac{36" COR Fe}{39}$ ✓+59 $\frac{4" PINE}{54}$ ✓+50 +56 $\frac{30" Maple}{43}$ ✓+53 $\frac{8" Maple}{39}$ ✓+55 $\frac{22" ELM}{40}$ ✓

RF6
GA
LDD
JA
DS
BW

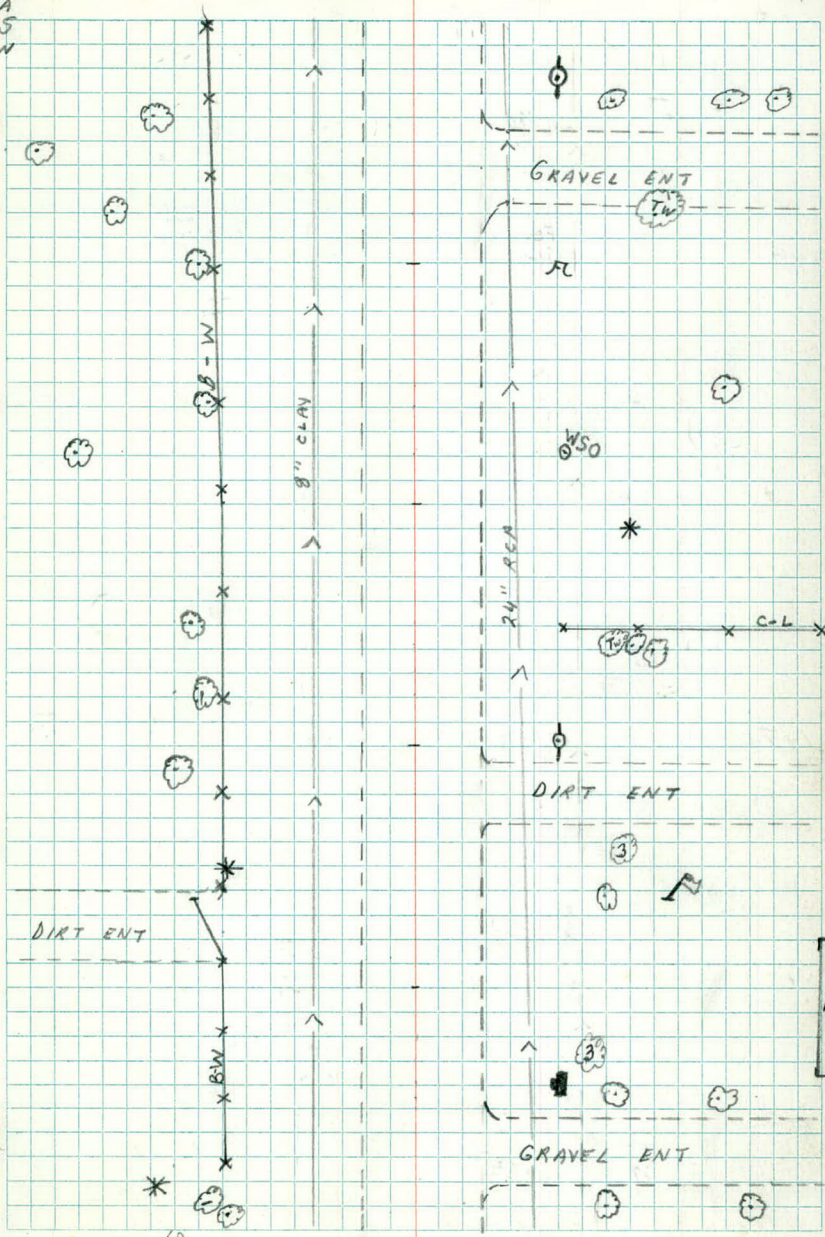
4-26-76
Clear 42°

17

LT

±

RT



50

LT

E

RT

+50

cor Fe
+42 $\frac{55}{100}$ ✓Rd
11Rd
13+29 $\frac{12'' \text{ COTT}}{46}$ ✓+21 $\frac{\text{MH}}{24:48}$ ✓+31 $\frac{\text{Arc ltc}}{30}$ ✓+11 $\frac{\text{Tw } 2'' \text{ ELM}}{45}$ +15 $\frac{\text{Lift Sta}}{48}$ ✓+15 $\frac{\text{PF}}{28}$ ✓

148

cor. Fe
+09 $\frac{41-55}{11}$ ✓ Rd ✓Rd
13+09 $\frac{\text{Hyd}}{28}$ ✓+68 $\frac{\text{Lot IRON}}{50}$ ✓

+50

+34 $\frac{\text{st p}}{38}$ ✓ +34 $\frac{\text{st p}}{37}$ ✓+19 $\frac{\text{st p}}{40}$ ✓+17 $\frac{2'' \text{ ELM}}{44}$ ✓147 $\frac{\text{st p}}{40}$ ✓ $\frac{\text{st p}}{39}$ ✓ Fe $\frac{44}{11}$ ✓ Rd ✓Rd
14+99 $\frac{\text{st p}}{39}$ ✓ +98 $\frac{\text{st p}}{36}$ ✓ +94 $\frac{\text{st p}}{40}$ ✓+68 $\frac{\text{st p}}{40}$ ✓

+50

+53 $\frac{\text{beg Lilac}}{49-150}$ ✓+53 $\frac{7'' \text{ ELM}}{66}$ ✓+45 $\frac{\text{st p}}{42}$ ✓ +48 $\frac{\text{WSD}}{36}$ ✓+46 $\frac{\text{MH}}{17}$ ✓+48 $\frac{4'' \text{ PINE}}{38}$ ✓+35 $\frac{\text{MH}}{16}$ ✓+33 $\frac{21'' \text{ ELM}}{42}$ ✓+40 $\frac{\text{NW COR Ho}}{78}$ ✓+23 $\frac{\text{st p}}{37}$ ✓+09 $\frac{24'' \text{ OAK}}{41}$ ✓+20 $\frac{\text{WSD}}{33}$ ✓+17 $\frac{15'' \text{ ELM}}{42}$ ✓

146+00

Fe $\frac{43}{11}$ ✓ Rd ✓Rd
14+16 $\frac{\text{SW COR Ho}}{78}$ ✓

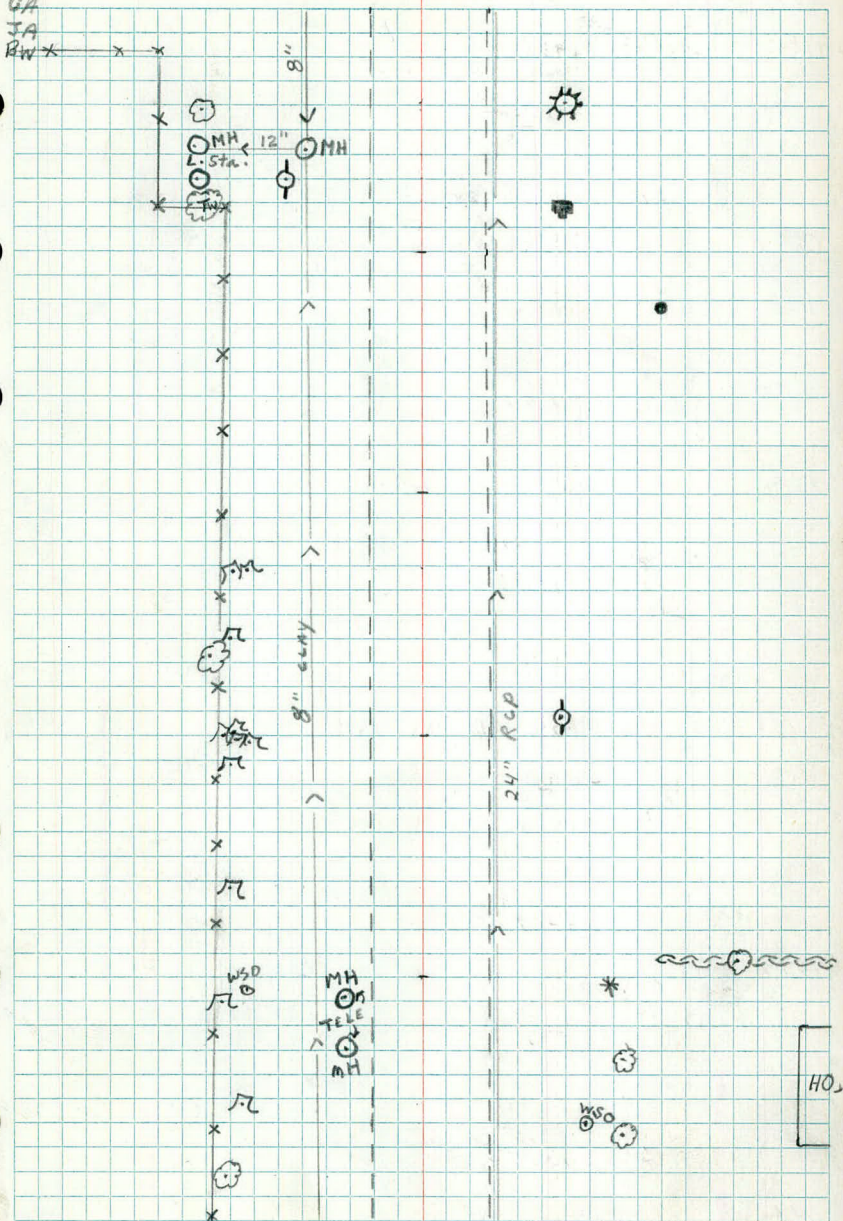
RFG
LPD
DS
QA
JA
RW

LT

E

RT

4-26-76
clear 450



151
 +99 $\frac{6" \text{cott}}{36}$ ✓
 +80 $\frac{\text{Hedge}}{43-100}$ ✓
 +50
 +82 $\frac{22" \text{cott}}{35}$ ✓
 +68 $\frac{10' \text{ DIRT ENT}}{10'}$ ✓
 +70 $\frac{\text{PP}}{28}$ ✓
 +00 $\frac{7" \text{cott}}{35}$ ✓
 +98 $\frac{\text{Tw cott}}{34}$ ✓
 +95 $\frac{\text{Tw cott}}{38}$ ✓
 Rd 11 ✓
 Rd 13 ✓
 Rt

150
 +19 $\frac{24" \text{ RCP (W. END)}}{31}$ ✓
 +24 $\frac{15" \text{ SCP (N. END)}}{27}$ ✓
 +79 $\frac{\text{WSO}}{39}$ ✓
 +90 $\frac{\text{MH}}{24}$ ✓
 +190 $\frac{\text{MH}}{47}$ ✓
 +85 $\frac{\text{Tw-poplar}}{33}$ ✓
 +87 $\frac{4" \text{ poplar}}{36}$ ✓
 +73 $\frac{18" \text{ RCP (EAST END)}}{30}$ ✓
 +78 $\frac{8" \text{ Tw ELM}}{30}$ ✓
 +75 $\frac{\text{MH}}{17}$ ✓
 +69 $\frac{12" \text{ SCP (N. END)}}{35}$ ✓
 +58 $\frac{\text{PP}}{29}$ ✓
 +50
 +54 $\frac{10' \text{ DIRT ENT}}{10'}$ ✓
 +37 $\frac{12" \text{ SCP (S. END)}}{36}$ ✓
 +26 $\frac{\text{WSO}}{32}$ ✓
 +07 $\frac{19" \text{ cott}}{37}$ ✓
 Rd 11 ✓
 Rd 13 ✓
 Rt

149
 +97 $\frac{14" \text{ cott}}{31}$ ✓
 +63 $\frac{22" \text{ Will}}{62}$ ✓
 148+50

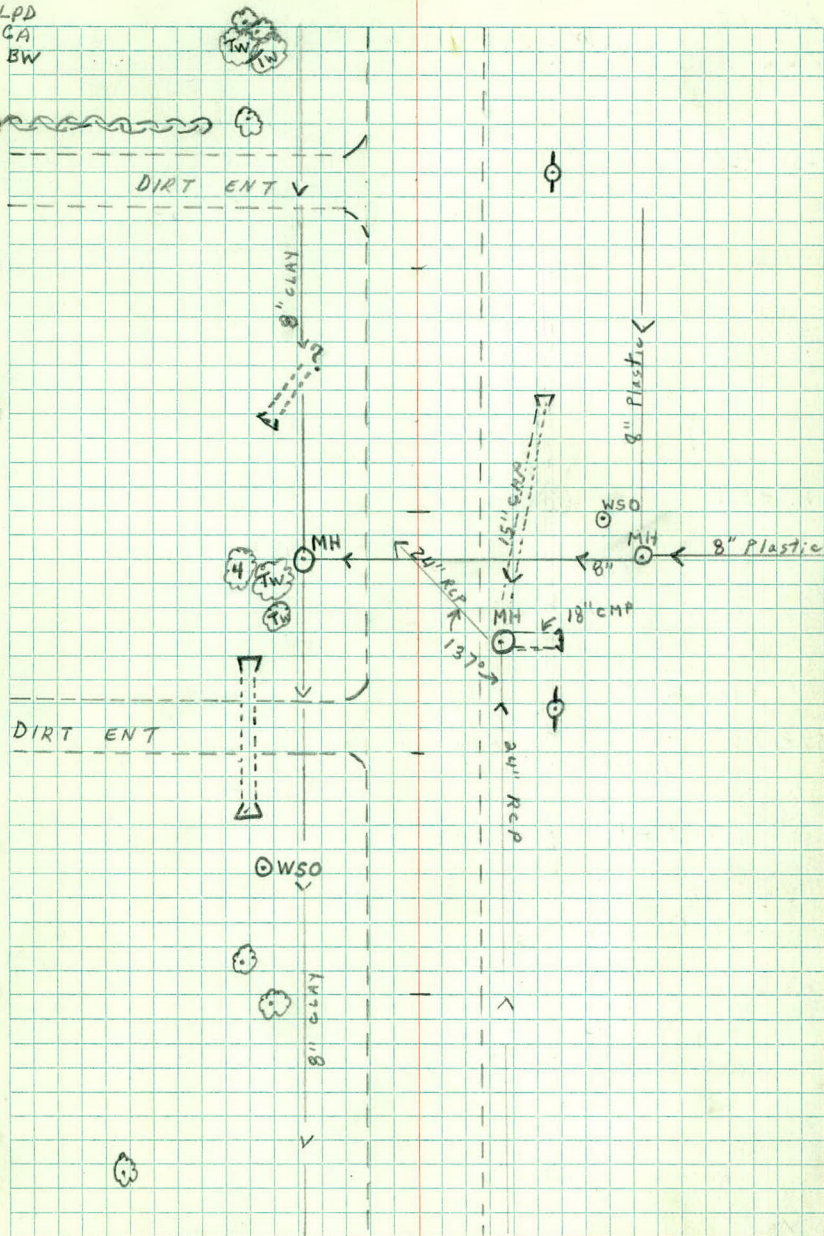
RF6
DS
JA
LPD
GA
BW

LT

RT

RT

4-26-76
clear 46°



LT

E

RT

+50

+40 $\frac{10'' \text{ POP}}{32}$ ✓+38 $\frac{8'' \text{ POP}}{34}$ ✓+35 $\frac{6'' \text{ Maple}}{46}$ ✓+31 $\frac{5'' \text{ Maple}}{55}$ ✓+28 $\frac{5'' \text{ Maple}}{51}$ ✓+13 $\frac{3-8'' \text{ ELMS}}{38}$ ✓
48

153

+00 $\frac{\text{END WOODS}}{46-60}$ ✓Rd ✓
12Rd
12+10 $\frac{15'' \text{ CMP}}{23}$ ✓ +10 $\frac{\text{PP}}{28}$ ✓+86 $\frac{15'' \text{ CMP}}{23}$ ✓+78 $\frac{10' \text{ Drt ENT}}{105}$ ✓+67 $\frac{15'' \text{ CMP}}{23}$ ✓

+50

+56 $\frac{\text{Tw- } 4'' \text{ ELM}}{68}$ ✓+48 $\frac{\text{WSO}}{47}$ ✓+08 $\frac{62 \text{ Woods}}{32-75}$ ✓+02 $\frac{\text{MH}}{24}$ ✓Rd ✓
12+36 $\frac{\text{NW COR HO}}{97}$ ✓+13 $\frac{\text{WSO}}{47}$ ✓+03 $\frac{\text{Hyd}}{20}$ ✓ +12 $\frac{\text{NE COR HO}}{96}$ ✓+99 $\frac{\text{PP}}{62}$ ✓+94 $\frac{\text{PP}}{29}$ ✓+92 $\frac{10' \text{ Drt ENT}}{105}$ ✓+78 $\frac{\text{bush}}{39}$ ✓+80 $\frac{4'' \text{ PINE}}{52}$ ✓+71 $\frac{\text{WSO}}{35}$ ✓+79 $\frac{12'' \text{ SEP (N. END)}}{25}$ ✓+69 $\frac{12' \text{ ENT BIT}}{105}$ ✓+59 $\frac{12'' \text{ SEP (S. END)}}{26}$ ✓

+50

+47 $\frac{\text{SE COR HO}}{93}$ ✓+43 $\frac{8'' \text{ birch}}{41}$ ✓+36 $\frac{\text{bush}}{43}$ ✓+32 $\frac{6'' \text{ Apple}}{46}$ ✓+33 $\frac{\text{bush}}{62}$ ✓+33 $\frac{\text{bush}}{50}$ ✓

151

Rd ✓
11Rd ✓
13

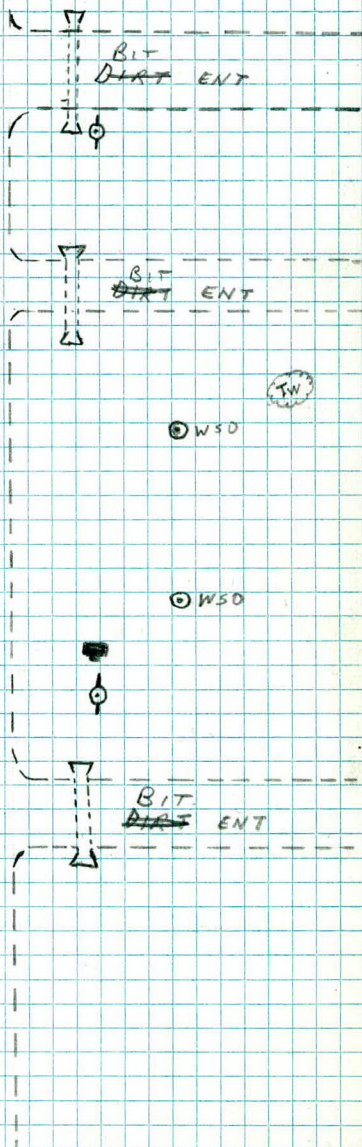
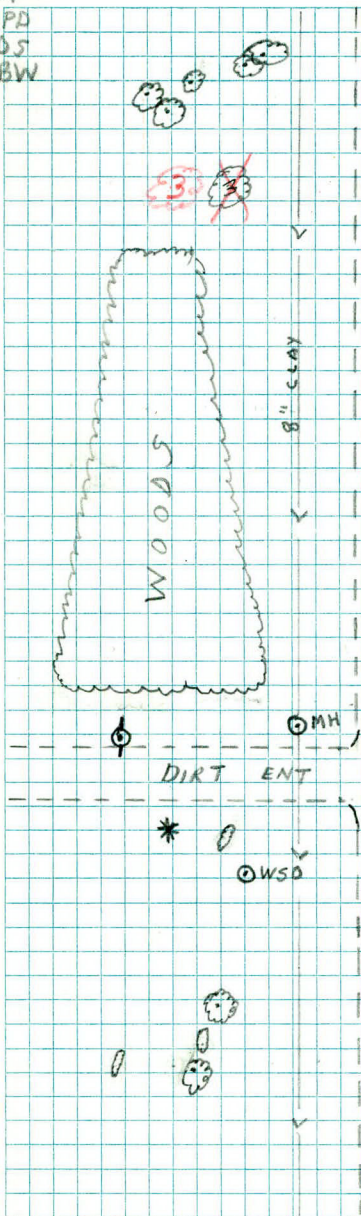
NEG
GA
JA
LPD
PS
BW

LT

E

RT

4-26-76
clear 58°



LT

£

RT

156

Rd
12 ✓Rd
12 ✓

+94 $\frac{24'' \text{ELM}}{35}$ ✓ +87 dead tree ✓
55

+89 MH $\frac{21}{21}$ +74 £ 12' Gravel ENT ✓

dead tree ✓
+63 $\frac{43}{43}$

+60 $\frac{6'' \text{ELM}}{60}$

+50 +59 $\frac{6'' \text{ELM}}{54}$ ✓ +59 $\frac{8'' \text{ELM}}{50}$ ✓

+46 £ $\frac{10' \text{ CONC ENT}}{35}$ ✓

+45 $\frac{15'' \text{CMP}}{24}$ ✓

+33 £ 14' BIT ENT ✓

+12 $\frac{8'' \text{cedar}}{44}$ ✓ +28 $\frac{20'' \text{ELM}}{59}$ ✓

+24 $\frac{15'' \text{CMP}}{24}$ ✓

155

+01 $\frac{18'' \text{ELM}}{59}$ ✓

Rd
13 ✓

Rd
12 ✓

+18 $\frac{2'' \text{Lilac}}{32}$ ✓

+95 Arb bush $\frac{43}{43}$ ✓

+77 $\frac{10'' \text{CEDAR}}{44}$ ✓

+90 $\frac{16'' \text{Box E}}{35}$

+68 $\frac{15'' \text{ELM}}{59}$ ✓

+62 $\frac{2'' \text{Lilac}}{46}$

+71 $\frac{15'' \text{CMP}}{23}$ ✓

+69 $\frac{8'' \text{ELM}}{55}$ ✓

+50 +54 $\frac{4'' \text{ELM}}{44}$ ✓ +53 $\frac{2'' \text{Lilac}}{45}$

+52 Arc light $\frac{29}{29}$ ✓

+61 £ 10' Dirt ENT ✓

+45 $\frac{PP}{44}$ ✓

+44 Tw $\frac{4'' \text{POP}}{30}$ ✓

+32 $\frac{15'' \text{CMP}}{31}$ ✓

+43 £ 10' Dirt ENT ✓

+36 $\frac{8'' \text{POP}}{39}$ ✓

+20 $\frac{10'' \text{POP}}{36}$ ✓

+06 MH $\frac{31}{31}$ ✓

+28 Arb bush $\frac{67}{67}$ ✓

+30 $\frac{15'' \text{Maple}}{35}$ ✓ +28 $\frac{4'' \text{PINE}}{72}$

+29 $\frac{DRIVE}{47-61}$ ✓

+12 $\frac{65}{65}$ ✓

154

+92 MH $\frac{13}{13}$ ✓

+92 $\frac{W50}{36}$ ✓

Rd
12 ✓

Rd
12 ✓

+14 $\frac{LIFE}{65}$ ✓

+12 $\frac{DRIVE}{49-59}$ ✓

+07 $\frac{4'' \text{PINE}}{50}$

+82 $\frac{4'' \text{Maple}}{52}$ ✓

153+50

Rd
12 ✓

Rd
12 ✓

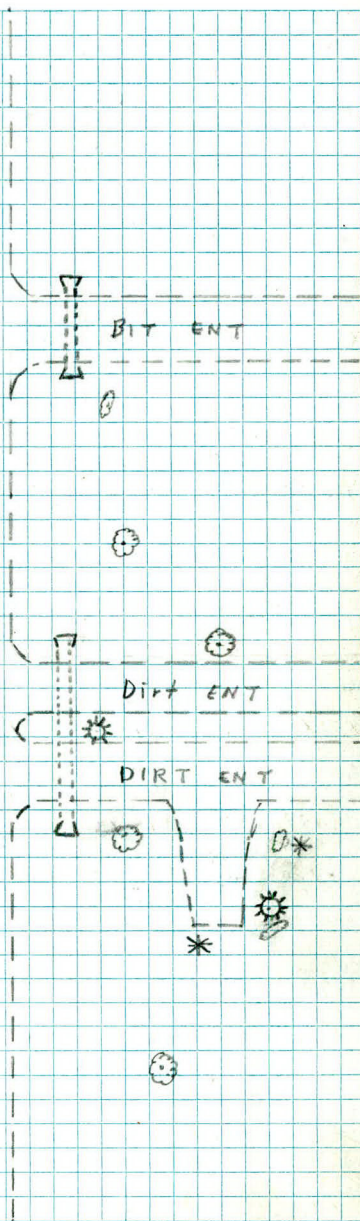
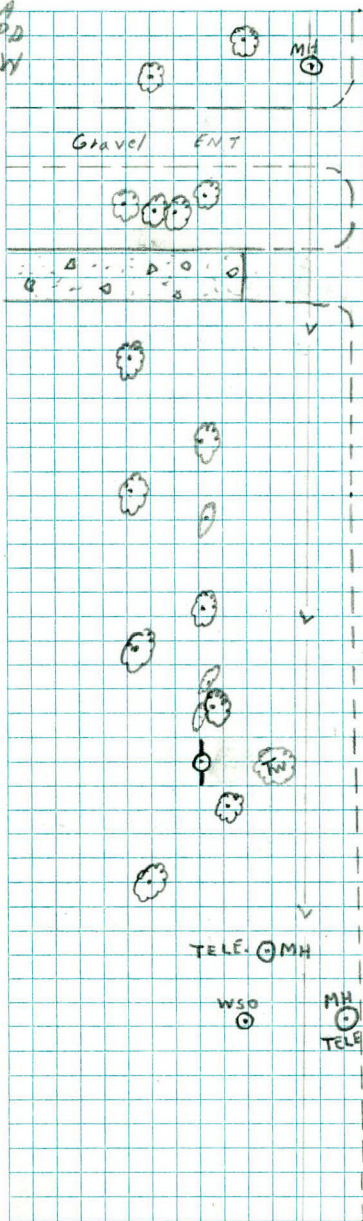
RFG
GA
DS
GA
LPD
BY

LT

£

RT

4-26-76
Clear 60°



+50

LT

E

RT

+15 $\frac{24'' \text{ B.E.}}{24}$ ✓+14 $\frac{2' \text{ SW}}{40-100+}$ ✓+19 $\frac{20'' \text{ ELM}}{35}$ ✓

+08 £ 10' Grav ENT ✓

+14 $\frac{\text{bush}}{29}$ ✓+18 $\frac{\text{bush}}{29}$ ✓

158

+01 Hedge ✓
34-100+Rd ✓
12Rd ✓
12+03 $\frac{\text{bush}}{29}$ +00 $\frac{\text{conc}}{53-85}$ ✓+92 $\frac{\text{PP}}{30}$ ✓+92 $\frac{\text{bush}}{29}$ ✓+87 $\frac{4'' \text{ PINE}}{67}$ ✓+88 $\frac{15'' \text{ CMP}}{23}$ +88 $\frac{20'' \text{ ELM}}{35}$ +86 $\frac{29-36-52}{\text{conc}}$ +52 $\frac{\text{B.E. } 12''}{64}$ ✓

+76 £ 14' CONC ENT ✓

+68 $\frac{15'' \text{ CMP}}{24}$ ✓+62 $\frac{\text{bush}}{29}$ +73 $\frac{\text{conc}}{29-42}$ ✓

+50

+52 $\frac{24'' \text{ ELM}}{32}$ ✓+52 $\frac{\text{PP}}{28}$ ✓+56 $\frac{22'' \text{ ELM}}{35}$ ✓+49 $\frac{15'' \text{ CMP}}{22}$ ✓

+32 £ 12' BIT ENT ✓

+39 £ 12' BIT ENT ✓

+29 $\frac{15'' \text{ CMP}}{22}$ ✓+25 $\frac{15'' \text{ ELM}}{36}$ ✓

157

+00 $\frac{18 \text{ cott}}{39}$ ✓Rd ✓
12Rd +01 ✓
1217'' B.E. ✓
58
38+10 $\frac{\text{NW cor } 110}{63}$ ✓+85 $\frac{\text{TW-18'' cott}}{53}$ ✓+77 $\frac{\text{bush}}{43}$ ✓+78 $\frac{\text{bush}}{35}$ ✓+67 $\frac{\text{SW cor } 110}{63}$ ✓ +78 $\frac{24'' \text{ B.E.}}{39}$ ✓+72 $\frac{9'' \text{ ELM}}{43}$ ✓+76 $\frac{10'' \text{ PINE}}{29}$ ✓+52 $\frac{\text{Hyd}}{44}$ ✓+52 $\frac{\text{WSO}}{41}$ ✓+61 $\frac{8'' \text{ PINE}}{43}$ ✓

+50

+52 $\frac{12'' \text{ ELM}}{38}$ ✓+45 $\frac{15'' \text{ ELM}}{28}$ ✓+45 $\frac{26'' \text{ ELM}}{34}$ ✓+41 $\frac{2' \text{ SW}}{28-100+}$ ✓+42 $\frac{15'' \text{ CMP}}{22}$ ✓+30 $\frac{12'' \text{ ELM}}{39}$ ✓

+30 £ Bit 17' ENT ✓

+17 $\frac{15'' \text{ CMP}}{22}$ ✓+10 $\frac{12'' \text{ ELM}}{41}$ ✓+14 $\frac{\text{PP}}{28}$ ✓+13 $\frac{24'' \text{ ELM}}{53}$ ✓

156 +00

Rd ✓ +06 $\frac{\text{WSO}}{35}$ ✓
12Rd ✓ +10 $\frac{\text{bush}}{31}$ ✓
12

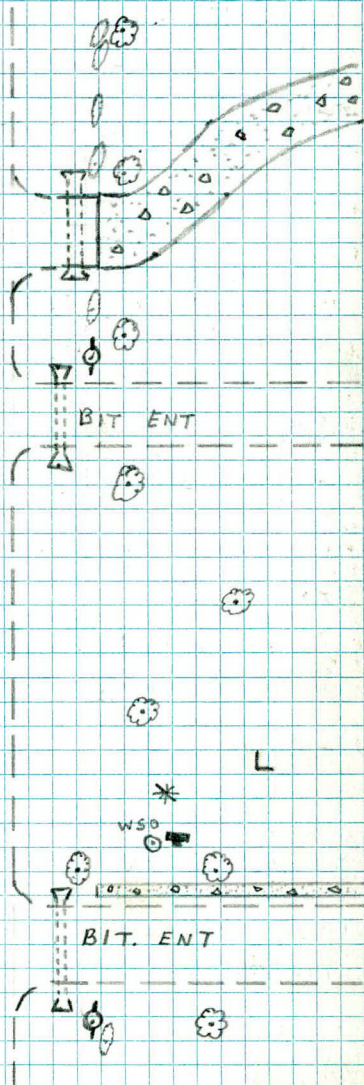
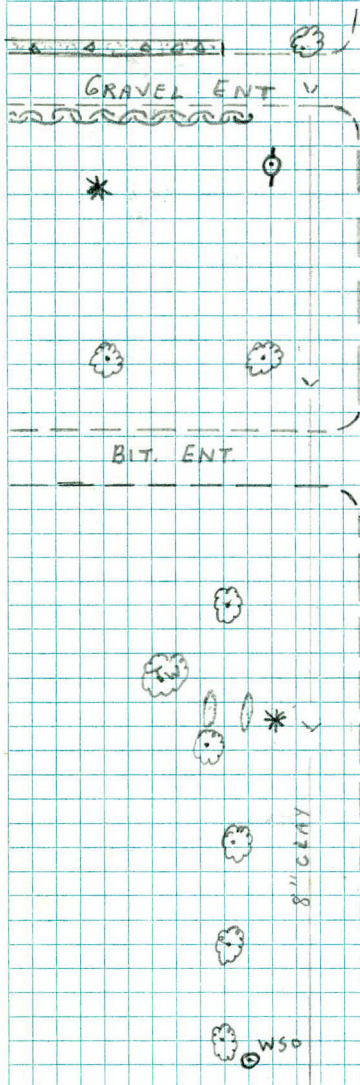
REF
GA
JA
LPD
DS
BW

LT

E

RT

4-28-76
clear 60°



161	+99 GP 35 ✓	+96 GP 38 ✓	RT
GP ✓ +89 52 ✓	+90 GP 47 ✓	+93 GP 43 ✓	+00 Fe 41 ✓
+88 58 ✓	+95 POR 35 ✓	+86 BR 52 ✓	+93 Fe 47-55 ✓
+93 MH 30 ✓	+92 MH 21 ✓	+85 MH 17 ✓	+98 ER 19 ✓
+81 MH 14 ✓	+73 MH 14 ✓	+60 & Co. Rd D	+71 BR 41 ✓
+50	+42 GSO 29 ✓	+60 & Co. Rd D	+71 BR 41 ✓
+39 ER 48 ✓	COR CONC +39 48-78 ✓	COR CONC +28 54-78 ✓	+32 POR 25 ✓
+30 POR 31 ✓	Fill Pipe +26 47 ✓	+23 bush 48 ✓	+20 MH 22 ✓
+20 Bush 49 ✓	+20 Lite Base 44 ✓	+15 Lite 48 ✓	+19 BR 17 ✓
COR CONC +14 24 ✓	+14 BR 24 ✓	+15 BUSH 46 ✓	+35 PP 35 ✓
160	+13 MH 24 ✓	+10 COR CONC 34 ✓	+02 sign 62 ✓
+90 CONC Gr 22-33 ✓	+85 COR CONC 33 ✓	+90 & 24' BIT ENT ✓	+02 bit 64 ✓
+80 CONC 47-71 ✓	NO END PUMP ISLAND ✓		
+76	59		
So END PUMP BLAND			
+61 59	+60 CONC 47-71 ✓	+70 CONC 50-100+ ✓	
+50			
+40 & 38' BIT ENT			
+22 CONC SLAB 34 ✓			
+08 & 12' GRAV ENT	+17 CONC SLAB 25-34 ✓		
159			
COR CONC +98 33 ✓	MT ASH +90 50 ✓	COR CONC +91 25 ✓	+03 CONC cor. 33 ✓
MH +74 26 ✓	+82 9" ELM 43 ✓	+91 Rd ✓	+99 PP 28 ✓
+73 VENT PIPE 30 ✓	+73 GSO 28 ✓		+94 cor CONC 12 ✓
+70 GSO 28 ✓	+74 Rd 12 ✓		
158+50	+68 GSO 32 ✓	+69 CAS METER 30 ✓	+65 6" ELM 47 ✓
			+7-6" ELM 58 ✓
			+64 9" ELM 44 ✓
			+51 12" ELM 35 ✓

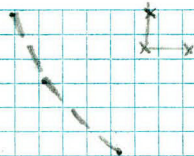
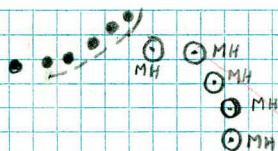
RFG
GA
LPD
JA
DS
BW

LT

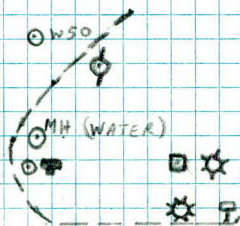
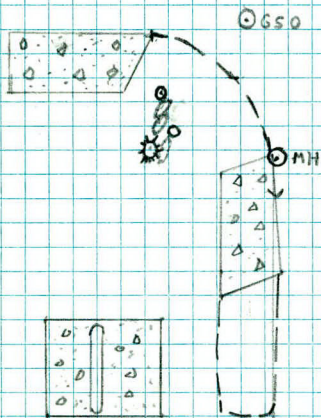
E

RT

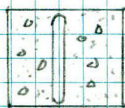
4-26-76
clear 61°



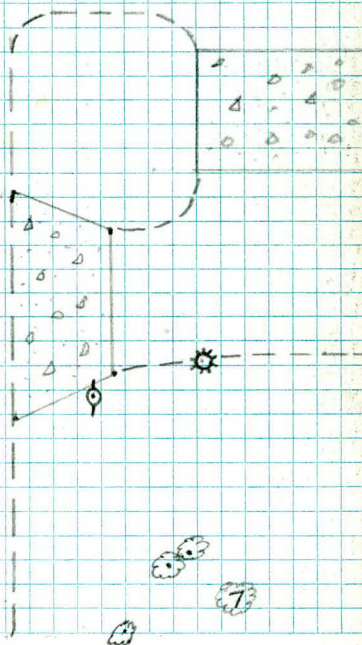
Co. Rd D



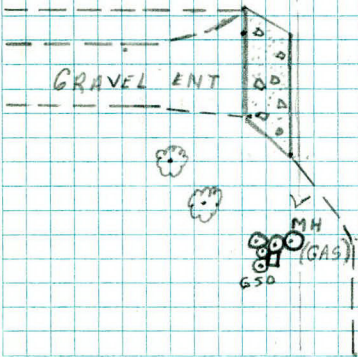
BIT ENT

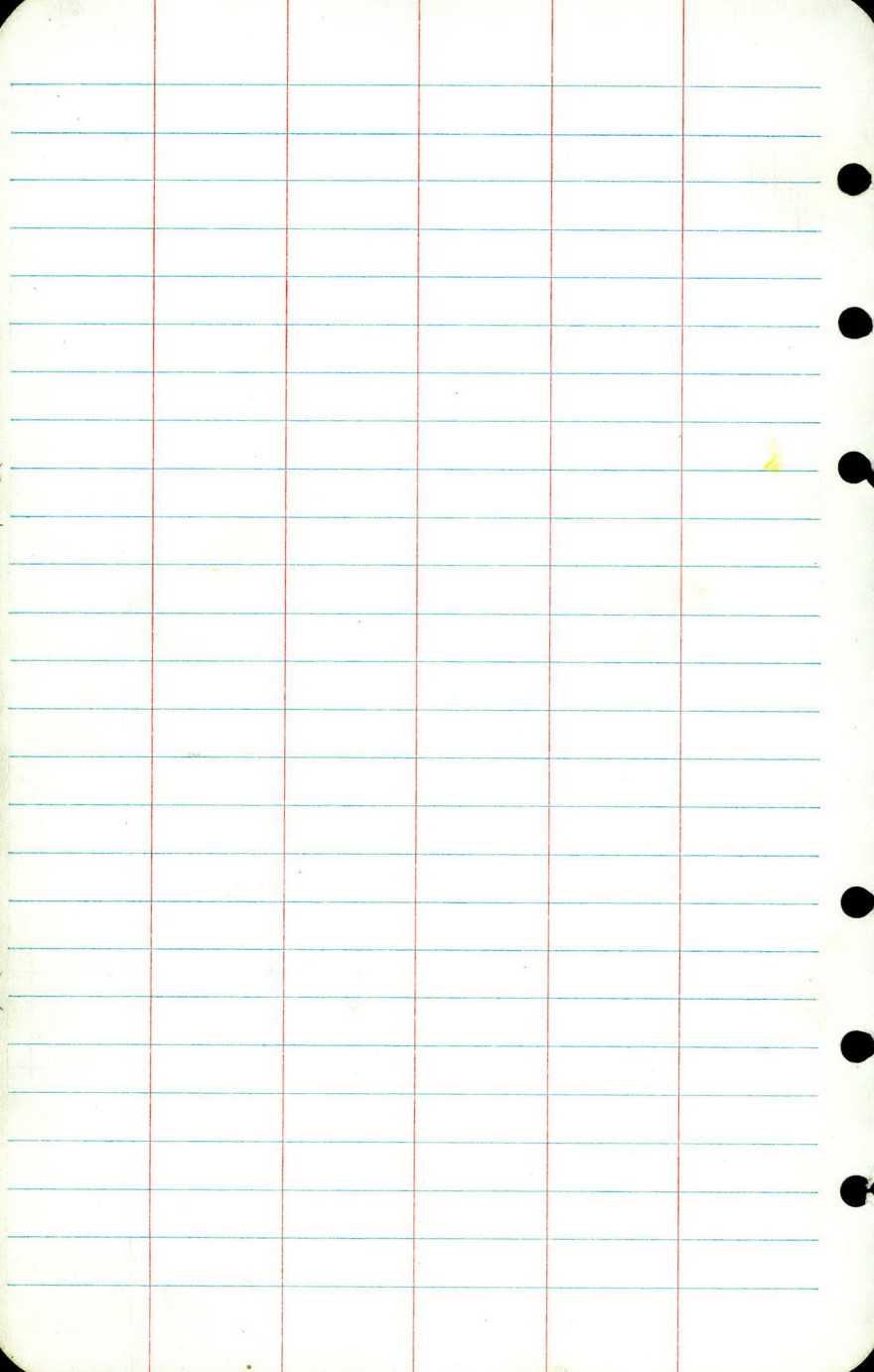


BIT ENT



GRAVEL ENT





RG
LPD
JA

Apr. 22, 1976
Cldy 50°

Cleveland Ave

X-Sections

Sta	+	π	-	Elv.
BM	0.33	917.21		916.88

106 + 54

✓

107

✓

132

Ent 1st

✓

+90

✓

R.G
L.P.D
J.R

Apr. 22, 1976

LT

E

RT

Top Hyd RT 106+75

910.11	912.51	912.61	913.01	913.11	913.21	913.59	913.53	913.11	912.61
7.1	4.7	4.6	4.2	4.1	4.0	3.62	3.68	4.1	4.6
41	30	25	12		12	13	18	19	39
FC			E SBL			conc med.			

916.11	915.31	914.71	914.21	913.11
1.1	1.9	2.5	3.0	4.1
85	85	63	63	50
T.C		T.C		

909.61	912.31	912.41	912.61	912.71	912.81	912.80	913.10	912.71	912.41	912.21
7.6	4.9	4.8	4.6	4.5	4.4	4.41	4.11	4.5	4.8	5.0
43	31	25	12		12	13	19	20	30	44
Fe			E SBL			conc med.				

915.21	915.91	913.81	912.71
2.0	1.3	3.4	4.5
93	93	65	44
	T.C		T.C

909.11	911.91	912.21	912.31	912.41	912.61	912.99	912.78	912.41	912.21
8.1	5.3	5.0	4.9	4.8	4.6	4.22	4.23	4.8	5.0
42	31	25	12		12	13	18	19	29
Fe			E SBL			conc med.			

914.81	913.41	912.21	912.01
2.4	3.8	5.0	5.2
100	72	50	43

909.21	912.51	911.91	911.91	912.11	912.31	912.63	912.60	912.11	911.91
8.6	4.7	5.3	5.3	5.1	4.9	4.58	4.61	5.1	5.3
42	31	25	12		11	12	17	19	30
Fe						conc med.			

914.91	913.91	912.61	912.31	911.81
2.3	3.3	4.6	4.9	5.4
90	72	54	42	42
			T.C	B.C

STA	+	π	-	ELEV	
108+00		917.21			
✓					
+46					Ent Rt.
✓					
B.M.	3.18	915.58	4.81	912.40	912.40
+68					
✓					
✓					
+84					
✓					

R.G.
LPD
JA

Apr 12 22, 476

909.11 Lt 8.1 5.8 5.6 5.6 5.3 5.2 4.85 4.89 5.4 5.5
41 29 24 12 8 9 conc med 13 14 27
Fe

915.51 913.41 912.31 912.21 911.61
1.7 3.8 4.9 5.0 5.6
94 70 50 41 41
BIT TC

909.31 909.11 910.71 911.11 911.21 911.41 911.51 911.91 911.81 911.41 911.21
7.9 8.1 6.5 6.1 6.0 5.8 5.7 5.30 5.34 5.8 6.0
41 38 31 24 12 4 5 conc med 9 10 28
Fe

913.41 912.01 911.21 911.11
3.8 5.2 6.0 6.1
100 70 50 41

Top Hyd Rt, 54A 110+50 ±

(Front of Cummins Co)

908.53 908.68 910.18 910.78 911.08 911.28 911.28 911.71 911.68 911.28 911.08
7.0 6.9 5.4 4.8 4.5 4.3 4.3 3.87 3.90 4.3 4.5
41 38 32 24 12 2 3 conc med 8 9 24
Fe

908.81 910.88 911.18 911.28 905.76 906.93 910.77
6.7 4.7 4.4 4.3 7.82 7.65 4.81
65 64 54 46 44 44 44
15" RCP TC FL WINV 15" RCP eB rim cast.

908.18 908.48 910.38 910.58 910.98 911.18 911.57 911.55 911.08 910.98 910.68 911.28
7.4 7.1 5.2 5.0 4.6 4.4 4.01 4.03 4.5 4.6 4.9 4.3
41 37 30 25 12 1 conc med 6 7 23 41 41
Fe TC

911.78 911.58 911.18
3.8 4.0 4.4
84 70 50

STA

+

Δ

-

915.58

109+00

Bit. Ent Rt.

✓

TP

4.54

915.14

4.98

910.60

+08

✓

109+50

✓

110

✓

RG WS
L.P.O. GP
JA AJ
BW

Lt

E

April 22, 1976

Rt

907.58	907.98	910.08	910.48	910.78	911.08	911.40	911.40	910.98	910.88	910.68	910.58	910.88
8.0	7.65	5.1	4.8	4.5	4.18	4.18	4.6	4.7	4.9	5.0	4.7	
41	38	31	24	14	1	conc med	5	6	23	41	50	71
Fe												

911.58
4.0
100

MH 36' Rt 109+10 No. Rim

907.04	910.24	910.44	910.94	911.30	911.30	910.94	910.74	910.64	910.64
8.1	4.9	4.7	4.2	3.84	3.84	4.2	4.4	4.5	4.5
41	30	25	1		5	6	19	41	58
FE				conc median					

910.94
4.2
75

906.54	909.64	910.14	910.54	910.95	910.95	910.54	910.44	910.14	910.74
8.6	5.5	5.0	4.6	4.19	4.19	4.6	4.7	5.0	4.4
42	30	25	1		5	6	18	40	40
FE				conc median				T.C.	

913.64
1.5
75

906.14	909.44	909.64	910.14	910.52	910.52	910.04	909.74	910.34	910.84
9.0	5.7	5.5	5.0	4.62	4.62	5.1	5.4	4.8	4.3
42	29	25	1		5	6	41	41	54
FE				conc median				T.C.	

913.64
1.5
75

912.34
2.8
61

STA

+

K

-

ELEV

915.14

110+50

✓

+57

5.73

909.41

+75

✓

+93

7.29

907.85

+95

WLS
6.8
84
BW

LT

£

RT

4-28-16
CLEAR 55'

906.64	908.14	908.24	909.64	909.94	909.98	909.54	909.34	909.94	910.44
8.5	7.0	6.2	5.5	5.15	5.16	5.6	5.8	5.2	4.7
42	35	26	1		5	6	40	40	54
FE					CONC M&D				
								913.24 19 75	912.04 3.1 60

MH. RT, 30

906.04	908.04	908.44	908.64	909.34	909.74	909.24	909.84	910.24	911.94
9.1	7.1	6.7	6.5	5.8	5.7	5.9	5.3	4.9	3.2
64	45	39	25		18	40	40	53	60
904.65 10.49 66 FL 12" C.M.P.	905.18 12.96 76 FL 36" R.C.P.	904.3 10.84 45 FL 12" C.M.P.							913.04 2.1 75

CB LT, 63

908.16	908.04	908.14	908.64	909.14	909.24	908.94	909.54	910.34	911.54
6.98	7.1	7.0	6.5	6.0	5.9	6.2	6.6	4.8	3.6
85	65	55	25		17	40	40	54	60
CONC									
908.07 7.07 94 CB.									912.94 2.2 75

STA

+

K

-

ELEV.

915.14

+11 +05

E

EXIT RAMP

✓

+17

NORTH GUTTER EXIT RAMP

✓

+31

ENT RT & SOUTH GUTTER ENT. RAMP

✓

+50

NORTH GUTTER ENT. RAMP

✓

W.S
G.A
R.J
BW

LT

Q

RT

4-28-76
CLEAR 57°

908.37	908.24	908.54	909.04	909.04	908.84	909.44	910.14	911.24
6.77	6.9	6.6	6.1	6.1	6.3	5.7	5.0	3.9
85	55	24		18	40	43	54	60
CONC								

912.54
2.8
75

908.90	908.39	908.34	908.94	908.94	908.64	909.44	911.14
6.24	6.75	6.8	6.2	6.2	6.5	6.0	4.0
54	54	29		18	43	54	75
T.C	CONC. GUTTER						

909.58
6.56
85
CONC
GUTTER

909.06
6.08
85
T.C

908.51	908.02	908.24	908.94	908.84	908.54	909.44	910.04
6.63	7.12	6.9	6.2	6.3	6.6	6.7	5.1
66	66	33		19	43	59	75
T.C	CONC GUTTER						

907.89
7.25
85
CONC
GUTTER

908.38
6.76
85
T.C

908.10	907.78	908.24	908.74	908.64	908.34	908.44	908.94
7.04	7.36	6.9	6.4	6.5	6.8	6.7	6.2
57	57	23		20	42	47	48
T.C	CONC GUTTER						T.C

907.47
7.67
85
CONC
GUTTER

907.68
7.46
85
T.C

907.22
7.92
100
CB

910.24
4.9
75

909.74
5.4
55

STA

+

PI

-

ELEV

915.14

111+61

✓

+74

CE

6.86

908.28

5.05

903.23

+77

✓

T.P

1.34

913.74

2.74

912.40

912.40

112+00

W.S
C.A
BT
BW

LT

£

RT

4-28-76
CL 58'

908.08 907.87 908.34 908.74 908.64 908.54 908.24 908.84
7.06 7.25 6.8 6.4 6.5 6.6 6.9 6.3
36 32 17 15 30 40 40
T.C. CONC GUTTER

906.44 901.72
8.7 13.42
59 75
FL 36" R.C.P

910.14 909.34
5.0 5.8
75 56

CB RT 42'

904.94 907.54 908.14 908.54 908.54 908.34 908.84 908.94
10.2 7.6 7.0 6.6 6.6 6.8 6.3 6.2
56 38 22 17 39 39 53

902.54
12.6
65
H₂O

909.14 907.94 906.31
6.0 7.2 8.83
75 66 56
FL 15" R.C.P

TOP HYD IN FRONT OF CUMMINS

903.24 904.14 907.94 908.14 908.44 908.34 908.24 909.24 909.64
10.5 9.6 5.8 5.6 5.3 5.4 5.5 4.5 4.1
68 49 27 15 13 41 65 75

902.70
11.04
10
H₂O

STA	+	Δ	-	ELEV.
		913.74		
112+19	±	ENT	RT.	
✓				
+40			5.91	907.83
+50				
+55				
✓				
+65			6.36	907.38
113+00				
✓				

W.S.
G.A.
B.J.
B.W.

LT

±

RT

4-28-76
CL 600

903.04

10.7
69

903.94

9.8
41

908.04

5.7
25

908.04

5.7
13

908.34

5.4
21

908.14

5.6
40

908.14

5.6
58

908.74

5.0
75

909.34

4.4
100

909.94

3.8

902.70

11.04
72

CENTER MH LT. 14'

902.94

10.8
65

902.94

10.8
41

907.54

6.2
22

907.74

6.0
12

907.94

5.8
20

907.54

6.2
37

907.44

6.3
37

908.04

5.7
T.C.

907.64

6.1
42

908.84

4.9
63

902.74

11.0
75

909.34

4.4
75

CENTER MH RT. 22'

902.24

11.5
40

907.04

6.7
24

907.44

6.3
13

907.64

6.1
12

907.44

6.3
31

907.14

6.6
31

907.74

6.0
T.C.

902.34

11.4
60

902.64

11.1
75

909.34

4.4
75

908.64

4.9
65

906.94

6.8
51

STA

+

A

-

ELEV

913.74

113+50

✓

+60

✓

114+00

✓

T.P

4.09

913.11

4.72

909.02

909.04

+30

10.77

902.34

+50

W.S.
G.A.
B.J.
B.W.

LT

£

RT

4-28-76
CL 600

903.44

10.3
34

906.64

7.1
24

907.14

6.6
12

907.34

6.4
12

907.24

6.6
12

906.64

7.1
28

907.24

6.5
28
T.C

906.34

7.4
43

902.34

11.4
53

902.24

11.5
75

908.24

5.5
75

908.04

5.7
70

907.04

6.7
53

905.24

8.5
43

906.54

7.2
23

907.14

6.6
12

907.34

6.4
12

907.14

6.6
12

906.64

7.1
26
T.C

906.24

7.5
38

905.94

7.8
40

902.52

11.22
43

FL. 24" RT

902.34

11.4
52

902.14

11.6
75

908.24

5.5
75

907.44

6.3
61

906.24

7.5
40

905.54

8.2
32

906.34

7.4
21

906.94

6.8
12

907.14

6.6
12

906.94

6.8
12

906.54

7.2
23
T.C

907.14

6.6
30
T.C

906.54

7.2
35

902.71

11.03
40
H₂O

902.70

11.04
68
H₂O

908.44

5.3
75

908.24

5.5
65

906.34

7.4
44

904.14

9.6
38

TOP 144 DT. ENT. TO DO HRN TRANS.

FL 24" CMP RT

902.61

10.5
35
H₂O

906.31

6.8
26

906.81

6.3
12

906.91

6.2
18

906.51

6.6
18
T.C

907.11

6.0
18

906.41

6.7
28

903.71

9.4
36

904.91

8.2
44

908.41

4.7
75

907.71

5.4
55

STA

+

Δ

-

ELEV

913.11

114+86

✓

115+12 & ENT RT

✓

+36

✓

116+00

✓

W.S.
G.A.
B.S.
B.W.

LT

£

RT

4-28-76
CL 65°

902.01
11.1
55
H2O

904.41
8.7
46

906.31
6.8
26

906.71
6.4

906.91
6.2

906.61
6.5
16

905.41
7.7
39

902.60
10.51
35

FL 12" CMP

902.21
4.9
75

907.31
5.8
51

903.81
9.3
64

904.71
8.4
32

906.11
7.0
23

906.61
6.5
12

906.81
6.3

906.61
6.5
12

906.11
7.0
34

906.91
6.2
38

907.71
5.4
75

908.41
4.7
100

902.01
11.1
68 H2O

902.01
11.1
44
H2O

902.81
10.3
36

905.91
7.2
23

906.61
6.5
12

906.81
6.3

906.61
6.5
12

906.41
6.7
27

905.71
7.4
31

903.18
9.93
36

906.01
7.1
36
FL 24" CMP

908.21
4.9
75

907.31
5.8
48

904.21
8.9
32

906.41
6.7
23

906.61
6.5
12

906.81
6.3

906.61
6.5
12

906.41
6.7
25

904.41
8.7
30

904.21
8.9
38

902.01
11.1
57

908.81
4.3
75

907.91
5.2
51

STA

+

T

-

ELEV.

913.11

116+58

+70

+82

117+00

6.60

906.51

+17

✓

+42

¢ ENT RT

+67

+67

✓

W
GA
BS
BW

4 28-76
CL 650

LT

C

RT

902.61 10.5 75	903.81 10.1 50	904.51 8.6 35	906.41 6.7 25	906.61 6.5 12	906.81 6.3	906.61 6.5 12	906.41 6.7 26	904.61 8.5 30	904.41 8.7 37	908.41 4.7 52	908.91 4.2 75
905.51 7.6 75	905.71 7.4 51	905.21 7.9 33	906.51 6.6 23	906.61 6.5 12	906.81 6.3	906.61 6.5 12	906.71 6.4 25	904.71 8.4 32	904.81 8.3 39	908.51 4.6 53	909.01 4.1 75
903.31 9.8 75	904.81 8.3 53	906.51 6.6 25	906.61 6.5 12	906.71 6.4	906.61 6.5 12	906.51 6.6 27	905.01 8.1 31	904.81 8.3 39	908.61 4.5 52	909.01 4.1 75	

CENTER MH LT 28'

903.41 9.7 75	905.71 7.4 32	906.51 6.6 22	906.61 6.5 12	906.81 6.3	906.61 6.5 12	906.21 6.9 25	906.01 7.1 30	902.78 10.33 35	906.11 7.0 35
								FL 24" CMP	
								908.51 4.6 75	907.81 5.3 48
903.51 9.6 75	905.01 8.1 46	906.41 6.7 22	906.51 6.6 12	906.81 6.3	906.61 6.5 12	906.61 6.5 33	907.21 5.9 53	908.01 5.1 75	908.41 4.7 100
903.31 9.8 75	905.01 8.1 43	906.47 6.7 23	906.51 6.6 12	906.71 6.4	906.51 6.6 12	906.41 6.7 31	903.63 9.48 35	906.31 6.8 35	
								FL 24" CMP	
								908.31 4.8 75	907.61 5.5 58
								906.81 6.3 40	

STA

+

 $\overline{1}$

—

ELEV.

913.11

118+00

✓

TP

2.68

912.31

3.50

909.61

909.63

+35

✓

+68

5.63

906.68

+71

✓

WS
GA
BT
BW

LT

C

RT

4-28-76
CL 65°

904.01 904.91 906.31 906.61 906.81 906.51 906.91 906.11 906.51
9.1 8.2 6.8 6.5 6.3 6.6 6.2 7.0 6.6
50 41 24 12 12 30 35 41
903.51
9.6
75
908.11 907.91
5.0 5.2
75 50

TOP HYDT ENT. MIDWEST TRANS. CO.

904.61 906.51 906.71 906.91 906.61 907.31 907.61 906.71
7.7 5.8 5.6 5.4 5.7 5.0 4.7 5.6
37 26 12 12 35 53 63
903.41 903.01
8.9 9.3
64 75
908.91 908.21
3.4 4.1
75 66

CTR M.A. LT. 14

902.61 904.01 906.61 906.71 906.81 906.71 906.61 905.91 906.01
9.7 8.3 5.7 5.6 5.5 5.6 5.5 6.4 6.3
71 41 24 12 12 24 42 49
901.98
10.33
8.2
H₂O
907.91 908.11
4.4 4.2
75 57

STA

+

K

-

ELEV

91231

119+00

✓

+50

✓

120+00

✓

+50

✓

T.P

596

912.85

5.42

906.89

W.S
6.1A
BT
BW

LT

±

RT

4-28-76
CL-62°

904.01 906.51 906.71 906.81 906.71 906.61 905.61 905.61
8.3 5.8 5.6 5.5 5.6 5.7 6.7 6.7
36 25 12 12 24 31 39

902.21 902.01
10.1 10.3
62 75

908.41 908.71 908.21
3.9 3.6 4.1
75 63 49

902.71 906.51 906.71 906.81 906.81 906.91 905.61 905.41
9.6 5.8 5.6 5.5 5.5 5.4 6.7 6.9
39 22 12 12 24 30 38

902.11 902.01
10.2 10.3
61 66

910.11 910.11 909.81 907.91
2.2 2.2 2.5 4.4
75 69 58 47

902.131 906.51 906.81 906.91 906.91 906.81 905.51 905.41
10.0 5.8 5.5 5.4 5.4 5.5 6.8 6.9
39 24 12 12 24 31 37

902.01
10.3
52
H₂O

911.11 911.11 908.51
1.2 1.2 3.8
75 66 52

902.11 902.71 906.61 906.71 906.91 906.81 906.81 905.61 905.51
10.2 9.6 5.7 5.6 5.4 5.5 5.5 6.7 6.8
45 38 25 12 12 23 28 38

902.01
10.3
59
H₂O

911.61 911.21 908.71
0.7 1.1 3.6
75 66 52

TURNING PT. STA 121+00 TOP P.K.

STA	+	π	-	ELEV
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		912.85		
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121+00				
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✓				
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+50				
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✓				
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122+00				
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		ENT. RT.		
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+50				
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✓				
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T.P.				
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5.96				
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912.33				
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6.48				
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906.37				
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123+00				
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+50				
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WVS
CVA
BS
BW

LT

⊥

RT

4-29-76
CL-45°

901.95 902.55 904.45 906.35 906.65 906.85 906.95 906.85 906.25 906.35 908.35
10.9 10.3 8.4 6.5 6.2 6.0 5.9 6.0 6.6 6.5 4.5
65 43 31 15 12 12 23 30 38 51
H₂O

911.95
0.9
75

902.85 903.75 904.75 906.15 906.85 906.95 907.05 907.05 906.55 907.55 911.25
10.0 9.1 8.1 6.7 6.0 5.9 5.8 5.8 6.3 5.3 1.6
75 40 28 22 12 12 24 30 45 65

911.75
1.1
75

904.15 905.35 905.45 906.35 906.75 906.95 907.05 907.45 908.75 909.75 910.65
8.7 7.5 7.4 6.5 6.1 5.9 5.8 5.4 4.1 3.1 2.2
75 53 26 18 12 12 36 62 75 100

908.05 908.95 908.75 906.45 906.15 906.55 906.75 906.75 906.65 907.35 909.65
4.8 3.9 4.1 6.4 6.7 6.3 6.1 6.1 6.2 5.5 3.2
75 63 53 33 25 12 12 33 48 75

P.K. ⊥ STA 123+00

907.73 907.03 905.53 906.03 906.33 906.43 906.23 906.63 907.63 908.33 908.73
4.6 5.3 6.8 6.3 6.0 5.9 6.1 5.7 4.7 4.0 3.6
75 40 25 12 12 25 40 55 64 75

908.03 906.13 904.93 905.03 905.83 906.13 906.23 906.83 908.23
4.3 6.2 7.4 7.3 6.5 6.3 6.2 6.1 5.5 4.1
75 41 30 23 12 12 25 44 75

STA + π - ELEV

912.33

124+00

¢ ENT. RT.

SIDE SHOT

3.2 909.21 909.24

+17

24" Culvert Lt, 35'

+50

¢ ENT. LT.

+94

24" Culvert Lt, 35'

T.P

7.59

912.11

7.81

904.52

125+00 ✓

W.S.
G.A.
B.J.
B.W.

4-27-76
CLOY 50°

LT

2

RT

907.83	905.83	903.43	904.83	905.43	905.83	905.83	905.33	907.33	908.33
4.5	6.5	8.9	7.5	6.9	6.5	6.5	7.0	5.0	3.0
75	40	34	24	12		12	26	48	75

TOP NYA SO ENT TO AMERICAN

907.83	905.83	905.23	902.23	904.93	905.33	905.63	905.73	905.23	907.43	909.23
4.5	6.5	7.1	10.10	7.4	7.0	6.7	6.6	7.1	4.9	3.1
75	40	35	35	26	12		12	25	50	75

FL. 24" C.M.P.

907.73	906.13	905.63	905.23	905.43	905.33	904.93	905.93	908.33	909.23
4.6	6.2	7.3	7.1	6.9	7.0	7.4	6.4	4.0	3.1
75	41	21	12		12	24	40	61	75

907.9	907.3	905.3	903.9	901.3	904.5	904.7	904.9	904.8	904.6	905.3	907.8
4.4	5.0	7.0	8.4	11.05	7.8	7.6	7.4	7.5	7.7	7.0	4.5
80	75	40	34	34	24	12		12	24	42	75

FL. 24" C.M.P.

Top of Rock

905.2	902.7	902.7	904.2	904.4	904.7	904.9	904.8	904.5	904.9	905.7	907.7
6.9	9.4	9.4	7.9	7.7	7.4	7.2	7.3	7.6	7.2	6.4	4.4
41	37	32	30	25	12		12	21	34	46	75

→ 907.3 907.1 907.9

4.8	5.0	4.2
67	69	73

STA

+

π

-

ELEV

9.12.11

+50

✓

126+00

✓

+50

✓

127+00

£ ENT RT

W.S.
GA.

BT
BW

LT

2

RT

4-29-76
cldy 50°

902.8 901.2 901.5 904.1 904.3 904.5 904.3 904.0 904.6 906.7

93	10.9	10.6	8.0	7.8	7.6	7.8	8.1	7.5	5.4
34	33	25	24	12		12	25	46	75

904.6 906.5 905.9 907.4

75	5.6	6.2	4.7
41	73	75	80

904.4 901.7 901.7 902.8 903.8 904.1 903.9 903.7 905.1 906.7

7.7	10.4	10.4	9.3	8.3	8.0	8.2	8.4	7.0	5.4
40	31	24	23	12		12	28	55	75

906.2 905.6 906.9

5.7	6.5	5.2
73	75	80

906.4 904.2 901.5 903.1 903.9 904.1 903.9 903.4 904.8 906.7

5.7	7.9	10.6	9.0	8.2	8.0	8.2	8.7	7.3	5.4
73	40	27	22	12		12	32	50	75

906.0 907.5

6.1	4.6
75	80

Hyd.

5.98

901.9 901.3 903.3 904.0 904.1 903.9 903.3 904.6 906.3

10.2	10.8	8.8	8.1	8.0	8.2	8.8	7.5	5.8
33	29	21	12		12	33	51	75

8.0 904.1 906.7 906.2 907.6

40	5.4	5.9	4.5
	73	75	80

STA

+

K

-

ELEV

9/2.11

BM

5.61

911.80

5.95

906.16

906.19

127+50

✓

✓

128+00

✓

128+50

✓

129+00

WS
GA
BJ
BW

LT

2

RT

4-29-76
cldy 50°

TOP NUT HYD NO. ENT TO AMERICAN

905.8
904.2
901.9
901.8
903.5
903.9
904.1
903.8
903.3
903.0
904.0
904.5

6.0	7.6	7.9	10.0	8.3	7.9	7.7	8.0	8.5	8.8	7.8	7.3
63	40	34	28	19	12		12	25	39	50	75

906.8
906.4
907.8

5.0	5.4	4.0
73	75	80

906.9
905.8
904.4
901.8
901.8
903.5
903.8
904.1
903.9
903.5
902.6
902.9
904.2
904.4

4.9	6.0	7.4	10.0	10.0	8.3	8.0	7.7	7.9	8.3	9.2	8.9	7.6	7.4
73	62	49	32	28	19	12		12	25	33	43	51	75

906.3
907.9

5.5	4.1
76	81

904.5
902.0
901.8
903.3
903.8
904.0
903.8
903.4
902.5
903.3
904.5
904.8

7.3	9.8	10.0	8.5	8.0	7.8	8.0	8.4	9.3	8.5	7.3	7.0
40	33	28	22	12		12	24	31	41	50	75

906.2
907.1
906.5
907.9

5.6	4.7	5.3	3.9
64	73	76	81

907.9
906.7
906.9
904.2
901.7
903.3
903.9
904.1
903.8
903.2
904.9
902.1
904.2
904.4

3.9	5.1	4.9	7.6	10.1	10.1	8.5	7.7	7.7	8.0	8.6	9.9	9.7	7.6	7.4
80	76	73	40	32	27	20	12		12	23	31	44	51	75

STA

+

K

-

ELEV

911.80

129+50

129+95

15" CMP RT 35'

130+11

ENT. RT.

+26

15" CMP RT 35'

+50

✓

WS
GA
BS
RW

LT

♀

RT

4-29-76
cidy 53°

907.8 906.8 906.9 904.1 901.8 901.7 903.0 903.6 903.7 904.1 903.8 903.2 901.8 901.8 902.4 904.3 904.6
40 50 49 77 10.0 10.1 8.8 82 7.9 7.7 8.0 8.6 10.0 10.0 7.4 7.5 7.6
81 77 74 40 34 28 22 17 12 12 23 29 40 46 50 75

907.7 906.5 906.9 904.0 901.7 901.4 903.1 903.9 904.2 903.9 902.9 F.L. 900.60 902.6 903.9 903.2
4.1 5.3 4.9 7.8 10.1 10.2 8.7 7.9 7.6 7.9 8.9 11.19 9.2 7.9 8.6
81 77 74 40 34 28 22 12 12 26 35 35 50 75

904.2 904.0 903.5 903.7 904.2
7.2 7.8 8.3 8.1 7.6
12 24 46 75

907.5 905.8 906.4 903.8 901.9 901.6 903.2 904.0 904.2 904.1 903.6 900.0 903.2 903.9 904.3
4.3 6.0 5.4 8.0 9.9 10.2 8.6 7.8 7.6 7.7 8.2 11.83 8.6 7.9 7.5
81 77 74 40 33 26 23 12 12 24 35 35 50 75

901.7 901.7 903.3 903.9 904.2 904.1 903.6 901.3 901.3
10.1 10.1 8.5 7.9 7.6 7.7 8.2 10.5 10.5
33 27 22 12 12 12 23 27 39

904.1 906.5 905.8 907.2 904.1 903.8
7.7 5.3 6.0 4.6 7.7 8.0
40 75 77 81 75 50

STA	+	$\bar{\Delta}$	-	ELEV
		911.80		
131+00				
✓				
TP	5.38	909.57	7.61	904.19
+07			5.95	903.62
+20			5.70	903.87
+22			6.22	903.35
+26		36" CMP	INVERT	LT 48'
+40				

WS
GA
BI
BW

LT

E

RT

7-27-76
cloudy 52°

901.8	902.1	903.5	903.8	904.2	904.0	903.5	901.3	901.2
10.0	9.7	8.3	8.0	7.6	7.8	8.3	10.5	10.6
34	28	24	12		12	23	31	43

904.4	905.7		904.1	903.8
7.4	6.1		7.7	8.0
40	75		75	50

PK E STA 131+00

MH LT 18

MH LT 14

MH RT 22

902.6	902.2	902.8	900.43	902.3	903.3	904.0	904.3	904.1	903.4	901.7	901.0	901.0
7.0	7.4	6.8	7.14	6.3	6.3	5.6	5.3	5.5	6.2	7.9	8.6	8.6
75	67	48	48	33	23	12		12	27	38	59	75

FL

903.5	903.2	903.5	904.1	904.3	904.1	903.1	902.9	903.0	902.9
6.1	6.4	6.1	5.5	5.3	5.5	6.5	6.7	6.6	6.7
75	57	35	12		12	27	59	75	100

STA

+

K

-

ELEV

909.57

+53

Co. Rd C2

+66

+77

36" cnp LT 48'

+83

5.94

903.63

side shot

3.52

906.05

906.06

132+00

✓

WS
GA
BS
BW

LT

E

RT

4-30-76
cldy 51°

904.1	904.0	903.7	903.7	904.2	904.4	904.1	903.8	903.8	903.7	903.7
5.5	5.6	5.9	5.9	5.4	5.2	5.5	5.8	5.8	5.9	6.1
100	75	54	33	12		12	32	55	75	100

903.6	903.4	903.5	904.2	904.2	904.1	903.5	903.3	903.3
6.0	6.2	6.1	5.4	5.2	5.5	6.1	6.3	6.3
75	59	38	12		12	37	61	75

901.0	901.3	899.9	904.3	904.4	904.6	904.1	903.5	903.1	902.4	901.4
8.6	8.3	9.58	5.3	5.2	5.0	5.5	6.1	6.5	7.2	8.2
75	62	48	28	12		12	23	37	58	75

MH RT 23'

Top Hyd NE cor Co. Rd C2

903.9	900.9	900.9	903.8	904.5	904.9	904.5	903.8	902.5	901.8	901.4
5.7	8.7	8.7	5.8	5.1	4.7	5.1	5.8	7.1	7.8	7.7
40	31	26	20	12		12	21	28	49	75

903.9	905.2	904.0
5.7	4.4	5.6
65	71	75

STA

+

Δ

-

ELEV

909.57

+50

✓

133+00

✓

+50

✓

WS
GA
BJ
BW

LT

Σ

RT

4-30-76
cldy 51°

900.7 900.8 901.4 904.8 905.2 905.2 904.3 902.4 901.6
8.9 8.8 5.2 4.8 4.4 4.4 5.3 7.2 8.0
31 24 18 12 12 12 21 26 34

904.3 904.4 905.5 904.3 902.2 902.1
5.3 5.2 4.1 5.3 7.4 7.5
37 61 67 75 75 54

900.7 900.7 901.4 905.2 905.6 905.4 904.7 902.6 901.9 903.0
8.9 8.9 5.2 4.4 4.0 4.2 4.9 7.0 7.7 6.6
30 23 19 12 12 12 19 25 31 51

905.3 905.0 905.5 904.8 902.8
4.3 4.6 4.1 4.8 6.8
37 63 71 75 75

900.6 900.6 905.2 905.5 905.8 905.6 905.1 902.9 902.4
7.0 7.0 4.4 4.1 3.8 4.0 4.5 6.7 7.1
30 23 19 12 12 12 19 24 35

905.4 904.3 904.0 904.4 905.6 903.4
4.2 5.3 3.6 5.2 6.0 6.2
36 59 65 75 75 50

STA

+

PI

-

ELEV

909.57

134+00

✓

+50

✓

BM

2.05

908.93

2.73

906.84

906.88

135+00

✓

WS
GA
BJ
BW

LT

E

Rt

4-30-76
cldy to
light rain.
50°

905.7 900.6 900.8 905.6 905.7 905.9 905.8 905.4 903.0

3.7	7.0	8.8	4.1	3.9	3.7	3.8	4.2	6.6
37	28	25	16	12		12	19	25

904.3 906.4 904.4 903.3 903.7 902.1

5.3	3.2	5.2	6.3	5.9	7.5
61	67	75	75	56	34

905.8 900.3 900.9 905.1 905.6 906.1 905.9 905.4 902.1 901.4

3.8	7.3	8.7	4.5	4.0	3.5	3.7	4.2	7.5	8.2
38	30	24	16	12		12	19	26	35

904.7 909.5 906.3 901.6 902.9

4.9	0.1	3.3	8.0	7.7
58	68	75	75	52

TOP NUT HYD 500' N OF C²

905.2 904.0 902.6 901.1 905.5 905.7 906.0 905.8 905.2 902.0 901.0 901.1

3.7	2.9	6.3	7.7	3.4	3.2	2.9	3.1	3.7	6.9	7.9	7.8
57	38	29	23	16	12		12	18	26	34	52

0.0
66

8.3
75

STA	+	K	-	ELEV
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		900.93		
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35+36		18" CMP	LT 23'	
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✓

453		⌀	ENT LT	
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468		18" CMP	LT 23'	
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✓

36+12		24" X-CULVERT CMP	LT 24'; RT 38'	
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WS
GA
BS
BW

LT

2

4-30-76
LT Rain
RT 50°

905.4 901.0 900.21 905.6 905.8 906.0 905.9 905.3 902.0 900.9 900.8

3.5	7.9	8.72	3.3	3.1	2.9	3.0	3.6	6.9	8.0	8.1
36	27	23 FL	17	12		12	18	27	39	60

905.5 908.9

9.4	0.0
54	66

900.3

8.5
75

906.5 906.2 905.8 905.9 906.0

2.4	2.7	3.1	3.0	2.9
75	48	28	12	

904.7 899.79 905.6 905.8 906.1 905.9 905.2 902.4 901.0

4.2	9.14	3.3	3.1	2.8	3.0	3.7	6.5	7.9
35	23 FL	17	12		12	19	28	40

905.6 906.2

3.3	2.7
47	75

900.2

8.7
75

904.6 900.9 905.6 905.7 906.0 905.9 905.4 899.49 899.7

4.3	8.0	8.92	3.6	3.2	2.9	3.0	3.5	9.44	9.2
37	30	24	19	12		12	23	38	47

904.9 906.2 904.9

4.0	2.7	4.0
55	65	75

900.2 901.0

8.7	7.9
75	49

STA	+	π	-	ELEV
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		908.93		
--	--	--------	--	--

136+50				
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✓				
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137+00				
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✓				
---	--	--	--	--

+50				
-----	--	--	--	--

✓				
---	--	--	--	--

+68				
-----	--	--	--	--

		3.64	905.29	
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WS
GA
BJ
RW

LT

Σ

4-30-76
RT cldy 52°

902.4 903.2 905.1 905.8 906.1 905.9 905.3 899.5 899.6

6.5	5.7	3.8	3.1	2.8	3.0	3.6	9.4	9.4
32	24	20	12		12	19	34	44

903.8 903.0 903.3 901.0 900.9 900.8

5.1	5.9	5.6	7.9	8.0	8.0
37	57	75	75	59	46

902.2 903.5 902.0 902.6 905.2 905.7 906.1 905.9 904.9 899.4 899.5

6.7	5.4	6.9	6.0	3.7	3.2	2.8	3.0	4.0	9.5	9.3
67	61	49	32	20	12		12	22	32	43

902.5 904.0 901.1 901.6

6.4	5.9	7.8	7.3
75	75	72	48

903.1 904.3 905.3 905.8 906.0 905.8 905.3 901.8 899.3

5.8	4.6	3.5	3.1	2.9	3.1	3.6	7.1	9.6
52	31	22	12		12	21	29	32

901.7 902.3 900.7 901.2 899.4

6.2	6.6	8.2	7.6	9.5
75	75	69	47	44

MH LT 22'

STA	+	K	-	ELEV
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		908.93		
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137+99		18" x-culvert RCP		RT 30' : LT 24'
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✓				
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138+50				
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✓				
---	--	--	--	--

139+00				
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✓				
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WS
GA
BJ
BW

LT

E

RT

4-30-76
cloudy 53

901.4	901.8	FL 901.02	905.2	905.6	905.9	905.7	905.3	FL 900.38	899.7
7.5	7.1	7.91	3.7	3.3	3.0	3.2	3.6	8.55	9.2
75	42	24	20	12		12	19	30	35

700.6	900.7	899.4
8.3	8.0	9.5
75	47	45

907.4	903.1	903.4	905.4	905.7	906.0	905.9	905.5	899.5	899.7
5.5	5.8	5.5	3.3	3.2	2.9	3.0	3.4	9.4	9.2
75	63	31	22	12		12	22	34	46

902.0	901.1	901.2
6.9	7.8	7.7
75	70	49

903.9	903.8	905.7	906.1	906.1	906.0	905.3	899.8	899.6
5.0	5.1	3.2	2.8	2.3	2.9	3.6	9.1	9.3
75	44	21	12		12	21	32	42

905.0	904.3
3.9	4.6
75	63

STA	+	π	-	ELEV
-----	---	---	---	------

		908.93		
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BM	4.89	913.37	0.49	908.44	908.48
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139+27		SPECIAL	STORM	STRUCT.	RT 30'
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✓

151		ENT	RT
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194		ENT	LT
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140+00

WS WS
GA GA
BJ BJ
BW BW

LT

£

RT

4-30-76
cldy 55°

5-3-76
clear 42°

TOP NUT HYD SO. ENT DATA GRAPH INC

8.3 75	7.9 57	7.8 38	7.5 22	7.1 12	7.0	7.2 12	7.7 19	7.72 30	15.13 30
905.1	905.5	905.4	905.9	906.3	906.4	906.2	905.7	905.6	905.4

7.8 75	7.9 65	8.0 53	9.8 34
905.6	905.5	905.4	905.1

7.2 75	7.1 42	7.4 29	7.0 12	6.9	7.1 12	7.5 39	7.5 53	7.3 75
906.2	906.3	906.0	906.4	906.5	906.3	905.7	905.9	906.1

6.5 75	6.2 49	7.1 19	6.7 12	6.6
906.9	907.2	906.3	906.7	906.8

4.1 59	4.5 37	6.3 29	7.0 19	6.7 12	6.5	6.5 12	6.7 19	6.7 49	5.9 75
909.3	908.9	907.1	906.4	906.7	906.9	906.9	906.7	906.7	907.5

4.8 75
908.6

STA	+	K	-	ELEV
-----	---	---	---	------

		913.37		
--	--	--------	--	--

140+50				
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141+00				
--------	--	--	--	--

+10				
-----	--	--	--	--

	¢	ENT	LT	
--	---	-----	----	--

+22				
-----	--	--	--	--

+29				
-----	--	--	--	--

	MH	LT 22'		
--	----	--------	--	--

		5.91		
--	--	------	--	--

		907.46		
--	--	--------	--	--

+36				
-----	--	--	--	--

	¢	ENT	LT : RT	
--	---	-----	---------	--

+53				
-----	--	--	--	--

GA
BJ
BW

LT

£

RT

5-3-76
clear 43"

910.7	910.8	910.3	907.0	907.2	907.4	907.3	907.1	908.5	909.7
2.7	2.6	3.1	6.4	6.2	6.0	6.1	6.3	4.9	3.7
75	56	35	22	12		12	20	44	75

910.5	910.6	910.2	907.1	907.5	907.6	907.4	907.8	909.0	909.6	910.1
2.9	2.8	3.2	6.3	5.9	5.8	6.0	5.6	4.4	3.8	3.2
75	51	34	22	12		12	21	39	60	75

910.4	909.8	907.1	907.5	907.6
3.0	3.6	6.3	5.9	5.8
75	52	21	12	

912.7	911.1	908.5	907.1	907.5	907.6	907.6	908.4	908.9	909.1
0.7	2.3	4.9	6.3	5.9	5.8	5.8	5.0	4.5	4.3
75	47	35	20	12		12	37	58	75

912.8	912.0	909.5	907.3	907.4	907.6	907.5	907.9	908.4	908.6
0.6	1.4	3.9	6.1	6.0	5.8	5.9	5.5	5.0	4.8
75	63	40	20	12		12	35	54	75

912.4	911.1	909.8	907.7	907.5	907.7	907.6	907.6	907.9	908.2
1.0	2.3	3.6	5.7	5.9	5.7	5.8	5.8	5.5	5.2
75	51	33	23	12		12	33	54	75

STA	+	π	-	ELEV
-----	---	-------	---	------

		913.37		
--	--	--------	--	--

+62				
-----	--	--	--	--

+91	$\neq$	ENT	LT	RT
-----	--------	-----	----	----

142+00				
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TP	5.73	913.40	5.70	907.67
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+50				
-----	--	--	--	--

+75	$\neq$	ENT	RT	
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WS
GA
BJ
BW

LT

£

RT

5-3-76
clear 430

912.7	909.9	907.7	907.5	907.7	907.5	906.3	905.7	907.7
0.7	3.5	5.7	5.9	5.7	5.9	7.1	7.7	5.7
75	34	23	12		12	31	49	75

911.6	909.5	907.7	907.5	907.7	907.6	906.2	906.0	905.4
1.8	3.9	5.7	5.9	5.7	5.8	7.2	7.4	7.8
75	47	23	12		12	28	50	75

912.2	911.2	909.2	907.3	907.6	907.7	907.6	906.3	906.0	906.3
1.2	2.2	4.2	6.1	5.8	5.7	5.8	7.1	7.4	7.1
75	58	33	18	12		12	27	46	75

PK £ 142 + 00

910.6	908.9	907.5	907.8	907.8	907.6	907.0	906.7	907.1
2.8	4.5	5.9	5.6	5.6	5.8	6.4	6.7	6.3
75	45	20	12		12	21	49	75

907.9	907.6	906.9	907.4	907.4
5.5	5.8	6.5	6.0	6.0
12		34	53	75

STA	+	π	-	ELEV
-----	---	---	---	------

		913.40		
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143+00				
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+40				
-----	--	--	--	--

	£	ENT	LT	
--	---	-----	----	--

+68				
-----	--	--	--	--

	£	ENT	RT	
--	---	-----	----	--

144+00				
--------	--	--	--	--

+42				
-----	--	--	--	--

	£	ENT	RT	
--	---	-----	----	--

+67				
-----	--	--	--	--

WS
CA
BJ
BW

LT

£

RT

5-3-76
Clear 43°

2.7	3.7	5.1	5.6	5.6	5.4	5.6	6.1	7.0	6.4	5.54
75	61	38	20	12		12	20	29	36	72
910.7	909.7	908.3	907.8	907.8	908.0	907.8	907.3	906.4	907.0	907.86

CONC

3.4	4.0	4.7	5.5	5.2	5.0	5.1	6.5	6.1	5.9
75	68	36	21	12		12	28	53	75
910.0	909.4	908.7	907.9	908.2	908.4	908.3	906.9	907.3	907.5

4.1	4.7	5.7	5.2	4.9	4.7	4.9	5.7	5.9	6.0
75	63	39	19	12		12	26	50	75
909.3	908.7	907.7	908.2	908.5	908.7	908.5	907.7	907.5	907.4

4.6	4.7	4.2	4.9	4.6	4.4	4.7	4.9	5.3	5.2
75	57	39	22	12		12	20	49	72
908.8	908.7	909.2	908.5	908.8	909.0	908.7	908.5	908.1	908.2

2.6	2.5	3.8	4.8	4.4	4.2	4.3	4.7	4.6	4.7
75	55	40	23	12		12	29	52	75
910.8	910.9	909.6	908.6	909.0	909.2	909.1	908.7	908.8	908.7

1.5	1.6	1.8	4.8	4.4	4.2	4.3	4.6	3.6	4.1	4.1
75	63	38	25	12		12	21	29	57	75
911.9	911.8	911.6	908.6	909.0	909.2	909.1	908.8	909.8	909.3	909.3

STA	+	π	-	ELEV
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		913.40		
--	--	--------	--	--

144+79

TP	5.84	915.10	4.14	909.26
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145+00

+50

+70	$\neq$	ENT	RT
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146+00

WS
GA
BJ
BW

LT

£

RT

5-3-76
P.C. 44°

911.7	911.6	911.4	908.8	909.0	909.3	909.1	908.7	908.5	909.3	909.3
1.7	1.8	2.0	4.6	4.4	4.1	4.3	4.7	4.9	4.1	4.1
75	61	39	25	12		12	23	29	66	75

PK £ STA 145+00

912.6	912.2	911.1	908.3	909.0	909.3	909.1	908.5	909.4	910.0
2.5	2.9	4.0	6.8	6.1	5.8	6.0	6.6	5.7	5.1
75	59	37	24	12		12	23	49	75

914.20	913.30	912.80	908.4	909.2	909.3	909.2	908.7	909.6	910.4	910.0
0.9	1.8	2.3	6.7	5.9	5.8	5.9	6.4	5.5	4.7	5.1
75	57	42	24	12		12	25	44	59	75

909.4	909.3	909.3	909.8	909.6
5.7	5.8	5.8	5.3	5.5
	12	23	56	75

912.8	908.0	909.1	909.2	909.4	909.5	908.6	909.8	910.2
2.3	7.1	6.0	5.9	5.7	5.6	6.5	5.3	4.9
40	24	19	12		12	25	33	66

913.6	913.6
1.5	1.5
60	75

STA

+

π

-

ELEV

915.10

146+24

✓

+ 45

6.25

908.85

+52

+60

4 DITCH RT

+ 67

WS
GA
BS
BN

LT

E

RT

5-3-76
P.C. 43°

910.9 909.4 907.8 908.9 909.4 909.4 909.4 908.5 909.9 910.9

4.2 5.5 7.3 6.2 5.7 5.7 5.7 6.6 5.2 4.9
39 31 25 19 12 12 12 25 33 66

912.4 912.6

2.7 2.5
52 75

MH LT 17

906.8 906.9 906.3 907.3 908.7 909.3 909.4 909.3 908.0 909.4 909.3 909.9

8.3 8.2 6.8 7.8 6.4 5.8 5.7 5.8 7.1 5.7 5.8 5.2
75 56 33 28 21 12 12 12 26 35 55 75

909.4 909.3 908.4 907.7 907.2 906.6 906.4

5.7 5.8 6.7 7.4 7.9 8.5 8.7
12 21 28 44 64 75

905.8 905.7 907.3 907.0 908.7 907.2 907.4 907.3 908.5 909.1 908.8 908.4

9.3 9.4 7.8 8.1 6.4 5.9 5.7 5.8 6.6 6.0 6.3 6.7
75 53 34 28 20 12 12 12 20 28 45 75

STA	+	Δ	-	ELEV
		915.10		
147+00				
TP	3.26	912.40	5.96	909.14
146+35			3.50	
✓	3.01		3.01	909.39 (909.38)
+50				
148+00				
✓				

5-3-76
P.C. 43

11.1 75	11.3 62	10.8 43	6.7 20	6.2 12	6.0 12	6.1 12	6.4 20	6.0 40	5.7 25	5.7 75
904.0	903.8	904.3	908.4	908.9	909.1	909.0	908.7	909.1	909.4	909.4

PK ϕ STA 147+00

CENTER MH STA. 146+35 LT 16'

TOP NUT HYD 125' N H₀. # 2010

903.0	903.3	904.1	908.2	908.6	908.7	908.6	908.2	908.7	908.8	909.2
9.4	9.1	8.3	4.2	3.8	3.5	3.8	4.2	4.2	4.4	3.2
75	61	36	18	12		12	20	30	50	75

[illegible]

STA

+

A

-

ELEV

912.40

148+16

✓

+21

6.35 906.05

+21

8.96 903.44

+24

✓

+50

✓

WS
GA
BS
BW

LT

£

RT

5-3-76
P.C. 45°

303.7 906.4 907.8 908.3 908.5 908.2 907.7 904.5 907.4

8.7	6.0	4.6	4.1	3.9	4.2	4.7	7.9	5.0
40	27	18	12		12	19	29	35

903.0
9.4
75

902.4 902.8
10.0 9.6
65 55
H2O

CENTER MH LT, 24'

CENTER MH LT 48'

903.2 904.2 907.9 908.3 908.5 908.2 907.7 902.9 902.9

9.2	8.2	4.5	4.1	3.9	4.2	4.7	8.5	9.5
63	37	18	12		12	18	27	45

903.0
9.4
75

902.4
10.0
69
H2O

902.7 904.6 907.6 908.2 908.4 908.1 907.6 903.5 902.8

9.7	7.8	4.6	4.2	4.0	4.3	4.8	8.9	9.6
43	25	16	12		12	18	25	42

903.0
9.4
75

902.4
10.0
75
H2O

STA

+

π

—

ELEV.

912.40

149+00

✓

+ 37

✓

+54

€ ENT. LT.

+69

✓

GA
BT
BW

5-3-76
45°C

LT

♀

RT

903.7

907.8

908.0

908.2

907.8

907.3

903.4

902.0

8.7
29

4.6
16

4.4
12

4.2
12

4.6
12

5.1
17

9.0
25

10.4
40

902.4

903.0

9.8
39

9.4
75

905.9

906.0

902.1

6.5
75

6.4
68

10.3
55

902.04

907.6

907.9

908.0

907.8

907.3

903.4

901.8

10.36
35
FL 12"SCP

4.8
18

4.5
12

4.4
12

4.6
12

5.1
19

9.0
25

10.6
39

902.7

902.80

9.7
53

9.6
75

907.5

908.7

4.9
75

3.7
63

904.30

904.8

906.9

907.9

908.0

8.1
75

7.6
60

5.5
32

4.5
12

4.4

903.5

901.34

907.1

907.8

907.9

907.7

906.8

903.5

901.3

8.9
53

11.06
35

5.3
21

4.6
12

4.5

4.7
12

5.6
19

8.9
24

11.1
29

903.0

907.9

909.0

902.2

9.4
75

4.5
75

3.4
51

10.2
38

STA	+	$\bar{A}$	-	ELEV.	
		912.40			
149+73			11.55	900.85	
+75			5.18	907.22	
+90					
✓					
+ 19			12.34	909.06	
150+25					
✓					

W
GA
BJ
RW

LT

✗

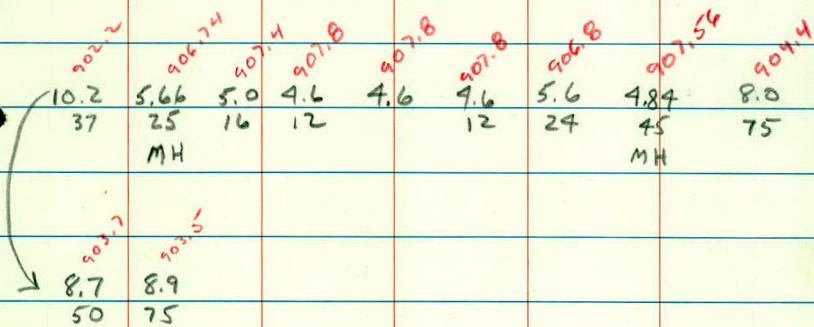
RT

RT

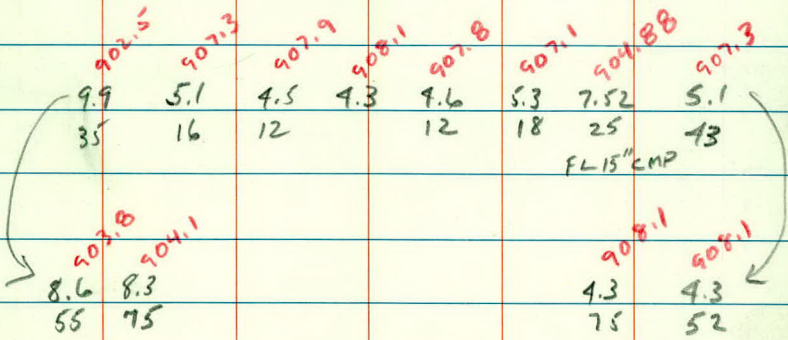
5-3-76
P.C 450

18" RCP RT 30'

CENTER MH RT. 17'



W. END 24" RCP LT 31'



STA

+

$\overline{\Delta}$

-

ELEV

912.40

150+52

✓

+68

¢ ENT, LT

+82

✓

151+00

✓

WS
BA
BJ
BW

5-3-76
P.C. 45°

903.8 LT 907.7 908.1 908.2 908.0 RT 907.5 905.1

8.6	4.7	4.3	4.2	4.4	4.9	7.2	4.9
30	11	12		12	17	24	26

903.7 904.0

8.7	8.4
45	75

907.6 909.4

30
75

904.9 905.0 906.1 908.1 908.2

7.5	7.4	6.3	4.3	4.2
75	50	32	12	

903.6 907.2 908.1 908.3 908.2 907.7 905.4 907.3

8.8	5.2	4.3	4.1	4.2	4.7	7.0	5.1
39	20	12		12	17	24	37

902.8

9.6
75

908.2

4.2
75

903.8 907.2 908.0 908.3 908.1 907.7 905.3 907.4

8.6	5.2	4.4	4.1	4.3	4.7	7.1	5.0
32	18	12		12	18	24	39

903.2 903.0

9.2	9.4
50	75

904.7

2.7
75

STA	+	π	-	ELEV	
		912+40			
TP	4.83	913.12	4.11	908.29	
151+18	€	ENT RT			
+60					
✓					
+71	€	ENT RT			
+79					
✓					

GA
BT
BW

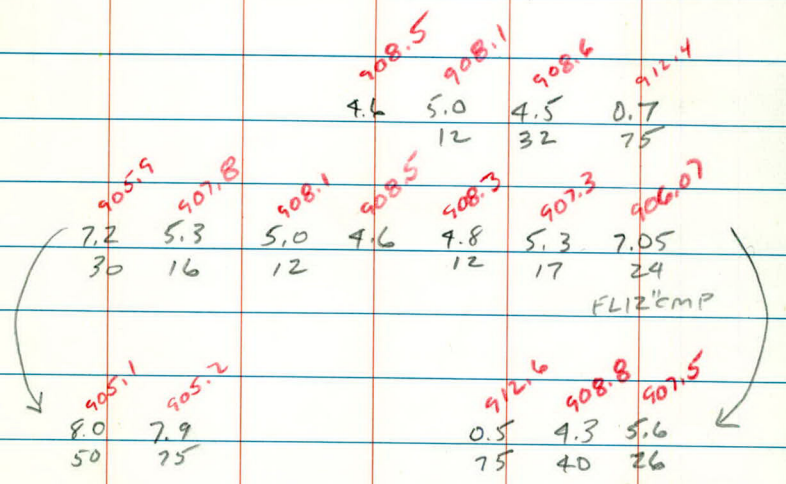
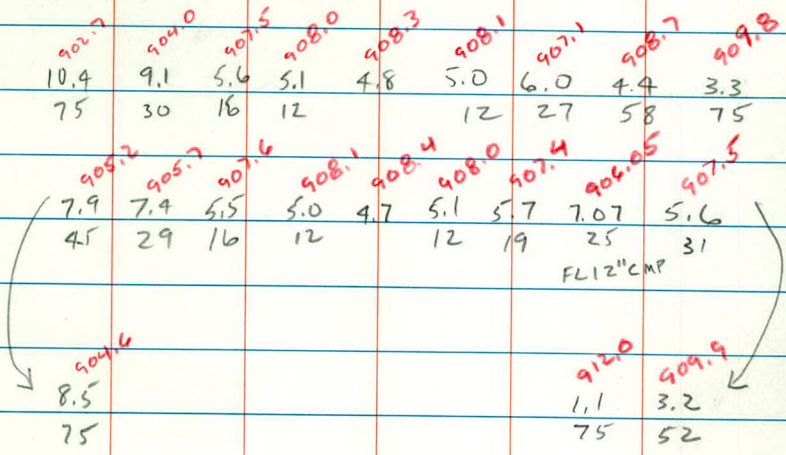
LT

±

RT

5.4-76
clear 450

PK ± STA. 151+00



STA

+

π

-

ELEV

913.12

151+92

¢

ENT

LT

152+00

✓

+40

✓

+67

15" CMP RT

GA
RT
BW

LT

C

RT

5-4-76
clear, 50°

405.3
7.8 6.9 5.8 4.9 4.6
75 37 21 12

405.2 406.2 407.3 408.2 408.6
7.9 6.02 5.0 4.9 4.6 4.8 5.2 6.6 4.1 0.6
43 24 15 12 12 17 26 41 75
MH

403.7
9.4
75

402.4 405.2 408.0 408.4 408.7 408.6 408.4 406.8 409.8 912
9.7 7.9 5.1 4.7 4.4 4.5 4.7 6.3 3.3 0.
67 35 16 12 12 16 24 41 7

403.1
10.0
75

403.2 404.7 408.2 408.7 408.9 408.7 408.4 406.86
9.9 8.4 4.9 4.4 4.2 4.4 4.7 6.26
75 40 17 12 12 16 23

FL 15" CMP

913.1 911.1 908.5
0.0 2.0 4.6
75 49 29

STA	+	π	-	ELEV
		913.12		
152+78		ENT.	RT	
+86		15" CMP	RT	
✓				
T.P.	7.55	916.78	3.89	909.23
153+00				
✓				
+10		15" CMP	RT	
✓				

5-4-76
CLEAR 50°

8.5

4.6
26

26

2.5

43

P.K. & STA. 153+00

909.22
L 9

901

36

912.25

4.5

58

909.4

72

1.2

907.28

900
61

9.3

909.4

7.2

1.2

FL 15" EMP

21-18

411.

5.0

STA	+	π	-	ELEV
-----	---	-------	---	------

		916.78		
--	--	--------	--	--

153+22				
--------	--	--	--	--

	ENT	RT		
--	-----	----	--	--

+35				
-----	--	--	--	--

	15" CMP	RT		
--	---------	----	--	--

✓				
---	--	--	--	--

+60				
-----	--	--	--	--

✓				
---	--	--	--	--

+92				
-----	--	--	--	--

	6.74	910.04		
--	------	--------	--	--

154+00				
--------	--	--	--	--

✓				
---	--	--	--	--

GA
BJ
BW

5-4-76
CLEAR 550

909.48 7.3
909.38 7.4 12
909.68 7.1 21
911.78 4.8 46
914.18 2.6 75

907.38 9.4 28
909.08 7.7 16
909.38 7.4 12
909.68 7.1 12
909.48 7.3 12
909.08 7.7 19
907.94 8.84 23
909.18 7.6 25

FL 15" CMP

906.78 10.0 40
910.78 6.0 65
910.78 6.0 75

914.68 2.1 75
910.98 5.8 35

908.08 8.7 39
908.28 8.5 26
908.38 7.4 15
909.68 7.1 12
909.98 6.8
909.78 7.0 12
909.38 7.4 17
908.68 8.1 24
911.88 4.9 39

911.88 4.9 65
912.98 4.4 75

915.08 1.7 75

MH LT. 14'

909.28 7.5 26
910.08 6.7 16
910.18 6.6 12
910.48 6.3
910.18 6.6 12
909.78 7.0 18
909.18 7.6 26
911.58 5.2 35
910.38 6.4 53
912.38 4.4 69
912.18 4.6 75
915.78 1.0 75

STA	+	π	-	ELEV
		916.78	909.48 7.30	
154+06				

+32		15" CMP	RT	
-----	--	---------	----	--

✓

+44	⊕	ENT	RT	
-----	---	-----	----	--

+62	⊕	ENT	RT	
-----	---	-----	----	--

+71		15" CMP	RT.	
-----	--	---------	-----	--

✓

6A
8J
BW

LT

E

RT

5-4-76
Clear 600

MH LT. 31'

910.18

6.6
22

910.28

6.5
17

910.48

6.3
12

910.88

5.9
12

910.58

6.2
18

910.48

6.3
23

908.30

8.98
28

910.58

6.2
28

FL 15" CMP

911.78

5.0
37

911.78

5.0
75

915.58

1.2
75

914.68

2.1
69

912.48

4.3
61

911.68

5.1
36

910.98

5.8

910.78

6.0
12

910.88

5.9
26

911.68

5.1
50

912.98

3.8
75

911.28

5.5

911.08

5.7
12

910.78

6.0
24

911.48

5.3
51

912.38

4.4
75

910.68

6.1
29

910.78

6.0
18

911.08

5.7
12

911.38

5.4

911.28

5.5
12

910.88

5.9
19

908.39

8.39
23

911.38

5.4
29

FL 15" CMP

912.48

4.3
37

912.48

4.3
75

913.08

3.7
75

911.88

4.9
48

STA	+	Δ	-	ELEV
		916.78		
155+00				
✓				
T.P.	6.02	917.75	5.05	911.73
+25	15" CMP CULVERT RT 23'			
+36	E ENT RT			
+45	E ENT LT : 15" CMP RT 24'			

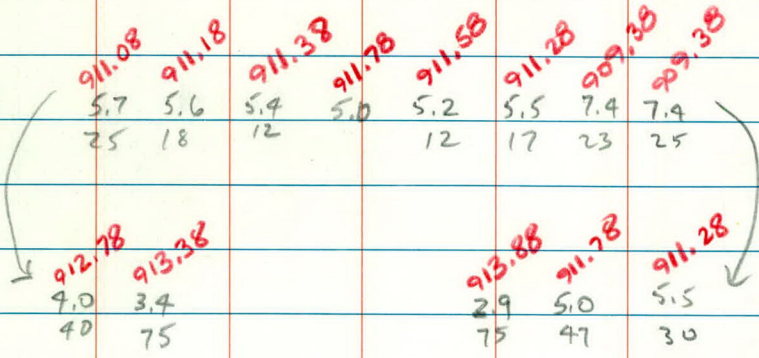
GA
BS
BW

LT

⊕

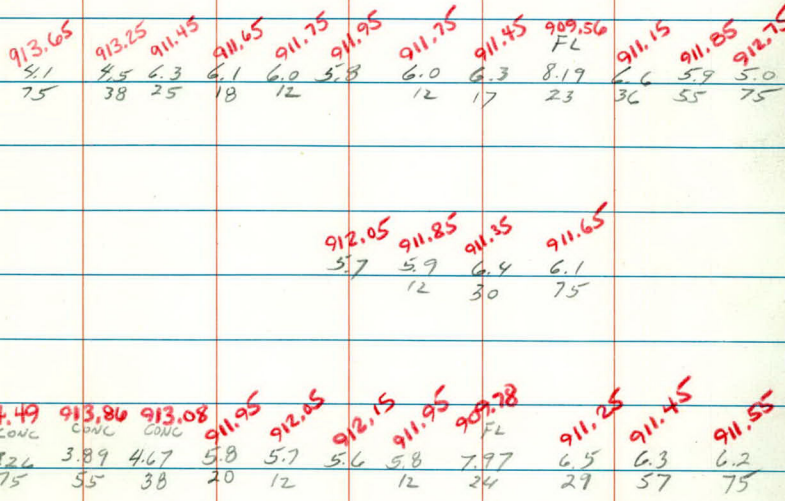
RT

5-4-76
Clear 600



WS
GA
BS

P.K. ⊕ STA. 155+00



STA.	+	π	-	ELEV
		917.75		

155+76	$\neq$	ENT LT		
--------	--------	--------	--	--

+89	MH LT 21'	5.36	912.39
-----	-----------	------	--------

156+18	15" CMP	RT 22'
--------	---------	--------

+30	$\neq$	ENT RT
-----	--------	--------

+42	15" CMP	RT 22'
-----	---------	--------

+75	✓
-----	---

VS
GA
BJ

LT

£

RT

3-4-76
Clear 62°

914.75

3.0
75

913.45

4.3
48

912.45

5.3
24

912.45

5.3
12

912.55

5.2

912.15

5.6
12

911.75

6.0
17

910.45

7.7
24

911.35

6.4
31

912.05

5.7
75

914.55

3.2
75

912.85

4.9
40

912.55

5.2
21

912.95

4.8
16

913.05

4.7
12

913.15

4.6

912.95

4.8
12

912.55

5.2
16

910.47

FL
7.28
22

912.75

5.0
28

912.95

4.8
52

912.75

5.4
75

913.35

4.4

913.15

4.6
12

912.65

5.1
27

912.75

5.0
50

912.75

5.0
75

913.65

4.1
75

913.15

4.6
36

912.55

5.2
26

913.25

4.5
21

913.35

4.4
12

913.55

4.2

913.25

4.5
12

912.65

5.1
19

911.10

FL
6.65
22

912.87

conc side work
4.88
28

913.12

4.63
50

913.00

4.75
75

912.85

4.9
75

913.45

4.3
32

913.15

4.6
20

913.75

4.0
12

913.95

3.8

913.65

4.1
12

913.25

4.5
16

911.55

6.2
23

913.05

4.7
30

913.25

4.5
62

STA

+

X

-

ELEV

917.75

157+30

ENT LT 6' 15" CMP RT 22'

+40

ENT RT

+50

15" CMP RT 22'

+70

15" CMP RT 22'

+78

CONC ENT RT

+88

15" CMP RT 22'

WS
GA
BS

LT

E

RT

5-4-76
Clear 62°

913.25	913.35	913.95	913.75	914.15	914.35	914.85	913.55	911.73	913.15	912.65	912.65
4.6	4.4	3.8	4.0	3.6	3.4	3.7	4.2	6.32	4.6	5.1	5.1
75	41	32	24	12		12	16	22	28	50	75

914.45	914.15	913.15	912.75	912.85
3.3	3.6	4.6	5.0	4.9
	12	22	50	75

913.75	913.85	914.05	914.25	914.55	914.25	913.75	911.70	912.75	912.75	912.85
4.0	3.9	3.7	3.5	3.2	3.5	4.0	6.05	5.0	5.0	4.9
75	41	19	12		12	17	22	27	48	75

914.05	914.05	914.05	914.45	914.65	914.25	913.55	911.84	913.15	913.15	913.25
3.7	3.7	3.7	3.3	3.1	3.5	4.2	5.91	4.6	4.6	4.5
75	31	22	12		12	18	22	27	51	75

914.75	913.35	913.55	913.61	913.56	913.45
3.0	3.4	4.2	4.14	4.19	4.3
	12	23	30	49	75

914.35	914.35	914.45	914.65	914.85	914.45	913.75	911.73	913.35	913.67
3.4	3.4	3.3	3.1	2.9	3.3	4.0	6.02	4.4	4.08
75	39	20	12		12	18	22	26	39

913.75	913.75
4.0	4.00
75	62

STA

+

X

-

ELEV

917.75

158+08

✓

ENT LT

✓

+24

DRAINAGE DITCH RT, ENT LT

TP

5.97

920.92

2.80

914.95

+26

✓

+74

ELEV

RT

WS
CA
BJ

LT

E

RT

3-4-76
Clear 65°

915.15

2.6
75

914.95

2.8
50

914.65

3.1
24

914.85

2.9
12

915.05

2.7
12

914.75

3.0
12

914.25

3.5
19

912.45

5.3
24

913.35

4.4
30

913.05

4.7
50

913.81

CONC
3.94
66

913.89

CONC

3.86

75

915.25

2.5
75

915.35

2.4
36

914.75

3.0
22

914.95

2.8
12

915.15

2.6
12

914.95

2.8
12

914.45

3.3
18

912.95

4.8
24

912.55

5.2
43

912.55

5.2
75

PK E STA 158+00

915.42

55

46

914.82

61

25

914.82

6.1

16

915.02

5.9

12

5.7

915.22

914.92

6.0

12

914.52

6.4

18

914.02

6.9

23

913.92

7.0

45

913.72

7.2

75

915.22

5.7

75

915.72

915.12

5.8

42

915.18

5.74

25

mt.

915.02

5.9

20

915.42

5.5

12

5.2

915.42

5.5

12

915.12

5.8

18

914.82

6.1

21

915.22

5.7

31

914.42

6.5

75

914.92

6.0

75

STA

+

π

-

ELEV

920.92

159+00

✓

✓

+09

EUT

LT.

✓

+35

EUT

RT.

X

✓

+74

✓

W3
GA
BJ
BW

RT

£

LT

5-5-76
cloudy 53

916.18 915.47 915.62 915.92 915.72 915.52 916.02 916.02
4.74 5.45 5.3 5.0 5.2 5.4 4.9 4.9
33 24 14 12 27 47 75
CONC. CONC.

915.02 914.22
5.9 6.7
38 75

916.24 915.55 915.72 916.02
4.68 5.37 5.2 4.9
32 23 12
CONC. CONC.

916.32 915.62 914.92
4.6 5.3 6.0
51 71 75

916.42 915.72 915.92 916.12 915.92 915.72 915.92 916.42
4.5 5.2 5.0 4.8 5.0 5.2 5.0 4.5
39 23 12 12 28 46 75

917.32
3.6
75

916.88 916.52 916.12 916.12 916.32 916.12 915.92 916.26 916.48
4.04 4.4 4.8 4.8 4.6 4.8 5.0 4.66 4.44
46 33 24 12 12 22 49 75
CONC. CONC. CONC.

917.37 917.42
3.55 3.5
70 75
CONC.

/

STA	+	π	-	ELEV.
		920.92		
159+90	ENT	RT:LT		✓
✓				
160+13		x	4.74	916.18
+29				
✓				
+20			4.69	916.23
✓				
+41			x	✓
+61	¢	CO. RD 'D'	x	

W
G
13T
BW

LT

¢

RT

5-5-76
cloudy 53°

916.90	916.03	916.22		916.52	916.22	916.12	916.62	916.62
4.02	4.89	4.7	4.4	4.7	4.8	4.3	4.3	
32	21	12		12	22	45	75	
CONC.	CONC.							

917.12	917.22
3.8	3.7
53	75

MH RT 24

916.72	916.42	916.62		916.92	916.82	916.52	917.02	916.42
4.2	4.5	4.3	4.0	4.1	4.4	3.9	4.5	
47	30	12		12	22	36	59	

916.52
4.4
75

916.32
4.6
75

MH RT 22

916.12	916.32	916.82		917.02	917.02	916.52	916.12	916.32
4.8	4.6	4.1	3.9	3.9	4.4	4.8	4.6	
61	41	12		12	34	49	75	

916.22	916.42	916.82		917.02	916.92	916.82	916.52
4.7	4.5	4.1	3.9	4.0	4.1	4.4	
75	50	25		25	50	75	

STA	+	K	-	ELEV.
-----	---	---	---	-------

		920.92		
--	--	--------	--	--

+73				
-----	--	--	--	--

			4.12	
--	--	--	------	--

				916.80
--	--	--	--	--------

+81				
-----	--	--	--	--

			4.20	
--	--	--	------	--

				916.72
--	--	--	--	--------

+85				
-----	--	--	--	--

			4.44	
--	--	--	------	--

				916.48
--	--	--	--	--------

+92				
-----	--	--	--	--

			4.60	
--	--	--	------	--

				916.32
--	--	--	--	--------

+93				
-----	--	--	--	--

			4.74	
--	--	--	------	--

				916.18
--	--	--	--	--------

B.M.				
------	--	--	--	--

			2.47	
--	--	--	------	--

				918.45
--	--	--	--	--------

				918.44
--	--	--	--	--------

W.S
G.A
B.J
B.W

LT

Q

RT

5-5-75
CLINOV 49°

MA LT 14

1

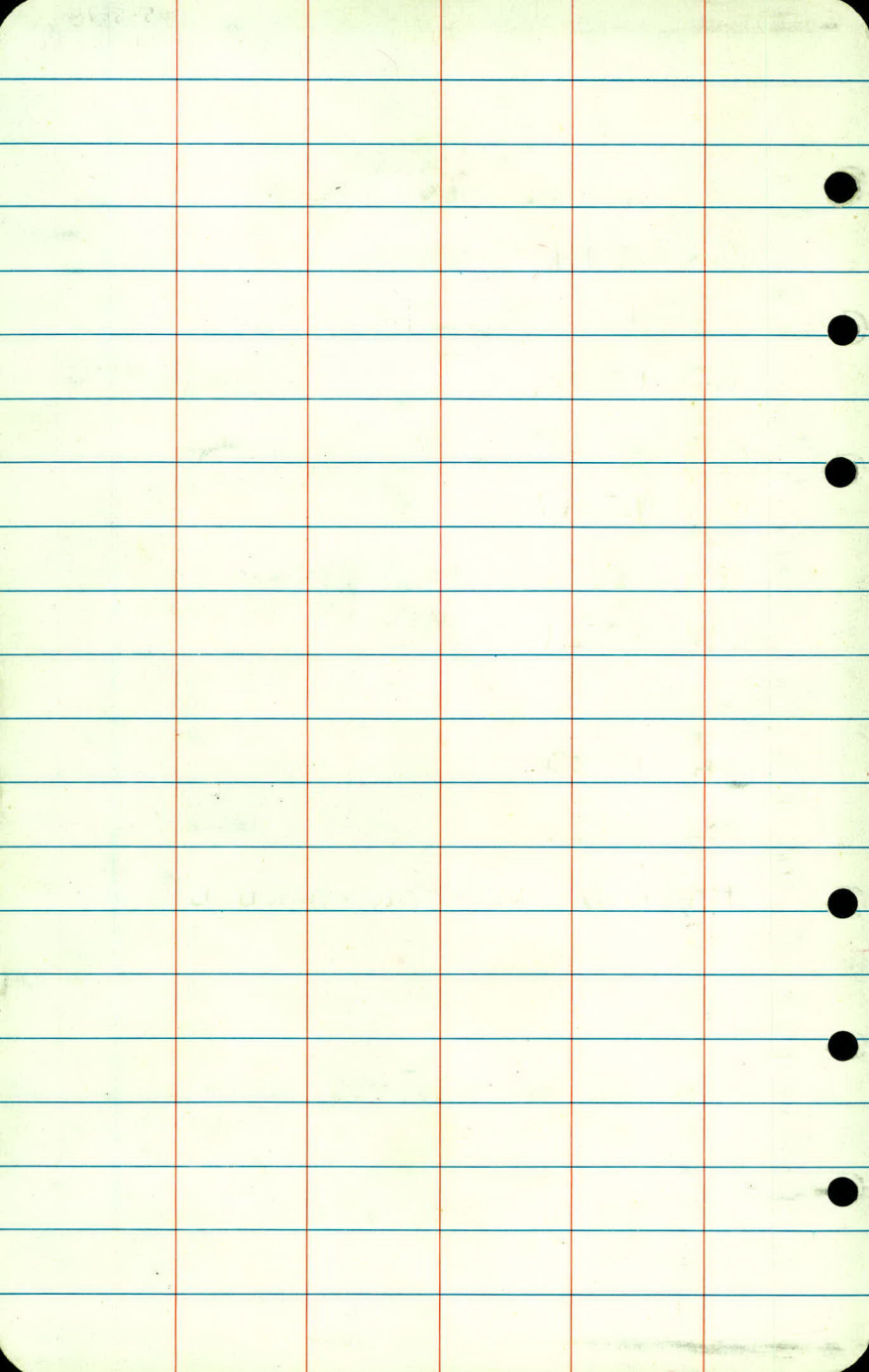
MA LT 14

MA LT 17

MA LT 21

MA LT 30

TOP HYD NW COR CO. RD "D"



WLS
G.A
R.T

5-28-76
CL0004360° 1.

SOUNDINGS

CLEVELAND AVE

FROM

CO. RD "C"

TO

CO. RD "D"

3 PAGES

113+00 DEPTH AT WHICH 6 BLOWS/FT IS ATTAINED

114+00

114+85

116+00

123+00

124+00

125+00

126

127

128

129

130

131

132

133

134

135 to 140 Same as 134 ~~134~~

	LT	E		RT	5-28-76 CLUBHOUSE 65'	2.
	35'				35'	
● 4-5'					0-1	
4-5'	25'			31'		
	0-1			0-1	1-2	
	25'			30'		
4-5	0-1			0-1	2-3	
	30'			28'		
1-2	0-1			0-1	1-2	
0-1					0-1	
0-1					0-1	
	27'					
4-5	0-1				0-1	
	27'					
4-5	0-1				0-1	
	27'					
1-2	0-1				0-1	
	27'			30'		
2-3	0-1			0-1	1-2	
	24'					
4-5	0-1				0-1	
0-1					0-1	
	26			27'		
7-8	0-1			0-1	2-3	
	28'	25'				
5-6	5-6	0-1			0-1	
35'	30 25'	20'	22'	25'		
0-1	1-2 3-4	0-1	0-1	3-4	3-4	
35'	30 25'	20'	25'	30'		
0-1	2-3 2-3	0-1	0-1	4-5	3-4	

146 DEPTH WHICH 6 BLOW/FT IS ATTAINED

147

148 + 25

149

150

W.S
C/A
RT

LT

£

RT

5-28-76
CLOUDY 68°
3.

35'

35'

0-1

0-1

0-1

0-1

0-1

22

28

35

0-1

6-7

5-6

0-1

22

28

35

0-1

7-8

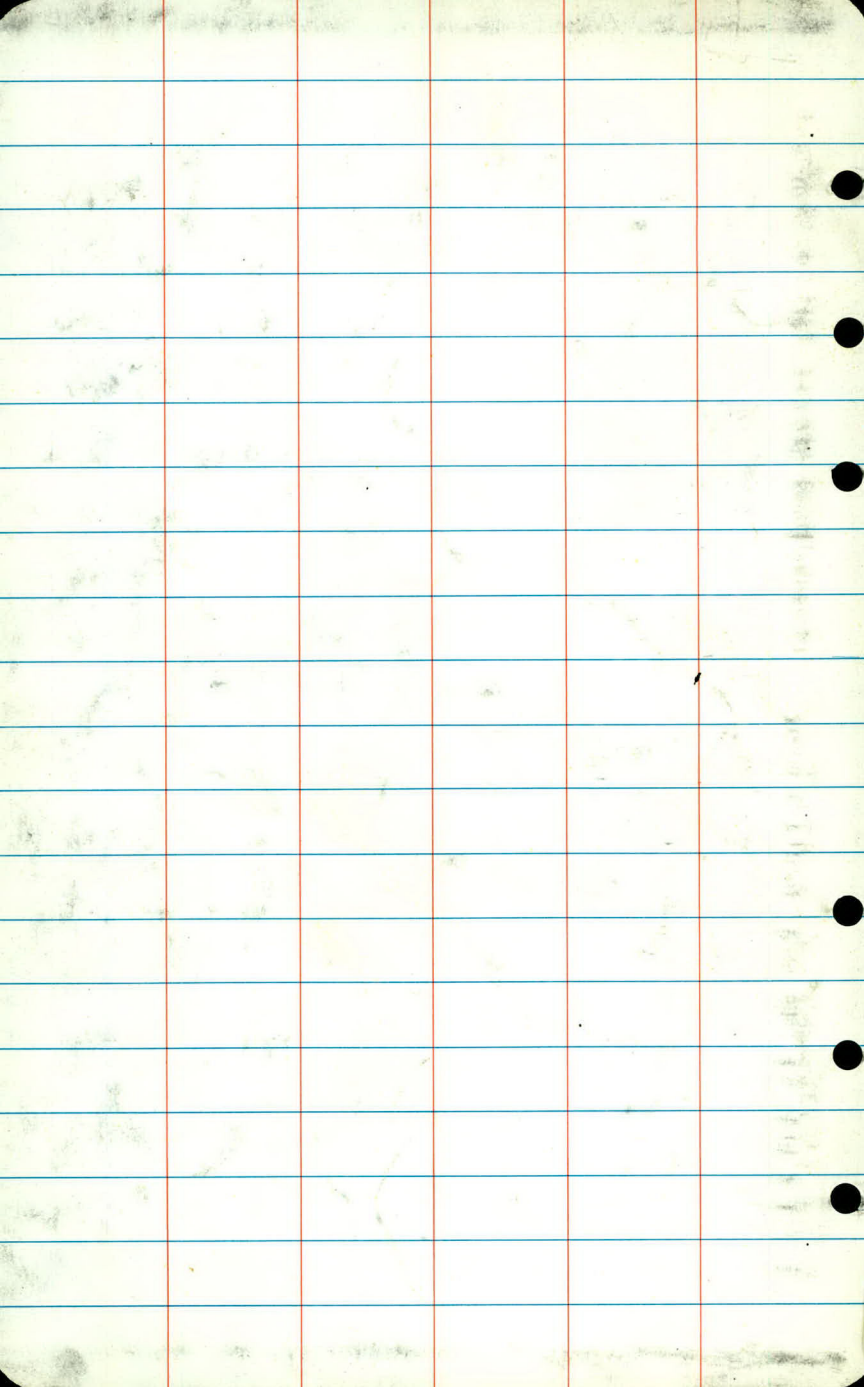
6-7

0-1

22

0-1

3-4



RG
ML
LAD
BW

MAR 29, 78

62-646-04

SUNNY 50°

1

BORROW PIT

ALINEMENT

CO R0 C2

WOODED AREA

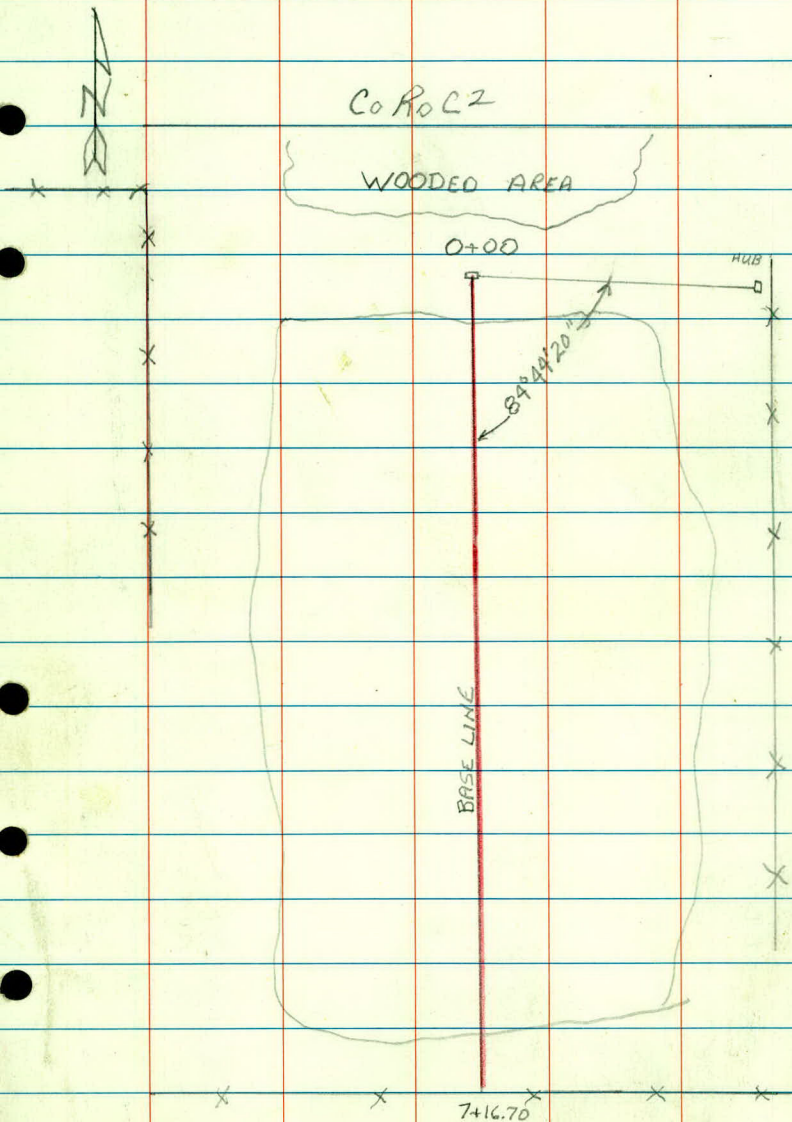
0+00

HUB

84°44'20"

BASE LINE

7+16.70



STA

0+10

HUB AND TACK LT 135'

0+00

HUB AND TACK

KP
JA
ML
LPO

MAR 30, 78

SUNNY 35°

2

3 NAILS
TWIN 18" OAK
OK 48.04'



3 NAILS IN F.P.

← 1.55' →

3 NAILS
TWIN 24" OAK

OK 26.50'



3 NAILS
18" OAK

← 29.17' →

STA	+	π	-	ELEV.
BM	18.92	118.92		(100.00)
0+00				
+25				
+50				
+75				
✓				
TP	12.61	130.40	1.13	117.79

LT

A

RT

3

SPIKE IN FP 135' LT STA 0+10

V
A

22.2	21.0	20.6	20.4	19.2	19.1	19.7	20.6
135	100	50		50	100	156	165
FE							

21.7	21.8	20.8	20.1	18.9	19.1	21.5
135	100	50		50	100	159
FE						

21.1	18.9	16.0	15.2	12.8	11.4	11.5	15.8	18.7	22.6
135	100	79	50		50	70	100	113	156
FE									

45.7

19.4	19.1	16.7	6.5	4.3	5.0	14.4	17.7	19.5
143	121	100	50		48	100	112	125
FE								

21.9
155

TOP ROCK

STA

+

π

-

ELEV

130.40

1+00

+50

+80

2+00

+50

3+00

TP

LT

2

RT

4

24.0	19.9	9.2	8.2	8.8	15.7	25.0
100	82	43		39	65	100

22.3	17.3	9.0	7.9	8.0	16.1	25.4
100	85	59		38	71	100

20.9	13.7	6.1	4.3	6.3	13.1	24.2
100	75	45		31	63	100

20.8	12.3	5.8	3.5	6.0	11.9	23.9
100	72	46		31	57	100

19.8	13.3	4.6	3.2	4.6	9.4	19.3	24.3
100	77	42		23	50	87	100

18.9	15.5	5.5	3.8	6.4	13.8	23.2
100	89	49		34	70	100

TG 2.5 1.5 2.5 1.5 2.5

STA

+

π

-

ELEV.

130.40

3+50

TP

5.32

130.91

4.81

125.59

4+00

✓

+50

✓

LT

E

RT

5

16.1	12.4	5.7	4.4	5.7	10.8	16.9	21.5
100	85	56		30	58	84	100

TOP SPIKE $\neq$ STA 4+00

20.1	12.1	8.3	6.4	5.3	10.4	14.4	17.5	21.7
165	130	100	77		51	65	81	100

→ 25.6
185

14.8	5.5	5.3	5.9	7.4	14.2	17.5	17.6
147	100	61		38	70	80	87

→ 21.4 24.8
171 184

21.5 ←
100

STA

130.91

5+00

✓

+75

6+00

+25

✓

TP

15.24 1/5.67

LT

L

RT

6

15.1	5.3	4.7	7.0	8.3	18.4	21.7
140	100	63		34	80	100

21.4	24.2
160	170

24.3	19.1	12.8	4.5	6.6	10.2	20.4	24.2
143	126	100	60		23	73	100

24.6	17.5	9.7	9.8	20.8	23.2	26.1
125	100	55		57	91	100

21.4	18.1	16.0	15.2	20.2	23.5	23.1
100	86	55		40	62	80

25.5
116

25.1
89

TOP SPIKE ± STA 6+25

130.91

TP

2.00

114.31

18.60

112.31

14.24

100.07

ML
MR
JT
RD
RN

AUG 16, 78

SUNNY 65°

ASBUKT STORM SEWER
CLEVELAND & COUNTY RD. D

	+	π	-	
B.M.	3.57	923.25		919.68
			13.10	910.15
			13.47	909.78
			14.25	909.27
			12.50	911.02
			11.69	911.93
T.P.	1.88	920.61	4.52	918.73
			11.14	909.47
			10.88	909.73
			10.50	910.11
T.P.			1.72	918.89 (918.88)
B.M.	2.43	916.15		913.72
			8.78	907.37
			8.45	907.70
B.M.			0.74	915.41

Top H40 Mt. Rock & GORD

INVERT OF APRON 86+55 66' R

INVERT M.H. 80

INVERT M.H. 79

C.B. 83

C.B. 84

H.

M.H. 78

M.H. 78A

C.B. 82

Top H40 GORD + CLEVELAND

M.H. 77

M.H. 73

C.B. 72

M.H. 73

C.B. 74

Top of H40 156+50

	+	π	-	ELEV	
B.M.	0.55	913.15		912.60	
			10.35	902.80	
			10.69	902.46	
T.P.	1.88	911.46	3.57	909.58	909.59
			9.41	902.05	
			10.38	901.08	
			7.93	903.53	
			10.37	902.09	
			2.15	909.31	909.34
B.M.	0.72	911.34		910.62	
			8.66	902.74	
			9.78	901.56	
T.P.	0.24	909.23	2.35	908.99	

SPIKE IN PP 154+53 Rt

C.B. 65

M.H. 66

C.B. 67

Top H40 152+04 Rt

C.B. 58

M.H. 60

M.H. 61

C.B. 59

C.B. 53

M.H. 54

C.B. 55

SPIKE IN PP 148+25 Rt

Top H40 143+80

C.B. 46

M.H. 47

C.B. 48

Top H40 139±

	+	π	-	ELEV	
		909.23			
			9.08	900.15	
			8.32	900.91	
			7.39	901.84	
			6.75	902.48	
B.M.			2.95	906.28	(906.30)
B.M.	2.35	908.83		906.48	
			8.34	900.49	
			8.94	899.89	
			8.29	900.54	
			8.15	900.68	
			7.00	901.82	
			7.52	901.31	
B.M.	4.50	910.69	2.62	906.21	(906.19)
			8.85	901.84	
			9.14	901.55	
			8.82	901.87	

C.B. 40

M.H. 41A

M.H. 41

C.B. 42

C.B. 37

C.B. 38

Top H4D 135+92 Rt

Top H4D 131+85 Rt

C.B. 33

APRON C.B. 33

C.B. 28

APRON C.B. 33

C.B. 26

C.B. 27

Top H4D 127+45

C.B. 24

C.B. 25

C.B. 20

	+	+	-	ELEV	
		910.69			
			10.07	900.62	
B.M.	2.36	911.61	1.41	909.28	909.25
			11.61	900.00	
			11.09	900.52	
B.M.	3.04	912.69	1.96	909.65	909.66
			6.26	906.43	
			9.82	902.87	
			3.74	908.95	908.93
B.M.	4.53	913.58		909.05	
			7.94	905.64	
			10.88	902.70	
			10.85	902.58	
			8.65	905.02	
	4.54	913.43	4.69	908.89	908.89

C.B. 21

Top H4D 123+60 RT

C.B. 17

C.B. 18

Top H4D IONA LAKE + CLEVELAND NE. CO.

C.B. 34

APRON to CB 35

C.B. 35

APRON FROM C.B. 35

HUB 118+00 LT

Top H4D 115+61

APRON TO M.H. 12

M.H. 12

APRON FROM M.H. 12

HUB. 112+50

2.31

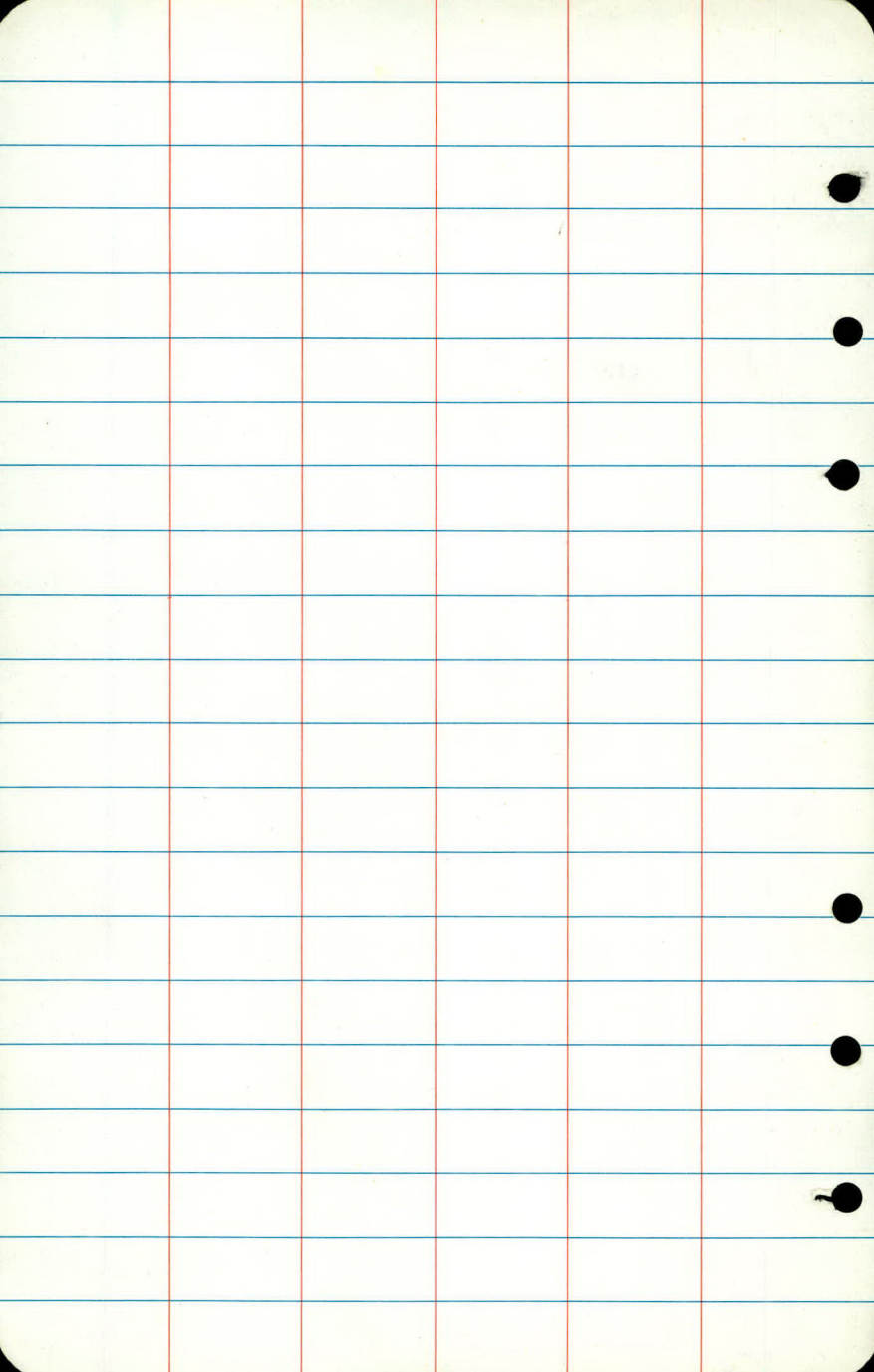
906.37

10.46

10.66

M. 16 60 A

60 B



ML
RC
MR
JT

OCT 4, 78

Cloudy 55°

ASBUILT'S CLEVELAND

STA	+	π	-	ELEV	
	0.54	912.94		912.40	
C.B. 6			9.62		
			4.96		
C.B. 9			7.51		
			5.17		
M.H. 10			4.88		
M.H. 10A			4.75		
M.H. 11			4.40		
112+30 APRON			8.10		
114+00 APRON (EAST)			7.06		
114+00 APRON (WEST)			10.81		
B.M.	5.48	914.52	3.91	909.03	909.04
M.H. 16A			5.63		
M.H. 16 (IONA LANE) WEST			5.61		
APRON			7.52		
B.M.	3.00	910.98		907.98	
M.H. 29			5.92		
M.H. 30			5.74		

Top HYD 110+56 Rt

INVERT

Top CASTING

INVERT

Top CASTING

Top CASTING

Top CASTING

Top CASTING

INVERT

INVERT

INVERT

Top HYD CORP C-7 CLEVELAND

STA	+	T	-	ELEV
		910.98		
M.H. 31			5.78	
M.H. 32			5.44	
C.B. 28 (W)			5.35	
C.B. 33 (E)			5.34	
132 (E)				
APRON			11.06	
132 (W)				
APRON			10.31	
C.B. 37			5.95	
C.B. 38			5.99	
B.M.	2.84	910.66	3.16	907.82
C.B. 42 (W)			5.06	
C.B. 40 (E)			4.80	
			10.95	
M.N. 41A			4.61	
M.N. 41				
C.B. 46 (E)			3.26	
C.B. 48 (W)			2.97	
(14200)				
M.N. 47			3.31	
BELL TALK				
M.H. 43A			5.02	
BELL TALK				
M.N. 43			5.01	
SAN. SEW.				
M.N. 44			3.82	

Top CASTING

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Top HYD 135+95

INVERT

Top CASTING

Top CASTING

	-	π	+	ELEV
		910.66		
T.P.	5.92	913.27	3.31	907.35
M.H. 47			14.03	
B.M. (144.90)			2.17	
M.H. 49		COVERED		
M.H. 50			4.68	
M.H. 50			14.58	
T.P.	4.54	911.89	5.92	907.35
M.H. 54			12.05	
M.H. 54			4.54	
C.B. 53(E)			4.25	
C.B. 55(W)			4.20	
M.H. 56			4.50	
C.B. 59			5.02	
C.B. 58			5.05	
			<u>14.15</u>	
M.H. 60			4.96	
M.H. 61			4.96	
M.H. 63		BURIED		
M.H. 64		BURIED		

INVERT

Top HYD 143+80[±]

Top CASTING

INVERT

M.H. # 54

INVERT

Top CASTING

INVERT

Top

	-	π	τ		
		911.89			
T.P	6.45	914.80	3.54	908.35	
M.H. 66			13.22		
M.H. 66			6.45		
C.B. 67(W)			6.02		
C.B. 68(E)			6.08		
M.H. 69			5.89		
M.H. 69A			5.85		
M.H. 70			5.17		
(55+75)EXTAN					
M.H. 73A			4.43		
M.H. 73A			12.32		
M.H. 71			4.26		
B.M.	4.00	917.91	0.89	913.91	
			2.35	915.56	
M.H. 73			6.92		
M.H. 73			12.80		
C.B. 72(E)			5.73		
C.B. 74			5.66		

INVERT

Top

Top

INVERT

Top

INVERT

