

OFFICE OF COUNTY ENGINEER
RAMSEY COUNTY, MINN.

PLAN

Survey

McKNIGHT RD

From 11th AVE To BEAM AVE

Road Acc't. No. 68

Date Filed 4-7-81

File _____

W.S
K.G
E.Y

9-7-76
CLEAR 195°

13

BENCA LEVELS

Mc KNIGHT RD

HWY 36 TO CO. RD "C"

STA	+	Σ	-	ELEV	
Bm	3.67	943.66			939.99
Bm	0.64	941.51	2.79	940.87	
Bm	7.76	945.93	3.34	938.17	
T.P	10.20	954.22	1.91	944.02	
Bm	7.23	960.11	1.34	952.88	
T.P	8.39	966.33	2.17	957.94	
Bm	3.42	969.71	0.04	966.29	966.40
Bm	3.16	969.59	3.28	966.43	
Bm	3.12	968.96	3.75	965.84	
Bm	2.64	969.04	2.56	966.40	966.40
Bm	3.78	969.62	3.20	965.84	
Bm	3.09	969.52	3.19	966.43	
Bm	0.11	966.40	3.23	966.29	
T.P	1.91	959.87	8.44	957.96	
Bm	0.22	953.11	6.98	952.89	
T.P	0.97	944.99	9.09	944.02	
Bm	2.22	940.38	6.83	938.16	
TP	5.16	941.48	4.06	936.32	
Bm	2.47	943.34	0.61	940.87	

W.S
K.V.
P.4

9-8-76 7-7-76

Clear: windy
93°

14

DESCRIPTION

TOP HYD NE CORNER 11th AVE : MCKNIGHT

TOP HYD NE CORNER 12th AVE : MCKNIGHT

TOP HYD NE CORNER 13th AVE : MCKNIGHT

TOP P.K STA. 47+00

TOP HYD NE CORNER 14th AVE : MCKNIGHT

TOP P.K STA 50+00

TOP HYD NE CORNER 15th AVE : MCKNIGHT

TOP HYD NE CORNER 16th AVE : MCKNIGHT

TOP CONC. NW CORNER GARAGE APRON

TOP HYD ON COR'D "C" EAST OF MCKNIGHT HO # 2295

TOP CONC NW CORNER GARAGE APRON

TOP HYD NE CORNER 16th AVE : MCKNIGHT

TOP HYD NE CORNER 15th AVE : MCKNIGHT

TOP P.K STA. 50+00

TOP HYD NE CORNER 14th AVE : MCKNIGHT

TOP P.K STA. 47+00

TOP HYD N.E CORNER 13th AVE : MCKNIGHT

TOP P.K STA 43+00

TOP HYD NE CORNER 12th AVE : MCKNIGHT

[illegible]

WS
K.L.
E.V.

9-8-76
cloudy: 72°

15

TOP HYD NE CORNER 11TH AVE : MCKNIGHT

TOP HYD NE CORNER 11TH AVE : MCKNIGHT

TOP SPIKE IN ARCHLIGHT POLE STA. 36+35 RT. 30

TOP SPIKE IN ARCHLIGHT POLE STA. 33+92 RT. 30

TOP SPIKE IN POWER POLE (GUIDE) STA 34+85 RT. 30

TOP SPIKE IN ARCHLIGHT POLE STA 33+92 RT. 30

TOP SPIKE IN ARCHLIGHT POLE STA 36+35 RT. 30

TOP HYD NE CORNER 11TH AVE : MCKNIGHT

STA	+	π	-	ELEV.
BM	5.48	939.88		934.40
30+00				
✓				
+50				
✓				
T.P.	4.43	939.22	5.09	934.79
31+00				
✓				

W.S
K.6
E.M

LT

Q

RT 4-9-16
CLEAR 72°
16

SPIKE IN P.P. 31+85 RT. 31'

33.1	34.1	34.1	35.0	35.1	35.6	35.2	35.0	31.5	31.7	34.4
6.8	5.8	5.8	4.9	4.8	4.3	4.7	4.9	8.4	8.2	5.5
100	67	52	32	24		23	28	36	47	55

32.6	32.8	35.3
7.3	7.1	4.6
86	72	66

32.6	33.5	33.9	34.5	34.7	35.1	34.7	33.7	33.7	31.8	34.9
7.3	6.4	6.0	5.4	5.2	4.8	5.2	6.2	6.2	8.1	5.0
100	63	31	32	24		23	32	27	49	58

32.5	33.0	34.8
7.4	6.9	5.1
80	70	66

PK STA 31+00

32.2	32.3	33.0	34.2	34.4	34.8	34.2	33.8	32.2	32.1	32.4
7.0	6.9	6.2	5.0	4.8	4.4	5.0	5.4	7.0	7.1	2.8
100	75	45	32	24		23	31	38	48	56

32.2	32.3	32.5
7.0	6.9	2.7
85	76	65

STA.	+	π	-	ELEV.
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		939.22		
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31+50

T. P.	4.24	938.48	4.98	934.24
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32+00

✓

Bm	4.05	938.15	4.37	934.11	934.10
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+50

WS
KG
EX.

LT.

E

RH

9-9-76
CLR. 730

17

32.1	32.6	34.0	34.5	34.0	32.8	32.0	32.6	33.6
21	66	5.2	4.7	5.2	54	7.2	6.6	5.6
100	50	32		24	29	36	45	62
							32.4	33.6
							6.8	5.6
							78	73

P.K. STA. 32100

31.6	32.5	33.5	33.7	34.3	33.8	33.2	32.0	32.2
6.9	6.0	5.0	4.8	4.2	4.7	5.3	6.5	6.3
109	46	34	24		24	32	35	46
					32.0	32.2	35.0	33.6
					6.5	6.3	3.5	4.9
					85	69	61	50

SPIKE IV PP 33+92 RT 30'

31.8	32.6	33.2	33.2	33.6	34.1	33.6	33.5	31.9	31.9	34.4
6.4	5.6	5.0	4.9	4.6	4.1	4.6	4.7	6.3	6.3	3.8
100	49	44	39	24		24	28	34	46	63
								30.9	31.6	33.6
								7.3	6.6	4.6
								80	73	67

STA	+	π	-	ELEV
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		938.15		
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33+00				
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T.P.	5.44	939.24	4.35	933.80
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+50				
-----	--	--	--	--

✓				
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+64				
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			8.75	
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34+00				
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T.P.	4.31	938.41	5.16	934.08	934.10
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WS
KG
EX.

Lt.

Lt.

Rt.

9-9-76
CLR 68°
18

31.4	31.9	33.0	33.4	33.8	33.3	32.9	31.6	31.7
4.8	6.3	5.2	4.8	4.4	4.9	5.3	6.6	6.5
121	55	42	24		24	32	36	47

35.3	29.3	29.2	30.9	33.2	32.4
29.89	9.0	7.3	5.0	5.8	
92.82	72	66	61	51	

P.K. STA. 33+00

30.9	33.1	33.4	33.4	33.9	33.9	33.4	33.8	33.3	33.1	31.6	31.3	32.0
8.3	6.1	5.8	5.8	5.3	5.3	5.8	5.4	5.9	6.1	7.6	7.9	7.2
100	75	66	36	36	24	24		24	31	36	48	54
			TOC	TOC								

34.8	29.8	28.8	28.1	30.8
4.4	9.4	10.4	10.6	8.4
85	68	67	60	57

F.L. SOUTH END 36" CMP

34.7	35.3	34.7	34.2	33.5	33.6	34.0	33.6	33.4	31.3	30.4	28.5
4.5	3.9	4.5	5.0	5.7	5.6	5.2	5.6	5.8	7.9	8.8	10.7
75	75	60	60	31	24		24	31	38	48	52
Gutter	TOC	T.O.C.									

34.5	30.6	28.8
4.7	8.6	10.4
82	65	62

SPIKE IN P.P. STA. 33+92

STA.	+	π	-	ELEV
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		938.41		
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34+37				
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			7.79	
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34+50				
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35+00				
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T.P.	5.09	939.70	3.80	934.61
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35+50				
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WS
KG
R.J
EV

LI

L

RT

9-13-76
C164 60°
19

N. END 36" CMP

30.4	31.4	32.9	33.7	34.0	34.3	33.9	33.5	30.8	30.3	28.4
8.0	70	55	4.7	4.4	4.1	4.5	4.9	7.6	8.1	10.0
92	89	60	38	22		24	30	40	45	46
							34.4	31.4	29.8	29.1
							4.0	7.0	8.6	9.3
							79	69	59	62

31.8	32.4	33.5	34.0	34.2	34.6	34.2	33.9	31.3	30.5	28.2
6.6	60	49	44	4.2	3.8	4.2	4.5	7.1	7.9	10.2
75	52	41	32	22		24	31	36	41	45
								32.9	31.4	28.9
								5.5	7.0	8.5
								75	66	63

P.K. @ STA 35+00

31.9	32.2	34.3	34.6	34.7	35.1	34.6	34.6	31.0	30.4	27.8
7.8	7.5	5.4	5.1	5.0	4.6	5.1	5.1	8.7	9.3	11.9
75	53	39	33	21		23	30	37	44	46
			29.7	31.5	33.9	33.7	31.0	29.2	27.6	
			10.0	8.2	5.8	6.0	8.7	10.5	12.1	
			89	85	75	69	61	53	51	

STA.	+	π	-	ELEV.
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		939.70		
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36+00				
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36+30				
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36+41				
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B. M.				
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3.36	936.34	936.37		
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WS
1KG
RT
FY

Lt

R

RT.

1-13-76
Oldy 60°
20

31.4	31.9	34.7	35.1	35.3	35.5	35.0	34.8	31.2	29.9	30.2
8.3	7.8	5.0	4.6	4.4	4.2	4.7	4.9	8.5	7.8	9.5
82	54	40	33	21		23	29	36	42	44

→ 29.6
10.1
86

34.8 26.7 27.2 29.4
4.9 13.0 12.5 10.3
75 54 47 46

31.6	31.7	34.7	35.2	35.5	35.8	35.3	34.4	31.4	27.85
8.1	8.0	5.0	4.5	4.2	3.9	4.4	5.3	8.3	11.85
77	58	41	32	21		23	32	39	46

F.L.
6"x9" Arch
pipe

→ 29.5
10.2
82

35.4 34.4 32.0
4.3 5.3 7.7
75 67 57

29.7	31.5	32.1	35.0	35.4	35.6	35.9	35.4	34.6	35.5	36.7
10.0	8.2	7.6	4.7	4.3	4.1	3.8	4.3	5.1	4.2	2.0
82	77	55	39	32	21		23	34	50	59

37.4
2.3
75

SPIKE IN. P.P. 36+35 RT.

STA.

+

π

LEW KER Rod

-

ELEV

939.99

37+00

37+00

37+35

37+46

37+50

J.A.
D.S.

4. 2

Rt.

9-13-76
Cldy 60°
21TOP Hyd N.E. COR 11th Ave & McKnight

<u>32.6</u>	<u>35.7</u>	<u>35.8</u>	<u>36.1</u>	<u>36.8</u>	<u>36.3</u>	<u>36.0</u>	<u>36.0</u>	<u>36.4</u>
52	40	33	26		22	23	32	43
			Rd		Rd			

<u>36.9</u>	<u>29.5</u>	<u>32.2</u>	<u>36.8</u>		<u>37.3</u>	<u>37.4</u>
67	80	90	105		54	53
					Bt	

<u>31.8</u>	<u>33.3</u>	<u>36.6</u>	<u>37.2</u>	<u>36.7</u>	<u>37.2</u>
69	56	42	26	25	
			conc	Bt	
			curb		

<u>29.3</u>	<u>31.1</u>	<u>37.1</u>
77	90	109

<u>33.2</u>	<u>35.6</u>	<u>37.2</u>	<u>37.4</u>	<u>36.9</u>	<u>37.3</u>
69	56	42	26	25	
			T.C.	conc	
				Gutter	

<u>32.14</u>	<u>29.40</u>	<u>32.5</u>	<u>37.3</u>
77	77	87	100
TOP	F.L.		
26" REP	26" REP		
APRON			

<u>37.4</u>	<u>36.9</u>	<u>37.0</u>	<u>37.7</u>	<u>38.3</u>
	24	43	61	76
	Rd			

T.C.
Bt
Gutter
37.6
76

STA

+

π

-

ELEV

37+55

37+74

GUTTER LT

37+80

GUTTER RT

38+00

MM LT 4 E 11th AVE

+09

37.75 1+

J.A.
D.S

LT

E

SEPT 17, 1916
Sunny 80°
RT 22

37.3 37.6 37.56 37.1 37.5

62

45

27

TOP

CIG

26

37.4

77

37.42 37.07 37.60 37.16 37.6

75

75

50

50

TIC.

GUTTER

TIC.

GUTTER

36.91

37.32

100

100

GUTTER

TIC.

37.6

37.30

37.67

37.70

34

GUTTER

35

T.C.

48

TOP

C.B.

37.52

37.37

36.93

100

GUTTER

75

GUTTER

48

GUTTER

37.4

37.7

37.6

37.87

37.9

37.6

37.8

38.0

100

60

26

4

MH

24

50

100

RT 34' MH

STA

+

π

-

LENKER
ELEV

38+24

GUTTER RT

+26

GUTTER LT

+43

35,07

38+53

39+00

J.A.
D.S.
B.L.
D.W.

Lt

2

Rt

SEP 17, 1976
Sunny 80°

23

38.1 37.40 37.87 37.01 37.71
36 36 47 47
GUTTER T.C. GUTTER T.C.

38.08 37.59 37.90 37.46
100 100 75 75
T.C. GUTTER T.C. GUTTER

37.47 36.97 37.70 37.29 38.2
75 75 47 47
T.C. GUTTER T.C. GUTTER

36.87 37.31
100 100
GUTTER T.C.

FL 12" RCP + APRON Rt 34

36.6 37.9 38.22 37.75 38.3 38.1 38.4 35.9 37.6
59 42 27 26 27 24 33 44
T.C. GUTTER Bit

36.4
75

38.1
75

38.1
57

34.4 35.1 37.9 38.3 38.6 38.3 38.6 36.4 38.2
56 42 27 21 23 25 35 47

34.3
75

39.5
75

LEWKE

STA

+

A

-

ELEV

39+50

40+00

T.P

38.68

40+50

+92

36.82

41+00

B.M.

0.87

940.87

940.87

J.A.
D.S.
B.L.
D.W.

Lt

C

SEP 17, 1976
Sunny 80°
RT 24

35.6	35.9	37.0	38.0	38.4	38.8	38.5	37.0	40.5	41.9
75	54	40	25	20		23	34	38	75

37.1	39.8	38.1	38.2	38.3	38.7	38.4	38.5	36.9	40.4
64	57	42	26	21		23	26	33	41

34.9
67

31.2
75

44.0
75

43.8
53

PK STA 40+00

32.4	39.2	38.0	38.1	38.4	38.1	38.3	36.6	43.2
51	38	26	21		22	24	31	46

31.3
57

38.6
75

44.8
75

44.6
65

Top 12" RCP + APRON

38.1	31.1	37.1	37.7	38.0	37.7	37.2	38.1	38.0	38.4
64	43	31	21		22	34	42	63	75

38.1
75

Top Hyd 12th Ave & McKnight W.E. Cor

Sta

+

T

-

ELEV

LEADER

B.M.

0.87

940.87

41+11

37.89

+17

GUTTER RT

+29

E 12th Ave

+32

37.69

+39

37.50

+39

+46

GUTTER RT

41+50

J.A.
D.S.
B.L.

Lt

L

Rt 9-23-76
Sunny 50°

25

Top Hyd 12th Ave $\frac{1}{2}$ McKnight Rd NE Cor

MH Rt 46'

CB T.C. gutter

<u>37.9</u>	<u>37.6</u>	<u>37.2</u>	<u>38.0</u>	<u>37.4</u>
23		45	45	75

T.C.

37.9

75

MH

37.75
6

37.8

37.6
23

37.6
46

37.8
75

38.2
100

MH Lt 5'

MH Rt 46'

T.C.

37.7

37.5
23

37.1
46

37.6
46

37.4
75

T.C.

37.9

75

B/C

32.8
38

34.1
32

37.1
26

37.2
21
Rd

37.6

37.5
26
Rd

37.9
26

37.8
50

38.0
75

32.2
42

39.0
49

37.6
56

37.4
75

Sta

+

π

-

ELEV

41+60

30.30

42+00

38.18

938.17

+50

+81

Ent Rt

43+00

J/A,
D.S,
B.L

E

SEP + 23, 1976
SUNNY 50

26

F.L. 18" RCP L 41'

<u>32.5</u>	<u>31.5</u>	<u>36.1</u>	<u>36.7</u>	37.2	<u>37.0</u>	<u>37.8</u>	38.41
41	37	33	21 Rd		23	40	57

conc

<u>32.8</u>	<u>37.2</u>	<u>37.2</u>
48	56	75

36.80
32.40
44

Top Hyd 13th Ave & McKnight

<u>31.0</u>	<u>35.4</u>	<u>36.3</u>	<u>36.8</u>	<u>36.5</u>	<u>36.2</u>	<u>37.4</u>
43	36	21		23	37	61

F.E.

<u>30.9</u>	<u>36.2</u>	<u>36.9</u>
45	53	75

36.6	<u>36.2</u>	<u>35.9</u>	<u>36.9</u>	<u>37.4</u>
	23	27	58	75

<u>36.7</u>	<u>30.2</u>	<u>35.4</u>	<u>35.9</u>	<u>36.4</u>	<u>36.1</u>	<u>35.6</u>	<u>36.0</u>	<u>36.4</u>
55	44	35	21		23	29	31	54

35.6
75

37.3
75

Sta

+

π

-

ELEV

38.18

43+50

+93

44+00

+12

E Ditch Lt

+ 39

J.A.
D.S.
B.L

14

L

K+

SEPT 23, 1976

27

29.6 34.3 34.9 35.4 35.8 35.6 35.1 35.3 35.6 36.2
46 38 30 21 23 28 31 53 75

35.6 36.2
54 75

29.5 32.0 34.3 35.0 35.4 35.1 33.8 35.3 35.4
46 40 29 21 23 33 44 75

29.5 36.5 36.3
50 63 75

FL 18" Arch
29.3 30.2 31.65 34.6 35.0 35.3 35.0 32.1 31.2 34.4 35.4
47 35 29 27 21 23 29 34 42 47

29.8 34.4 35.6
52 63 75

35.4
75

29.2 29.4 32.9 34.1 34.8 35.2
75 53 46 30 21

34.3 34.4 34.5 34.6 35.2 34.8 34.3 32.25 34.8
75 56 37 21 23 32 15" C.M 46

39.

35.3
75

STA

+

π

-

ELV

38.18.

+ 46

GUTTER RT

+ 60

+ 75

GUTTER RT

45+00

+ 33

T.P

9.86

J. A
D. S
B. L

LT

LENICER SEP 23, 1976
E

RT

28

						CUIN T.C	GUTTER T.C
35.2	34.8	34.3	34.8	34.4	34.8		
	23	38	38	46	40		

34.9	35.3		
75	75		

34.5	34.6	34.8	35.3	35.0	34.7	35.0	35.2
75	50	21		23	44	58	75

						GUTTER T.C	GUTTER T.C
35.4	35.2	34.5	34.8	34.2			
	23	39	39	47			

						T.C GUTTER	T.C GUTTER	T.C
5.2	34.7	35.0	34.6	34.8				
75	75	60	60	47				

36.2	36.4	36.6	35.7	36.0	35.9	36.7	37.4
75	46	29	21		23	58	75

39.7	36.7	37.6	36.8	37.1
70	43	33	21	

40.1
75

P. K & STA 46+00

STA

+

 π

-

ELV

39.86

45+50

46+00

+50

47+00

B.M

952.99 952.88

938.25 938.17

940.94 940.87

952.88

952.88

47+50

47+76

Gutter Rt

J. A.
D. S.
B. L.

LENKER

LT

Q

RT

54°
SEPT 23, 1976
29
SEPT 28, 1976

41.7 37.7 37.6 37.8 37.6 38.3 38.6
86 42 21 23 50 75

43.5 39.9 39.7 39.9 39.6 39.9 40.3
75 38 21 23 50 75

45.3 42.9 41.6 42.0 41.8 41.7 42.0
75 50 21 23 50 75

47.1 47.0 45.4 43.8 44.1 43.8 43.4 42.7
75 75 50 21 23 50 75

HYD MCKNIGHT & 14TH AVE

Top Hyd McKnight & 13th AVE

Top Hyd McKnight & 12th AVE

Top Hyd McKnight & 14th AVE

48.5 48.7 47.0 46.2 45.7 46.1 45.9 46.6 46.8 45.9 46.6
80 60 45 21 21 22 24 55 68 85

CB T.C. T.C.
47.3 47.0 47.0 47.7 47.7 49.2
22 44 44 75 75

LENKER

Sta

+

Δ

-

ELEV

47+78

947.17

+88

E 14th Ave

48+98

948.15

48+00

+02

947.56

+05

Gutter Rt

949.00

+32

E

Dr

Lt

48+50

30

47.8	47.4	47.8	48.1
	22	45	75

49.6	49.6	48.0	47.8	48.3	47.9	47.7	48.0
75	52	27	22		22	52	75

		CB GUTTER	T.C.	GUTTER	T.C
48.5	48.1	47.0	47.70	47.6	48.14
	22	44	44	25	25

50.5	50.6	50.0	49.4	49.7
75	52	31	21	

[illegible]

LENKER

STA

+

π

-

ELEV

953.05

49+00

+50

+52

955.19

+57

Q DR RT 13.4

50+00

+50

T.P.

961.67

51+91

961.20

51+00

J.A.
D.S.
B.L.

LT

C Sep 28, 1976
Windy 50 RT

31

PK STA 49+00 E

53.1 53.2 53.4 53.2 52.3 53.0 52.8 53.5 54.6 54.7 53.5
75 52 34 24 21 23 25 34 58 68

53.8
75

54.2 54.6 55.2 55.2 54.7 55.6 55.2 56.1 57.8 57.8
75 46 34 23 21 23 27 39 75

B.7

MH LT 15'

55.9 55.7 57.2 58.1 58.1
23 34 48 75

55.9 56.0 57.4 57.7 57.3 57.9 57.5 58.1 60.2 60.2
75 53 22 21 23 25 33 75

F.B.

58.8 59.5 60.0 60.1 59.5 60.0 59.7 60.3 63.8 64.2
75 45 36 23 21 23 25 34 40

H₀

PK STA 51+00 E

MH RT 13'

62.1 62.3 61.8 61.3 61.7 61.3 63.8 63.99 64.2
75 57 20 26 26 33 52 65

Conc
slw

63.5
75

LEWIS

STA

+

π

-

ELEV

51+08

Gutter Rt & Lt

+22

962.24

+22

Q

15th AVE

+21

+31

961.92

+37

962.42

+37

Gutter Rt & Lt

+50

+55

CB

Lt & Rt

+66

963.20

52+00

J.A.
D.S.
B.L

LT

Sept 28 1976
windy 55 Rt

32

T.C. 13.4		T.C. Bit						T.C. Bit	
63.1	62.7	62.2	61.9	61.5	61.9	61.6	61.8	62.2	62.7
75	75	40	40	22		22	42	42	75

MH 9

63.0	62.3	61.8	62.2	62.1	62.7	63.1
75	48	23		22	56	75

MH LT 33'

MH LT 12'

	T.C. Bit	OB Gutter					OB	T.C. OB	
62.5	62.0	61.7	62.1	62.6	62.4		62.0	62.5	62.6
71	40	40	22		22		40	40	75
									63.1
									75

	TC								S/W conc
64.0	63.8	63.0	62.4	62.9	62.6	63.1	63.8	63.89	64.4
75	60	22	22		22	23	30	62	75

T.E	Gutter		OB Gutter	T.C
62.8	62.5	63.0	62.7	63.2
22	22		22	22

MH Rt 13

FE	T.C.				T.C	S/W
65.5	65.1	64.2	63.6	64.0	63.6	64.13
45	33	22	22		22	24
						33
						31W
						65.5B
						65.42
						H3
						39

		LEUKER			
Sta	+	⌞	-	ELEV	
B.M.				966.29	966.29
52+16		Edge Bit Ent.			
+36		DRIVE	Rt	(Bit)	
+46		DRIVE	Lt.	(Conc)	
+65		DRIVE	Rt & Lt	Bit	
53+00					
+09		DRIVE	Rt	Conc	
+17		WALL	Rt,	DRIVE Lt	GRAVEL
T.P				963.32	

J.A.
D.S.
B.L.

LT

2

SEP 28, 1976
Windy 55° RT

33

Top Hyd 15th Ave McKnight

				Cone SLN	No.
64.2	63.9	64.6	65.4	65.70	66.6
22		33	43	43	58

64.3	64.0	64.8	65.4	66.0
22		35	45	48

Cone GAC	Cone		
65.57	64.67	64.0	64.3
54	33	21	

Bit	Bit					GAC Cone
65.6	64.9	64.6	63.9	64.2	63.9	64.9
57	33	27	21		22	36
						47

		FE.	T.C Bit				Cone	Cone
64.2	64.6	64.8	64.3	63.8	64.0	63.8	64.93	65.63
75	49	32	22	21		22	34	54

				Cone	Cone GAC
		64.0	63.8	64.95	65.63
		22		34	54

				Cone	Cone GAC
64.4	64.5	63.7	63.9	63.7	65.03
75	37	21		22	34
					53

PK Sta 54+00 2

LEWKEP

Sta

+

π

-

ELEV

53+23

+50

54+00

+18

+36

Gutter Rt

B.M.

966.44

966.43

+50

962.97

+50

E 16th Ave

+59

962.39

+65

Gutter Rt

54+72

962.84

J. A.
D. S.
B. L.

L4

Q

SEPT 29, 1976
CLR 60°

C
RT

34

T.C.					F.E.			
64.5	64.6	64.5	63.7	63.9	63.7	64.2	66.9	64.9
75	52	34	21		22	22	37	54

T.C.					F.E.			
63.7	63.8	64.0	63.4	63.7	63.4	63.9	67.3	
75	47	21	21		22	22	37	

T.C.					T.C.			
62.7	63.4	63.5	63.0	63.3	62.8	63.4	67.3	67.6
75	54	21	21		22	22	36	70

T.C.				
		63.2	62.6	63.2
		22	22	38

CB GUTTER		T.C.		T.C.	
63.1	62.6	61.8	62.4	62.4	62.1
22	39	39	75	75	75

Hyd Cor McKnight 1/16th AVE

MH Q

T.C.				
62.8	63.2	62.6	63.0	62.6
75	21	21		22

MH RT 36

CB GUTTER		T.C.			
63.0	62.6	62.3	62.6	62.4	62.7
22	37	37	75	75	75

MH Lt 12'

STA	+	LENKER π	-	ELEV	
54 +85		CB	RT & LT		
55+00					
+54		DRIVEWAY	RT & LT		
+69					
+74					
+87					
+90		So Edge	Bt ENT		
56+00		ENT	RT		
+06		Bottom of WALL	No Edge ENT		

35

63.6	63.5	64.1	64.5
	22	29	58

STA

+

T

LENKER

-

ELEV

56+09

T.P.

166.0

966.20

+50

+63

ENT LT (Cone)

+70

B.M.

166.1

966.44

966.44

B.M.

940.87

940.87

B.M.

938.17

938.17

T.P.

944.03

B.M.

952.90

952.88

T.P.

960.05

B.M.

966.30

966.29

J.A.
D.S.
B.C

Lt

Q

Sept 29, 1976
Sunny 65°

Lt

Rt

36

T.C.

63.6	63.4	64.0	64.7	68.5	68.5
22	22	24	24	38	

P.K STA 57+00

Bit Bit

T.C.

66.3	65.4	63.6	63.9	63.6	64.1	68.2	68.8	69.6
72	35	21		22	22	32	54	75

conc conc conc

T.C.

66.80	65.91	64.8	63.6	64.0	63.6	64.2	66.8	67.4	67.8
75	56	33	21		22	22	31	52	70

T.C.

64.0	63.6	64.2	65.0	65.4	65.5
22	22	37	56	66	

Top Hyd on "C" E. of McKnight Ho^d 2295

Top Hyd N.E. Cor 12th Ave & McKnight

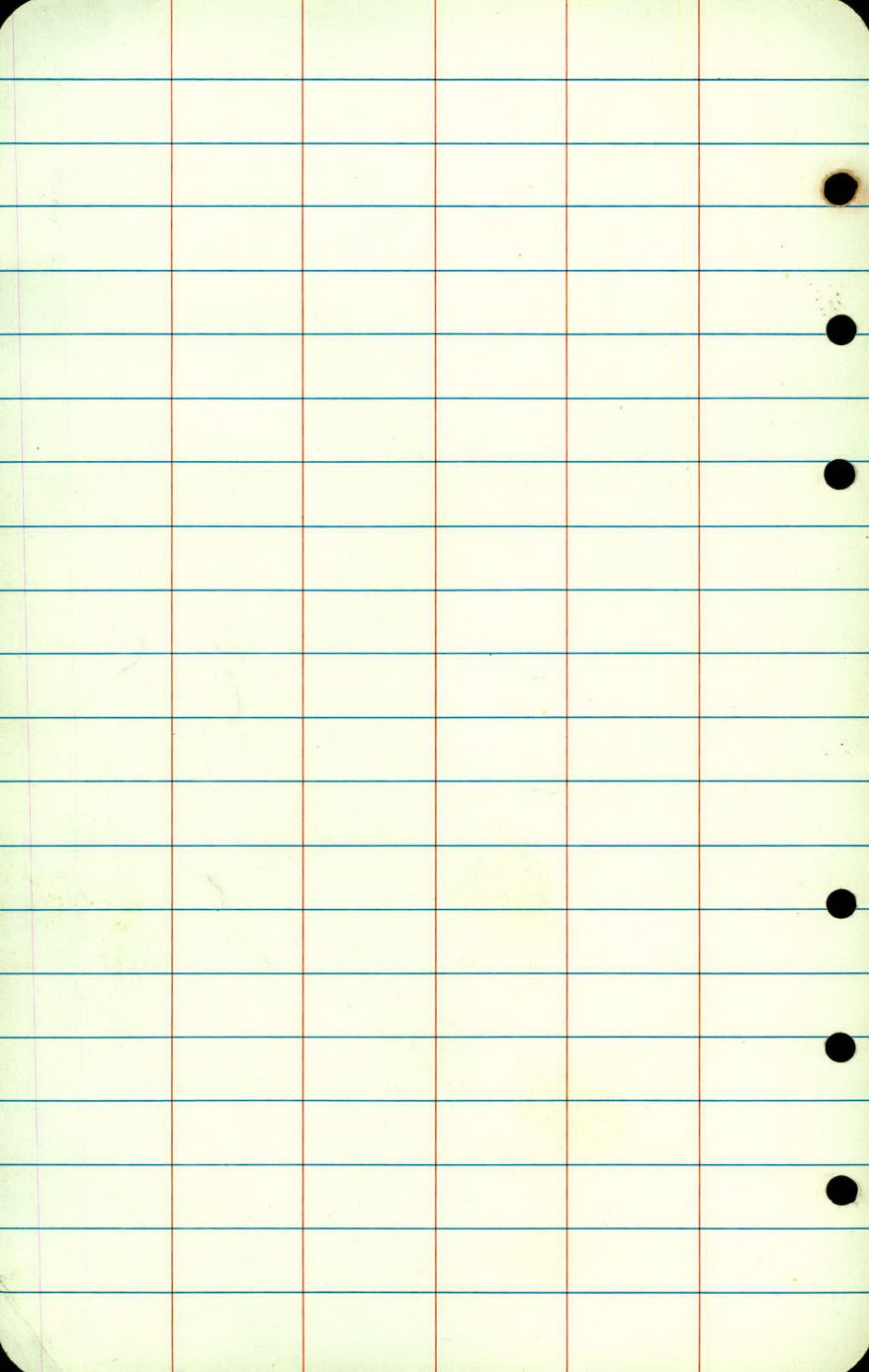
Top Hyd N.E. Cor 13th Ave & McKnight

P.K STA 47+00 Q

Top Hyd NE Cor 14th Ave & McKnight

P.O.T. Q 50+52±

Top Hyd NE Cor 15th Ave & McKnight



FK
CM
AS
DW

8-4-69

B-1

Bench Levels

Sta + π - Elev.

BM 3.64 969.15 965.51

BM 2.86 969.73 2.28 966.87 #345

BM 2.52 969.00 3.24 966.48 Dell 4C

BM 3.26 966.47

BM 2.88 968.98 2.90 966.10 966.04

B.M 3.58 970.06 2.50 966.48 966.42

BM 2.40 969.30 3.16 966.90 966.88

BM 3.74 965.56 965.51

8-4-69

B-2

Top Hyd by Ho # 2171 E. Co. Rd. "C"

Top Hyd by Ho # 2295 E. Co. Rd. "C".

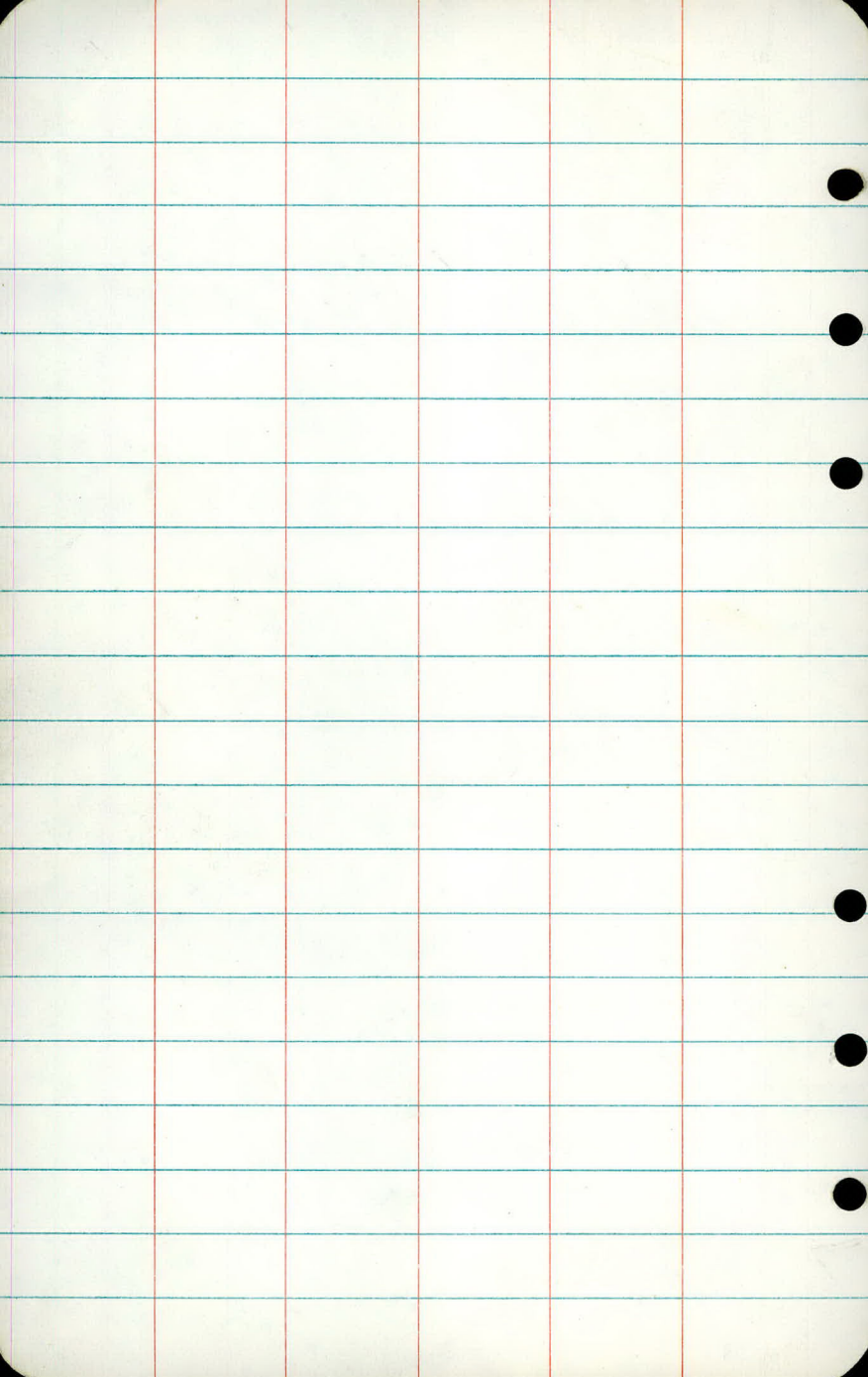
Top Hyd N.E. Corner 16th & McKnight

Top Hyd N.E. Corner Delaware & C

Top Hyd. by Ho. # 2295 E. Co. Rd. "C"

Top Hyd by Ho # 2239 E. Co. Rd. "C"

Top Hyd by Ho # 2171 E. Co. Rd. "C"



Bench Level Check

Sta	+	π	-	Elev
BM	1.07	971.96		(970.89)
BM	1.636	969.506	4.09	967.87
BM	3.12	969.176	3.45	966.056
BM	3.602	970.054	2.724	966.452
BM	3.114	969.905	3.263	966.791 (966.79)
BM	2.187	969.040	3.052	966.853
	1.001	969.048	0.993	968.047 <i>Fe post</i>
BM			3.528	965.520 (965.51)

BM 4.528 971.318 966.79

BM 3.89 974.43 0.78 (970.54)

BM 0.25 972.513 2.165 972.263

BM 1.234 970.757 2.99 969.523

BM 9.88 976.924 3.713 967.044

BM 12.49 989.154 0.26 976.664

BM 5.49 994.284 0.36 988.794

BM 3.92 997.294 0.91 993.374

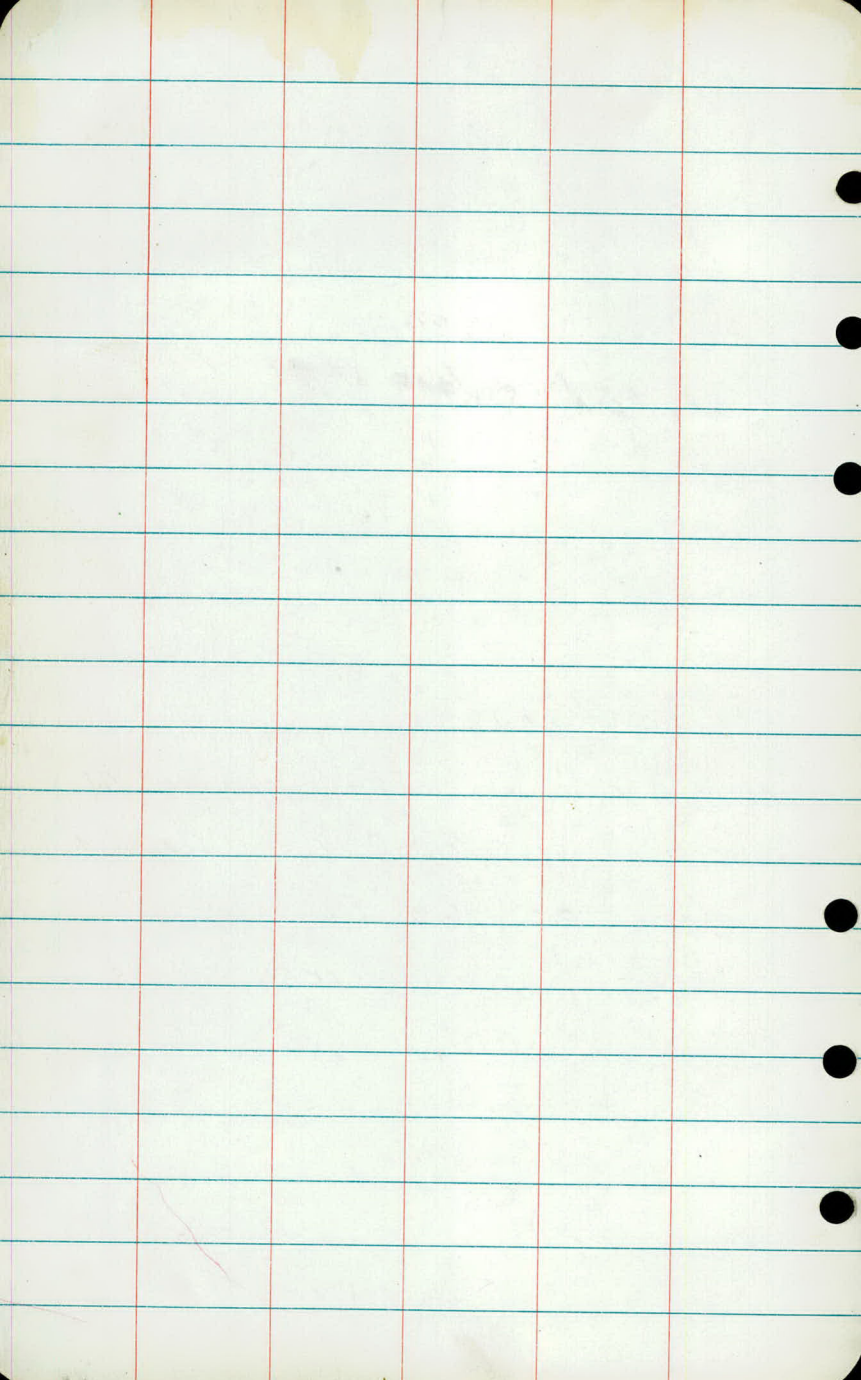
BM 0.00 997.294

USE THESE

FK
LPD

Feb. 10, 1970

- Top Hyd S.E. Corner 2nd St + 17th Ave or "C"
- Top Hyd Across From Ho[#] Co Rd "C"
- Top Hyd NW Corner Delaware + "C"
- Top Hyd by Ho[#] 2295 Co Rd C
- Spike in Arc Light Pole S.E. Corner McKnight
- Top Hyd Front Ho Co Rd "C"
- Top Hyd Lt. Sta 148 + 50' by #2171
- Spike in Arc Light Pole S.E. Corner "C" + McKnight
- Top Hyd at Mohak
- Top Hyd by Ent to 2700 McKnight Rd
- Top Hyd between Ent to #2736 + #2742 McKnight ✓
- Top Hyd. S.E. Corner Shawnee Drive.
- Top Hyd. S.E. Corner Navajo Road
- Top Hyd. S.E. Corner Shoshone
- Top Hyd. N.W. Corner Maple View Ave.
- Top Hyd. S.E. COR. BEAM



RP
LPO
ML
CM

18 DEC 1969 1.
Cloudy 20°

McKNIGHT RD
Co. RD C TO Co. RD. D
X-SECTIONS

STA	+	π	-	ELEV
-----	---	-------	---	------

BM	4.35	974.95		970.60
----	------	--------	--	--------

$$0-100 = 56 + 76.89$$

$$0-50 = 57 + 26.89$$

$$0-25 = S. GUTTER CO. RDC$$
$$57 + 51.89$$

$$0+100 = \neq CO. RDC$$

✓

$$+20 = N. GUTTER CO. RDC$$

LT

E

18 DEC 1969

2.

RT

TOP HYD N.E. COR MOHAWK

66.6	66.3	64.3	63.9	64.2	63.9	64.7	64.7	65.1
8.4	8.7	10.7	11.1	10.8	11.1	10.3	10.3	9.3
73	61	23	18		19	25	28	50
40								

65.0	64.6	64.3	64.5	64.4	65.6	65.4	65.6
10.0	10.4	10.7	10.5	10.6	9.4	9.6	9.4
74	43	18		18	25	46	57

64.1	64.2	64.2	64.7	64.9	64.7	64.6	64.7
10.9	10.8	10.8	10.3	10.1	10.3	10.4	10.3
76	48	25		21	40	56	78

64.6	64.7	64.7	64.8	64.8	65.0	65.0	64.9
10.4	10.3	10.3	10.2	10.2	10.0	10.0	10.1
100	75	50	25		27	50	75
64.5	64.7				64.3	64.5	64.8
10.5	10.3				10.7	10.5	10.2
150	200				200	150	100

64.5	64.4	64.3	64.2	64.8	64.6	64.7	64.5	64.5
10.5	10.6	10.7	10.8	10.2	10.4	10.3	10.5	10.5
100	84	49	28		28	57	80	100

STA	+	π	-	ELEV
-----	---	-------	---	------

		974.95		
--	--	--------	--	--

0+29				
------	--	--	--	--

✓				
---	--	--	--	--

0+50				
------	--	--	--	--

1+00				
------	--	--	--	--

120	± ENT. RT (CONC.)			
-----	-------------------	--	--	--

TP	6.11	972.84	8.22	966.73
----	------	--------	------	--------

18 DEC. 1969 3.

LT

E

RT

65.1	65.4	65.6	64.4	65.0	64.7	64.9	65.34
9.9	9.6	9.4	10.6	10.0	10.3	10.1	9.61
79	55	31	19		19	28	43 SW

69.8	65.32	69.90
4.97	9.63	5.05
68	68	43
WALL	SW	WALL

66.6	65.1	65.2	65.6	65.3	66.0	71.0	71.6
8.4	9.3	9.8	9.4	9.7	9.0	4.0	3.5
47	28	16		19	23	34	50

67.0	66.1	65.8	65.9	65.8	66.5	71.2	72.0
8.0	8.9	9.2	9.10	9.2	8.5	3.8	3.0
43	25	18		16	22	33	49
							HO

66.0	65.9	65.71	65.8	65.82
9.0	9.1	9.24	9.17	9.13
16	25	38	48	
	conc.	conc.	conc.	

PK E STA 2+00

STA	+	π	-	ELEV.
-----	---	-------	---	-------

		972.84		
--	--	--------	--	--

1+50				
------	--	--	--	--

2+00				
------	--	--	--	--

+50				
-----	--	--	--	--

+61 = GUTTER (S) MOHAWK (RT)				
------------------------------	--	--	--	--

+74 = E MOHAWK (RT)				
--------------------------------	--	--	--	--

+86 = GUTTER (N) RT				
GUTTER (S) LT				

18 DEC 1969

LT

E

RT

66.9	66.3	66.0	66.2	66.1	66.3	68.4
5.9	6.5	6.8	6.6	6.7	6.5	4.4
43	22	17	18	24	35	Fe

66.4	66.7	66.6	66.7	66.4	66.5	67.7
4.4	6.1	6.2	6.1	6.4	6.3	5.1
43	23	17	17	23	34	Fe

69.5	68.1	67.6	67.1	67.1	67.0	67.2	67.4	67.4
3.3	4.7	5.2	5.7	5.7	5.8	5.6	5.4	5.4
44	31	26	17	18	26	38	57	

67.2	67.8	67.3	67.3	67.0	67.2	67.3	67.4
3.6	5.0	5.5	5.5	5.8	5.6	5.5	5.4
45	27	16	18	30	51	75	

69.3	68.1	67.5	67.5	67.2	67.5	67.6	67.6
3.5	4.7	5.3	5.3	5.6	5.3	5.2	5.2
46	31	18	16	25	53	100	

67.2	67.8	67.7	67.4	67.6	67.4	67.4
5.1	5.0	5.1	5.4	5.2	5.4	5.4
67	47	26	17	18	37	62

STA + π - ELEV

972.84

3+00 = $\neq$ MOHAWK (LT)

+16 = GUTTER N (LT)

TP 6.29 974.12 5.01 967.83

3+50

4+00

+11 = $\neq$ ENT LT (DIRT)

LT

E

18 DEC. 1969

RT

67.7	67.9	67.8	67.6	67.8	67.7	68.1	68.1	68.2
5.1	4.9	5.0	5.2	5.0	5.1	4.7	4.7	4.6
100	62	30	17	18	26	48	66	

67.3	67.5	67.8	67.8	68.0	67.9	68.5	68.5
5.5	5.3	5.0	5.0	4.8	4.9	4.3	3.3
100	66	38	16	17	33	66	40

PK E STA 3400

70.6	70.5	69.1	68.9	68.2	68.0	68.8	69.9
3.5	3.6	5.0	6.1	5.9	6.1	5.3	4.2
64	46	30	17	17	32	64	40

70.4	69.2	68.3	68.6	68.4	69.1	70.6	71.2
3.7	4.9	5.8	5.46	5.7	5.0	3.5	2.9
64	29	16	17	26	43	65	40

69.7	69.2	68.4	68.7
4.4	4.9	5.7	5.4
49	31	17	

STA + π - ELEV.

974.12

4+21 = $\neq$ ENT RT (BT)

+50

BM	0.22	972.54	1.89	972.23	972.32
----	------	--------	------	--------	--------

4+90 = $\neq$ ENT. RT (DIRT)

5+00

+50 $\neq$ ENT LT RT (DIRT)

LT

18 DEC 1969

RT

69.8	68.5	69.5	70.8	71.2
5.3	5.6	4.6	3.3	2.9
17	31	50	66	

69.8	69.5	69.3	68.6	69.0	68.8	69.6	71.0	71.6
4.3	4.6	4.8	5.5	5.1	5.3	4.5	3.1	2.5
63	48	26	16	17	26	48	64	Ho

TOP HYD RT STA 6 + 96

69.6	69.3	71.0	71.3
2.9	3.2	1.5	1.2
17	40	62	

70.9	70.5	70.1	69.1	69.7	69.4	70.5	70.7
1.6	2.0	2.4	3.4	2.84	3.1	2.0	1.8
66	47	30	15	17	31	65	Ho

70.8	70.2	70.1	69.4	69.6	69.4	70.3	71.4
1.7	1.8	2.4	3.1	2.9	3.1	2.2	1.1
58	50	30	15	17	33	57	

STA	+	π	-	ELEV
-----	---	-------	---	------

		972.54		
--	--	--------	--	--

6+00				
------	--	--	--	--

BM	0.09	972.41	0.22	972.32	972.32
----	------	--------	------	--------	--------

6+17		Q ENT Rt. CONC.		
------	--	-----------------	--	--

6+30		Q ENT Lt Bit		
------	--	--------------	--	--

+50				
-----	--	--	--	--

+82		Q ENT Rt Diet		
-----	--	---------------	--	--

LT

E

18 DEC. 1969

RT

7.1	7.9	6.9	6.4	6.2	7.3	7.1	7.4
1.3	2.1	3.3	3.07	3.3	2.2	1.4	1.1
64	33	17		18	30	49	61
HO							HO

HYD RT 6+96

7.1	7.7	6.9	6.2	6.9	6.1	7.3	7.9	7.2
1.3	1.7	2.5	3.2	3.04	3.3	2.12	1.48	1.15
65	50	25	15		17	35	50	67
HO								

7.1	6.7	6.1	6.4	6.1	7.2	7.0
1.3	2.7	3.3	3.0	3.3	2.2	1.4
52	28	15		17	36	66
						HO

6.7	6.6	6.9	6.2	6.0	6.6	7.6
2.7	2.8	3.5	3.7	3.4	2.6	1.8
54	39	16		17	32	59
HO						HO

6.1	6.9	6.9	7.7
3.3	3.5	2.5	1.7
15	36	65	

Sta. + π - ELEU

972.41

6+93 ENT Lt.

7+00

+50 ENT Rt Bit.

+59 & ENT Lt CONC

8+00

+15 ENT Rt Bit

19 DEC 1969

Lt.

L

Rt

69.9	68.8	68.6	69.0
3.0	3.6	3.8	3.4
68	34	16	

69.3	68.8	68.5	68.9	68.7	69.2	70.7
3.1	3.6	3.9	3.51	3.7	3.2	1.7
64	40	16		15	26	62
						Ho

69.3	68.7	68.2	68.3	68.0	69.6	70.5
3.1	3.7	4.2	4.1	4.4	2.8	1.9
64	40	16		16	37	67

69.2	66.9	68.0	68.3
3.24	5.54	4.4	4.1
66	55	16	

70.2	68.7	67.5	67.8	67.5	69.2	69.9
2.2	3.7	4.9	4.57	4.9	3.2	2.5
65	36	16		16	40	60
Ho						Ho.

67.2	67.5	68.4	69.1
4.7	4.9	4.0	2.7
	17	31	64

Sta	+	π	-	Elev
-----	---	-------	---	------

		972.41		
--	--	--------	--	--

8+31	Ent	Lt	Bit
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TP	3.67	971.51	4.57	967.84
----	------	--------	------	--------

+50

+70	Ent	Lt	Bit
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+77	Ent	Rt	Bit
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9+00

19 DEC 1969

L+

E

R+

69.7	68.7	67.4	67.6
2.7	3.7	5.0	4.8
63	41	18	

E STA 8+00

68.1	67.7	67.0	67.3	66.9	66.7
3.4	3.8	4.5	4.2	4.6	3.3
60	30	16		16	30
Ho					

68.3	68.1	67.7	66.9	67.1
3.2	3.4	3.8	4.6	4.4
66	53	33	17	

67.1	66.8	66.3	66.4
4.4	4.7	3.2	2.1
	17	32	62

68.4	67.3	67.1	67.0	66.7	67.0	68.4	69.4
3.1	4.2	4.8	4.5	4.8	4.5	3.1	2.1
60	28	17		17	25	36	59
Ho.							

Sta	+	π	-	ELEV
-----	---	-------	---	------

971.51

9+42		ENT Rt	Dirt	
------	--	--------	------	--

+45		ENT Lt	CONC	
-----	--	--------	------	--

10+00

+10		ENT Rt	Bit	
-----	--	--------	-----	--

+54		ENT Lt	CONC	
-----	--	--------	------	--

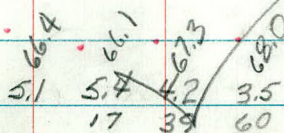
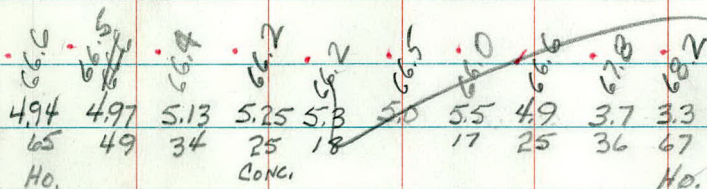
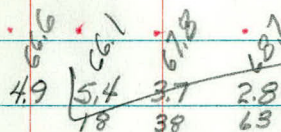
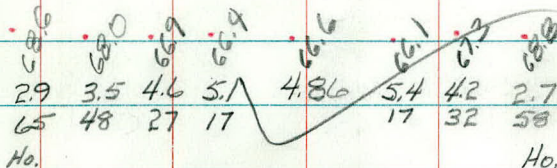
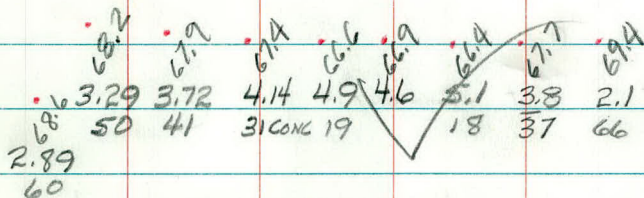
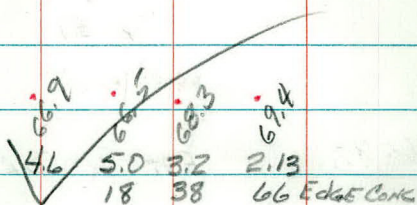
+72		ENT Rt	Dirt	
-----	--	--------	------	--

19 DEC 1969

L+

E

R+



Sta + π - ELEV

971.51

10+93

Ent Rt Dirt

11+00

BM 0.63 970.20 2.07 969.44 969.57

+39

Ent Lt Conc

+56

Ent Rt Dirt

12+00

Rt.

$\cdot$	$\cdot$	$\cdot$	$\cdot$	$\cdot$	$\cdot$	$\cdot$	$\cdot$
67.0	69.8	69.5	65.9	66.3	65.9	66.9	68.1
4.5	4.7	5.0	5.6	5.19	5.6	4.6	3.4
63	45	31	18		18	33	57
H ₀							H ₀

67.68	66.99	66.58	66.20	65.9	65.1
2.52	3.21	3.62	4.00	4.3	4.1
67	51	34	25	17	CONC

7.6	9	1	5.8	0	6	5	7
6	6	6	6	6	6	6	6
2.6	3.3	4.1	4.4	4.2	4.6	3.7	2.7
67	47	28	17		17	33	58

[illegible]

STA	+	π	-	ELEV
-----	---	-------	---	------

		970.20		
--	--	--------	--	--

12+10		ENT LT CONC		
-------	--	-------------	--	--

+22		ENT Rt DIRT		
-----	--	-------------	--	--

+58		ENT LT Bit		
-----	--	------------	--	--

13+00				
-------	--	--	--	--

+50				
-----	--	--	--	--

14+00		ENT Bit Lt		
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BM	4.32	971.45	3.11	967.09
----	------	--------	------	--------

				967.13
--	--	--	--	--------

19 DEC 1969

L+

E

R+

66.05
65.91
65.81
65.57
65.34
65.3
65.6
4.29 4.39 4.63 4.86 4.9 4.6
52 41 29 20 17
4.15
63
CONC

65.6
65.4
65.1
66.9
4.6 4.8 4.1 3.3
17 33 59

66.1 65.5 65.0 65.5 65.2 65.8 67.1
4.1 4.7 5.2 4.7 5.0 4.4 3.1
63 36 17 17 31 64

66.1 65.5 65.2 65.1 65.4 65.1 65.4 67.0 64.2 60.7
4.1 4.7 5.0 5.1 4.76 5.1 4.8 3.2 6.0 9.5
69 52 27 16 17 31 59 68 80

66.4 65.8 65.0 65.2 65.3 65.0 65.5 66.4 61.2
3.8 4.4 5.2 5.0 4.9 5.2 3.7 3.8 9.0
68 47 26 16 17 46 54 68

66.1 65.4 65.1 65.37 65.1 65.7 65.8
4.1 4.8 5.1 4.83 5.1 4.5 4.4
61 38 16 17 33 74

TOP HYD AT SHAWNEE

STA	+	π	-	ELEV
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		971.45 ^c		
--	--	---------------------	--	--

14+50

+57

GUTTER Lt & Rt (S)

+70

& SHAWNEE

+85

GUTTER Lt & Rt (N)

15+00

+50

T.P.

8.25

978.03^c

1.67

969.78^c

22 DEC 1969
SUNNY 100°
R4

L4

4

63.7	64.6	65.3	65.6	65.3	65.5	65.6
7.8	6.9	6.2	5.9	6.2	6.0	5.9
67	40	16		16	40	62

62.1	63.2	64.3	65.1	65.1	65.3	65.1	64.9	64.6
8.8	8.3	7.2	6.4	5.8	6.2	6.5	6.6	6.9
100	78	45	21		21	46	73	100

63.0	64.0	64.7	65.4	65.7	65.5	65.2	64.9
8.5	7.5	6.8	6.1	5.8	6.0	6.3	6.6
100	69	41	17		19	51	100

63.2	64.3	65.0	65.6	65.8	65.5	65.5	65.3	65.1
8.3	7.2	6.5	5.9	5.7	6.0	6.0	6.2	6.4
100	62	39	17		19	4.9	76	100

65.7	65.9	65.7	65.87	65.7	65.8	65.1
5.8	5.6	5.8	5.58	5.8	4.7	4.4
62	33	17		16	29	49

66.8	67.1	67.5	67.7	67.6	67.9	69.6
2.7	3.8	4.0	3.8	3.9	2.6	1.9
64	35	17		16	30	49
Ho.						Ho

Sta	+	π	-	ELEV
-----	---	-------	---	------

		978.03		
--	--	--------	--	--

16+00				
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+50				
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17+00				
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BM	7.71	984.44	1.30	976.73	976.74
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+50	Gutter	Rt	(S)		
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+66	& Navajo				
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22 DEC 1969

Lt,

L

Rt.

68.1	70.1	69.6	69.78	69.5	70.2	70.1
9.9	7.9	8.4	8.25	8.5	7.8	7.9
68	36	17		16	30	49

70.8	72.0	71.5	71.8	71.4	72.0	70.9
7.2	6.0	6.5	6.2	6.6	6.0	7.1
72	36	17		16	30	50

70.2	74.0	73.7	73.95	73.5	75.0	77.1	79.0
5.8	4.0	4.3	4.08	4.5	3.0	0.9	0.0
69	30	16		15	2.8	37	48

Ho.

Top Hyd S.E. Cor NAVAJO

73.1	76.9	76.6	75.5	75.7	75.7	76.4	76.5	76.6
10.7	7.5	7.8	8.9	8.7	8.7	8.0	7.9	7.8
62	49	30	15		21	25	75	100

73.5	77.3	76.5	76.0	76.2	76.2	76.5	76.8	77.0
10.9	7.1	7.9	8.4	8.2	8.2	7.9	7.6	7.4
67	45	30	15		18	48	7.8	100

Sta

+

K

-

Elev

984.44

17+78

Gutter Rt (N)

18+00

+50

19+00

T.P.

11.27

992.73

2.98

981.46

+50

Δ E R
 $\dot{14.0}$ $\dot{11.8}$ $\dot{10.8}$ $\dot{16.3}$ $\dot{16.6}$ $\dot{16.6}$ $\dot{16.4}$ $\dot{16.5}$ $\dot{16.8}$
 10.4 6.6 7.6 8.1 7.8 7.8 8.0 7.9 7.6
 73 49 30 15 22 49 73 100

$\dot{11.2}$ $\dot{11.9}$ $\dot{11.6}$ $\dot{11.1}$ $\dot{11.43}$ $\dot{11.0}$ $\dot{11.9}$ $\dot{11.5}$
 7.2 6.5 6.8 7.3 7.01 7.4 6.5 5.9
 70 48 31 17 16 29 50

$\dot{19.9}$ $\dot{19.8}$ $\dot{19.6}$ $\dot{19.2}$ $\dot{19.4}$ $\dot{19.5}$ $\dot{20.0}$ $\dot{20.7}$
 4.5 4.6 4.8 5.2 5.0 5.1 4.4 3.7
 78 49 30 16 15 27 45
 Ho

$\dot{81.7}$ $\dot{82.0}$ $\dot{81.6}$ $\dot{81.2}$ $\dot{81.46}$ $\dot{81.2}$ $\dot{80.7}$
 2.7 2.4 2.8 3.2 2.98 3.2 3.7
 68 39 28 16 17 33
 FE

Top PK E Sta 19+00

$\dot{84.5}$ $\dot{84.1}$ $\dot{83.2}$ $\dot{83.5}$ $\dot{83.5}$ $\dot{85.2}$ $\dot{87.1}$
 8.2 8.6 9.5 9.2 9.2 7.5 5.6
 65 37 21 15 26 35
 FE

STA	+	π	-	ELEV
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		992.73		
--	--	--------	--	--

19+58		GUTTER Lt. (S)		
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+71		& Radatz		
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+86		GUTTER Lt (N)		
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20+00				
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+48		GUTTER Rt (S)		
-----	--	---------------	--	--

+58		& Sho stone		
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Lt

E

Rt

83.4	83.5	83.6	83.6	83.8	83.8	85.3	87.2
9.3	9.2	9.1	9.1	8.9	8.9	7.4	55
100	72	34	15		16	25	35
							FE

83.7	83.8	83.7	84.0	84.4	84.3	85.6	87.6	88.3
9.0	8.9	9.0	8.7	8.3	8.4	7.1	5.1	44
100	75	46	15		16	24	36	47

83.5	83.6	83.9	84.7	85.0	84.9	86.2	88.1	88.2
9.2	9.1	8.8	8.0	7.7	7.8	6.5	4.6	4.5
100	62	34	15		16	25	38	47
								Ho

84.9	85.4	85.2	85.54	85.4	86.3	88.0	88.3
7.8	7.3	7.5	7.19	7.3	6.4	4.7	4.4
61	27	14		16	35	38	49

86.7	86.6	86.5	86.7	86.7	87.0	87.4	87.5
6.0	6.1	6.2	6.0	6.0	5.7	5.3	5.2
56	30	15		15	37	67	100

86.9	86.6	86.6	86.8	86.9	86.9	87.4	87.7	87.9
5.8	6.1	6.1	5.8	5.8	5.8	5.3	5.0	4.8
64	50	31	15		16	33	67	100

STA	+	T	-	ELEV
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		992.73		
--	--	--------	--	--

20+70		GUTTER Rt (N)		
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21+00				
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+54		± ENT Rt		
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TP	6.34	995.55	3.52	989.21
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22+00		± ENT Lt CONC		
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+53		± ENT Rt Bit		
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Lt

E

Rt

~~96.8 96.9 97.1 97.2 97.1 97.4 97.6 97.7
 5.9 5.8 5.6 5.5 5.6 5.3 5.1 5.0
 67 31 15 16 46 81 100
 Ho.~~

~~96.7 97.7 97.5 97.9 97.6 98.2 99.5 99.1
 6.0 5.0 5.2 4.82 5.1 4.5 3.2 3.6
 80 31 14 16 26 49 73~~

~~97.6 98.4 98.4 98.7 98.4 99.0 99.6
 5.1 4.3 4.3 4.0 4.3 3.7 1.1
 73 30 15 15 26 5.6~~

Top PK E Sta 22+00

~~99.40 99.16 99.02 98.9 99.23 98.8 99.9 99.23 99.9
 6.15 6.39 4.53 6.7 6.32 6.8 5.7 3.3 2.7
 67 52 34 16 15 28 57 73
 Ho. CONC Ho~~

~~92.8 92.0 90.2 99.9 99.6 99.8 99.6 99.9 99.4 92.8
 2.8 3.6 5.4 5.7 6.0 5.8 6.0 4.7 3.2 2.8
 65 50 32 27 16 16 38 61 73~~

Sta	+	π	-	ELEV
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		995.55		
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22+84		GUTTER Lt (S)		
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23+00		& MAPLEVIEW		
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+19		GUTTER Lt (N)		
-----	--	---------------	--	--

+34		& ENT Rt Bit		
-----	--	--------------	--	--

+50				
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24+00				
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Lt

E

Rt

$\dot{q}1.5$ $\dot{q}1.2$ $\dot{q}0.9$ $\dot{q}0.8$ $\dot{q}0.2$ $\dot{q}0.1$ $\dot{q}0.6$ $\dot{q}3.8$
 4.1 4.4 4.7 5.8 5.4 5.9 4.9 3.0 1.8
 100 61 43 17 16 29 55 74
 Ho.

$\dot{q}1.7$ $\dot{q}1.5$ $\dot{q}1.0$ $\dot{q}0.1$ $\dot{q}0.37$ $\dot{q}0.9$ $\dot{q}0.8$ $\dot{q}3.0$ $\dot{q}3.7$
 3.9 4.1 4.6 5.5 5.18 5.7 4.8 2.6 1.9
 100 76 73 16 16 29 56 73
 Ho

$\dot{q}1.5$ $\dot{q}1.2$ $\dot{q}0.9$ $\dot{q}0.7$ $\dot{q}0.3$ $\dot{q}0.5$ $\dot{q}0.1$ $\dot{q}0.9$ $\dot{q}3.3$ $\dot{q}3.9$
 4.1 4.4 4.7 4.9 5.3 5.1 5.5 4.7 2.3 1.7
 100 70 56 28 15 15 28 56 70

$\dot{q}3.1$ $\dot{q}2.0$ $\dot{q}1.2$ $\dot{q}0.6$ $\dot{q}0.8$ $\dot{q}0.6$ $\dot{q}2.2$ $\dot{q}3.9$ $\dot{q}4.1$
 2.5 3.6 4.4 5.0 4.8 5.0 3.3 1.7 1.5
 71 46 25 12 15 41 63 74

$\dot{q}3.4$ $\dot{q}2.9$ $\dot{q}1.7$ $\dot{q}0.7$ $\dot{q}1.0$ $\dot{q}0.6$ $\dot{q}1.5$ $\dot{q}4.7$
 2.2 2.7 4.3 4.9 4.6 5.0 4.1 0.9
 65 54 31 16 14 28 65
 Ho

$\dot{q}4.8$ $\dot{q}4.4$ $\dot{q}1.7$ $\dot{q}1.3$ $\dot{q}1.56$ $\dot{q}1.3$ $\dot{q}2.1$ $\dot{q}4.5$ $\dot{q}4.7$
 0.8 1.2 3.9 4.3 3.99 4.3 3.5 1.1 0.9
 72 63 24 11 15 29 57 74
 Ho.

Sta	+	π	-	ELEV
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		995.55		
--	--	--------	--	--

24+13	4	ENT	Rt	Dirt
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+50				
-----	--	--	--	--

+92	£	ENT	Rt	(Dirt)
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25+00				
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+24	£	ENT	Rt	(Bit)
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BM	5.43	998.76	2.33	993.22	993.33
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L+	L	R+
95.4	94.7	93.5
0.2	0.9	2.1
70	59	43

92.5	90.4	91.8	92.3	92.0	92.7	95.1	95.4
3.1	3.2	3.8	3.3	3.6	2.9	0.5	0.2
33	28	14		14	27	58	72

94.1	94.4	92.8	92.4	92.7	92.6	94.9	95.6
1.5	1.2	2.8	3.2	2.9	3.0	0.7	0.0
64	41	27	15		14	47	56

94.4	93.1	92.5	92.76	92.7	93.7	95.6
1.2	2.5	3.1	2.79	2.9	1.9	0.0
65	31	15		14	29	61

95.3	93.6	92.8	93.0	92.8	94.8	95.5
0.3	2.0	2.8	2.6	2.6	0.8	0.1
70	31	15		14	44	73

TOP HYD N.W. COR MAPLEVIEW

STA

+

 π

-

ELEV

998.76

25+50

26+00

+13 GUTTER LINE Lt¹/₂Rt (S)

+28 & BEAM

+44 GUTTER LINE Lt¹/₂Rt (N)

B.M. 0.65 997.93 1.65 997.11 997.29

LT

E

RT

94.3	94.0	93.1	92.3	93.3	94.2	95.1	96.8
4.5	4.8	5.7	5.5	5.5	4.6	3.1	2.0
61	30	15		15	28	52	70

Ho

94.0	94.1	94.0	93.7	93.91	94.1	94.5	95.3
4.8	4.7	4.8	5.1	4.85	4.7	4.3	3.5
67	49	30	16		16	30	73

92.1	93.3	93.8	93.9	94.2	94.3	94.8	95.1	96.0
6.1	5.5	5.0	4.9	4.6	4.5	4.0	3.7	2.8
100	66	35	16		16	38	60	100

92.9	93.4	93.7	94.0	94.3	94.5	95.0	95.1	96.3
5.9	5.4	5.1	4.8	4.8	4.3	3.8	3.1	2.5
100	73	49	19		15	42	71	100

92.1	93.0	93.6	93.9	94.3	94.5	94.9	95.5	95.9
6.1	5.6	5.2	4.9	4.5	4.3	3.9	3.3	2.9
100	69	40	17		20	48	78	100

Top Hyd S.E. COR BEAM

STA

+

π

-

ELEV

997.93

27+00

+07

ENT RT

+50

28+00

+50

29+00

KP
DS
LPD
CM
GA

7 APRIL 1970
SUNNY 50°

McKNIGHT RD.
Co. RD. C - Co. RD. D

X- SECTION

STA	+	π	-	ELEV.
BM	7.08	973.87		966.79

1+07

✓

BM		3.28	970.59	970.60
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LT

7 APRIL 1970

RT

S PIKE IN ARC-LITE POLE S.E. Cor
 MC KNIGHT RD & Co. RD. "C."

65.8 65.7 65.6 65.7⁹ 71.30

8.1 8.2 8.3 8.14 2.57
 10 19 34 34
 BOTTOM TOP

71.33 65.76

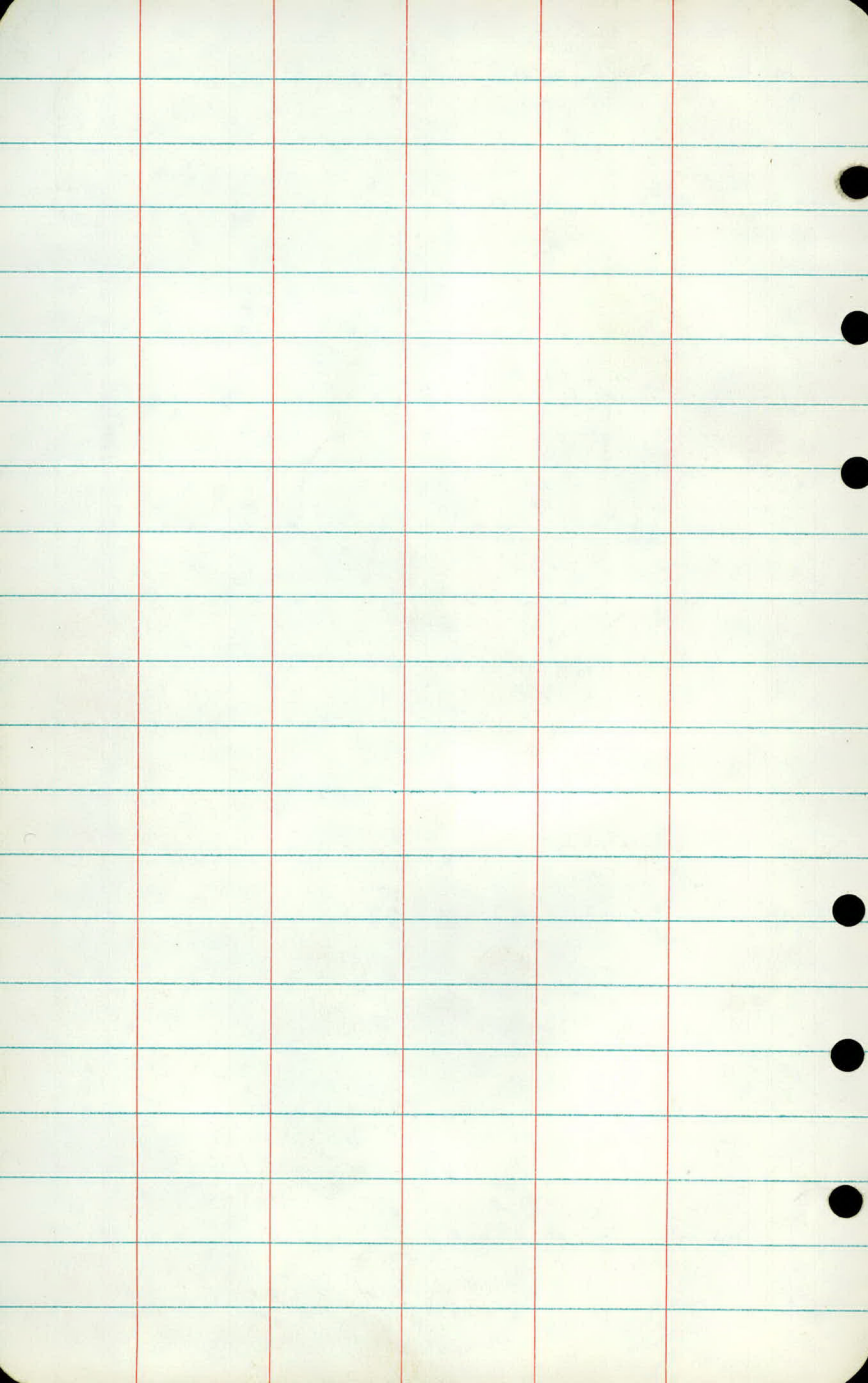
2.52 8.11

49 49

HO HO

BOTTOM TOP

TOP HYD. AT MOHAWK



FK
CM
PK
BP
CP

August 18, 1970

1

Co Rd "C"

X-Sections

Mc Knight to East

Sta + Δ - Elev.

BM 5.42 972.21

966.79

0+20

+33

+53

+73

1

+28

BM

5.75 966.46

966.45

August 18, 1970

2

Lt

Spike in PP SE Cor

65.6	65.4	65.1	64.5	64.6	64.9
6.6	6.8	7.1	7.7	7.6	7.3
100	84	61	36	23	

71.9	71.2	70.9	69.8	65.26	65.27	64.7	64.9
0.8	1.0	1.3	24	695	6.94	7.5	7.3
74	61	48	32	30	25	19	
			Wall	Sidewalk			

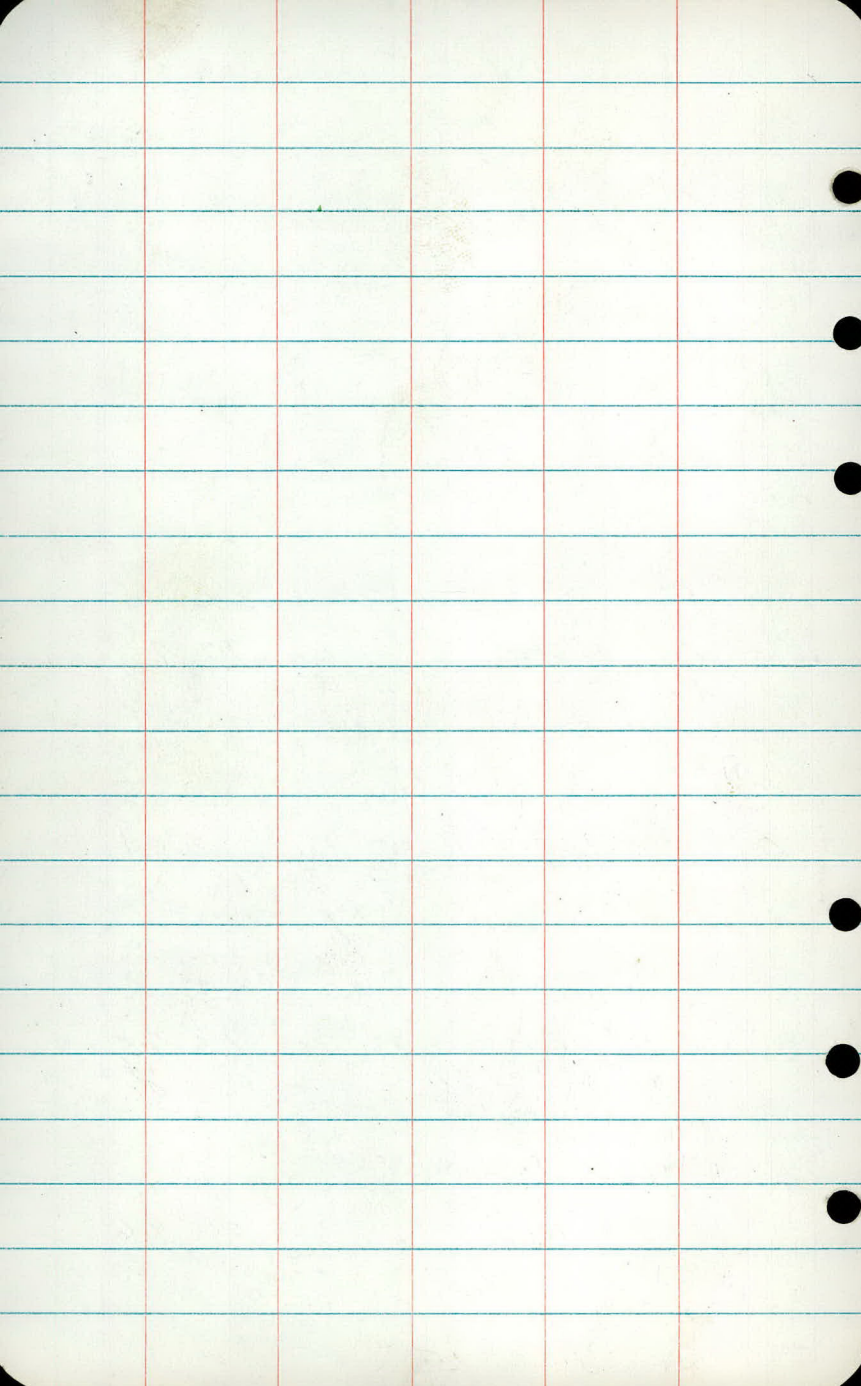
71.9	71.3	71.1	70.0	65.32	65.29	64.5	64.9
0.3	0.9	1.1	2.2	6.89	6.97	7.7	7.3
60	47	39	Wall	30	25	17	
Ho			32	Walk			

70.0	71.6	71.1	70.1	65.32	65.18	64.4	64.8
0.19	0.6	1.1	2.1	6.89	7.03	7.8	7.4
58	50	38	Wall	30	25	18	
Walk			32	Walk			

70.8	69.8	69.4	65.3	65.06	64.3	64.7
1.4	2.4	2.8	69.0	7.15	7.9	7.5
60	42	31	30	25	19	
		Wall	Walk			

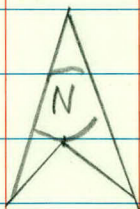
67.7	67.0	66.7	66.0	65.19	64.86	64.3	64.6
4.5	5.2	5.5	6.2	7.02	7.35	7.9	7.6
69	50	39	30	30	25	18	
			Wall	Walk			
			End				

Top Hyd by #2295



KP
DS
LPD
GA

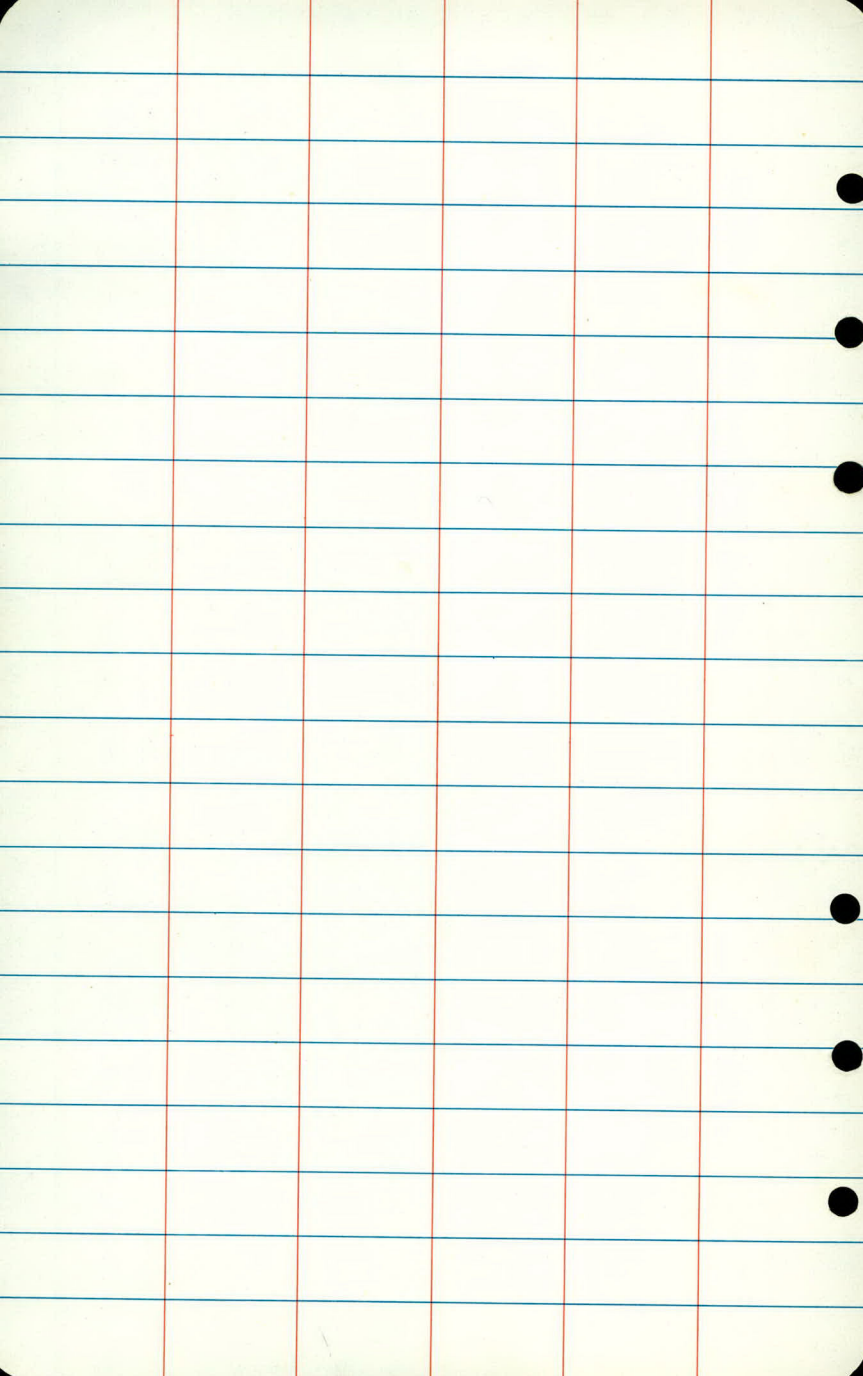
17 MAR 1977
SNOW 400



57+76.89

□ E Co. RD C

E McKnight Rd



W.S
K.G
R.J

11-17-76
CLEM: WINDY
39°

STADIA

McKNIGHT ROAD

LOW AREA

STA. 54-55

+

ELEVATIONS OF A MA & APRONS

↑
N

• 55

Y 54

SET INSTRUMENT

ON STA. 54+00. SET

PLATES ON ZERO AND

SIGHTED SOUTH.

0° 00' 00"

POINT	HORT. ANGLE	DISTANCE	ROD. IN. READING	ELEVATION
Bm	5.50	968.60		963.1
1	83°	50'	5.23	63.37
2	85°	70'	5.91	62.69
3	86°	95'	5.04	63.56
4	104°	105'	5.05	63.55
5	109°	90'	6.15	62.45
6	117°	65'	6.14	62.46
7	133°	45'	5.69	62.91
8	146°	60'	5.76	62.84
9	130°	80'	5.79	62.81
10	119°	105'	5.63	62.97
11	116°	135'	5.37	63.23
12	154°	90'	5.54	63.06
13	131°	125'	5.51	63.09
14	122°	185'	5.55	63.05
15	123°	220'	5.48	63.12
16	124°	240'	5.03	63.57
17	123°	295'	4.03	64.57

W.S
K.G
R.J

11-11-76
CLEAR, WINDY
38°

2.

STA 55+00 (TOP P.K.)

STA	+	π	-	ELEV
Bm	4.18	942.35		938.17

LT. 17
46+48

0.64

LT. 160
44+15

12.15

LT. 165
44+21

12.31

T.P.

2.55

939.80

39.9

WIS
K.6
R.I

11-17-76
CLEAR WINDY
41°

3

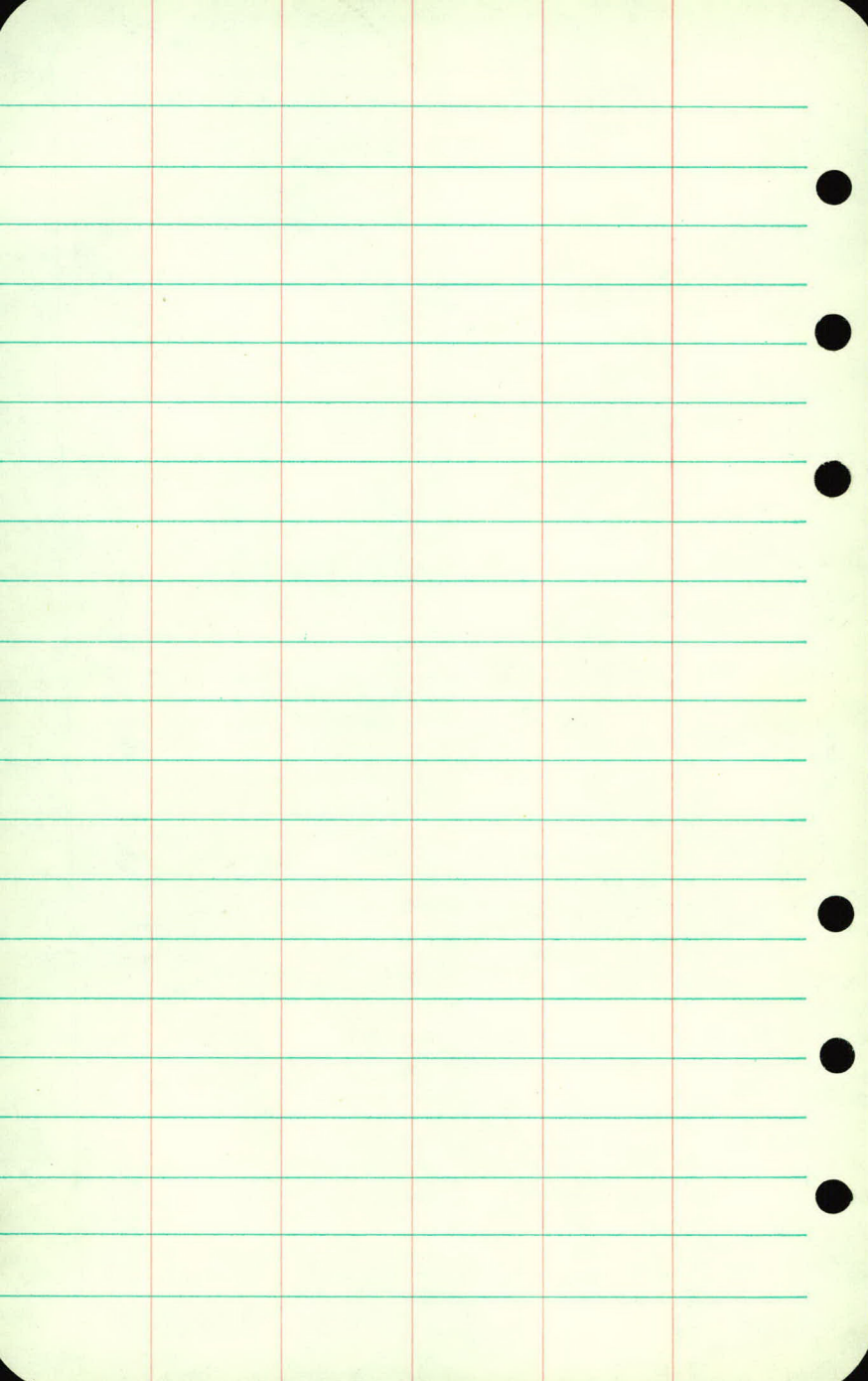
TOP HYD NE CORNER 13th MCKINLEY

TOP OF M.A

F.L OF APRON

F.L OF APRON

TOP P.K STA. 46+00



McKNIGHT RD

HWY 36

TO

CORR 'C'

INDEX

TOPOGRAPHY 2-12

CROSS SECTIONS

+50

LT

RD
39

C

RD
24

RT

32

£ 4' DITCH
125RD
37RD
24£ 10' DITCH
39WOODS
39£
10' CREEK
99+92 BIT
33.36+85 PP CAIDE
31

+50

31

£ 4' DITCH
138RD
33RD
24£ 10' DITCH
42WOODS
48£
8' CREEK
123

+50

30+00

£ 8' DITCH
144RD
33RD
24£ 10' DITCH
43WOODS
50 → E 149

W.S
K6
EW

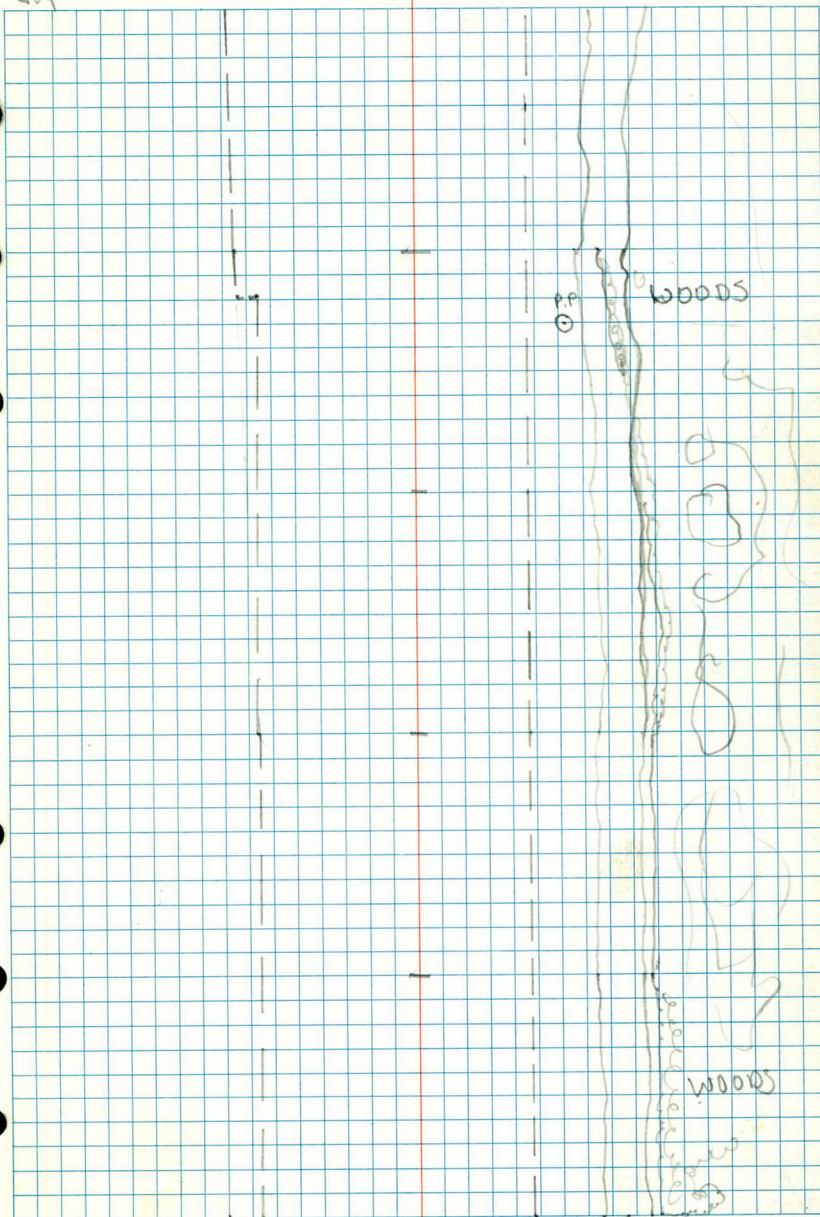
LT

C

RT

8-26-16
CLIMATE: 87°

2



35	10' DITCH 92	LT	RD 32	RD 24	RT 10' DITCH - CREEK 47'	WOODS 56
				+96	5' WILLOW 40	
+67	ERAD 32	+56	P.O.R. 35			
	+50					
+43	P.P. RURAL LIGHT 74	+46	P.O.R. 41			
+37	N END 36" CMP 100					
		+26	B.G. RAD 84	+36	P.R. 49	
+03	N SIDE RAD 61-100+					
34			RD 24	10' CREEK 55	WOODS 55	PITCHED MIDGE 36 - OTHER 10' DITCH
+99	SOUTH SIDE MEDIAN 61-100+					
+80	E MED 27-61	+64	S END 36" CMP 105	+92	P.P. RURAL LIGHT 30	
+76	ERAD 134	+77	MED 24-62			
+60	MEDIAN 24-46	+60	P.O.R. 80			
	+50					
+40	MEDIAN 24-31	+45	P.P. RURAL LIGHT 80			
+40	P.O.R. 59	+37	B.G. MEDIAN 27			
+20	P.O.R. 46					
33	4' DITCH 115	RD 41	RD 24	12' DITCH 43	WOODS 71	10' CREEK 76
32 + 50		RD 39	RD 24			

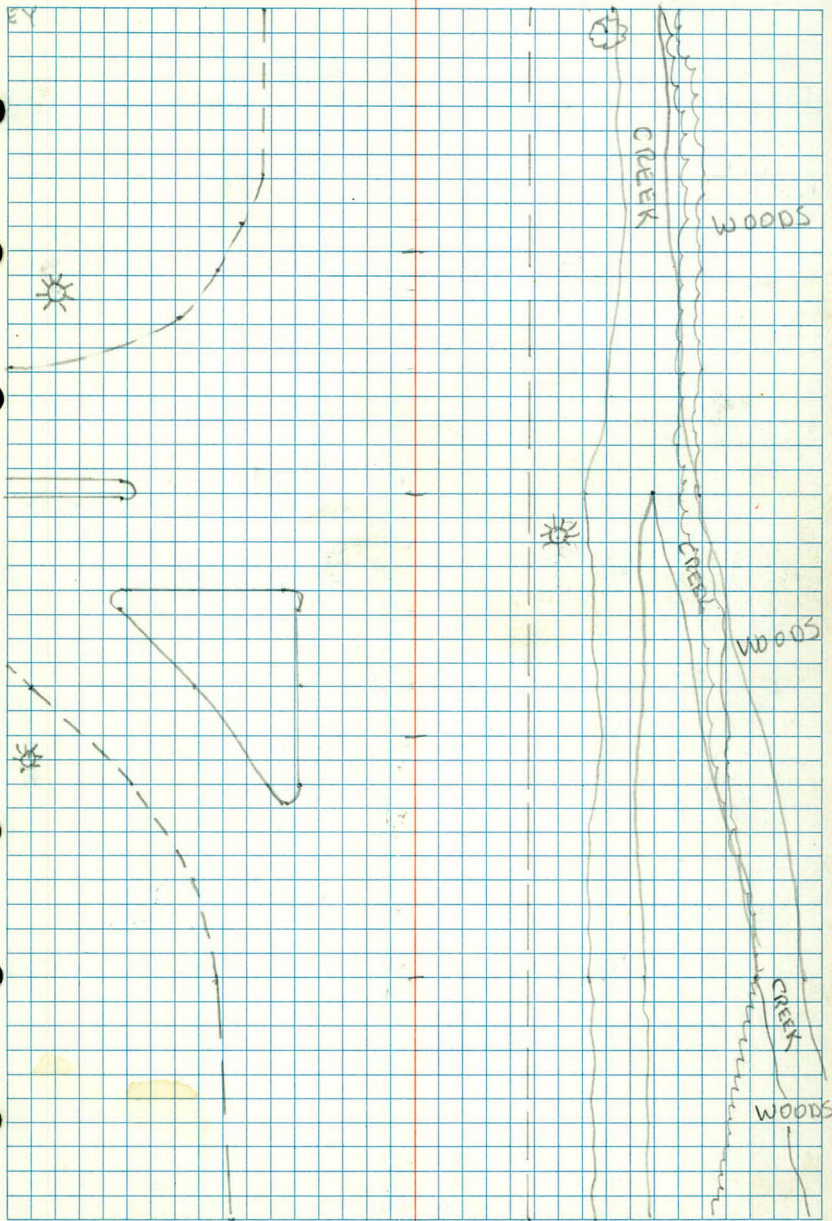
W.S
K.G
R.J

LT

C

RT

826-76
01:42
8-27-76 3



+50

LT

E

RT

^{BL}
 +48 30" CONC PIPE
 79

PARKING LOT

+41 77
 +44 BL RAIL
 26

PHONE BOOTH 4'x4'

+37 62+40 SIGN
67+30 E GUARD RAIL
58+35 NO COX PARKING LOT
59-70
 +20 BL BL-12 CURB
 26
+26 E BIT CURB
57

37

 E
 6' DITCH
 87
RD
25RD
24BIT CURB
56GUARD RAIL
58
 +70 BL BIT CURB
 56
+41 BL GUARD RAIL
58+39 BL BIT CURB
59

+50

+39 BL BIT SPILLWAY
56+36 BL S.C. PK
75+38 E 8' BIT SPILLWAY
38+37 E APRON
48+35 BIT
32+35 P.P.
30+40 BL 4' BIT SPILLWAY
24+30 BL 6'x9' ARCH PIPE (APRON)
49+11 E WOODS
37-50+27 E BIT SPILLWAY
44

36

 E
 8' DITCH
 90
RD
33RD
24
WOODS
37
 E
 6' CREEK
 55
+74 BL WOODS
41-52+54 E WOODS
56

+50

RD
24
 E
 7' CREEK
 50

35

 E
 10' DITCH
 92
RD
32RD
24
 E
 10' DITCH : CREEK WOODS
 47 56

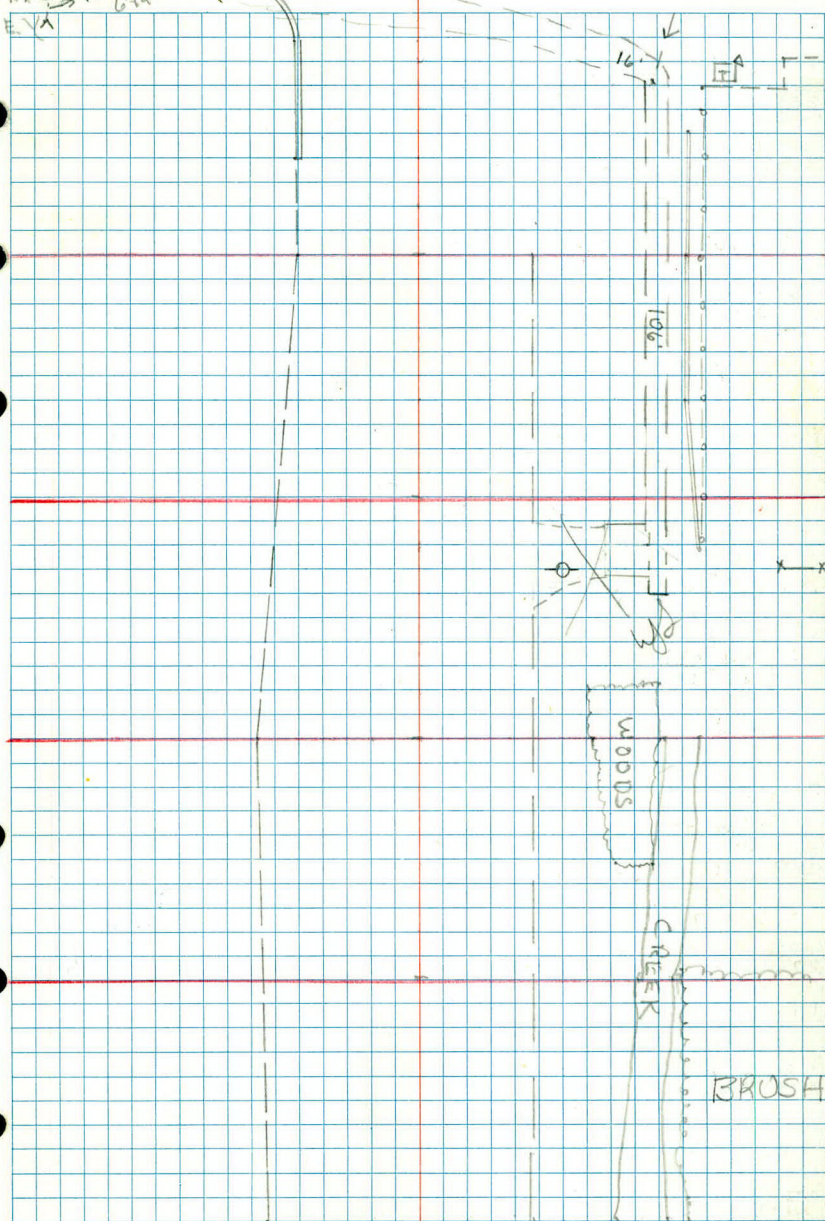
W.S.
K.G.
R.I. → TO ARCHA
6' x 9'

LT

Q

8-27-16
RT CL: 73°

4



LT

40 £10' DITCH 78
WOODS 69

RD 21

RD 23

£4' DITCH 32

+57 5" POPULAR 42

+57 WOODS: BRUSH 54

+66 P.P 28

+50

39

B6 WOODS 65

RD 21

RD 23

£5' DITCH 35

+94 BIT RD 21

+78 E B6-18 CURB 26

+56 E RAD 26

+50

12' CMP

+45 36

+33 P.O.R 27

+45 E RAD 24

+45 E CONC CURB 24

+28 HVD 43

+28 P.O.R LIGHT 56

+24 B6 RAD 46

+24 CB 48

+33 PULLBOX 41

+36 P.O.R 34

+26 B6 RAD 57

+09 M.A. (20) 35

38

+99 M.H 3

+75 E RAD 57

+69 P.O.R 39

+69 PULLBOX 55

+55 P.O.R 30

+60 ARCH LIGHT 38

+80 B6 RAD CONC OR 66

+66 CONC DRIVE 75

+73 P.O.R 29

+80 E RAD 47

+80 CB 49

37+50

+57 B6 B6-18 25

+57 B6 RAD 25

WS
KG.
RJ.
EX.

H.

Q

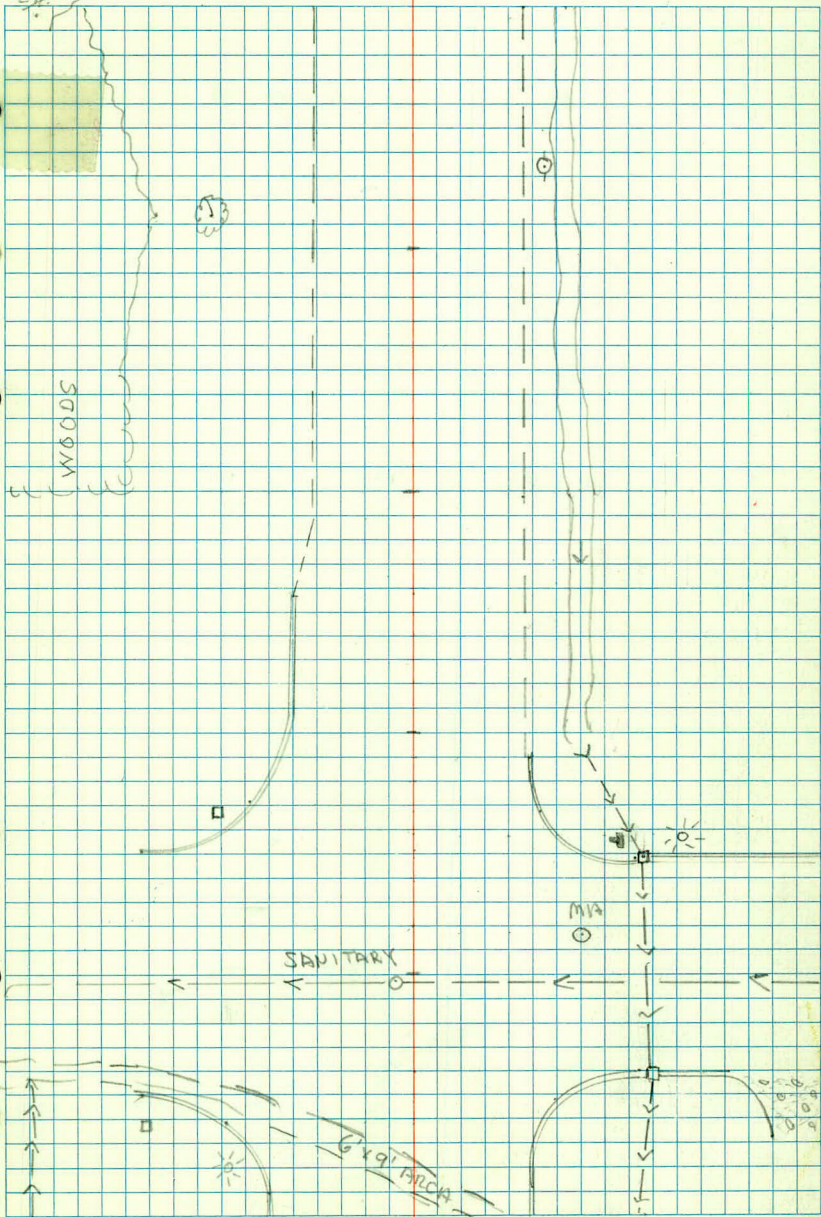
8-1-76

8-27-76

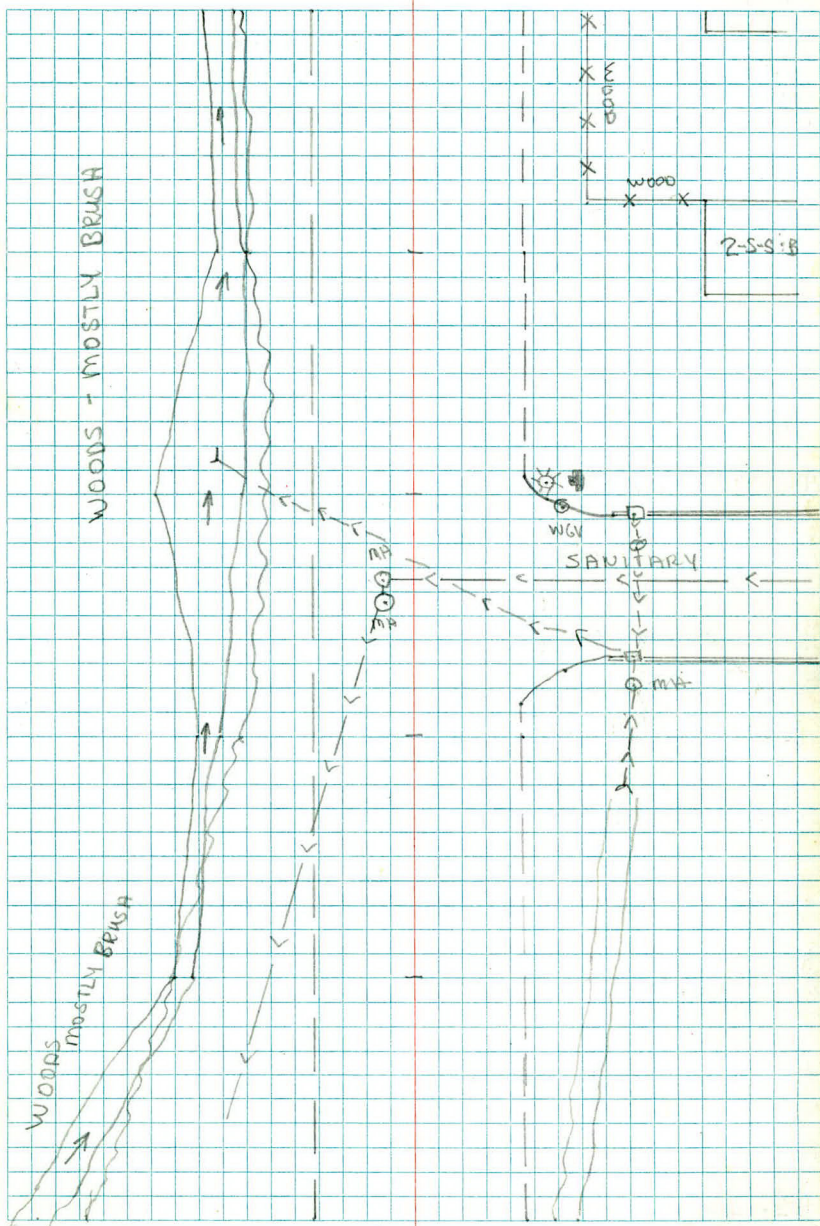
RA

CLR. 730

5



	LT		RT
+50	46' DITCH BRUSH 43 36	RD RD 21 23	SW COR GARAGE +46 62
		+21 COR 4' WOOD FE 37-62	NW COR HO +21 62
42	46' DITCH BRUSH 38 35	RD RD 21 23	2-S-B SW COR HO +92 62
			+53 HYD 34
	24" R.C.P. +57 41	E RAD BIT CURB +53 23	
			ARCH LIGHT POLE +52 28
+50	E 15' DITCH 43	+46 B. BL-18 42-E	+49 RD 28 +49 W6V 36
		+46 CB 46	+46 B. RAD BIT CURB 42
	41 CB +32 MH 61	+39 MH 46	+16 B. BL-24" CURB 42 +16 E RAD 42
+28 MH 6		+16 CB 46	+13 P.O.R 32 +10 MH 46
		+07 B. RAD (BIT CURB) 23	
41	45' DITCH WOODS BRUSH RD 43 37 21	RD 23	18" R.C.P. +90 44
+50	WOODS 45' DITCH 50 47		
40	WOODS 41' DITCH RD RD 69 78 21 23	44' DITCH 32	



RT

RD

23

$$\begin{array}{r} 23 \\ + 89 \\ \hline \end{array}$$
$$+84 \quad \frac{\text{EBIT CURB}}{23}$$

+69	<u>WOOD POST</u>	+78	<u>ELPH</u>
	60		58

$$+84 \frac{E \text{ RAD}}{23}$$
$$+79 \quad \begin{array}{r} \checkmark \\ \text{P.O.} \\ 30 \end{array}$$
$$\begin{array}{r} + 82 \\ \hline 42 \end{array}$$

+55 @ 24' DIRT ENT

✓ B RAD: BIT
+76 37

$\begin{array}{r} \text{CURB} \\ + 76 \\ \hline \end{array}$
 $\begin{array}{r} \text{BG-18 CURB} \\ 37 \text{ EF} \end{array}$

+50	+51	$\frac{1000}{59}$
-----	-----	-------------------

$$\begin{array}{r} \checkmark CB \\ +76 \quad \underline{47} \end{array}$$

✓
B. BL-18 CURD
746 38

✓ WOOD POST
+ 45 59

✓ P.O.R
+44 31

+ 46 ERRAD (BIT CURR)
38

$$\frac{2'7'' \times 4'2'' \text{ APPROX}}{165}$$
$$\begin{array}{r} + 35 \\ \hline 18 \text{ R.C.P} \\ \hline 39 \end{array}$$

✓
+ 37

8 RAD : BITCHES
23

$$\begin{array}{r} 27^{\circ} 14' 2'' \text{ APPROX} \\ + 15 \\ \hline 160 \end{array}$$

+10 COR DITCH
60 → W

14 31" x 20" ARCH R.C.F.
29

COR DITCH RD
47 22

$$\begin{array}{r} 120 \\ 23 \end{array}$$

31" X 20" ARC R. L.P	COR. 5' DITCH
79	35

+50	45' DITCH
	46

$$+13 \quad \frac{P.P}{27}$$

43	£ 6 ⁰	DITCH	RD	RD
	45		21	23

• $\pm 18'$ GRAVEL ENT
+ 82

$+70 \quad \frac{\text{COR FE}}{37}$
 $+71 \quad \frac{\text{COR FE}}{62}$

+65 E BRUSH
36 - 45

$$\begin{array}{r} + 68 \text{ NW COR GARAGE} \\ \hline 62 \end{array}$$

EWODFE
62

42+50	£ 6' DITCH	BRUSH RD	RD
	43	36	23

W.S
R.T
E.V

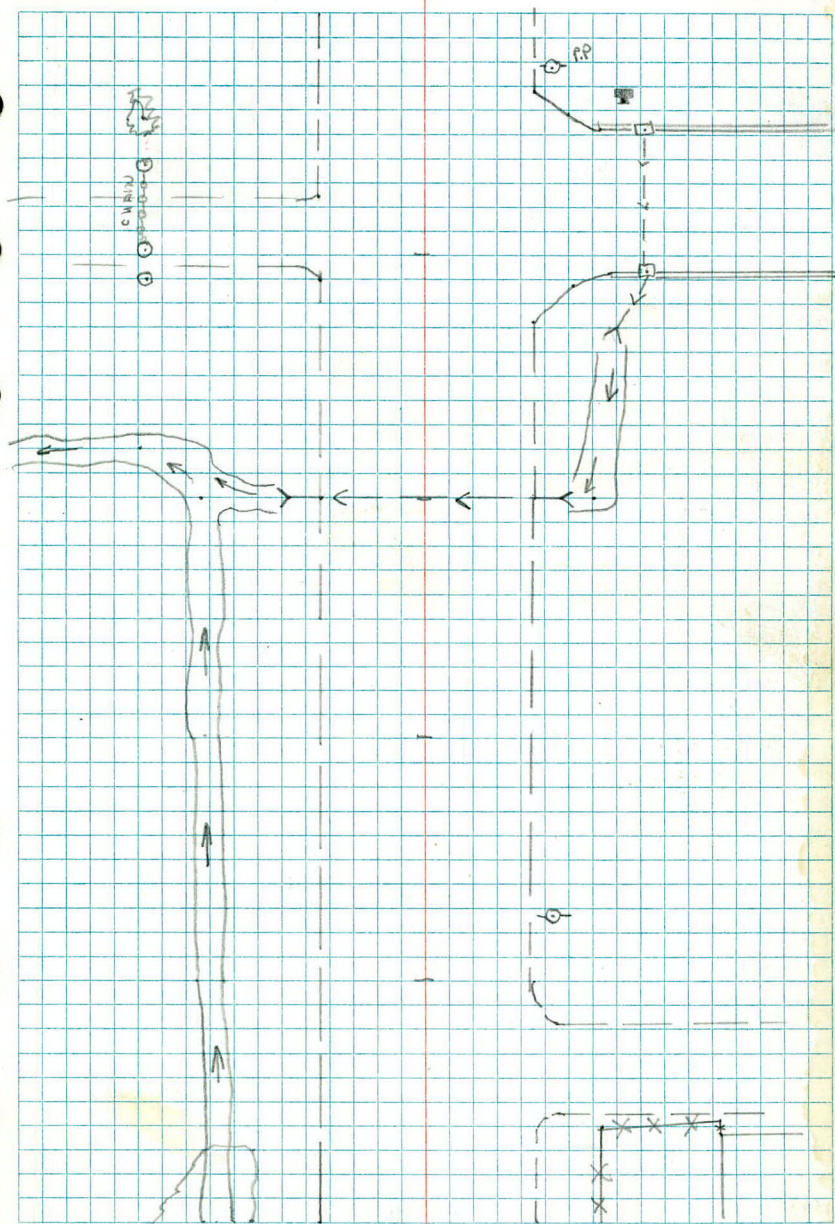
LT

C

RT

4-1-76
CL 70°

7



+50

LT

Q

✓

RT

+49 $\frac{G \text{ WIRE}}{26}$

47

✓
RD
22

✓
RD
23

+50

+48 $\frac{mit}{17}$

✓
+46 $\frac{PP}{25}$

46

✓
RD
22

✓
RD
23

+50

✓
+02 $\frac{3-6" \text{ WILLOW}}{64}$

45

✓
RD
22

✓
RD
23

W.S.
K.G.
B.R.
J.G.
X

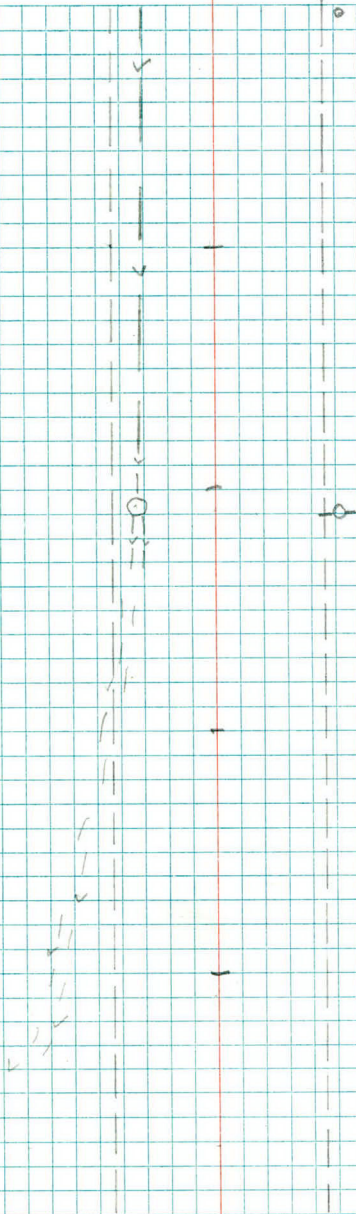
LT

C

RT

9-1-76
a: 72°

8



50	LT	✓ Q ✓	✓ RD	✓ FE	RT
		RD 22	RD 23	FE 32	
✓ +66 <u>GUIDE POLE</u> 36	✓ +80 <u>14" DRAIN</u> 51	✓ +71 <u>FE COR</u> 33	✓ +66 <u>PP</u> 25	✓ +68 <u>BIT</u> 59	
✓ +52 <u>COR LOT</u> 80		✓ +65 <u>BIT</u> 22	✓ +53 <u>BIT</u> 23	✓ +66 <u>FE COR</u> 36-53	
✓ +52 <u>MH</u> 15		✓ +49 <u>BIT COR</u> 54			
+50					
	✓ +25 <u>LOT</u> 65				
✓ +05 <u>2" APPLE</u> 45					
49	✓ LOT 56	✓ RD 22	✓ RD 23		
	✓ +86 <u>2" APPLE</u> 45				
✓ +68 <u>LOT</u> 56	✓ +69 <u>3" APPLE</u> 45				
+50					
	✓ +32 <u>24" GRAVEL ENT</u>	✓ +15 <u>BRAD</u> 23	✓ +15 <u>PP</u> 26	✓ +18 <u>MND</u> 35	
✓ +20 <u>LOT</u> 56-3W	✓ +15 <u>PP</u> 42	✓ +10 <u>WCU</u> 35	✓ +10 <u>P.O.R</u> 31	✓ +24 <u>CB</u> 22	
✓ +10 <u>TELE BOX</u> 28		✓ +06 <u>BRAD BIT CURB</u> 39	✓ +06 <u>B BL-18</u> 39-E		
48		✓ +05 <u>CB</u> 45	✓ +02 <u>MH</u> 57		
	✓ +89 <u>BACKSTOP (BB)</u> 79	✓ +99 <u>MH</u> 2			
✓ +87 <u>BACKSTOP (BB)</u> 70	✓ +78 <u>MH</u> 14	✓ +76 <u>CB</u> 45	✓ +76 <u>B BL-18</u> 40		
✓ +70 <u>BACKSTOP (BB)</u> 59	✓ +79 <u>BACKSTOP (BB)</u> 64	✓ +74 <u>P.O.R</u> 29	✓ +76 <u>BRAD + E BIT CURB</u> 40		
✓ +59 <u>BACKSTOP (BB)</u> 60		✓ +69 <u>BRAD</u> 23	✓ +69 <u>B BIT CURB</u> 23		
47+50		✓ +66 <u>PP</u> 26			

WIS.
KG
RJ.
E.X.

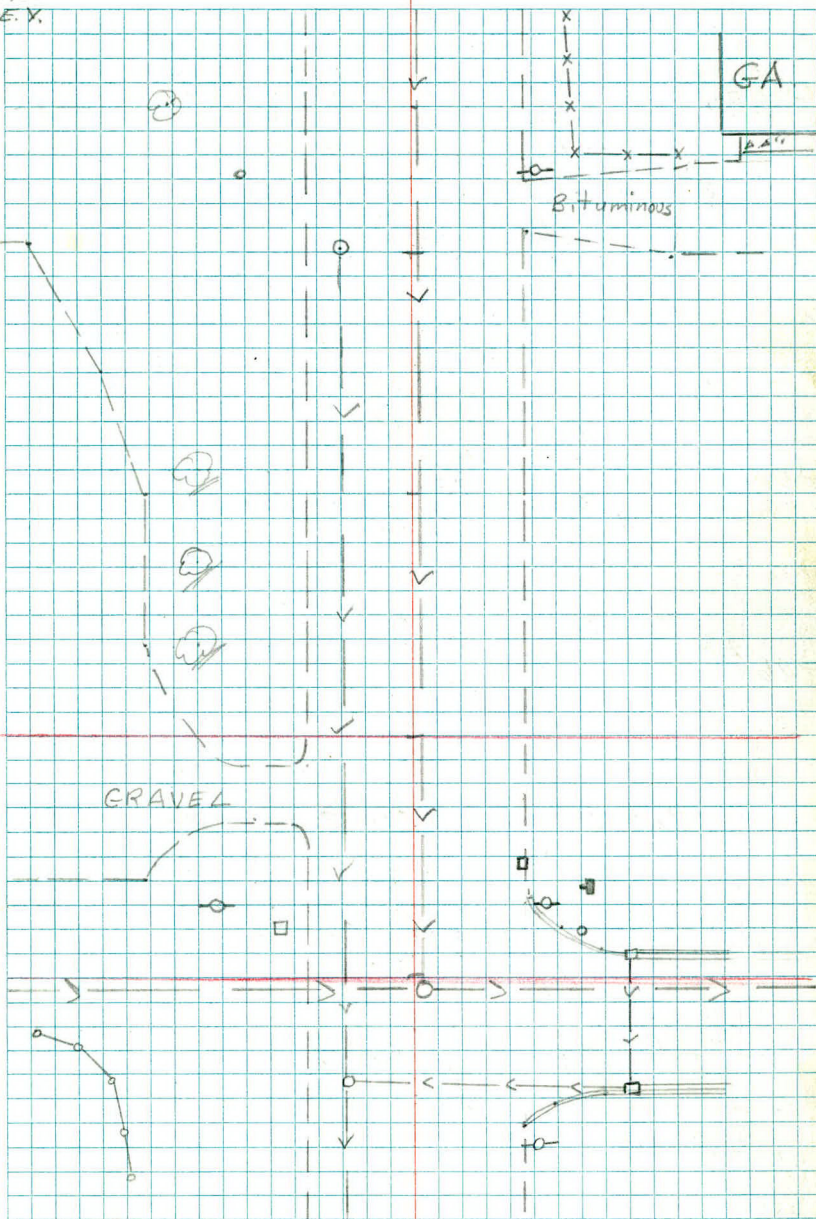
LT

Q

RT

9-1-76
CLIP 173°

9



+50

LT

C $\frac{B.t}{45}$
+50

RT

+50 $\frac{Cor Walk}{48}$ +36 $\frac{Cor Con}{34}$ +32 $\frac{Fe Cor}{33-44}$ +27 $\frac{Walk}{48}$
+12 $\frac{NW Cor Ho}{44}$ +23 $\frac{Cor Walk}{44}$ +26 $\frac{Cor B.t}{46}$
+17 $\frac{B.t Walk}{44-49}$ +10 $\frac{E 2' Walk}{24}$

52

 $\frac{Fe}{33}$ $\frac{Curb}{22}$ $\frac{22}{22}$ +17 $\frac{E Carb}{22}$ +87 $\frac{SW Cor Ho}{45}$ +72 $\frac{Hyd}{25}$ +87 $\frac{B 2' Walk}{24-26}$ +94 $\frac{SE Cor Ho}{49}$ +69 $\frac{14" Maple}{41}$ +55 $\frac{CB}{23}$ +66 $\frac{MH}{13}$ +65 $\frac{8" Mt. Ash}{40}$ +54 $\frac{ER @ CB}{22}$ +44 $\frac{POR}{24}$ +52 $\frac{Fe Cor}{33}$ +42 $\frac{POR}{28}$ +49 $\frac{Arc Lt}{25}$ +49 $\frac{ER}{23}$ +36 $\frac{BR}{35}$ +36 $\frac{CB}{39}$ +37 $\frac{MH}{11}$ +22 $\frac{MH}{E}$ +37 $\frac{BR @ CB}{40-42}$ +06 $\frac{ER @ CB}{39}$ +100 $\frac{POR}{25}$ +30 $\frac{MH}{34}$ +08 $\frac{ER @ CB}{40-42}$ +100 $\frac{POR}{28}$

51

+94 $\frac{BR}{22}$ +92 $\frac{BR}{23}$ +92 $\frac{MH}{14}$

+50

+52 $\frac{NW Cor Ho}{40}$ +35 $\frac{Cor Sign}{42}$ +30 $\frac{Cor Sign}{36}$ +42 $\frac{14" Oak}{62}$ +28 $\frac{SW Cor Ho}{40}$ +28 $\frac{Fe Cor}{32}$

50

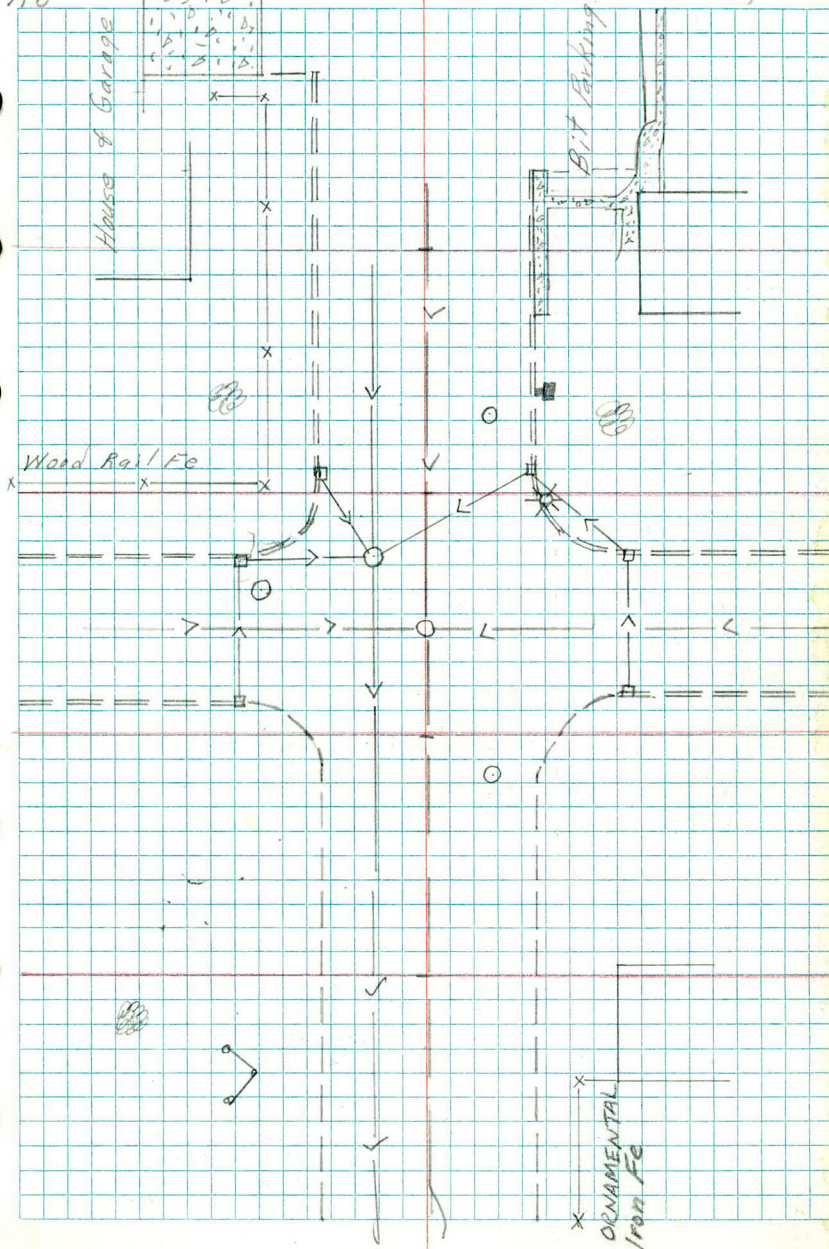
+24 $\frac{Cor Sign}{41}$

HK
HG
RJ

LT

C

Sept 2, 1976
RT clear Cool
Windy 10



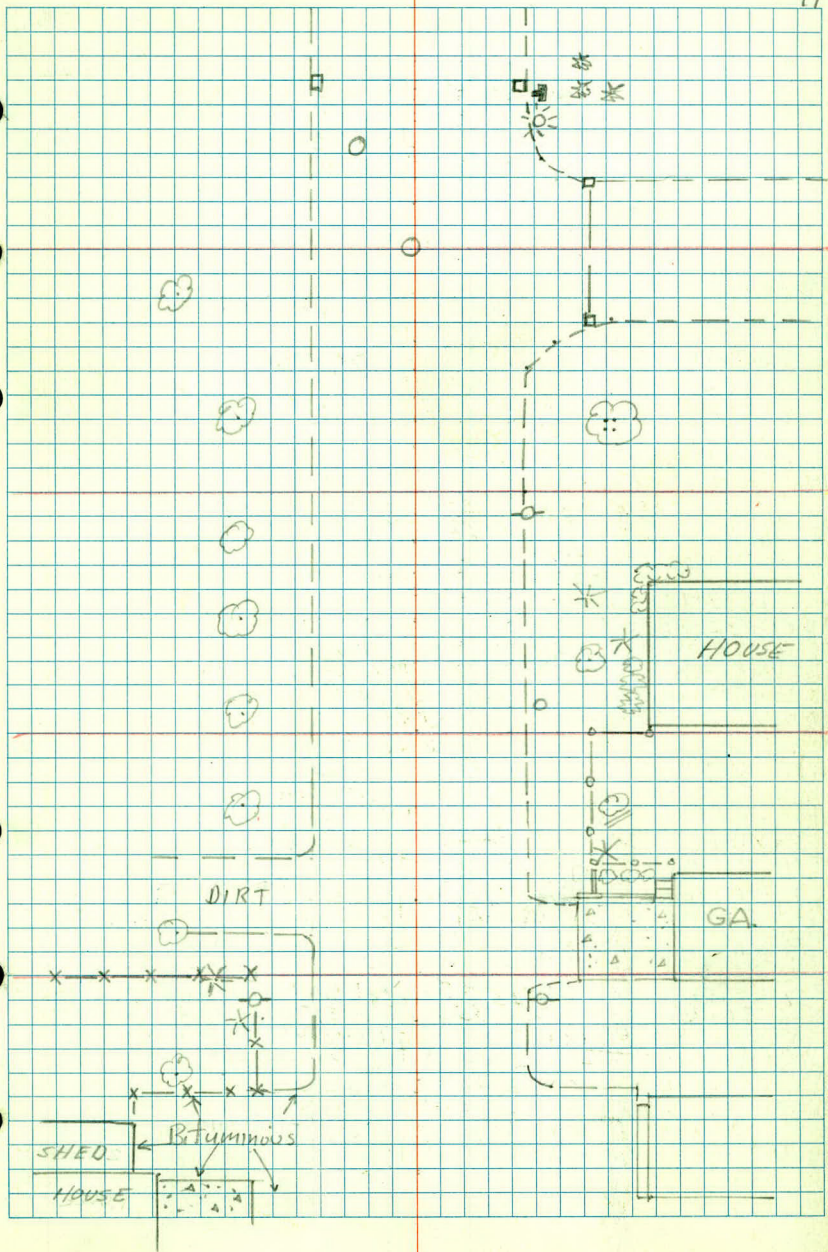
K.G.
R.T.
E.Y.

Lt.

Z

Rt

Sept. 2, 1976
CLEAR-WINDY
TEMP. 75° 11



4.

2

R1.

+51 $\frac{B. Rad.}{22}$	+156 $\frac{P.O.R.}{25}$	+160 $\frac{MH}{24}$	
		+58 $\frac{E. Rad.}{31}$	+58 $\frac{E. Rad.}{27}$
	+21 $\frac{18" Maple}{35}$	+50 $\frac{B. Rad.}{23}$	+50 $\frac{P. Park}{24}$
+11 $\frac{N.E. Cor. Ho.}{73}$		+12 $\frac{N.W. Cor. Ho.}{57}$	+18 $\frac{10' Bit. Ent}{22}$

57

Rd Rd
2222

		+87 $\frac{SW Cor Ho}{57}$	+92 $\frac{8" Maple}{38}$
+80 $\frac{24" Maple}{35}$	+57 $\frac{SE Cor Ho}{73}$	+83 $\frac{Cor 3' walk}{50}$	+85 $\frac{cor walk}{53}$
+69 $\frac{Cor. Cons}{83-71}$	+71 $\frac{2' X 4' Planter}{34-38}$	+67 $\frac{W50}{25}$	+73 $\frac{W50}{25}$
+46 $\frac{Cor Bit}{23-71}$	+57 $\frac{Cor Cons}{33-77}$	+48 $\frac{P.P.}{24}$	+54 $\frac{12" Pine}{50}$
		+43 $\frac{10" ELM}{32}$	+46 $\frac{W Cor Ho.}{54}$
			+46 $\frac{21" Maple}{42}$
	+34 $\frac{8" Apple}{52}$	+26 $\frac{23" Maple}{43}$	+30 $\frac{END Bit/Walk}{29}$
+21 $\frac{12" ELM}{32}$		+17 $\frac{E. cor walk}{43-46}$	+22 $\frac{Cor Ho}{54}$
		+107 $\frac{4 Conc Wall}{29-43}$	+12 $\frac{14" STP}{39}$

56

Rd Rd
22 22

+196 $\frac{4" Maple}{32}$		+86 $\frac{20" Maple}{42}$	+90 $\frac{4 Conc wall}{28-56}$	+98 $\frac{16' Bit Dr.}{22}$
+71 $\frac{4" Maple}{32}$	+76 $\frac{NE Cor Ho (SMALL)}{69}$	+70 $\frac{NW Cor Ho}{53}$	+86 $\frac{SW Cor Ho}{55}$	
+51 $\frac{12' Bit Ent}{22}$	+56 $\frac{SE Cor Ho}{69}$	+50 $\frac{SW Cor Ho}{53}$	+68 $\frac{Bit.}{51}$	+70 $\frac{wall (conc block)}{32-53}$

+37 $\frac{Lilac Hed}{31-75}$	+45 $\frac{P.P.}{33}$	+34 $\frac{1" Apple}{35}$	+41 $\frac{Bit.}{22-46}$	+41 $\frac{NW Cor Ho}{46}$
	+27 $\frac{6" STP}{34}$	+20 $\frac{1" Crab Apple}{34}$	+23 $\frac{P.P.}{25}$	

+104 $\frac{20" ELM}{55}$ +17 $\frac{Rose Bu.}{44}$ +17 $\frac{SW Cor Ho}{46}$ +18 $\frac{Rose Bu.}{45}$

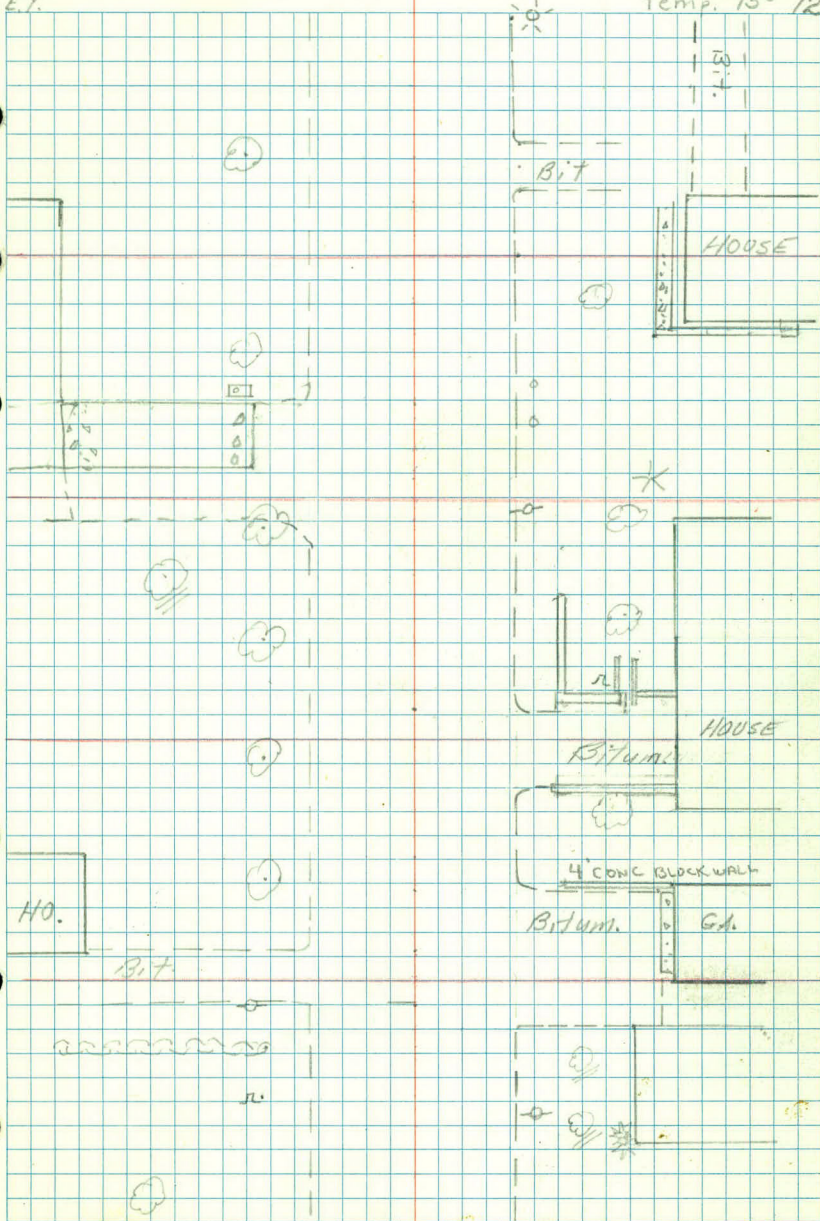
55

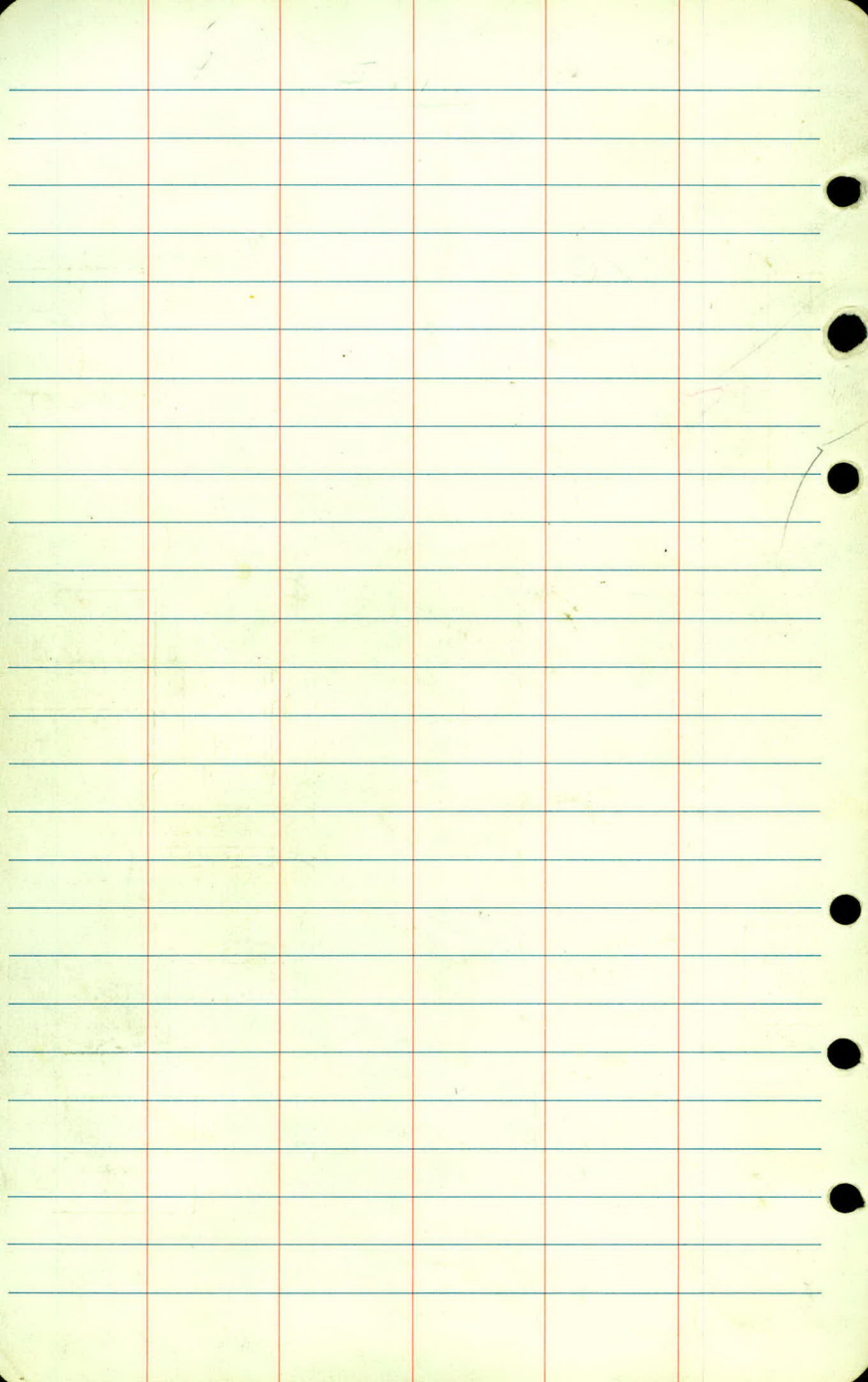
K.G.
R.J.
E.Y.

Lt.

2

Sept. 2, 1976
RT Clear & windy
temp. 75° 12



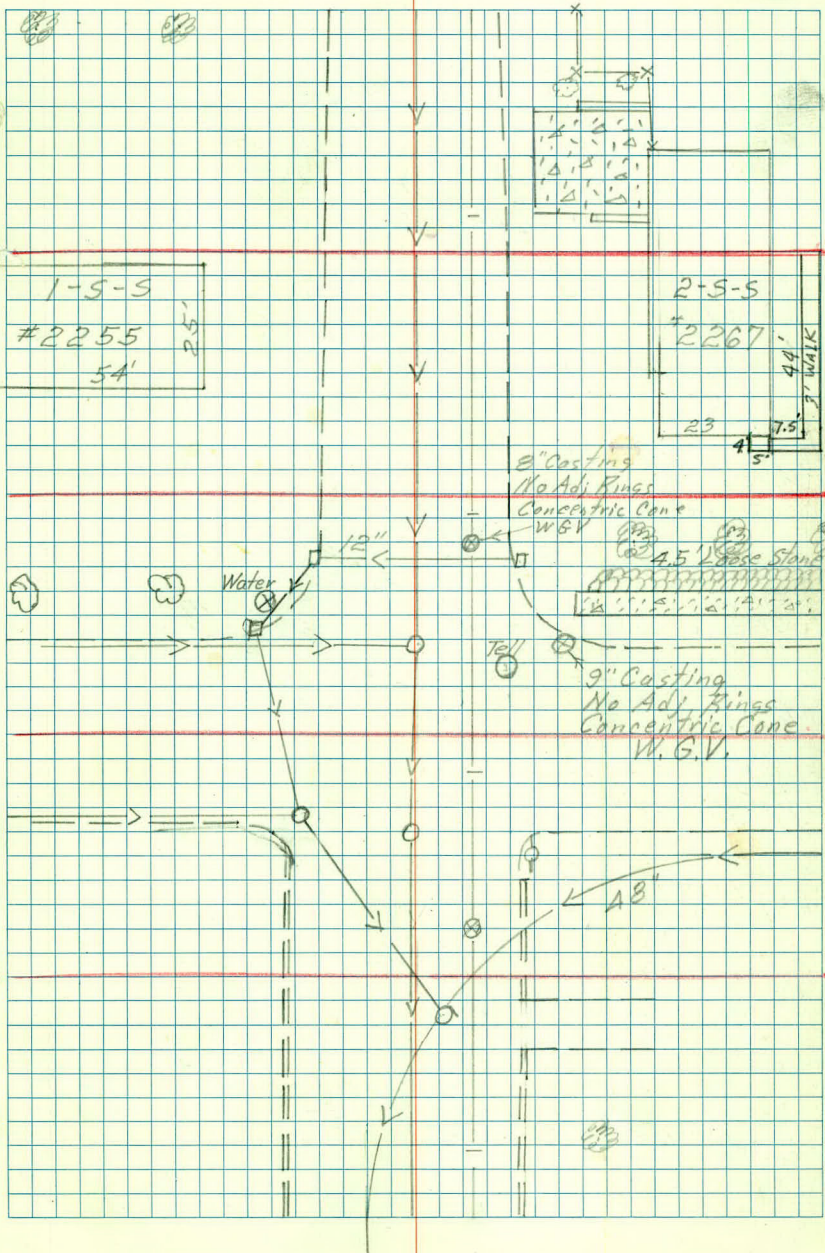


1
Mc Knight Road
"C" to Beam

Topography

1+50

✓ +46 $\frac{12" \text{ Apple}}{48}$	✓ +46 $\frac{3-5" \text{ Apple}}{77}$	✓ +36 $\frac{\text{Arbervida}}{45}$	✓ +37 $\frac{\text{Fe. Cor.}}{34+49}$
1	✓ +97 $\frac{\text{NE Cor. Ho}}{43}$	✓ +30 $\frac{\text{Wall}}{34-49}$ ✓ +20 $\frac{\text{N.W. Cor. Ho.}}{49}$ ✓ +18 $\frac{\text{Bit}}{20}$	✓ +34 $\frac{\text{Arbervida}}{35}$ ✓ +30 $\frac{\text{CONC. DR.}}{26-49}$ ✓ +21 $\frac{\text{B. Fe.}}{50}$ ✓ +108 $\frac{\text{CONC. DR.}}{26-49}$ ✓ +107 $\frac{\text{Steps}}{37-48}$
	✓ +72 $\frac{\text{SE Cor. Ho.}}{43}$	✓ +62 $\frac{\text{SW Cor. Ho.}}{51}$	✓ +14 $\frac{\text{Tel/MH}}{19.5}$
		✓ +40 $\frac{10" \text{ E/m}}{88}$	✓ +42 $\frac{\text{ER}}{20}$ ✓ +25 $\frac{\text{POR}}{26}$
		✓ +40 $\frac{\text{MH}}{12}$	✓ +40 $\frac{12" \text{ E/m}}{66}$ ✓ +40 $\frac{10" \text{ E/m}}{46}$
✓ +37 $\frac{\text{CB+ER}}{20}$	✓ +31 $\frac{8" \text{ ASA}}{51}$ ✓ +31 $\frac{14" \text{ ASA}}{85}$		✓ +36 $\frac{\text{CB}}{22}$
✓ +22 $\frac{\text{CB}}{33}$	✓ +27 $\frac{\text{POR}}{25}$	✓ +27 $\frac{\text{W. MH}}{31}$	✓ +30 $\frac{\text{Dep. Wall}}{36}$
	✓ +20 $\frac{\text{BR}}{44}$		✓ +25 $\frac{\text{Cor. Walk}}{33}$
0 ✓ +82 $\frac{\text{ERAD}}{37}$	✓ +80 $\frac{\text{P.O.R.}}{29}$	✓ +84 $\frac{\text{MH}}{24}$	✓ +18 $\frac{\text{BR}}{44}$
✓ +74 $\frac{\text{BL RAY}}{22}$	✓ +79 $\frac{\text{E. Bit Curb}}{26}$	✓ +80 $\frac{\text{MH}}{1}$	✓ +80 $\frac{\text{ER}}{27}$
		✓ +70 $\frac{\text{BR}}{22}$	✓ +75 $\frac{\text{PP}}{24}$
	✓ +42 $\frac{14" \text{ Maple}}{35}$		✓ +60 $\frac{\text{MH}}{11}$
		✓ +42 $\frac{\text{MH}}{6}$	
		✓ +40 $\frac{10" \text{ Ent Bit}}{1}$	
	✓ +03 $\frac{14" \text{ Maple}}{35}$	✓ +16 $\frac{3" \text{ Maple}}{38}$	
0-100		✓ Curb 22 22	



4

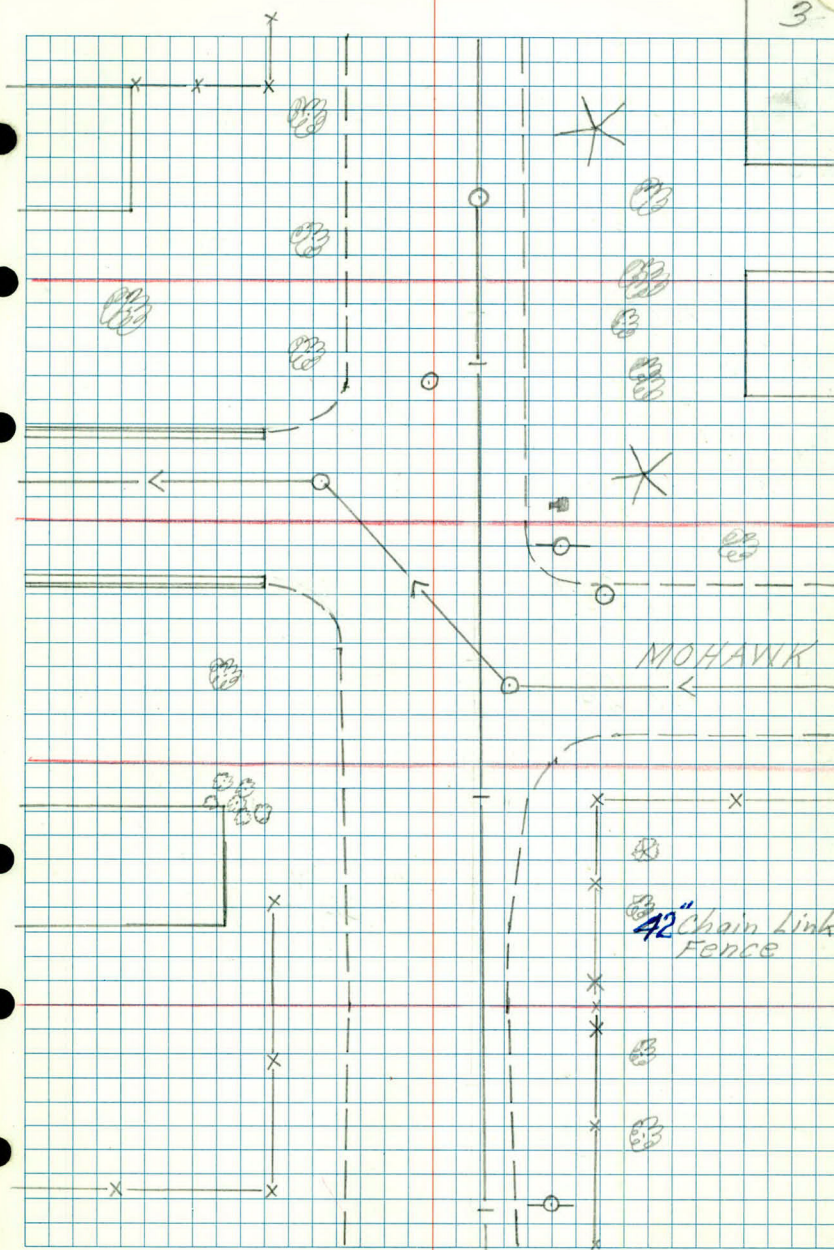
Fe	Bit
34	18 18

+90	NE Cor Ho	+Cor Fe	+81	B"P	
	63	34		34	
+84	6" Ash		+74	SW Cor Ho	
	26			65	
+64	SE Cor Ho		+67	6" Ash	
	63			45	
+44	18" Birch	+58	5" Linden	+67	MH
	63		25		9
+35	5" Ash	+41	3" Ash	+52	NW Cor Ho
	26		40		65
+27	ER	+24	POR	+51	6-3" Birch
	18		22		44
+29	MH	+26	SW Cor Ho	+30	Tw 4" Birch
	1		65		43
+19	B-B 18 C. Curb	+10	10" P		
	← 33 @ BR		44		
3	+08	MH	+03	Hyd	+00
	23		26		ER
+87	B-B 18 C. Curb	+87	BR	+91	POR
	← 35 @ ER		36		24
+69	3" Maple	+74	BR	+95	7" Beach
	43		19		64
+47	Bush	+56	ER	+95	PP
	43		38		27
+42	Bush	+51	POR	+66	MH
	41		26		16
+42	Bush	+43	BR	+43	Fe Cor
	46		20		34
+39	Bush	+40	36	+41	NE Cor Ho
	40		44		44
+16	SE Cor Ho	+19	1" Maple	+32	Pine Bush
	43		44		44
+21	E Fe	+17	Bit	+10	Gate
	33		16		34
2	Fe	+17	Bit	+90	1" Apple
	33		17 16		44
+61	Cor W. W. Fe	+71	Beg Bush	+86	34
	33		34		34
				+59	PP
					25

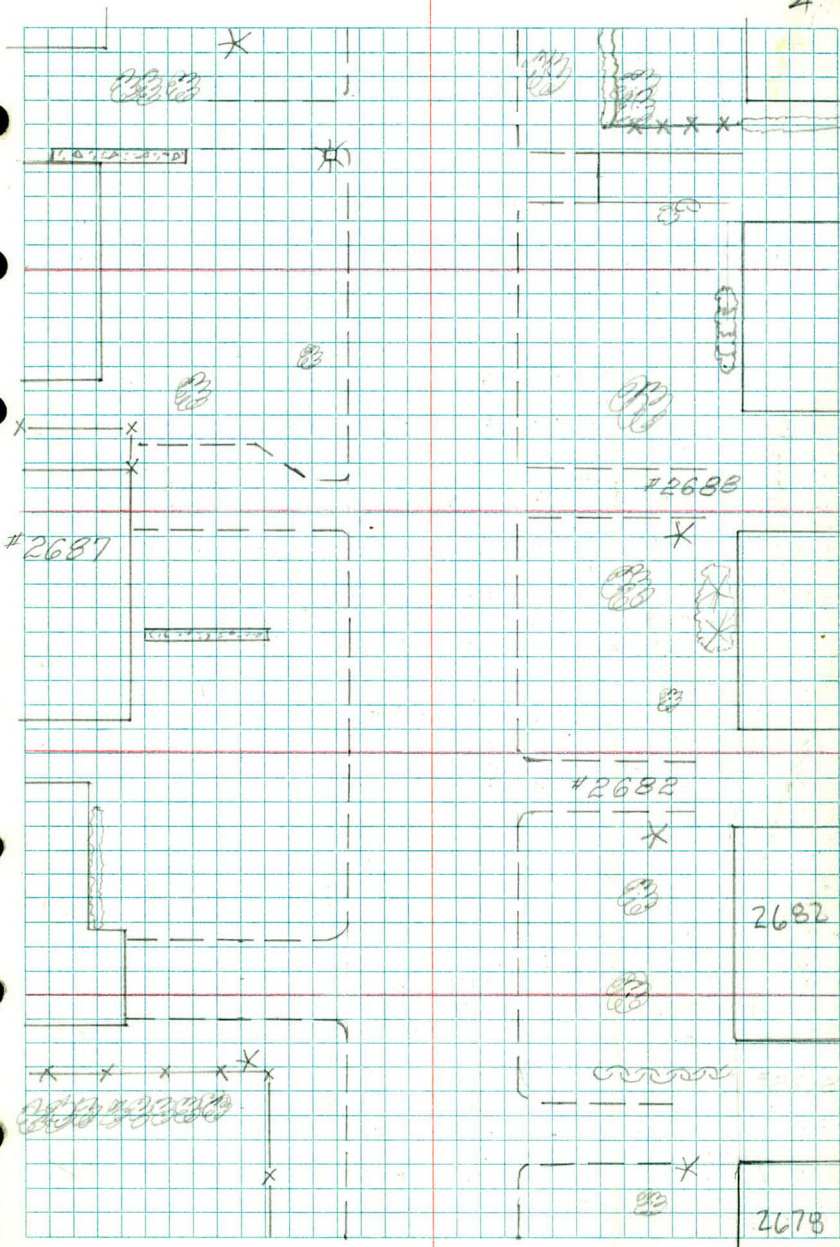
FK Copied

8-26-1976

3



6+50	+46 <u>SE Cor Ho</u> 68	+37 <u>12" Birch</u> 43	+41 <u>9" Ash</u> 24
+30 <u>£ Ent</u>	+47 <u>2" P</u> 41	+35 <u>SW Cor Ho</u> 66	+30 <u>BLFE (wood)</u> 36-64
	+38 <u>Apple trees</u> 64-58-52	+34 <u>8" Birch</u> 43	+30 <u>BL HEDGE</u> 64 → E
+23 <u>Lite</u> 21	+23 <u>£ 3' SW</u> 79-52	+11 <u>Bush</u> 49	+30 <u>BG HEDGE</u> 36
	+22 <u>NE Cor Ho</u> 69	+13 <u>Hedge</u> 51-56	+19 <u>£ 10' Conc En</u> 35
6		+10 <u>NW Cor Ho</u> 65	
	+77 <u>SE Cor Ho</u> 69		+95 <u>£ SARB</u> 62
+82 <u>4" Ash</u> 25	+67 <u>Fe Cor</u> 64		
	+75 <u>5" Maple</u> 50	+72 <u>18" Elm</u> 44	+80 <u>BG SARB</u> 62
+59 <u>Bit</u> 28	+64 <u>Bit</u> 61-37	+71 <u>SW Cor Ho</u> 65	
	+59 <u>NE Cor Ho</u> 63	+54 <u>£ Ent</u> Gravel	
+52 <u>£ Ent</u> Bit	+59 <u>B Fe</u> 64	+46 <u>NW Cor Ho</u> 64	
	+24 <u>£ 3' SW</u> 60-34	+38 <u>EP Bush</u> 59	+45 <u>1" P</u> 52
		+34 <u>14" Maple</u> 41	
	+107 <u>S.E. Cor Ho</u> 63	+11 <u>2" Apple</u> 50	+21 <u>B P Bush</u> 59
5		+05 <u>SW Cor Ho</u> 64	
	+94 <u>NE Cor Ho</u> 72	+85 <u>E Hedge</u> 34	+93 <u>£ Ent</u>
		+85 <u>NW Cor Ho</u> 63	
	+89 <u>E Bush</u> 70	+71 <u>8" Maple</u> 43	+83 <u>2" P</u> 47
+63 <u>NE Cor Ga</u> 72-64		+50 <u>8" Elm</u> 41	
	+62 <u>B Bush</u> 70	+33 <u>Hedge</u> 33-64	+41 <u>SW Cor Ho</u> 63
+53 <u>£ 16 Ent</u> Bit		+21 <u>£ Ent</u>	
	+44 <u>SE Cor Ho</u> 64	+15 <u>NW Cor Ho</u> 64	+13 <u>1" P</u> 53
+26 <u>8-8" Pop</u> 83-45	+37 <u>1" P</u> 38	+07 <u>4" Elm</u> 46	
	+34 <u>Cor WW Fe</u> ← 34		
4			



9	LT	£	RT
		RD 17	RD 19
		SW COR HO +99 66	6" ASH +97 28
		B-W.FE-E. +88 65	MH +90 11
#27	27 £18' CONC ENT	SE COR HO +89 66	+79 £10' BIT ENT
+50	+71 26	8" ASH +62 28	NW COR HO +69 67
	PP +48 28		
NE COR HO +43 68	£18' BIT ENT #2723 +33	BUSH +27 39	SW COR HO +29 67
8	2" MAPLE +14 48	RD RD+16 £16 BIT ENT	3-6" BIR +47 51
COR FECL. +74 71-101	E FECL. +85 71	1" PINE 17 +84 49	NW COR HO +04 67
NE COR HO +69 70	B FECL. +69 71	SECOR HO +85 68	PINE BUSH +98 59
#2709	£17' CON ENT +61 23	4" MAPLE +84 27	
+50	E PINE BUSH +50 62	2-5" BIR +83 48	3-3" CAT +64 67
2" PINE +44 36	2" PINE +48 40	3 W.FE +60 65-E.	5" MAPLE +68 38
B PINE BUSH +28 62		#2706 £10' BIT ENT +54	
7" MAP +20 25	B PINE BUSH +24 37	E PINE BUSH +32 37	NW COR HO +44 66
2" PINE +08 39	2" PINE +11 36	2-2" BIR +16 48	10" CAT +05 44
7	PP +03 28	SECOR HO +09 70	3-6" ASH +10 51
£ ENT BIT		RD 17	8" ELM +35 28
+93		RD 17	SW COR HO +94 66
		RD 17	FE +94 69
		RD 17	WSD +94 16
		RD 17	£10' GRAVEL ENT
+81 MH 1	1" PINE +79 49	DECOR HO +84 69	NW COR HO +76 66
+57 1" BIR 47	7" MAPLE +66 47	TW2' P +78 41	6" ELM +58 44
6+50			E HLOW +67 36
			B" P +73 38

W.S
B.J

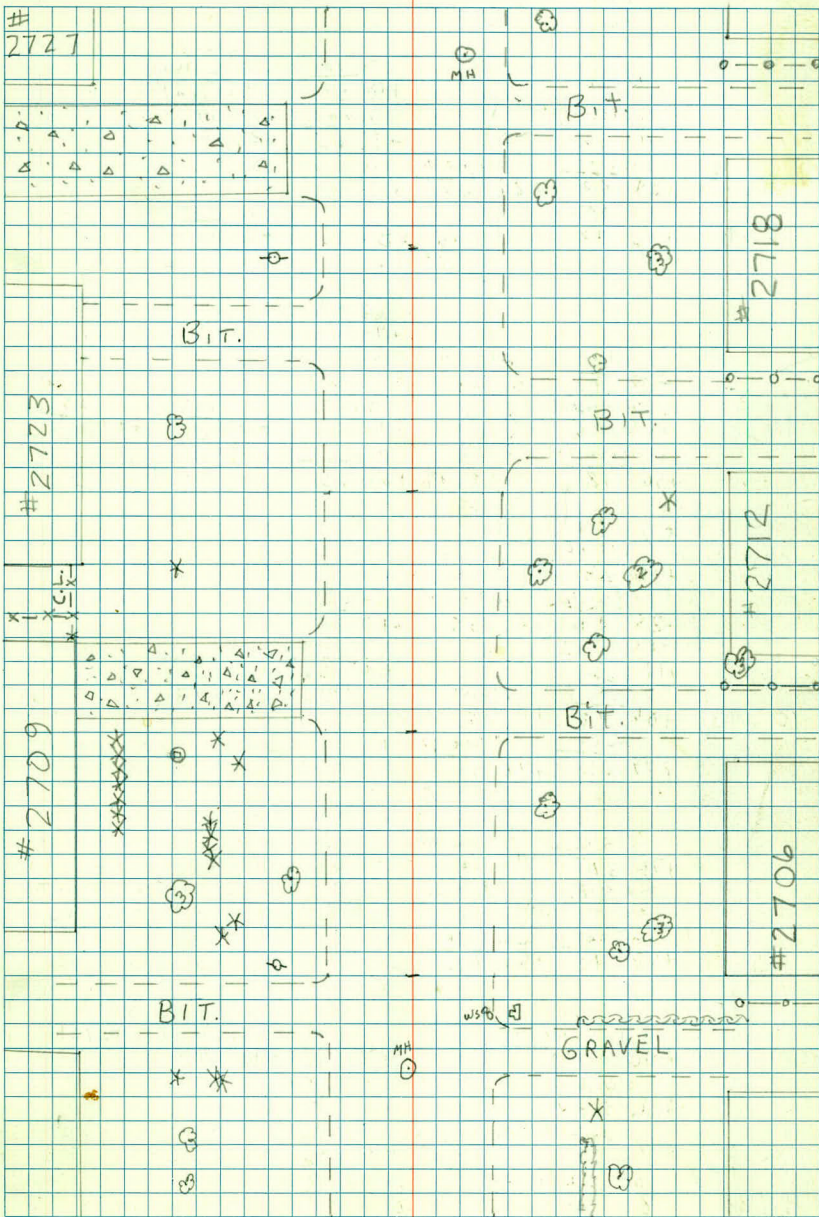
LT

E

RT

8-16-16
crow 72°

5



+50

LT
NE Cor Ho
68

C

RT

17' Conc Ent

+41 18

+24 53

6" MAPLE

+06 43

3-Pine Bushes

+27 53

RD RD
18 19

X Fe
+48 33 →

NW Cor Ho

+43 66

+26 39

14" PWE

Con Hedge
+48 33-70+

B Hedge

+41 33

+15 40

13" PINE

+15 40

5" CAT

+20 26

1" PINE
+86 47

NE Cor Ho

+66 66

16' Conc Ent

+56 18

SE Cor Ho

+87 64

15' Bit Ent
+93

SW Cor Ho

+86 67

10' Bit Ent

+72 20

NW Cor Ho

+65 66

MH
+80 1

H/D

+81 27

W50

+81 24

1" PINE
+34 28

3" Berry Tree

+25 44

SE Cor Ho

+17 66

PP

+06 28

NE Cor Ho

+99 66

PINE BUSH

+30 55

3" CAT

+45 26

SW Cor Ho

+25 66

NW Cor Ho

+03 66

2" PINE

+15 55

RD RD

+03 66

+11 20

12' Bit

+11 20

Pine Bush

+22 39

2" BIR
+76 37

+50

+57 42

G. LITE

+57 42

SE Cor Ho

+57 66

14' Conc Ent

+46 30

B. W. Fer 2'

+36 53-W

NE Cor Ho

+28 66

RD RD

+11 43

RD RD

17 19

2730

1" MAPLE

+66 40

B.C.L. Fe

+55 66

SW Cor Ho

+61 66

16' Conc Ent

+46 33

2724

8" ASH

+31 26

NW Cor Ho

+35 66

8" MAPLE

+11 43

RD RD

17 19

9

WS
BJ

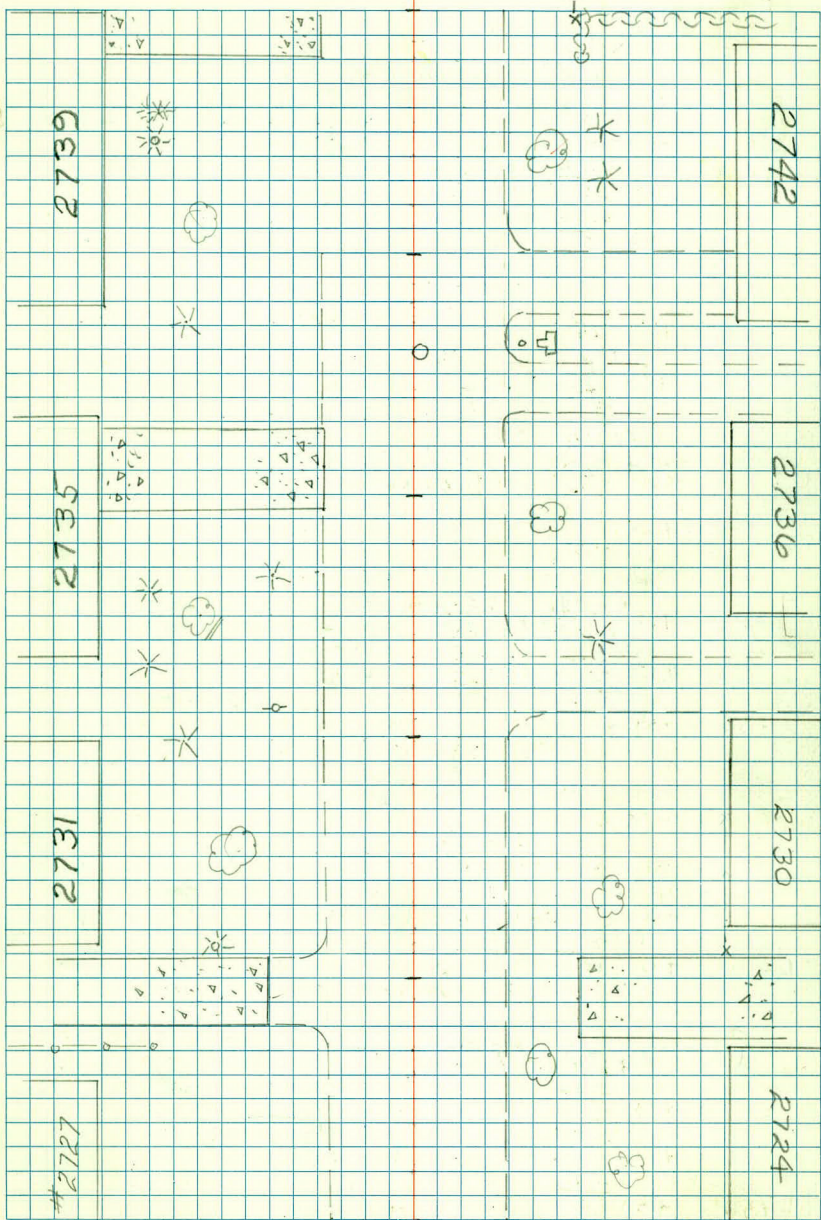
LT

E

RT

8-16-76
CLOUDY 75°

6



14

LT

C

RT

$$+98 \frac{8' 16' B. ENT}{18} \quad +90 \frac{End Fe}{34}$$

$$+85 \frac{vd Lto}{35} \quad +87 \frac{Cor. Ho.}{64}$$

+50

$$+56 \frac{4' Crab}{53}$$

13

$$+18 \frac{Cor. B. L Fe}{34-73} \quad +28 \frac{S.E. Cor Ho}{72}$$

$$+10 \frac{NEC Ho}{73} \quad +10 \frac{B. Ch. L Fe}{73} \quad RD \quad RD$$

18 17

$$+83 \frac{Cor Ho}{65-73}$$

$$+78 \frac{2'' PINE}{50}$$

+50

$$+59 \frac{16' B. ENT}{59}$$

$$+72 \frac{8'' PINE}{41}$$

$$+70 \frac{NW Cor Ho}{66}$$

$$+49 \frac{SE Cor Ho}{65}$$

$$+36 \frac{B. C. L. Fe}{34-W} \quad +42 \frac{3'' Berry Tree}{41}$$

$$+22 \frac{NE Cor Ho}{65} \quad +29 \frac{3-1'' trees}{51}$$

$$+13 \frac{18' Con Ent}{18}$$

12

RD RD
18 18

$$+32 \frac{SW Cor Ho}{66}$$

$$+37 \frac{10'' PINE}{42}$$

$$+32 \frac{NW Cor Conc}{60}$$

$$+24 \frac{10' B. ENT}{66}$$

$$+08 \frac{SW Cor EAR}{66}$$

$$+17 \frac{SW Cor Conc}{60}$$

$$+97 \frac{1'' PINE}{41}$$

$$+91 \frac{6'' CAT}{26}$$

$$+71 \frac{2'' PINE}{42}$$

$$+59 \frac{10' Dirt Ent}{66}$$

$$+68 \frac{SW Cor Ho}{66}$$

$$+73 \frac{SE Cor Ho}{67}$$

$$+71 \frac{Pine Bush}{62}$$

$$+53 \frac{Pine Bush}{64}$$

11 +50

W.S
B.S

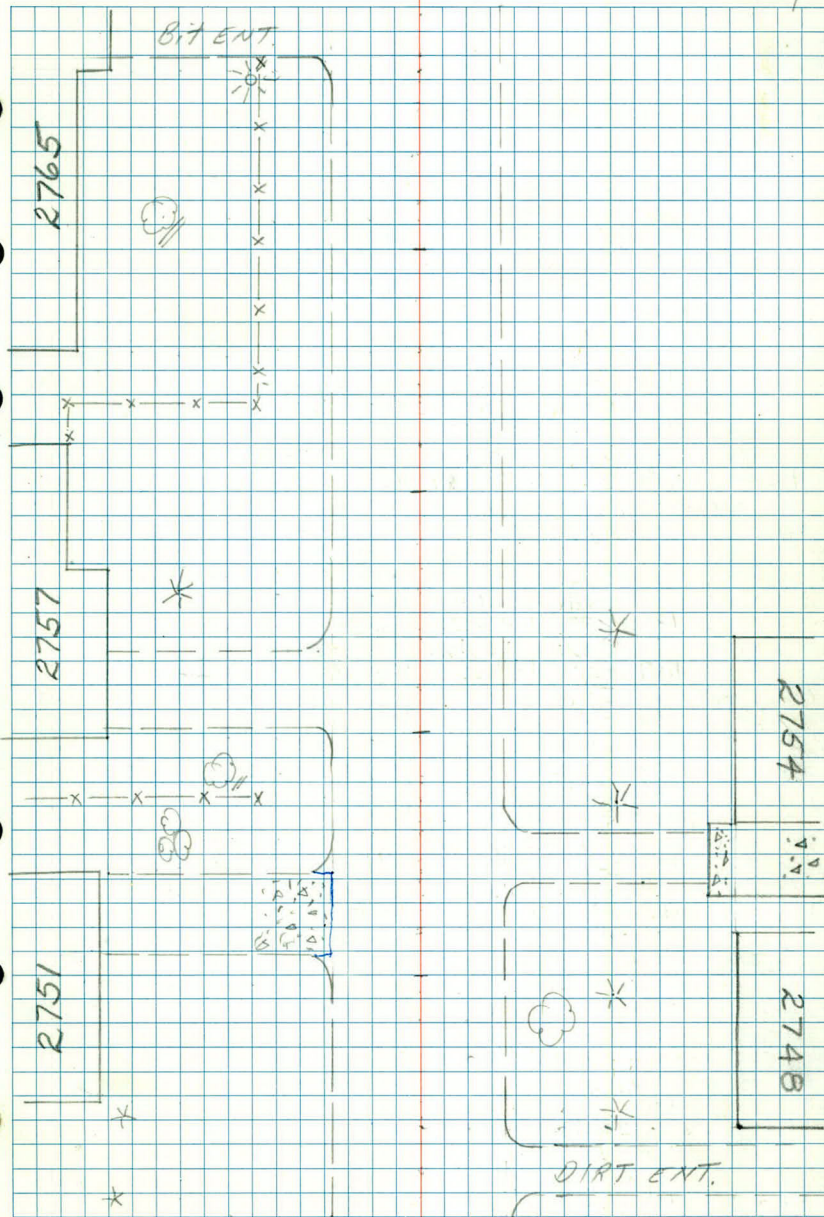
LT

C

RT

8-16-76
Cloudy 75°

7



+50

47. 2 R+

✓
+33 $\frac{3' \text{ Ash}}{43}$
+26 $\frac{PP}{26}$ ✓
+18 $\frac{5' \text{ Pine}}{36}$ ✓
+103 $\frac{2' \text{ Ash}}{36}$ ✓
+107 $\frac{2' \text{ Ash}}{36}$ ✓
+30 $\frac{SW cor Fe}{32}$ ✓
+21 $\frac{3' \text{ Pine}}{36}$ ✓

16

✓
+79 $\frac{PP}{26}$ ✓
+70 $\frac{1' \text{ Pine}}{44}$ ✓
+64 $\frac{NE cor Ho}{169}$ ✓
+72 $\frac{4' \text{ Apple}}{74}$ ✓
+73 $\frac{1' \text{ Apple}}{58}$ ✓
+69 $\frac{1' \text{ Pine}}{44}$ ✓
+178 $\frac{6' \text{ Apple}}{36}$ ✓
+17 $\frac{4' \text{ Maple}}{26}$ ✓

+50

✓
+56 $\frac{1' \text{ Pine}}{43}$ ✓
+40 $\frac{1' \text{ Pine}}{43}$ ✓
+58 $\frac{cor. Ho}{65-69}$ ✓
+153 $\frac{1' \text{ Maple}}{27}$ ✓
+167 $\frac{NWC. Ho}{50}$ ✓
+41 $\frac{SW cor Ho}{50}$ ✓

15

✓
+130 $\frac{3' \text{ Apple}}{52}$ ✓
+107 $\frac{2' \text{ Apple}}{51}$ ✓
+100 $\frac{P.O.R.}{19}$ ✓
+195 $\frac{P.O.R.}{22}$ ✓
+188 $\frac{C.R.}{35}$ ✓
+35 $\frac{SE cor Ho}{63}$ ✓
+120 $\frac{6' \text{ Cat}}{41}$ ✓
+120 $\frac{3' \text{ Apple}}{52}$ ✓
+15 $\frac{C.B.}{17}$ ✓
+100 $\frac{P.O.R.}{18}$ ✓
+15 $\frac{9' \text{ Ash}}{52}$ ✓

+64 $\frac{MH}{34}$

✓
+180 $\frac{M.H.}{25}$ ✓
+155 $\frac{P.O.R.}{21}$ ✓
+161 $\frac{E. Rad}{29}$ ✓
+93 $\frac{P.O.R.}{21}$ ✓
+84 $\frac{MH}{29}$ ✓
+86 $\frac{B. Rad}{35}$ ✓

+50

✓
+45 $\frac{Reg. Rad}{18}$ ✓
+46 $\frac{Cor Fe}{37-40}$ ✓
+123 $\frac{Bit Dr}{44}$ ✓
+12 $\frac{Bach Ho}{33}$ ✓
+11 $\frac{NE cor Ho}{64}$ ✓
+188 $\frac{B. Rad}{31}$ ✓
+12 $\frac{C.B.}{18}$ ✓
+12 $\frac{B. + D. Ho}{32}$ ✓
+150 $\frac{P.O.}{28}$ ✓
+41 $\frac{C.B.}{18}$ ✓
+135 $\frac{Hyd}{27}$ ✓
+58 $\frac{B. Rad}{35}$ ✓
+41 $\frac{P.O.R.}{21}$ ✓
+35 $\frac{B. Rad}{17}$ ✓

14

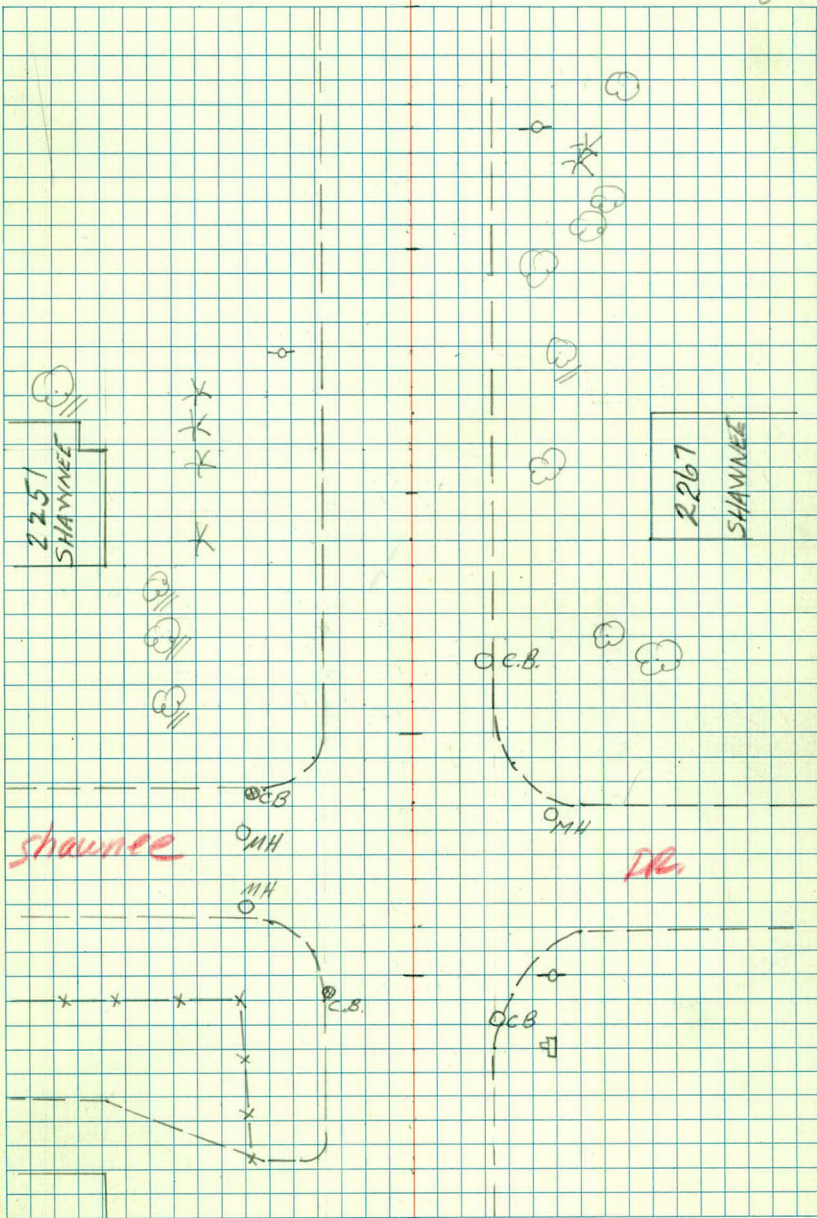
Rd Rd
18 17

WJS
K.G.

Lt.

8-18-76
Rt. CLK 80°

8



19

L4

EN

R4

Rd Rd

17 18

$$+96 \text{ ENOROW Poplars } \frac{33}{33.5} \quad +97 \text{ Beg Fegote } \frac{33.5}{33.5}$$

$$+64 \text{ NW Cor Ho } \frac{50}{50}$$

+50

$$+18 \frac{CB}{17}$$

$$+16 \frac{CB}{17}$$

$$+37 \frac{SW Cor Ho.}{50}$$

18

Rd Rd

$$17 \quad 17 \quad \text{Beg CLFC } \frac{1' 2' m}{45} \quad +93 \text{ Beg Row tree } \frac{31}{31}$$

$$+190 \frac{17}{17} \quad +95 \frac{1' pine}{36} \quad +96 \frac{1' pine}{51}$$

$$+81 \frac{Beg Rd}{36} \quad +85 \frac{POR}{22}$$

$$+79 \frac{MH}{39} \quad +81 \frac{CB}{44}$$

$$+48 \frac{POR}{24} \quad +52 \frac{END R.}{30}$$

$$+45 \frac{P.P.}{26} \quad +46 \frac{9' e/m}{47}$$

$$+23 \frac{1' pine}{38} \quad +93 \frac{Beg Rd}{17}$$

$$+17 \frac{W SO}{20} \quad +23 \frac{CB}{17}$$

$$+101 \frac{SW Cor Ho}{49} \quad +17 \frac{Hyd}{25}$$

Rd Rd

17 17

$$+90 \frac{7' tree}{36}$$

$$+76 \frac{SW Cor Ho}{49}$$

$$+63 \frac{6' Mule}{48} \quad +71 \frac{NE Cor Fegh Lk.}{32}$$

16/50

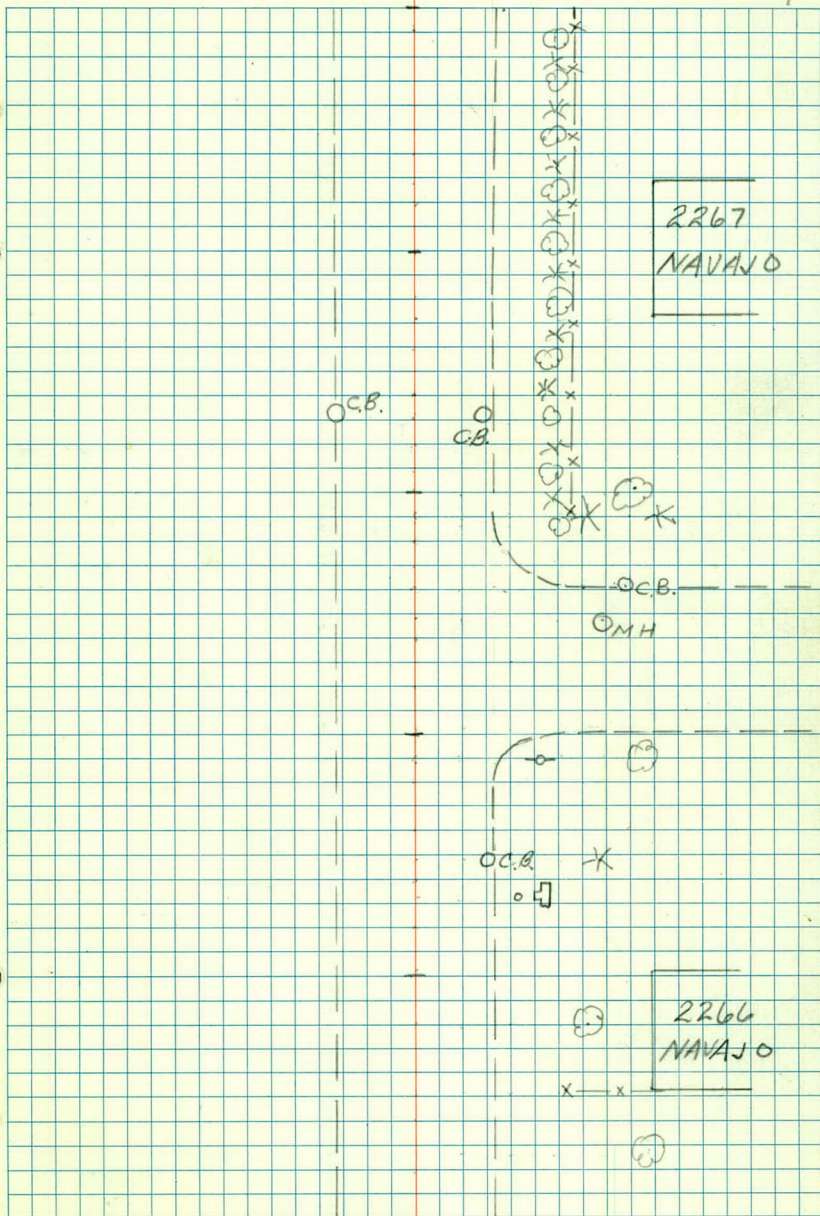
WS
KG

LT.

Q

8-18-76
RT C/80°

9



LT

E

RT

+50

+40 BURIED TLE
33+09 CB
18+07 4" MAPLE
38

21

+84 RUSSIAN PINE
63+76 12" P
42+79 NE COR HO
74+57 PINE
60+51 NE COR HO
63

+50

MT
10+40 STR
39+34 SW COR HO
94

20

+98 4" ASP
48+87 BL-18 COR
31+72 MT
72+57 BL-18
31

+50

+44 BL RAD
18

19+00

RD RD

17 18

+49 NW COR HO
73+48 2 X 3 PLANTER AND YARD LITE
35+39 8" ASP
50+16 5" ASP
26+19 CONC CURB B'D'D
53+08 SW COR HO
73+10 CB
18

RD

16

+97 MAPLE
38+89 ERAD
17+82 P.D.B
20+71 MA
38+77 BL RAD
38+77 CB
38+41 6" ASP
49+45 P.D.B
36+48 ERAD
53+35 P.D.B
21+35 PP
26+25 BLW FE
34+30 BL RAD
18+32 FE COR
34-42+11 HVD
26+15 6" P
45+21 CB
18

RD

17

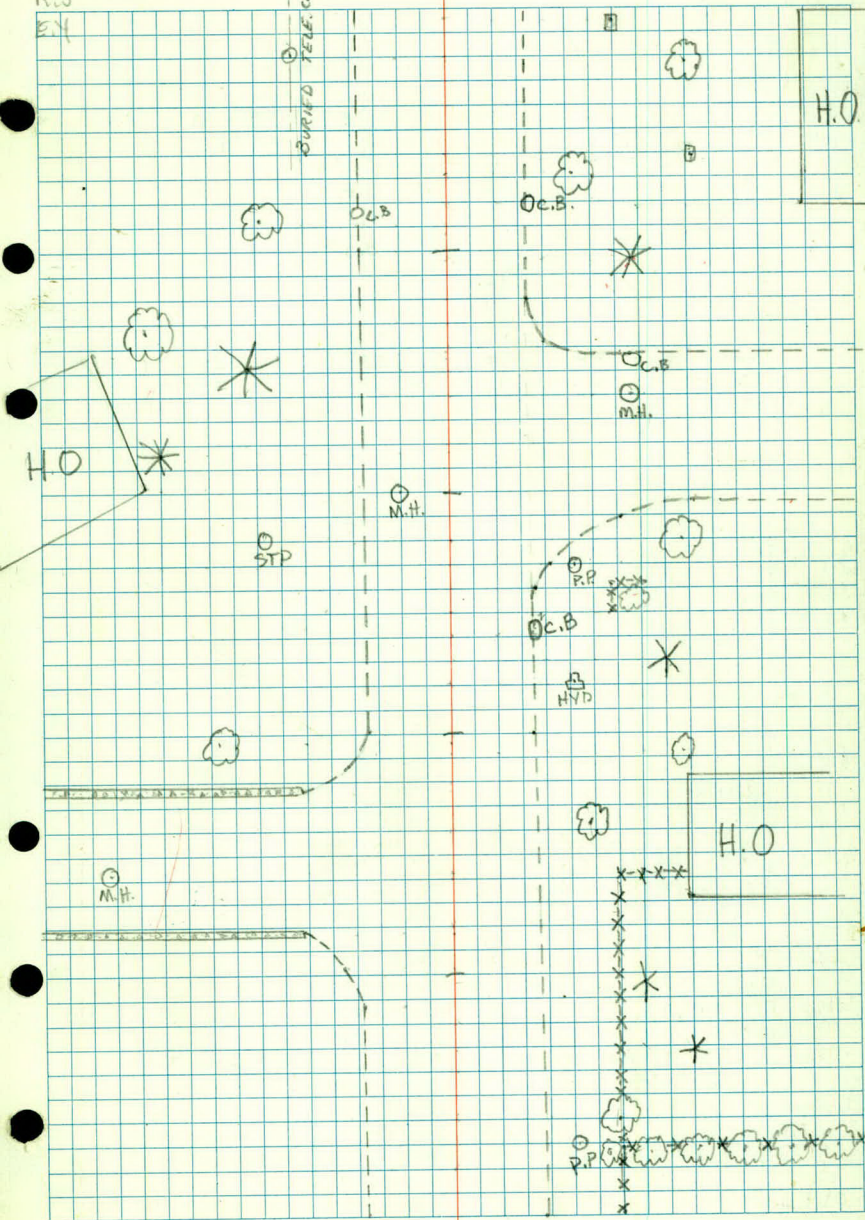
+96 BUSH
48+91 NW COR HO
49+81 4" ELM
27+66 SW COR HO
49+72 FE COR
35-49+52 P.D.B
23+20 1/2" ASP
35+34 5" P
50+47 5" P
40+14 FE COR
34+13 BL RAD POPULUS
34 → E+15 PP
26+11 E GATE
35

RD

18

FE

35



24

+08

177

SE CORN
RANTIVE TO HO

B6 CL FENCE

2" TREE

NE CORN

+99

57

+99

79

+78

SE CORN HO

69

+84

6" PINE

64

+74

BUSH

52

+92

8" ELM

51

+57

TW. 4" BPC

69

+78

4" PINE

59

+61

4" ELM

25

+50

+37

6" PINE

40

+44

6" FRUIT TREE

72

+35

HYD

25

+20

PP

21

+23

50

6" ASH

+28

EOR

17

+47

HYD

26

+52

SW CORN HO

73

+15

B6 RAD + B6 15 CURB

29

+19

POR

20

+22

2" PINE

31

+21

NW CORN HO

73

+34

1/6 GRAV ENT

23

+100

M/H

79

17

RD

+09

8" ASH

52

+17

2" PINE

31

+19

2" PINE

27

+19

2" PINE

27

+72

8" ASH

27

+75

8" PINE

72

+74

4" TRI-BIRCH

52

+70

P. BUSH

74

+73

SW CORN HO

74

+53

1/6 BIT ENT

CORNWOOD FENCE

+67

77-100+

77

77

77

77

77

77

77

77

+72

8" ASH

27

+75

8" PINE

72

+74

4" TRI-BIRCH

52

+70

P. BUSH

74

+73

SW CORN HO

74

+53

1/6 BIT ENT

CORNWOOD FENCE

+67

77-100+

77

77

77

77

77

77

77

77

+72

8" ASH

27

+75

8" PINE

72

+74

4" TRI-BIRCH

52

+70

P. BUSH

74

+73

SW CORN HO

74

+53

1/6 BIT ENT

CORNWOOD FENCE

+67

77-100+

77

77

77

77

77

77

77

77

+72

8" ASH

27

+75

8" PINE

72

+74

4" TRI-BIRCH

52

+70

P. BUSH

74

+73

SW CORN HO

74

+53

1/6 BIT ENT

CORNWOOD FENCE

+67

77-100+

77

77

77

77

77

77

77

77

+72

8" ASH

27

+75

8" PINE

72

+74

4" TRI-BIRCH

52

+70

P. BUSH

74

+73

SW CORN HO

74

+53

1/6 BIT ENT

CORNWOOD FENCE

+67

77-100+

77

77

77

77

77

77

77

77

+72

8" ASH

27

+75

8" PINE

72

+74

4" TRI-BIRCH

52

+70

P. BUSH

74

+73

SW CORN HO

74

+53

1/6 BIT ENT

CORNWOOD FENCE

+67

77-100+

77

77

77

77

77

77

77

77

+72

8" ASH

27

+75

8" PINE

72

+74

4" TRI-BIRCH

52

+70

P. BUSH

74

+73

SW CORN HO

74

+53

1/6 BIT ENT

CORNWOOD FENCE

+67

77-100+

77

77

77

77

77

77

77

77

+72

8" ASH

27

+75

8" PINE

72

+74

4" TRI-BIRCH

52

+70

P. BUSH

74

+73

SW CORN HO

74

+53

1/6 BIT ENT

CORNWOOD FENCE

+67

77-100+

77

77

77

77

77

77

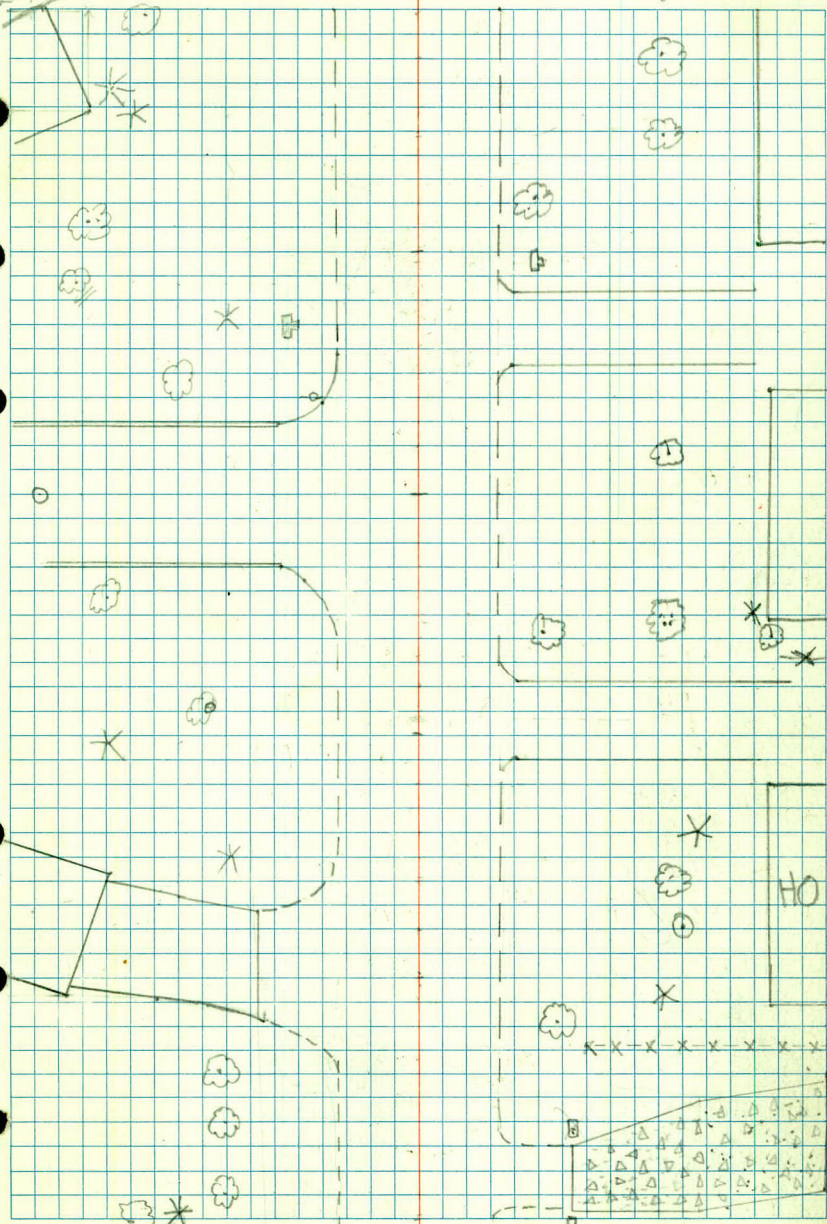
77

77

WS P.
K6
EY *4

8-25 76
Overcast 75°F
Breezy

11



+50

¢

26

+50

25 +00

PINE BUSH
48

HEDGE RD.
33 17 17

+93 ¢ 10 GRAVEL
ENT

+94

3" PINE
45

+81 NW CORN HO.
74

+77

3" PINE
46

+86 TW. 3" PINE
49

+81 BUSH
51

+66 UNDERGROUND TELE.
44

+74 6" ELN
52

+50

+35 RT HO

(BG. HEDGE)
(CORN FENCE)

+43 6" ASH
24

+53 TRI-4" BIRCH
52

+60 PP
32

+60

33

+31 4" PINE
71

+33 SW CORN HO
73

+19

CL. FENCE CORN + HEDGE
34

+16 ¢ 16' DIRT ENT

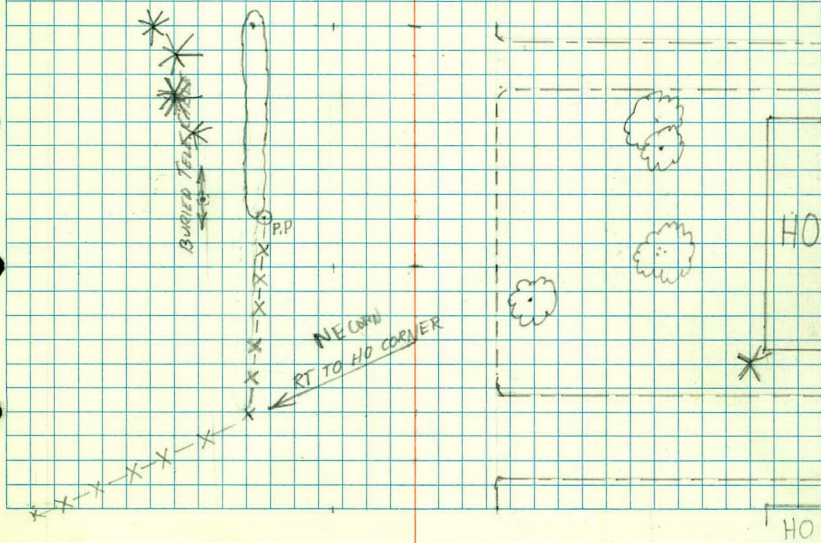
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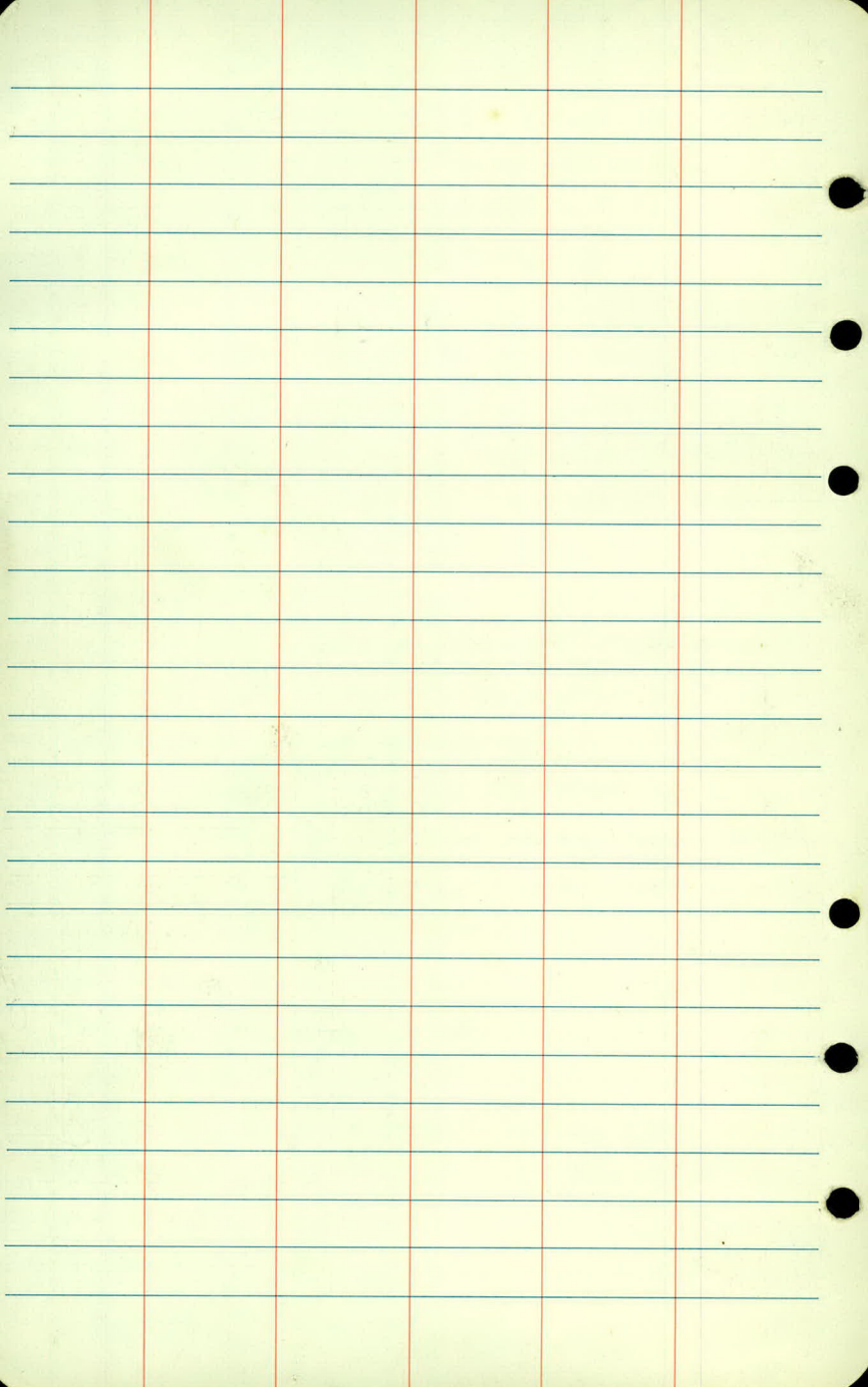
+01 NW CORN HOUSE
73

WS
K6
EY

8-25-76
OVERCAST 75°F
Breezy

12





STRUCTURAL DATA TYPE

STORM	✓	ELECTRIC		WATER	
SANITARY		TELEPHONE		OTHER	
STATION	RIGHT	LEFT	SIZE	INCH CASTING	
0-100 +85		24	9"		

TYPE OF CONST.	X	COMMENTS
BLOCK		
BRICK		
SECTIONAL		

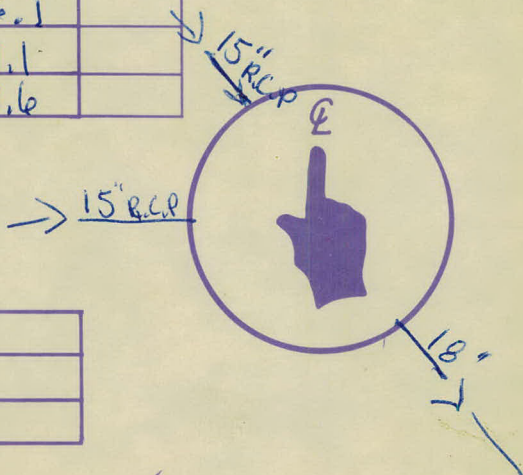
ADJUSTING RINGS	TYPE	NO.	DEPTH	COMMENTS
BLOCK				
BRICK				
CONC. RINGS	P	2	.4	

DEPTH FROM BOTTOM OF M.H.		ELEV.	
TO TOP OF CASTING	9.60		
DISTANCE FROM HIGHEST FLOW LINE TO TOP OF CASTING	6.1		
ETC.	9.1		
INV.	9.6		

SIZES OF ALL PIPES AND DIRECTION OF FLOW	
---	--

DESIGN	
ELEVATION - TOP	
FINAL ELEVATION	
DIFFERENCES	

ADJUST	
RECONSTRUCT	



STRUCTURAL DATA TYPE

STORM	ELECTRIC	WATER	✓
SANITARY	TELEPHONE	OTHER	
STATION	RIGHT	LEFT	SIZE
0+27		31	6" INCH CASTING

TYPE OF CONST.	COMMENTS
BLOCK	
BRICK	
SECTIONAL	✓

ADJUSTING RINGS	TYPE	NO.	DEPTH	COMMENTS
BLOCK	✓	2'	1.0'	
BRICK				
CONC. RINGS				

DEPTH FROM
BOTTOM OF M.H
TO TOP OF CASTING

ELEV.

TOP OF VALVE

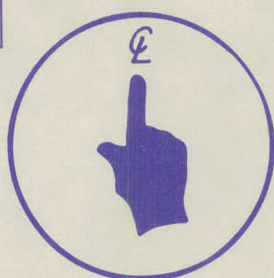
6.8	
-----	--

DISTANCE
FROM HIGHEST
FLOW LINE TO
TOP OF CASTING

ETC.

INV.

SIZES OF ALL
PIPES AND
DIRECTION OF
FLOW



DESIGN

ELEVATION - TOP

FINAL ELEVATION

DIFFERENCES

--	--

ADJUST

RECONSTRUCT

STRUCTURAL DATA TYPE

STORM	✓	ELECTRIC		WATER	
SANITARY		TELEPHONE		OTHER	
STATION	RIGHT	LEFT	SIZE	INCH CASTING	
37+80	49				

TYPE OF CONST.	✓	COMMENTS
BLOCK		<i>Precast top section</i> CATCH BASIN
BRICK		
SECTIONAL		

ADJUSTING RINGS	TYPE	NO.	DEPTH	COMMENTS
BLOCK				
BRICK				
CONC. RINGS				

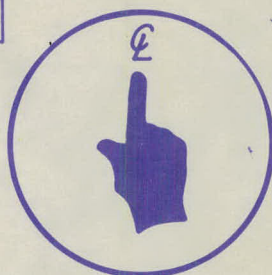
DEPTH FROM BOTTOM OF M.H.		ELEV.	
TO TOP OF CASTING	6.3		
DISTANCE FROM HIGHEST FLOW LINE TO TOP OF CASTING			
ETC.			
INV.			

SIZES OF ALL
PIPES AND
DIRECTION OF
FLOW

DESIGN
ELEVATION - TOP
FINAL ELEVATION
DIFFERENCES

ADJUST

RECONSTRUCT



↓
↓
↓ 18" rcp

↓
↓
↓ 24" rcp

STRUCTURAL DATA TYPE

STORM

ELECTRIC

WATER

SANITARY



TELEPHONE

OTHER

STATION

RIGHT

LEFT

SIZE

37+99

3

9

INCH CASTING

TYPE OF CONST.

COMMENTS

BLOCK

BRICK

SECTIONAL



ADJUSTING RINGS

TYPE

NO.

DEPTH

COMMENTS

BLOCK

BRICK

CONC. RINGS

0

may be adjusted
.1 ft.

DEPTH FROM
BOTTOM OF M.H.

ELEV.

TO TOP OF CASTING

4.2

DISTANCE

FROM HIGHEST

FLOW LINE TO

TOP OF CASTING

ETC.

INV.

SIZES OF ALL

PIPES AND

DIRECTION OF

FLOW

12" dep



12" dep

DESIGN

ELEVATION - TOP

FINAL ELEVATION

DIFFERENCES

ADJUST

RECONSTRUCT

STRUCTURAL DATA TYPE

STORM	ELECTRIC	WATER	✓
SANITARY	TELEPHONE	OTHER	
STATION	RIGHT	LEFT	SIZE
38+09	35		7
			INCH CASTING

TYPE OF CONST.	COMMENTS
BLOCK	GATE VALVE 6.2' from
BRICK	
SECTIONAL	

ADJUSTING RINGS	TYPE	NO.	DEPTH	COMMENTS
BLOCK				
BRICK				
CONC. RINGS	✓	8	1.8	

DEPTH FROM BOTTOM OF M.H. TO TOP OF CASTING	TOP OF VALVE ELEV.
DISTANCE FROM HIGHEST FLOW LINE TO TOP OF CASTING	6.2
ETC.	
INV.	

SIZES OF ALL PIPES AND DIRECTION OF FLOW	
DESIGN	
ELEVATION - TOP	
FINAL ELEVATION	
DIFFERENCES	
ADJUST	
RECONSTRUCT	



STRUCTURAL DATA TYPE

STORM

ELECTRIC

WATER

SANITARY

TELEPHONE

OTHER

STATION

RIGHT

LEFT

SIZE

38+24

48

INCH CASTING

TYPE OF CONST.

COMMENTS

BLOCK

BRICK

SECTIONAL

precast top

catch basin

ADJUSTING RINGS

TYPE

NO.

DEPTH

COMMENTS

BLOCK

BRICK

CONC. RINGS

DEPTH FROM
BOTTOM OF M.H.

ELEV.

TO TOP OF CASTING

5.9

DISTANCE
FROM HIGHEST
FLOW LINE TO
TOP OF CASTING

ETC.

INV.

SIZES OF ALL
PIPES AND
DIRECTION OF
FLOW

DESIGN

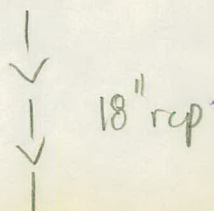
ELEVATION - TOP

FINAL ELEVATION

DIFFERENCES

ADJUST

RECONSTRUCT



STRUCTURAL DATA TYPE

STORM	☒	ELECTRIC	☐	WATER	☐
SANITARY	☐	TELEPHONE	☐	OTHER	☐
STATION	RIGHT	LEFT	SIZE		
41+10	46		9 1/2"	INCH CASTING	

TYPE OF CONST.	COMMENTS	
BLOCK		
BRICK		
SECTIONAL	☒	

ADJUSTING RINGS	TYPE	NO.	DEPTH	COMMENTS
BLOCK				
BRICK				
CONC. RINGS	☒	4	.85'	

DEPTH FROM
BOTTOM OF M.H.
TO TOP OF CASTING

DISTANCE
FROM HIGHEST
FLOW LINE TO
TOP OF CASTING

ETC.

INV.

ELEV.
6.15
2.40

SIZES OF ALL
PIPES AND
DIRECTION OF
FLOW

DESIGN

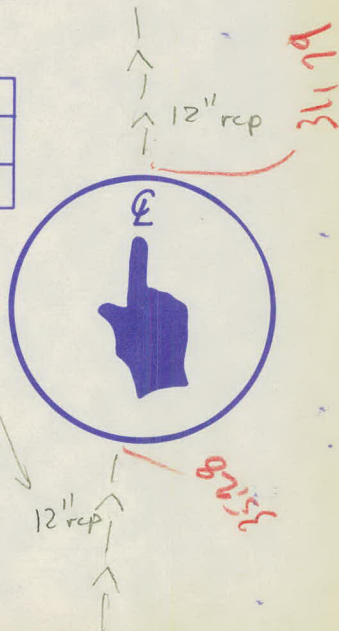
ELEVATION - TOP

FINAL ELEVATION

DIFFERENCES

ADJUST

RECONSTRUCT



STRUCTURAL DATA TYPE

STORM



ELECTRIC

WATER

SANITARY

TELEPHONE

OTHER

STATION

RIGHT

LEFT

SIZE

41 + 16

46

INCH CASTING

TYPE OF CONST.

BLOCK

BRICK

SECTIONAL

COMMENTS

precast C.B

ADJUSTING RINGS

TYPE

NO.

DEPTH

COMMENTS

BLOCK

BRICK

CONC. RINGS

DEPTH FROM
BOTTOM OF M.H

ELEV.

TO TOP OF CASTING

6.1

DISTANCE
FROM HIGHEST
FLOW LINE TO
TOP OF CASTING

ETC.

INV.

12" ↓
rcp

SIZES OF ALL
PIPES AND
DIRECTION OF
FLOW

24" rcp
←



24" rcp
←

DESIGN

ELEVATION - TOP

37.2

FINAL ELEVATION

DIFFERENCES

ADJUST

RECONSTRUCT

12" ↑

STRUCTURAL DATA TYPE

STORM		ELECTRIC		WATER		
SANITARY	✓	TELEPHONE		OTHER		
STATION		RIGHT		LEFT	SIZE	
411+28				6	9 1/2	INCH CASTING

TYPE OF CONST.		COMMENTS
BLOCK	✓	
BRICK		
SECTIONAL		

ADJUSTING RINGS	TYPE	NO.	DEPTH	COMMENTS
BLOCK				
BRICK				
CONC. RINGS	✓	1	3"	

DEPTH FROM BOTTOM OF M.H TO TOP OF CASTING		ELEV.	
	4.5		
DISTANCE FROM HIGHEST FLOW LINE TO TOP OF CASTING			
ETC.			
INV.			
SIZES OF ALL PIPES AND DIRECTION OF FLOW			
DESIGN			
ELEVATION - TOP			
FINAL ELEVATION			
DIFFERENCES			
ADJUST			
RECONSTRUCT			



STRUCTURAL DATA TYPE

STORM		ELECTRIC		WATER	
SANITARY	✓	TELEPHONE		OTHER	

STATION	RIGHT	LEFT	SIZE	
41+32		6	9 1/2"	INCH CASTING

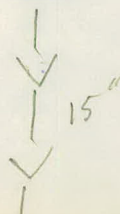
TYPE OF CONST.		COMMENTS
BLOCK	✓	
BRICK		
SECTIONAL		

ADJUSTING RINGS	TYPE	NO.	DEPTH	COMMENTS
BLOCK				
BRICK				
CONC. RINGS	✓	2	5"	

DEPTH FROM BOTTOM OF M.H. TO TOP OF CASTING		ELEV.	
DISTANCE FROM HIGHEST FLOW LINE TO TOP OF CASTING			
ETC.			
INV.			

SIZES OF ALL PIPES AND DIRECTION OF FLOW	
---	--

DESIGN	
ELEVATION - TOP	
FINAL ELEVATION	
DIFFERENCES	
ADJUST	
RECONSTRUCT	



STRUCTURAL DATA TYPE

STORM	☒	ELECTRIC	☐	WATER	☐
SANITARY	☐	TELEPHONE	☐	OTHER	☐
STATION	RIGHT	LEFT	SIZE		
411+39	46		7	INCH CASTING	

TYPE OF CONST.	COMMENTS		
BLOCK			
BRICK			
SECTIONAL			

ADJUSTING RINGS	TYPE	NO.	DEPTH	COMMENTS
BLOCK				
BRICK				
CONC. RINGS	☒	3	11"	

DEPTH FROM BOTTOM OF M.H TO TOP OF CASTING	ELEV.	5.5	
DISTANCE FROM HIGHEST FLOW LINE TO TOP OF CASTING		3.60	
ETC.			
INV.			

SIZES OF ALL PIPES AND DIRECTION OF FLOW	
---	--

DESIGN	
ELEVATION - TOP	
FINAL ELEVATION	
DIFFERENCES	

ADJUST	
RECONSTRUCT	



STRUCTURAL DATA TYPE

STORM	✓	ELECTRIC		WATER	
SANITARY		TELEPHONE		OTHER	
STATION	RIGHT	LEFT	SIZE	INCH CASTING	
41+46	46				

TYPE OF CONST.	COMMENTS
BLOCK	CATCH BASIN
BRICK	
SECTIONAL	

ADJUSTING RINGS	TYPE	NO.	DEPTH	COMMENTS
BLOCK	✓			
BRICK				
CONC. RINGS				

DEPTH FROM BOTTOM OF M.H.	ELEV.
TO TOP OF CASTING	3.0
DISTANCE FROM HIGHEST FLOW LINE TO TOP OF CASTING	
ETC.	
INV.	

SIZES OF ALL PIPES AND DIRECTION OF FLOW	
DESIGN	
ELEVATION - TOP	
FINAL ELEVATION	
DIFFERENCES	
ADJUST	
RECONSTRUCT	



1
 ✓
 12' ref
 ✓

STRUCTURAL DATA TYPE

STORM ☒	ELECTRIC ☐	WATER ☐	
SANITARY ☐	TELEPHONE ☐	OTHER ☐	
STATION	RIGHT	LEFT	SIZE
44+46	46		
			INCH CASTING

TYPE OF CONST.	COMMENTS
BLOCK ☒	CATCH BASIN
BRICK ☐	
SECTIONAL ☐	

ADJUSTING RINGS	TYPE	NO.	DEPTH	COMMENTS
BLOCK	☒			
BRICK	☒		.9	
CONC. RINGS				

DEPTH FROM
BOTTOM OF M.H
TO TOP OF CASTING

DISTANCE
FROM HIGHEST
FLOW LINE TO
TOP OF CASTING

ETC.

INV.

ELEV.	
2.1	
2.0	

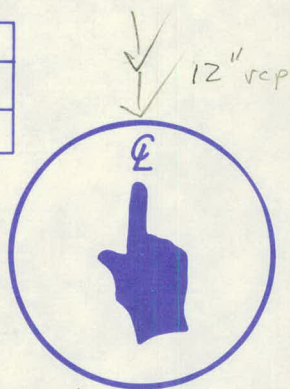
SIZES OF ALL
PIPES AND
DIRECTION OF
FLOW

DESIGN

ELEVATION - TOP	
FINAL ELEVATION	
DIFFERENCES	

ADJUST

RECONSTRUCT



STRUCTURAL DATA TYPE

STORM	☒	ELECTRIC		WATER	
SANITARY	☐	TELEPHONE		OTHER	
STATION	RIGHT	LEFT	SIZE	INCH CASTING	
44+76	46				

TYPE OF CONST.		COMMENTS
BLOCK	☒	CATCH BASIN
BRICK		
SECTIONAL		

ADJUSTING RINGS	TYPE	NO.	DEPTH	COMMENTS
BLOCK				concrete .5'
BRICK				
CONC. RINGS				

DEPTH FROM BOTTOM OF M.H.		ELEV.
TO TOP OF CASTING	2.0	
DISTANCE FROM HIGHEST FLOW LINE TO TOP OF CASTING		
ETC.		
INV.		

SIZES OF ALL
PIPES AND
DIRECTION OF
FLOW

DESIGN

ELEVATION - TOP

FINAL ELEVATION

DIFFERENCES

ADJUST

RECONSTRUCT



12" r4p

STRUCTURAL DATA TYPE

STORM	☒	ELECTRIC		WATER		
SANITARY		TELEPHONE		OTHER		
STATION		RIGHT	LEFT	SIZE		
46+48			17	9	INCH CASTING	

TYPE OF CONST.	COMMENTS
BLOCK	8' x 10'
BRICK	
SECTIONAL	
	POURED

ADJUSTING RINGS	TYPE	NO.	DEPTH	COMMENTS
BLOCK				
BRICK				
CONC. RINGS	✓	4	0.9	

DEPTH FROM BOTTOM OF M.H. TO TOP OF CASTING DISTANCE FROM HIGHEST FLOW LINE TO TOP OF CASTING ETC. INV.	ELEV.	
	10.0	①
	7.5	②

42" R.C.P.

2' 7" HIGH

4' 3" WIDE

TWO PIPES

SIZES OF ALL
PIPES AND
DIRECTION OF
FLOW

DESIGN

ELEVATION - TOP

FINAL ELEVATION

DIFFERENCES

ADJUST

RECONSTRUCT

STRUCTURAL DATA TYPE

STORM	✓	ELECTRIC		WATER		
SANITARY		TELEPHONE		OTHER		
STATION	RIGHT	LEFT	SIZE	INCH CASTING		
47+76	45					

TYPE OF CONST.		COMMENTS
BLOCK		CATCH BASIN
BRICK		
SECTIONAL	✓	

ADJUSTING RINGS	TYPE	NO.	DEPTH	COMMENTS
BLOCK				
BRICK				
CONC. RINGS				

DEPTH FROM BOTTOM OF M.H TO TOP OF CASTING	ELEV.	
		4.8
DISTANCE FROM HIGHEST FLOW LINE TO TOP OF CASTING		
ETC.		
INV.		

SIZES OF ALL PIPES AND DIRECTION OF FLOW	
---	--

DESIGN	
ELEVATION - TOP	
FINAL ELEVATION	
DIFFERENCES	

ADJUST

RECONSTRUCT

↓
↓ 12" rcp
↓



15" rcp
← — — — →

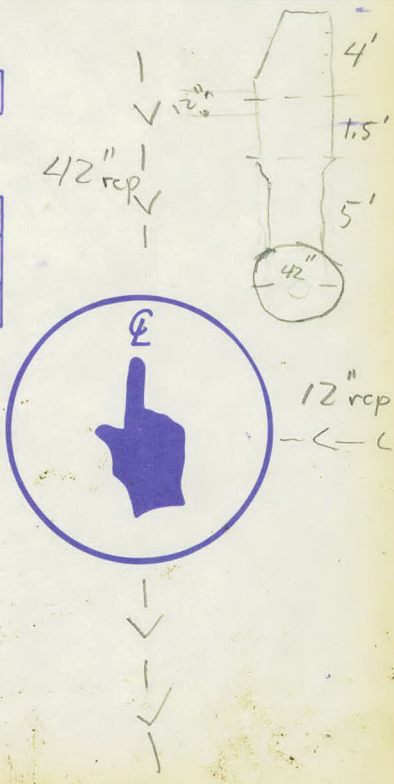
STRUCTURAL DATA TYPE

STORM	✓	ELECTRIC		WATER		
SANITARY		TELEPHONE		OTHER		
STATION	RIGHT	LEFT	SIZE			
47+78		14	9	INCH CASTING		

TYPE OF CONST.	COMMENTS
BLOCK	see drawing below
BRICK	
SECTIONAL	

ADJUSTING RINGS	TYPE	NO.	DEPTH	COMMENTS
BLOCK				
BRICK				
CONC. RINGS				

DEPTH FROM BOTTOM OF M.H TO TOP OF CASTING	ELEV.	11.6	
DISTANCE FROM HIGHEST FLOW LINE TO TOP OF CASTING		5.7	
ETC.			
INV.			
SIZES OF ALL PIPES AND DIRECTION OF FLOW			
DESIGN			
ELEVATION - TOP			
FINAL ELEVATION			
DIFFERENCES			
ADJUST			
RECONSTRUCT			



STRUCTURAL DATA TYPE

STORM		ELECTRIC		WATER	
SANITARY	✓	TELEPHONE		OTHER	
STATION		RIGHT	LEFT	SIZE	INCH CASTING
47+99		2		9	

TYPE OF CONST.		COMMENTS
BLOCK		
BRICK		
SECTIONAL		✓

ADJUSTING RINGS	TYPE	NO.	DEPTH	COMMENTS
BLOCK				
BRICK				
CONC. RINGS	✓	2	.6'	

DEPTH FROM
BOTTOM OF M.H.
TO TOP OF CASTING

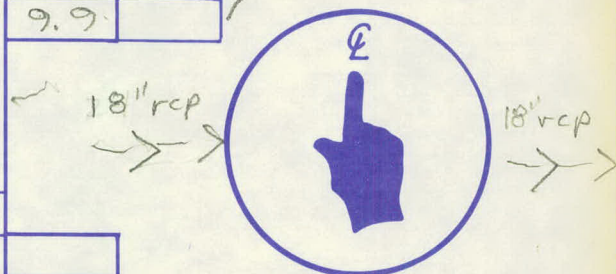
DISTANCE
FROM HIGHEST
FLOW LINE TO
TOP OF CASTING

ETC.

INV.

ELEV.
13.5
13.5
9.9

SIZES OF ALL
PIPES AND
DIRECTION OF
FLOW



DESIGN

ELEVATION - TOP

FINAL ELEVATION

DIFFERENCES

ADJUST

RECONSTRUCT

STRUCTURAL DATA TYPE

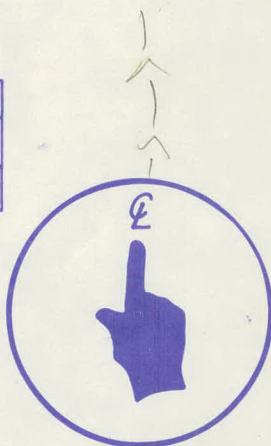
STORM	ELECTRIC	WATER	✓
SANITARY	TELEPHONE	OTHER	
STATION	RIGHT	LEFT	SIZE
48+02	57		7
			INCH CASTING

TYPE OF CONST.	COMMENTS
BLOCK	water Gate Valve.
BRICK	
SECTIONAL	

ADJUSTING RINGS	TYPE	NO.	DEPTH	COMMENTS
BLOCK				
BRICK				
CONC. RINGS	✓	1	.1	

DEPTH FROM BOTTOM OF M.H. TO TOP OF CASTING	TOP OF VALVE ELEV.
DISTANCE FROM HIGHEST FLOW LINE TO TOP OF CASTING	3.3
ETC.	
INV.	

SIZES OF ALL PIPES AND DIRECTION OF FLOW	
DESIGN	
ELEVATION - TOP	
FINAL ELEVATION	
DIFFERENCES	
ADJUST	
RECONSTRUCT	

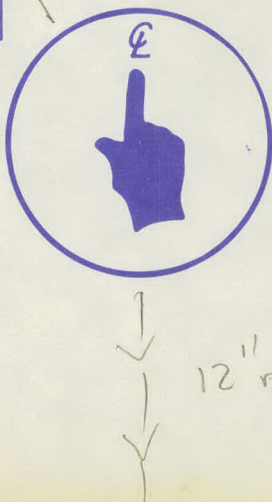


STRUCTURAL DATA TYPE

STORM	✓	ELECTRIC		WATER	
SANITARY		TELEPHONE		OTHER	
STATION	RIGHT	LEFT	SIZE		
48+05	45			INCH CASTING	

TYPE OF CONST.	COMMENTS
BLOCK	CATCH BASIN
BRICK	
SECTIONAL	

ADJUSTING RINGS	TYPE	NO.	DEPTH	COMMENTS
BLOCK				
BRICK				
CONC. RINGS				

DEPTH FROM BOTTOM OF M.H TO TOP OF CASTING	ELEV.		
	3.4		
DISTANCE FROM HIGHEST FLOW LINE TO TOP OF CASTING			12" rcp.
ETC.			
INV.			
SIZES OF ALL PIPES AND DIRECTION OF FLOW			
DESIGN			
ELEVATION - TOP			
FINAL ELEVATION			
DIFFERENCES			
ADJUST			
RECONSTRUCT			

STRUCTURAL DATA TYPE

STORM	✓	ELECTRIC		WATER	
SANITARY		TELEPHONE		OTHER	
STATION	RIGHT	LEFT	SIZE		
48 + 24	22			INCH CASTING	

TYPE OF CONST.	COMMENTS
BLOCK	CATCH BASIN
BRICK	
SECTIONAL	

ADJUSTING RINGS	TYPE	NO.	DEPTH	COMMENTS
BLOCK				
BRICK				
CONC. RINGS			.7	

DEPTH FROM BOTTOM OF M.H TO TOP OF CASTING	ELEV.	
		4.2
DISTANCE FROM HIGHEST FLOW LINE TO TOP OF CASTING		
ETC.		
INV.		

SIZES OF ALL
PIPES AND
DIRECTION OF
FLOW

DESIGN

ELEVATION - TOP

FINAL ELEVATION

DIFFERENCES

ADJUST

RECONSTRUCT



12" RCP
→

STRUCTURAL DATA TYPE

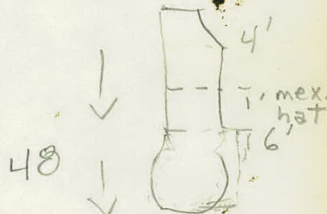
STORM	✓	ELECTRIC		WATER	
SANITARY		TELEPHONE		OTHER	
STATION	RIGHT	LEFT	SIZE	INCH CASTING	
49+52		15	9		

TYPE OF CONST.	COMMENTS ← Bottom 6'	
BLOCK		
BRICK		
SECTIONAL		

ADJUSTING RINGS	TYPE	NO.	DEPTH	COMMENTS
BLOCK				
BRICK				
CONC. RINGS			0.1	

DEPTH FROM
BOTTOM OF M.H.
TO TOP OF CASTING
DISTANCE
FROM HIGHEST
FLOW LINE TO
TOP OF CASTING
ETC.
INV.

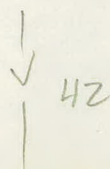
ELEV.
14.0
10.4



SIZES OF ALL
PIPES AND
DIRECTION OF
FLOW



DESIGN
ELEVATION - TOP
FINAL ELEVATION
DIFFERENCES
ADJUST
RECONSTRUCT



STRUCTURAL DATA TYPE

STORM	ELECTRIC	WATER	✓
SANITARY	TELEPHONE	OTHER	
STATION	RIGHT	LEFT	SIZE
50+92	14		9" INCH CASTING

TYPE OF CONST.	COMMENTS
BLOCK	
BRICK	
SECTIONAL	✓

ADJUSTING RINGS	TYPE	NO.	DEPTH	COMMENTS
BLOCK				
BRICK				
CONC. RINGS	✓	2	.6	

DEPTH FROM BOTTOM OF M.H.	Top of ^{manhole} ELEV.
TO TOP OF CASTING	5.1
DISTANCE FROM HIGHEST FLOW LINE TO TOP OF CASTING	
ETC.	
INV.	

SIZES OF ALL PIPES AND DIRECTION OF FLOW	
---	--

DESIGN	
ELEVATION - TOP	
FINAL ELEVATION	
DIFFERENCES	

ADJUST	
RECONSTRUCT	



STRUCTURAL DATA TYPE

STORM



ELECTRIC

WATER

SANITARY

TELEPHONE

OTHER

STATION

RIGHT

LEFT

SIZE

51706

39

8

INCH CASTING

TYPE OF CONST.

BLOCK

BRICK

SECTIONAL



COMMENTS

CATCH BASIN

3 1/2' cone

ADJUSTING RINGS

TYPE

NO.

DEPTH

COMMENTS

BLOCK

BRICK

CONC. RINGS



2

.50

DEPTH FROM
BOTTOM OF M.H.

ELEV.

TO TOP OF CASTING

4.60

DISTANCE

FROM HIGHEST

FLOW LINE TO

TOP OF CASTING

ETC.

INV.

SIZES OF ALL

PIPES AND

DIRECTION OF

FLOW

DESIGN

ELEVATION - TOP

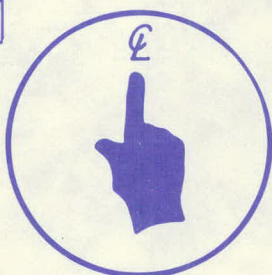
FINAL ELEVATION

DIFFERENCES

ADJUST

RECONSTRUCT

1
^
1
^
12" rep



STRUCTURAL DATA TYPE

STORM



ELECTRIC

WATER

SANITARY

TELEPHONE

OTHER

STATION

RIGHT

LEFT

SIZE

51+08

42

INCH CASTING

TYPE OF CONST.

BLOCK

BRICK

SECTIONAL



1 1/2' precast

COMMENTS

CATCH BASIN

ADJUSTING RINGS

TYPE

NO.

DEPTH

COMMENTS

BLOCK

BRICK



4

1.0

CONC. RINGS

DEPTH FROM
BOTTOM OF M.H.

ELEV.

TO TOP OF CASTING

3.8

DISTANCE

FROM HIGHEST

FLOW LINE TO

TOP OF CASTING

ETC.

INV.

SIZES OF ALL

PIPES AND

DIRECTION OF

FLOW

DESIGN

ELEVATION - TOP

FINAL ELEVATION

DIFFERENCES

ADJUST

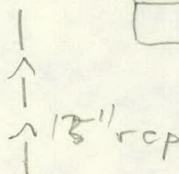
RECONSTRUCT



brick

masonry

1 1/2'



STRUCTURAL DATA TYPE

STORM		ELECTRIC		WATER	
SANITARY	✓	TELEPHONE		OTHER	
STATION	RIGHT	LEFT	SIZE		
51+22	—	€ —	9	INCH CASTING	

TYPE OF CONST.	COMMENTS
BLOCK	
BRICK	
SECTIONAL	✓

ADJUSTING RINGS	TYPE	NO.	DEPTH	COMMENTS
BLOCK				
BRICK				
CONC. RINGS	✓	1	.25	

DEPTH FROM BOTTOM OF M.H TO TOP OF CASTING DISTANCE FROM HIGHEST FLOW LINE TO TOP OF CASTING ETC. INV.	ELEV.	
	22.1	
	7.3	

SIZES OF ALL PIPES AND DIRECTION OF FLOW	
DESIGN	
ELEVATION - TOP	
FINAL ELEVATION	
DIFFERENCES	
ADJUST	
RECONSTRUCT	

STRUCTURAL DATA TYPE

STORM

ELECTRIC

WATER ☒

SANITARY

TELEPHONE

OTHER

STATION

RIGHT

LEFT

SIZE

51+30

34

9

INCH CASTING

TYPE OF CONST.

BLOCK

BRICK

SECTIONAL

COMMENTS

Gate valve

4' cone

1 1/2' bottom

ADJUSTING RINGS

TYPE

NO.

DEPTH

COMMENTS

BLOCK

BRICK

CONC. RINGS

☒

4

.90

DEPTH FROM
BOTTOM OF M.H.

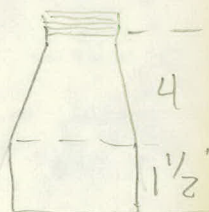
TOP of VALVE
ELEV.

TO TOP OF CASTING
DISTANCE
FROM HIGHEST
FLOW LINE TO
TOP OF CASTING

6.0

ETC.

INV.



SIZES OF ALL
PIPES AND
DIRECTION OF
FLOW



DESIGN

ELEVATION - TOP

FINAL ELEVATION

DIFFERENCES

ADJUST

RECONSTRUCT

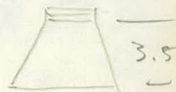
STRUCTURAL DATA TYPE

STORM	☒	ELECTRIC	☐	WATER	☐
SANITARY	☐	TELEPHONE	☐	OTHER	☐
STATION	RIGHT	LEFT	SIZE	INCH CASTING	
51+36		39	8½		

TYPE OF CONST.	COMMENTS
BLOCK	CATCH BASIN 3½ concentric cone
BRICK	
SECTIONAL	

ADJUSTING RINGS	TYPE	NO.	DEPTH	COMMENTS
BLOCK				
BRICK				
CONC. RINGS	☒	1	.40	

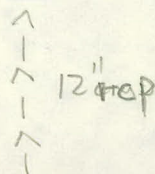
DEPTH FROM BOTTOM OF M.H. TO TOP OF CASTING	ELEV.	
	5.0	
DISTANCE FROM HIGHEST FLOW LINE TO TOP OF CASTING	5.0	
ETC.		
INV.		



SIZES OF ALL PIPES AND DIRECTION OF FLOW	
---	--



DESIGN	
ELEVATION - TOP	
FINAL ELEVATION	
DIFFERENCES	



ADJUST	
RECONSTRUCT	

STRUCTURAL DATA TYPE

STORM



ELECTRIC

WATER

SANITARY

TELEPHONE

OTHER

STATION

RIGHT

LEFT

SIZE

51+37

11

9

INCH CASTING

TYPE OF CONST.

COMMENTS

BLOCK

BRICK

SECTIONAL

ADJUSTING RINGS

TYPE

NO.

DEPTH

COMMENTS

BLOCK

BRICK

CONC. RINGS



8

1.9

DEPTH FROM
BOTTOM OF M.H.
TO TOP OF CASTING

ELEV.

16.0

DISTANCE
FROM HIGHEST
FLOW LINE TO
TOP OF CASTING

5.70

ETC.

5.1

INV.

5.9

SIZES OF ALL
PIPES AND
DIRECTION OF
FLOW

15" rcp

12" rcp

4.4

1.35

2.6

5'

DESIGN

ELEVATION - TOP

FINAL ELEVATION

DIFFERENCES

ADJUST

RECONSTRUCT



48"

STRUCTURAL DATA TYPE

STORM	☒	ELECTRIC		WATER	
SANITARY		TELEPHONE		OTHER	
STATION	RIGHT	LEFT	SIZE		
51+37	42			INCH CASTING	

TYPE OF CONST.	COMMENTS
BLOCK	CATCH BASIN
BRICK	
SECTIONAL	
	✓ 1½"

ADJUSTING RINGS	TYPE	NO.	DEPTH	COMMENTS
BLOCK	✓	2	1.4	
BRICK				
CONC. RINGS				

DEPTH FROM BOTTOM OF M.H.	ELEV.	
TO TOP OF CASTING	4.55	
DISTANCE FROM HIGHEST FLOW LINE TO TOP OF CASTING		
ETC.		
INV.		

SIZES OF ALL PIPES AND DIRECTION OF FLOW	12" rcp ← ← ← £
---	--

DESIGN	
ELEVATION - TOP	
FINAL ELEVATION	
DIFFERENCES	

ADJUST	
RECONSTRUCT	

15" rcp

↑
↑
↑

STRUCTURAL DATA TYPE

STORM ☒

ELECTRIC ☐

WATER ☐

SANITARY ☐

TELEPHONE ☐

OTHER ☐

STATION

RIGHT

LEFT

SIZE

51+54

22

8 1/2

INCH CASTING

TYPE OF CONST.

BLOCK ☒

BRICK ☐

SECTIONAL ☐

COMMENTS

CATCH BASIN

ADJUSTING RINGS

TYPE

NO.

DEPTH

COMMENTS

BLOCK ☐

BRICK ☐

CONC. RINGS ☒

4

9

DEPTH FROM
BOTTOM OF M.H.

ELEV.

TO TOP OF CASTING

5.08

DISTANCE
FROM HIGHEST
FLOW LINE TO
TOP OF CASTING

ETC.

INV.

SIZES OF ALL
PIPES AND
DIRECTION OF
FLOW

DESIGN

ELEVATION - TOP

FINAL ELEVATION

DIFFERENCES

ADJUST

RECONSTRUCT



12" rep

STRUCTURAL DATA TYPE

STORM	☒	ELECTRIC	☐	WATER	☐
SANITARY	☐	TELEPHONE	☐	OTHER	☐
STATION	RIGHT	LEFT	SIZE		
51+55	23		8"	INCH CASTING	

TYPE OF CONST.	COMMENTS
BLOCK	CATCH BASIN
BRICK	
SECTIONAL	

ADJUSTING RINGS	TYPE	NO.	DEPTH	COMMENTS
BLOCK				
BRICK				
CONC. RINGS	☒	5	1.4	

DEPTH FROM BOTTOM OF M.H. TO TOP OF CASTING	ELEV.	
DISTANCE FROM HIGHEST FLOW LINE TO TOP OF CASTING		
ETC.		
INV.		

SIZES OF ALL PIPES AND DIRECTION OF FLOW	
---	--

DESIGN	
ELEVATION - TOP	
FINAL ELEVATION	
DIFFERENCES	

ADJUST	
RECONSTRUCT	



STRUCTURAL DATA TYPE

STORM	ELECTRIC	WATER	✓
SANITARY	TELEPHONE	OTHER	
STATION	RIGHT	LEFT	SIZE
51+66	13		11
			INCH CASTING

TYPE OF CONST.		COMMENTS
BLOCK	✓	Gate VALVE
BRICK		
SECTIONAL		

ADJUSTING RINGS	TYPE	NO.	DEPTH	COMMENTS
BLOCK	✓			
BRICK				
CONC. RINGS	✓	2	.7	

DEPTH FROM BOTTOM OF M.H TO TOP OF CASTING		TOP of VALVE ELEV.
DISTANCE FROM HIGHEST FLOW LINE TO TOP OF CASTING	5.5	
ETC.		
INV.		

SIZES OF ALL PIPES AND DIRECTION OF FLOW	
---	--

DESIGN ELEVATION - TOP	
FINAL ELEVATION	
DIFFERENCES	

ADJUST	
RECONSTRUCT	



STRUCTURAL DATA TYPE

STORM	✓	ELECTRIC		WATER	
SANITARY		TELEPHONE		OTHER	
STATION		RIGHT	LEFT	SIZE	
54+36		41		8 1/2	INCH CASTING

TYPE OF CONST.		COMMENTS
BLOCK		CATCH BASIN 2 1/2'
BRICK		
SECTIONAL	✓	

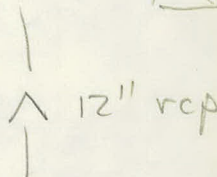
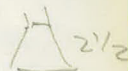
ADJUSTING RINGS	TYPE	NO.	DEPTH	COMMENTS
BLOCK				
BRICK				
CONC. RINGS			1.5	

DEPTH FROM BOTTOM OF M.H. TO TOP OF CASTING		ELEV.	
	3.5		
DISTANCE FROM HIGHEST FLOW LINE TO TOP OF CASTING			
ETC.			
INV.			

SIZES OF ALL PIPES AND DIRECTION OF FLOW	
---	--

DESIGN	
ELEVATION - TOP	
FINAL ELEVATION	
DIFFERENCES	

ADJUST	
RECONSTRUCT	



STRUCTURAL DATA TYPE

STORM		ELECTRIC		WATER	
SANITARY	✓	TELEPHONE		OTHER	

STATION	RIGHT	LEFT	SIZE	
54+50		1	9	INCH CASTING

TYPE OF CONST.	COMMENTS
BLOCK	Left station
BRICK	
SECTIONAL	

ADJUSTING RINGS	TYPE	NO.	DEPTH	COMMENTS
BLOCK				
BRICK				
CONC. RINGS				

DEPTH FROM
BOTTOM OF M.H
TO TOP OF CASTING

DISTANCE
FROM HIGHEST
FLOW LINE TO
TOP OF CASTING

ETC.

INV.

ELEV.	
24.2	
11.2	
15.1	
23.7	

SIZES OF ALL
PIPES AND
DIRECTION OF
FLOW

DESIGN

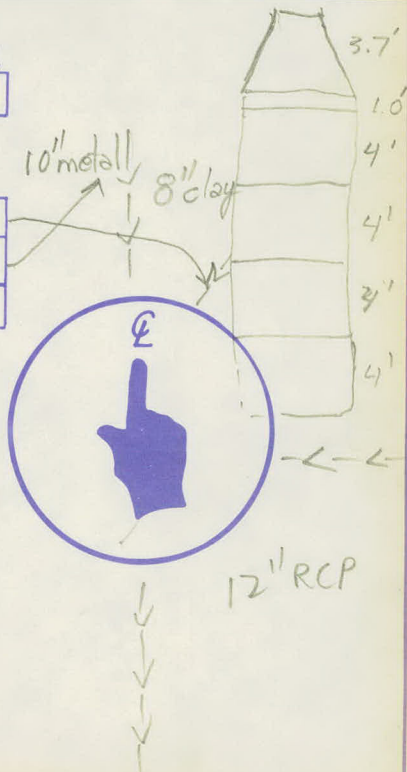
ELEVATION - TOP

FINAL ELEVATION

DIFFERENCES

ADJUST

RECONSTRUCT



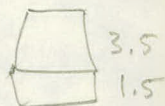
STRUCTURAL DATA TYPE

STORM	ELECTRIC	WATER	✓
SANITARY	TELEPHONE	OTHER	
STATION	RIGHT	LEFT	SIZE
54+59	35		9
			INCH CASTING

TYPE OF CONST.	COMMENTS
BLOCK	
BRICK	
SECTIONAL	✓

ADJUSTING RINGS	TYPE	NO.	DEPTH	COMMENTS
BLOCK				
BRICK				
CONC. RINGS			.15	

DEPTH FROM BOTTOM OF M.H.	TOP OF VALVE ELEV.
TO TOP OF CASTING	4.1
DISTANCE FROM HIGHEST FLOW LINE TO TOP OF CASTING	
ETC.	
INV.	



SIZES OF ALL
PIPES AND
DIRECTION OF
FLOW



DESIGN	
ELEVATION - TOP	
FINAL ELEVATION	
DIFFERENCES	
ADJUST	
RECONSTRUCT	

STRUCTURAL DATA TYPE

STORM ☒	ELECTRIC ☐	WATER ☐			
SANITARY ☐	TELEPHONE ☐	OTHER ☐			
STATION 54+65	RIGHT 36	LEFT 8	SIZE 8 INCH CASTING		
TYPE OF CONST.		COMMENTS CATCH BASIN			
BLOCK ☐					
BRICK ☐					
SECTIONAL ☒ 3,4					
ADJUSTING RINGS		TYPE	NO.	DEPTH	COMMENTS
BLOCK ☐					
BRICK ☐					
CONC. RINGS ☐					
DEPTH FROM BOTTOM OF M.H. TO TOP OF CASTING DISTANCE FROM HIGHEST FLOW LINE TO TOP OF CASTING ETC. INV.		ELEV.			
		4.35			
SIZES OF ALL PIPES AND DIRECTION OF FLOW		 12" rcp 12" rcp			
DESIGN					
ELEVATION - TOP					
FINAL ELEVATION					
DIFFERENCES					
ADJUST					
RECONSTRUCT					

STRUCTURAL DATA TYPE

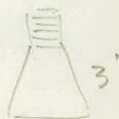
STORM	ELECTRIC	WATER	
SANITARY	TELEPHONE	OTHER	
STATION	RIGHT	LEFT	SIZE
54+84	22		8
INCH CASTING			

TYPE OF CONST.	COMMENTS
BLOCK	CATCH BASIN
BRICK	
SECTIONAL ☒	
	3.0

ADJUSTING RINGS	TYPE	NO.	DEPTH	COMMENTS
BLOCK				
BRICK				
CONC. RINGS ☒		5	1.2	

DEPTH FROM BOTTOM OF M.H. TO TOP OF CASTING	ELEV.	
	5.2	
DISTANCE FROM HIGHEST FLOW LINE TO TOP OF CASTING		
ETC.		
INV.		

SIZES OF ALL PIPES AND DIRECTION OF FLOW	
DESIGN	
ELEVATION - TOP	
FINAL ELEVATION	
DIFFERENCES	
ADJUST	
RECONSTRUCT	



STRUCTURAL DATA TYPE

STORM	✓	ELECTRIC		WATER	
SANITARY		TELEPHONE		OTHER	
STATION	RIGHT	LEFT	SIZE		
54+72		1.2	9	INCH CASTING	

TYPE OF CONST.	COMMENTS
BLOCK	
BRICK	
SECTIONAL	

ADJUSTING RINGS	TYPE	NO.	DEPTH	COMMENTS
BLOCK				
BRICK				
CONC. RINGS	✓	2	.62	

DEPTH FROM
BOTTOM OF M.H.
TO TOP OF CASTING

DISTANCE
FROM HIGHEST
FLOW LINE TO
TOP OF CASTING

ETC.

INV.

ELEV.	
14.8	
5.2	
5.9	

SIZES OF ALL
PIPES AND
DIRECTION OF
FLOW

DESIGN

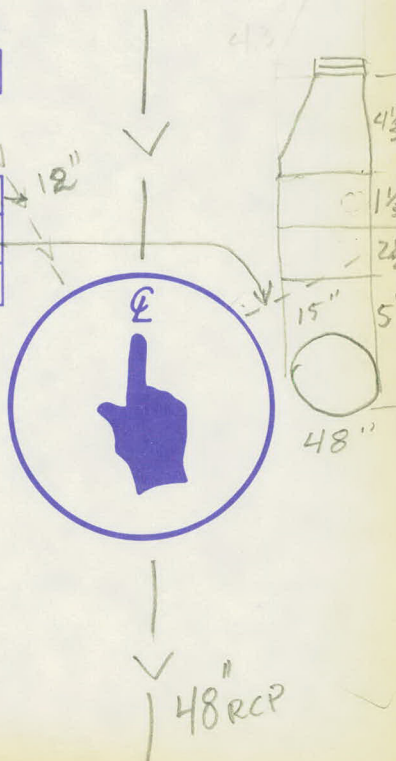
ELEVATION - TOP

FINAL ELEVATION

DIFFERENCES

ADJUST

RECONSTRUCT



STRUCTURAL DATA

TYPE

STORM ☒

ELECTRIC ☐

WATER ☐

SANITARY ☒

TELEPHONE ☐

OTHER ☐

STATION

RIGHT

LEFT

SIZE

54+85

22

INCH CASTING

TYPE OF CONST.

BLOCK

BRICK

SECTIONAL ☒

COMMENTS

CATCH BASIN

ADJUSTING RINGS

TYPE

NO.

DEPTH

COMMENTS

BLOCK

BRICK

CONC. RINGS ☒

3

17

DEPTH FROM
BOTTOM OF M.H.

ELEV.

TO TOP OF CASTING

4.9

DISTANCE

FROM HIGHEST

FLOW LINE TO

TOP OF CASTING

ETC.

INV.

SIZES OF ALL

PIPES AND

DIRECTION OF

FLOW



3.2



12" ecp

DESIGN

ELEVATION - TOP

FINAL ELEVATION

DIFFERENCES

ADJUST

RECONSTRUCT

McKnight Rd. - "C" to "D"
manhole elevations

STA.	+	π	-	ELEV	
B.M.	0.27	970.87			970.60
* 0-58			6.51	64.36	
0-40			6.37	64.50	
0-20			6.17	64.70	
0+14			6.01	64.86	
0+18			6.08	64.79	
+20			6.06	64.81	
+22			7.06	63.81	
+28			5.61	65.26	
+37			6.42	64.45	
+35			6.36	64.51	
+39			5.65	65.22	
2+66			3.57	67.30	
+85			3.46	67.41	
3+08			2.89	67.98	
+29			2.60	68.27	
+66			2.54	68.33	
* 0-16			6.63	64.24	
T.P.	4.33	972.66	2.54	968.33	

Description

Top hydrant. N.E. cor. Mohawk

● Top of manhole #1 - 6' Rt.

Top of manhole #2 - 11' Rt.

● Top of manhole #3 1' Lt.

Top of manhole #4 19 Rt.

● Top of manhole #5 31' Rt.

Top of manhole #6 X

Top of C.B. # 7 - 33 Lt.

Top of manhole #8 - 32' Lt.

Top of C.B. # 9 - 22' Lt.

Top of C.B. # 10 - 22' Rt.

Top of manhole #11 - 11' Rt.

● Top of manhole #12 - 16' Rt.

Top of manhole #13 - 36' Rt.

● Top of manhole #14 - 23' Rt.

Top of manhole #15 1' Lt.

Top of manhole #16 - 9' Rt.

Top of manhole #3A - 24' Lt.

Top of manhole #16 - 9' Rt. Sta 3+66

STA	+	π	-	ELEV	
		972.66			
6+81			3.63	69.03	
8+89			5.80	66.86	
10+80			6.00	66.66	
B.M.	1.60	971.17	3.07	969.59	969.57
14+40			6.49	64.68	
+47			6.30	64.87	
+56			5.89	65.28	
+61			5.73	65.44	
+64			6.56	64.61	
+71			5.61	65.56	
+78			6.50	64.67	
+88			5.53	65.64	
+88			6.62	64.55	
15+08			5.31	65.86	
+14			5.59	65.58	
B.M.			4.15	967.02	967.13

Description

Top M.N. #17 - 1' Lt.

Top M.N. #18 - 10 Rt.

Top M.N. #19 - 1 Rt.

Top hyd. Rt. Sta 10+80

Top C.B. #20 - 18' Rt

Top C.B. #21 - 19' Lt.

Top M.N. #22 - 8' Rt.

Top M.N. #23 - 8' Lt.

Top M.N. #24 - 34' Lt.

Top M.N. #25 - 1' Lt.

Top M.N. #26 - 36' Lt

Top M.N. #27 - 8' Lt.

Top C.B. #28 - 35' Lt.

Top M.N. #29 - 6' Rt.

Top C.B. #30 - 17' Rt.

Top hyd. S.E. cor Shawnee

STA	+	π	-	ELEV.	
B.M.	13.14	989.88			976.74
17+06			15.80	74.08	
+22			15.88	74.00	
+55			14.10	75.78	
+55			13.66	76.22	
+75			13.41	76.47	
+80			13.85	76.03	
18+16			12.28	77.60	
+18			12.22	77.66	
19+83			5.07	84.81	
20+00			4.49	85.39	
+21			4.02	85.86	
+49			3.35	86.53	
+60			2.92	86.96	
+70			2.54	87.34	
+76			2.88	87.00	
21+09			2.64	87.24	
21+09			2.40	87.48	
B.M.	12.12	997.86	4.31	985.57	985.54

Description

Top hyd. S.E. cor. Navajo

TOP MH 31 8' RT

TOP CB 32 16' RT

TOP MH 33 10' LT

TOP MH 34 1' LT

TOP MH 35 40' RT

TOP CB 36 44' RT

TOP CB 37 17' RT

TOP CB 38 17' LT

TOP MH 39 7' RT

TOP MH 40 11' RT

TOP CB 41 19' RT

TOP MH 43 10' LT

TOP MH 44 1' RT

TOP MH 45 39' RT

TOP CB 46 37' RT

TOP CB 47 19' LT

TOP CB 48 18' RT

Top. Pk. $\angle$ Sta 20+00

STA	+	π	-	ELEV.
		997.86		
23+10			7.38	90.48
+49			6.67	91.19
25+86			4.09	93.77
26+12			3.74	94.12
26+13			3.71	94.15
26+22			3.60	94.26
26+56			3.98	93.88
BM			6.77	991.09 (991.09)
39+49 $\neq$				63.48
45+84 $\neq$				67.20
50+88 $\neq$				74.34

Description

TOP MH 49 7' RT

TOP MH 50 1' RT

TOP MH 51 11' RT

TOP MH 52 34' RT

TOP MH 53 7' RT

TOP MH 54 1' RT

TOP MH 55 14' LT

TOP HYD. NW COR. MAPLE LANE

