

OFFICE OF COUNTY ENGINEER
RAMSEY COUNTY, MINN.

PLAN Survey

STILLWATER STREET

From Curves at To Dillon St.

Road Acc't. No. _____

Date Filed _____

File _____

Feb 27, 1970

1

STILLWATER ST

77' B & L of #
1' below Profile

Sta Point ΔL ΔR

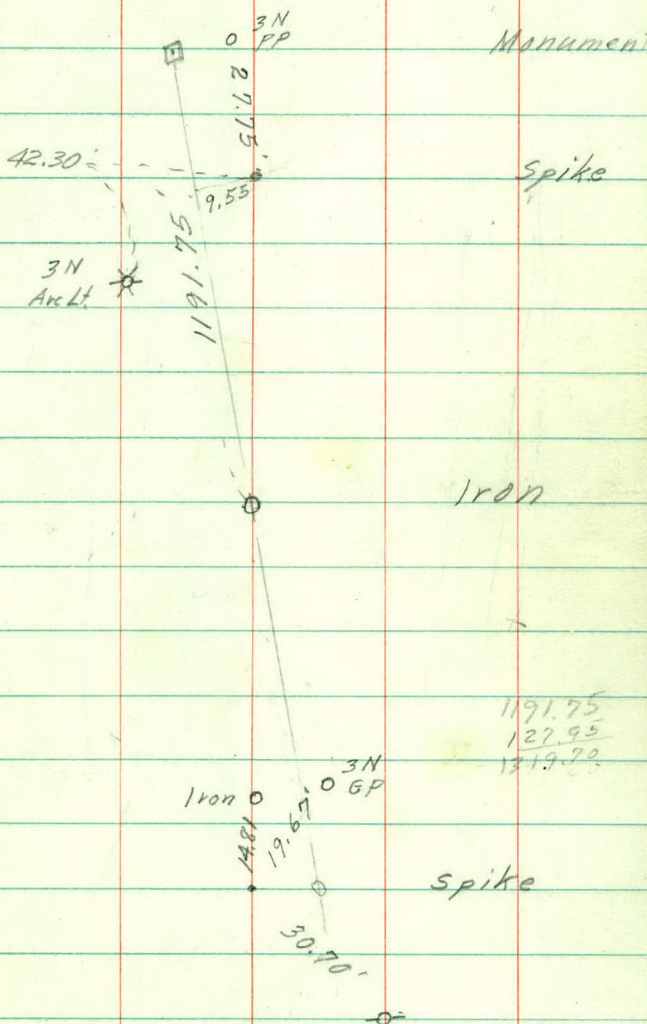
28+14.00 P.I.

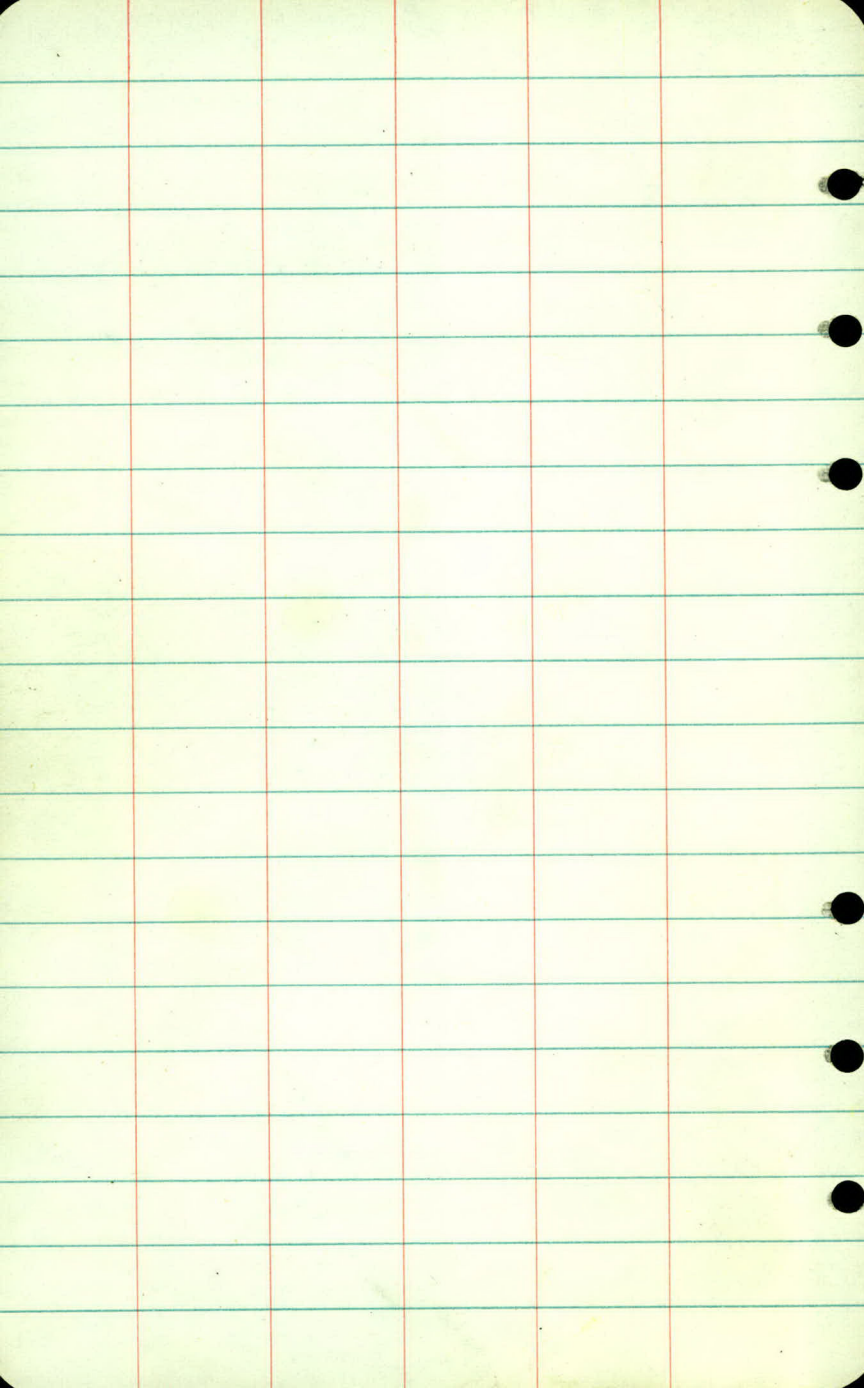
27+30.80 P.O.T. Section Line

26+28.30 P.I.

Feb 27, 1970

2





Feb 22, 1970

3

1243.75
1191.75
52

76.03
1243.75
1319.78

1244.12
- 37
1243.75

2639.92
78
2639.14
1319.57

18' 

E $\frac{1}{4}$ Corner

Sec 10-30-22

S. Edge Porch Pillar West



PK

18'

90°

1439.92 NTC

1200 NTC

1243.75' M

PK

2639.14-M

1191.75 R

1319.45 R do Iron

1319.98 M

18' 

S.E. Corner

Sec. 10-30-22

Road Map Survey P.T. 

PK Nail

10.104

Found Iron

Spike 

10.95

S.W. Corner Lot D

THE EYRIE

35'

36.72



$\frac{1}{4}$ $\frac{1}{4}$ Corner

FX
LPD
ML
GA

March 23, 1970

3A

New Alinement

Sta Point ΔL ΔR

+52.79 P.T. $20^{\circ}16'20''$

+50 $19^{\circ}41'$

+25 $14^{\circ}23'30''$

P.I. OK

26+07.01 P.I. $40^{\circ}32'40''$

26 $9^{\circ}06'$

+75 $3^{\circ}48'30''$

25+57.01 P.C.

$\Delta = 40^{\circ}32'40''$

$\frac{1}{2}\Delta = 20^{\circ}16'20''$

$D = 42^{\circ}20' \pm$

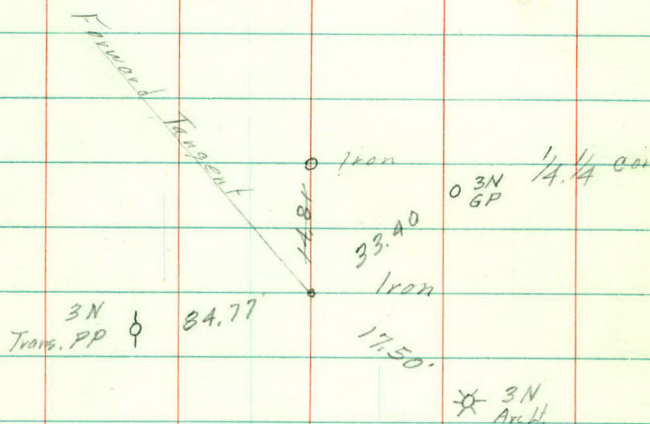
$T = 50'$

$L = 95.78'$

$R = 135.35'$

March 23, 1970

36



old P.C. = New P.C.

Sta Point ΔL ΔR

$$\Delta = 40^{\circ} 47' 40''$$

$$\frac{1}{2}\Delta = 20^{\circ} 23' 50''$$

+71.19 P.T.

$$20^{\circ} 23' 50'' \quad D = 42^{\circ} 36' 12''$$

+50

$$15^{\circ} 54' 12'' \quad T = 50'$$

29+25.45 P.I.

$$40^{\circ} 47' 40'' \quad L = 95.74$$

+25

$$10^{\circ} 35' \quad R = 134.46'$$

29

$$5^{\circ} 15' 12''$$

28+75.45 PC

$$0^{\circ} 00'$$

$$\frac{95.74}{91.19}$$

$$91.19$$

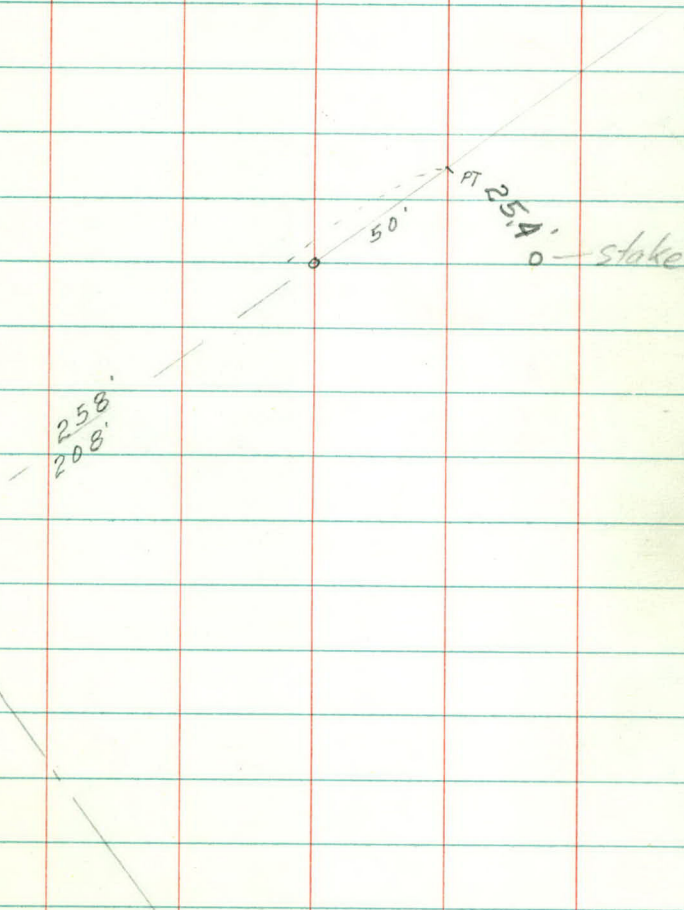
$$D = 21^{\circ}$$

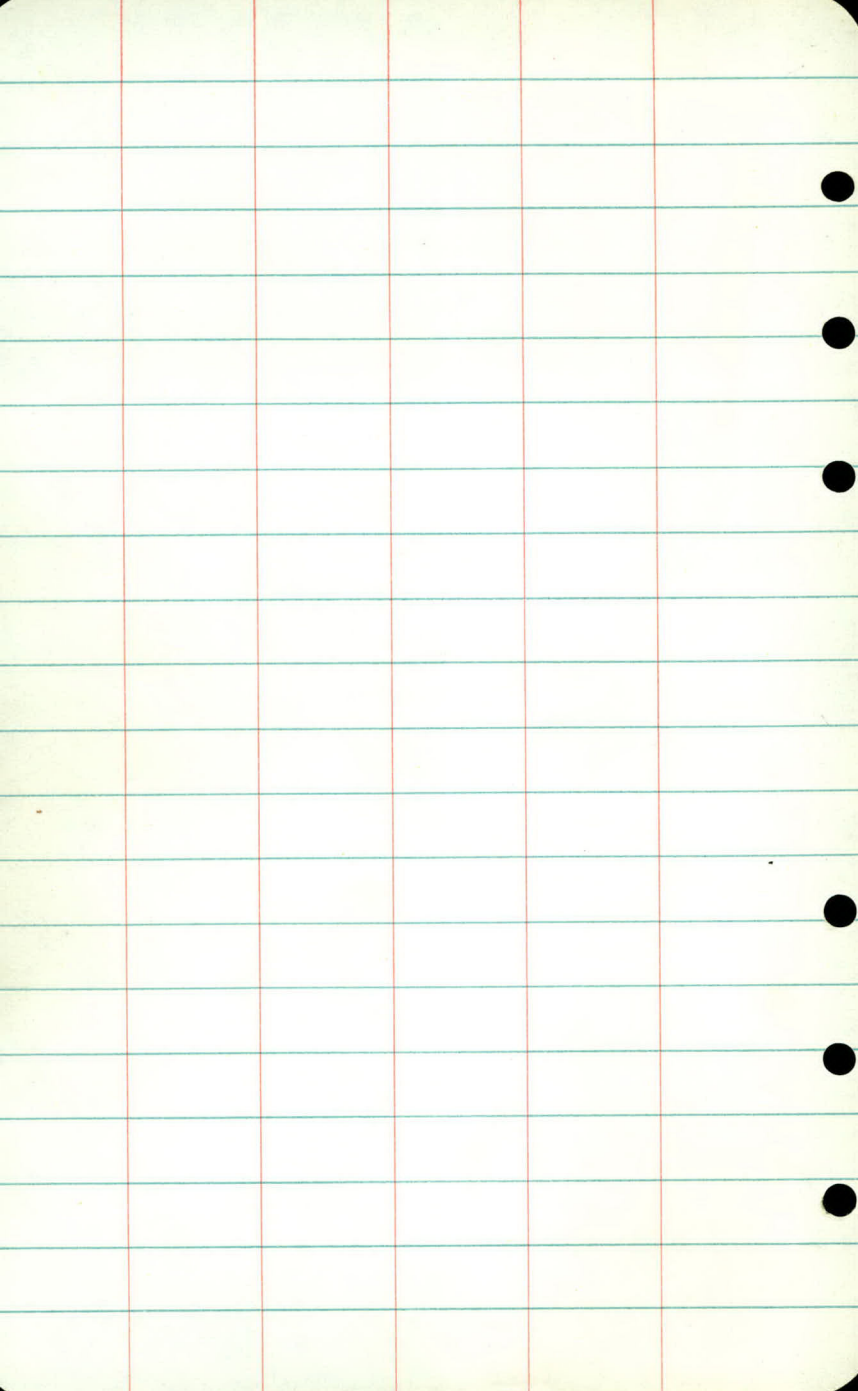
for 30 MPH

$$T = 125'$$

March 23, 1970

30





FK
RG

£

April 23, 1970

3d

30.36
13.2

26.57 150'

33.70

26.03

25.99

2987

34.12

Iron
SE Cor Lot 34.14

P. 128 + 14.00 → 175.57'

34.1

old
Iron
1/4

Sta Point ΔL ΔR

FINAL

+103.93	PT	$20^{\circ}16'20''$	
27		$19^{\circ}52'45''$	
+75		$17^{\circ}22'45''$	$\frac{1}{2}\Delta = 20^{\circ}16'20''$
+50		$14^{\circ}52'45''$	$\Delta = 40^{\circ}32'40''$
+25		$12^{\circ}22'45''$	$D = 20^{\circ}$
26+07.01	P.I.	$40^{\circ}52'$	$T = 105.80'$
26		$9^{\circ}52'45''$	$L = 202.72$
+75		$7^{\circ}22'45''$	$R = 286.48$
+50		$4^{\circ}52'45''$	
+25		$2^{\circ}22'45''$	
25+01.21	P.C.	$0^{\circ}00'$	

FK
CM
DR
BP

June 12, 1970

3e

3N
GP

33.40

Bolt

3N
Transf.
P.P.



84.77

17.50

3N
Arc Lt.

Sta Point Δ Lt. Δ Rt.

FINAL

+2299	PT	$20^{\circ} 26'$
30		$18^{\circ} 08' \frac{1}{2} \Delta = 20^{\circ} 26'$
+75		$15^{\circ} 38' \Delta = 40^{\circ} 52'$
+50		$13^{\circ} 08' D = 20^{\circ}$
29+25.40	P.I	' $T = 106.74$
+25		$10^{\circ} 38' L = 204.33'$
29		$8^{\circ} 08' R = 286.48$
+75		$5^{\circ} 38'$
+50		$3^{\circ} 08'$
+25		$0^{\circ} 38'$
28+18.66	PC	$0^{\circ} 00'$

June 12, 1970

3f

Lot Platted
Stillwater St.

30' 30'

o Iron

54.26

Iron Pin

63.95

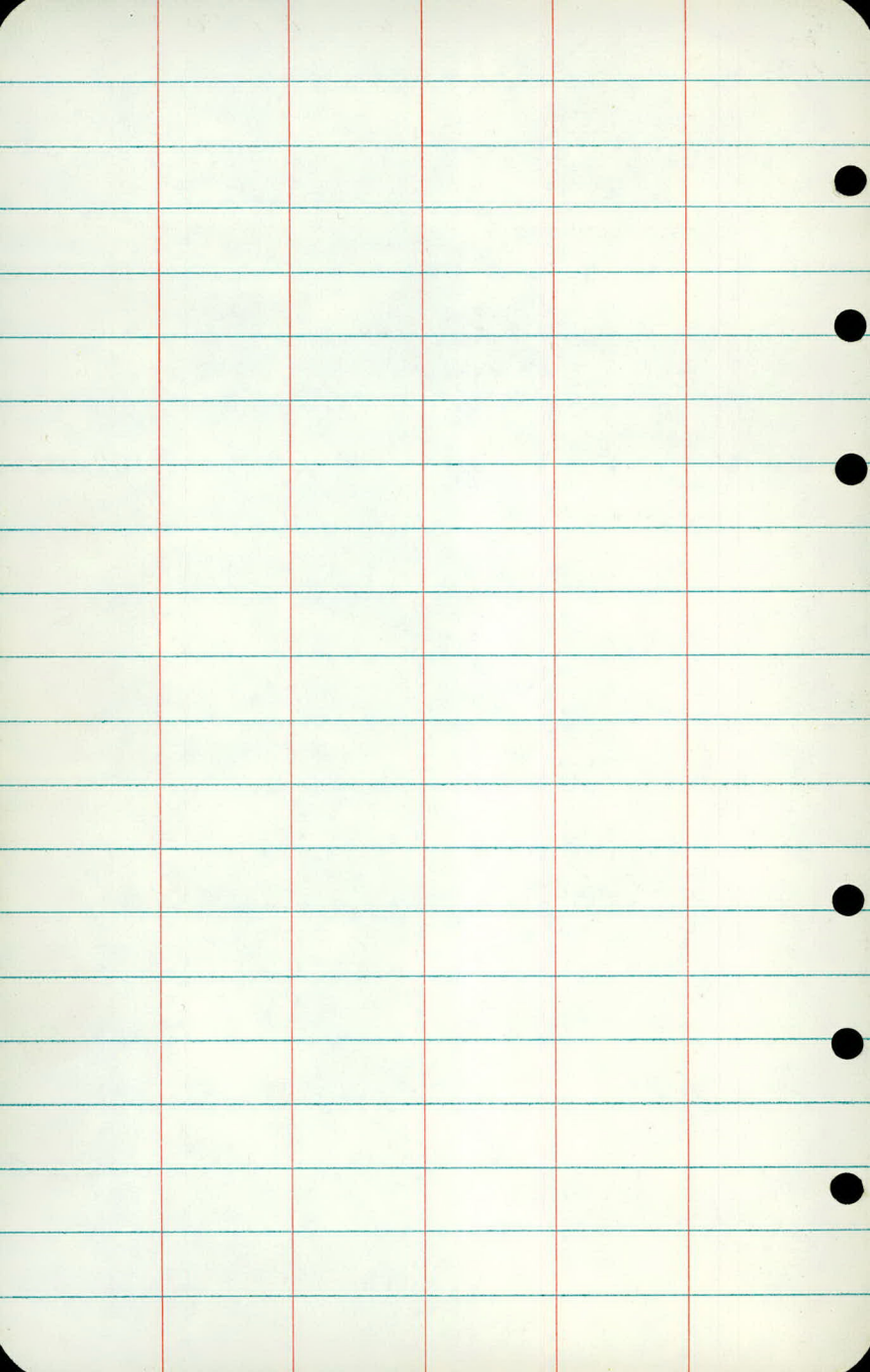
65.86

73.23

New P.I.

P.K.
S.T.
PP

o



FK
DS
CM

March 2, 1970

4

Topography

ROAD LOCATION

$$+42 \overline{26} \ 8$$

$$+27 \overline{28} \ 8 \checkmark$$

$$26 \quad +12 \overline{29} \ 7$$

$$97 \overline{30} \ 6 \checkmark$$

$$+87 \overline{29} \ 13$$

$$+72 \overline{26} \ 8$$

137 PC

$$+57 \overline{23} \ 9 \text{ Road}$$

$$+35 \overline{18} \ 12 \text{ Road}$$

25

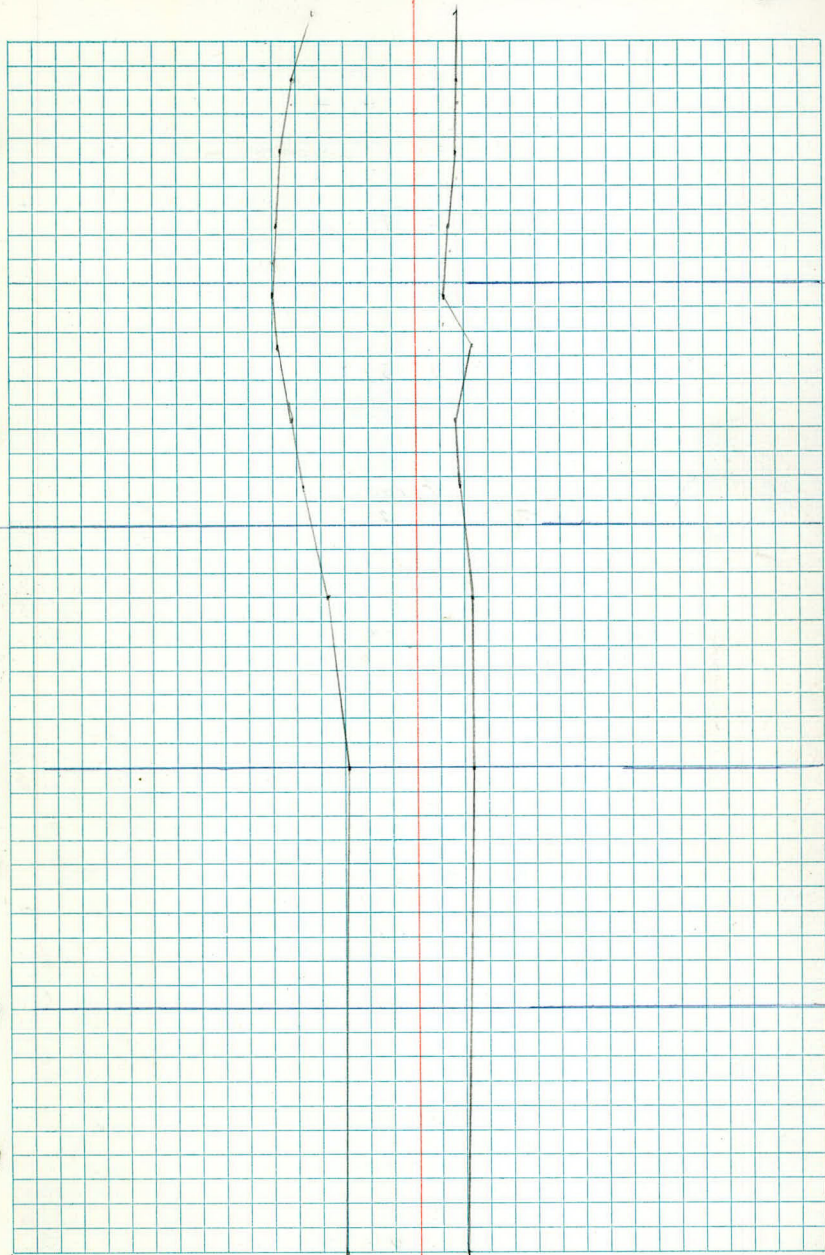
$$\overline{14} \ 12 \text{ Road}$$

24

$$\overline{15} \ 10 \text{ Road}$$

March 2, 1970

5



29

6 19.

+59 PT

+59 3 31.

+29 7 39.

28

+08 Road
5 40.+75 Road
11 38.

+42 PC

+42 10 31.+31 Road
11 27.

27

Road
13 16.

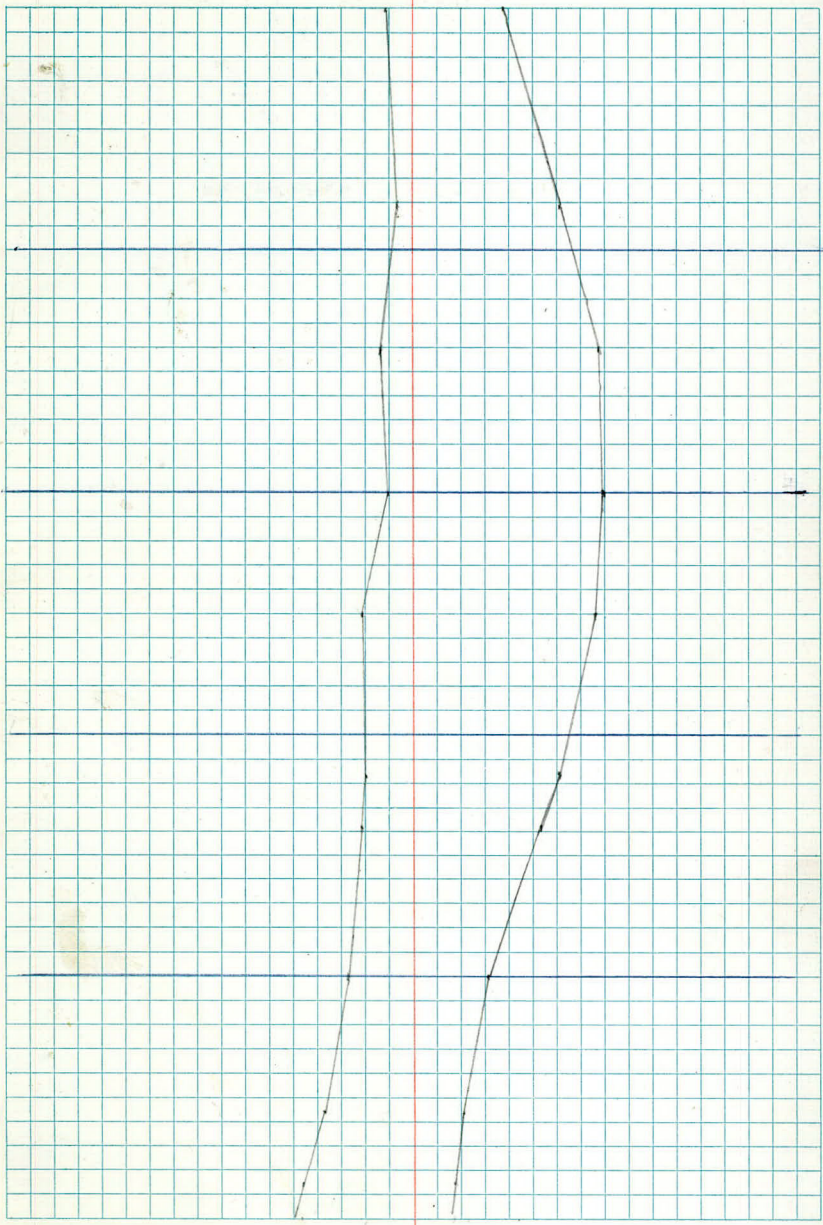
+53 PT

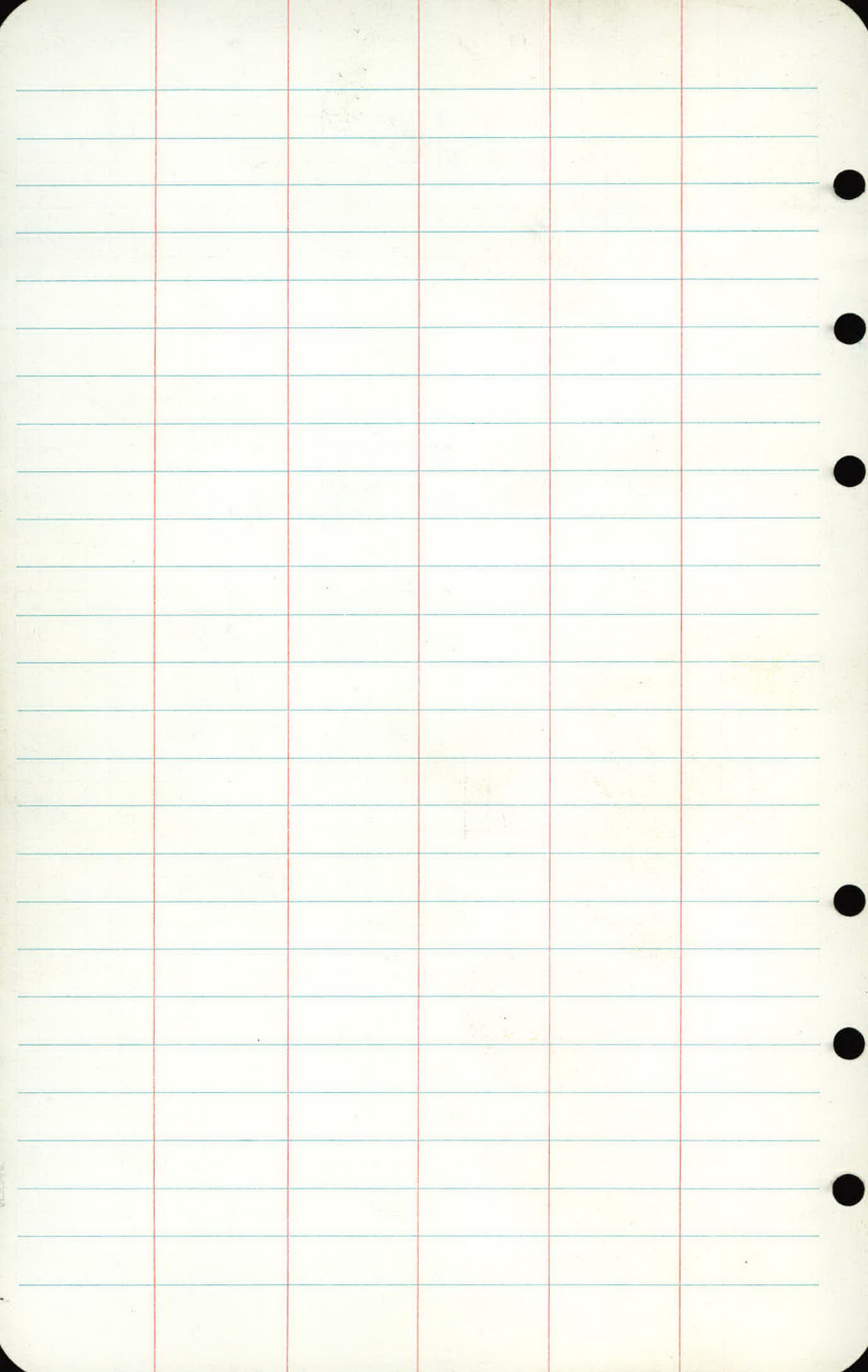
+73 Road
18 11.

+57 23 8.

March 2, 1970

6





March 24, 1970

7

x-sections

No close Bench!

Elevations from old
Profile

Sta + π - Elev.

945.08 average used

23 45.11 3.20 41.91
45.07

24 3.46 41.61
45.56

25 3.85 41.3

+37 PC 5.3' Lt

✓

26 9.4' Lt

+50 4.5' Lt

Lt.

March 24, 1920

Rt

8

39.7	40.0	39.9	40.7	41.3	40.0	42.8	41.7	41.9
5.4	5.1	5.2	4.4	3.8	4.1	2.3	1.4	1.2
50	37	25	14		13	23	36	50

40.6	39.9	39.8	40.3	40.5	40.7	40.7	40.4	40.0	42.1
4.5	5.2	5.3	4.8	4.4	4.4	4.7	4.3	3.0	
33	28	23	10	8	5	8	10	14	21
28	23	14	5	0		13	15	19	26

39.7	41.2				44.0	43.7	43.7
5.4	5.9				1.1	1.4	1.4
44	50				50	41	30
39	45				55	46	35

39.8	38.9	38.8	39.4	40.1	40.3	40.1	40.3	40.6
73	62	63	57	50	48	50	48	45
50	44	34	25	9	9	15	21	52
41	35	25	16	4	9	24	40	59

39.1	38.2	39.2	39.9	39.8	39.6	39.5	39.0	39.8	39.7	38.8	38.6	5	6
8.0	6.9	5.9	5.2	5.3	5.6	6.1	7.3	7.4	6.6	6.6			
50	45	32	15	7	7	6	11	26	43	50			
45	40	27	10	2	5	11	16	31	48	55			

Sta + X - E/ev.

945.08

27

✓

+50

✓

28

✓

March 24, 1970

9

Lt.

Rt.

38.1	38.1	36.3	36.3	36.4	37.0	37.3	38.9	38.9
6.2	6.4	8.8	8.8	8.7	8.1	7.8	6.2	6.2
40	33	21	12		16	31	42	50

37.0	38.9	38.4	35.0
6.1	6.2	6.7	10.1
46	60	72	88

37.3	35.3	32.9	23.3	34.6	35.3	36.3	36.4
7.8	11.8	12.2	11.8	10.5	9.8	8.8	8.7
53	43	30	14		19	39	50

37.2	37.8	38.2	38.7	38.5
7.9	7.3	6.9	6.4	6.6
60	75	89	104	120

36.7	34.4	33.7	33.1	33.2	34.0	34.6	35.0
8.4	10.7	11.4	12.0	11.9	11.1	10.5	10.1
55	45	28	12		14	31	50

36.9	37.3	37.7	38.2	38.4	38.6
8.2	7.8	7.4	6.9	6.7	6.5
60	69	82	92	106	118

Sta + π - Elev.

945.08

28+50

Rt 2'

✓

28+75.45 P.C. 5' Rt

✓

29

Rt 10'

✓

March 24 1970

10

37.2	37.9	33.6	33.2	32.8	33.2	32.9	33.8	34.2
79	10.2	11.5	11.9	12.3	11.9	12.1	11.3	10.9
41	27	14	9	2	15	30	40	50
43	29	16	11		13	28	38	48

37.7	37.9	38.1	37.9	37.6	37.7
74	72	70	72	75	74
53	60	72	77	79	98
55	62	74	79	81	100

37.9	37.3	37.3	37.5	33.8	33.6	33.1	33.4	33.9
72	78	78	10.6	11.3	12.0	11.7	11.2	
44	30	25	12	5	16	32	50	
49	35	30	17		11	28	45	

37.9	37.7	37.2	37.3
72	74	79	78
55	60	74	86
60	65	79	91

37.6	37.4	37.9	37.1	35.3	34.3	34.2	33.7	34.7
75	73	72	8.0	8.8	10.8	10.9	11.4	10.9
33	28	16	6	10	10	26	38	50
42	33	26	16		0	16	28	40

36.7	36.6
8.4	8.5
40	50
50	60

Sta	+	x	-	Elev.
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		945.08		
--	--	--------	--	--

29+50				
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		9' RT		
--	--	-------	--	--

29+71.19 = 30+36.21 Equation

30+50				
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		1' RT		
--	--	-------	--	--

✓

30				
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		7.27		
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31				
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		7.56		
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32				
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		7.25		
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March 24, 1970

11

38.6	37.5	37.1	37.6	37.8	37.5	37.2	37.0	35.5	35.3	35.3
6.5	7.6	8.0	7.5	7.3	7.9	8.1	9.6	9.8	9.8	9.8
50	40	23	9	9	11	15	26	38	50	50
59	49	32	18		2	6	17	27	41	

36.0	36.2	37.2	37.3	37.7	37.1	36.9	36.2	35.4
9.1	8.9	7.9	7.8	7.4	7.7	8.2	8.9	9.7
32	18	11	8	1	8	14	19	24
33	19	12	9		7	13	18	23

36.7	36.6
8.4	8.5
41	50
42	51

34.5	34.7
10.6	10.4
50	39
49	38

44.95
 99.20
 45.11
 45.07

 33

Staking

+1.38

BM	2.95	944.56		941.61	Sta 24
----	------	--------	--	--------	--------

BM			4.24	940.32	
----	--	--	------	--------	--

27+0393	39.97	4.59	5.97		
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+50	39.67	4.89 1.38	6.27		
-----	-------	--------------	------	--	--

28	39.35	5.21	6.59		
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BM	3.32	940.53	7.35	937.21	
2a	38.45				

28+50	38.30	2.23	3.51		
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29	38.15	2.38	3.76		
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+50	38.00	2.53	3.91		
-----	-------	------	------	--	--

30	37.85	2.68 1.38	4.06		
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+24	37.95		4.16		
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+50	37.7	2.83		2.93	✓
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Roofing Nail in G.P.

Tie Nail
Spike in P.P.

1.38

Sta	PG	PCR	SGGR	Elev.
BM	4.25	944.57		940.32

25	41.37	^{1.38} 3.20	4.58
----	-------	-------------------------	------

+50	40.78	3.8- ^{1.38}	5.18
-----	-------	-------------------------	------

26	40.18	4.4-	5.78
----	-------	------	------

+50	39.58	5-	6.38
-----	-------	----	------

27	38.98	5.6-	6.98
----	-------	------	------

✓ +50	38.60	6-	7.38
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28	38.45	6.12 ^{1.38}	7.50
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+50	38.30	6.27 ^{1.38} 7.65
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29	38.15
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$$\begin{array}{r} 18 \\ 33 \\ \hline 4.12 = 13 \end{array}$$

Roofing Nail in Guy Pole

✓ 17.5 ✓
35.0

✓ ✓

✓ ✓

✓ ✓

Sta	PG	PGR	+0.43 @ 13' = Top C/5 - Elev.	
BM	4.88	945.20		940.32
25	41.37	3.83	4.26	
+50	40.78	4.42	4.85	5.80
		$\frac{1.38}{5.80}$		
26	40.18	5.02	5.45	
+50	39.58	5.62	6.05	
27	38.98	6.22	6.65	
+50	38.60	6.60	7.03	
TP	3.80	(941.97)		938.17
28	38.40	3.52	3.95	
✓			4.78	937.19
				(937.20) 937.21
+50	38.30	3.67	4.10	
29	38.15	3.82	4.25	

✓

✓

✓

✓

✓

✓

✓

✓

✓

✓

✓

✓

✓

✓

✓

✓

✓

Sta

PG

PGR

GR

941.97

29+50

38.00

3.97

4.40

43

30

37.85

4.12

4.55

7

+24

37.75

4.22

4.65

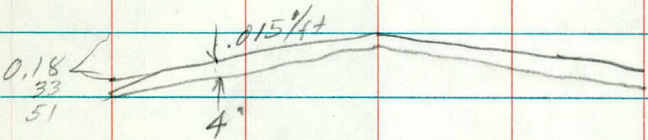
7"

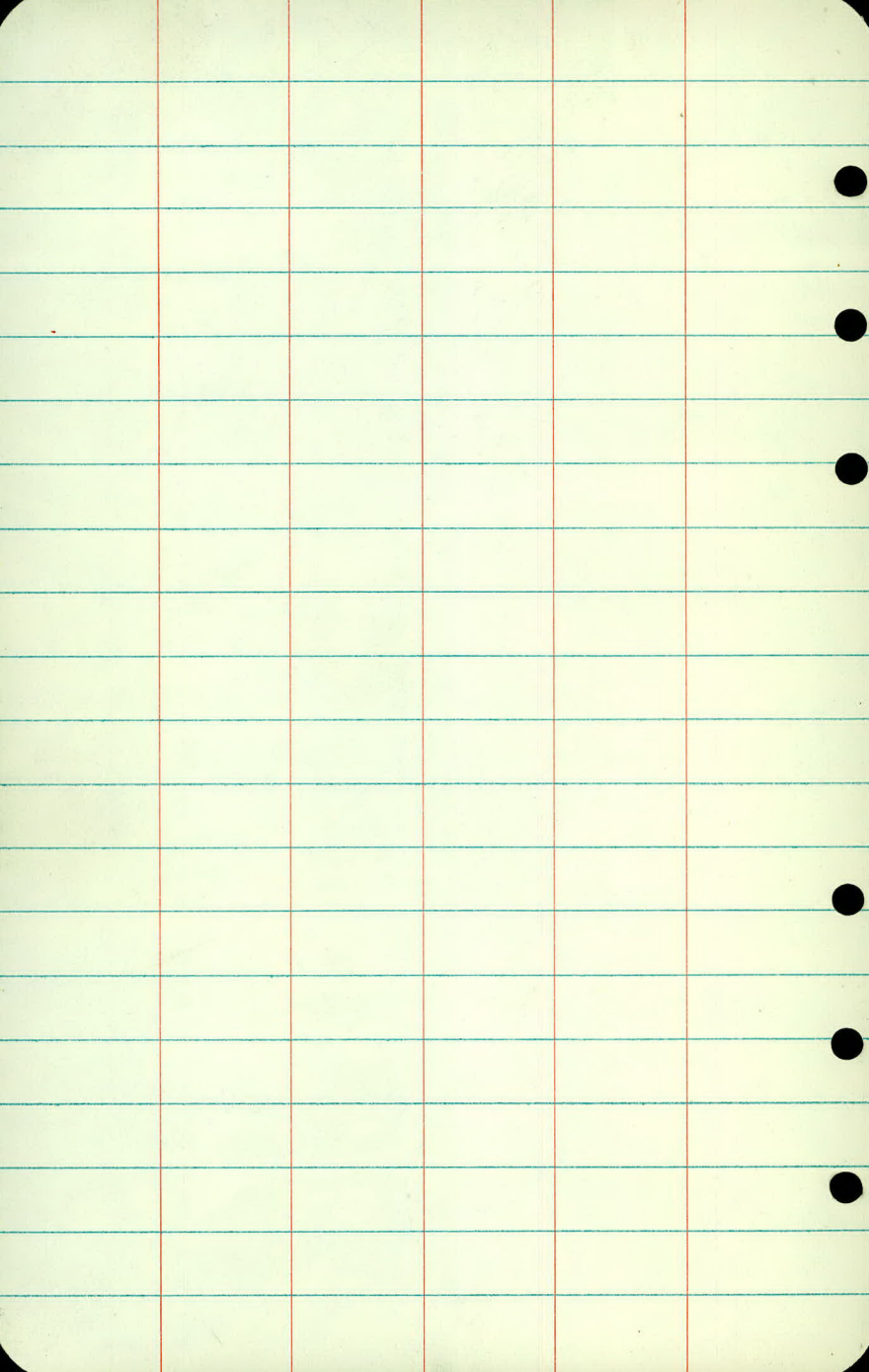
.58

June 8, 1970



02
10





April 6, 1970

1

NEW LINE TOPOGRAPHY

4 Pages

+50 Road
47-12
+48 PP
55

+34 Road
2

+18 GP
49

+28 Btie
Ent

26

Road
26 10

+103 Ent
42

+
+96 PP
33

+57 6" P
45

Road
+57 17 14

25

Road
14 12

+98 5" Pine
38

+89 Ent + Lt
Dirt

+84 Ent
Dirt

+70 PP
18

+60 Cor Trees
20'

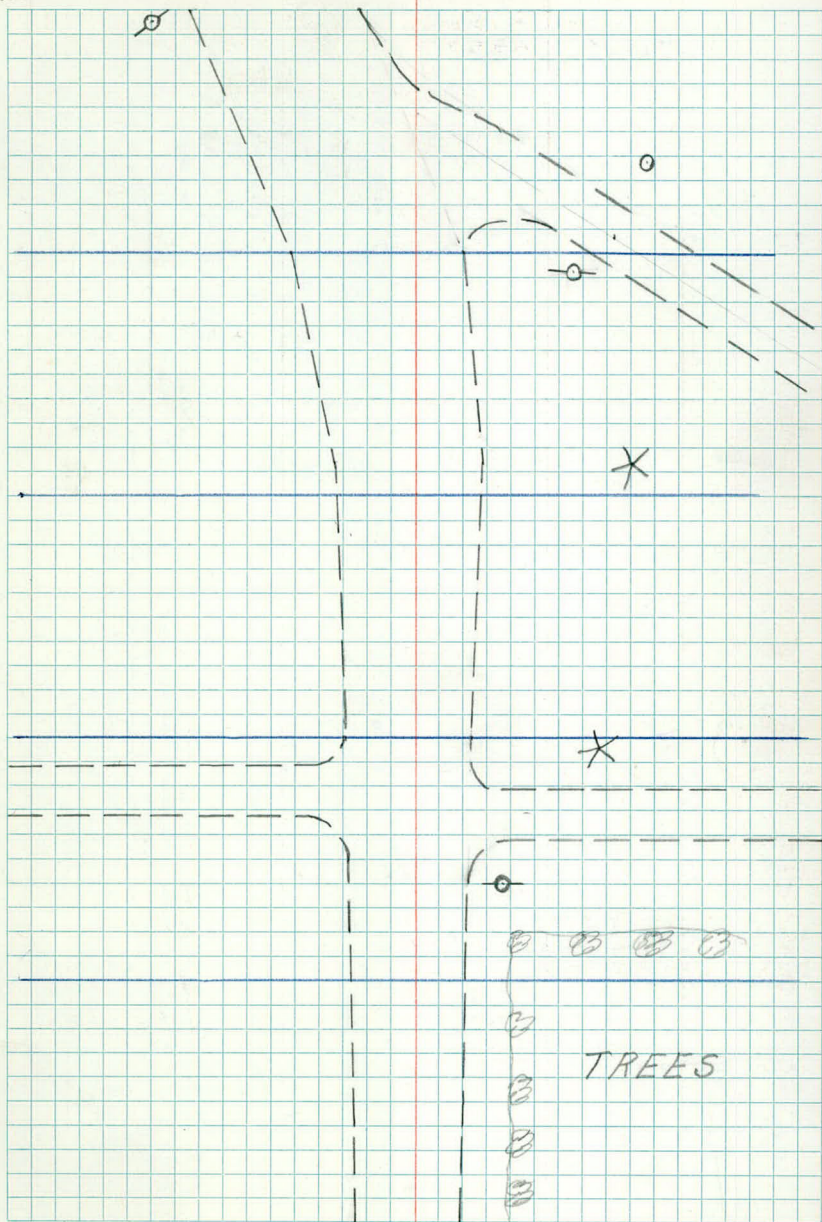
24

Road
12 9

FK
GA
CM

April 6, 1970

2



29

Road
36-12

+90 $\frac{\text{Ent}}{\text{Dirt}}$

+150 $\frac{\text{Ent}}{\text{Dirt}}$

+50 $\frac{\text{PP}}{27}$

Road
60-36

28

Road
60

+88 $\frac{4' \text{EE}}{52}$

+83 $\frac{\text{Trip } 8' \text{EE}}{44}$

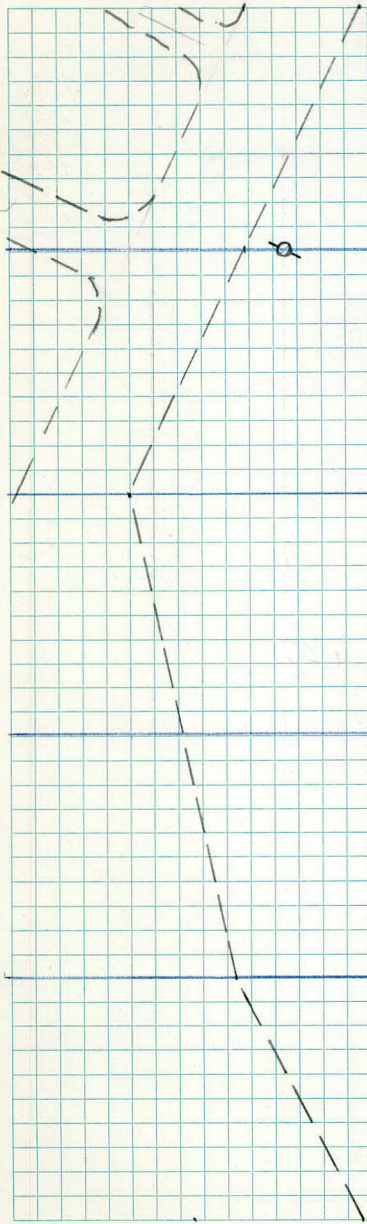
+70 $\frac{6' \text{ Cherry}}{7}$

27

Road
38

April 6, 1970

3



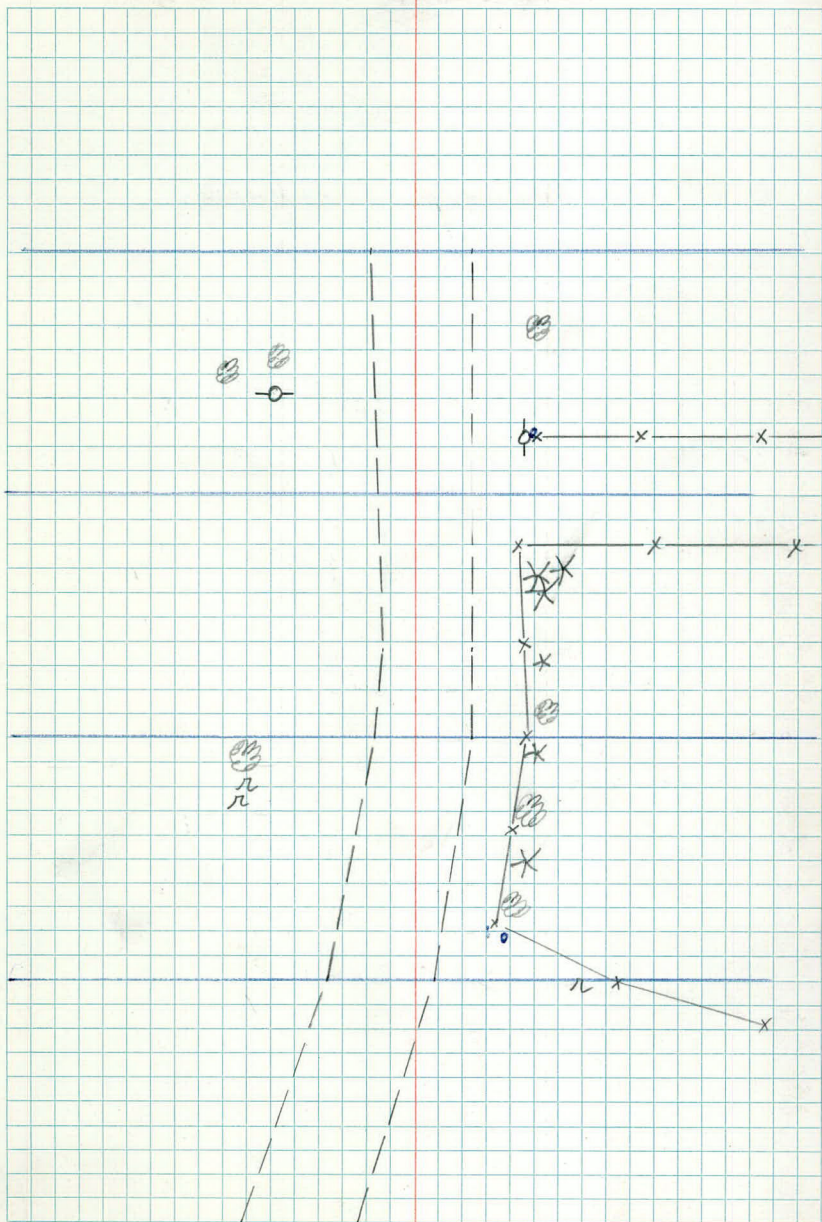
m

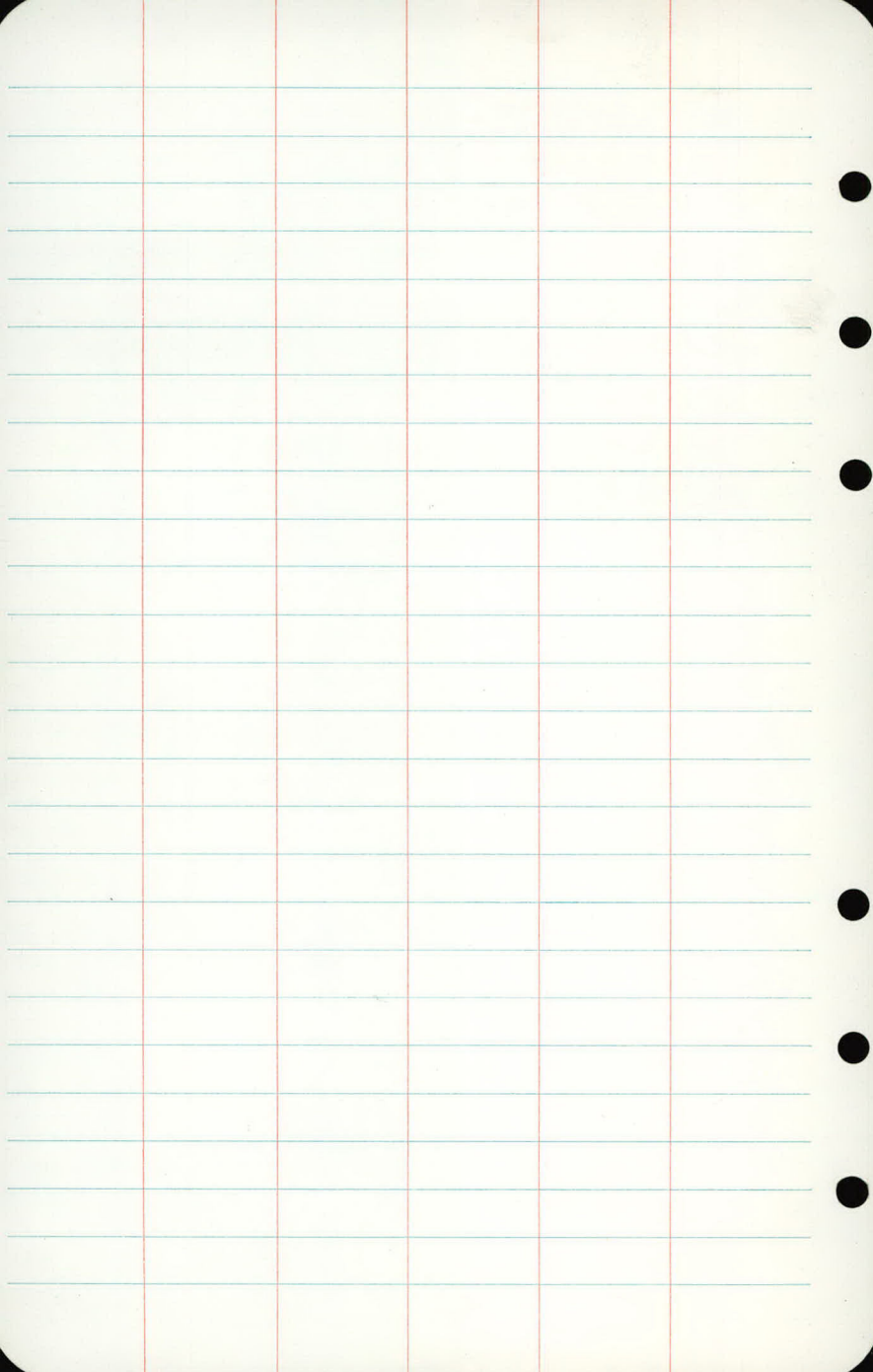
22

31
 +75 $\frac{5'' \text{Oak}}{39}$
 +71 $\frac{PP}{29}$
 Road
 9 12
 +77 $\frac{4'' \text{Oak}}{28}$
 +84 $\frac{6'' \text{CE}}{26}$
 +62 $\frac{\text{Fe Line}}{25}$
 +62 $\frac{PP}{23}$
 +49 $\frac{\text{E Ent}}{\text{Dirt}}$
 +40 $\frac{\text{Fe Cor}}{22}$
 +34 $\frac{12'' P}{31}$
 PT+18.23 Road
 7 12
 +17 $\frac{1'' P}{27}$
 Road
 8 12
 +85 $\frac{6'' \text{E/Lm}}{24}$
 +74 $\frac{3'' P}{23}$
 +65 $\frac{6'' \text{Maple}}{21}$
 +62 $\frac{\text{Fe Cor}}{17}$
 Road
 18 4
 +48 $\frac{\text{STR}}{34}$
 +84 $\frac{6'' \text{CE}}{26}$
 +62 $\frac{\text{Iron}}{26.0}$
 +34 $\frac{12'' P}{26}$
 +30 $\frac{10'' P}{27}$
 +65 $\frac{6'' \text{E/Lm}}{27}$
 +93 $\frac{2'' P}{26}$
 +96 $\frac{30'' \text{Oak}}{35}$
 +85 $\frac{\text{STR}}{37}$
 +90 $\frac{\text{STR}}{36}$
 PT 26.0 Iron
 1-2-0-1

April 6, 1970

4





3737
3766

33

26

198

⁴
³
²
¹
⁰
286.48
3726

171888

57296

200536

85944

106.742448

