

OFFICE OF COUNTY ENGINEER
RAMSEY COUNTY, MINN.

PLAN

Survey

Co. Rd "E"

From CENTERVILLE To T. H. 61

Road Acc't. No. 15

Date Filed 4-7-81

File _____

42

dv 13

GA
DS
LPD
RJ

1-5-76
cold clear 10°

Ditch Survey for Sewer

Alignment

"E" to south along

T.H. No. 61

Co Rd E : T.H. # 61

$$86 + 72.67$$

$$Co R_0 "E" = 0 + 00$$

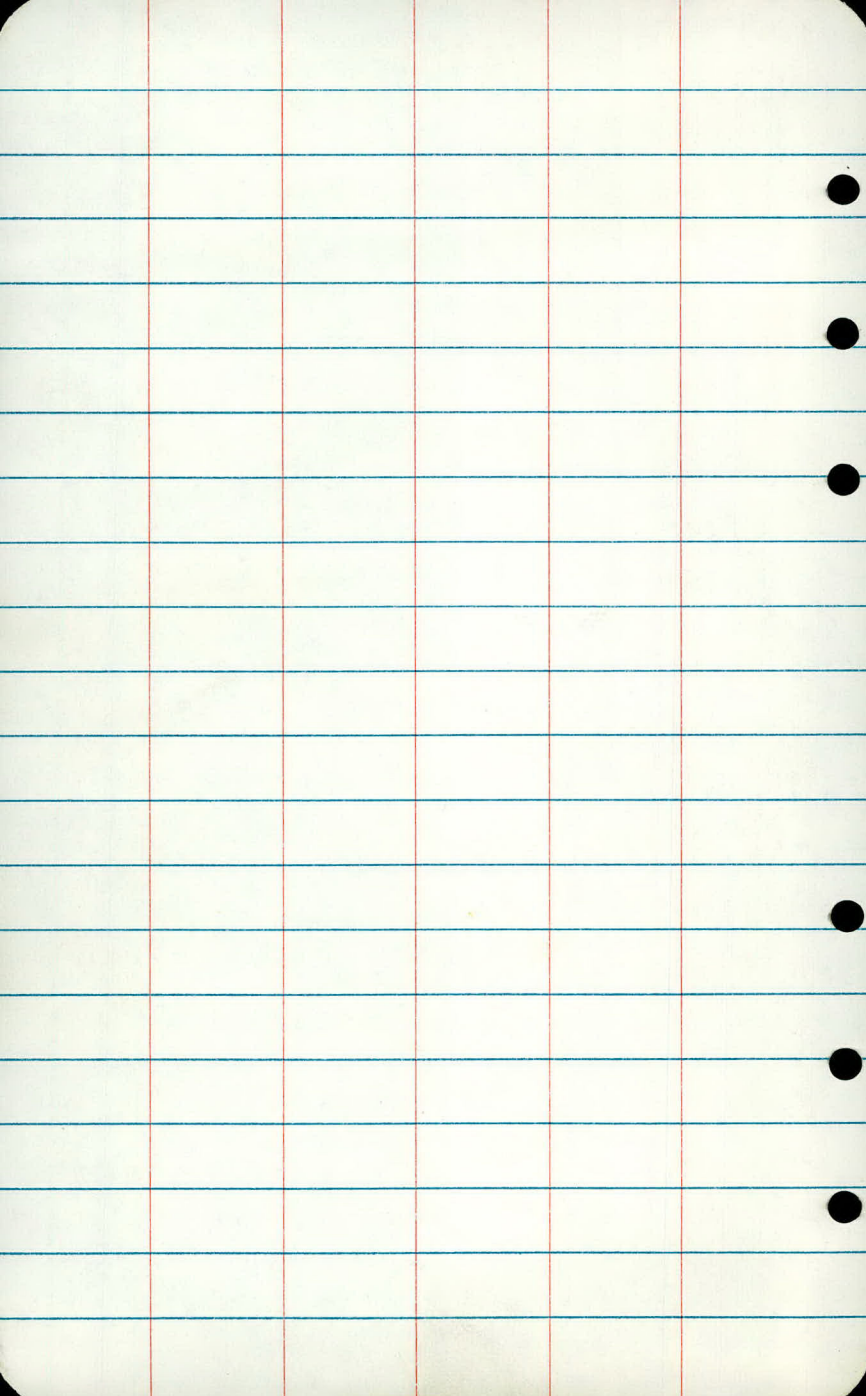
GA
DS
LPD
RJ

1-5-76

2

WEST EDGE CONC PAVE

$\swarrow 75^{\circ} 24' 30'' \searrow$



W.S.
R.T.
E.Y.

7-28-76
CLEAR: 88°

1

TIES TO MAD R/W
MONUMENTS

SW CORNER OF

HWY 61

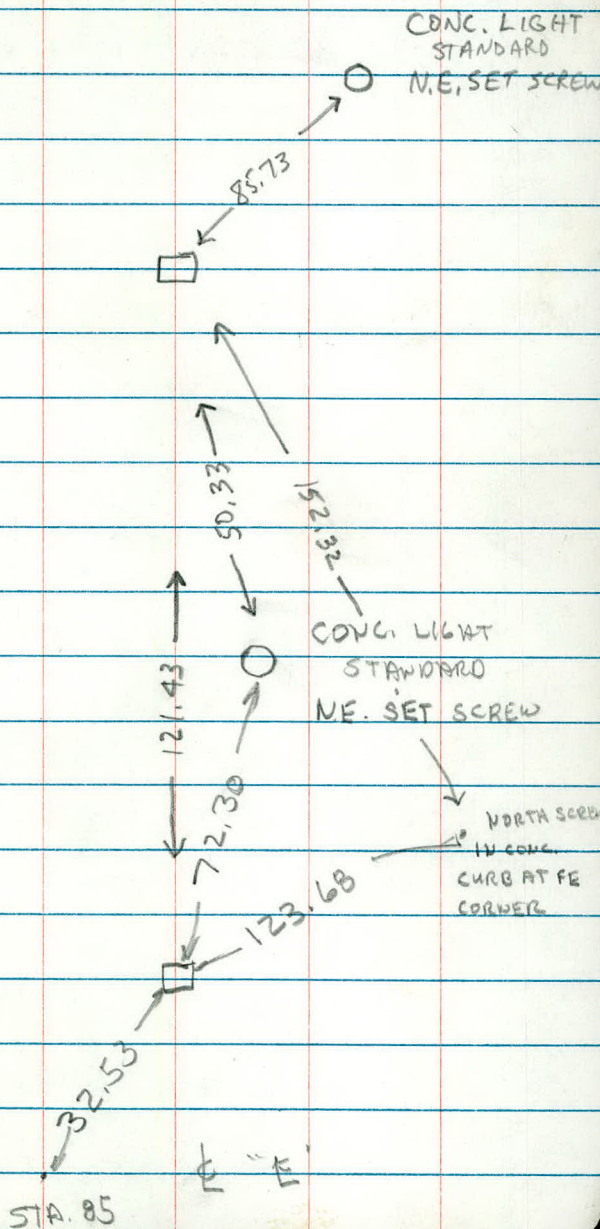
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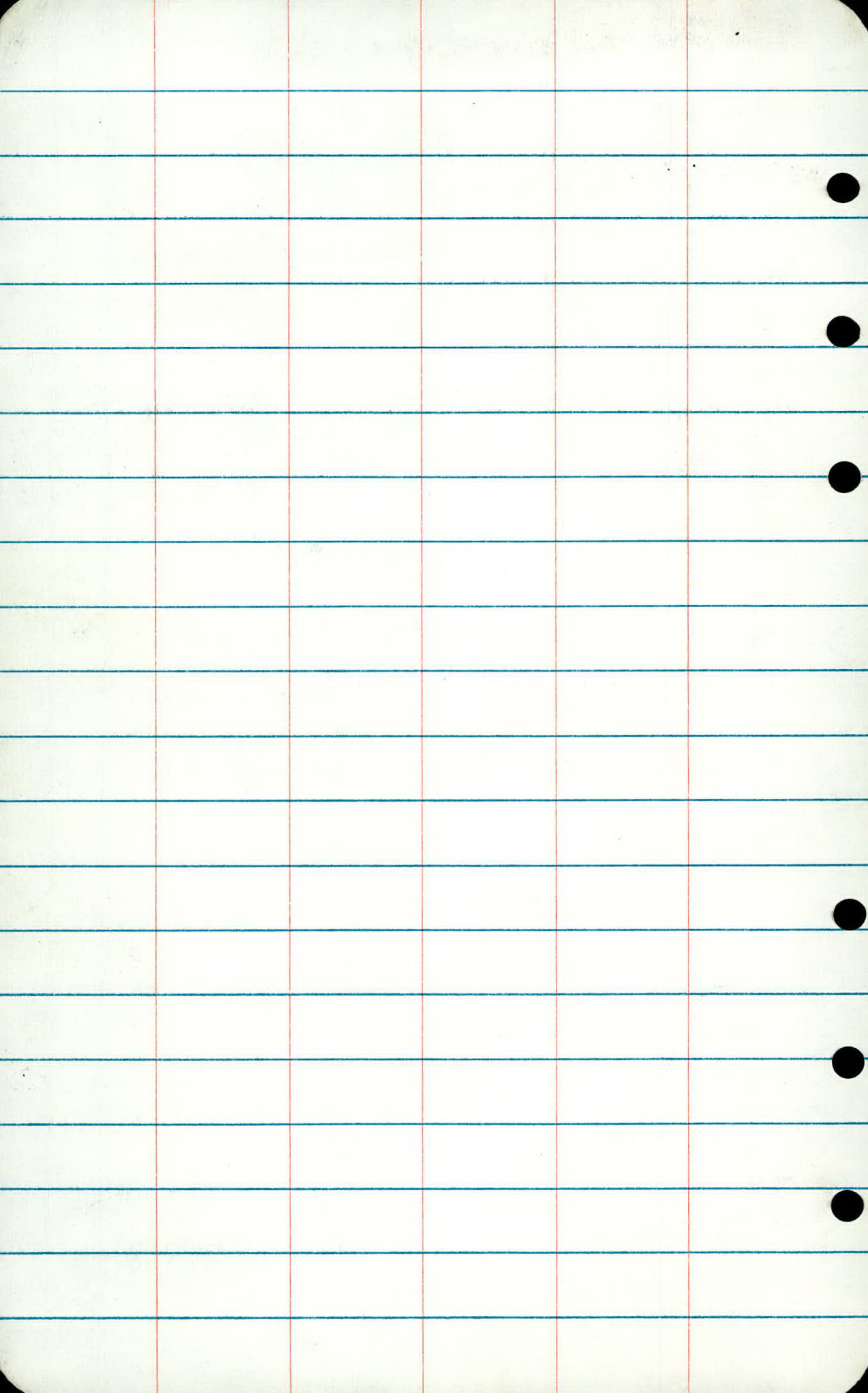
COORD 'E'

TIES TO MONUMENTS (MAD R/W)

W.S.
R.P.
E.Y.

7-28-76
CLEAN: 89° 2





RG
LPD
DS
GA
RJ

Jan. 16, 1976
Clear 50

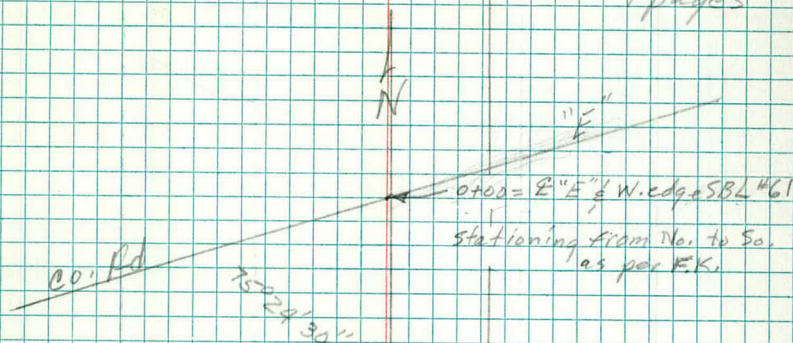
1.

Topography

S.W. Cor. T.H. #61, E "E"

STORM SEWER SURVEY

4 pages



Baseline D
S.R.L. T.H. #61

+50

LT

P

RT

Light

+36

79

4 Pine

+27

44

+39

12" Elm
53

2+00

Bit
10'

+94

8" Elm
43

steel

R/W post

+51

62

Breather

+51

PP
59

+47

Pipe
57

MH

+37

42

+38

6" Elm
53

1+00

Bit
10'

0+00

Jan 16, 1976

Lt

E

Rt

2



SAN. MH

7" Cast,
3 Rings
15' ± deep



5+00

1+

Bit
10'

RT

499 $\frac{12'' Elm}{53}$

Conc.
R/W marker

+59 $\frac{62}{}$

+41 $\frac{6'' Elm}{41}$

4+00

Bit
10'

+86 $\frac{10'' Elm}{51}$

+83 $\frac{Light}{67}$

RR
+34 58

6" Pine

+24 $\frac{52}{}$

3+00

Bit
10'

4" Pine

+96 $\frac{41}{}$

5" Pine

+76 $\frac{54}{}$

2+50

Jan 16, 1976

Lt

2

Rt

3

□ R/W

*

○

*

*

*

Lt

Rt

Rt

S. end Culv

+25 24

POR

+27 43

POR

+18 27

ER

+33 10

+107 61

+22 64

ENT RT

+uo

Edge ENT

45

7+00

ER

+87 27

N. end Culv

+76 25

POR

+79 17

PP

+67 59

B12

+61 10

2" Pine

W End Culv

+50 41

+55 16

6" Pine

+27 54

B12

10

6+00

4" Pine

+94 43

8" Pine

+68 53

MH

+51 43

PP

+18 59

B12

10'

5+00

RG
LPD
DS
GA
RT

Jan 16, 1976
Clear 5°

5

S.W. Cor. Co. Rd "E" $\frac{1}{2}$ T.H. #61

X-Sections

pages 5-9

Sta	+	π	-	E/V
B.M.	5.30	968.25		962.95

0+00

2 CORDS

+35

+47

1+00

+37

7.88

60.37

+50

2+00

Jan 16, 1976

RT

6

Top Mont (#62226)

6.4^A
3.85

6.4 ²⁹	6.4 ²	6.3 ⁶	6.4 ²	6.4 ⁸
3.96	4.1	4.7	4.0	3.4
	21	34	68	100

6.4 ²²	6.4 ⁴	6.3 ⁶	6.2 ⁰	6.1 ⁴	6.2 ⁰
4.03	3.9	4.7	4.2	6.8	6.3
	5	17	31	57	77
Bit					

6.4 ⁰	6.3 ⁶	6.2 ²	6.1 ⁶	6.1 ²	6.2 ⁴
4.23	4.6	6.0	6.7	7.1	5.9
	10	19	29	52	69
Bit					

rim MH

6.3 ⁸⁴	6.3 ⁶	6.2 ²	6.1 ²	6.0 ⁸	6.1 ⁸
4.41	4.7	6.0	7.1	7.5	6.5
	10	19	29	47	64
Bit					

6.3 ⁶¹	6.3 ⁰	6.1 ⁹	6.0 ⁹	6.1 ⁹	6.3 ⁶
4.64	5.2	6.1	7.1	6.1	4.4
	10	19	34	52	68
Bit					

Sta + $\bar{A}$ - Elev

968.25

+50

3+00

TP 3.42 965.12 6.55 961.70

+50

4+00

+50

5+00

Jan 16, 1976

2

RT

7

63.16	62.5	60.8	60.9	61.7	63.4
5.09	5.7	7.4	7.3	6.5	7.8
	11	20	31	44	65
	BIT				

62.73	62.1	60.4	59.9	61.0	62.9
5.52	6.1	7.8	8.3	7.2	5.3
	10	22	35	48	66
	BIT				

spike in PP Rt. 3+34

62.03	61.6	59.9	59.4	59.8	62.2
3.09	3.5	5.2	5.7	5.3	2.9
	10	17	32	53	67
	BIT				

61.09	60.6	58.8	57.9	58.3	60.6
4.03	4.5	6.3	7.2	6.8	7.5
	10	18	33	50	65
	BIT				

60.04	59.6	58.2	56.92	57.52	59.1
5.08	5.5	6.9	8.2	7.6	6.0
	10	18	33	51	65
	BIT				

59.22	58.7	57.3	55.8	57.2	59.8
5.90	6.4	7.8	9.3	7.9	5.3
	10	17	31	52	70
	BIT				

Sta	+	π	-	E/V.
-----	---	-------	---	------

		965.12		
--	--	--------	--	--

5+50				
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TP	4.22	960.12	9.22	955.90	MH Rt
----	------	--------	------	--------	-------

6+00					
------	--	--	--	--	--

+55					culv.
-----	--	--	--	--	-------

+76					culv.
-----	--	--	--	--	-------

7+00					E Ent.
------	--	--	--	--	--------

+25					culv.
-----	--	--	--	--	-------

Jan 16, 1976

Q

RT

8

58.02	57.6	55.5	54.7	55.2	55.90	58.0
7.10	7.5	9.6	10.4	9.9	9.22	7.1
	10	19	26	37	44	66
	Bit				MH	

56.69	56.2	55.0	53.4	54.6	57.3
3.43	3.9	5.1	6.7	5.5	2.8
	10	14	25	41	62
	Bit				

54.98	54.5	53.8	51.42	51.0	52.9	55.4	56.1
5.14	5.6	6.3	8.70	9.1	7.2	4.7	4.0
	10	14	16	26	37	52	65
	Bit		Inv.				
			18" RCP				

54.26	53.9	52.9	49.65	52.9	54.8	55.8
5.86	6.2	7.2	10.47	7.2	5.3	4.3
	15	22	25	30	48	63
	Bit		24"			
			cm			
			Inv.			

53.54	53.1	53.0	53.4
6.58	7.0	7.1	6.7
	26	45	60
	Bit	Bit	Bit

52.63	52.2	50.9	49.37	52.7	52.2	52.8
7.49	7.9	9.2	10.75	7.4	7.9	7.3
	10	22	26	32	44	64
	Bit		Inv.		Bit	Bit
			24" RCP			

Sta	+	π	-	EIV
		960.12		
TP	5.08	951.70	13.50	946.62
TP	4.12	946.37	9.45	942.25
10+34			9.71	936.66
+60			5.5	940.87
TBM	9.33	951.70	4.00	942.37
TP	11.83	963.12	0.42	951.29
BM	6.60	968.28	1.44	961.68 (961.70)
BM			5.36	962.92 (962.95)

END

Jan 16, 1976

9

West
edge conc. SBL sta 9

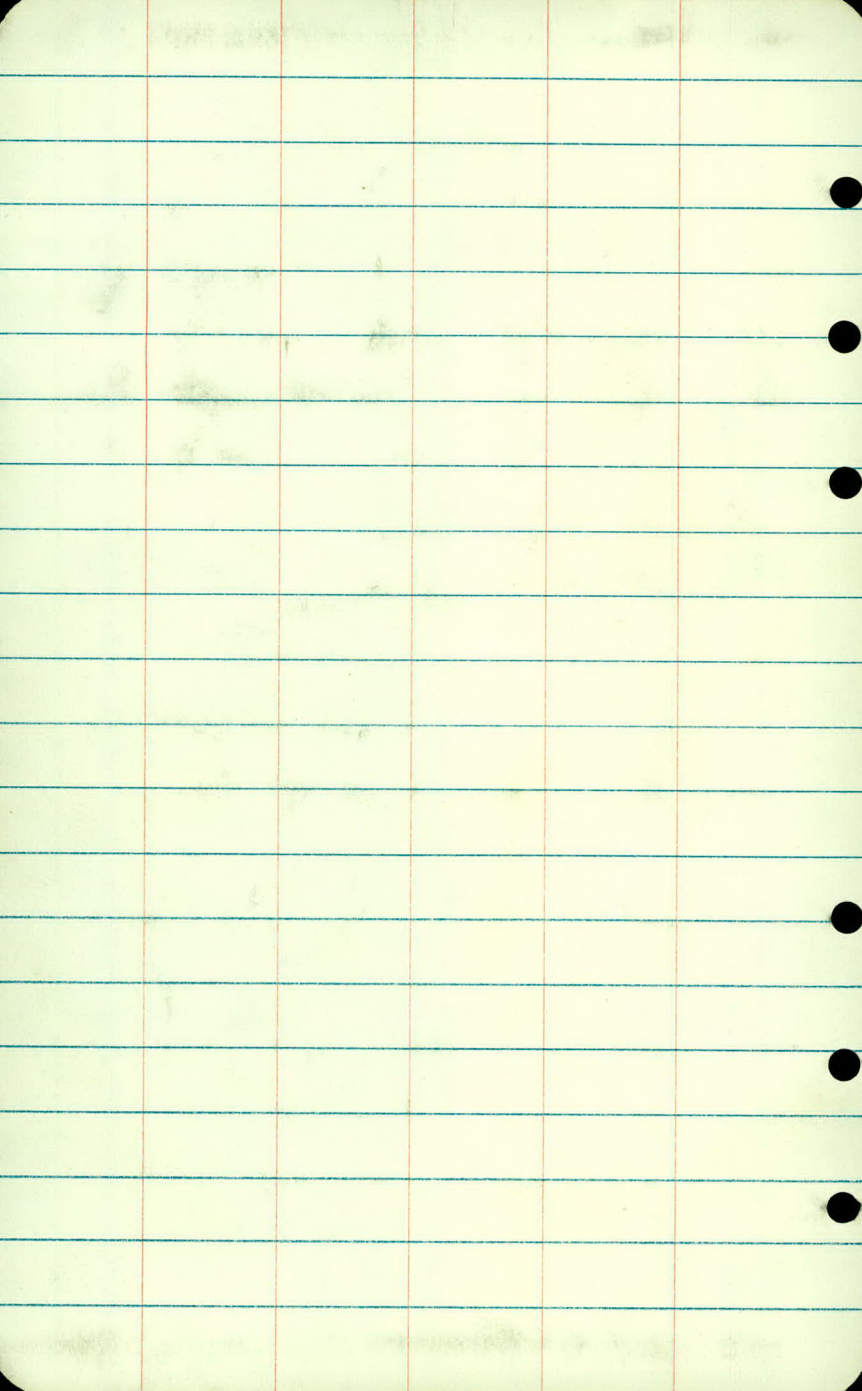
" " " 10

inv 24" CMP (No. end)

Top Hyd 100'± RT Sta 10+80±

spike in PP RT 3+34

Top Mont. # 62226



RG
LPD
GA
RJ

Jan 30, 1976
Cloudy 20°
D-1

Topography



Ditch 1A Area

7100

90° 00' 00"

5 1/4 Cr 528, T30, R23

Co. Rd.

40+00 "E"

35+04.35

Jan. 30, 1976

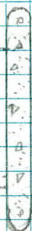
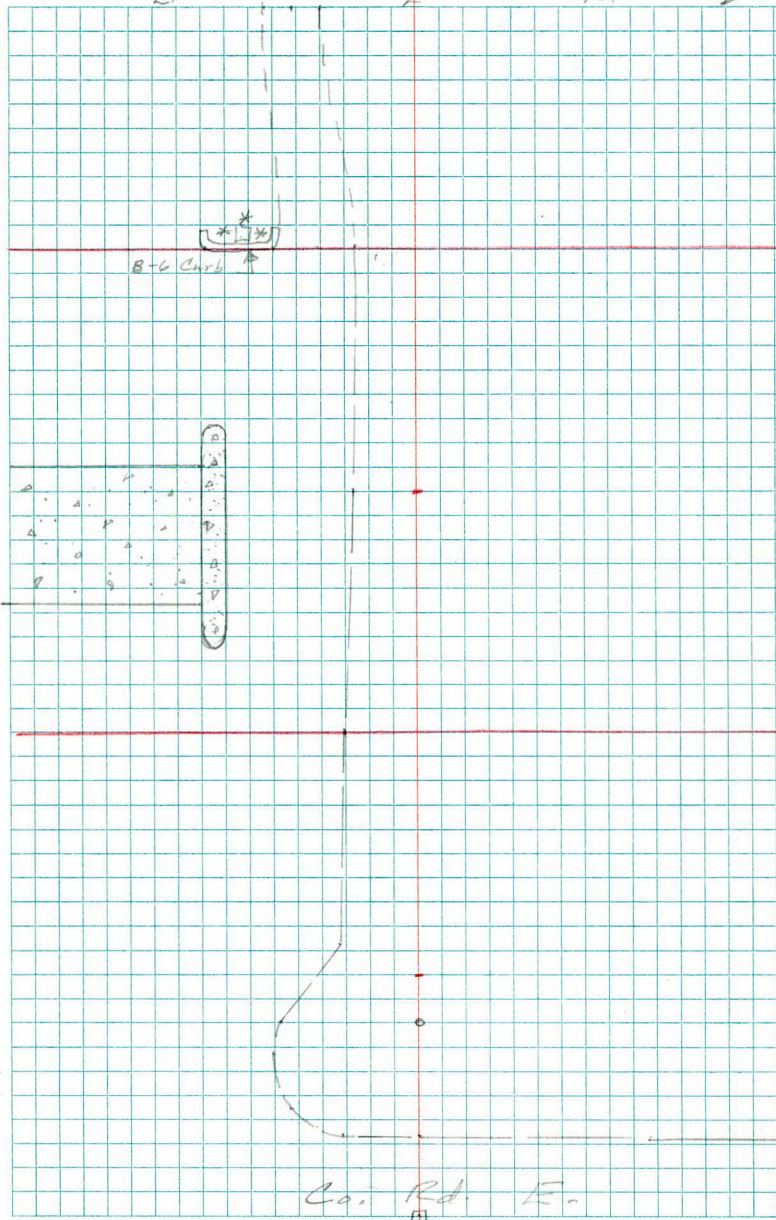
Lt

ℓ

Rt

D-2

B-6 Curb



Co. Rd. E.

5+00

Lt

Lt

Lt

4+00

3+00

End
212' Ent
+00 26

2+50

212' Ent
+50 26

Jan 30, 1976

Lt

Rt

D-3

ENT TO FIELD

Lt

L

Rt

7+00

+38

Beg ditch to East
L

6+00

5+00

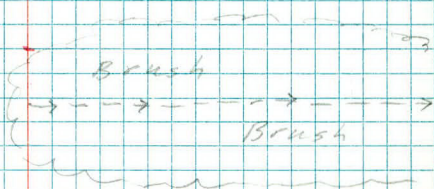
Jan 30, 1976

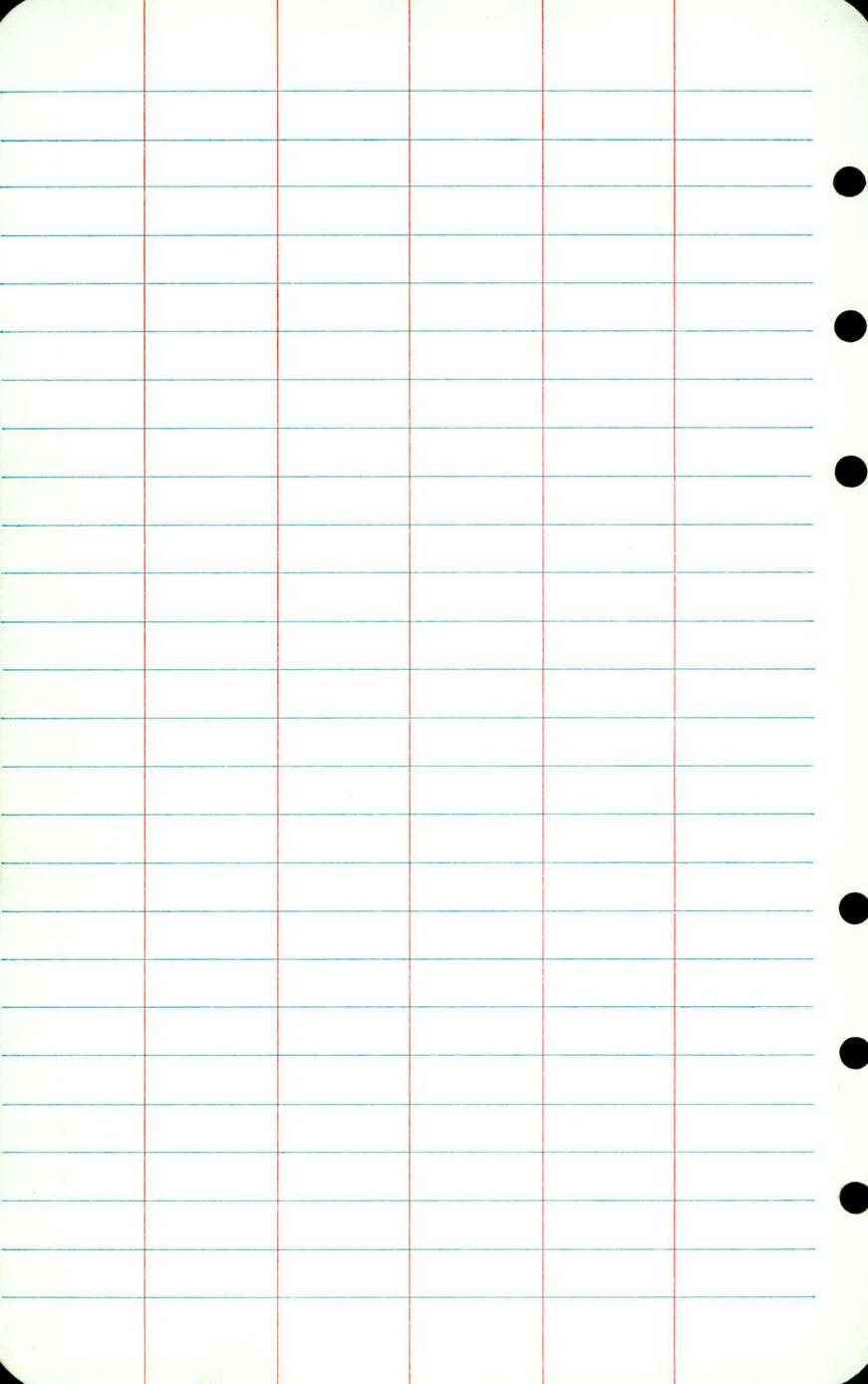
Lt

E

Rt

D-4





x-sections

STA	+	Σ	-	ELEV
BM	3.29	938.16		934.87
TP	0.28	928.27	10.17	927.99
TP	3.27	923.67	7.87	920.40

0+40
P.L.

1400

+31

+64

LT

E

RT

D-6

DISC #

SE COR Bridge Abut. 35E: "E"

STANDARD OIL
 BASE OF LIGHT Standard at ENT TO (SE COR BASE)

18.1 ^A	18.5	18.1	17.3	16.3	17.6	18.1 ^A	18.3
5.3	5.2	5.6	6.4	7.4	6.1	5.3	5.4
50	31	17	8		16	29	50

18.2	18.1	17.7	17.4	17.4 ^A	17.8	17.8	17.9
5.5	5.6	6.0	6.3	6.3	5.9	5.9	5.8
50	19	5		15	35	43	50

18.8 ¹	18.6 ⁵	19.0 ⁵	19.00	18.50	17.8	17.1	17.1	17.4	18.0
CONC	GWH	TC	TC	GWH					
4.86	5.02	4.62	4.67	5.27	5.9	6.6	6.6	6.3	5.7
50	43	43	40	40	16		16	36	50

18.46	18.46	19.08	19.05	18.35	17.5	16.8	16.9	17.3	18.2
CONC	GWH	TC	TC	GWH					
5.21	5.21	4.59	4.62	5.32	6.2	6.9	6.8	6.4	5.5
50	45	45	40	39	18		18	37	50

$+$	π	$-$	E/eV
-----	-------	-----	--------

	923.67		
--	--------	--	--

2+00			
------	--	--	--

3+00			
------	--	--	--

4+00			
------	--	--	--

5+00			
------	--	--	--

TP	2.97	920.87	5.77	917.90	Rock
----	------	--------	------	--------	------

TP 6					
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+40	Profile Low area or Ditch Rt				
-----	------------------------------	--	--	--	--

AK
GA
DS
RJ

LT

Feb 6, 1976
Clear Cold 10°
RT

D-7

17.7 17.6 17.5 16.6 16.8 17.1 17.1 ✓
6.0 6.1 6.2 7.1 6.9 6.6 6.6
50 34 20 21 39 50

19.3 18.4 15.9 14.9 15.2 16.7 16.8 ✓
4.4 5.3 7.8 8.8 8.5 7.0 6.9
50 23 12 15 29 50

17.7 17.7 17.0 17.8 14.1 13.9 14.0 14.9 ✓
6.0 6.0 6.7 9.9 9.6 9.8 9.7 8.8
50 33 13 7 14 31 50

18.6 17.5 13.1 12.4 12.5 12.7 12.9 ✓
5.1 6.2 10.6 11.3 11.2 11.8 10.8
50 20 7 16 33 50

18.2 17.2 14.1 10.5 06.7 910.0 99.4 ✓
2.7 3.7 6.8 10.4 14.2 10.9 11.5
50 32 15 13 30 50

17.0 16.0 14.7 08.6 08.9 07.6 08.7 07.8 ✓
3.9 4.9 6.2 12.3 12.0 13.3 12.2 13.1
50 29 15 14 33 70 100
07.9 08.1 08.1
13.0 12.8 12.8
250 200 150

Sta	+	π	-	Elev.
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		920.87		
--	--	--------	--	--

6+78				
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7+00				
------	--	--	--	--

TP	5.71	923.61	2.97	917.90 Rock
----	------	--------	------	-------------

60/H₂O, SE Cov

TP	3.94		3.21	920.40 (920.68)
----	------	--	------	-----------------

0-36				
------	--	--	--	--

0-60				
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0-100				
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FH
DS
GA
RJ

Feb 6, 1976
Cold Clear 10°

D-8

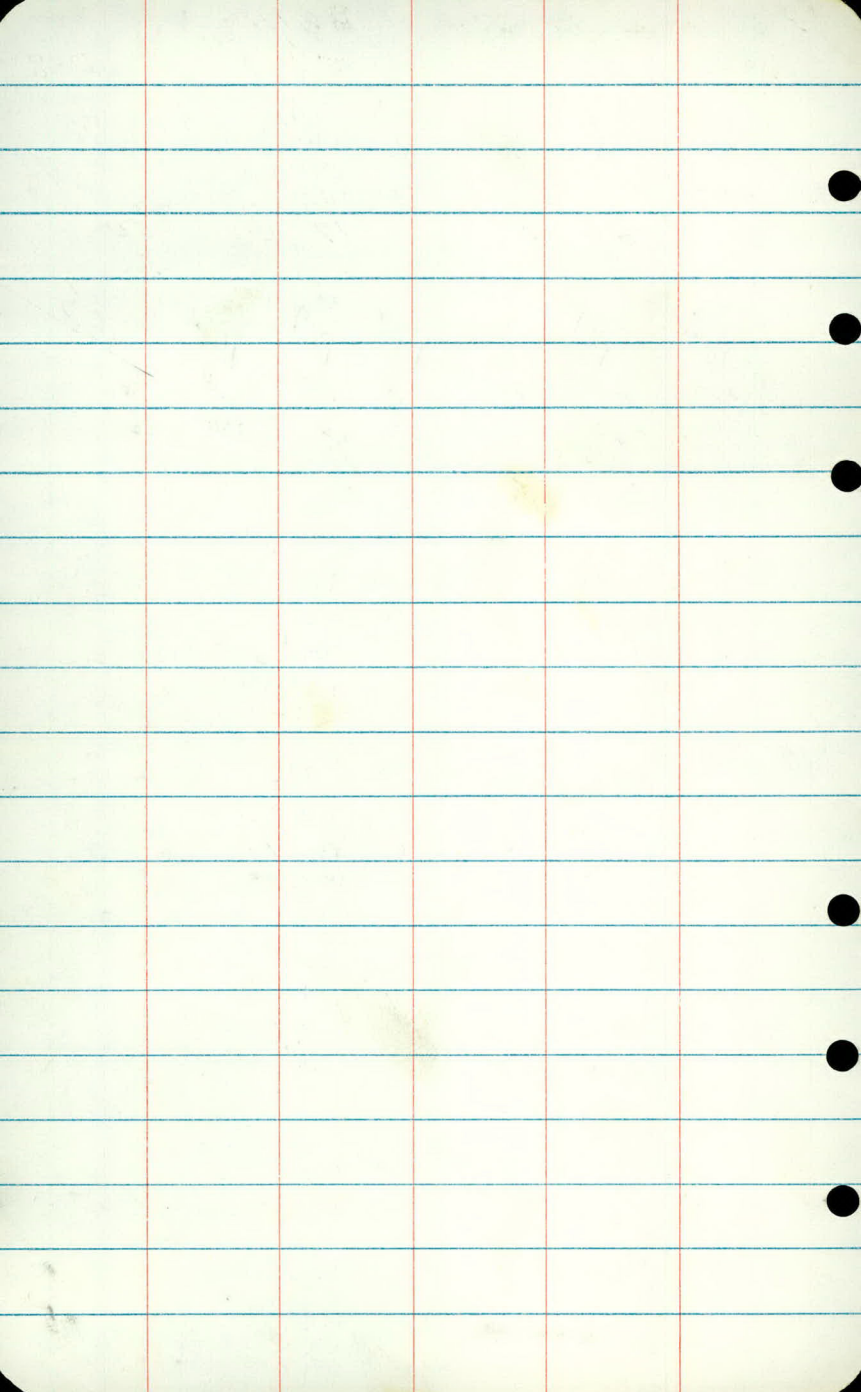
17.2	17.2	16.3	16.4	16.3	16.3	15.3
3.7	3.7	4.6	4.5	4.6	4.6	5.6
50	25	11		17	37	50

✓

16.9	17.1	16.7	16.6	16.7	16.4	15.3
4.0	3.8	4.2	4.3	4.2	4.5	5.4
50	27	11		16	28	50

SE COR LIGHT BASE AT ENT TO STANDARD OIL

8.3	8.4	10.0
	16	26



KP
GA
JA
RJ

9 FEB 1976 1.
SUNNY 38°

NW EXIT RAMP 35E & Co. Rd E.

X-SECTIONS

STA	+	T	-	ELEV	
BM	8.68	938.77			930.09
TP			3.91	934.86	934.87
TP			3.99	934.78	
TP	3.01	930.60	11.18	927.59	

125+00

✓

+50

✓

XP
GA
JA
RJ

LT DESCRIPTION

9 Feb 76 2
SUNNY 30°

£ STA 31+00

DISC. ON S.E. COR BRIDGE #9838

£ STA 28+00

BRASS PLUG STA 24+49.26

RC 24+49.26 = MHD 124+42.77

	22.10	22.30	23.00	24.80	27.02	27.26
FE						
8.5	8.3	7.6	3.9	3.58	3.34	
87	45	37	21	14		

	22.70	22.60	22.30	25.50	26.71	26.49	26.69
Fe							
7.9	8.0	8.3	5.1	3.89	4.11	3.91	
87	49	36	24	13	12		

STA	+	π	-	ELEV.
-----	---	-------	---	-------

		930.60		
--	--	--------	--	--

126+00				
--------	--	--	--	--

+50				
-----	--	--	--	--

127				
-----	--	--	--	--

+50				
-----	--	--	--	--

128				
-----	--	--	--	--

+50				
-----	--	--	--	--

GA
JA
RJ

LT

L

2-9-76 3
SUNNY 38°

22.20 22.40 21.9 24.70 25.95 25.74 25.92

FE

8.4 8.2 8.7 5.9 4.65 4.86 4.68
87 46 37 24 13 12

22.60 22.40 21.90 24.30 24.92 24.70 24.89

FE

8.0 8.2 8.7 6.3 5.68 5.90 5.71
87 47 36 22 13 12

22.70 22.80 20.60 22.50 22.70 23.46 23.67

FE

7.9 7.8 10.0 8.1 6.90 7.14 6.93
87 53 39 27 13 12

23.00 22.00 19.40 21.60 22.48 22.25 22.44

FE

7.6 8.6 11.2 7.0 8.12 8.35 8.16
87 52 35 25 13 12

23.10 21.90 18.40 20.30 21.30 21.06 21.26

FE

7.5 8.7 12.2 10.3 9.30 9.54 9.34
87 57 37 26 13 12

23.30 21.60 17.00 19.00 20.09 19.86 20.04

FE

7.3 9.0 13.6 11.6 10.51 10.74 10.56
87 60 40 27 13 12

STA	+	K	-	ELEV
-----	---	---	---	------

TP	7.36	924.94	13.02	917.58
----	------	--------	-------	--------

129+00

+50

130+00

+50

131+00

+50

GA
JA
RI

LT

±

2-9-76
sunny 38° 4

SE COR TOP of CB Grate 129+50 LT 12'

23.34	22.54	15.84	17.44	18.84	18.59	18.82
1.6	2.4	9.1	7.5	6.10	6.35	6.12
87	68	39	24	13	12	

23.24	22.14	14.24	14.11	17.04	17.49	17.24	17.56
1.7			CULV				
87			FL				
2.8	10.7	10.83	7.9	7.45	7.70	7.38	
69	38	32	21	13	12		

23.64	22.94	13.14	14.94	16.28	16.03	16.26
Fe						
1.3	2.0	11.8	10.0	8.66	8.91	8.68
99	76	38	24	13	12	

23.94	23.24	11.74	14.54	15.02	14.78	15.02
Fe						
1.0	1.7	13.2	10.4	9.92	10.16	9.92
108	82	40	21	13	12	

22.34	22.74	10.24	13.24	13.93	13.70	13.89
1.6	2.2	14.7	11.7	11.01	11.24	11.05
113	87	40	25	13	12	

22.34	21.74	08.34	11.74	12.94	12.71	13.05
2.6	3.2	16.6	13.2	12.00	12.23	11.89
114	82	32	25	13	12	

STA	+	PK	-	ELEV
		924.94		
132 ✓ 02				
TP	6.10	917.78	13.26	911.68
+48			10.29	907.49
+48			11.6	906.18
133+00			11.7	906.08
133+18			12.0	905.78
133+18			11.72	906.06
TP	10.55	928.11	0.22	917.56
TP	5.69	932.93	0.87	927.24
			5.30	927.63
				927.59

GA
JA
RJ

LT

£

2-9-76
SUNNY 38° 5

14.04

05.54

06.56

09.94

11.97

11.73

12.37

FL

10.9 19.4 18.38 15.0 12.97 13.21 12.57
70 46 35 25 13 12

SW COR TOP OF CB Grate 132 + 48 ± LT 12'

FL 15" CM 35.0 LT

DITCH 46.0 LT

DITCH 46.0 LT

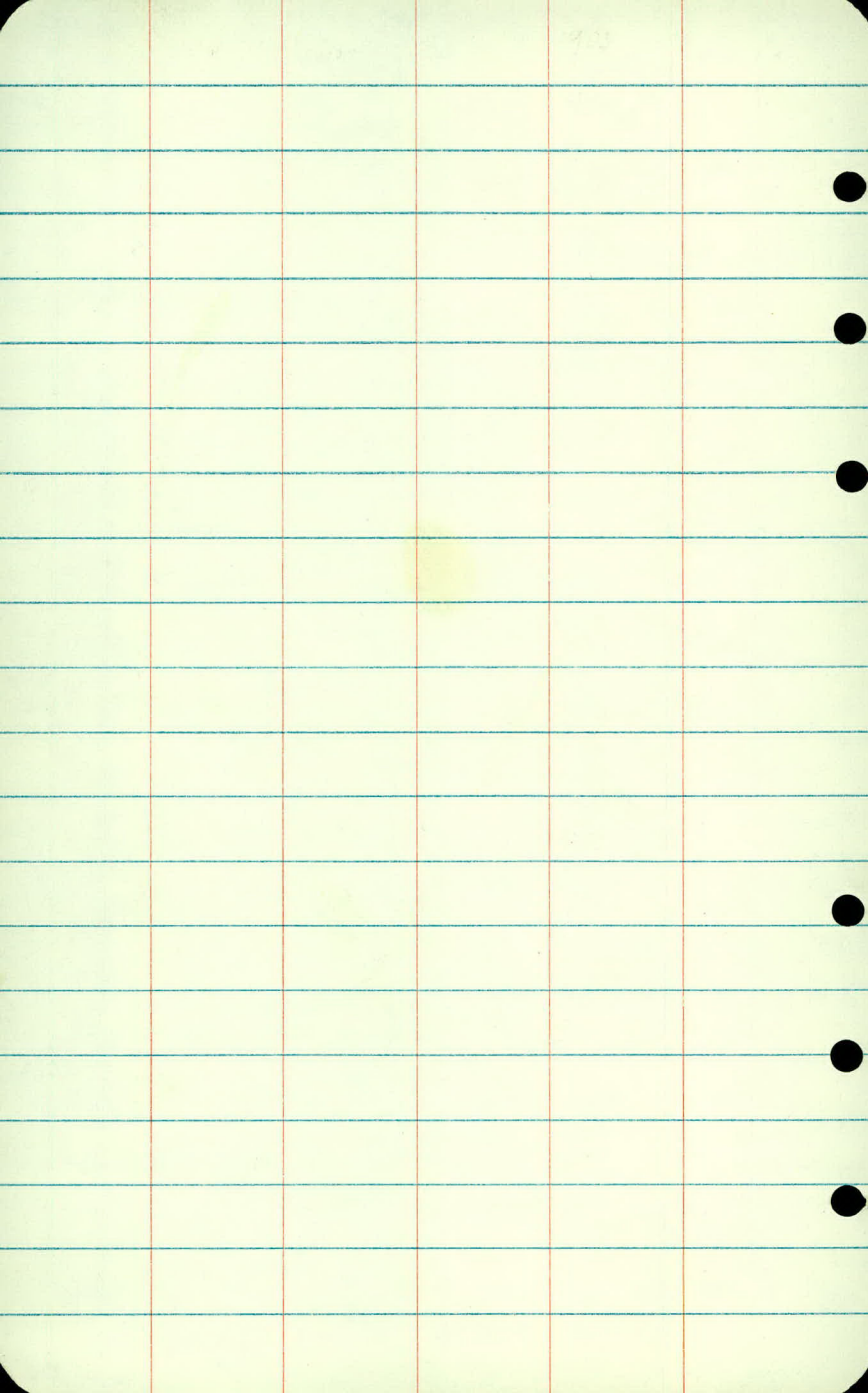
DITCH 46.0 LT

FL 15" CM 35.0 LT

TOP SW COR CB 12' LT 129 + 50

CONC. SLAB

BRASS PLUG £ STA 24 + 49.26 CORDE

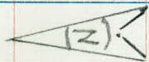


KP
DS
GA

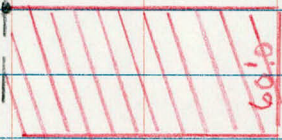
10 FEB 1976
CLOUDY 40°

1

X-SECTIONS



35+04.9



0-100

60'0"

STA + π - ELEV.

BM 3.50 924.18

920.68

0-100

0-67

0-34

BM

5.16 919.02

LT

E

10 FEB 1976

RT

S.E BOLT LIGHT STD LT 34+40

9.8

10.1

10.2

10.6

20

40

60

9.8

9.7

10.6

9.9

20

40

60

13.6

8.0

10.6

9.8

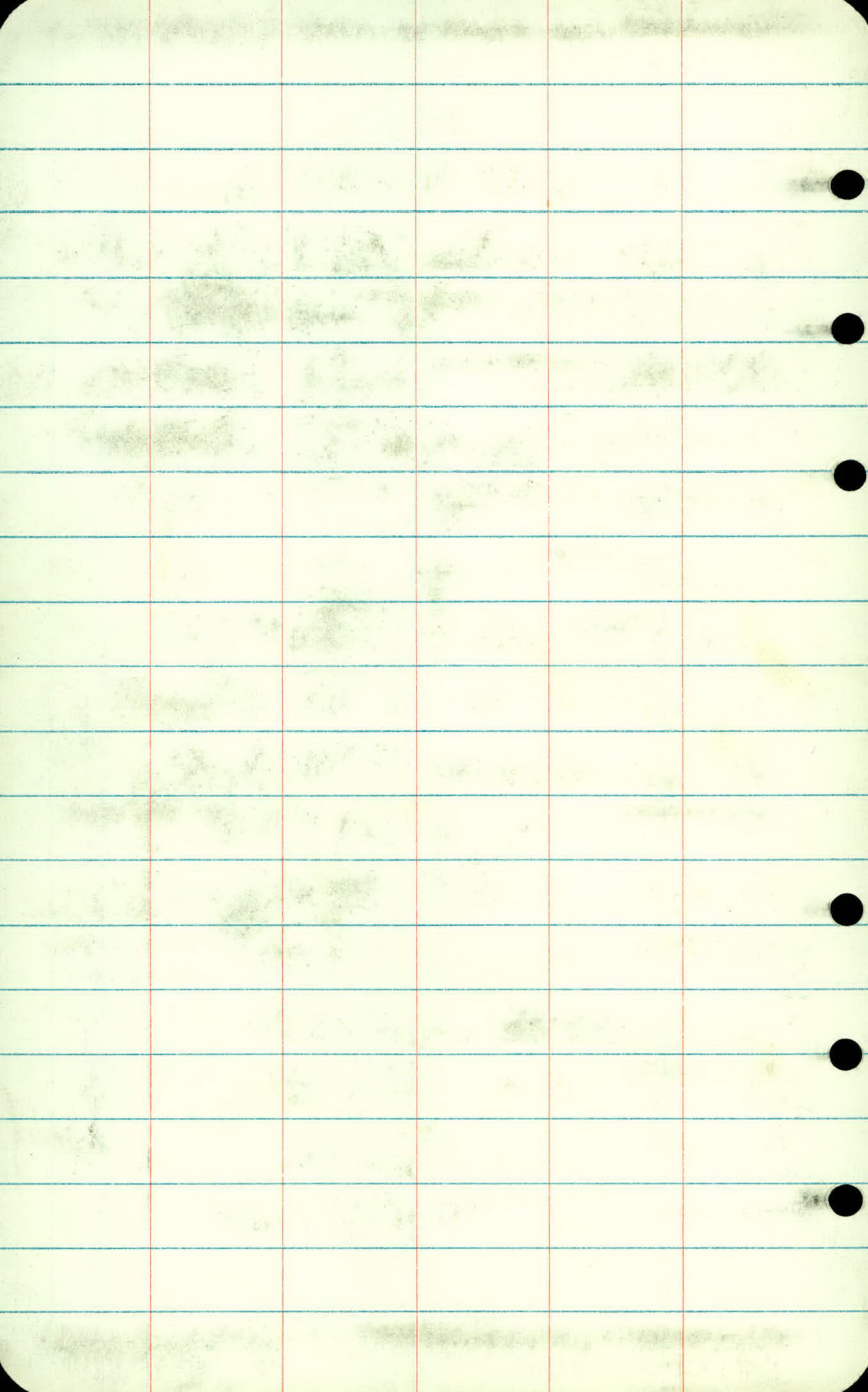
9.3

26

45

60

E STA 35+00



CENTERVILLE ROAD

alinement

119+33.12 P.O.T.

600'

54° X

764.36'

Co Rd E

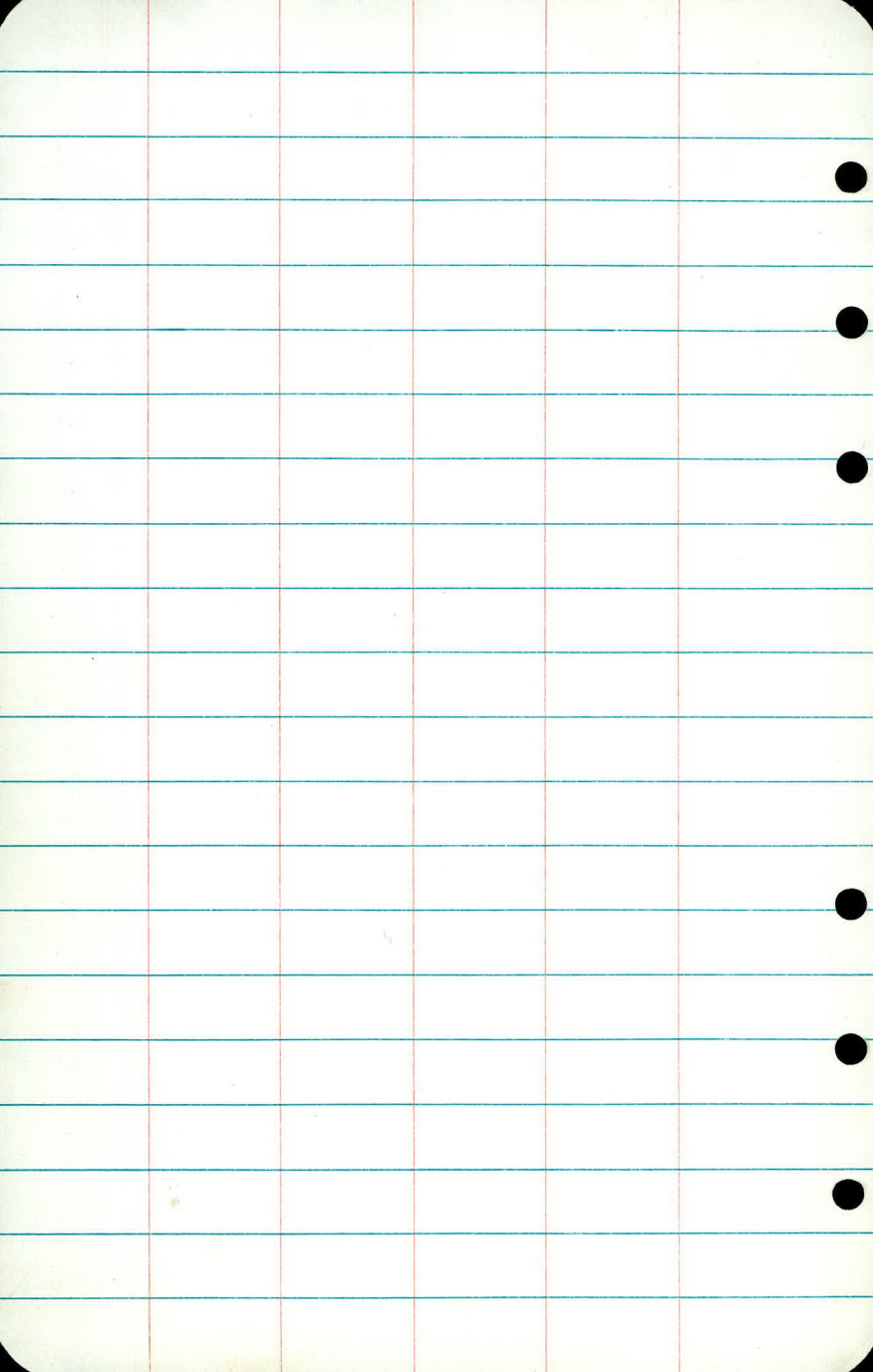
PK nail

Kochler Road

E
Section Line

Section Line

800'



CENTERVILLE RD.

TOPOGRAPHY

	LT.	RT.
+50	+50 SECOR HO 100 +46 14" PINE 76 +31 12" PINE 75	RD 10 RD 10 LILACS 35
+15 SWCOR HO 103	+11 15" CMP 21 +02 12' BIT ENT	
113+00	+91 15" CMP 21 +85 STUMP 64	RD +00 LILACS 10 40 +83 BE. LILACS +93 TP 40 27 +66 HEDGE 51-100+ +57 8" PINE +57 8" PINE 44 58 +53 8" PINE 58
+50		RD RD 10 10 +35 NECOR +48 8" PINE HO. 69 51 +35 10" ASH 44 +12 1" BERRY TREE 43
	+35 PP 28 +13 MH TELE 15	
112+00		RD BIT. RD 10 10 +84 6" PINE +85 6" PINE +86 7" ASH 33 33 40 +85 STUMP +75 15" CMP +90 NW COR 30 21 HO. 68 +66 14' GR. ENT. +97 MH +53 24" TILE SAN 21 PIPE 22 +53 15" CMP 21
+50		RD RD 10 10 +48 PP +49 14" ELM +49 15" ELM 28 56 88 +31 14" TILE PIPE 22
111+00		RD RD 10 10

CA
ML
LI
CG

LT.

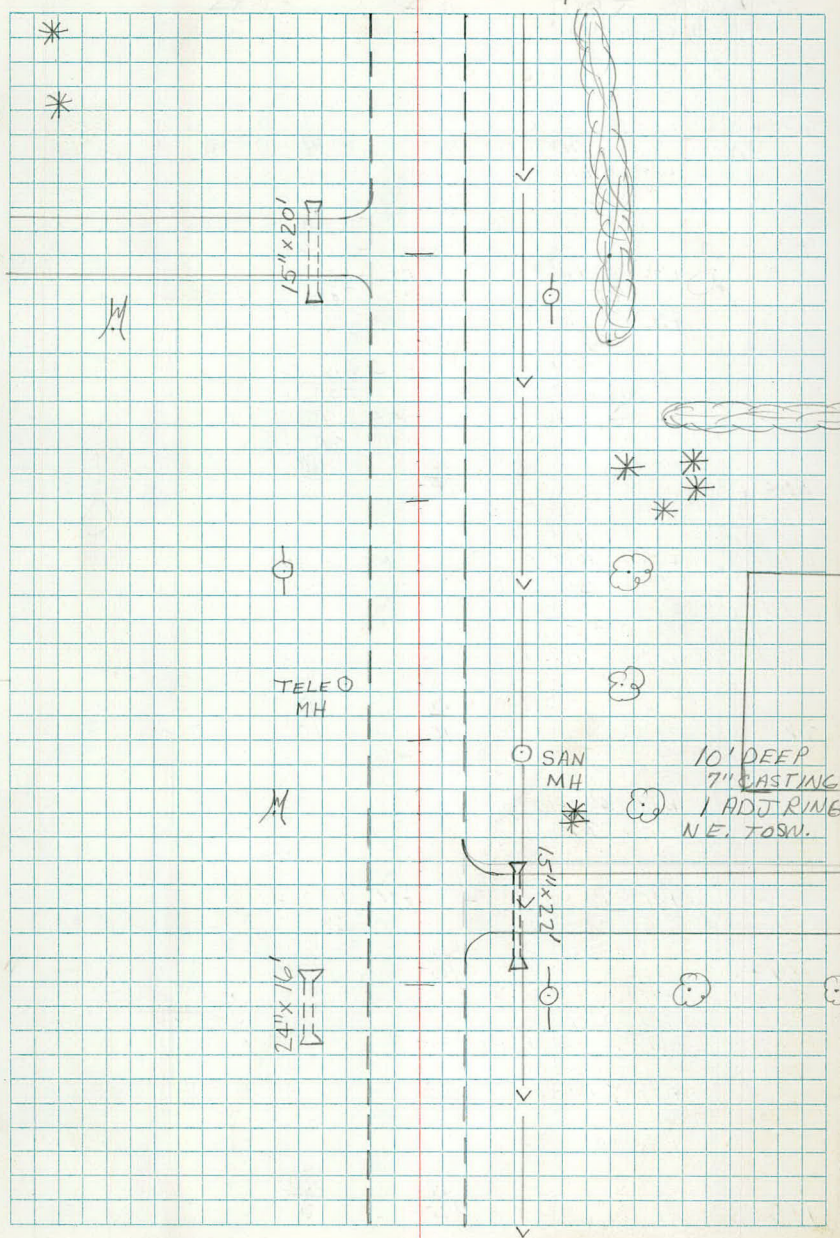
¢

RT

7-1-75
SUNNY

54

NE ↗



LT.

2

RT.

116 +00

RD
10RD
10+92 7" PINE
38+95 5" PINE
44+75 5" PINE
81+76 3" ASH
70+75 6" PINE
59+73 PP
28+69 6" PINE
42+74 18" ELM
52+56 STUMP
37

+50

RD
10RD
10+48 BUSH
41+49 TP
28+28 9" PINE
40+21 SE COR 10
105+42 E LILACS
33+02 9" PINE
40+23 MH
SAN 21

115 +00

RD
10RD
10LILACS
30+94 SW COR
HO 105+91 15" ASH
71+92 BUSH
40+76 15" CMP
21+84 BRICK BOX
2'x3' 53+67 12"
DIRT ENT+56 15" CMP
21+57 24" POPLAR
63

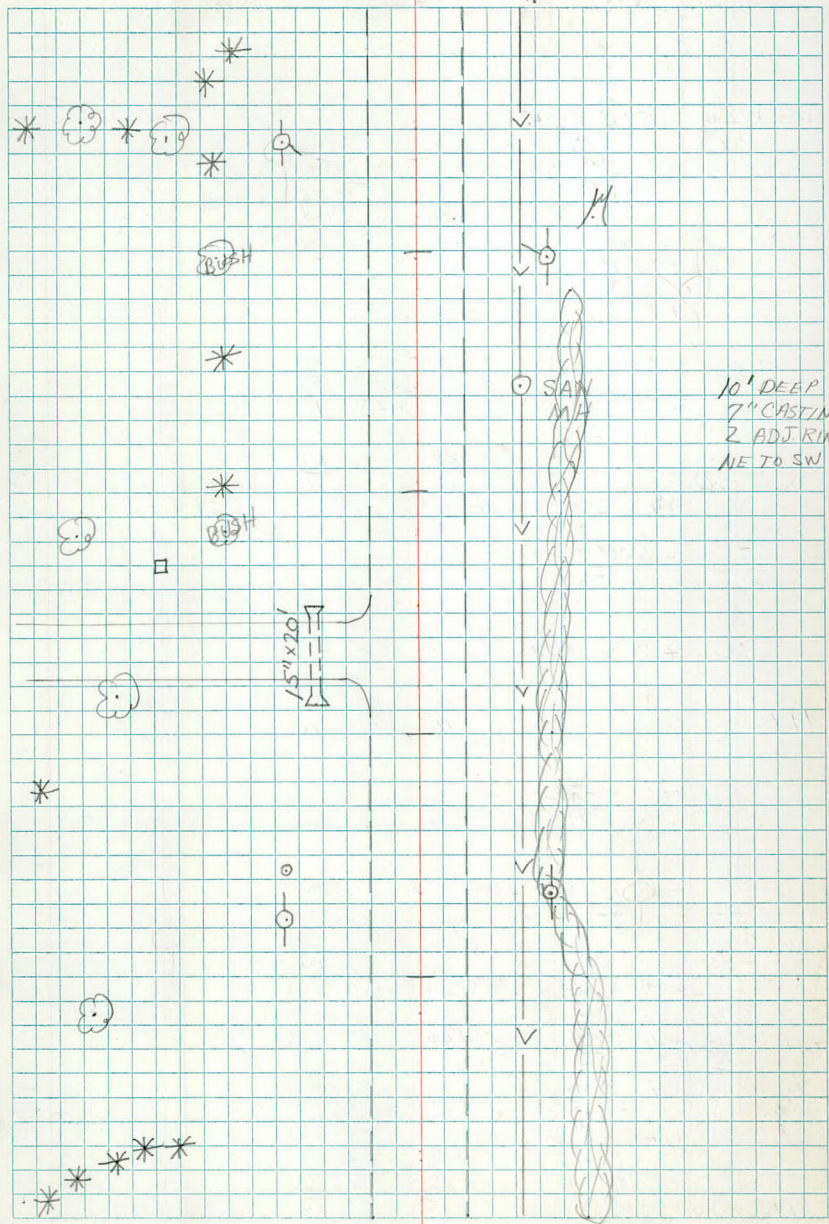
+50

RD
10RD
10LILACS
28+39 12" PINE
79+22 GUY WIRE
28+11 PP
28+17 TP
28+17 LILACS
28

114 +00

RD
10RD
10LILACS
35+92 6" ASH
67+64 8" PINE
57+61 7" PINE
64+64 8" PINE
50+59 7" PINE
71+54 8" PINE
78+50 SE COR
HO 100RD
10RD
10LILACS
35

113 +50

NE Δ 

LT

E

RT

✓
+50WOODS
52✓
+34 16" CTN W.
38✓
+34 24" C. PIPE
19

+13 TW 5" ASH

✓
38

+00 WOODS

✓
72

+70 4" ASH

✓
43

+91 3" ASH

39

118+00

✓
+50 COR WOODS✓
+52 3" POPLAR

29

78-100+

+50

+45 2" MAPLE +47 PP

29

+35 6" PINE

58

+30 6" PINE

75

+27 4-12" POPLAR

31

117+00

+96 SECOR HD +99 5" CEDAR

81

+63 SW COR

H.O. 81

+62 12" BIRCH

32

+52 CONC +57 15" CMP

32-70

21

+50

+37 15" CMP

20

+37 EDGE C.

12

+40 CONC +46 4 121

32-52 GR. ENT.

+29 BUSH +33 EDGE CONC

52 64

+17 SW COR +20 4" MAPLE

GARAGE 93 49

+14 COR. CONC.

63-72

116+00

✓
+35 POR

12

+12 MH

22

+00 B.E.R.

10

✓
+79 PROP. COR.

33

✓
+58 TP

28

RD

RD

10

+44 BUSH

31

+08 BUSH

32

RD

RD

10

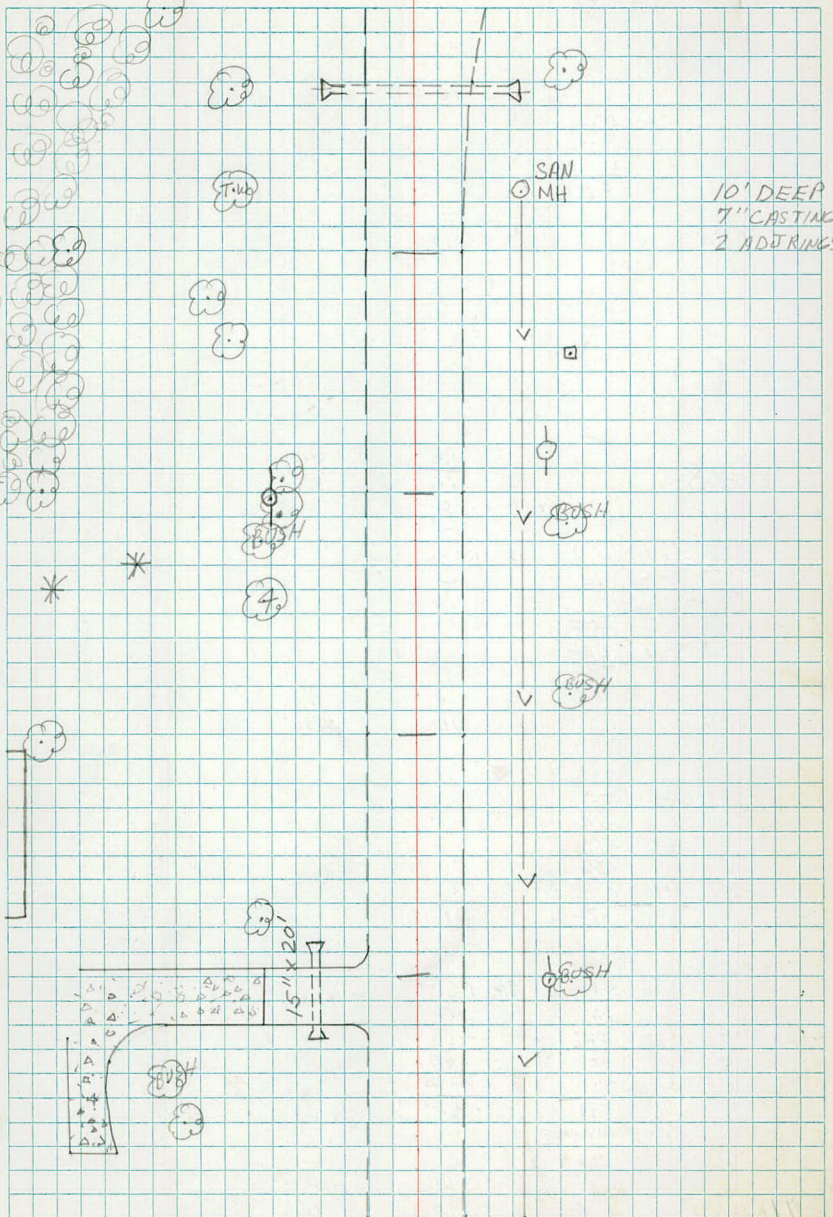
GA
ML
LI
CG

LT



RT

7-1-75 56
SUNNY



121+00

+00 5" ELM
40

LT. RD
12

RT. RD
10

+85 RD
10

+68 PP
32

+52 2" ASH
42

+50

RD
10

RD
10

+37 4" ASPEN
76

120+00

+79 24" CARBON
47

RD
11

+74 E.R
10

+67 ARC LT.
PP 32

+57 POR
26

+67 GUYWIRE
23

+51 BER
40

+50

+24 ER
51

+18 POR
26

+08 POR
16

+08 GP
21

+34 POR
45

119+00

+00 COR WOODS
56-100+

+94 GP
17

+94 DE.R
10

+82 MH
TELE 15

+75 PP
31

+75 WOODS
52-100+

+65 3" ASH
41

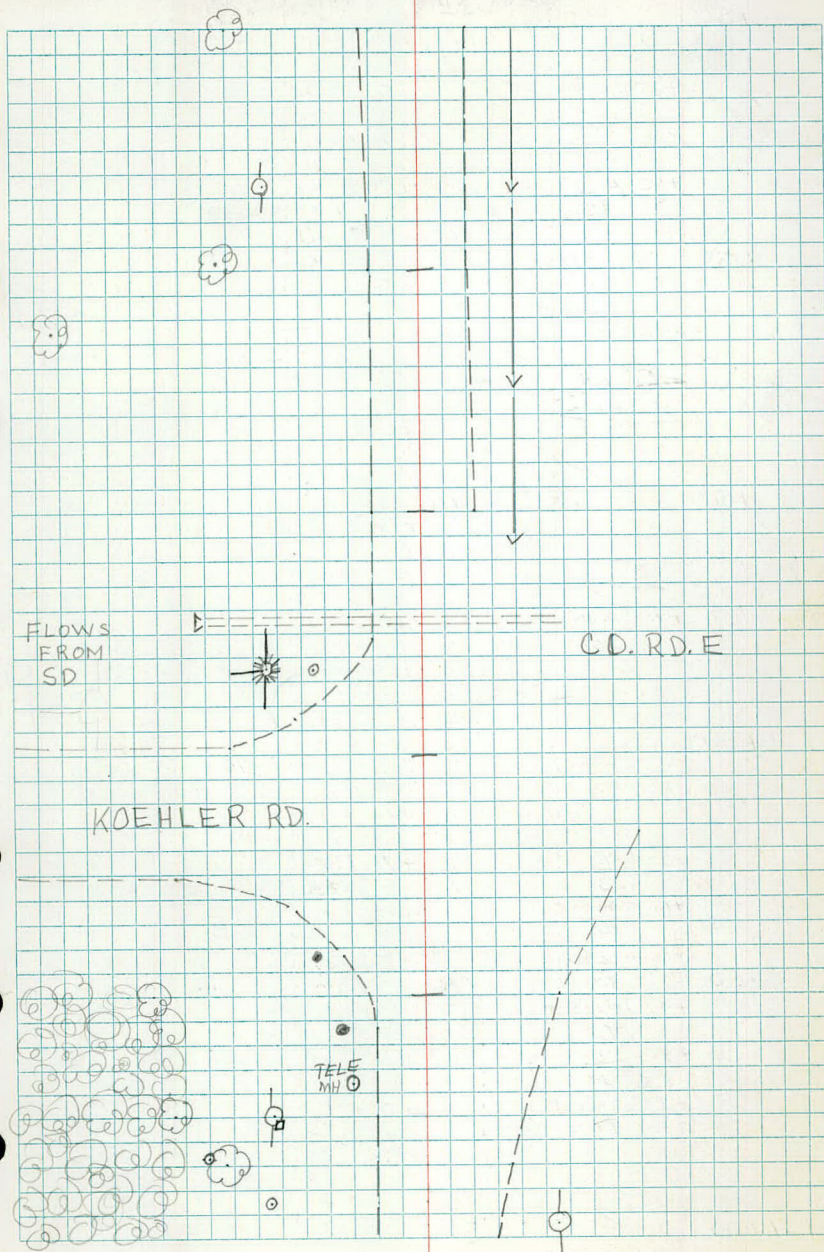
+66 GUYWIRE
45

+65 POR
17

+57 GUYWIRE
33

+52 TP
28

118+50



LT.

Q

RT.

+50

+35 SW COR
VADNAIS HEIGHTS
SCJL
75-100+

+03 ER
35

+00 BIT LOT
35-99

123+00
+99 GUY POLE
40

+98 PP
34

+91 PBR
20

+75 BER
12

+50

+41 COR BIT
PARKING LOT
36-99

122+00

RD
12

+66 PP
33

+60 GUY WIRE
49

+50 5-2" ELM
83

+50

+47 TW 19" ELM
75

+44 Q 12'
BIT ENT

+43 BRUSH HL
70 L ENT

+00 5" ELM
40

121+00

+33 10" ASH

54

+23 2" ELM

59

+10 10" ELM

49

+04 2" PINE

65

RD

10

+89 12" ASPEN

39

+83 TW 10" ASPEN

70

+51 TW 7" ASPEN

51

+51 4"
ASPEN
67

+44 1" ASPEN

40

+37 TR-12" ASPEN

52

+25 TW 6" ASPEN

92

+15 6" ASPEN

82

RD

10

+89 GUY WIRE +90 3" ASPEN

34

32

+72 GUY WIRE

40

+71 PP

32

+65 RD

12

+50 RD

10

+50 RD

10

+50 RD

10

+50 RD

10

+50 RD

10

+50 RD

10

+50 RD

10

GA
ML
LI

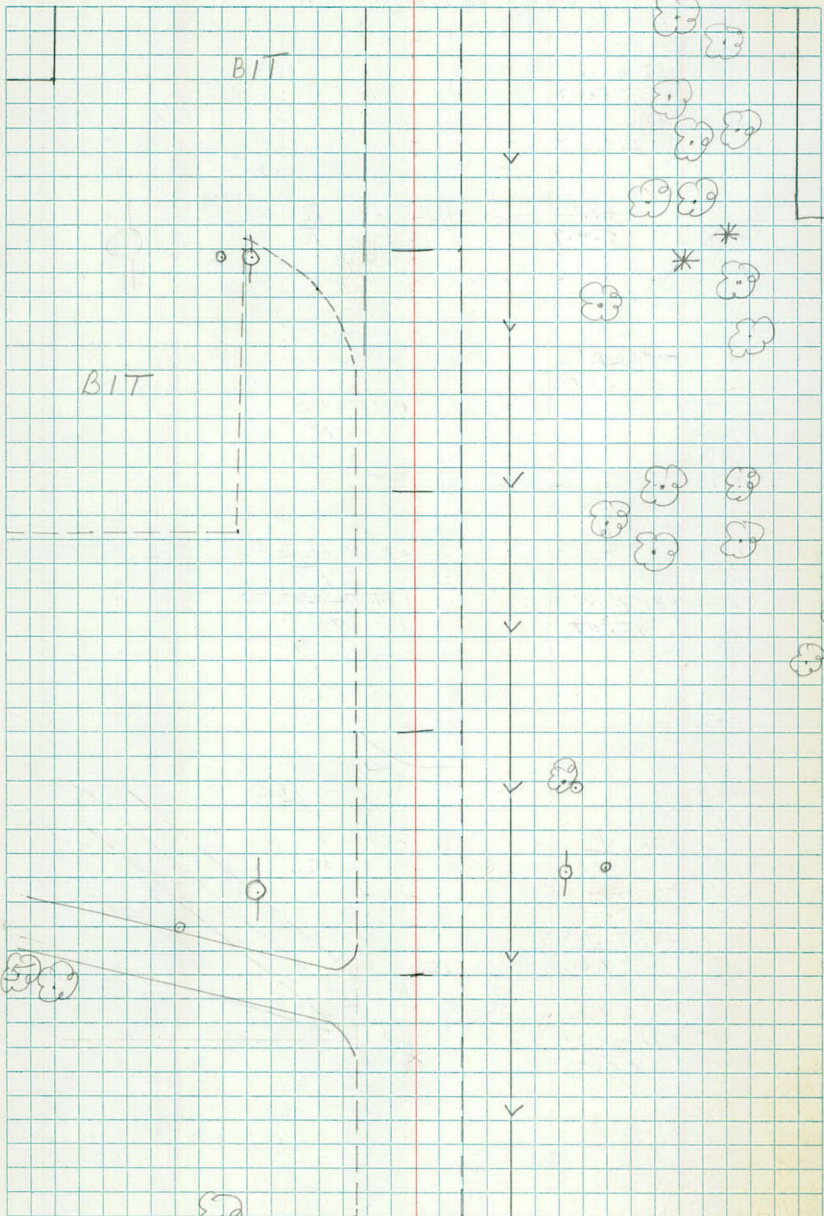
LT

2

RT

7-2-75
SUNNY

58



LT.

CL

RT.

126+00

+00 SCH
106

RD
10

RD
10

+00 BIT
28

+87 CL 18'
BIT ENT

+75 BIT
27-55-81

+50

BIT
27-71-90

RD
10

RD
10

+75 BIT
BIT ENT

+05 6" ASH
37

+08 PP
51

+03 BUSH
70

175+00

BIT
28

RD
10

+00 SCH
110

+72 BIT
44-75

+80 4" MAPLE
51

+95 BIT +81 CL 18'
28 BIT ENT.

+79 NE COR
HO. 80

+76 EDGE BIT
50

RD
10

+50

+63 EDGE BIT
29

+31 COR BIT
31

+03 COR BIT
LOT 45

+30 PP
ARCLT. 33

+25 CL 16'
GR. ENT.

+03 COR BIT
LOT 75

+16 FLAG POLE
75

+13 NW COR
HO. 84

+00 SCH
110

RD
10

RD
10

124+00

+98 3" POT ALD
50

+91 COR SCH
110

+91 COR SCH
75-110

+76 MH
20

+78 1" BERRY
36

+65 CL 15'
GR. ENT

+65 NE COR
HO. 81

+54 12" ELM
29

123+50

GA
ML
LI

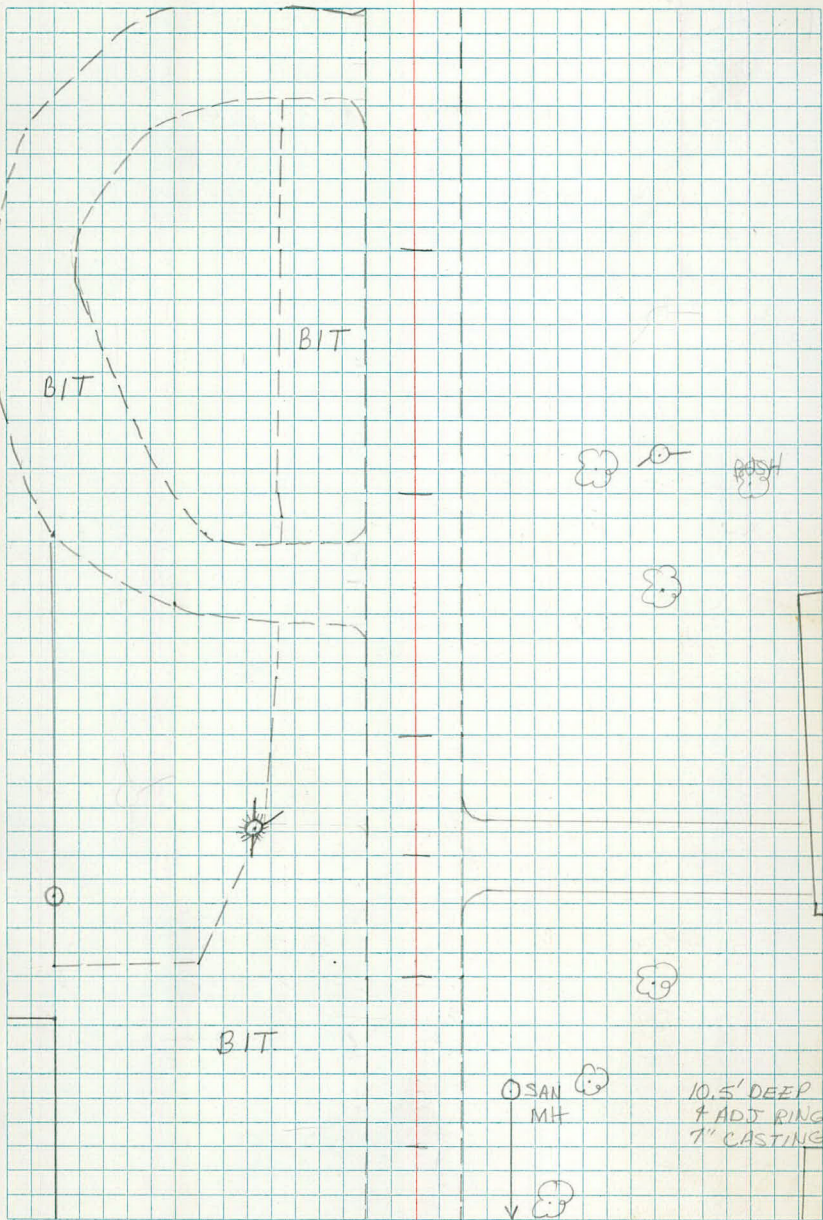
LT.

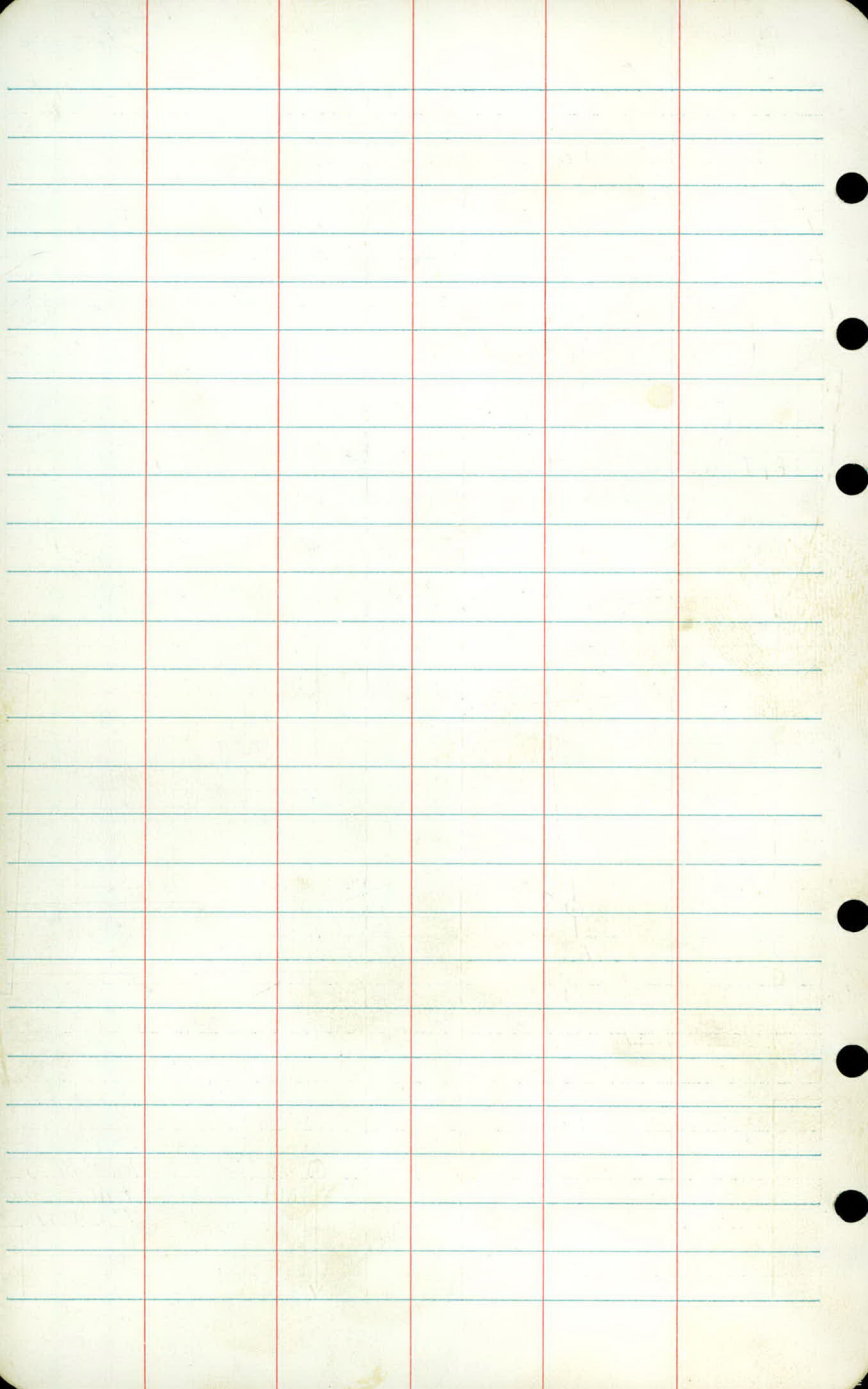
2

RT.

7-2-75
SUNNY

59





BENCH LEVELS

CENTERVILLE RD.

KOEHLER RD.

STA	+	$\bar{\Delta}$	—	ELEV
BM.	5.65	928.19		922.54
BM	8.72	931.69	5.22	922.97
BM	2.80	931.77	2.72	928.97
BM	5.22	928.19	8.80	922.97
BM	1.50	924.04	5.66	922.53
BM	1.12	918.66	6.50	917.54
BM	3.65	918.19	4.12	914.54
BM	7.01	924.55	0.65	917.54
BM			2.02	922.53

SPIKE IN PP SE COR CENT $\frac{1}{4}$ " E"

SPIKE IN PP STA 121+66 LT. 33'

SPIKE IN PP STA 126+10 LT. 33'

SPIKE IN PP STA 121+66 LT. 33'

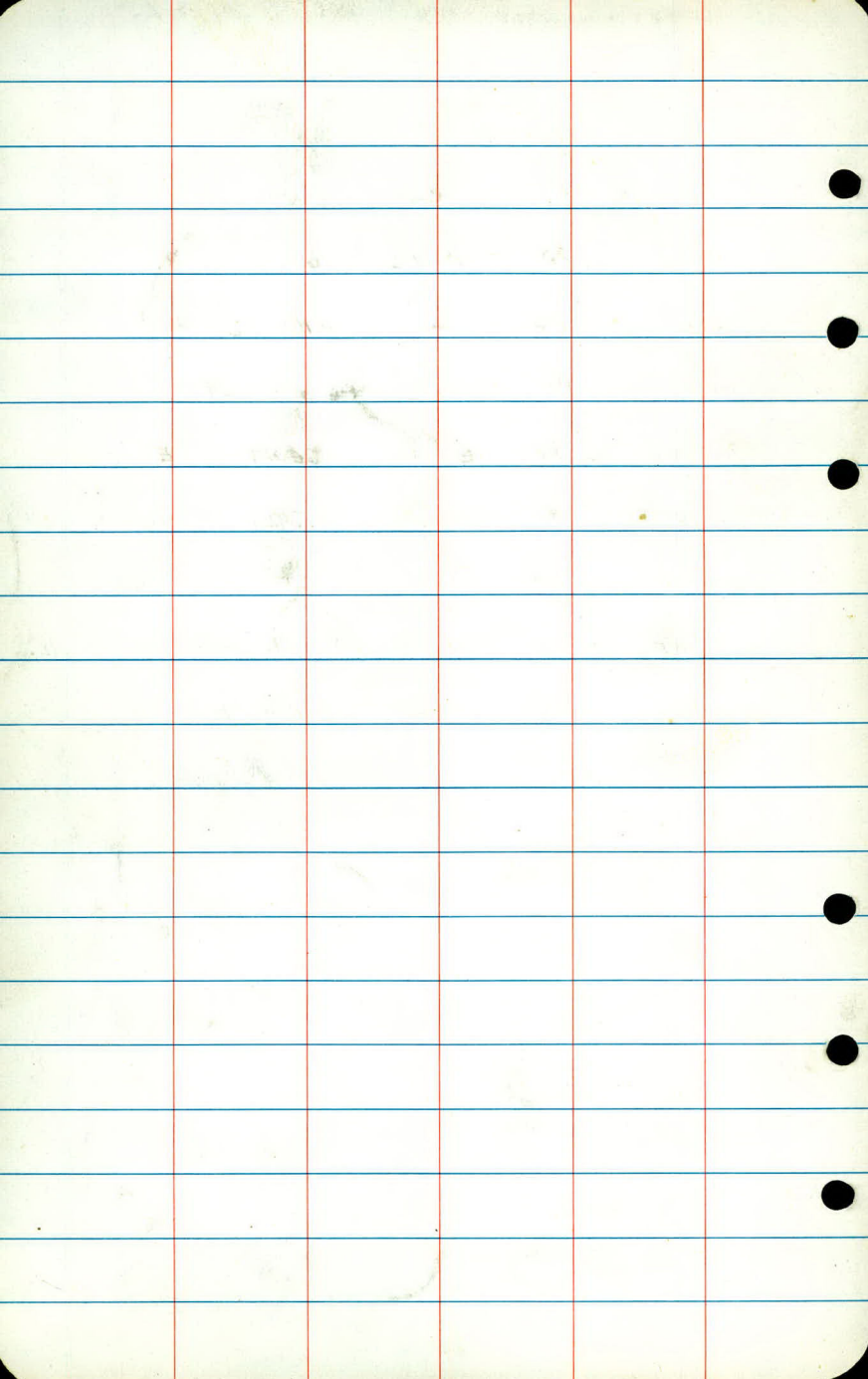
SPIKE IN PP SE COR CENT $\frac{1}{4}$ " E"

SPIKE IN PP STA 14+79 LT. 21 KOEHLER RD.

SPIKE IN PP STA 12+80 LT. 21 KOEHLER RD.

SPIKE IN PP STA 14+79 LT. 21 KOEHLER RD.

SPIKE IN PP SE COR CENT $\frac{1}{4}$ " E"



Rd 15 CONST. 15

X - SECTIONS

CENTERVILLE ROAD

STA. 111+00 To 126+00

STA. 131+00 To 144+00

STA	+	π	-	Elev
BM	4.32	926.86		(922.54)
TP	3.98	925.41	5.43	921.43
TP	4.60	924.40	5.61	919.80
111+00				
+37				
+53				
+66	ENT RT			

GA
ML
LI1-3-75
HOT 94°

LT

E

RT

SPIKE IN PP SE COR CENTERVILLE

SPIKE IN PP 115+73 LT 28'

SPIKE IN PP Sta 112+35 LT 28'

18.5	18.5	18.8	17.9	19.3	19.5	19.6	19.6	19.1	18.1	12.6	17.4
5.9	5.9	5.6	6.5	5.1	4.9	4.8	4.8	5.3	6.3	6.8	7.0
75	51	31	25	16	10	4.8	10	15	25	50	75

19.1	19.2	18.9	16.4	19.7	19.6	19.7	19.7	19.4	18.5	17.7	17.5
5.3	5.2	5.5	8.0	4.7	4.8	4.7	4.7	5.0	5.9	6.7	6.9
75	50	24	22	15	10	4.7	10	15	21	50	75

CULV.

18.9	19.2	19.2	15.8	19.7	19.7	19.8	19.7	19.4	17.9	19.1	18.9	18.4
5.5	5.2	5.2	8.6	4.7	4.7	4.6	4.7	5.0	6.5	5.3	5.5	6.0
75	50	28	22	18	10	4.6	10	17	20	23	50	75

INV. INV.

19.1	19.2	17.7	20.0	19.7	19.8	19.8	19.4	18.9	19.4
5.3	5.1	6.7	4.4	4.7	4.6	5.0	5.5	5.0	5.0
75	29	22	14	16	4.6	10	29	55	100

STA	+	π	-	ELEV
		924.40	1	
+75				
+97	MH RT. 21'		5.50	918.90
112+00				
TP	4.48	924.82	4.06	920.34
112+14	MH	LT. 16'	5.25	919.57
+50				

GA
ML
LE

LT.

2

RT

7-3-75
SUNNY
HOT

18.9

19.1

19.2

17.6

19.8

19.8

19.8

19.8

19.5

18.1

19.5

19.6

19.4

$\frac{5.5}{75}$

$\frac{5.3}{50}$

$\frac{5.2}{31}$

$\frac{6.8}{22}$

$\frac{4.6}{14}$

$\frac{4.6}{10}$

4.6

$\frac{4.6}{10}$

$\frac{4.9}{18}$

$\frac{6.3}{21}$

$\frac{4.9}{23}$

$\frac{4.8}{36}$

5

6

INV.

19.2

19.1

18.5

19.7

19.8

19.9

19.9

19.6

18.8

19.2

19.7

$\frac{5.2}{75}$

$\frac{5.3}{31}$

$\frac{5.9}{23}$

$\frac{4.7}{15}$

$\frac{4.6}{10}$

4.5

$\frac{4.5}{10}$

$\frac{4.8}{15}$

$\frac{5.6}{19}$

$\frac{5.2}{30}$

$\frac{4.7}{64}$

PK STA. 113+00 2

19.3

19.3

18.9

19.9

20.0

20.1

20.1

19.9

18.9

19.2

19.2

$\frac{5.5}{50}$

$\frac{5.5}{27}$

$\frac{6.3}{21}$

$\frac{4.9}{15}$

$\frac{4.8}{10}$

4.7

$\frac{4.7}{10}$

$\frac{4.9}{13}$

$\frac{5.9}{19}$

$\frac{5.6}{44}$

$\frac{5.6}{75}$

19.2

$\frac{5.6}{75}$

STA

+

K

-

ELEV

924.82

+ 92

113+00

¢

ENT LT.

+ 12

+ 50

114+00

TP

4.92

925.70

4.04

920.78

6A
ML
LT

LT

£

RT

7-3-75
SUNNY
HOT

DIETZGEN NO. 384-5

19.4	19.4	19.4	17.8	20.2	20.2	20.3	20.2	20.1	18.7	19.2	18.8
$\frac{5.4}{75}$	$\frac{5.4}{50}$	$\frac{5.4}{23}$	$\frac{7.0}{21}$	$\frac{4.6}{17}$	$\frac{4.6}{10}$	4.5	$\frac{4.6}{10}$	$\frac{4.7}{14}$	$\frac{6.1}{21}$	$\frac{5.6}{28}$	$\frac{6.0}{69}$

INV.

19.5	19.7	20.2	20.3	20.3	20.0	18.7	19.3	18.4
$\frac{5.3}{75}$	$\frac{5.1}{36}$	$\frac{4.6}{10}$	4.5	$\frac{4.5}{10}$	$\frac{4.8}{19}$	$\frac{6.1}{23}$	$\frac{5.5}{50}$	$\frac{6.4}{75}$

19.6	19.7	19.4	17.4	20.2	20.3	20.4	20.3	20.1	18.8	19.2	18.5
$\frac{5.2}{75}$	$\frac{5.1}{50}$	$\frac{5.4}{25}$	$\frac{6.9}{22}$	$\frac{4.6}{16}$	$\frac{4.5}{10}$	4.4	$\frac{4.5}{10}$	$\frac{4.7}{14}$	$\frac{6.0}{24}$	$\frac{5.6}{35}$	$\frac{6.3}{78}$

19.4	19.6	19.5	18.8	20.4	20.4	20.5	20.4	20.1	18.8	19.1	18.6
$\frac{5.4}{68}$	$\frac{5.2}{50}$	$\frac{5.3}{28}$	$\frac{6.0}{22}$	$\frac{4.4}{15}$	$\frac{4.4}{10}$	4.3	$\frac{4.4}{10}$	$\frac{4.7}{14}$	$\frac{6.0}{23}$	$\frac{5.7}{34}$	$\frac{6.2}{60}$

19.6	19.6	19.7	19.2	20.7	20.6	20.7	20.6	20.2	19.2	19.3	18.6
$\frac{5.2}{75}$	$\frac{5.2}{55}$	$\frac{5.1}{30}$	$\frac{5.6}{22}$	$\frac{4.1}{15}$	$\frac{4.2}{10}$	4.1	$\frac{4.2}{10}$	$\frac{4.6}{15}$	$\frac{5.6}{22}$	$\frac{5.5}{33}$	$\frac{6.2}{65}$

SPIKE IN PP STA 114+10 LT. 28'

STA

+

π

-

ELEV

925.70

+ 5

114+56

+68

ENT LT.

+76

115+00

+22

MH RT. 21' 5.35 920.35

+50

GA
ML
LI

LT

E

RT.

7-3-75
SUNNY
HOT

20.1	20.1	20.3	18.7	21.2	20.9	21.0	21.0	20.5	19.4	20.0	19.3
$\frac{5.6}{75}$	$\frac{5.6}{50}$	$\frac{5.4}{25}$	$\frac{7.0}{22}$	$\frac{4.5}{16}$	$\frac{4.8}{10}$	4.7	$\frac{4.7}{10}$	$\frac{5.2}{15}$	$\frac{6.3}{23}$	$\frac{5.7}{29}$	$\frac{6.4}{60}$
			INV								
20.2	20.2	20.6	20.9	21.0	21.0	20.5	19.4	19.7	19.4		
$\frac{5.5}{75}$	$\frac{5.5}{47}$	$\frac{5.1}{27}$	$\frac{4.8}{10}$	4.7	$\frac{4.7}{10}$	$\frac{5.2}{15}$	$\frac{6.3}{23}$	$\frac{6.0}{31}$	$\frac{6.3}{60}$		
20.3	20.4	20.7	18.9	21.0	20.9	21.1	21.1	20.6	19.5	19.8	19.5
$\frac{5.4}{87}$	$\frac{5.3}{40}$	$\frac{5.0}{26}$	$\frac{6.8}{21}$	$\frac{4.7}{16}$	$\frac{4.8}{10}$	4.6	$\frac{4.6}{10}$	$\frac{5.1}{16}$	$\frac{6.2}{22}$	$\frac{5.9}{30}$	$\frac{6.2}{65}$
			INV								
19.8	20.2	19.3	20.8	21.0	21.2	21.1	20.8	19.8	19.9	19.4	
$\frac{5.9}{65}$	$\frac{5.5}{29}$	$\frac{6.4}{23}$	$\frac{4.9}{15}$	$\frac{4.7}{10}$	4.5	$\frac{4.6}{10}$	$\frac{4.9}{15}$	$\frac{5.9}{24}$	$\frac{5.8}{50}$	$\frac{6.3}{75}$	
20.2	20.4	20.5	19.6	21.0	21.2	21.4	21.3	20.9	19.9	20.2	19.6
$\frac{5.5}{75}$	$\frac{5.3}{50}$	$\frac{5.2}{27}$	$\frac{6.1}{22}$	$\frac{4.7}{15}$	$\frac{4.5}{10}$	4.3	$\frac{4.4}{10}$	$\frac{4.8}{15}$	$\frac{5.8}{23}$	$\frac{5.5}{50}$	$\frac{6.1}{75}$

DIETZGEN NO. 384-5

STA	+	+	-	ELEV	
		925.70			
116+00					
B.M.	5.05	926.48	4.27	921.43	921.43
+38					
+47					
+57					
117+00					

WS
GA
ML
LI

LT

Q

RT

7-7-75
SUNNY
HOT

20.2

20.1

19.5

21.4

21.5

21.6

21.5

21.1

20.3

20.6

19.8

 $\frac{5.5}{50}$ $\frac{5.0}{27}$ $\frac{6.2}{22}$ $\frac{4.3}{15}$ $\frac{4.2}{10}$

4.1

 $\frac{4.2}{10}$ $\frac{4.6}{15}$ $\frac{5.4}{29}$ $\frac{5.1}{50}$ $\frac{5.9}{75}$

19.9

 $\frac{5.8}{75}$

SPIKE IN PP 115+73 LT. 28'

20.7

20.6

20.7

19.2

21.4

21.7

21.8

21.6

21.3

20.5

20.5

19.7

 $\frac{5.8}{75}$ $\frac{5.9}{51}$ $\frac{5.8}{28}$ $\frac{7.3}{21}$ $\frac{5.1}{15}$ $\frac{4.8}{10}$

4.7

 $\frac{4.9}{10}$ $\frac{5.2}{14}$ $\frac{6.0}{24}$ $\frac{6.0}{50}$ $\frac{6.8}{75}$

CONC

INV

20.7

20.8

21.0

21.7

21.8

21.7

21.4

20.5

20.5

19.7

 $\frac{5.8}{75}$ $\frac{5.7}{53}$ $\frac{5.5}{33}$ $\frac{4.8}{10}$

4.7

 $\frac{4.8}{10}$ $\frac{5.1}{14}$ $\frac{6.0}{24}$ $\frac{6.0}{50}$ $\frac{6.8}{75}$

CONC

20.8

20.9

20.6

19.3

21.0

21.7

21.8

21.7

21.3

20.5

20.5

19.9

 $\frac{5.7}{75}$ $\frac{5.6}{50}$ $\frac{5.9}{25}$ $\frac{7.2}{22}$ $\frac{5.5}{19}$ $\frac{4.8}{10}$

4.7

 $\frac{4.8}{10}$ $\frac{5.2}{15}$ $\frac{6.0}{24}$ $\frac{6.0}{50}$ $\frac{6.6}{75}$

INV

20.6

20.8

20.7

20.1

21.8

21.8

22.0

21.9

21.4

20.8

20.6

20.0

 $\frac{5.9}{75}$ $\frac{5.7}{50}$ $\frac{5.8}{33}$ $\frac{6.4}{24}$ $\frac{4.7}{14}$ $\frac{4.7}{10}$

4.5

 $\frac{4.6}{10}$ $\frac{5.1}{15}$ $\frac{5.7}{22}$ $\frac{5.9}{54}$ $\frac{6.5}{75}$

STA

+

K

-

ELEV

926.48

117 +50

118 +00

+ 12

MH

RT. 22'

4.47

922.01

+34

TP

3.61

926.15

3.93

922.55

922.54

118 +66

WS
GA
ML
LI

LT.

E

RT

7-7-75
SUNNY
HOT

19.5	20.9	20.7	22.0	22.1	22.1	22.1	21.5	20.6	21.0	20.0
$\frac{7.0}{75}$	$\frac{5.6}{50}$	$\frac{5.8}{23}$	$\frac{4.5}{17}$	$\frac{4.4}{10}$	4.7	$\frac{4.4}{10}$	$\frac{5.0}{16}$	$\frac{5.9}{23}$	$\frac{5.5}{50}$	$\frac{6.5}{75}$

18.5	20.7	21.7	20.7	22.0	22.2	22.4	22.2	21.9	21.2	21.5	20.6
$\frac{8.0}{75}$	$\frac{5.8}{52}$	$\frac{4.8}{29}$	$\frac{5.8}{24}$	$\frac{4.5}{17}$	$\frac{4.3}{10}$	4.1	$\frac{4.3}{10}$	$\frac{4.6}{14}$	$\frac{5.3}{24}$	$\frac{5.0}{50}$	$\frac{5.9}{75}$

18.3	20.4	21.5	19.7	17.8	22.0	22.3	22.5	22.2	21.8	18.5	22.2	21.3	20.9
$\frac{8.2}{71}$	$\frac{6.1}{53}$	$\frac{5.0}{31}$	$\frac{6.8}{25}$	$\frac{8.7}{19}$	$\frac{4.5}{17}$	$\frac{4.2}{11}$	4.0	$\frac{4.3}{12}$	$\frac{4.7}{17}$	$\frac{8.0}{21}$	$\frac{4.3}{31}$	$\frac{5.2}{56}$	$\frac{5.6}{75}$

FL.24"

FL.24"

SPIKE IN PP SE COR CENT. 4" E"

17.8	20.3	21.5	19.9	22.0	22.6	22.7	22.0	21.1	20.1	22.5	21.6	21.0
$\frac{8.4}{75}$	$\frac{5.9}{50}$	$\frac{4.7}{31}$	$\frac{6.3}{23}$	$\frac{4.2}{18}$	$\frac{3.6}{10}$	3.5	$\frac{4.2}{16}$	$\frac{5.1}{23}$	$\frac{6.1}{28}$	$\frac{3.7}{33}$	$\frac{4.6}{54}$	$\frac{5.2}{75}$

STA

+

π

-

ELEV

926.15

119+00

+21

+35

+49

+58

+76

WS
GA
ML
LI

LT.

E

RT

7-7-75
SUNNY
HOT

16.8	18.5	18.4	19.6	22.4	22.7	22.8	22.7	21.3	21.1	21.0	21.3
$\frac{9.4}{75}$	$\frac{7.7}{57}$	$\frac{7.8}{42}$	$\frac{6.6}{26}$	$\frac{3.8}{17}$	$\frac{3.5}{10}$	3.4	$\frac{3.5}{10}$	$\frac{4.9}{27}$	$\frac{5.1}{41}$	$\frac{4.4}{56}$	$\frac{4.9}{75}$

21.4	21.8	22.4	22.9	22.9	22.9	21.3	20.5	21.7	21.2
$\frac{4.8}{75}$	$\frac{4.4}{56}$	$\frac{3.8}{35}$	$\frac{3.3}{10}$	3.3	$\frac{3.3}{10}$	$\frac{4.9}{38}$	$\frac{5.7}{53}$	$\frac{4.5}{57}$	$\frac{5.0}{75}$

21.8	22.3	22.5	22.9	23.0	22.9	21.4	20.0	21.8	21.8
$\frac{4.4}{75}$	$\frac{3.9}{50}$	$\frac{3.7}{30}$	$\frac{3.3}{10}$	3.2	$\frac{3.3}{10}$	$\frac{4.8}{50}$	$\frac{6.2}{58}$	$\frac{4.4}{64}$	$\frac{4.4}{75}$

21.3	22.1	22.6	22.9	23.0	23.0	22.4	21.3	20.9	19.9	21.9
$\frac{4.9}{75}$	$\frac{4.1}{46}$	$\frac{3.6}{30}$	$\frac{3.3}{10}$	3.2	$\frac{3.2}{10}$	$\frac{3.8}{40}$	$\frac{4.9}{56}$	$\frac{5.3}{66}$	$\frac{6.3}{72}$	$\frac{4.3}{75}$

20.8	21.9	22.5	23.0	23.1	23.1	22.8	21.4
$\frac{5.4}{75}$	$\frac{4.3}{46}$	$\frac{3.7}{24}$	$\frac{3.2}{10}$	3.1	$\frac{3.1}{10}$	$\frac{3.4}{39}$	$\frac{4.8}{71}$

11.1	12.0	15.70	20.0	22.2	23.1	23.2	23.1	23.0	22.4	21.6
$\frac{15.1}{65}$	$\frac{14.2}{47}$	$\frac{10.45}{46}$	$\frac{6.2}{36}$	$\frac{4.0}{25}$	$\frac{3.1}{10}$	3.0	$\frac{3.1}{10}$	$\frac{3.2}{39}$	$\frac{3.8}{61}$	$\frac{4.6}{75}$

FL 24"

10.6
→ $\frac{15.6}{75}$

STA

+

K

—

ELEV

926.15

119+78

MH RT. 21'

3.19

922.96

+85

120+00

TP

4.84

928.09

2.90

923.25

120+50

121+00

WS
GA
ML
LI

LT.

⊥

RT.

7-7-75
SUNNY
HOT

14.6	16.9	19.8	22.8	23.0	23.2	23.2	21.9	20.30	21.2	23.8
<u>11.6</u>	<u>9.3</u>	<u>6.4</u>	<u>3.4</u>	<u>3.2</u>	<u>3.0</u>	<u>3.0</u>	<u>4.3</u>	<u>5.85</u>	<u>5.0</u>	<u>3.4</u>
75	48	34	20	10	3.0	10	23	26	90	52

W.EDGE S.D.

22.6
3.6
75

16.0	17.2	19.5	22.7	23.2	23.3	23.2	22.4	21.0	20.5	22.1	22.9
<u>10.2</u>	<u>9.0</u>	<u>6.7</u>	<u>3.5</u>	<u>3.0</u>	<u>3.0</u>	<u>3.0</u>	<u>3.8</u>	<u>5.2</u>	<u>5.7</u>	<u>4.1</u>	<u>3.3</u>
75	50	32	17	10	2.9	10	20	29	44	60	70

22.9
3.3
75

PK ⊥ STA 120+00

14.4	16.4	18.3	20.0	18.7	23.2	23.4	23.5	23.4	22.5	21.7	22.1
<u>13.7</u>	<u>11.7</u>	<u>9.8</u>	<u>8.1</u>	<u>9.4</u>	<u>4.9</u>	<u>4.7</u>	<u>4.6</u>	<u>4.7</u>	<u>5.6</u>	<u>6.4</u>	<u>6.0</u>
75	57	39	31	25	16	10	4.6	10	24	45	75

14.3	18.1	18.7	23.4	23.9	24.0	23.9	23.4	21.7	21.2	21.1
<u>13.8</u>	<u>10.0</u>	<u>9.4</u>	<u>4.7</u>	<u>4.2</u>	<u>4.1</u>	<u>4.2</u>	<u>4.7</u>	<u>6.4</u>	<u>6.9</u>	<u>7.0</u>
75	50	34	20	10	4.1	10	19	26	50	75

STA

+

K

-

ELEV

928.09

121 +31

+45 ϕ ENT LT.

+60

122 +00

+50

BM

8.69

931.66

5.12

922.97

922.97

WS
GA
ML
LI

LT.

♀

RT.

7-7-75
SUNNY
HOT

15.3	17.2	21.4	22.5	24.2	24.3	24.2	23.7	21.8	21.1	21.1
<u>12.8</u>	<u>10.9</u>	<u>6.7</u>	<u>5.6</u>	<u>3.9</u>	2.8	<u>3.9</u>	<u>1.4</u>	<u>6.3</u>	<u>7.0</u>	<u>7.0</u>
75	59	38	28	10		10	16	26	50	75

19.9	20.9	22.5	24.4	24.5	24.4	23.7	22.1	21.4	21.2
<u>8.2</u>	<u>7.2</u>	<u>5.6</u>	<u>3.7</u>	3.6	<u>3.7</u>	<u>4.4</u>	<u>6.0</u>	<u>6.7</u>	<u>6.9</u>
63	47	28	10		10	18	26	50	75

19.3	19.5	19.5	20.8	23.0	24.5	24.7	24.6	23.8	22.1	21.7	21.3
<u>8.8</u>	<u>8.4</u>	<u>8.6</u>	<u>7.3</u>	<u>5.1</u>	<u>3.6</u>	3.4	<u>3.5</u>	<u>4.3</u>	<u>6.0</u>	<u>6.4</u>	<u>6.8</u>
75	60	46	30	21	10		10	18	28	50	75

20.9	22.5	22.0	22.4	24.3	25.1	25.2	25.1	24.6	23.3	23.5	22.7
<u>7.2</u>	<u>5.6</u>	<u>6.1</u>	<u>5.7</u>	<u>3.8</u>	<u>3.0</u>	2.9	<u>3.0</u>	<u>3.5</u>	<u>4.8</u>	<u>4.6</u>	<u>5.4</u>
75	45	28	22	17	10		10	19	30	50	75

24.0	24.7	25.0	24.1	25.2	25.8	25.9	25.8	25.5	25.7	25.5	25.1
<u>4.1</u>	<u>3.4</u>	<u>3.1</u>	<u>4.0</u>	<u>2.9</u>	<u>2.3</u>	2.2	<u>2.3</u>	<u>2.6</u>	<u>2.4</u>	<u>2.6</u>	<u>3.0</u>
75	50	37	24	18	10		10	19	27	39	75

SPIKE IN PP STA 121+66 LT. 33'

STA

+

K

-

ELEV

931.66

123+00

+40

+65 ϕ ENT. RT.

+76 MH RT. 22' 4.69 924.97

124+00

+24 ϕ ENT RT.

WS
GA
ML
LI

LT,

Ⓢ

RT,

7-7-75
SUNNY
HOT

25.1	25.1	26.1	25.6	26.4	26.5	26.4	26.3	26.2	26.3	26.7
$\frac{6.6}{75}$	$\frac{6.0}{57}$	$\frac{5.6}{36}$	$\frac{6.1}{22}$	$\frac{5.3}{10}$	5.2	$\frac{5.3}{10}$	$\frac{5.4}{18}$	$\frac{5.5}{36}$	$\frac{5.4}{54}$	$\frac{5.0}{75}$

26.3	26.6	26.6	26.1	26.8	26.9	26.8	26.7	26.5	27.0	27.6
$\frac{5.4}{75}$	$\frac{5.1}{59}$	$\frac{5.1}{36}$	$\frac{5.6}{21}$	$\frac{4.9}{10}$	4.8	$\frac{4.9}{10}$	$\frac{5.0}{19}$	$\frac{5.2}{31}$	$\frac{4.7}{50}$	$\frac{4.04}{75}$

C.WALK

27.1	26.8	26.3 26.4	27.0	27.1	27.0	26.9	27.0	27.6
$\frac{4.6}{75}$	$\frac{4.9}{40}$	$\frac{5.3}{20}$	$\frac{4.7}{10}$	4.6	$\frac{4.7}{10}$	$\frac{4.8}{28}$	$\frac{4.7}{50}$	$\frac{4.1}{75}$

27.6	27.5	27.4	26.8	27.3	27.3	27.2	27.2	27.2	27.2	27.8
$\frac{4.07}{75}$	$\frac{4.2}{56}$	$\frac{4.3}{35}$	$\frac{4.9}{20}$	$\frac{4.4}{10}$	4.4	$\frac{4.5}{10}$	$\frac{4.5}{18}$	$\frac{4.5}{36}$	$\frac{4.5}{50}$	$\frac{3.9}{75}$

C.WALK

27.8	27.8	27.6	27.0	27.4 27.4	27.3 27.5	27.4 27.4	27.1	27.0	27.3	28.3
$\frac{3.9}{75}$	$\frac{3.9}{50}$	$\frac{4.1}{35}$	$\frac{4.7}{20}$	$\frac{4.3}{10}$	4.2	$\frac{4.3}{10}$	$\frac{4.6}{20}$	$\frac{4.7}{35}$	$\frac{4.4}{50}$	$\frac{3.4}{75}$

STA

7

K

—

ELEV

931.66

124+81 $\frac{1}{2}$ ENT LT.

125+00

+50

+87 $\frac{1}{2}$ ENT LT.

126+00

Bm

2.69 928.97 928.97

WS
GA
ML
LI

LT.

Q

RT.

7-7-75
SUNNY
HOT

28.0	28.2	28.0	27.6	27.8	27.8	27.8	27.6	27.7	28.5
$\frac{3.7}{75}$	$\frac{3.5}{50}$	$\frac{3.7}{31}$	$\frac{4.1}{20}$	$\frac{3.9}{10}$	3.9	$\frac{3.7}{10}$	$\frac{4.1}{20}$	$\frac{4.0}{40}$	$\frac{3.2}{75}$

28.4	28.2	28.1	27.7	27.9	27.9	27.9	27.8	27.9	27.8
$\frac{3.3}{75}$	$\frac{3.5}{50}$	$\frac{3.6}{28}$	$\frac{4.0}{20}$	$\frac{3.8}{10}$	3.8	$\frac{3.8}{10}$	$\frac{3.9}{20}$	$\frac{3.8}{50}$	$\frac{3.9}{75}$

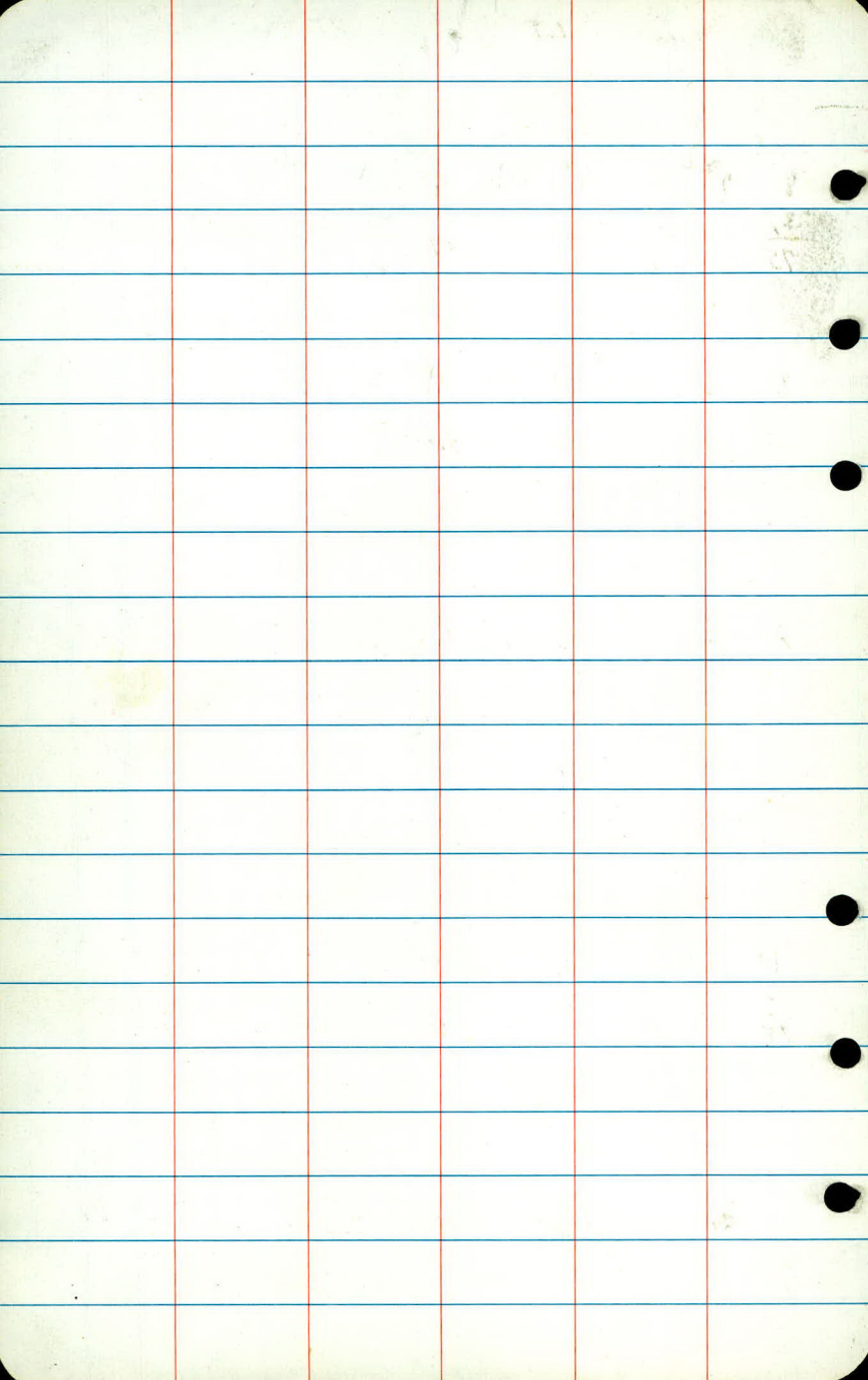
28.4	28.3	28.2	28.0	28.1	28.1	28.1	27.9	27.8	28.0
$\frac{3.3}{75}$	$\frac{3.4}{50}$	$\frac{3.5}{27}$	$\frac{3.7}{18}$	$\frac{3.6}{10}$	3.6	$\frac{3.6}{10}$	$\frac{3.8}{20}$	$\frac{3.9}{50}$	$\frac{3.7}{75}$

28.5	28.5	28.0	28.1	28.2	28.2	27.9	27.8	27.9
$\frac{3.2}{75}$	$\frac{3.2}{50}$	$\frac{3.7}{18}$	$\frac{3.6}{10}$	3.5	$\frac{3.5}{10}$	$\frac{3.8}{20}$	$\frac{3.9}{50}$	$\frac{3.8}{75}$

27.9
~~27.86~~

28.4	28.4	28.2	28.1	28.1	28.2	28.2	28.0	28.0	28.0
$\frac{3.3}{75}$	$\frac{3.3}{50}$	$\frac{3.5}{36}$	$\frac{3.6}{18}$	$\frac{3.6}{10}$	3.5	$\frac{3.5}{10}$	$\frac{3.7}{20}$	$\frac{3.7}{50}$	$\frac{3.7}{75}$

SPIKE IN PP STA. 126 +10 LT. 33"



TOPOGRAPHY

LABORE RD.

STA. 118 TO 127

LT

E

RT

+50

120+00

$$\frac{RD}{12}$$

$$\frac{RD}{13}$$

+85 BIRD HSE
ON POLE 84

+60 5" ASH
86

+60 7" ASH
39

+60 5" ASH
62

+50

+40 3-6" ASH
39-62-83

+20 TP
28

+19 5" ASH
39

+16 PP
29

+11 SECOR
HSE 69

$$\frac{RD}{12}$$

$$\frac{RD}{13}$$

119+00

+99 6" MTN
ASH 39

+79 8" MTN
ASH 39

+79 SECOR
HSE 67

+60 SECOR
2. PATIO 68

+60 5" ASH
61

+57 6" ASH
39

+55 2" GAL
DRAIN
PIPE 20

+50

+39 SECOR
GAR. 93

+38 6" ASH
39

+35 6" ASH
61

+45 & 15'
GR. ENT

+33 2" GAL.
DRAIN
PIPE 20

+12 6" ASH
61

+12 5" ASH
39

$$\frac{RD}{12}$$

$$\frac{RD}{13}$$

118+00

8-20-75
CLOUDY

LT.

RT

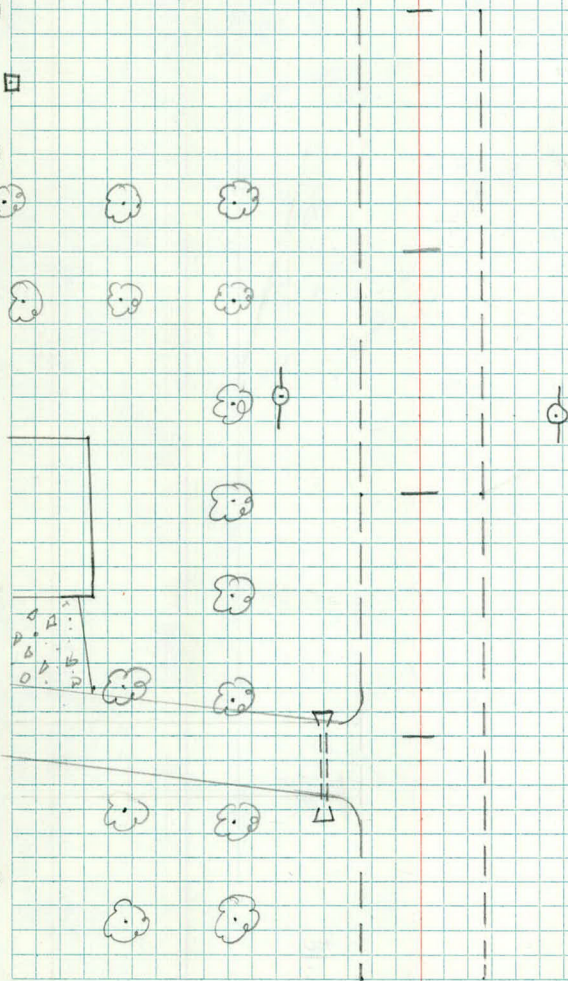
RT

WS
GA
ML

61

SEE TOPOGRAPHY

CO. RD. E PAGE 28



LT.

♀

RT

3 ROWS
+00 PINES

123+00

 $\frac{RD}{12}$ $\frac{RD}{12}$

34-43-53

+99

 $\frac{PP}{28}$ +99 BARB WIRE 1 STR.
ATT TO PP.+93 7" ELM
27+81 TP
27

+50

+00 ROW PINES

3-1-47-58

122+00

 $\frac{RD}{12}$ $\frac{RD}{12}$ +00 BE. 2 STR.
BARB WIRE 31
FE.

+50

121+00

120+50

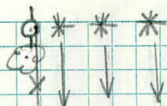
8-20-75
CLOUDY 69°
RAIN

LT

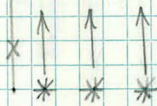
E

RT

WS
GR
ML 62



3 ROWS PINE
VARY 1" TO 4"



SEE TOPOGRAPHY
CO. RD. E PAGE 28

LT

Q

RT

+50 $\frac{2" \text{ASH}}{47}$

125+00

+00 $\frac{2" \text{OAK}}{37}$

$\frac{RD}{12}$

$\frac{RD}{12}$

+00 $\frac{2 \text{ STR. BARB}}{29} \text{ FE.}$

+83 $\frac{18" \text{ELM}}{57}$

+00 $\frac{\text{PINES}}{33-45-54}$

+64 $\frac{2" \text{OAK}}{28}$

+50

+15 $\frac{TP}{28}$

+08 $\frac{3" \text{ELM}}{29}$

124+00

$\frac{RD}{12}$

$\frac{RD}{12}$

+00 $\frac{2 \text{ STR. FE.}}{29} \text{ BARB}$

+00 $\frac{\text{PINES}}{35-44-54}$

+50

123+00

$\frac{RD}{12}$

$\frac{RD}{12}$

+00 $\frac{\text{PINES}}{34-43-53}$

8-20-75
CLOUDY 69°
RAIN

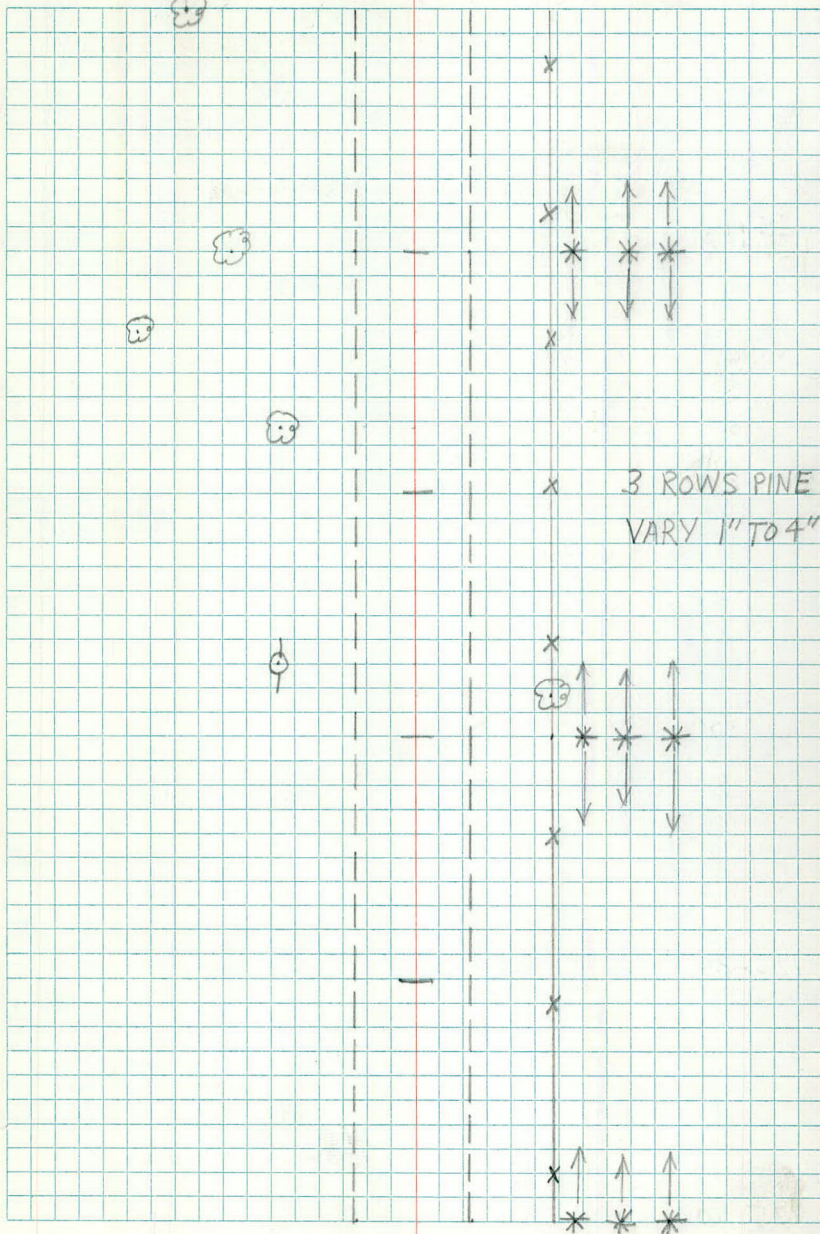
LT

2

RT

WS
GA
ML

63



LT,

¢

RT,

127+00

 $\frac{RD}{12}$ $\frac{RD}{12}$ $+00 \frac{FE.}{28}$ $+00 \frac{PINES}{35-44-55}$ $+87 \frac{24" OAK}{57}$ $+81 \frac{TP}{28}$

+50

126+00

 $\frac{RD}{12}$ $\frac{RD}{12}$ $+00 \frac{2 STR BARB FE.}{29}$ $+99 \frac{18" OAK}{63}$ $+90 \frac{E. 1" OAKS}{40}$ $+99 \frac{2" OAK}{35}$ $+94 \frac{PP}{27}$ $+00 \frac{PINES}{35-45-56}$ $+99 \frac{10 \text{ E. } 1" OAKS}{41}$ $+53 \frac{TP}{28}$ $+50 \frac{2" ASH}{27}$

125+50

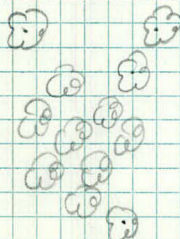
8-20-75
CLOUDY 69°
RAIN

LT

Q

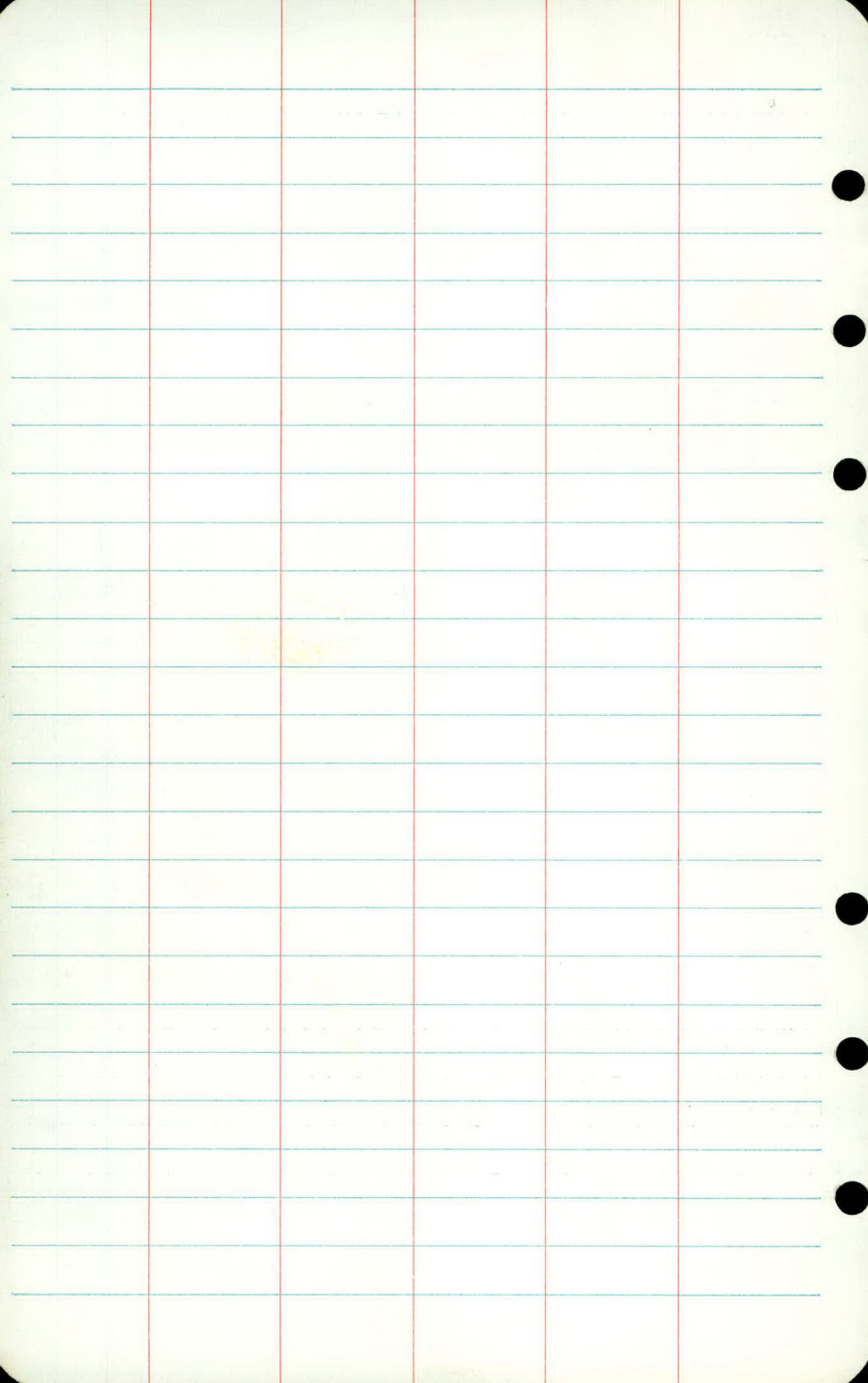
RT

WS
GA
ML 69



3 ROWS PINE
VARY 1" TO 4"





X-SECTIONS

LABORE RD

STA. 118 TO 127

STA	+	π	-	ELEV.
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BM	0.24	937.86		937.62
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118+00

118+34

118+45 E ENT LT

118+70

8-20-75
SUNNY

LT

Q

RT

WS
GA
ML

SPIKE IN ARC POLE NE COR. LABORE RD

26.9	27.9	27.9	27.4	28.3	28.8	29.0	28.1	27.7	29.3	28.4	28.3	27.3
$\frac{11.0}{75}$	$\frac{10.0}{48}$	$\frac{10.0}{29}$	$\frac{10.5}{20}$	$\frac{9.6}{79}$	$\frac{9.1}{12}$	$\frac{8.9}{12}$	$\frac{9.2}{13}$	$\frac{10.2}{22}$	$\frac{8.6}{35}$	$\frac{9.5}{44}$	$\frac{5.6}{53}$	$\frac{5.6}{75}$

27.1	28.1	28.6	28.37 INV	29.3	29.6	29.3	28.2	27.6	27.1
$\frac{10.8}{75}$	$\frac{9.8}{51}$	$\frac{9.3}{35}$	$\frac{9.49}{21}$	$\frac{8.6}{12}$	$\frac{8.3}{12}$	$\frac{8.6}{13}$	$\frac{9.7}{22}$	$\frac{6.3}{40}$	$\frac{5.8}{75}$

29.9	29.7	29.5	29.3	29.5	29.8	29.5	28.4	27.3	27.4	27.0
$\frac{8.0}{75}$	$\frac{8.2}{51}$	$\frac{8.4}{36}$	$\frac{8.6}{22}$	$\frac{8.4}{12}$	$\frac{8.1}{12}$	$\frac{8.4}{12}$	$\frac{9.5}{24}$	$\frac{6.6}{37}$	$\frac{6.3}{53}$	$\frac{6.9}{75}$

29.3	29.1	29.2	29.6	29.0	29.3	29.0	28.8	27.2	27.2	27.4
$\frac{7.6}{67}$	$\frac{7.8}{52}$	$\frac{7.7}{37}$	$\frac{8.3}{18}$	$\frac{7.9}{12}$	$\frac{7.6}{12}$	$\frac{7.9}{12}$	$\frac{9.1}{22}$	$\frac{6.7}{37}$	$\frac{6.7}{53}$	$\frac{6.5}{75}$

STA + π - Elev

937.86

119+00

+27

+35

+62

8-20-75

LT

E

RT

CA
W.S
M.L

30.4	30.5	30.4	30.3	30.7	31.0	30.5	30.5	29.9	30.2	31.5
$\frac{7.5}{69}$	$\frac{7.4}{47}$	$\frac{7.5}{35}$	$\frac{7.6}{20}$	$\frac{7.2}{12}$	6.9	$\frac{7.4}{12}$	$\frac{8.4}{25}$	$\frac{8.0}{40}$	$\frac{7.7}{60}$	$\frac{6.4}{75}$

30.5	30.5	30.3	31.1	31.4	31.6	31.2	30.3	31.3	31.9	32.7
$\frac{7.4}{75}$	$\frac{7.4}{45}$	$\frac{7.6}{21}$	$\frac{6.8}{17}$	$\frac{6.5}{12}$	6.3	$\frac{6.7}{12}$	$\frac{7.6}{25}$	$\frac{6.6}{36}$	$\frac{6.0}{57}$	$\frac{5.2}{75}$

30.1	30.3	30.3	31.3	31.6	31.7	31.3	30.5	31.4	31.9	32.0
$\frac{7.8}{75}$	$\frac{8.6}{45}$	$\frac{7.6}{21}$	$\frac{6.6}{17}$	$\frac{6.3}{12}$	6.2	$\frac{6.6}{12}$	$\frac{7.4}{25}$	$\frac{6.5}{35}$	$\frac{6.0}{53}$	$\frac{4.9}{75}$

29.8	30.0	29.0	31.5	32.1	32.4	32.1	31.1	32.0	32.2	32.5
$\frac{8.1}{75}$	$\frac{8.9}{50}$	$\frac{8.9}{27}$	$\frac{6.4}{18}$	$\frac{5.8}{12}$	5.5	$\frac{5.8}{12}$	$\frac{6.8}{23}$	$\frac{5.9}{35}$	$\frac{4.7}{54}$	$\frac{4.4}{75}$

Sta

+

A

-

ELEV

937.86

120+00

+25

TOP OF MANHOLE WEST EDGE

4.66

933.20

+50

TP

4.19

933.67

8-20-75

LT

E

RT

M.L
G.A
W.S

28.2	28.0	27.8	27.1	27.4	27.9	27.3	27.0	27.3	27.5	27.3	27.1
<u>9.7</u>	<u>9.9</u>	<u>10.1</u>	<u>7.8</u>	<u>5.5</u>	<u>5.0</u>	<u>4.6</u>	<u>4.9</u>	<u>5.6</u>	<u>4.4</u>	<u>3.6</u>	<u>2.8</u>
75	60	40	25	17	12		12	20	34	59	75

28.2	28.5	27.2	27.3	27.8	27.0	27.5	27.1	27.0	27.8	27.3	27.6
<u>9.7</u>	<u>9.4</u>	<u>6.7</u>	<u>6.6</u>	<u>5.1</u>	<u>3.9</u>	<u>3.4</u>	<u>3.8</u>	<u>4.3</u>	<u>3.1</u>	<u>2.6</u>	<u>1.3</u>
75	65	50	34	23	12		12	22	33	49	75

PK

STA

47+00

COUNTY

RD E

STA	+	π	-	ELEV
B.M.	4.02	941.64		937.62
B.M			1.86	939.78
BM				(937.62)
BM	3.85	943.63		939.78
122+00				
✓				
122+50				

LT

C

RT

8-20-75
9-25-75
CLEAR: 64°

SPIKE IN ARC POLE N.E COR LABORE RD

124+15 SPIKE IN P. PLT 24.0'

~~SPIKE IN ARC POLE N.E COR LABORE RD~~

SPIKE IN P.P. STA 124+15 LT. 24.0'

33.1	34.7	36.9	37.7	38.0	37.9	37.3	36.5	38.9	38.2
10.5	8.9	6.7	5.9	5.6	5.7	6.3	7.1	4.7	5.4
75	50	20	12		12	17	21	30	50

37.6
6.0
75

34.5	35.1	37.0	38.4	38.7	38.6	37.4	37.6	37.7
9.1	8.5	6.6	5.2	4.9	5.0	6.2	6.0	5.9
75	50	25	12		12	21	34	75

STA + π - ELEV

943.63

123+00

+50

124+00

+50

125+00

+50

W.S
G.A
R.T

LT

£

RT

4-25-75
CLEAR: 65°

34.6	34.8	36.5	38.0	38.9	39.1	39.0	37.9	38.3	38.2
9.0	8.8	7.1	5.6	4.7	4.5	4.6	5.7	5.3	5.4
75	50	23	19	12		12	24	43	75

35.0	35.3	37.3	38.6	39.3	39.5	39.4	38.4	38.8	38.3
8.6	8.3	6.3	5.0	4.3	4.1	4.2	5.2	4.8	5.3
75	47	23	18	12		12	22	41	75

34.4	36.0	38.5	39.6	39.9	39.8	38.7	41.4	42.1	41.6
9.2	7.6	5.1	4.0	3.7	3.8	4.9	2.2	1.5	2.0
75	47	21	12		12	23	33	54	75

34.7	37.9	38.6	39.9	40.2	40.0	38.8	42.1	43.6	42.9
8.9	5.7	5.0	3.7	3.4	3.6	4.8	1.5	0.0	0.7
75	35	21	12		12	24	31	50	75

33.9	38.7	39.7	38.4	40.0	40.2	40.1	38.9	40.8	40.9	40.8
9.7	4.9	3.9	5.2	3.6	3.4	3.5	4.7	2.8	2.7	2.8
75	44	28	21	12		12	23	29	50	75

33.9	36.1	38.5	39.3	40.0	40.3	40.1	39.6	39.1	39.3	39.1
9.7	7.5	5.1	4.3	3.6	3.3	3.5	4.0	4.5	4.3	4.1
75	50	34	19	12		12	20	34	51	75

STA + K - ELEV

943.63

126+00

+50

TP 2.35 941.46 4.52 939.11

BM 3.86 937.60 (937.62)

WLS
C.A.
R.J.

LT

E

RT

9-25-75
CLAM 64°

40.3

3.3

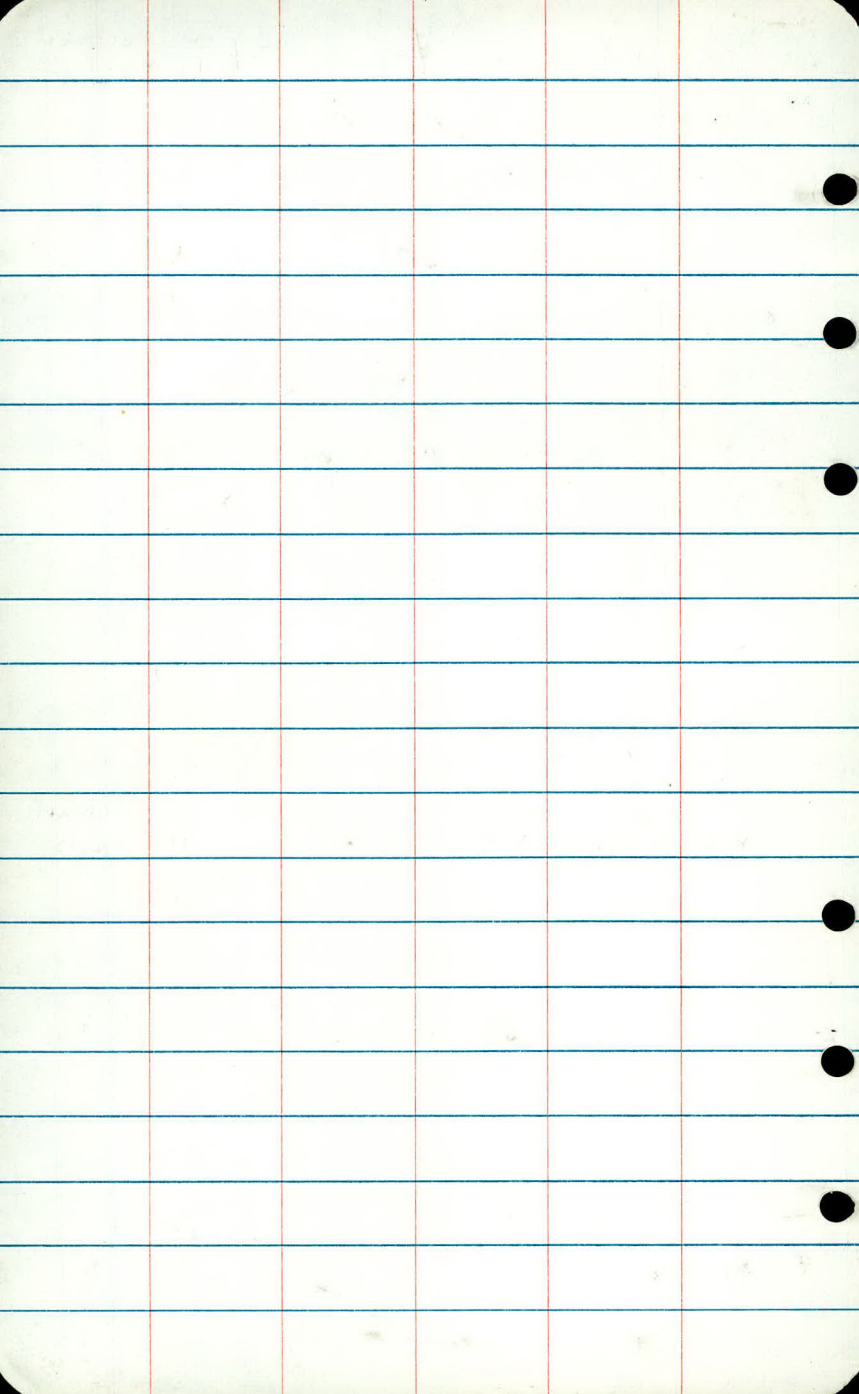
40.4

3.2

PK STA 123+00

SPIKE IN ARCH LIGHT POLE N.E. CORN

LABORE RE



GA
LPD
DS
RJ

12-31-75
cloudy 26°

Co. Rd "E"

X- Sections

at Culvert 66+62

Sta	+	K	-	Elev
-----	---	---	---	------

BM	3.32	957.75		954.43
----	------	--------	--	--------

66+62		CROSS	CULVERT	
-------	--	-------	---------	--

BM		3.91	953.84	953.77
----	--	------	--------	--------

GA
LPO
AS
RJ

LT

£

X7

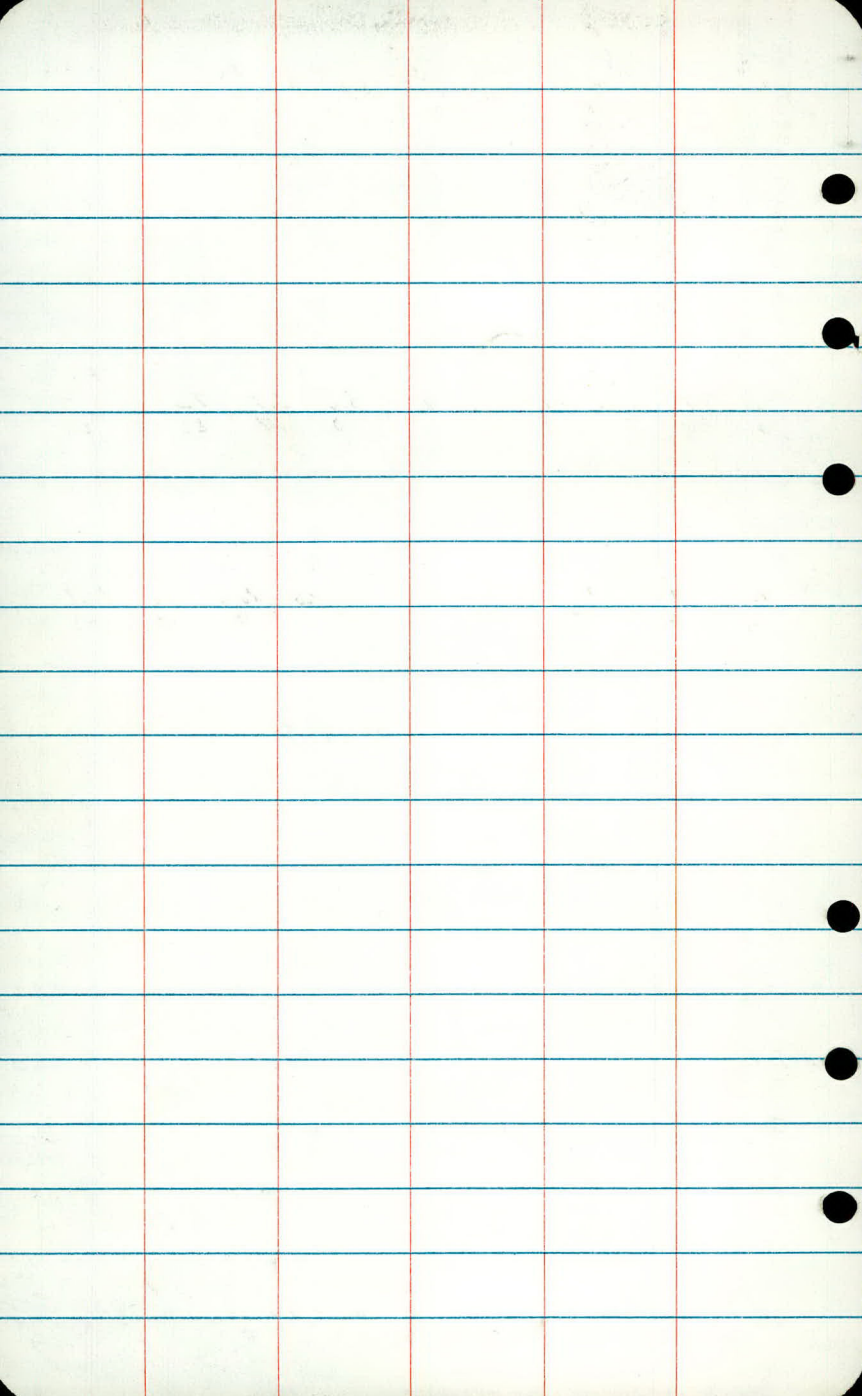
12-31-75
C/ody 26°

SPIKE IN PP SE COR ENGLISH: CO Rd E

49.6	48.8	47.74	52.6	53.2	53.15	52.75	952.0	50.6	48.18
P.2	8.9	FL	5.1	4.6	4.6	5.0	5.7	7.2	FL
33	28	22	18	10		10	17	23	9.57 + 21"
									29

50.4	50.9	50.4		48.2	47.2	47.2	47.0
7.3	7.3	7.3		9.5	10.6	10.6	10.7
38	52	75		100	83	68	43

PK NAIL £ Sta 68+00



Jan. 16, 1976

LT

2

RT

4

Phillips 66
Sta.

18" RCP



*

*

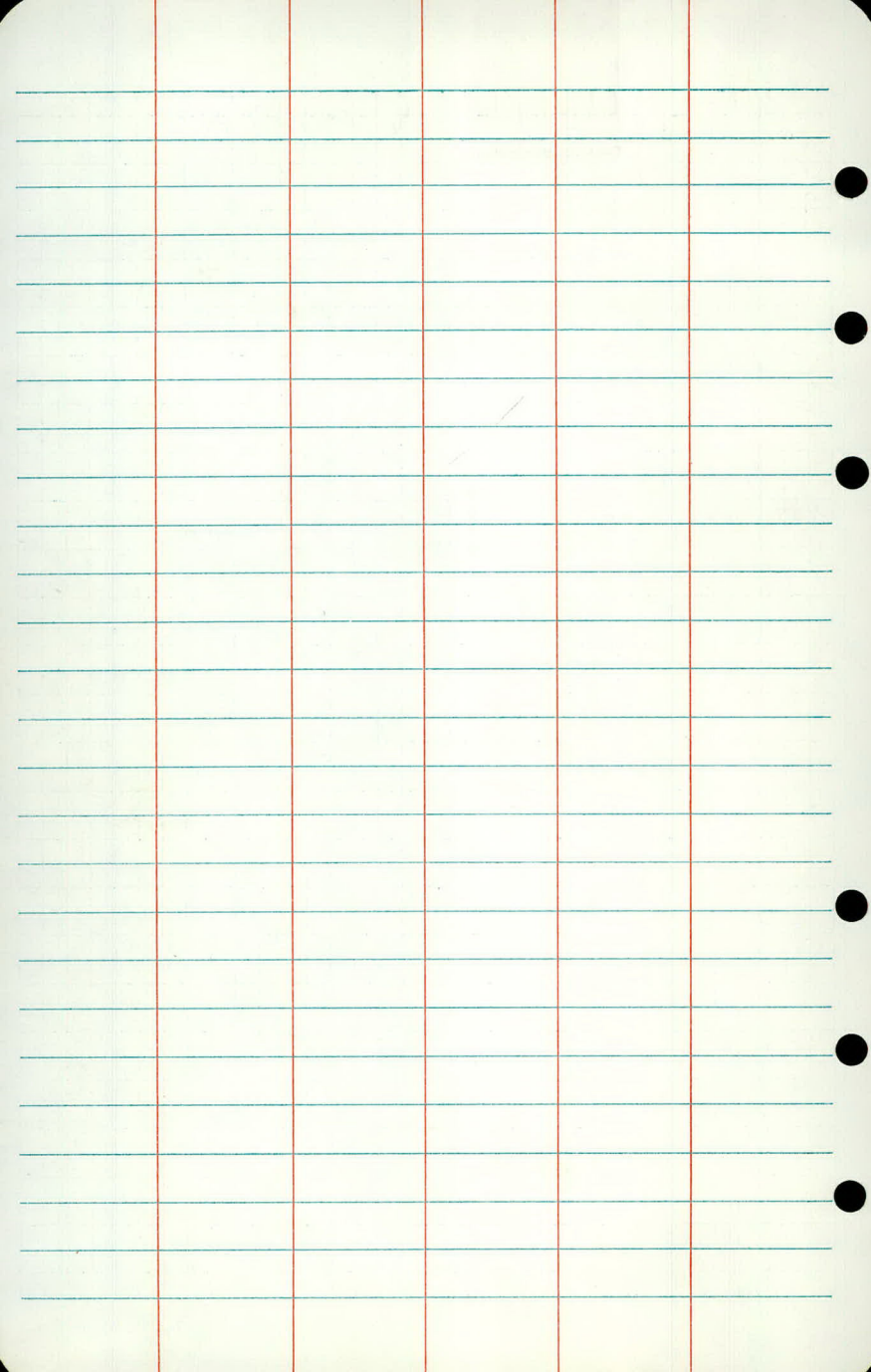
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*

SAN MH

7" Cast,
4 Rings
15' deep





GA
LPS
DS
RJ

12-31-75
cloudy 38°
1A

62-615-04

TOPOGRAPHY FOR

CULVERTS ON ENGLISH ST

2 pages

LT

¢

RT

64+00

 $+66 \quad \frac{15'' \text{ SCP}}{224}$ $+47.5 \quad \frac{CB}{224}$ $+30 \text{ ¢} \quad \text{ENGLISH ST}$ $+12.5 \quad \frac{CB}{224}$

63+00

+02

 $\frac{24'' \text{ SCP}}{224}$

GA
DS
LPD
RT

12-31-75

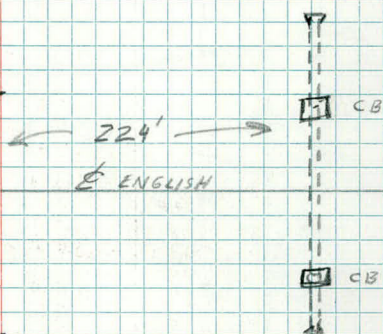
2A

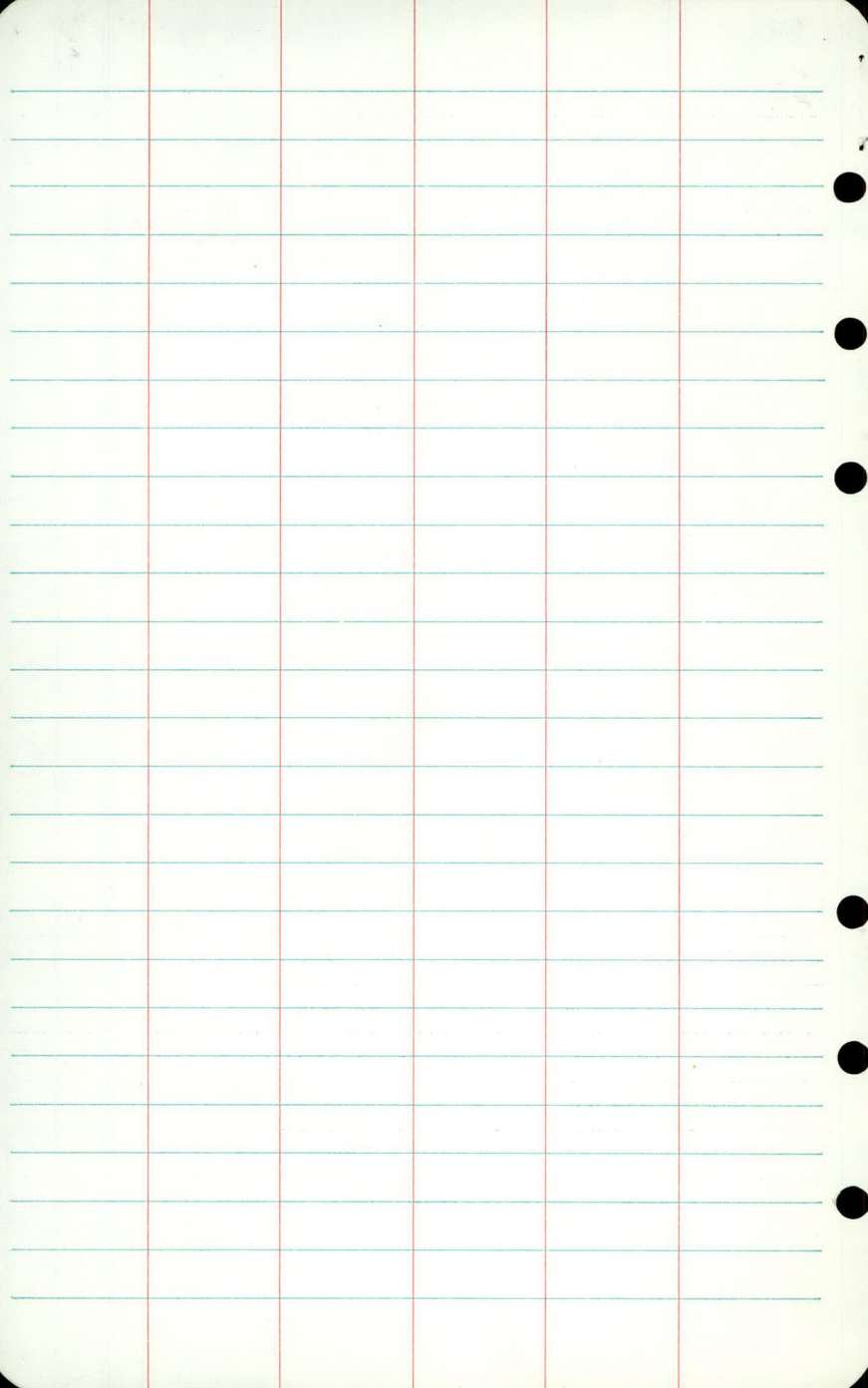
LT

Φ

RT

Φ CO. RD "E"





GA
DS
LPD
RS:

12-31-75
cloudy 28°
1B

62-615-04

Elevations

x-culvert

on English st

2 pages

STA	+	π	-	ELEV
BM	2.57	957.02		954.45

			10.47	46.55
--	--	--	-------	-------

			10.48	46.54
--	--	--	-------	-------

TP	4.64	957.16	4.50	952.52
----	------	--------	------	--------

BM			2.71	954.45	954.45
----	--	--	------	--------	--------

GA
DS
LPO
RJ

LT

~~LT~~

RT

12-31-75

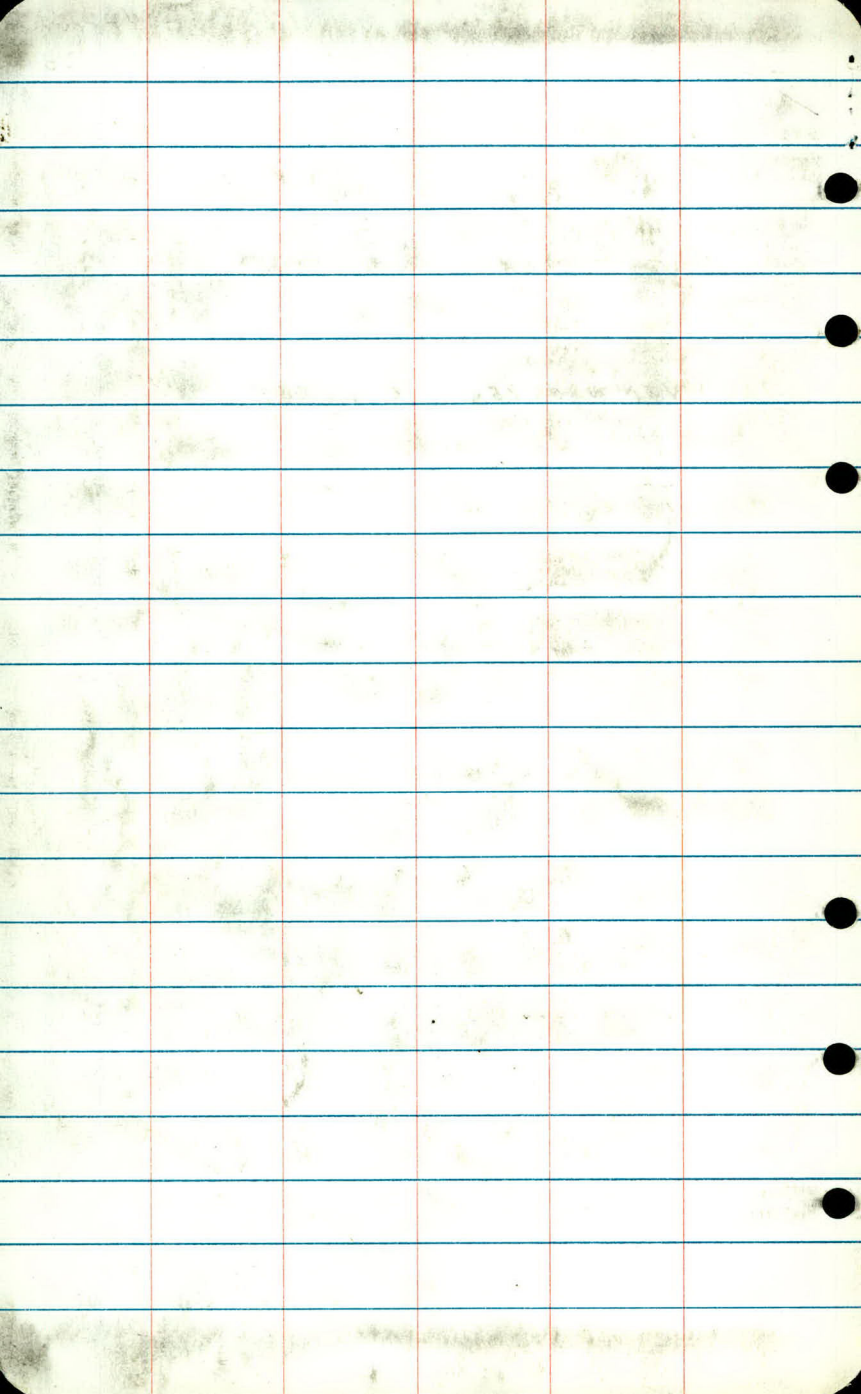
2B

SPIKE IN PP SE COR ENGLISH : CO RD "E"

INVERT EAST CULVERT

INVERT WEST CULVERT

SPIKE IN PP SE COR ENGLISH : CO RD E



Additional X-Sections

Co Rd "E" from CENTERVILLE RD
to Hwy #61.

EXTRA Common Excavation
for Project 62-615-04

4 PAGES

Sta.

B.M.

934.82

45+50
~~46+00~~

46+00

46+50

47+00

Exist. inc
119+27

119+35

Q

Rt

2

Top Hyd S.W. LABORE & Co Rd E

T.C.		Existing
29.5	29.3	29.8
26	34	45

T.C.		Existing
30.6	30.5	29.8
26	35	49
		66

T.C.				Existing
31.7	31.7	31.1	30.6	30.3
26	35	50	75	100
				125
				145

T.C.				T.C.
32.6	32.7	32.6	32.7	32.5
44	55	70	80	100

Lt

Q

T.C.		Exist
31.1	30.3	30.5
20	46	50
		85

T.C.		Existing
31.9	30.4	30.0
23	50	95

5th

119+62

B.M.

925.56

15+79

16+00

16+27

16+39

16+53

LT

E

3

T.C.
32.1
23

30.6
50

Existing
30.0
98

S. E. Cor East LEDGE Ho # 885

±

22.2

19.9

T.C.
19.5 E

45

32

26

22.6

19.6

T.C.

19.5

50

31

26

23.1

19.9

T.C.

19.6

62

31

26

Ent

Bit
23.2
69

Bit
21.7
45

20.0
32

T.C.
19.4
26

5th

16+69

16+81

17+00

17+50

17+75

17+93

Existing			
Bit	Bit	T.C.	
32.6	22.3	20.5	19.9
67	45	32	26

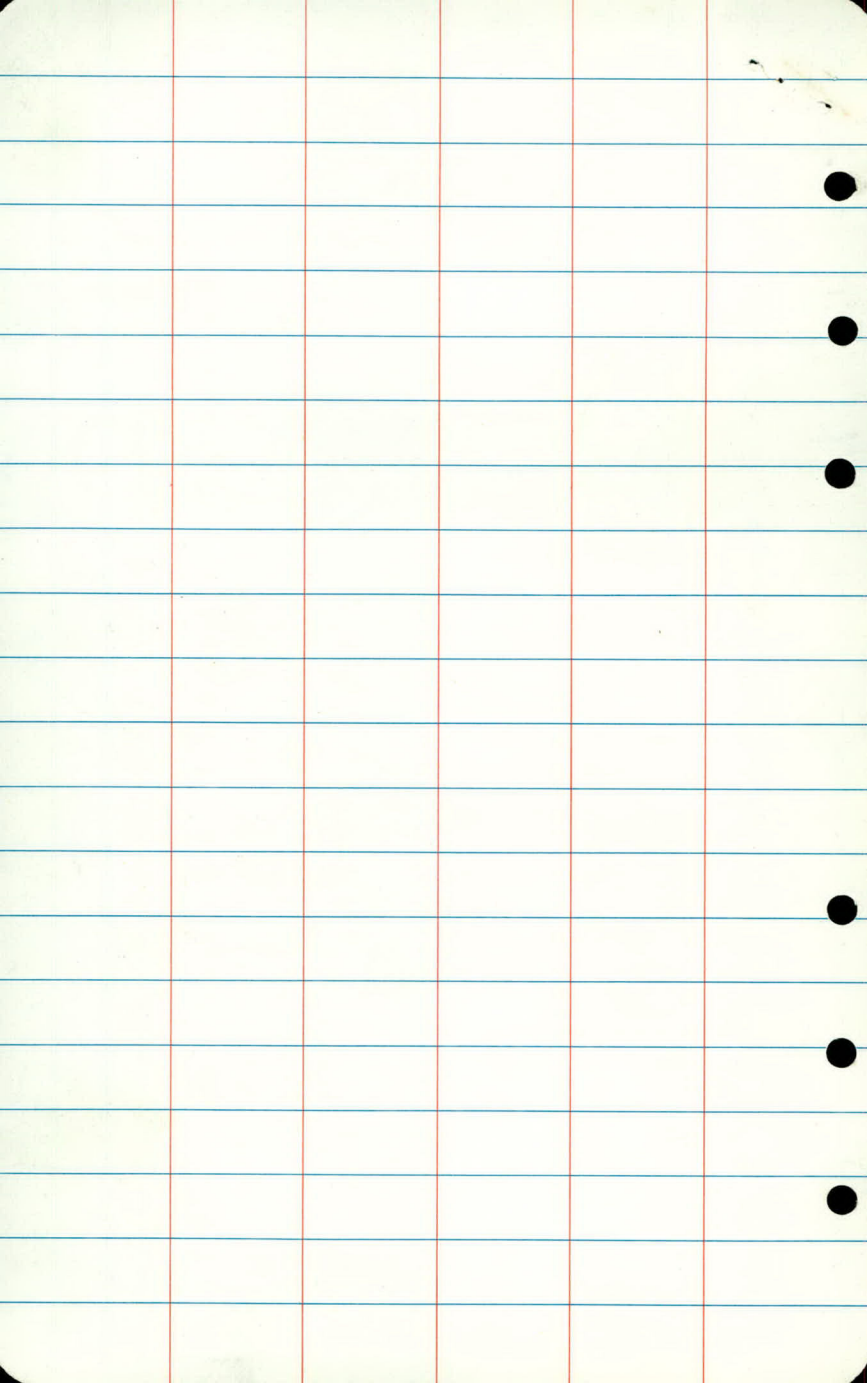
		T.C.
22.1	20.4	19.9
45	32	26

	T.C.
21.0	20.1
45	26

	T.C.
22.6	20.3
44	26

		T.C.
22.6	22.6	20.4
100	45	26

En t.



As built Manholes

Co Rd E from CENTERVILLE Rd

to Hwy #61

LENER

TOP

CASTING

ELEV

B.M.

922.90

MH 50

922.34

MH 51

921.17

MH 54

922.01

MH 56

922.69

APPROX =

920.02

B.M.

923.39

923.36

MH 57

922.45

SD 58 =

920.91

F

MH 59

920.37

MH 62

918.14

MH 65

919.55

MH 68

921.00

MH 71

922.39

T.P.

923.20

B.M.

923.78

923.80

Description

11-1-78

CLR 40-60'

N.E. Core Tower Step H[#] 790 Co. Rd E

Top to F.L. 13.00'

Top to F.L. (5.13 no.) (10.91 W.) (10.91 E.) (4.74 so.)

" " (5.84 no.) (11.19 East & West)

" " (5.16 no.) (10.72 East & West)

N.E. Core R.R. Signal Base Sta 6+95 Rt.

F.L. to Top S.D 3.78'

F.L. to Top (6.35 no.) (11.00 East & West)

" " (4.92 no.) (4.90 so.) (8.04 E & W)

" " (4.78 no, so, E, & W.)

" " (4.90 no) (4.80 so.) (5.22 E & W)

" " (5.86 no) (5.10 so) (5.46 E & W)

" " (4.94 no) (4.92 so.) (5.76 W)

P.K. Nail 22+00

Spike PP Sta 23+80 Rt

LENKER Rd TOP Casting ELEV

B.m. 920.40

MH 76 921.15

MH 79 Apron 904.07

MH 83 917.98

T.P. 921.63

MH 86 919.29

MH 89 921.63

B.m. 923.88

MH 92 930.17

MH 95 935.79

B.m. 934.82 934.82

MH 98 944.94 T.P. PK 942.22

MH 101 953.88

B.m. 948.62 948.64

MH 104 954.32

MH 107 952.36

B.m. 956.32 956.36

MH 110 954.40

B.m. 954.39

T.P. 954.40

Spike PP 36+75 Lt 46'

F.L. to Top (5.10 no) (5.20 so) (7.06 East)

" " (4.80 no) (4.84 so) (5.12 East)

" " (4.80 no.) (4.64 so) (5.84 E & W)

MH 89

F.L. to Top (4.85 no) (4.70 so.) (5.42 E & W)

" " (5.88 E) (6.40 W) (4.70 so) (4.80 n)

Top Hyd 42+10 Rt

F.L. to Top (4.92 no) (4.94 so) (6.12 E & W)

" " (5.02 no) (4.92 so.) (6.22 E & W)

Top Hyd LA BORE E E

F.L. to top (4.92 no) (5.08 so) (5.85 E & W)

" " (4.70 no) (4.74 so) (4.64 E & W)

N.E. Core From + Step Ho⁴ 1230

F.L. to top (4.79 no) (4.72 so) (5.50 E & W)

" " (5.19 no) (5.13 so) (5.12 E & W)

R/R Spike PP N.E. Core E & Big Fox

F.L. to top (4.88 no) (4.94 so) (5.40 E & W)

Spike PP S.E. Core English

MH 110

LEAKER

TP

954.40

MH 113

957.01

MH 116

960.93

B.M.

958.10

958.10

Top M.H. 110

F.L. to top (5.01 no) (5.32 so) (6.17 E & W)

F.L. to top (5.51 no) (5.46 so) (5.96 E & W)

N.W. Cor Bot Step Ho[#] 1400

