

OFFICE OF COUNTY ENGINEER
RAMSEY COUNTY, MINN.

PLAN

Survey

McKNIGHT ROAD

From

BEAM AVE.

To

Co. Rd. "D" &
I-694

Road Acc't. No.

68

Date Filed

File

RG
LPD
JA
KG

Oct. 30, 1975
clear, Windy 55°

TOPOGRAPHY

M^cKnight Rd.

from

Beam Ave.

to

Co. Rd. "D" § I 694

14 Pages

1+

2

RT

+50 $\frac{BIT}{16}$

4" Spruce
44

SW Cor Gar
63

+40

+45

Bay Hedge

+17

35

2" Mt Ash

+10

40

Cor Conc Ent
33

+21

+27

Mugha Pine
36

27+00

BIT
12

SECOR Ho

+90

64

Mugha Pine

+92

End Bit

+92

Curb

ER

+63

12

1" Mt Ash

+85

40

Bushes

+59

39-44

BR + Bay

B618 ch

+49

31

+52

13

MH

+28

71

Cor Conc Ent
33

+9.7

+86

18

+83 RT to Cor Garage

1" Pine

+67

+67

+74

41

BR

BR

B618

54

+52

33

Mount

+28 Beam Ave

MH

+22

1

MH

+12

7

MH

+12

33

+12

ER

45

End Bag

+06

B618 curb

30+

+04 NSP Gas X-ing

Arc Lt

26+00

+00

Cor He

+00

32+

+00

27

Hypel

+93

30

BR

+87

16

+88

5" Pine

49

+87

MH

5" Apple

+82

53

NW Cor. Ho.

+81

74

5" Pine

+79

40

3" Pine

+89

40

BR

+88

17

3" Pine

+72

27

5" Ash

+75

27

+67

5" Pine

44

+61

2" Pine

27

5" Maple

+47

40

8" Ash

+50

50

+24 E 16' Bit Ent

25+00

+00

Hedge

Maple

BT

32

+04

40

17

16

+04

5" Pine

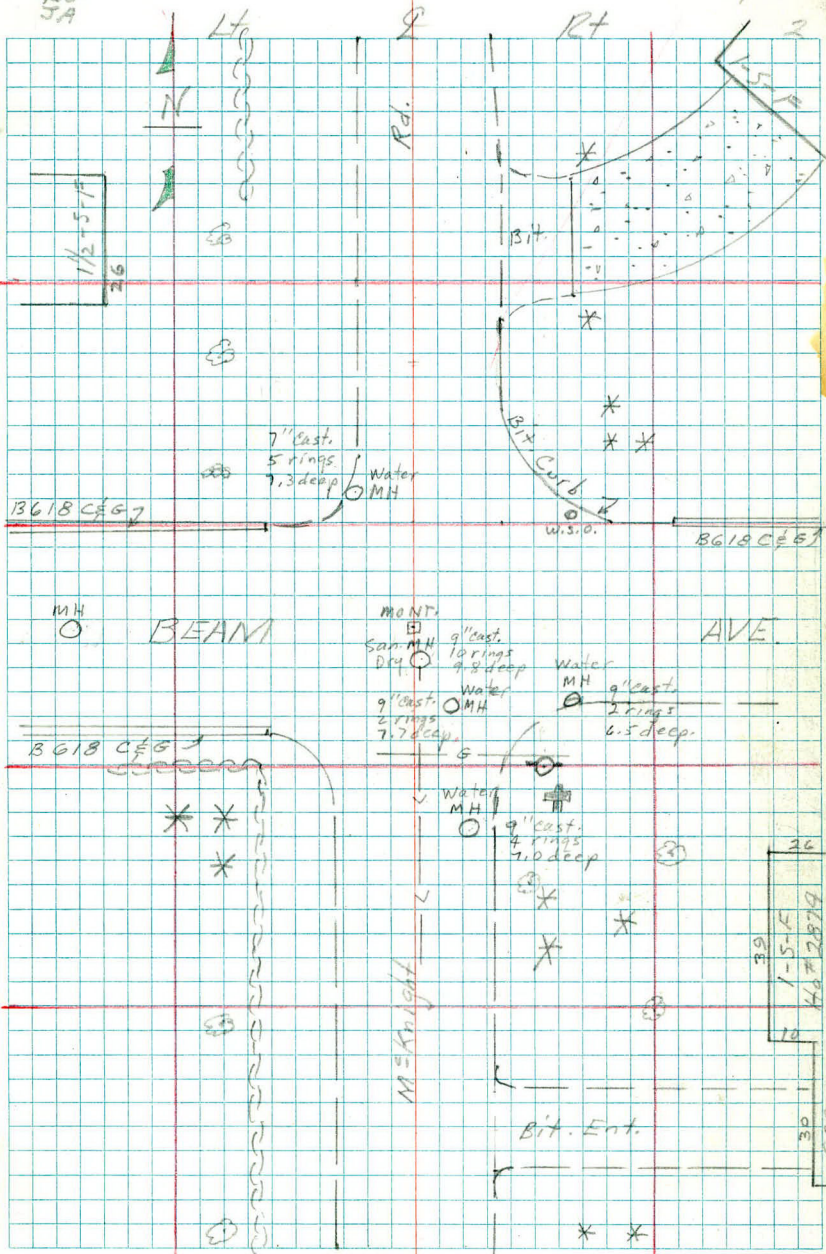
33

+04

8" Pine

46

Oct. 30, 1975.
clear 55° Windy



30+00

14

+00 $\frac{Bit}{20}$

9

+00 $\frac{Bit}{19}$ RT

1" Pine
45

ER + End B618

+83 $\frac{22}{22}$ +83 $\frac{31}{31}$ Arch Lt.

B.R. (B618) Hyd.

+73 $\frac{33}{33}$ +87 $\frac{26}{26}$

+97 $\frac{70}{70}$ NW Cor Ho

+74 $\frac{31}{31}$ 2" Ash

+06 $\frac{MH}{2}$

ER

+39 $\frac{35}{35}$ +37 $\frac{40}{40}$ GV

B.R. + Beg

+27 $\frac{13618}{22}$

+16 $\frac{Bit}{14}$

+44 $\frac{216}{216}$ Conc Ent

+33 $\frac{70}{70}$ SW Cor Ho #2912 +28 $\frac{45}{45}$ 1" Pine

29+00

RECOR

+96 $\frac{35+}{35+}$

+10 $\frac{45-55}{45-55}$ End Pkg
+13 $\frac{33-38}{33-38}$ SW

+96 $\frac{70}{70}$ NW Cor Ho #2902

+84 $\frac{16}{16}$ Bit Ent

+54 $\frac{1" MH Ash}{30}$

+40 $\frac{2" Maple}{49}$

+27 $\frac{SW Cor Ho #2903}{70}$

BIT

13 12

28+00

PP

+93 $\frac{31}{31}$ +96

Tel Box 3X3

+37 $\frac{37}{37}$

+92 $\frac{5' SW}{33}$

+98 $\frac{49}{49}$ Tel. Box 3'x3

+98 $\frac{35}{35}$ Box Board Fe.

+88 $\frac{35}{35}$ End Ho

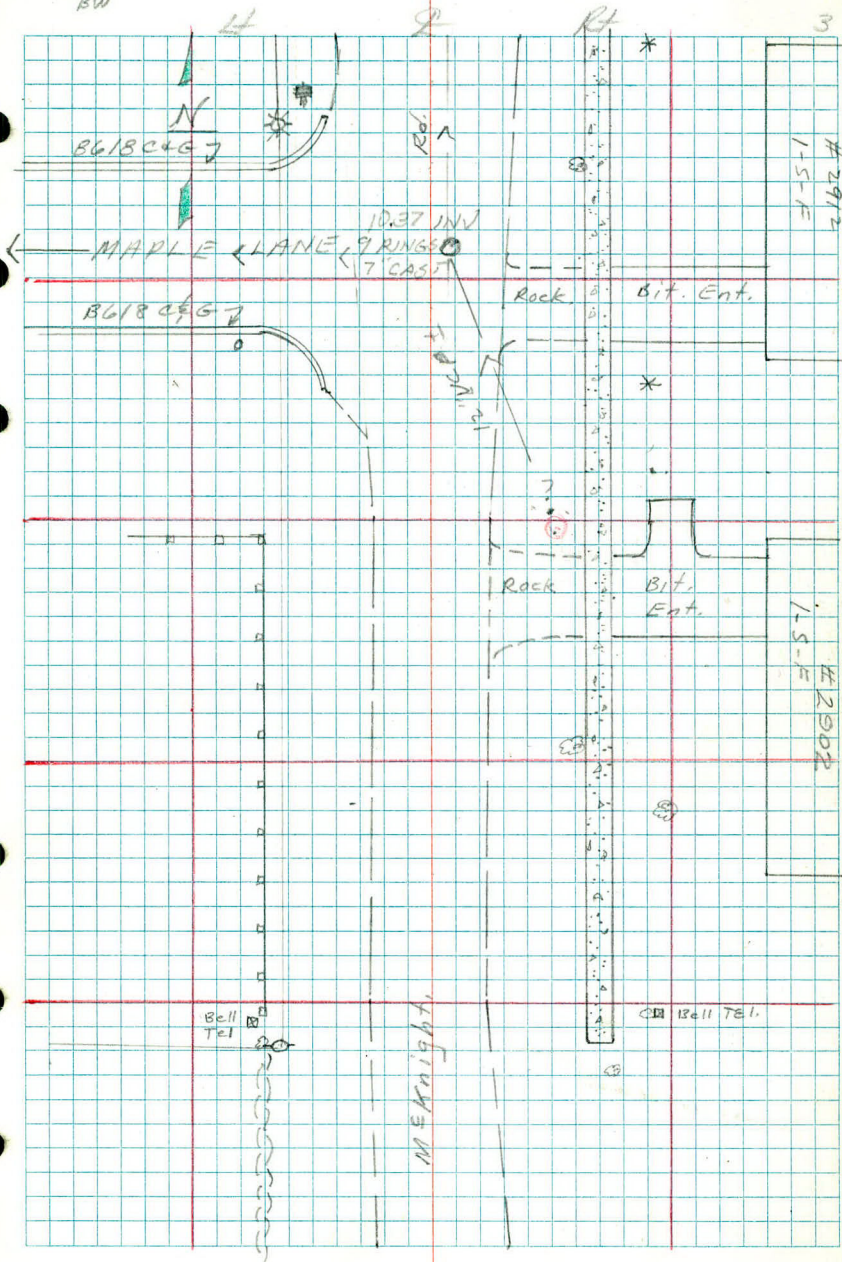
+87 $\frac{38}{38}$ Bush

+98 $\frac{45}{45}$ Bush

+93 $\frac{35}{35}$ Bush

RG
JA
KG
BW

Oct. 31, 1975
Clear 50° Windy



LT

RT

RT

$\begin{array}{r} \text{Beg B618} \\ +38 \quad 56+ \\ \hline \end{array}$
 $\begin{array}{r} \text{S.W.} \\ +41 \quad 34-39 \\ \hline \end{array}$
 $\begin{array}{r} \text{MH} \\ +33 \quad 40 \\ \hline \end{array}$
 $\begin{array}{r} \text{CB} \\ +38 \quad 54 \\ \hline \end{array}$
 $\begin{array}{r} \text{BR} \\ +38 \quad 54 \\ \hline \end{array}$

$\begin{array}{r} \text{MH} \\ +23 \quad 2 \\ \hline \end{array}$

$\begin{array}{r} +10 \text{ E } 16' \text{ Bit. Ent. } / 33' \\ \text{SW Cor Ho \# 2933} \\ \hline \end{array}$

$\begin{array}{r} \text{MH} \\ +08 \quad 30 \\ \hline \end{array}$

32+00

$\begin{array}{r} +00 \quad 71 \\ \hline \end{array}$

$\begin{array}{r} \text{BT} \\ 19 \\ \hline \end{array}$

$\begin{array}{r} \text{ER} \\ +06 \quad 54 \\ \hline \end{array}$

$\begin{array}{r} \text{CB} \\ +06 \quad 54 \\ \hline \end{array}$

$\begin{array}{r} \text{Beg B618} \\ +06 \quad 58+ \\ \hline \end{array}$

$\begin{array}{r} \text{RICKI} \\ +91 \quad 42 \\ \hline \end{array}$

$\begin{array}{r} \text{NE Cor Ho} \\ +90 \quad 78 \\ \hline \end{array}$

$\begin{array}{r} \text{BURIED CB} \\ +73 \quad 21 \\ \hline \end{array}$

$\begin{array}{r} \text{NW Cor Ho} \\ +61 \quad 69 \\ \hline \end{array}$

$\begin{array}{r} \text{Bit. BR \& curb} \\ +62 \quad 19 \\ \hline \end{array}$

$\begin{array}{r} 2" \text{ M + Ash} \\ +57 \quad 40 \\ \hline \end{array}$

$\begin{array}{r} \text{SE Cor Gar (20')} \\ +26 \quad 71 \\ \hline \end{array}$

$\begin{array}{r} +36 \text{ E } 16' \text{ Bit. Ent. } / 33' \\ \text{Te / Ex} \\ \hline \end{array}$

$\begin{array}{r} \text{SW Cor Ho} \\ +35 \quad 69 \\ \hline \end{array}$

+17 30

+19 37

$\begin{array}{r} \text{Gay Pole} \\ +18 \quad 40 \\ \hline \end{array}$

$\begin{array}{r} \text{BT} \\ 18 \\ \hline \end{array}$

18 19

$\begin{array}{r} \text{S.W.} \\ +00 \quad 33-38 \\ \hline \end{array}$

31+00

$\begin{array}{r} \text{NW Cor Ho} \\ +82 \quad 70 \\ \hline \end{array}$

$\begin{array}{r} 1/2" \text{ Maple} \\ +71 \quad 31 \\ \hline \end{array}$

$\begin{array}{r} 1" \text{ Maple} \\ +89 \quad 31 \\ \hline \end{array}$

$\begin{array}{r} 1/2" \text{ Maple} \\ +48 \quad 31 \\ \hline \end{array}$

$\begin{array}{r} \text{SE Cor Gar (22')} \\ +39 \quad 61 \\ \hline \end{array}$

$\begin{array}{r} +24 \text{ E } 16' \text{ Bit. Ent. } \\ \text{SW Cor Ho \# 2922} \\ \hline \end{array}$

+14

$\begin{array}{r} \text{BT} \\ 20 \\ \hline \end{array}$

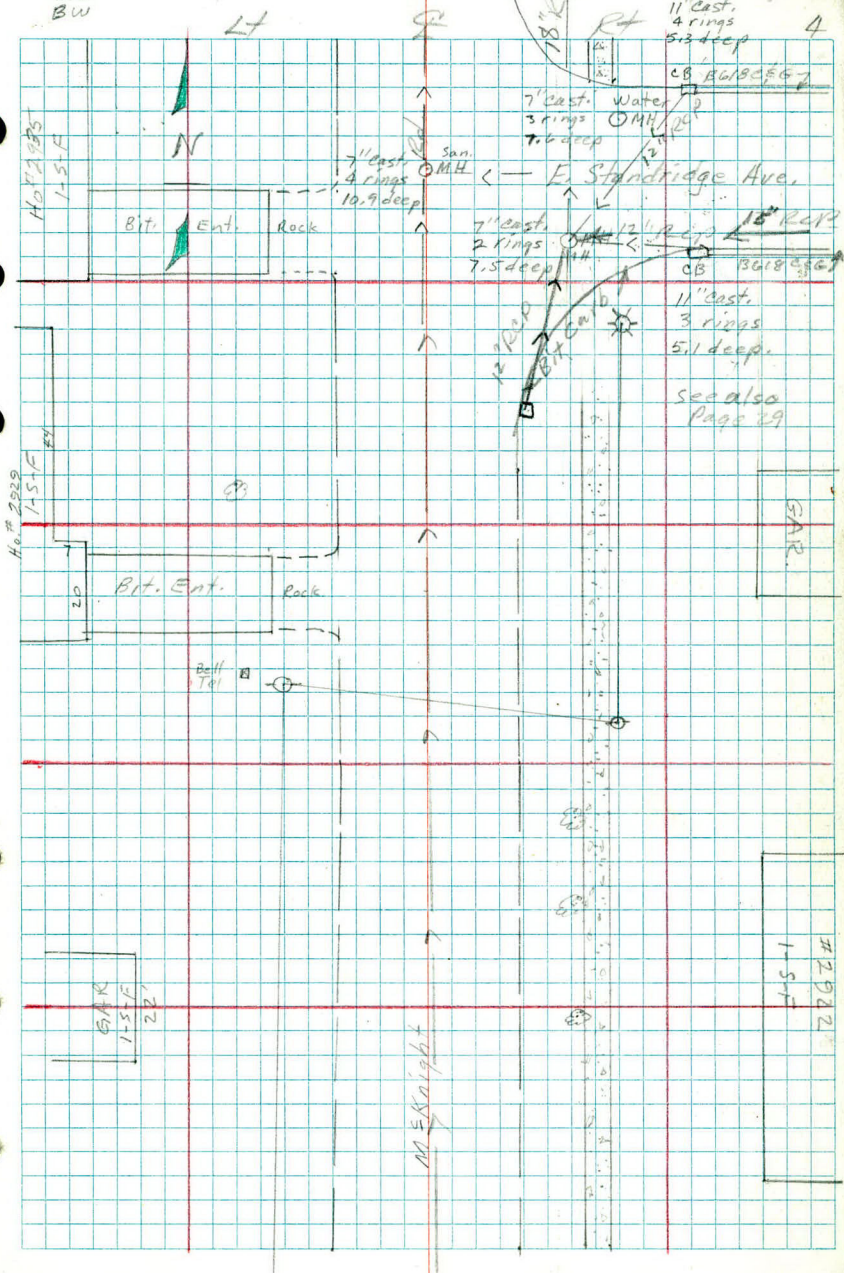
20 19

$\begin{array}{r} \text{S.W.} \\ +00 \quad 33-38 \\ \hline \end{array}$

30+00

RG
JA
KG
BW

Oct. 31, 1978
Clear 50° Windy



35+00 14 8 12

+90 NE Cor Ho
70
2" Maple
+97 41

20 20

+36 E 16' Bit Ent. / 33'
SE Cor Ho # 2957
70
+26
NE Cor Ho 70
+15 70 +19 Hyd 27

End 5' SW
+31 34-39
+25 MH ?
31
NW Cor Ho # 2946
71
+16 71 +18 ER 19
2" Ash CB + BR
+03 30 +13 24
SW Cor Ho # 2946
+90 71

34+00 +12 CB 23 19 19 Bit- +03 30 +13 24 19 19

+60 E 16' cone Ent / 40'

SE Cor Ho # 2951
+51 70
NE Cor Ho
+41 70

+68 E 16' Bit. Ent SW cor Gar # 2946
+60 92
SW
+54 34
SW
+50 34-39
NW Cor
+30 70

33+00

Bit-
19 19

SE Cor Ho # 2943
+76 70
4' Picket Fe.
+71 34+
NE Cor Ho # 2935
+65 70

+86 E 16' Bit. Ent. @ 33'
Bushes
35, 40, 45 etc

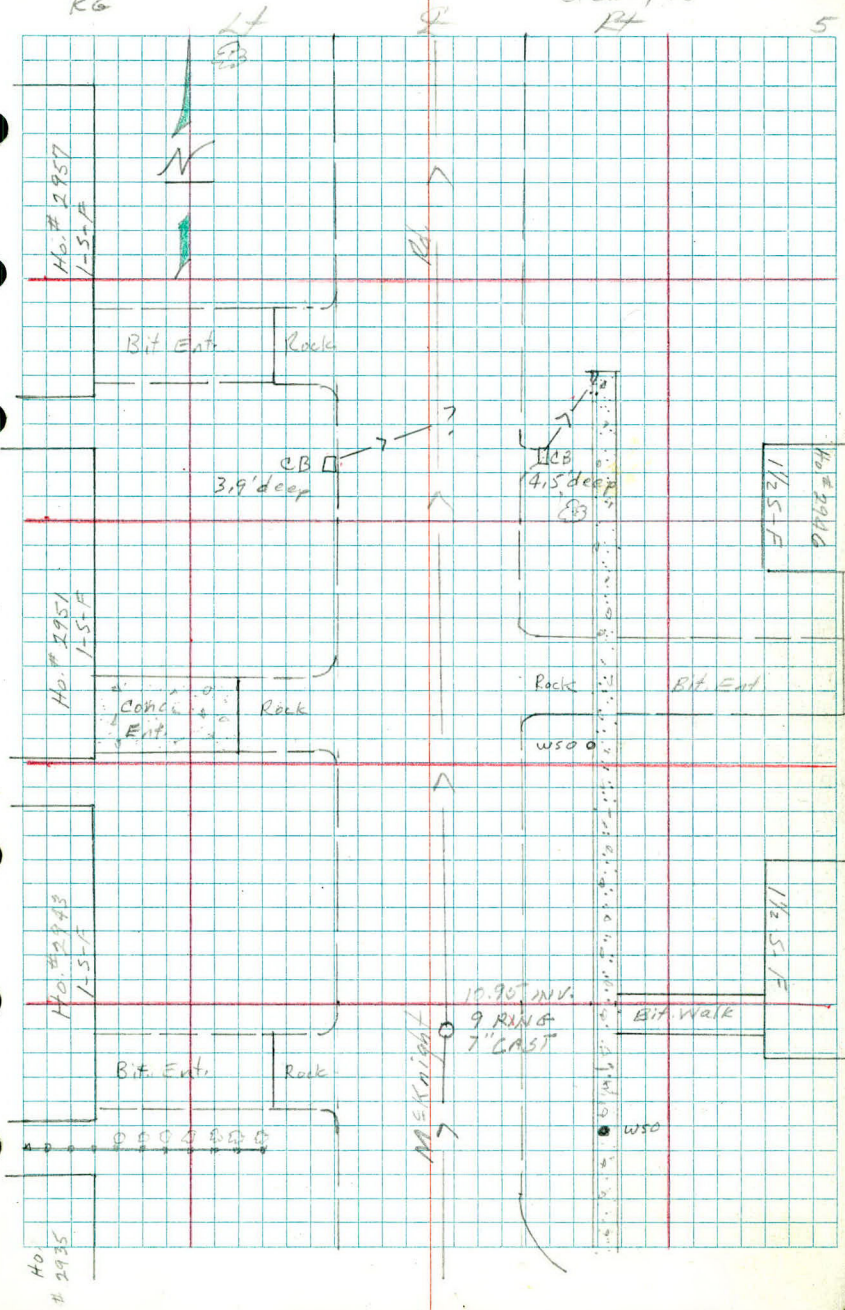
+98 E 8' Bit. Wall
SW Cor Ho
+89 70
SW
+74 37
ER 4
+62 Bit Curb
18

+95 MH
2

RG
DS
KG

Nov. 3, 1975
Clear, 65°
RT

5



1" Pine 1" Pine 2" Mt Ash

+40 34 +47 34 +46 42

1" Pine Lt Tri 3' Birch P
+34 34 +30 41
Juniper SE Cor Ho 2985

+24 41 +26 70
NE Cor Ho 2" Pine
+15 70 +23 34

1" Pine 1" Pine 1" Pine
+07 33 +15 35 +16 40
Tw 2" Birch Bit
37+00 +03 45 19 19

Rt

spread in
Juniper
+72 43

+59 E 16' Bit Ent / 36' SE Cor Ho
+51 70 2977

End Hedge
+43 39

+47 Mt
2

NE Cor Ho
+41 70
Tri 2' Birch
+29 46

36+00 Bit
19 19

+96 Beg Hedge
39

SE Cor Ho 2971
+76 70 +85 E 18' Conc Ent / 40'

NE Cor Ho End Hedge
+66 70 +66 36

2" Maple
+54 42

Beg Hedge
+48 36

1" Crab Apple
+21 50

+10 E 16' Conc Ent / 40'
SE Cor Ho 2963
35+00 +01 70

Bit
20 20

RG
LPD
DS
KG
RW

Nov. 4, 1975
Clear 50°
RT

C

Ho. #2985
1-5-F

Ho. #2977
1-5-F

Ho. #2971
1-5-F

Ho. #2963
1-5-F

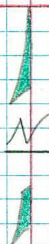
Handwritten symbols and asterisks in the top left area.

Rd

Rit.

Rock

10.25" IN V.
5" RINGS
7" CAST



OPEN FIELD

Rock

Rock

McKnight

+89 Beg Woods
41-57

$$+87 \frac{ER}{23} \quad +83 \frac{MH}{11}$$
$$\begin{array}{r} +74 \\ \hline 38 \end{array} \quad \begin{array}{r} \text{BR} \\ \text{Arc Lf} \\ +88 \\ \hline 38 \end{array}$$
$$\begin{array}{r} +60 \\ \hline 34 \end{array} \quad \begin{array}{r} +74 \\ \hline 48 \end{array} \quad \begin{array}{r} \text{Ben } 13618 \\ \hline \end{array}$$

Ben B618

127	50	110	1 Maple
			44

$$+19 \quad \frac{\text{cor} + e}{35 - 55 \text{ end}} + 27 \quad \frac{\text{ER}}{40 + \text{curb}}$$
$$+07 \quad \frac{CB}{26} \quad +10 \quad \frac{BR \text{ and } Hy}{22} \quad +12 \quad \frac{Hy}{25}$$

39 + 00 • $\frac{Fe \text{ cor}}{+100} \quad \underline{35}$

BIT curb
23 22

$$+84 \overline{) \begin{array}{r} \text{CORSW} \\ 28 \end{array}}$$

+72 BR +79 Cor 53. w.
50 32

[illegible]
$$\begin{array}{r} \text{MH} \\ 157 \overline{) 33} \end{array} \quad \begin{array}{r} \text{MH} \\ 149 \overline{) 2} \end{array} \quad \begin{array}{r} \text{MH} \\ 149 \overline{) 39} \end{array}$$
$$\begin{array}{r} \text{CB} \\ + 28 \overline{40} \end{array} \quad \begin{array}{r} \text{ER} \\ + 29 \overline{78} \end{array} \quad \begin{array}{r} \text{MH} \\ + 35 \overline{31} \end{array}$$

	Cor	Cor
--	-----	-----

$$\begin{array}{r} +17 \quad \text{S.W.} \\ \hline 25 \end{array} \quad \begin{array}{r} +22 \quad \text{S.W.} \\ \hline 30 \end{array}$$

Bit $\frac{BR + Bit \cdot curb}{22 + 100} = 30$

SE Corlto NE Corlto
+55 70 +80 70

[illegible]

+94	$\frac{NE \text{ Cor } 1 \text{ to}}{70}$	+97	$\frac{\text{Tree}}{36}$?
-----	---	-----	----------------------------

+84 £ 16 Bit Ent/29

1" Crab Apple
34

OPEN 1212-13

RG
LPD
KG
DS
BW

WOODS

CB
30" X 48"
14.5 deep

Nov 4, 1975
Clear 50°
3.9 Deep
Rt.

BUIB C&G

Bit. curb

MH (WATER)
11" Cast
10 Ad. Rings
6.9 Deep

OMH
7" Cast
9 Ad. Rings
7.0 Deep

MH (SAN.)
9" Cast
N Ad. Ring
14.0 Deep

Bit. curb

MH WATER
7" Cast
1 Ad. Ring
9.6 Deep

MH (SAN.)
7" Cast
1 Ad. Ring
12.0 Deep

MH (STORM) 36" R.C.P.

BUIB C&G

Bit. curb

2 wood rail fence

CB
3' X 4'
4.3 deep

15" R.C.P.

12" R.C.P.

Deep gate 3' X 4'
5.4 Deep

MH STORM
7" Cast
1 Ad. Ring
9.2 Deep
7' X 5' Precast

see also
page 30

2-5-F

Bit. Ent.

Rock

No. 2085
1-5-F

M Knight

UNCULTIVATED

Lt

£

Rt

$$+26 \frac{\text{Woods}}{48+}$$

42+00

$$+00 \frac{\text{Woods}}{50+}$$

$$\text{Bit} \\ 12/12$$

$$+00 \frac{\text{Woods}}{50+}$$

$$+81 \frac{\text{PP}}{38}$$

$$+77 \frac{12'' \text{ Ash}}{32}$$

$$+37 \frac{15'' \text{ oak}}{44}$$

$$+42 \frac{12'' \text{ oak}}{47}$$

$$+07 \frac{\text{Beg Woods}}{62-77}$$

41+00

$$+00 \frac{\text{Woods}}{50+}$$

$$\text{Bit} \\ 12/12$$

$$+88 \frac{15'' \text{ oak}}{51}$$

$$+73 \frac{\text{Tw } 15'' \text{ oak}}{43}$$

$$+77 \frac{\text{Tw } 8'' \text{ oak} + 18'' \text{ oak}}{58}$$

$$+50 \frac{\text{Woods}}{50+}$$

$$+60 \frac{\text{Tw } 12'' \text{ oak}}{43}$$

$$+68 \frac{5'' \text{ oak}}{40}$$

$$+44 \frac{\text{Tw } 18'' \text{ oak}}{38}$$

$$+26 \frac{\text{Tw } 10'' \text{ oaks}}{32}$$

$$+41 \frac{10'' \text{ oak}}{38}$$

$$+15 \frac{\text{Bit}}{13 \text{ Lt} + \text{RT}}$$

40+00

$$+12 \frac{\text{CB}}{22}$$

$$23/23$$

$$+12 \frac{\text{CB}}{24}$$

+09 end Bit curb
Lt + RT 23'

45+00 Lt

£

Rt

BR
+97 22 195 Conc 195 GA Bit 12

+71 Conc 75-94 94-118
+71 GA 75-94 94-118

+67 Flag Pole 50 Cor Conc Ent +46 Bit 12-21

+63 45 Rt +72

+42 Cor Conc Ent 39 Rt = +51

+51 NE Cor Ho

+20 8" Maple 40 +36 2" Maple 50

+15 3" Pine 47 +17 Tri 4" Birch 60

44+00 +07 3" Pine 44 +09 3" Pine Bit 12 12

Bush +90 47 +97 47

+95 SE Cor Ho 3045
+75 RT = +08

+83 4" Birch 46 +80 39

+76 24 oak 50

+62 £ 14' Bit Ent to Ho # 3033
+41 3" Pine 31 +50 Cor Woods 10" oak 42

+35 MH 2

+19 End Woods 24" oak 57

43+00 +00 Woods 41 + 12 12

+93 10" oak 49 +97 15" oak 62 +99 15" oak 50

+85 woods 65 +

RG
LPO
KG
VS
BW

Nov 4, 1975
clear 60°

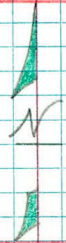
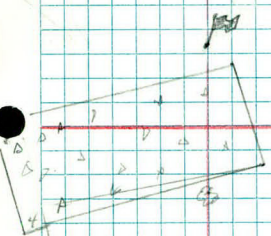
Lt

Rt

Rt

9

1 1/2 story
Hwy #3042



OPEN FIELD

Bit. Ent. to H₂ #3033

7' CAST
7' RINGS
13.70 INV

WOODS

McKnight

WOODS

H

E

R+

Quint.
 4" Poplars
 +21 38

47+00

Bit
 12 12

MH
 183 E

Bit
 +60 12-23

46+00 CB ER Bit CB
 +05 32 +09 24 12 +05 32

BR
 +84 52

MH
 +84 E

(+40 MH
 31)

ER
 +27 49

45+00 Hyd Bit
 +02 26 22 12

KG
LPD
DS
KG
BW

Nov. 4, 1975
clear 70°
Rt

H

E

10



7" CASTING
4 RINGS
14.1 FL TO TOP

OPEN FIELD

3.85' deep CB

CB 3.7' deep

sa

MH

7" cast
2 rings
14.1' deep

12" TO N
20" TO N

MEKNIGHT

36" TO 50"

11" CASTING
6 RINGS
8.75 FL TO TOP

50+00

Lt

2

Rt

Bit
16 16

+70 $\frac{Bit}{12}$

+70 $\frac{Bit}{12}$

+44 $\frac{Hyd}{27}$

+00 Power Line X-ing

Bit
12 12

49+00

$\frac{MH}{31}$
+72 ?

+60 $\frac{Pipeline Marker}{44}$

48+00

Bit
12 12

RG
LPD
DS
KG
BW

Lt

♀

Nov. 4, 1975
Clear 74°

Rt

11

N

Bd.



P

P

P

MH
O



FL TO TOP 8.65

11" CASTING
3 RINGS

M = Knight

Lt

Z

Rt

$$+34 \quad \frac{5' \text{ Poplar}}{29} \quad +41 \quad \frac{PP}{33}$$

52+00

 curb Bit curb
24 24

$$+78 \quad \frac{5-4'' \text{ cott}}{40}$$

$$+69 \quad \frac{MH}{20} \quad ?$$

$$+26 \quad \frac{3-4'' \text{ cott}}{36}$$

51+00

$$\begin{array}{ccc} \text{Bit} & \text{CB} & \text{ER} \\ \text{curb 23} & +06 \quad \frac{23}{23} & +09 \quad \frac{24}{24} \end{array}$$

$$+82 \quad \frac{MH}{10} \quad \text{WSO}$$

$$+88 \quad \frac{MH}{1}$$

$$+92 \quad \frac{BR+Bit}{40}$$

$$+79 \quad \frac{CB}{24}$$

$$\begin{array}{c} +69 \quad \frac{MH}{30} \\ +66 \quad \frac{ER+curb}{40} \end{array}$$

$$+68 \quad \frac{CB}{38}$$

$$+17 \quad \frac{\text{Beg bit curb}}{19}$$

$$\begin{array}{c} +48.21 \\ +13 \quad \frac{\text{Beg Bit curb}}{17} \end{array}$$

50+00

1614

RG
LPD
KG

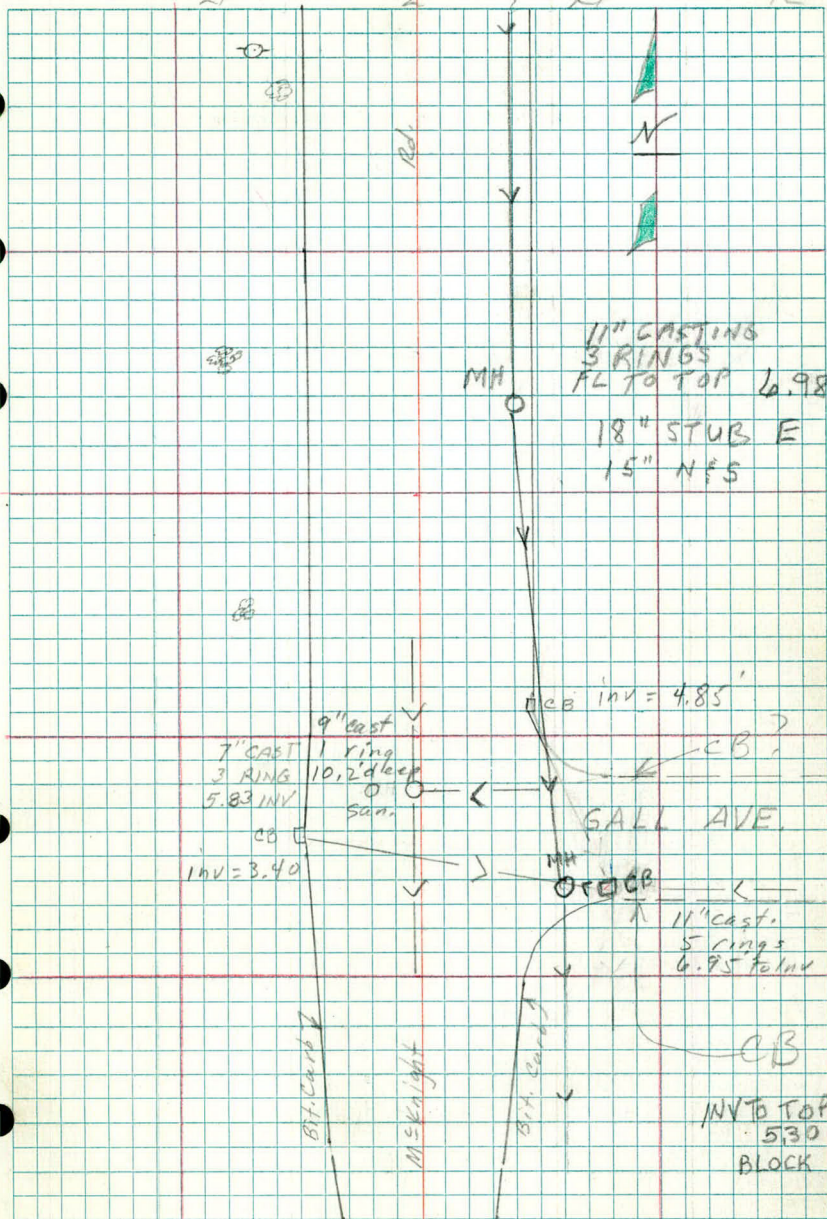
Nov 5, 1975
Clear 55°

Lt

St

Rt

12



55+00

Lt

$$\begin{array}{r} \text{ER} \\ +00 \quad 29 \end{array}$$

$$\begin{array}{r} \text{Bit} \\ 24 \quad 24 \end{array}$$

$$\begin{array}{r} \text{ER} \\ +00 \quad 32 \end{array}$$

$$\begin{array}{r} \text{Beg.} \\ \text{GVRail} \\ +74 \quad 32 \end{array}$$

$$\begin{array}{r} \text{ER} \\ +90 \quad 32 \end{array}$$

$$\begin{array}{r} \text{ER} \\ +62 \quad 25 \end{array}$$

$$\begin{array}{r} \text{ER} \\ +68 \quad 24 \end{array} +68$$

$$\begin{array}{r} \text{Beg.} \\ \text{Guard Rail} \\ 36 \end{array}$$

$$\begin{array}{r} \text{BR} \\ +36 \quad 57 \end{array}$$

$$\begin{array}{r} \text{BR} \\ +36 \quad 58 \end{array}$$

$$\begin{array}{r} \text{mont} \\ +24 \quad \text{CORD} \end{array}$$

$$\begin{array}{r} \text{ER} + \text{Bit} \\ \text{curb} \\ +05 \quad 44 \end{array}$$

$$\begin{array}{r} \text{MH} \\ +07 \quad 1 \end{array}$$

$$\begin{array}{r} \text{End Curb} \\ +10 \quad 60 \end{array}$$

$$\begin{array}{r} \text{Wood 15" cm} \\ +03 \quad 62 \end{array}$$

54+00

$$\begin{array}{r} \text{CIB + ER} \\ +09 \quad 44 \end{array}$$

$$\begin{array}{r} \text{Beehive} \\ \text{CB} \\ +02 \quad 45 \end{array}$$

$$\begin{array}{r} 6" \text{ Pine} \\ +90 \quad 41 \end{array}$$

$$\begin{array}{r} \text{Hyd} \\ +89 \quad 27 \end{array}$$

End Bit Curb

$$\begin{array}{r} \text{BR} \\ +91 \quad 24 \end{array}$$

$$\begin{array}{r} \text{Arch Lt} \\ +96 \quad 32 \end{array}$$

$$\begin{array}{r} 6" \text{ Pine} \\ +76 \quad 41 \end{array}$$

$$\begin{array}{r} \text{BR} \\ +77 \quad 24 \end{array}$$

$$\begin{array}{r} \text{MH} \\ +88 \quad 20 \end{array}$$

$$\begin{array}{r} \text{NW cor Bar} \\ +45 \quad 64 \end{array}$$

$$\begin{array}{r} \text{ER} \\ +48 \quad 24 \end{array}$$

$$\begin{array}{r} \text{SW cor Bar} \\ +21 \quad 64 \end{array}$$

$$\begin{array}{r} 10" \text{ Elm} \\ +32 \quad 50 \end{array}$$

$$\begin{array}{r} \text{Board} \\ +23 \quad 47 \end{array}$$

$$\begin{array}{r} \text{POR} \\ +37 \quad 26 \end{array}$$

$$\begin{array}{r} \text{POR} \\ +10 \quad 27 \end{array}$$

$$\begin{array}{r} \text{ER} \\ +07 \quad 37 \end{array}$$

53+00

$$\begin{array}{r} \text{BR} \\ +03 \quad 24 \end{array}$$

$$\begin{array}{r} \text{cor 170} \\ +95 \quad 66 \end{array}$$

Rt +37

$$\begin{array}{r} \text{Bit} \\ \text{curb} \\ 24 \quad +04 \end{array}$$

$$\begin{array}{r} 4" \text{ Pine} \\ +81 \quad 41 \end{array}$$

$$\begin{array}{r} 4" \text{ Pine} \\ +92 \quad 41 \end{array}$$

$$\begin{array}{r} 6" \text{ Pine} \\ +68 \quad 41 \end{array}$$

$$\begin{array}{r} \text{cor 6" Pines} \\ +54 \quad 40 \end{array}$$

RG
LPD
KG

Nov. 5, 1975
clear 60°

13

Lt

Rt

Rt.

PL

N

CO. RD.

7" Cast.
5 rings
14.2' deep San

"D"

CB

BH

20' x 15' CM

ENT

MAD

7 rings
11" CASTING *
FLTS TOP 6.12

SB GAR.

Bit. Curb

Bit. Ent

Bit. Curb

MSE Knight

Bit. Curb

*

* * * * *

LT

E

RT

56+00

56+00

+68 LT / Curb/26' +71.4 Bridge E +74 RT / Curb/26'

+35 E Beg Bridge Approach Slab

End B624
+35 26
Beg B624 CB
+27 26 +35 26

End B624
+35 26 +41 34 Hand Hole
B624
+28 26 +35 25 CB

56+00

24 24

RG
LPD
KG

Nov. 5, 1975
Clear 65°

LT

RD

RT

19

N

WBL

IG94

BRIDGE

IG94

EBL

15" CM

5.1' deep

MEK right

7.7 ?
Filled with Sand
4.7' deep

58400

58400

L.P.D.
GA.
B.J.

17- FEB-77
CLDY- 30°

1

TOPO

MC KNIGHT RD

BEAM AVE. to COUNTY RD. "D"

HO # 3101 LOC.

STA. 51 to 53

LT

2

RT

53+00

RD
23

+50

+61 WSO
30

+36 NE COR. HO[#] 3121
66-92

52+00

RD
23

+70 SE COR. HO[#] 3121
66-92

+50

51+00

50+93 RD
34

RD
23

L.P.D.
G.A.
B.J.

2T

4

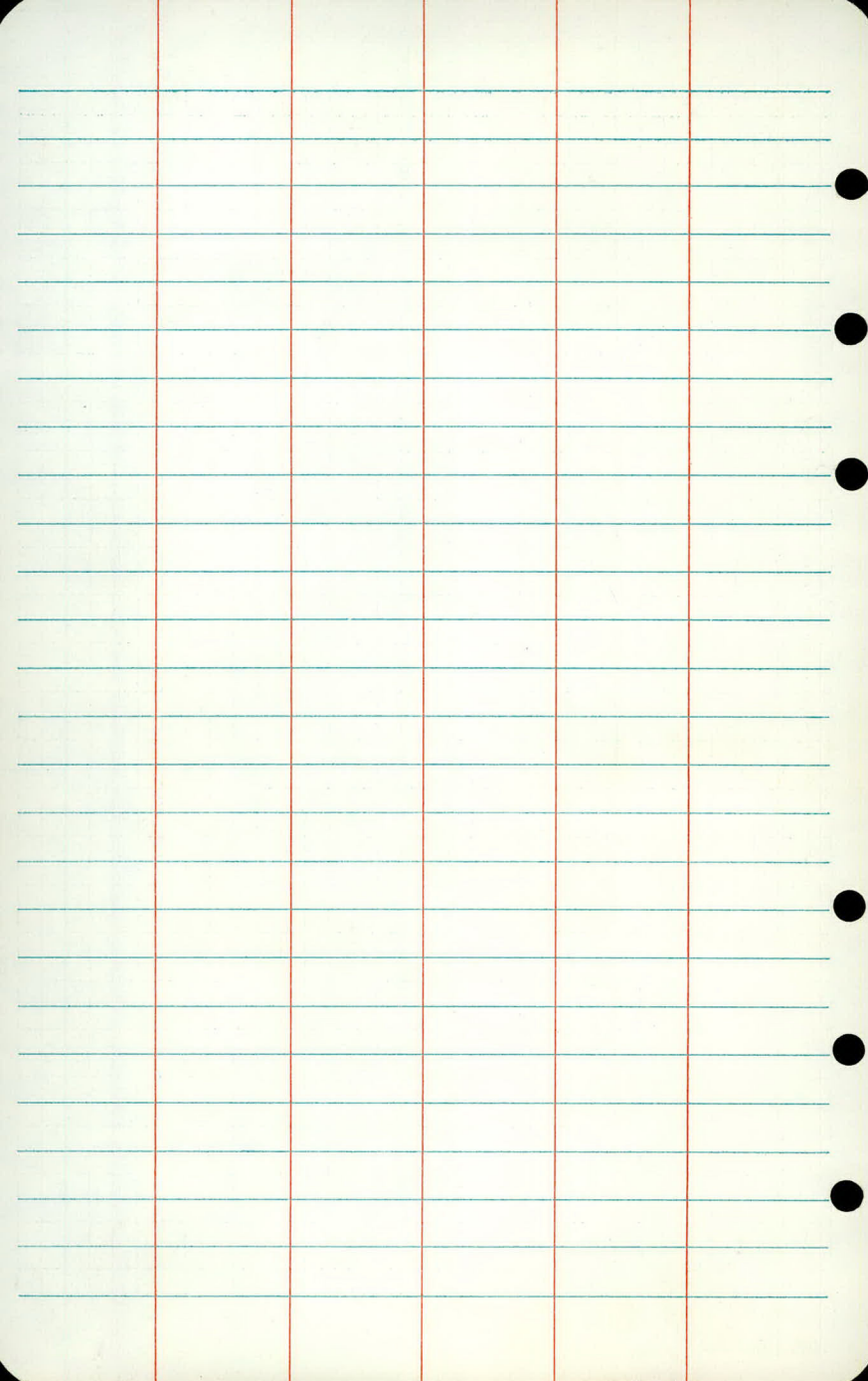
17-FEB-77
CLDY, 300
RT

2

HO 3121

WSD
9

9



RG
LPD
KG

Nov 6, 1975
Overcast 60°

1

BENCH LEVELS

McKnight Rd

from

Beam Ave. to Co. Rd. "D"

2 pages

Sta	+	-	E/V.	
BM ₁	0.79	998.07	997.28	
BM ₂	0.82	991.89	7.00	991.07
BM ₃	0.32	982.09	10.12	981.77
TP ₁	3.73	974.04	11.78	970.31
BM ₄	4.30	970.58	7.76	966.28
BM ₅	5.61	974.29	1.90	968.68
BM ₆	10.31	983.15	1.45	972.84
BM ₇	6.16	988.18	1.13	982.02
BM ₈	2.66	988.24	2.60	985.58
				985.470
BM ₇	0.80	982.82	6.22	982.02 ok
BM ₆	0.63	973.47	9.98	972.84 ok
BM ₅	1.08	969.77	4.78	968.69 968.68
BM ₄	7.62	973.93	3.46	966.31 966.28
TP ₁	11.54	981.87	3.60	970.33 970.31
BM ₃	9.65	991.45	0.07	981.80 991.77
BM ₂	6.86	997.95	0.36	991.09 991.07
BM ₁			0.66	997.29 997.28

RG
LPD
KG

Nov 6, 1975
Overcast 65°

Description

2

Top Hyd. SE cor M^sKnight $\frac{1}{2}$ Beam Ave.

" " N.W. " " $\frac{1}{2}$ Maple Lane

" " Lt. Sta. 34+20

E Sta 37+00

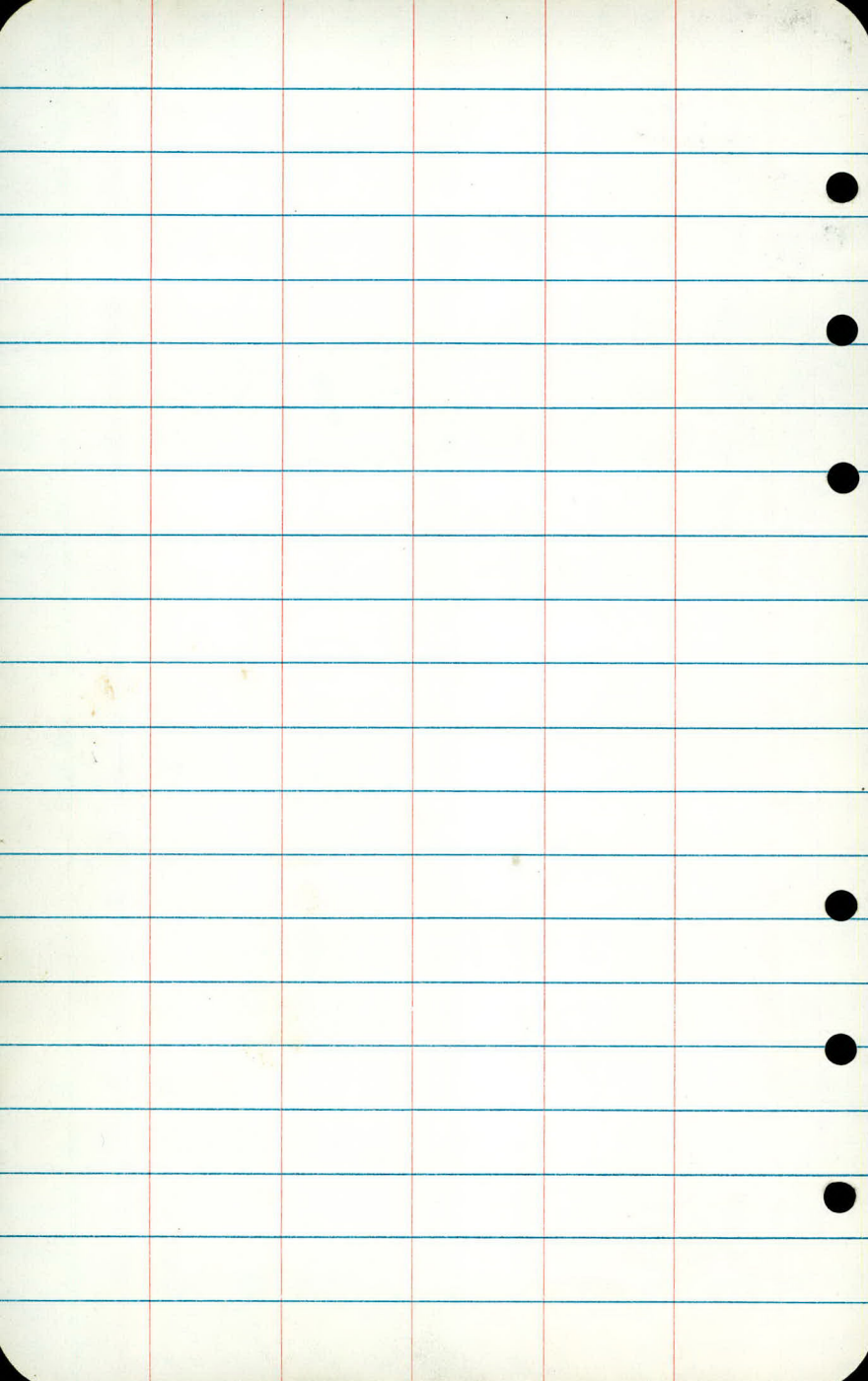
Top Hyd SW cor M^sKnight $\frac{1}{2}$ Lydia

" " Lt Sta 45+00

" " " " 49+40

" " S.W. cor. M^sKnight $\frac{1}{2}$ Co Rd "D"

MHD BM disk #6286 E on SE Wing wall Bridge #62837
over I 694.



RG
LPD
KG

Nov. 6, 1975
PC 60°

1

X-SECTIONS

McKnight Rd.

from

Beam Ave. to Co. Rd. "D"

pages

Sta	+	π	-	Elev.
BM	2.71	999.99		997.28
25+87			6.20	93.79

26+00

+06

Gutter Lt only

+13

Gutter Rt only

+22

5.71 94.28

+28

2 Beam E.

BM	2.72	1000.00	2.71	997.28
----	------	---------	------	--------

+28

E Beam W.

✓

RG
LPD
KG Lt

Nov 6, 1975
PE 60°
RT 2

Top Hyd. S.E. Cor. McKnight $\frac{1}{2}$ Beam
rim MH Rt 11'

94.1	94.3	94.2	93.6	94.0	94.0	94.7	94.8	94.8
5.9	5.7	5.8	6.4	6.0	6.0	5.3	5.2	5.2
50	40	24	16	18	24	43	50	
			BT	BT				

93.82	93.37	94.14	93.68	93.8	94.1
6.17	6.62	5.85	6.31	6.2	5.9
TC	BC	T.C.	32	TC	
50	50	32	24	BT	

94.2	94.17	94.3	94.08	94.6	94.7
5.8	5.82	5.7	5.91	5.4	5.3
	C	20	32	45	50
	MH		MH		

rim MH Rt 1'

94.3	94.6	95.3	95.8	96.4	97.3	98.3
5.7	5.4	4.7	3.6	2.7	1.7	
24	50	100	150	200		

RG
LPD
KG

Nov 7, 1975
Overcast 55°

92.9	93.52	93.8	94.1	94.3
7.1	6.48	6.2	5.9	5.7
100	70	50	16	
	MH			
92.0	91.2			
8.0	8.8			
150	200			

Sta	+	Δ	-	Elv.
-----	---	---	---	------

		1000.00		
--	--	---------	--	--

26+50				Gutter L+Rt
-------	--	--	--	----------------

Note: WSO 26+51 Rt 33'! put on top

✓

+56				
-----	--	--	--	--

27+00				Ent Rt.
-------	--	--	--	---------

+50				
-----	--	--	--	--

+90				Top Bank Rt.
-----	--	--	--	-----------------

TP	3.04	995.68	7.36	992.64
----	------	--------	------	--------

KG
LPD
KG
L+

Nov 7, 1975
overcast 550

RT

3

93.41	94.13	93.67	93.9	94.3	94.4	94.8	95.07	95.56
6.59	5.87	6.33	6.1	5.7	5.6	5.2	4.93	4.44
SD	34	34	14		18	42	57	T.C.
BC	T.C.	BC	BT		BT	BT	BC	
		Gutter					Gutter	

93.87	92.77	93.15
6.13	7.23	6.85
SD	93	93
T.C.	BC	T.C.

96.24	95.72
3.76	4.28
90	90
T.C.	BC

93.8	93.9	93.8	93.89	94.2	94.3	94.5	95.1	95.3	95.5
6.2	6.1	6.2	6.11	5.8	5.7	5.5	4.9	4.7	4.5
SD	31	17	14		16	29	30	33	SD
			MH		BT	BT	T.C.		
							(6.7)		

94.3	93.7	93.5	93.7	93.8	95.34	95.72	96.3
5.7	6.3	6.5	6.3	6.2	4.66	4.28	3.7
SD	27	14		17	34	45	SD
					conc	conc	NG

93.3	93.4	93.0	93.3	93.5	93.2	95.2	95.9
6.7	6.6	7.0	6.7	6.5	6.8	4.8	4.1
SD	24	14		11	18	33	SD
		BT		BT			

92.5	93.0	92.2	92.5	92.8	92.7	92.4	94.3	95.4
7.5	7.0	7.8	7.5	7.2	7.3	7.6	5.7	4.6
SD	24	18	13		11	16	33	SD
			BT		BT			

Sta 28+00

Sta	+	π	-	E/V
-----	---	-------	---	-----

		995.68		
--	--	--------	--	--

28+04				
-------	--	--	--	--

				Bottom Bank Rt
--	--	--	--	-------------------

+50				
-----	--	--	--	--

+82				
-----	--	--	--	--

				Ent. Rt
--	--	--	--	---------

✓				
---	--	--	--	--

29+00				
-------	--	--	--	--

+28				
-----	--	--	--	--

				B.R. Lt
--	--	--	--	---------

KG
LPD
KG

Lt

♀

Nov 6, 1975
overcast 55°
RT

4

92.2	92.7	92.0	92.3	92.6	92.4	92.3	93.68	92.73	94.1
3.5	3.0	3.7	3.4	3.1	3.3	3.4	2.00	1.95	1.6
50	23	19	14	✓	11	19	34	39	50
			BT		BT		S.W.	SW	

92.3	92.2	92.1	91.1	91.4	91.7	91.6	91.6	92.90	93.00	94.0
3.4	3.5	3.6	4.0	4.3	4.0	4.1	4.1	2.78	2.68	1.7
50	35	23	20	12	✓	12	19	34	39	50
				BT		BT		SW	SW	

91.5	91.5	91.3	90.4	90.6	91.0	90.8	91.2	92.17	92.25	93.4
4.2	4.2	4.4	5.3	5.1	4.7	4.9	4.5	3.51	3.43	2.3
50	35	23	20	13	✓	12	21	34	39	50
				BT				SW	SW	BT

95.02

0.66
66
conc

91.1	91.0	90.2	90.4	90.6	90.5	90.4	91.83	91.88	92.9
4.6	4.7	5.5	5.3	5.1	5.2	5.3	3.85	3.80	2.8
50	25	20	12	✓	11	15	34	39	50
					BT		SW	SW	BT

89.8	90.42	89.99	89.7	90.0	89.9	89.9	91.26	91.30	91.9
5.9	5.26	5.69	6.0	5.7	5.8	5.8	4.42	4.38	3.8
50	23	23	17	✓	13	18	34	39	50
	TC	BC	BT		BT		SW	SW	

gutter

Sta + T - Elev.

995.68

29+40

Gutter Lt
Ent Rt

+56

E Maple Lane

BM

4.60 991.08 991.07

TBM

5.33 990.35

BM

3.57 994.64 991.07

+73

Gutter
Lt

+86

B.R. Lt

30+00

BM

0.27 991.34 3.57 991.07

991.07

RG
LPD
ICG

Nov 6, 1975
Overcast 55°

Lt

Rt

Rt

5

89.21	88.74	89.72	89.27	89.5	89.7	89.6	90.2	90.94	91.02	91.71
6.47	6.94	5.96	6.41	6.2	6.0	6.1	5.5	4.74	4.66	3.97
SD	SD	34	34	18	✓	12	23	34	39	SD
TC	BC	TC	BC	BT		BT		SW	SW	Comp Ent.
84.9	86.2	87.5	88.9	89.1	89.4	89.3	89.2	90.64	90.68	91.7
10.8	9.5	8.2	6.8	6.6	6.3	6.4	6.5	5.04	5.00	4.0
200	150	100	50	18	✓	12	17	34	39	50
						BT		SW	SW	

Top Hyd NW cor Maple Lane $\frac{1}{2}$ M E K.

RR spike in Arc Lt Pole NW cor Maple Lane $\frac{1}{2}$ M E K.

88.77	88.32	89.16	88.70	88.5	89.1	88.8	89.6	90.30	90.32	91.6
5.87	6.32	5.48	5.94	6.1	5.5	5.8	5.0	4.34	4.32	3.0
SD	SD	33	33	17	✓	18	22	34	39	50
TC	BC	T.C.	BC	BT		BT		SW	SW	
88.9	89.11	88.73	88.3	88.8	88.7	88.4	89.4	90.00	90.01	91.5
5.7	5.53	5.91	6.3	5.8	5.9	6.2	5.2	4.64	4.63	3.1
50	21	21	16	✓	13	18	22	34	39	50
	T.C.	B.C.	BT		BT	BT		S.W.	SW	
89.4	89.1	88.8	88.1	88.4	88.4	88.2	89.1	89.74	89.78	91.1
5.2	5.5	5.8	6.5	6.2	6.2	6.4	5.5	4.90	4.86	3.5
50	40	23	19	✓	12	19	22	34	39	50
					BT	BT		SW	SW	

Above BM @ Maple Lane

Sta	+	π	-	Elev.
-----	---	-------	---	-------

		991.34		
--	--	--------	--	--

30+25				
-------	--	--	--	--

			2.15	89.19
--	--	--	------	-------

+50				
-----	--	--	--	--

31+00				
-------	--	--	--	--

+35				
-----	--	--	--	--

				B.4. Ent Lt
--	--	--	--	----------------

+70				
-----	--	--	--	--

32+00				
-------	--	--	--	--

TP	4.02	988.04	7.32	984.02
----	------	--------	------	--------

R6
LPD
KG

Nov. 13, 1975
PC 35°

Lt

♀

Rt

6

Wedge conc. S.W. Rt 34' Ent to H₂ #2922

90.3	90.2	87.8	88.0	87.5	87.0	87.3	87.1	86.9	87.6	88.62	88.71	90.1
1.0	1.1	3.5	3.3	3.8	4.3	4.0	4.2	4.4	3.7	2.72	2.63	1.2
60	50	32	23	20	19		11	18	20	34	39	50
				TC	BT	✓		BT		SW	SW	

88.9	88.4	86.6	86.5	85.9	86.2	86.1	85.6	86.5	87.42	87.48	87.7
2.4	2.9	4.7	4.8	5.4	5.1	5.2	5.7	4.8	3.92	3.86	3.6
60	50	30	20	19		12	19	23	34	39	50
			TC	BT	✓		BT		SW	SW	

87.5	86.2	85.2	85.5	85.1	84.8	85.7	86.75	86.80	87.9
3.8	5.1	6.1	5.8	6.2	6.5	5.6	4.59	4.54	3.4
50	33	18		12	18	21	34	39	50
BT	BT	BT	✓		BT		SW	SW	

87.3	85.7	84.8	84.4	84.7	84.3	84.0	84.6	85.96	86.01	87.0
4.0	5.6	6.5	6.9	6.6	7.0	7.3	6.7	5.38	5.33	4.3
50	25	19	18	✓	12	20	20	34	39	50
		TC	BT			BC	TC	SW	SW	

86.7	85.2	84.7	83.7	84.0	83.6	83.2	83.8	84.1	84.5
4.6	6.1	6.9	7.6	7.3	7.7	8.1	7.5	7.2	6.8
50	28	20	18	✓	12	39	39	50	75
		TC	BT			BC	TC		

PK nail ♀ Sta. 32+00

Sta	+	π	-	E/V.
-----	---	-------	---	------

		988.04		
--	--	--------	--	--

32+05				
-------	--	--	--	--

				Gutter Rt
--	--	--	--	-----------

				So edge Bit Ent Lt
--	--	--	--	-----------------------

+09				
-----	--	--	--	--

✓				
---	--	--	--	--

+08				
-----	--	--	--	--

			4.59	83.45
--	--	--	------	-------

+23				
-----	--	--	--	--

				R Stand- ridge Ave
--	--	--	--	-----------------------

+33				
-----	--	--	--	--

			4.95	83.09
--	--	--	------	-------

				MH Rt 40'
--	--	--	--	--------------

+38				
-----	--	--	--	--

				Gutter Rt
--	--	--	--	-----------

✓				
---	--	--	--	--

+50				
-----	--	--	--	--

RG
LPD
KG

Nov. 13, 1975

Lt

2

Rt

7

86.9

85.1

83.6

83.9

83.5

83.4

83.14

83.40

83.86

1.1

2.9

4.4

4.1

4.5

4.6

4.90

4.64

4.18

50

31

18

12

27

5.1

57

57

BT

BT

BT

BT

BT

CB

BC18

TC

84.17

83.72

387

4.32

91

91

TC

BC

MH 12+30'

see also page 29

86.6

83.8

83.2

83.38

83.1

83.2

83.3

84.2

85.4

87.4

1.4

4.2

4.8

4.66

4.9

4.8

4.7

3.8

2.6

0.6

50

19

18

MH

12

38

50

100

150

200

TC

BC

BT

BT

BT

BT

BT

BT

BT

86.5

84.9

83.3

82.7

83.1

82.6

82.9

83.5

83.4

83.42

1.5

3.1

4.7

5.3

4.9

5.4

5.1

4.5

4.70

4.62

50

34

20

19

18

43

43

55

58

58

TC

BC

BT

BT

BT

BT

BT

BT

BT

84.30

83.82

83.90

3.74

4.22

4.14

100

100

58

TC

BC

TC

46

86.3

84.8

83.2

82.5

82.8

82.3

82.4

83.0

83.98

84.06

84.2

1.7

3.2

4.8

5.5

5.2

5.7

5.4

5.0

4.06

3.98

3.8

50

35

20

19

18

24

24

24

35

40

50

TC

BC

BT

BT

BT

TC

SW

SW

SW

Sta	+	x	-	Elev.
-----	---	---	---	-------

988.04

So. edge
Bit, Ent Lt.

32+81

TP	4.50	986.32	6.22	981.82
----	------	--------	------	--------

33+00

+61

End of Ent Lt
So edge Bit Ent
Rt

34+00

BM	1.94	983.71	4.55	981.77	981.77
----	------	--------	------	--------	--------

+13

1.94
3.11

+30

End S.W.
Rt
Ent Lt

RG
LPD
KG

Nov. 13, 1975

LT

L

RT

8

842	824	818	821	818	826	83.21	83.27	845
3.8	4.6	6.2	5.9	6.2	3.4	4.83	4.77	3.5
50	35	18	✓	19	25	35	40	50
BT	BT	BT		BT		SW	SW	

PK sta 33

840	825	819	816	818	814	817	82.97	83.08	827
2.3	3.8	4.4	4.7	4.5	4.9	4.6	3.35	3.24	2.6
50	29	20	19	✓	18	19	35	40	50
		TC	BC		BT		SW	SW	BT
									ENT

81.79	81.41	81	80.1	80.3	80.1	79.7	81.52	81.52	82.5
4.53	4.91	5.2	6.2	6.0	6.2	6.6	4.80	4.80	3.8
48	40	38	18	✓	12	20	35	40	50
Cone joint	Cone	Rock	BT			BT	SW	SW	BT

816	806	79.6	79.0	79.4	79.0	78.5	79.2	80.49	80.52	82.3
4.7	5.7	6.7	7.3	6.9	7.3	7.8	7.1	5.83	5.80	4.0
50	35	20	18	✓	12	19	24	35	40	50
		TC	BT			BT		SW	SW	
			(BC)							

Top Hyd LT 34+20

Nov. 17, 1975

810	79.1	78.10	78.9	79.0	78.6	77.81	78.8	80.15	80.24	82.3
2.7	4.6	5.61	4.8	4.7	5.1	5.90	4.9	3.51	3.47	1.4
50	25	24	12	✓	12	24	25	35	40	50
	NG	CB	BT		BT	CB	NG	SW	SW	

79.6	79.1	78.3	78.5	78.6	78.2	77.7	79.63	79.70	81.7
4.1	4.6	5.4	5.2	5.1	5.5	6.0	4.08	4.01	2.0
50	37	20	12	✓	12	19	35	40	50
BT	BT	BT			BT		SW	SW	NG

Sta	+	π	-	E/V.
-----	---	-------	---	------

		983.71		
--	--	--------	--	--

34+65				
-------	--	--	--	--

35+00				
-------	--	--	--	--

+10				
-----	--	--	--	--

		6.64	77.07	
--	--	------	-------	--

+50				
-----	--	--	--	--

+85				
-----	--	--	--	--

		8.93	74.78	
--	--	------	-------	--

36+00				
-------	--	--	--	--

✓				
---	--	--	--	--

Nov. 17, 1975
Clear 40°

LT E RT 9

79.5	78.9	77.8	77.2	77.4	77.5	77.3	77.0	77.4	78.7	79.7
4.2	4.8	5.9	6.5	6.3	6.2	6.4	6.7	6.3	5.0	4.0
50	36	28	18	11	✓	12	18	20	35	50
			BT				BT	TC		

77.5	77.0	76.4	75.9	76.2	76.4	76.2	76.0	76.4	78.0	79.9	80.4
6.2	6.7	7.3	7.8	7.5	7.8	7.5	7.7	7.3	5.7	3.8	3.3
50	34	20	20	12	✓	12	19	20	33	43	50
		TC	BT				BT	TC			

Edge Conc Ent LT 40'

76.8	75.8	75.4	74.6	74.8	74.9	74.7	74.4	74.8	76.0	79.9	79.1
6.9	7.9	8.3	9.1	8.9	8.8	9.0	9.3	8.9	7.7	3.8	4.6
50	36	20	18	11		13	20	21	32	44	50
			TC	BT			BT	TC			

Edge Conc Ent LT 40'

74.3	73.2	73.0	73.2	73.4	73.3	72.9	73.4	74.6	78.5	78.4
9.4	10.5	10.7	10.5	10.3	10.4	10.8	10.3	9.1	5.2	5.3
29	20	19	12		12	20	21	33	45	50
	TC	BT				BT	TC			

74.9	75.2
8.8	8.5
44	50

76.9	76.8
6.8	6.9
75	43

Sta	+	T	-	Elev.
-----	---	---	---	-------

		983.71		
--	--	--------	--	--

+50				
-----	--	--	--	--

✓				
---	--	--	--	--

+60				
-----	--	--	--	--

			11.6	
--	--	--	------	--

				72.1
--	--	--	--	------

37+00				
-------	--	--	--	--

✓				
---	--	--	--	--

TP				
----	--	--	--	--

	6.08			
--	------	--	--	--

		978.43		
--	--	--------	--	--

			11.36	
--	--	--	-------	--

				972.35
--	--	--	--	--------

+50				
-----	--	--	--	--

✓				
---	--	--	--	--

Nov. 17, 1973

LT

R

RET

10

13.2	12.7	12.1	11.5	11.8	11.9	11.7	11.3	11.8	13.2	14.6
10.5	11.0	11.6	12.2	11.9	11.8	12.0	12.4	11.9	10.5	9.1
50	37	21	20	12		12	19	21	29	37
		TC	BT				BT	TC		

78.3	78.7	79.6	79.4
5.4	5.0	4.1	4.3
75	61	50	47

Edge Bit Ent Lt 37'

72.4	71.9	70.8	70.4	70.0	70.3	69.9	69.7	70.0	70.5	72.7
11.3	11.8	12.9	13.3	13.7	13.4	13.8	14.0	13.7	13.2	11.0
50	41	28	19	18		12	20	21	26	32
			TC	BT			BT	TC		

80.6	80.9	78.7
3.1	2.8	5.0
75	50	48

Top 2x6 Lt Sta 36 + 75 ±

70.9	70.2	69.1	68.5	68.5	68.7	68.6	68.3	68.6	68.8	70.8	76.2
7.5	8.2	9.3	9.9	9.9	9.7	9.8	10.1	9.8	9.6	7.6	2.2
50	37	21	19	12		12	19	19	24	26	41
		TC	BT				BT	TC			

see pg. 14

11.2
1.2
43

Sta	+	π	-	Elev.
-----	---	-------	---	-------

		978.43		
--	--	--------	--	--

37+85				
-------	--	--	--	--

			9.3	
--	--	--	-----	--

				69.1
--	--	--	--	------

38+00				
-------	--	--	--	--

+13				
-----	--	--	--	--

TBM				
-----	--	--	--	--

		6.28	972.15	
--	--	------	--------	--

+50				
-----	--	--	--	--

✓				
---	--	--	--	--

BM				
----	--	--	--	--

	7.35			
--	------	--	--	--

		973.63		
--	--	--------	--	--

			12.17	
--	--	--	-------	--

				966.26
--	--	--	--	--------

				966.28
--	--	--	--	--------

Nov, 17, 1973

LT

E

RT

11

BT Ent @ 33'

70.0	68.9	67.6	67.0	67.1	67.2	67.1	66.9	67.3	69.6	74.9	76.5
8.4	9.5	10.8	11.4	11.3	11.2	11.3	11.5	11.1	8.8	3.5	6.9
50	32	20	19	12		12	18	19	32	47	50
		TC	BT				BT	TC			

see pg 14

66.7	66.9	67.2	66.5	66.7	66.8	66.6	66.4	66.8	68.5	72.6	75.2
11.7	11.5	11.2	11.9	11.7	11.6	11.8	12.0	11.6	9.9	5.8	3.2
50	40	20	19	12		12	19	20	27	44	50
		TC	BT				BT	TC			

see pg 14

Top 4x4 RT Sta 38

65.8	65.8	65.2	65.5	65.6	65.4	65.3	65.8	67.7	71.2
12.4	12.6	13.2	12.9	12.8	13.0	13.1	12.6	10.7	7.2
39	20	19	11		12	19	20	28	41
		TC	BT			BT	TC		

66.1

12.3
50

73.2

5.2
75

72.8

5.6
50

Top Hyd. sw cor Lydia & M&K.

Sta + π - Elev.

973.63

39+00

✓

+08

9.43 64.20

+08

8.66 64.97

+08

10.0 63.63

+17

So. edge
Sidewalk Rt.

+28

Gutter

✓

Nov. 17, 1973

LT RT 12

64.8	64.6	63.9	64.1	64.2	64.2	64.0	64.6	64.1	68.3
8.8	9.0	9.7	9.5	9.4	9.4	9.6	9.0	7.5	5.3
36	20	19	11		12	20	21	29	42
	TC	BT				BT	TC		

65.1
8.5
50

68.9
68.2
4.7
5.4
75
50

Lip of CB LT 24'

Top CB LT 24'

existing ^{gutter} FL at CB LT 24'

64.1	64.1	64.6	64.0	63.8	64.0	64.0	63.7	63.85	64.07	64.37	64.77
9.5	9.5	9.0	9.4	9.8	9.6	9.6	9.9	9.78	9.56	9.26	8.86
50	36	24	23	12		13	26	26	50	75	100
		TC	BT				BT	S.W.			

63.46	63.09	64.2	63.6	63.8	63.8	63.8	62.25	63.8	63.3	63.9
10.17	10.54	9.4	10.0	9.8	9.8	9.8	10.38	9.8	10.3	9.7
50	50	37	37	11		12	40	40	50	50
TC	B618 C46	TC					CB	TC	BC	TC

62.55
11.08
75
BC

63.03
10.60
75
TC

65.01
8.62
119
TC

64.54
9.09
119
C46

64.5
9.1
99
TC

63.99
9.64
99
CB

64.2
9.4
75
TC

63.6
10.0
75
BC

B624

Sta + π - E/v.

973.63

39+49

$\neq$ Lydia

✓

+57

10.10 63.53

+60

10.03 63.60

+73

Gutter RT
(+74 Gutter LT)

✓

✓

NOV. 17, 1975

LH

R

RT

13

62.9	63.5	63.6	63.6	63.64	63.5	63.3	63.64	63.7
10.7	10.1	10.0	10.0	9.99	10.1	10.3	9.99	9.9
75	50	37	12	MH	12	18	39	50
				R			MH	

62.4	61.5	60.7
11.2	12.1	12.9
100	150	200

MH RT 34'

MH LH 33'

61.5	65.9	64.5
6.1	7.7	9.1
200	150	100

63.08	63.9	63.3	63.4	63.5	63.2	63.3	63.8	63.3	63.9
10.55	9.7	10.3	10.2	10.1	10.4	10.3	9.8	10.3	9.7
48	35	35	14		19	46	46	50	50
B618	TC	BC				BT	TC	BC	TC
C4G									

63.55	63.21	62.78
10.08	10.42	10.85
48	64	64
TC	TC	BC

64.5	63.95	64.2	63.6
9.1	9.68	9.4	10.0
99	99	75	75
TC	CB	TC	BC

64.50	64.96
9.13	8.67
119	119
B624	TC
C4G	

Sta + π - E/V.

973.63

NO. side
of S.W.

39+84

40+00

BM

7.34 966.29

TBM

12.22 984.37

972.15

37+50

38+00

+13

TP

10.93 973.44

973.4

199

Nov 17, 1975

LT

R

RT

14

64.6	64.0	63.9	63.4	63.30	63.5	63.3	63.0	63.23	63.97	64.77
9.0	9.5	9.7	10.2	10.33	10.1	10.3	10.6	10.40	9.66	8.86
50	42	24	24	11		13	29	29	50	100
		TC	BT	MH				S.W.	S.W.	S.W.

67.1	66.5	63.7	63.1	63.2	63.4	63.3	62.9	63.4	64.2	65.0
6.5	7.1	9.9	10.5	10.4	10.2	10.3	10.7	10.2	9.4	8.6
50	32	25	24	16		11	22	22	40	50
		TC	BT				BT	TC		

Top Hyd Lydia

Top 4x4 Rt 38+00

77.3	82.8	83.4
7.1	1.6	1.0
43	59	77

76.5	80.4	80.5
7.9	4.0	3.9
50	60	75

75.3	78.3	79.5
9.1	6.1	4.9
50	59	75

Sta 36

Sta	+	π	-	Elev.
-----	---	-------	---	-------

BM	9.54	975.82		966.28
----	------	--------	--	--------

40+13

✓

+50

41+00

+50

42+00

Nov. 17, 1975

LT R RT 15

Top Hyd SW cor Lydia & McK.

64.0	64.01	62.8	63.2	63.4	63.2	61.5	63.80	64.3	65.0
11.8	11.81	13.0	12.6	12.4	12.6	14.3	12.02	11.5	10.8
30	26	24	16		12	23	23	36	50
CB	Top CB	FL CB	BT		BT	FL CB	Top CB		
65.2	66.6	68.7							
10.6	9.2	7.1							
30	34	50							
NG Bank									

73.4	73.9	69.5	63.6	63.4	63.7	63.3	63.4	65.0	67.7	64.3
2.4	1.9	6.3	12.2	12.4	12.1	12.5	12.4	10.8	8.1	9.5
50	36	30	20	16		12	19	28	40	50
				BT		BT				

70.8	72.0	72.5	67.7	63.9	63.9	64.1	63.8	62.7	65.4	68.1	68.5
5.0	3.8	3.3	8.1	11.9	11.9	11.7	12.0	12.1	10.4	7.7	10.3
50	37	30	26	18	12		12	16	27	43	50
					BT		BT				

64.4	65.0	67.0	64.1	64.0	64.3	64.3	64.2	66.6	72.4	74.7	73.1
11.4	10.8	8.8	11.7	11.8	11.5	11.5	11.6	9.2	2.4	1.1	2.7
50	35	29	19	12		12	17	30	50	54	60
				BT		BT					

65.0	64.9	66.8	64.4	64.5	64.6	64.6	65.5	68.6	74.8	79.4	
10.8	10.9	9.0	11.4	11.3	11.2	11.2	10.3	7.2	1.0	+3.6	
50	44	34	20	12		11	25	38	50	73	
				BT		BT					

sta + π - EIV

975.82

42+50

43+00

TP 2.88 970.93 7.77 968.05

+48

+60

Ent. Lt

44+00

+50

conc. ent
lt

Nov. 17, 1975

Lt

L

Rt

16

75.3

73.7

64.7

64.9

65.1

64.9

64.8

66.0

66.0

66.7

0.5

2.1

11.1

10.9

10.7

10.9

11.0

9.8

9.8

9.1

50

35

17

12

BT

11

BT

18

28

43

50

72.4

74.0

68.8

64.9

65.2

65.3

65.3

65.5

65.5

65.6

2.4

1.8

7.0

10.9

10.6

10.5

10.5

10.3

10.3

10.2

50

38

27

19

12

BT

12

BT

29

46

50

Rock

71.9

71.2

68.0

65.7

65.5

65.6

65.5

65.5

65.5

+1.0

+0.3

2.9

5.2

5.4

5.3

5.4

5.4

5.4

50

42

32

21

12

BT

12

BT

30

50

68.7

67.1

65.6

65.7

65.6

65.5

65.5

2.2

3.8

5.3

5.2

5.3

5.4

5.4

50

33

12

BT

12

BT

31

50

69.0

67.3

65.9

65.9

65.9

65.8

65.9

65.7

1.9

3.6

5.0

5.0

5.0

5.1

5.0

5.2

50

37

22

12

BT

12

BT

31

50

67.38

66.83

66.0

66.2

66.2

66.1

65.6

65.8

3.55

4.10

4.9

4.7

4.7

4.8

5.3

5.1

50

43

20

12

BT

13

BT

33

50

core

core

Sta + T - E/V

970.93

45+00

BM 9.52 978.20 2.26 968.67 968.68

+30

+55

L Woodlynn
Lt

✓

+82

+84

11.19 67.01

RG
LPD
DS
KG

LT

2

Nov 18, 1975
cidg 450
RT

17

66.5	66.4	66.4	66.5	66.3	66.3	66.2
4.4	4.5	4.5	4.4	4.6	4.6	4.7
50	25	10		12	33	50
		BT		BT		

Top Hyd LT Sta 45

66.3	66.4	66.4	66.2	66.7	66.5	66.2	67.0	66.5
11.9	11.8	11.8	12.0	11.5	11.7	12.0	11.2	11.7
75	50	38	12		12	18	33	50
BT	BT	BT	BT		BT			

66.6	66.9	66.5	66.4	66.6	66.8	66.6	66.4	67.4	67.8
11.6	11.3	11.7	11.8	11.6	11.4	11.6	11.8	10.8	10.4
100	50	32	12	12		12	18	26	50
		BT	BT	BT		BT			
			edge						

66.5	66.1
11.7	12.1
150	200

66.1	66.4	66.6	66.6	66.8	66.9	66.9	66.7	67.2	67.6	68.5
12.1	11.8	11.6	11.6	11.4	11.3	11.3	11.5	11.0	10.6	9.7
75	50	40	13	13		12	19	26	45	50
			BT	BT		BT				
			edge							

MH 2

Sta + π - E/U

978.20

45+88

46+00

+04

+50

47+00

+50

Nov. 18, 1975

Lt

L

Rt

18

67.2	67.2	66.7	66.9	67.2	67.0	66.8	67.3	67.7	69.0
11.0	11.0	11.5	11.3	11.0	11.2	11.4	10.9	10.5	9.2
50	37	34	12		12	17	24	39	50
		BT	BT		BT				

67.6	67.5	67.0	66.7	67.1	67.3	67.1	66.9	67.4	68.2	69.8
10.6	10.7	11.2	11.5	11.1	10.9	11.1	11.3	10.8	10.0	8.4
50	43	28	26	12		12	18	25	41	50
			BT	BT		BT				

67.68
10.52
33
CB

67.45
10.75
33
CB

67.3	67.5	66.8	67.5	67.8	67.7	67.5	68.2	68.8	72.6
10.9	10.7	11.4	10.7	10.4	10.5	10.7	10.0	9.4	5.6
50	26	22	12		12	18	26	39	50
			BT		BT				

67.1	67.4	67.7	68.2	68.4	68.4	68.2	68.9	69.7	74.6	74.6
11.1	10.8	10.5	10.0	9.8	9.8	10.0	9.3	8.5	3.6	3.6
50	39	20	12		12	18	28	38	47	60
			BT		BT					

67.2	68.7	68.4	69.0	69.2	69.0	68.8	69.7	70.3	76.1	76.2
11.0	9.5	9.8	9.2	9.0	9.2	9.4	8.5	7.9	2.1	2.0
50	28	20	12		12	17	26	41	50	60
			BT		BT					

Sta + π - FIV

978.20

48+00

TP 13.08 982.63 8.65 969.55

+50

49+00

+50

50+00

T.P 7.82 980.66 9.80 972.83 972.84

Nov. 18, 1975

LT

Q

RT

19

65.7	67.5	68.9	68.9	69.7	69.8	69.7	69.4	70.3	70.7	77.5	78.2
12.5	10.7	9.3	9.3	8.5	8.4	8.5	8.8	7.9	7.5	0.7	0.6
50	40	29	21	12		12	19	24	39	50	50
				BT		BT					

Rock

66.5	67.8	69.7	69.4	70.3	70.6	70.5	70.0	70.6	71.1	78.0
16.1	14.8	12.9	13.2	12.3	12.0	12.1	12.6	12.0	11.5	4.6
50	37	29	21	12		12	19	25	38	50
				BT		BT				

64.6	65.6	69.1	69.5	70.4	71.1	71.3	71.3	70.9	71.5	72.3	75.7	76.9
18.0	17.0	13.5	13.1	12.2	11.5	11.3	11.3	11.7	11.1	10.3	6.9	5.5
50	49	39	32	27	13		12	18	21	39	45	50
					BT		BT					

65.7	66.5	70.2	71.6	71.1	71.7	71.9	71.9	71.8	72.9	73.0
16.9	16.1	12.4	11.0	11.5	10.9	10.7	10.7	10.8	9.7	9.6
50	45	36	26	18	12		12	18	34	50
					BT		BT			

68.8	70.5	71.9	72.4	72.8	72.6	74.1	75.3
13.8	12.1	10.7	10.2	9.8	10.0	8.5	7.3
50	43	31	16		16	33	50
			BT		BT		

TOP HYD LT 49750

Sta + A - EIV

980.66

50+50

+68

Gutter Rt

MH Rt 28'

+80

7.12

73.54 H
~~75.51~~

+87

6.17

74.49 H
76.46

+80

E GALL ST Rt

+91

Gutter Rt

51+00

GA
DS
K6
RJ

11-24-75
cloudy 11°

LT

Q

R

20

72.2	73.8	74.0	73.8	73.3	73.4	73.5	73.3	73.2	73.1	73.6	74.1	76.4
8.5	6.9	6.7	6.9	7.4	7.3	7.2	7.4	7.5	7.6	7.1	6.6	4.3
50	40	34	25	24	17		11	17	24	25	28	50

74.1	74.7	74.4	74.2	73.7	73.8	74.0	73.8	73.96	74.8	75.6
6.6	6.0	6.3	6.5	7.0	6.9	6.7	6.9	6.70	5.9	5.1
50	41	36	25	24	17		13	28	50	25

CB LT 24'

MH Q

74.3	74.9	74.5	74.0	74.4	74.0	75.0	75.8	77.1	79.7
6.4	5.8	6.2	6.7	6.3	6.7	5.7	4.9	3.6	1.0
50	40	28	17		25	50	75	100	150

74.5	73.1	74.6	74.3	74.7	74.3	74.3	75.0	76.0
6.2	7.6	6.1	6.4	6.0	6.4	6.4	5.7	4.7
50	39	26	17		22	30	50	75

71.6	72.2	73.9	74.7	74.4	74.6	74.8	74.34	74.9	75.4	77.5
9.1	8.5	6.8	6.0	6.3	6.1	5.9	6.32	5.8	5.3	3.2
50	43	37	26	25	17		24	25	33	50

Sta	+	π	-	E/V.
-----	---	-------	---	------

		980.66		
--	--	--------	--	--

TP	8.67	983.42	5.91	974.75
----	------	--------	------	--------

51+50

52+00

+50

53+00

+20

ENT LEFT

GA
OS
K6
RJ

11-24-75
cldy cold 11°

Lt

2

12

21

PK Sta 51+00 2

74.4	75.3	75.3	74.8	75.6	75.7	75.8	75.7	75.3	75.8	76.3	75.6	74.5
9.0	8.1	8.1	8.6	7.8	7.7	7.6	7.7	8.1	7.6	7.1	7.8	8.9
50	29	25	24	17	14	26	13	25	26	33	41	50

75.1	76.5	77.1	76.6	76.7	77.0	77.0	76.8	77.6	77.1	75.2	75.2
8.3	6.9	6.3	6.8	6.7	6.4	6.4	6.6	5.8	6.3	8.2	8.2
50	30	25	24	17	13	23	24	31	39	50	50

77.4	77.2	78.6	78.1	77.8	78.2	78.3	78.0	78.4	78.4	75.4	74.9
6.0	6.2	4.8	5.3	5.6	5.2	5.1	5.4	5.0	5.0	8.0	8.5
50	38	25	24	18	13	24	25	29	36	50	50

81.2	80.8	79.4	78.9	79.3	79.1	79.6	80.1	79.2
2.2	2.6	4.0	4.5	4.1	4.3	3.8	3.3	4.2
50	30	25	24	24	25	38	50	50

81.1	80.3	79.4	79.6	79.3	79.8	80.6	81.1
2.3	3.1	4.0	3.8	4.1	3.6	2.8	2.3
50	35	24	24	25	31	50	50

Sta + Δ - I/V.

983.42

53+50

54+00

TP 4.37 984.58 3.21 980.21

+07 Gutter Pt: LT ^{NHE} 4.25 80.33

+23 ϕ Co Rd "D" Pt: LT

BM 7.13 989.15 2.55 982.03 982.02

GA
DS
KG
RJ

11-24-75
COLD 11°

Lt

2

Rt

22

81.0	80.7	79.8	79.3	79.7	79.5	80.1	80.9	81.3
2.4	2.7	3.6	4.1	3.7	3.9	3.3	2.5	2.1
50	31	25	24		24	25	37	50

79.2	79.9	79.4	79.5	80.2	80.4	80.4	80.9	80.0	80.1
4.2	3.5	4.0	3.9	3.2	3.0	3.0	2.5	3.4	3.3
50	30	29	22		19	33	34	42	50

PK sta 54+00 2

78.3	78.8	79.3	79.4	79.7	80.4	80.7	80.39	80.7	81.3	81.4
6.3	5.8	5.3	5.2	4.9	4.2	3.9	4.19	3.9	3.3	3.2
100	75	50	43	20		23	45	50	75	100

77.0	77.9	78.7	79.4	80.4	81.1	81.9	83.1	84.3
7.6	6.7	5.9	5.2	4.2	3.5	2.7	1.5	0.3
800	150	100	50		50	100	150	200

TOP HYD SIN COR MCKNIGHT'S "D"

Sta + π - E/V

989.15

54+36

+55

55+00

+39

Begin Conc Pave

+73

56+00

TP 6.46 994.62 0.99 988.16

GA
KG
DS
RT

11-24-75
Cold 11°

L+

L

R+

23

78.9	79.3	79.8	80.2	80.5	81.1	81.4
10.3	9.9	9.4	9.0	8.7	8.1	7.8
83	43	21		17	50	75

78.4	79.4	80.3	80.5	80.8	80.9	80.8	80.4	78.3
10.8	9.8	8.9	8.7	8.4	8.3	8.4	8.8	10.9
50	41	27	15		18	32	45	60

78.7	81.4	82.3	82.5	82.7	82.5	82.2	81.6	78.5
10.5	7.8	6.9	6.7	6.5	6.7	7.0	7.6	10.7
50	39	28	15		16	28	38	50

79.5	84.0	84.4	83.82	84.19	83.81	84.33	84.0	79.9
9.7	5.2	4.8	5.33	4.96	5.34	4.82	5.2	9.3
50	33	27	26		26	27	34	50

83.74	84.99	85.47	85.11	85.87
Tc			Tc	
3.41	4.16	3.68	4.04	3.28
27	26		26	27

86.71	85.95	86.52	86.17	86.98
Tc				Tc
2.44	3.20	2.63	2.98	2.17
27	26		26	27

COR COM - SW 56+30 RT 27'

Sta + π - EIV

994.62

56+50

57+00

+50

58+00

+50

59+00

GA
KG
DS
RJ

11-24-75.
cold 11°

LT

E'

RT

24

88.23

6.39

89.46

5.16

90.21

4.41

90.66

3.96

90.80

3.82

90.78

3.84

Sta + π - E/V.

994.62

59+50

12.58 982.04 982.02

GA
K6
DS
RJ

11-24-75
cold 119

LT

R

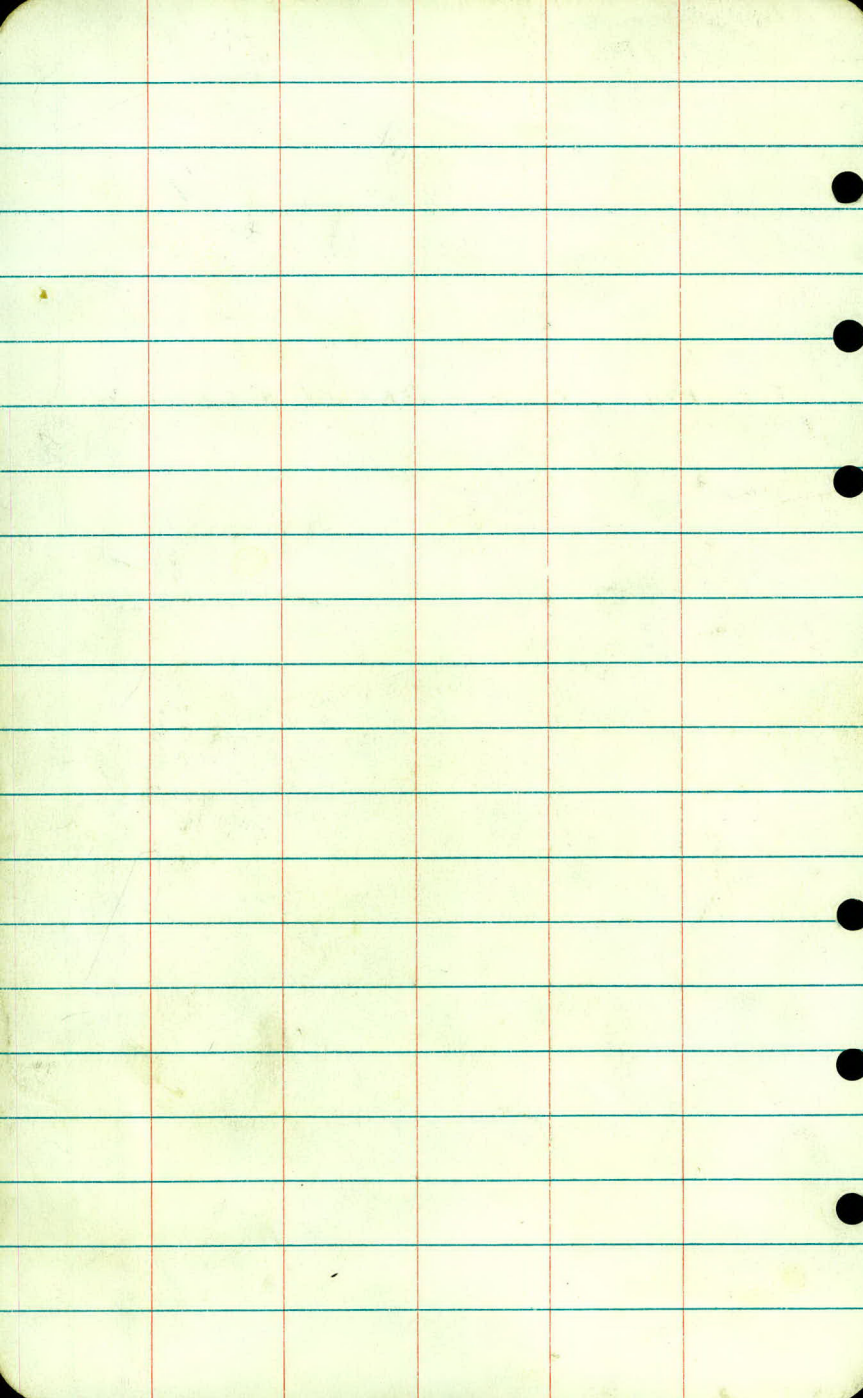
Rt.

25

90.7

4.45

TOP HYD SW COR McKnight & Co Rd "D"

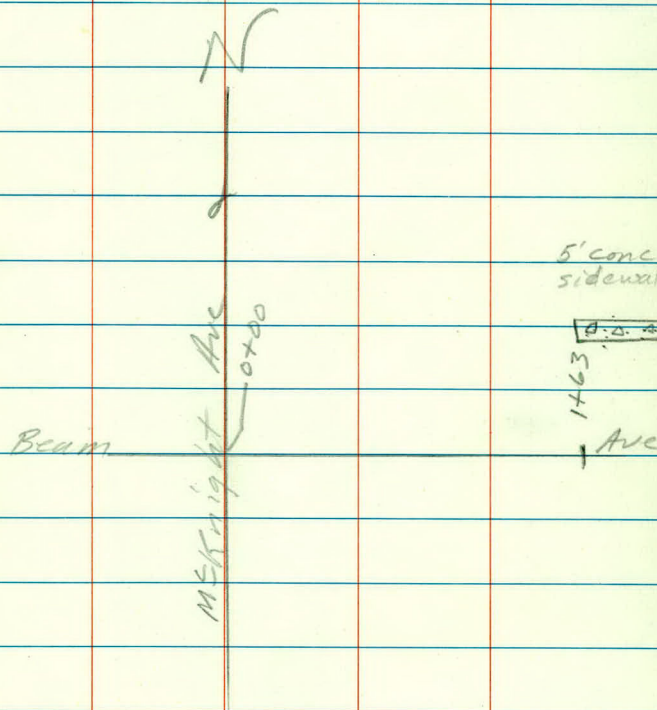


RG
LPD
DS
GA

Jan 14, 1976
Clear 10° 26

Additional X-Sections

NE Cor M^EKnight & Beam Aves.



Sta	+	Σ	-	Elv.
-----	---	----------	---	------

BM	2.82	1000.10		997.28
----	------	---------	--	--------

Beam Ave
0+25

0+50

0+75

1+00

+25

Jan 14, 1974

LT

E

27

Top Hyd SE Cor M[±] Knight & Beam

5.5	5.5	5.5	6.1	5.9	5.5
45	38	29	29	16	Bit
NG	NG	T.C. B.C.			

4.7	4.9	5.4	4.9
43	22	22	Bit
NG	T.C. B.C.		

2.9	4.50	4.95	4.2
42	22	22	Bit
NG	B618		

2.2	3.61	4.12	3.7
42	22	22	Bit
NG	B618		

2.0	3.16	3.66	3.2
41	22	22	Bit
NG	B618		

Sta

+

π

-

Elv

1000.10

1+50

+63

TBM

5.80

994.30

(94.28)

END

Jan 14, 1976

Lt

2

28

2.2	2.76	3.25	2.8
42	22	22	Bit
NG	B618		

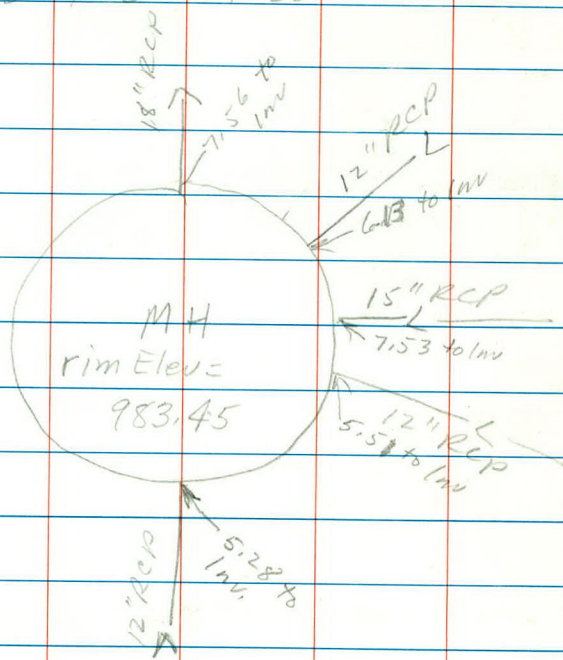
2.2	2.18	2.24	2.49	2.98	2.5
47	33	28	22	22	Bit
NG	S.W.	S.W.	B618		

Rim MH 26 + 22 Rt 1'

RCP
LPD
DS
GA

Jan 14, 1976
clear 10°

M 1+ 32+08 RT 30°

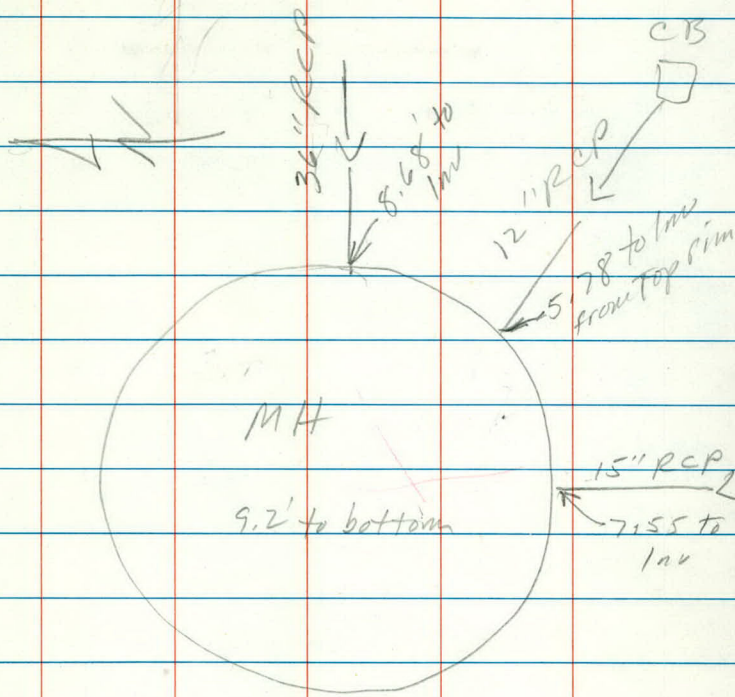


RG
LPD
DS
GA

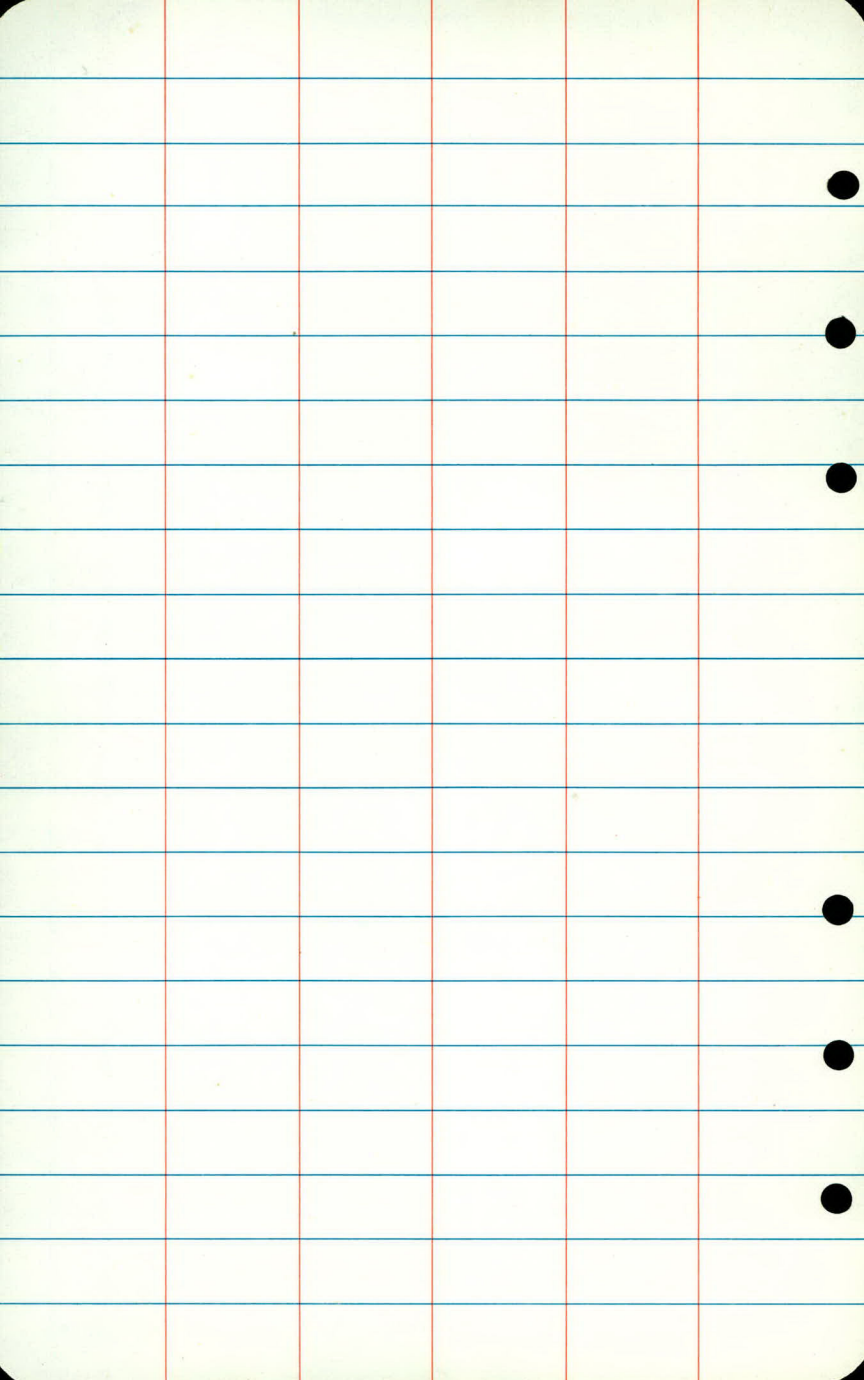
Jan 14, 1986
Clear 100

39+35 Rt 31

29



other inverts unobtainable



GA
LAD
DS
RT

1-23-76
cloudy 24°
30

62 - 668 - 14

MISC. MH : CB

ELEVATIONS

3 PAGES

Sta	+	-	Elev
BM	1.06	992.13	991.07
MH		981.56 10.57	
BM		10.37	981.76 981.77
BM	8.59	974.87	966.28
MH		971.54 3.33	
TP	6.55	970.08	11.34 963.53
MH		965.27 4.81	
BM		1.41	968.67 968.68
BM	6.42	979.26	972.84
MH		974.30 4.96	

GA
LPO
DS
RS

1-23-76
cloudy 23°

DESCRIPTION

31

TOP HYD NW COR MCKNIGHT; MAPLE LANE

32+95 RT 2'

TOP HYD 34+20 LT

TOP HYD SW COR MCKNIGHT; LYDIA

36+47 RT 2'

MH 39+35 RT 31'

43+35 RT 2'

TOP HYD LT 45+00

TOP HYD LT 49+40

50+88 LT 10'

STA	+	π	-	Elev
		979.26		
CB			974.21 5.05	974.21
TP	9.79	987.77	1.28	977.98
CB			979.81 8.42	979.35
CB			981.36 7.41	980.36
CB			983.53 4.24	
CB			983.40 4.37	
BM			982.02 5.75	982.02 (982.02)

GA
LPD
DS
RJ

125-76
cloudy 24"

DESCRIPTION

32

51+06 Rt 23'

COR OF ROCK IN BIT RW

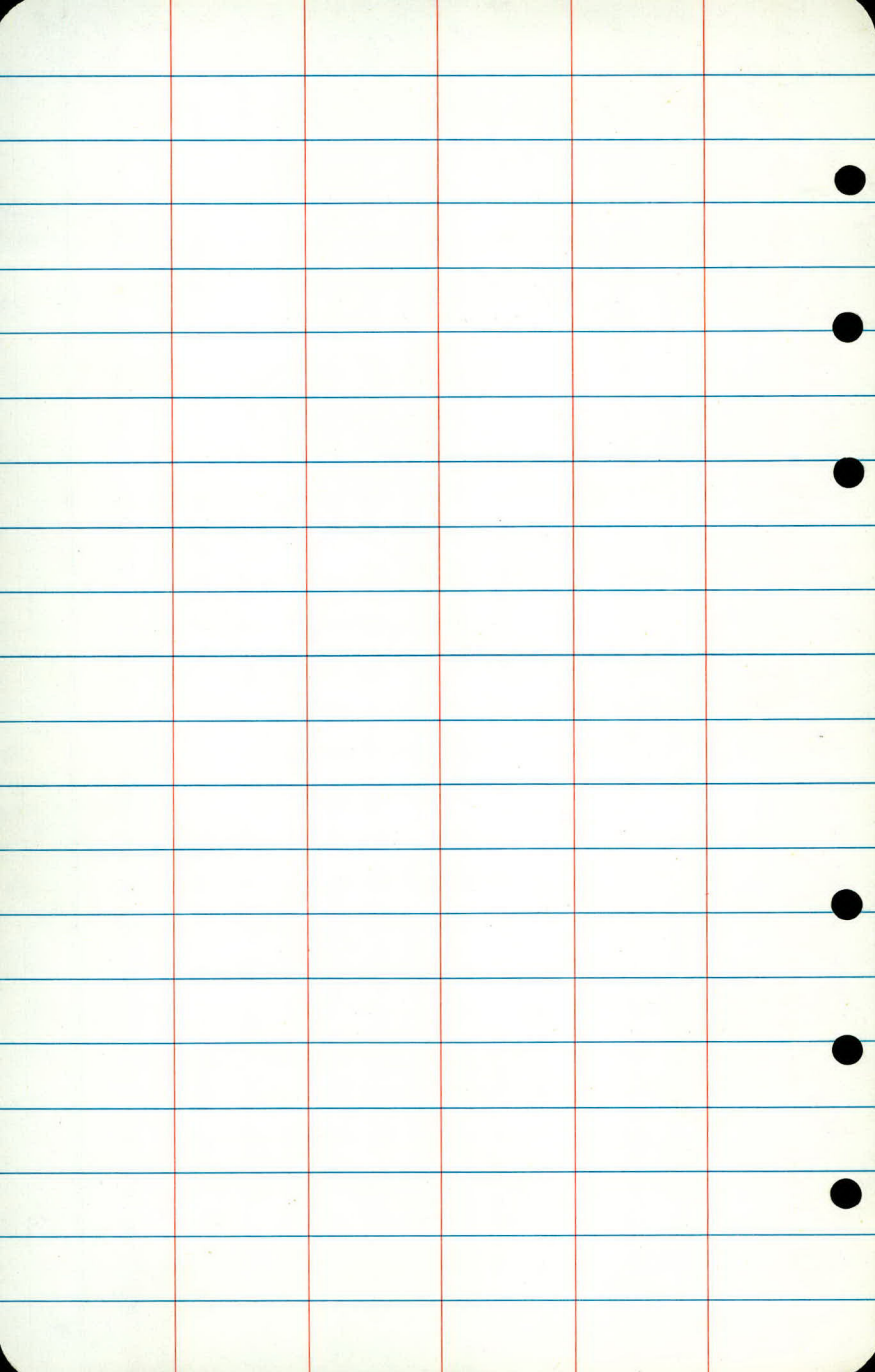
54+02 Rt 45'

54+09 Rt 44

55+35 Lt 25

55+35 Rt 25

TOP HYD SW COR "D" i MC KNIGHT



KP
GA
RJ

12 FEB 1976
P. CLOUDY 36°

33

62-668-1A

CB & MH ELEVATIONS

STA	+	π	-	ELEV
BM	4.44	973.12		968.68

6.68	976.44
------	--------

5.58	977.54
------	--------

BM	9.83	982.67	0.27	972.85	972.84
----	------	--------	------	--------	--------

12.05	970.62
-------	--------

8.92	973.75
------	--------

6.88	975.79
------	--------

3.31	979.36
------	--------

BM	0.68	981.99	982.02
----	------	--------	--------

DESCRIPTION

TOP HYDRANT LT STA 45+00

TOP MH 31.0 RT STA 45+40

TOP MH $\frac{1}{2}$ STA 46+83

TOP HYDRANT LT STA 49+40

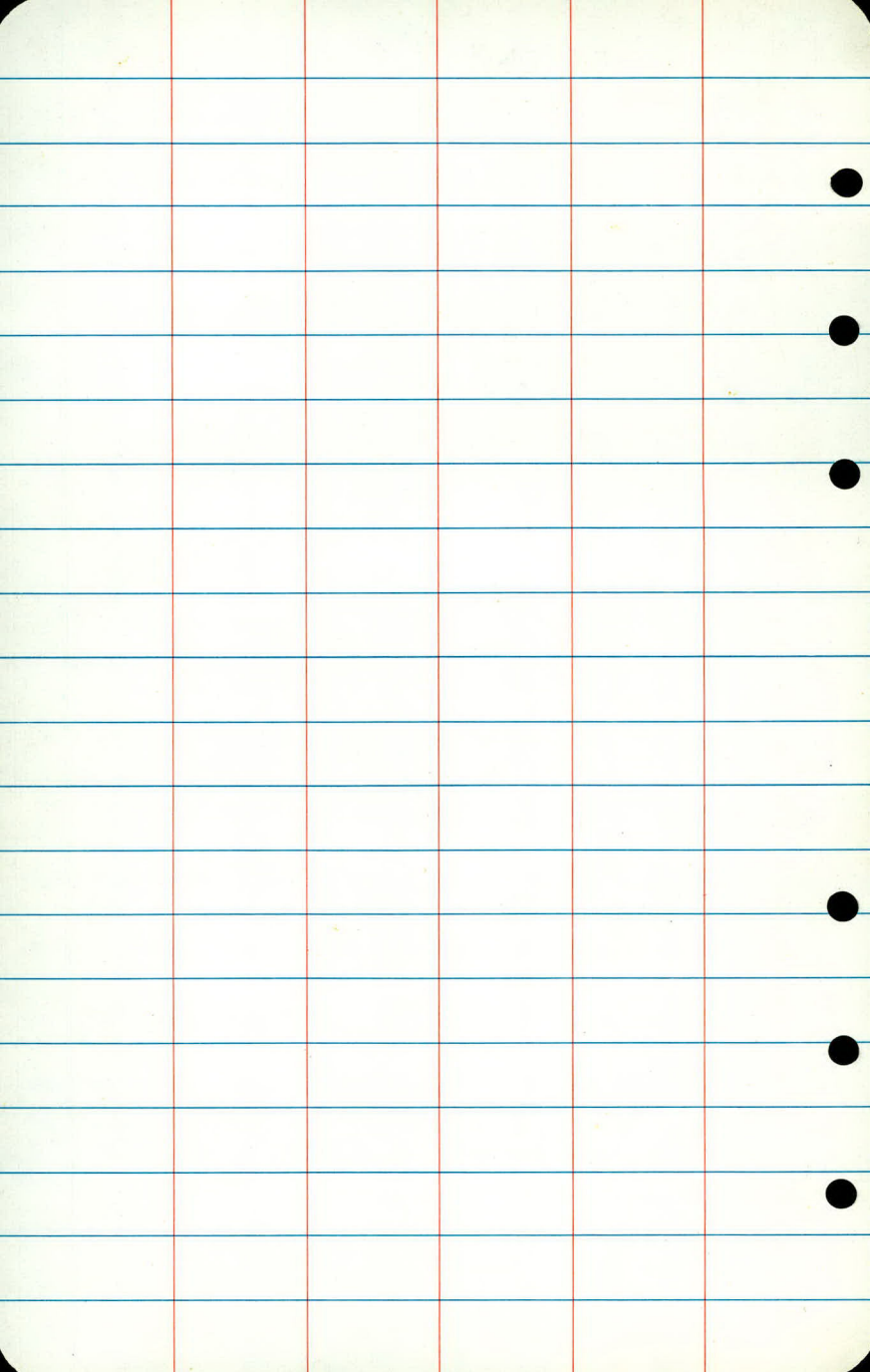
TOP MH 31' RT 48+72

TOP CB 38" RT 50+68

TOP MH 20' RT 51+69

TOP MH 20' RT 53+88

TOP HYD SW COR MCKNIGHT & CO. R.D.D.



KP
GA
RJ.

17 FEB 1975

35

LYDIA ST

McKNIGHT RD TO 200' E

ADDITIONAL
TOPOGRAPHY

+50

LT

E

RT

2+00

Curb
22 22

+50

+19 Begin B624 +19 Begin B624
22 22

+03 MH

1+00

OB SW curb SW
21 29-34 22 22 27-32

10

+95 LITC
26

+50

Curb
22 22+40 CB
23+39 MH
4+34 MH
8

0+00 = STA 39+49 MCKNIGHT RD

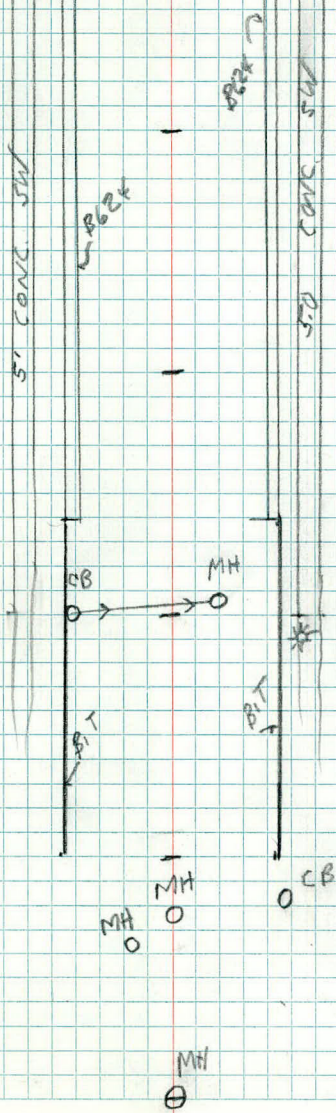
+00 MH
4

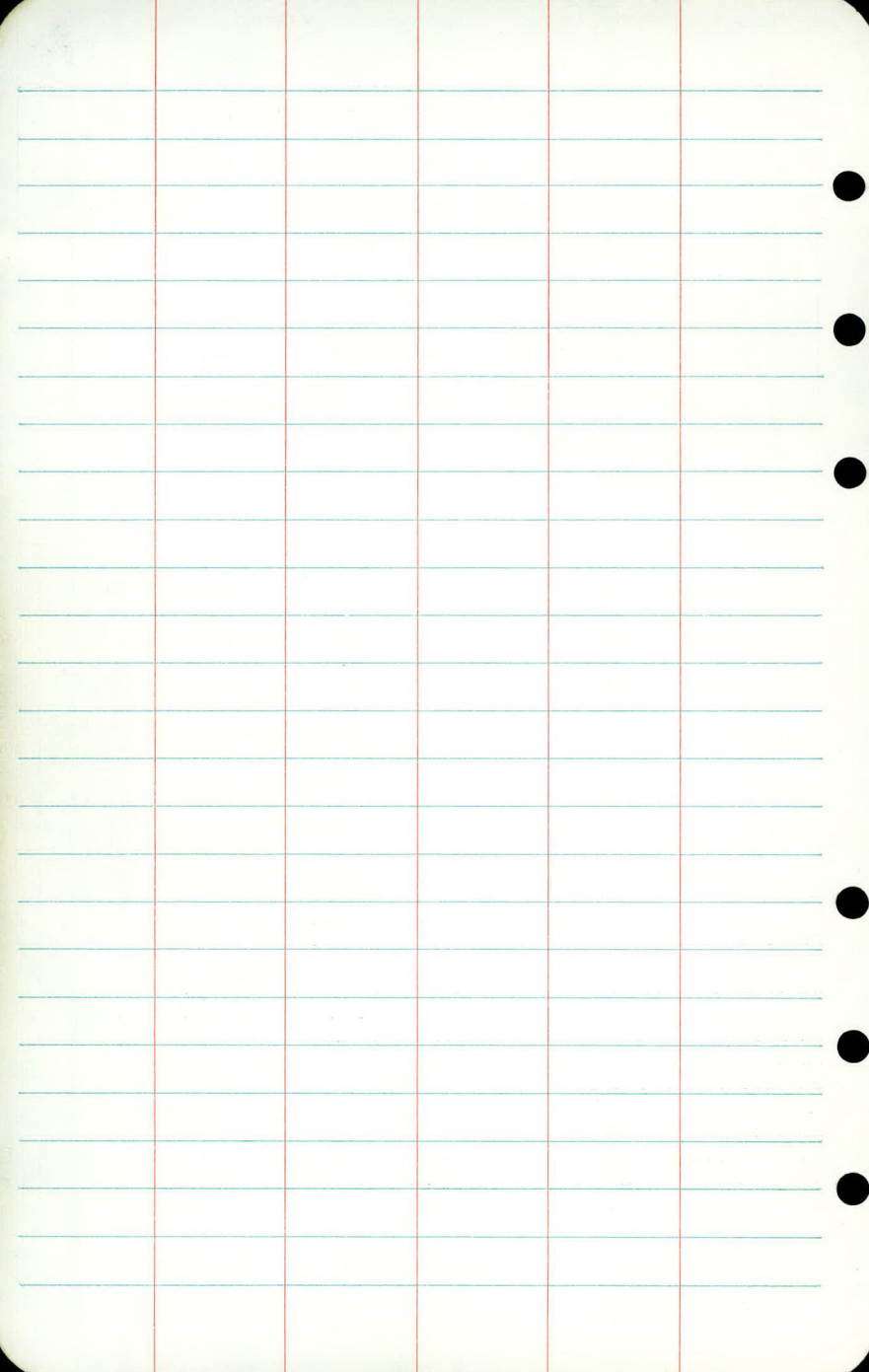
17 FEB. 1975

LT

RT

36





KP
GA
RJ

17 FEB 1976 37.
CLOUDY 40°

LYDIA ST

TOP B624 ELEVATIONS

2 PAGES

STA	+	π	-	ELEV.
BM	6.50	970.14		963.64

5.19

5.16

5.12

BM			3.85	966.29	966.28
----	--	--	------	--------	--------

LT

17 FEB 1976 38.

RT

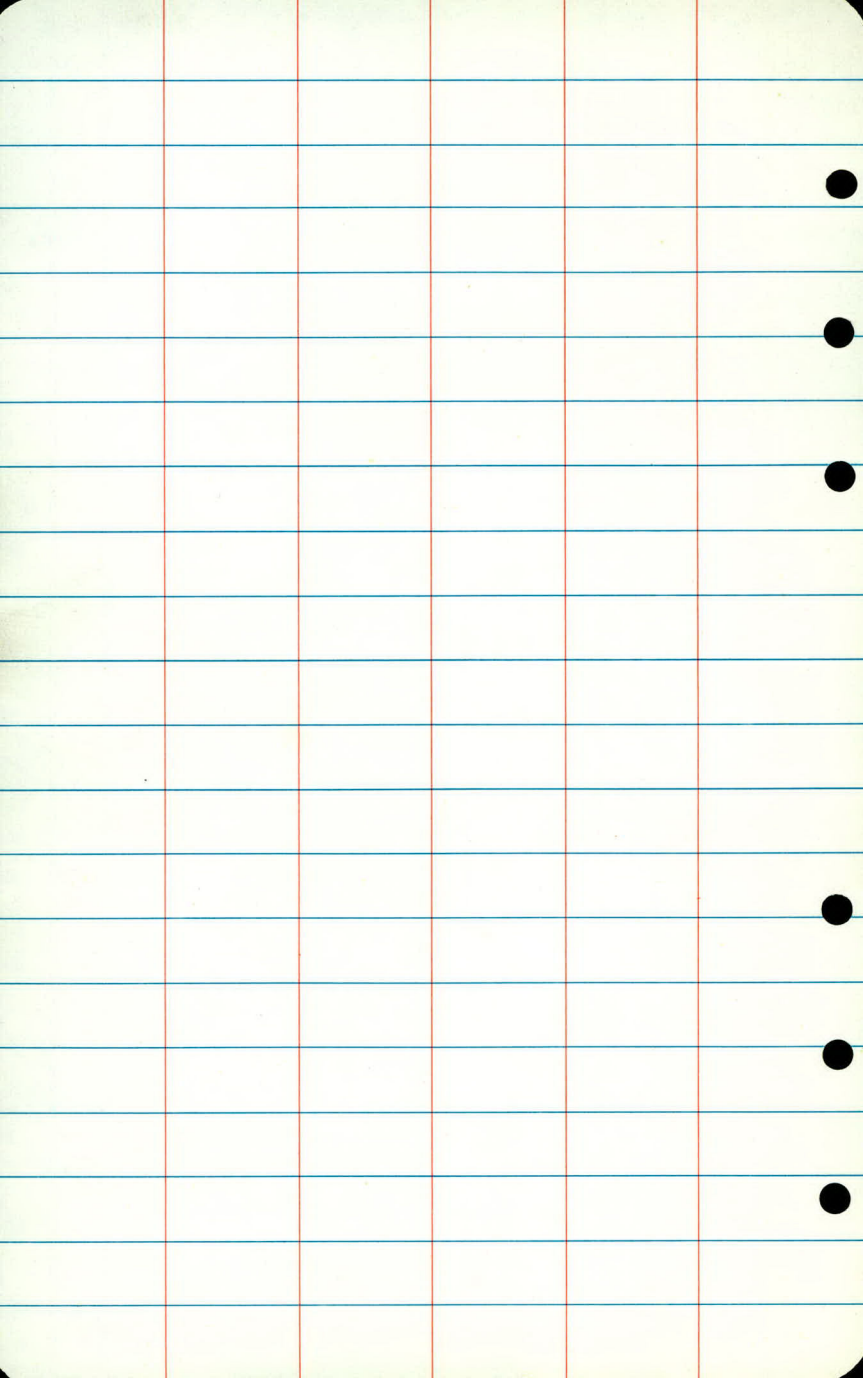
TOP MH & MCKNIGHT & LYDIA

TOP CURB 22' LT STA 1+19

TOP CURB 22' RT STA 1+19

& STA 1+19

TOP HYD. SW COR LYDIA & MCKNIGHT



KP
WS
GA
RJ

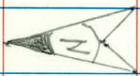
18 MAY 1976
SUNNY 60°

1.

BEAM AVE

X- SECTIONS

4+00



± McKnight Road

26+28

2+00

0+00

STA	+	π	-	ELEV.
BM	0.97	998.25		(997.28)

0 + 00 = ENT. RT

+44 = $\neq$ ENT LT

+91 = ENT LT & RT

1 + 00

+29

4.72 993.53

+50

KP
WS
GA
RJ

LT

£

18 MAY 1976
RT

2.

TOP HYD. S.E. COR McKnight & Beam

93.4	91.19	90.69	91.2	90.69	91.25	93.1	93.45
4.9	7.06	7.56	7.1	7.56	7.00	5.2	4.8
50	23	22		22	26	44	50
	TC	G		G			

94.0	93.3	92.30	91.54	92.2	91.47	91.96	94.1
4.3	5.0	5.95	6.71	6.3	6.78	6.29	4.2
50	34	26	22		22	23	50
				G		TC	

94.0	93.06	92.40	92.8	93.43	93.06	94.8
4.3	5.19	5.85	5.5	4.82	5.19	3.5
50	26	22		22	26	50
		G		G		

94.1	93.03	92.53	93.0	92.51	93.14	94.8
4.2	5.22	5.72	5.3	5.74	5.11	3.5
50	23	22		22	26	50
	TC	G		G		

TOP MH £

94.3	93.90	93.41	93.9	93.40	93.88	94.9
4.0	4.35	4.84	4.4	4.85	4.37	3.4
50	23	22		22	23	50
	TC	G		G	TC	

STA	+	T	-	ELEV.
-----	---	---	---	-------

		998.25		
--	--	--------	--	--

+84	=	GUTTER	LT & RT	
-----	---	--------	---------	--

TP	7.31	1001.51	4.05	994.20
----	------	---------	------	--------

2+00	=	McKnight Rd.		
------	---	--------------	--	--

+15	=	GUTTER	LT & RT	
-----	---	--------	---------	--

+10			7.78	993.73
-----	--	--	------	--------

+50				
-----	--	--	--	--

KP
WS
GA
RD

LT

2

18 MAY

1976
RT

3.

93.7	93.91	93.9	94.2	93.6	93.5
4.6	4.34	4.4	4.1	4.7	4.8
50	29 MH	25		25	50

TOP MH STA 2+07 RT 15.0

94.0	94.2	94.3	94.29	94.0	93.7
7.5	7.3	7.2	7.22	7.5	7.8
50	25		6 MH	25	50

93.9	94.4	94.6	94.0	93.6
7.6	7.1	6.9	7.5	7.9
50	25		25	50

TOP MH 41.0 RT

96.1	95.6	95.0	95.3	94.7	95.2	95.4
5.4	5.9	6.5	6.2	6.8	6.3	6.1
50	22 TL	21 G		15 G	17	50

STA

+

$\bar{x}$

-

ELEV.

1001.51

3+00

+50

4+00

V

BM

4.23

997.28

997.28

KP
WS
GA
RJ

LT

E

18 MAY 1976

RT

4.

97.9

96.49

95.99

96.4

95.9

96.4

96.6

3.6

5.02

5.52

5.1

5.6

5.1

4.9

50

23

22

15

16

50

TC

G

G

97.6

97.31

96.83

97.3

96.9

97.2

96.2

3.9

4.20

4.68

4.2

4.6

4.3

5.3

50

23

22

14

16

50

TC

G

G

98.51

98.45

98.28

97.79

98.3

97.8

98.2

1001.5

2.94

3.06

3.23

3.72

3.2

3.7

3.3

0.0

33

29

23

22

14

15

50

SW

SW

TC

G

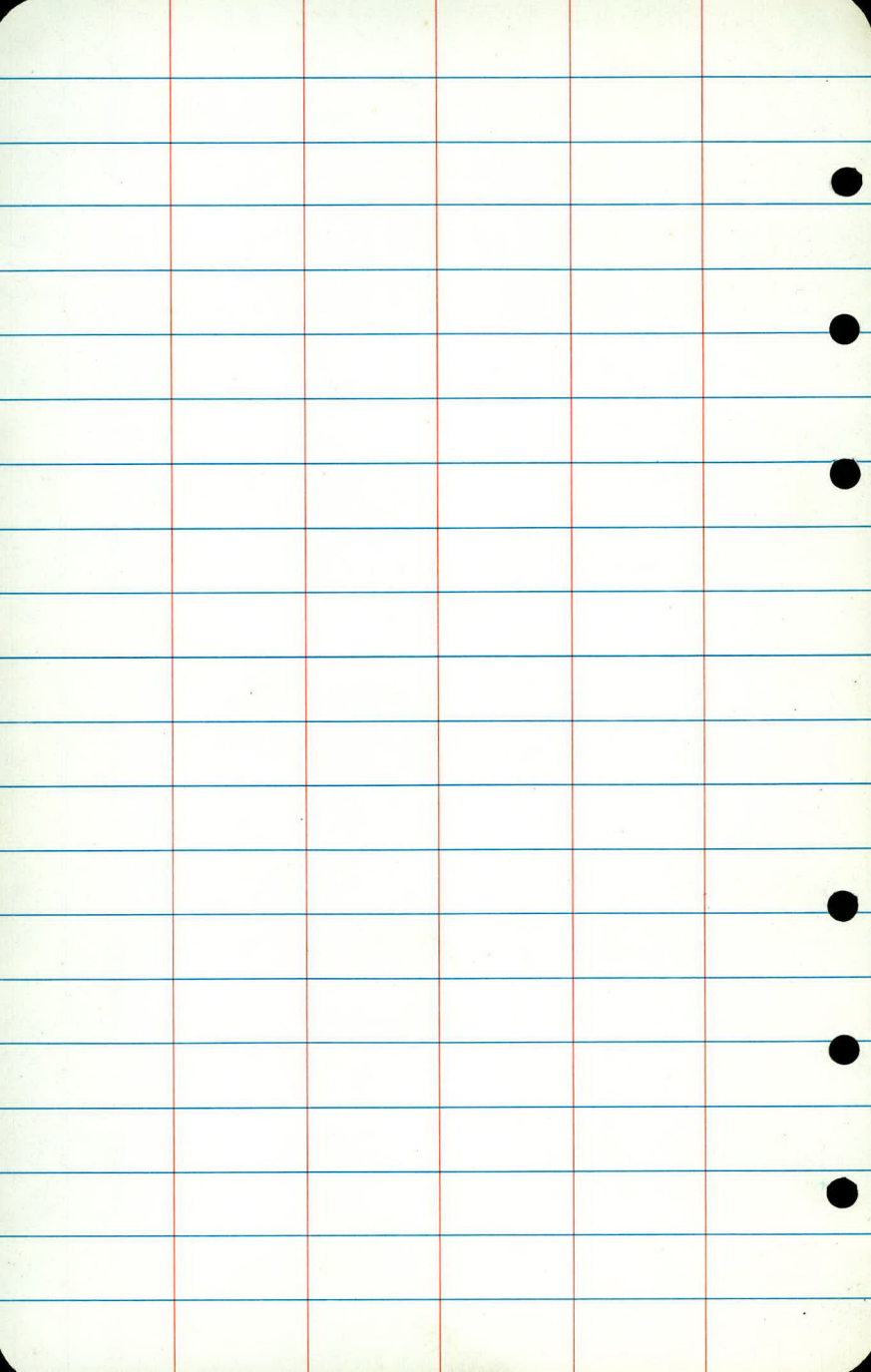
G

99.2

2.3

50

TOP HYD. SE COR McKnight & BEAM



KP
WS
GA
RJ

18 MAY 1976
SUNNY 58°

1.

McKNIGHT RD.

Co. Rd. D to I 694

ADDITIONAL TOPOGRAPHY

STA 39+75 TO 43+50

42+00 LT E R

+93 4" Pp +95 4" Pp +97 4" Pp
+69 5" 0 54 54
+57 6" 0 61 65

+76 8" BE
33

+50

+11 STP

+03 3" ELM +06 3" ELM

41+00 +88 STP +93 STP

+86 STP +87 STP +85 11" OAK

+83 5" OAK +86 12" OAK

+59 TW 14" OAK +78 4" OAK

+46 6" OAK +55 4" OAK

+50 +41 TW 6" OAK

+30 14" OAK +40 TW 18" OAK

+17 6" OAK +25 TW 6" OAK

+09 12" OAK

+07 TW 5" OAK +04 6" OAK

40+00

+91 12" OAK
41

39+50

KP
WS
GA
RJ

LT

~~E~~

18 MAY 1976 2

RT

+50

LT

£

RT

44+00

+43 2" P

+49 12" 0³² +45 Bush+44 4" 0⁴² +47 3" 0³⁶+35 3" P⁴⁴ +41 4" 0⁴⁹ +43 4" 0+50 4" 0⁴⁵ +32 4" POP⁴⁸ +33 4" POP⁴⁹+24 12" 0 +24 5" 0³¹ +26 8" 0³¹+09 6" 0⁴⁷ +15 5" EM⁴⁵ +19 8" OAK⁵⁴+05 9" OAK⁴⁷ +09 4" OAK³⁴ +09 6" OAK⁵³+03 8" OAK⁵⁰ +97 8" OAK⁴³ 4643+00⁵⁷ +87 6" OAK⁴⁸+76 15" OAK +84 TW 6" OAK³⁷42 +63 5" OAK⁵²+62 5" OAK⁴⁷

39

+50

+28 14" 0 +27 13" 0 +26 8" 0

+23 5" 0⁵⁷ +22 6" 0⁵⁰ +20 13" 0⁴⁹+15 4" POP⁵⁷ 56 +19 13" 0⁵⁴

+45 8" OAK

71 +09 5" 0⁵¹

40

62

+08 8" 0

50

42+00

KP
WS
GA
RJ

LT

£

18 MAY 1976

3

RT

