

OFFICE OF COUNTY ENGINEER
RAMSEY COUNTY, MINN.

PLAN Survey

Co. Rd. "I"

From GROVELAND To T.H. #10

Road Acc't. No. DR. 13

Date Filed 3-17-65 File BK 32

Co. Rd. "I"

~~Groveland~~

~~Kirchwood~~ Dr to TH #10

Sta Point ΔL ΔR

23

+50

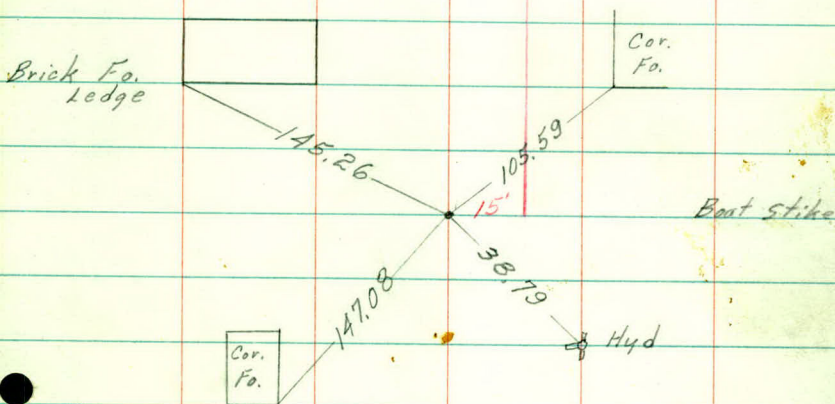
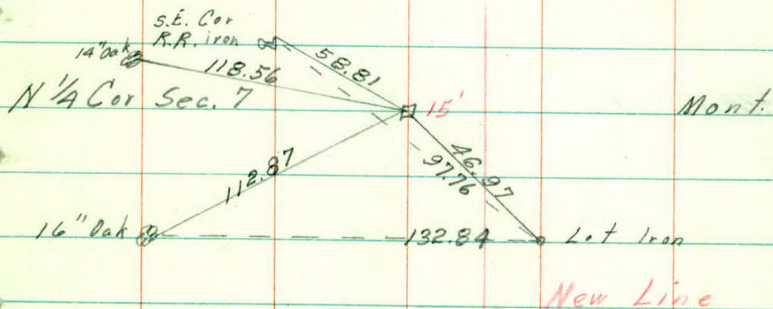
22+37.16 P.I. of Sec. Line $0^{\circ}01'45''$

22+36.92 P.C.

17+5400 P.O.T. ∇ GROVELAND ROAD

FR
RG
WM
LB
MMc

Nov. 7, 1962
Cold Overcast Windy 2
34°



Sta	Point	ΔL	ΔR
-----	-------	------------	------------

+22.63	P.T.	17° -	
--------	------	-------	--

27		16° 12'	
----	--	---------	--

+50		14° 27'	
-----	--	---------	--

26		12° 42'	
----	--	---------	--

+50		10° 57'	
-----	--	---------	--

✓
 $\Delta = 34^\circ R$

25		9 12'	
----	--	-------	--

$D = 7^\circ$

24+87.16	P.I.		
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$T = 250.24$

+50		7° 27'	
-----	--	--------	--

$L = 485.71$

24		5° 42'	
----	--	--------	--

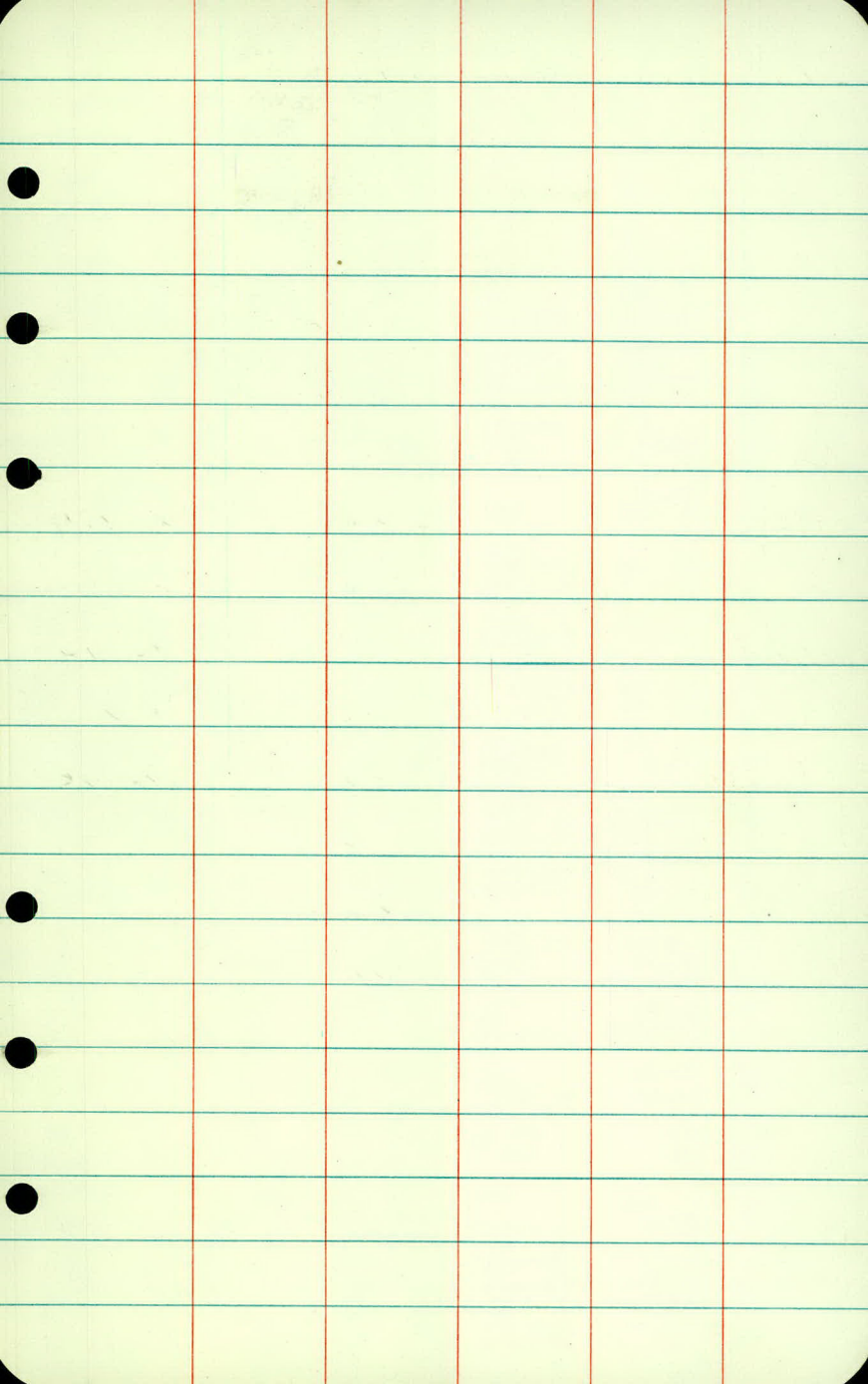
$R = 818.51$

+50		3° 57'	
-----	--	--------	--

23		2° 12'	
----	--	--------	--

+50		0° 27'	
-----	--	--------	--

22+36.92	P.C.	0° 00'	
----------	------	--------	--



New Curve

Sta Point ΔL ΔR

+74.59	PT	17° -	P.I. = 25+09.74
+50		15° 46'	$\Delta = 34^\circ R$
26		13° 16'	$D = 10^\circ$
+50		10° 46'	$T = 175.15'$
25		8° 16'	$L = 340'$
+50		5° 46'	$R = 572.96'$
24		3° 16'	
+50		0° 46'	
23+34.59	P.C.	0° 00'	

Nov. 7, 1962

3

595.00

• spike

○

iron

250

Sta	Point	ΔL	ΔR
-----	-------	------------	------------

+02.86	P.T.	$17^{\circ}00'$	
--------	------	-----------------	--

33		$16^{\circ}54'$	
----	--	-----------------	--

+50		$15^{\circ}09'$	
-----	--	-----------------	--

32		$13^{\circ}24'$	
----	--	-----------------	--

+50		$11^{\circ}39'$	
-----	--	-----------------	--

31		$9^{\circ}54'$	
----	--	----------------	--

20+67.39	P.I.		
----------	------	--	--

+50		$8^{\circ}09'$	
-----	--	----------------	--

30		$6^{\circ}24'$	
----	--	----------------	--

+50		$4^{\circ}39'$	
-----	--	----------------	--

29		$2^{\circ}54'$	
----	--	----------------	--

+50		$1^{\circ}09'$	
-----	--	----------------	--

28+17.15	P.C.	$0^{\circ}00'$	
----------	------	----------------	--

$\Delta = 34^{\circ}Lt.$

$D = 7^{\circ}$

$T = 250.24$

$L = 485.71$

$R = 818.51$

295.71
19

Nov. 7, 1962

4

545.43

0

iron

Sta Point ΔL ΔR

38+49.70 End at Edge Conc.

+59.99 P.T. 24 13.6

+50 23° 31.6

37 20° 01.6

+50 16° 31.6

$\Delta = 43^\circ 27' 15''$

36 13° 01.6

$D = 14^\circ$

35+98.05 P.I.

$T = 184.16$

+50 9° 31.6

$L = 346.10$

35 6° 01.6

$R = 409.26$

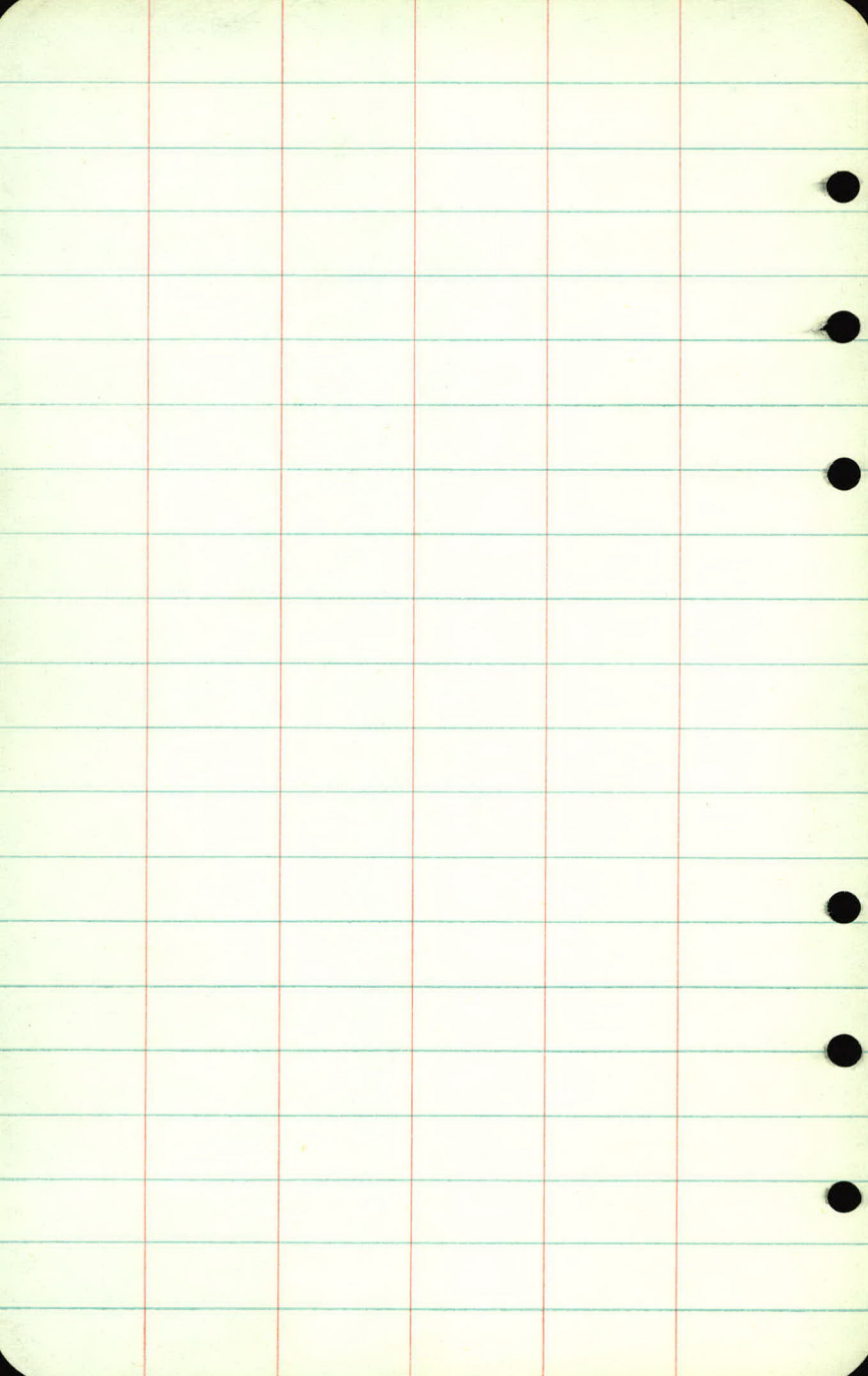
+50 2° 31.6'

34+13.89 P.C. 0° 00'

Nov. 7, 1962

5





RG
DS
WS

Dec 19, 1962
c/- 30°

T1

Topography

Lt

£

Rt

21+00 . Fe . Trees
+00 60 +00 90+

. Trees
+00 90+

20+00 +14 $\frac{3W Fe}{6}$. Fe Cor
+14 60

Cess Pool . MH 30 . End.
+60 48 +64 16 +95 66-91
+15 57 +27 58 +42 58
19+00 +00 . Beg. Scattered .
oaks Garden
91+ +03 66-91

+66 $\frac{4" Apple}{53}$ +66 $\frac{4" Apple}{65}$

. 1" Pine . 1" Pine . 3 Bushes
+98 86 +98 71 +99 61

. Tw. 0.12" . 5"p . Tw. 10"0. . 7"0. . 5"p
+53 19 +63 16 +67 53 +72 21 +84 13

. End SW
+50 73

. 14"0 . Tw. 12"0. . 8"0. . 5" Poplar
+36 30 +39 28 +41 42 +48 36

. NE Cor Ho . End £ . Tw. 4"0.
+30 81.5 +44 68 +44 61

. SE Cor Ho . 1" Pine . Tw. 7"0. . 8"0.
+28 76.5 +30 70 +34 55 +86 67

18+00

. 4"0. . 8"0 . 9"0. . Tw. 4"0.
+11 21 +19 27 +25 64 +26 30

. Beg 3'SW . PP
+82 73 +74 60

. Tw. 5"0. . 5" Apple . 9" Apple
+01 20 +07 65 +07 84

. 4 £ 8' Ent.
69

. 3"0. . 9"0. . 7"0. . 5"p
+91 18 +94 20 +96 29 +98 17

+64 Edge B.T. +74 17 +82 20 +98 19

+54 £ Groveland +91 Hedge
33-70+

17+00

Dec 19, 1962

Lt.

E

Rt.

T2

W

W

W

Scattered large oaks

Wood Posts 3 in. (Poor Cond)

4.5 ft. B.W. (Poor Cond)
Steel Posts

N

CORN
Cess Pool
GARDEN

MH 30

MH 30

20.8
20.3
1-5-F
4-1
26.2

24.5
1-5-F
16.5

Grove land

Rd.

Lt

E

Rt.

26+00

25+00

$\begin{array}{r} \text{MH 31} \\ +69 \quad 47 \end{array}$

24+00

23+00

$\begin{array}{r} \text{End Fe} \\ +11 \quad 60 \end{array} \quad \begin{array}{r} \text{End Trees} \\ +07 \quad 90+ \end{array}$

22+00

Dec. 19, 1962

Lt.

\$

Rt

T-3

Cult.

MH 31 O

Cult.

Lt.

£

Rt.

$$+60 \quad \frac{\text{Field}}{112}$$

$$+60 \quad \frac{\text{Field}}{4}$$

31+00

$$+60 \quad \frac{\text{Field}}{12}$$

$$+50 \quad \frac{\text{Field}}{23}$$

30+00

$$+60 \quad \frac{\text{Field}}{37}$$

$$+50 \quad \frac{\text{Field}}{55}$$

29+00

$$+60 \quad \frac{\text{Field}}{72}$$

$$+50 \quad \frac{\text{Field}}{90}$$

28+00

$$+60 \quad \frac{\text{Alfalfa} \cdot \text{Cor. Cult. Field}}{110} \quad \text{RT27+76}$$

27+00

Dec. 19, 1962

Lf.

E

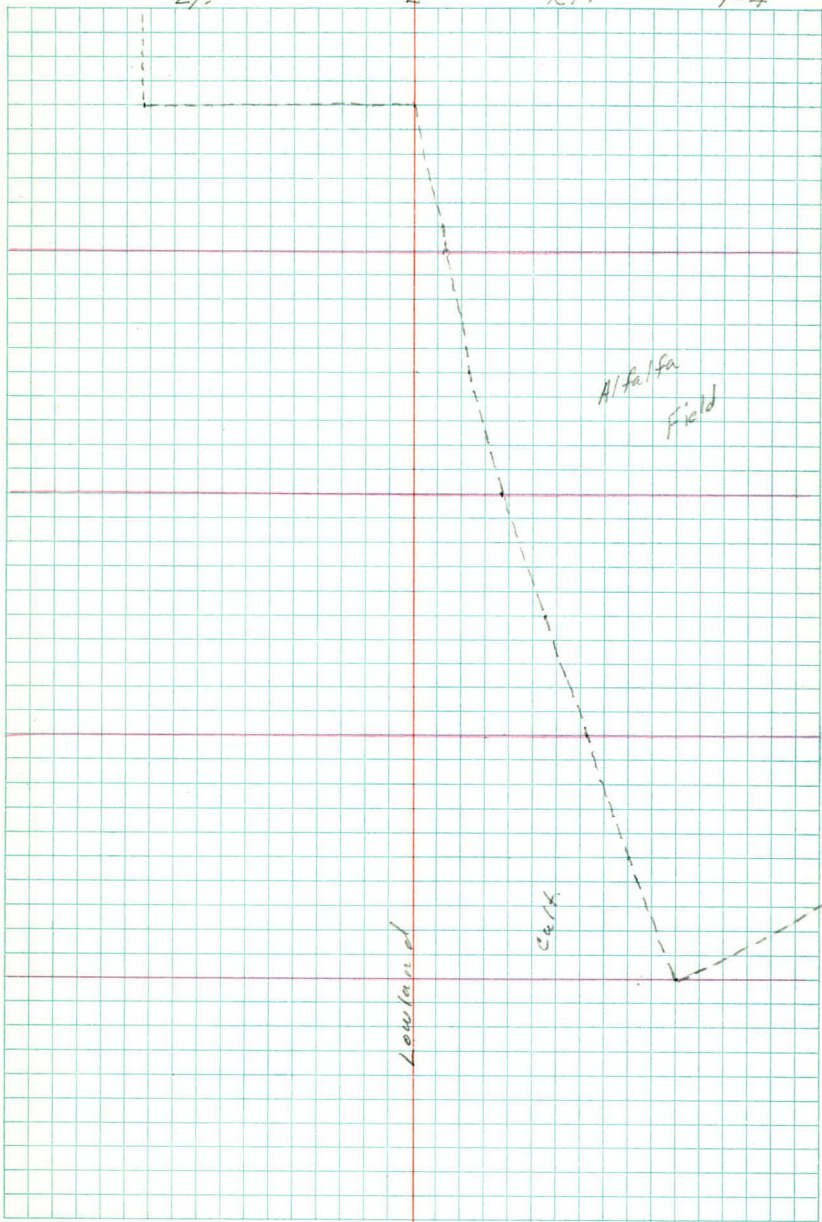
Rt.

T-4

Alfalfa
Field

Clark

Lowland



Lt.

±

Rt.

36+00

+00 Edge Field

66

± ditch

+00

27

1" Plum Tree

± ditch

1" Plum Tree

+70

2

+77

±

+70

1

1" Plum Tree

1" Plum Tree

+56

8

+66

4

+50

Edge Field

12

+42

Edge Field

±

+50

± ditch

37

35+00

+00

Edge Field

86

34+00

33+00

32+00

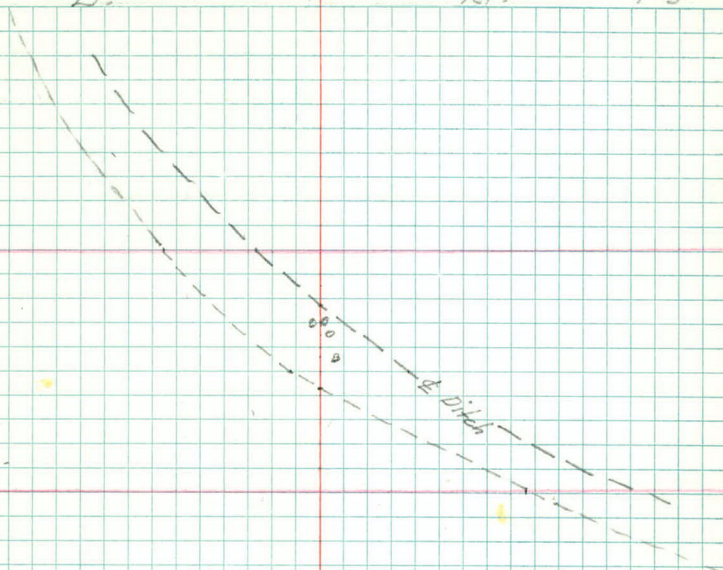
Dec. 19, 1962

Lt.

E

Rt.

T-5



Alfalfa
Field

Lt.

±

Rt.

39+00

+49.7 Edge Conc also ± 24' Ent
±• So. edge 12" x 36" CM
+32 20

38+00

• PP
+93 27also P.T. No. edge ent cor. PKg Let
+60 ± +15 33++23 Light Pole RT +16
• Bag. Fe ± cor. PKg. Let.
+23 32 RT = +17
Driving Tees
+06 41 RT = 36+98

37+00

Dec. 19, 1962

Lt.

E

Rt

T-6

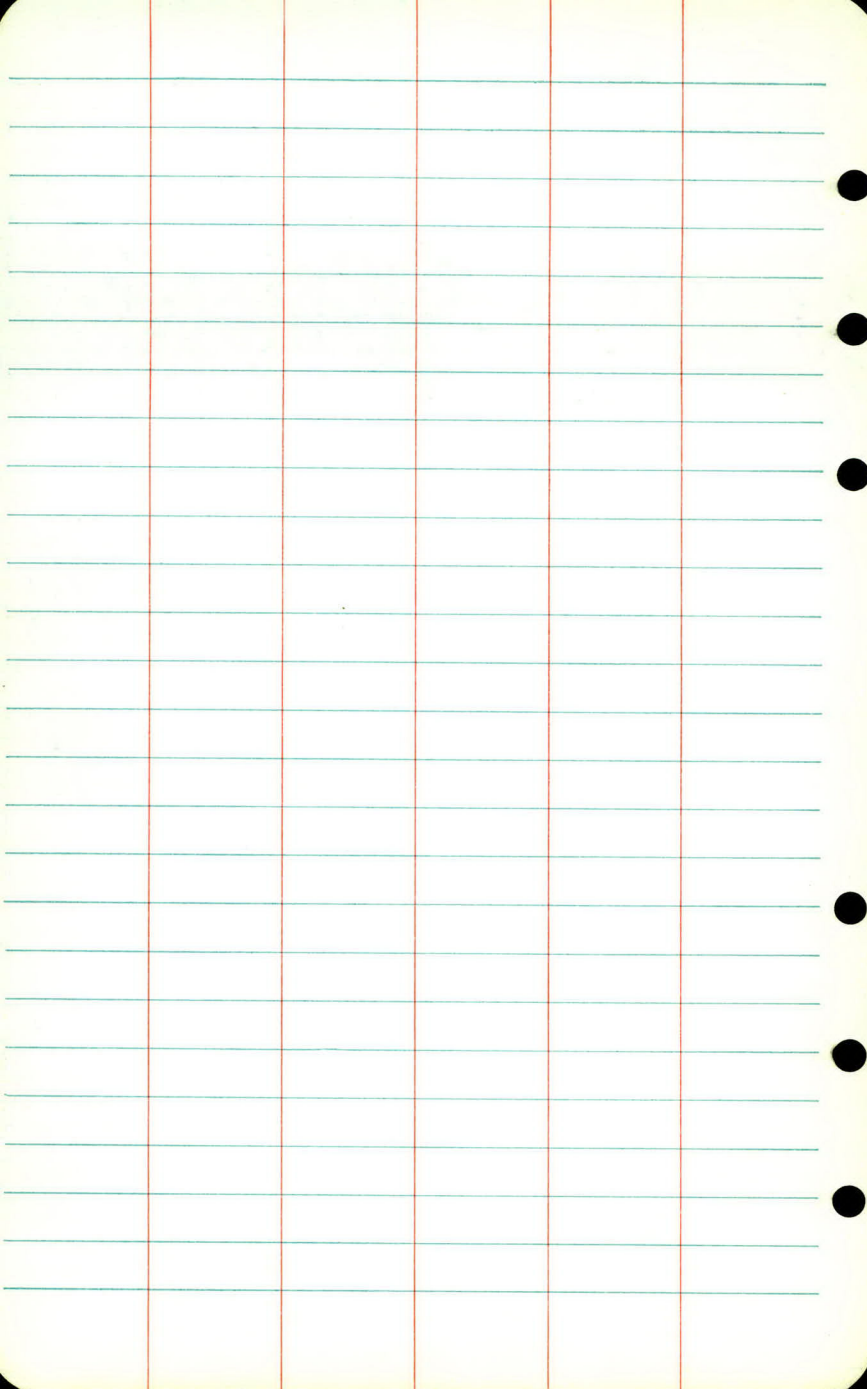


T.H. #10



φ

Wood sec 2 (2 board)
12' 13' 14' 15' 16' 17' 18' 19' 20' 21' 22' 23' 24' 25' 26' 27' 28' 29' 30' etc



R6
DS
WS

Dec 19, 1962
cl. 30°

B1

Bench Levels

Sta	+	π	-	Elev.	
BM ₁	3.90	915.04		911.14	911.14
TBM ₁	5.57	916.94	3.67	911.37	
BM ₂	5.26	920.86	1.34	915.60	
BM ₃	1.48	917.46	4.88	915.98	
BM ₄	3.17	912.28	8.35	909.11	
TBM ₂			2.73	909.55	
BM ₅	5.74	912.43	5.59	906.69	
TBM ₃			3.65	908.78	
BM ₆	6.10	913.81	4.72	907.71	
BM ₇	7.43	918.75	2.49	911.32	
TP ₁	2.33	918.73	2.35	916.40	
TP ₂	5.41	919.18	4.96	913.77	
BM ₈			4.94	914.24	913.91
BM ₈	4.90	919.14		914.24	
TP ₂	4.97	918.74	5.37	913.77	✓
TP ₁	2.07	918.48	2.33	916.41	916.40
BM ₇	2.46	913.79	7.15	911.33	911.32
BM ₆	5.06	912.78	6.07	907.72	907.71
BM ₅	6.42	913.12	6.08	906.70	906.69

Dec. 19, 1962

Description

52

NE Cor. Pump Ho. #11 Conc. Ent. Slab, Spring Lake

Spike in Ave. Lt. Pole Int. Co. Rd. I & Spring Lake Park Rd.

Top Arrow Point on Hyd. SW Cor. Knollwood Dr. & "I"

Top Arrow Point on Hyd. SW Cor. Groveland Rd. & "I"

(No. Edge)

Top R.R. Iron 58.8' No. of PI Sta 22+37.16

Se. rim MH #31

Top south end 30" CM 250'± East of MH #31

Se. Rim MH #32 100'± E. of above CM

Spike in PP 200' NW of Prep. Int. Co. Rd. "I" & Hwy 10

Spike in Trans. Pole 150'± So. of Prep. Int. Co. Rd. "I" & Hwy #10

Double spike in PP

nail in PP

RR Spike in 24" O. SW Int. Long Lake Rd & Hwy #10

Sta	+	π	-	Elv.	
BM4	7.94	917.05	4.01	909.11	909.11
BM3	5.22	921.20	1.07	915.98	915.98
BM2	0.58	916.18	5.60	915.60	915.60
TBM1	3.59	914.96	4.81	911.37	911.37
BM			3.82	911.14	911.14

KP
WM
DS
WS
R. BOSS

20 DEC. 1962
SUNNY 18°

1

CO. RD. I

GROVELAND RD TO STH#10

X- SECTIONS

STA + π - ELEV.

BM 2.34 918.32

915.98

17+54 = $\frac{1}{2}$ GROVELAND

✓

+66 = GUTTER

+74

✓

18+00

20 DEC. 1962

LT

d

RT

.2

TOP ARROW POINT ON HYD. SW. COR. GROVELAND? I

12.1	12.4	12.6	13.0	9/13.3	13.6	13.8	13.9	13.9
6.2	5.9	5.7	5.3	5.0	4.7	4.5	4.4	4.4
130	100	76	31		36	64	90	100

12.0	11.8	12.8	13.4	13.9	14.0
6.3	6.5	5.5	4.9	4.4	4.3
166	200	200	175	150	125

12.5	12.7	13.1	13.2	9/13.2	13.7	13.8	13.9
5.8	5.6	5.2	5.1	5.1	4.6	4.5	4.6
100	74	48	28	28	64	100	

13.5	13.7	13.2	13.1	9/13.4	13.7	14.4	14.6	14.1
4.8	4.6	5.1	5.2	4.9	4.6	3.9	3.7	4.2
60	49	21	8	10	16	44	73	

12.8	12.6	13.9
5.5	5.7	4.4
64	100	10.0

12.7	13.09	12.6	12.0	12.5	12.8	12.8	13.4	13.9	14.2	14.2
5.6	5.23	5.7	6.3	5.8	5.5	5.5	4.9	4.4	4.1	4.1
100	74	61	31	12	12	24	48	68	100	

±3.05W

STA	+	π	-	ELEV.
-----	---	-------	---	-------

		918.32		
--	--	--------	--	--

8+50				
------	--	--	--	--

✓				
---	--	--	--	--

9+00				
------	--	--	--	--

✓				
---	--	--	--	--

+31				
-----	--	--	--	--

✓				
---	--	--	--	--

TP	4.07	914.25	8.14	910.18
----	------	--------	------	--------

20 DEC. 1962

LT

RT

.3

13.1	10.9	10.7	10.4	10.7	10.7	11.1	11.9	13.2
5.2	7.4	7.6	7.9	7.6	7.6	7.2	6.4	5.1
71	56	39	11		12	25	42	61

13.55
4.77
74
← 3.0 SW

12.9
5.4
78
140

14.0
4.3
78
140

9.5	9.8	9.4	9.3	9.2	9.4	9.9	10.5	10.5
8.8	8.5	8.9	9.0	9.1	8.9	8.4	7.8	7.8
100	53	53	21		9	24	44	58

13.6
4.7
100

12.3
6.0
81

11.2
7.1
68

9.3	9.6	9.6	9.4	9.4	8.8	8.8	8.9	9.0	9.8	10.1
9.0	8.7	8.7	8.9	8.9	9.5	9.5	9.4	9.3	8.5	8.2
100	80	59	39	16		16	36	49	69	85

9.5
8.8
100

TOP S. RIMM H STA 19+64 LT 16.

STA

+

T

-

ELEV.

914.25

19458

6.92 907.33

+ 64

4.07 910.18

+ 75

✓

20400

✓

LT

E

20 DEC. 1962

RT

4

TOP CESSPOOL COVER 49.0 LT

TOP WATER DEPT. MH 16.0 LT

9.8	10.0	9.3	9.8	8.9	8.4	8.6	8.4	8.3	8.0
4.5	4.3	5.0	4.5	5.4	5.9	5.7	5.9	6.0	6.3
43	49	32	14	7		11	34	58	78
9.2	9.4								7.9
5.1	4.9								6.4
88	100								100

9.9	9.0	9.8	8.9	8.3	8.1	7.3	7.0	6.8
4.4	5.3	4.5	5.4	6.0	6.2	7.0	7.3	7.5
45	27	15	7		20	45	70	100

9.9	10.1	9.9
4.4	4.2	4.4
67	89	100

STA

+

K

-

ELEV.

914.25

20450

✓

✓

21400

✓

✓

20 DEC. 1962

LT

2

RT

.5

8.9	9.6	8.9	8.1	7.9	7.8	7.2	6.8	6.7
5.4	4.7	5.4	6.2	6.4	6.5	7.1	7.5	7.6
20	13	8	4		15	38	64	78

8.7	10.1	9.5	10.2
5.6	4.2	4.8	4.1
36	47	57	61

6.2	6.5
8.1	7.8
100	80

9.7	10.1	10.1
4.6	4.2	4.2
100	92	82

8.6	9.2	8.7	8.2	8.0	7.7	7.1	7.2	7.1
5.7	5.1	5.6	6.1	6.3	6.6	7.2	7.1	7.2
23	14	8	4		21	50	83	100

9.2	9.9	9.2	9.0
5.1	4.4	5.1	5.3
39	50	69	90

8.9
5.4
100

STA

+

π

-

ELEV.

914.25

21+50

✓

22+00

✓

✓

TP

3.96

913.06

5.15

909.10

(909.11)

LT

±

20 DEC. 1962

RT .6

9.2	8.2	9.1	8.3	8.2	7.9	7.7	8.1	8.2
5.1	6.1	5.2	6.0	6.1	6.4	6.6	6.2	6.1
39	21	14	4		24	52	65	86

9.0	8.8	8.7					8.1
5.3	5.5	5.6					6.2
61	85	100					100

8.9	8.2	9.1	9.4	8.5	8.7	8.8	9.1	8.6
5.4	6.1	5.2	4.9	5.8	5.6	5.5	5.2	5.7
34	25	20	10		24	43	69	90

10.7	9.3	8.2	8.1				8.4
3.6	5.0	6.1	6.2				5.9
42	51	58	78				100

8.7
5.6
100

TOP N. EDGE R.R. IRON 58.8 N. OF P1 STA 22+37.16

STA

+

π

-

ELEV.

913.06

22+50

✓

23+00

✓

23+50

✓

RG
DS
WS
R. Boss

LT

£

Dec 21, 1962
Snowing 25°
RT

.7

10.2	8.0	8.1	9.3	8.5	8.3	8.1	8.6	8.3	9.2
2.9	5.1	5.0	3.8	4.6	4.8	5.0	4.7	3.8	3.9
41	32	25	19	8		21	47	76	100

9.8	8.2	8.0	8.3
3.3	4.9	5.1	4.8
53	58	81	100

8.1	8.1	8.8	7.3	7.4	7.2	7.2	7.6	8.1	8.1
5.0	5.0	4.3	5.8	5.7	5.9	5.9	5.5	5.0	5.0
34	27	23	15	7		20	46	73	100

8.9	10.3	7.1	6.9	6.8
4.2	2.8	6.0	6.2	6.3
38	50	61	82	100

8.5	7.8	7.7	7.5	8.1	7.1	6.8	6.7	7.0	7.6	7.5
4.6	5.3	5.4	5.6	5.0	6.0	6.3	6.4	5.8	5.5	5.6
44	42	36	31	22	14		24	53	80	100

9.4	6.1	5.9	5.8
3.7	7.0	7.2	7.3
56	70	85	100

Sta

+

 π

-

E/V.

913.06

24+00

✓

24+50

✓

25+00

✓

TBM₂

1.69

911.24

3.51

909.55

909.55

Dec 21, 1962

LT

Z

RT

.8

8.7	7.7	7.9	7.8	7.1	6.8	6.7	7.1	7.3	7.5
4.4	5.4	5.2	5.3	6.0	6.3	6.4	6.0	5.8	5.6
57	50	39	32	23		28	50	74	100

9.0	7.5	5.9	5.7
4.1	5.6	7.2	7.4
67	74	79	100

8.9	7.7	8.7	9.0	7.2	6.6	6.8	6.8	6.6	6.9
4.2	5.4	4.4	4.1	5.9	6.5	6.3	6.3	6.5	6.2
71	64	53	44	34		22	47	80	100

8.7	6.2	6.0
4.4	4.9	7.1
83	92	100

7.8	9.6	9.7	7.5	6.9	6.4	6.2	6.6	6.3	6.2
5.3	3.5	3.4	5.6	6.2	6.7	6.9	6.5	6.8	6.9
87	73	65	52	25		23	57	79	100

8.9
4.2
100

Sta

+

π

-

ELV

911.24

25+50

✓

26+00

+50

27+00

+50

7.07 904.17

Dec 21, 1962

LT

4

RT

.9

9.2	8.2	6.8	5.8	5.6	5.4	5.5	5.6
2.0	3.0	4.4	5.4	5.6	5.8	5.7	5.6
87	80	72	31		33	68	100

8.1	7.3
3.1	3.9
97	100

8.1	6.8	5.8	5.8	5.5	5.1	5.1	5.3
3.1	4.4	5.4	5.4	5.7	6.1	6.1	5.9
100	91	68	35		35	76	100

5.5	5.5	6.0	6.4	5.9	5.4	5.6	5.7	6.1
5.7	5.7	5.2	4.8	5.3	5.8	5.6	5.5	5.1
100	86	60	28		25	52	79	100

5.3	5.4	5.5	6.1	6.2	6.5	6.0	5.5	6.2	6.2
5.9	5.8	5.7	5.1	5.0	4.7	5.2	5.7	5.0	5.0
100	87	63	37	16		28	58	84	100

5.3	5.4	5.7	6.1	6.4	6.0	5.7	6.0	6.9
5.9	5.8	5.5	5.1	4.8	5.2	5.5	5.2	4.3
100	73	46	19		20	46	72	100

FL S. END 30" CM 176" LT STA 27+50

STA	+	π	-	ELEV.
		911.24		
28+00				
+50				
29+00				
TP			4.39	906.85
BM	7.25	913.94	4.50	906.68 (906.69)

21 DEC 1962

LT

E

RT

.10

5.1	5.3	5.4	5.5	5.6	5.6	5.9	6.0	1.0
6.1	5.9	5.8	5.7	5.6	5.6	5.3	4.4	4.2
100	89	61	27		32	65	88	100

✓

5.3	5.3	5.3	5.5	5.7	5.9	6.5	7.0	7.4
5.9	5.9	5.9	5.7	5.5	5.3	4.7	4.2	3.8
100	87	62	29		21	40	63	100

✓

5.3	5.4	5.5	5.7	6.0	7.2	7.3	7.5	7.6
5.9	5.8	5.7	5.5	5.2	4.0	3.9	3.7	3.6
100	79	55	25		33	60	86	100

✓

TOP NAIL & STA 29+50

TOP S. END 30" CM 250'± E. MH# 31

STA

+

π

-

ELEV.

913.94

29+50

✓

30+00

+50

31+00

+50

26 DEC 1962

LT

Z

RT

.11

5.3	5.5	5.6	6.1	6.8	7.2	7.7	7.9	8.1
8.6	8.4	8.3	7.8	7.1	6.7	6.2	6.0	5.8
100	77	51	20		26	50	75	100

5.4	5.5	5.7	5.9	6.7	7.2	7.6	8.4	8.2
8.5	8.4	8.2	8.0	7.2	6.7	6.3	5.5	5.7
100	83	56	27		22	50	79	100

5.9	5.9	6.1	6.6	7.2	7.6	7.9	8.3	8.4
8.0	8.0	7.8	7.3	6.7	6.3	6.0	5.6	5.5
100	90	66	33		25	56	89	100

6.9	6.9	7.1	7.6	7.8	8.0	8.4	8.7	9.0
7.0	7.0	6.8	6.3	6.1	5.9	5.5	5.2	4.9
100	81	52	29		21	50	75	100

8.5	8.8	8.9	9.0	9.1	9.4	9.6	10.0	10.0
5.4	5.1	5.0	4.9	4.8	4.5	4.3	3.9	3.9
100	85	58	27		26	58	86	100

STA

+

π

-

ELEV

913.94

32+00

+27

TP 5.89 917.23 2.60 911.34

32+50

33+00

+50

26 DEC. 1962

L7

E

R7

.12

9.4	9.6	9.7	10.2	10.5	11.0	11.1	11.0	11.0
4.5	4.3	4.2	3.7	3.4	2.9	2.8	2.9	2.9
100	80	55	30		27	56	83	100

9.1	9.7	10.4	11.2	11.1	12.2	12.7	12.7	12.6
4.8	4.2	3.5	2.7	2.2	1.7	1.2	1.2	1.3
100	81	56	28		28	59	85	100

Top NAIL E STA 32+50

8.9	9.5	10.0	10.8	11.3	12.0	12.7	12.4	12.4
8.3	7.7	7.2	6.4	5.9	5.2	5.0	4.8	4.8
100	76	50	23		27	60	83	100

8.9	9.5	10.3	11.1	12.1	12.4	12.9	13.1	13.2
8.3	7.7	6.9	6.1	5.1	4.8	4.3	4.1	4.0
100	77	50	26		32	67	90	100

8.6	9.6	10.1	11.5	12.5	12.9	12.9	13.1	13.0
8.6	7.6	6.5	5.7	4.7	4.3	4.3	4.1	4.2
100	76	49	26		32	61	90	100

STA

+

π

-

ELEV.

917.23

34+00

+50

35+00

35+00

+25

+25

BM

9.54

907.69

907.71

26 DEC. 1962

LT

Z

RT

.13

9.1	9.1	10.6	11.3	11.9	12.1	12.0	11.8	11.7
8.1	7.5	6.6	5.9	5.3	5.1	5.2	5.4	5.5
100	79	54	29		28	56	82	100

✓

10.1	10.4	11.1	11.6	11.5	11.5	11.2	11.0	10.8
7.1	6.8	6.1	5.6	5.7	5.7	6.0	6.2	6.4
100	88	56	24		28	58	79	100

✓

10.0	10.6	11.3	11.7	11.8	11.7	11.3	11.0	11.0
7.2	6.7	5.9	5.5	5.4	5.5	5.9	6.2	6.2
100	90	64	29		27	57	83	100

✓

10.6	11.5	12.2	12.2	12.5	12.7	12.4	12.6	12.5
6.6	5.7	5.0	5.0	4.7	4.5	4.8	4.6	4.7
100	81	62	32		30	59	90	100

✓

SPIKE IN PP 200' NW OF Prop INT CORDI & STH #10

STA	+	π	-	ELEV.
-----	---	-------	---	-------

B.M.	9.36	917.07		
------	------	--------	--	--

				907.71
--	--	--	--	--------

35+50

✓

+74

✓

+80

FX
HP
WS
DS
R Boss

LT

27 DEC. 1962
Clear Cool 12°
RT

.14

B.M. Spike in PP 200' NW. of Prop.
Intersection Co Rd "I" & T.H. # 10

10.6	10.8	11.6	12.8	13.8	14.8	13.9	10.7	10.7	13.1
6.5	6.3	5.5	4.3	3.3	2.3	3.2	6.4	6.4	4.0
100	94	78	45	18		20	33	55	81

13.1	13.3
4.0	3.8
100	87

11.9	13.6	14.5	12.0	10.6	10.7	13.3	12.7	12.8
5.2	3.5	2.6	5.1	6.5	6.4	3.8	4.4	4.3
85	56	34	19		21	29	54	79

11.2
5.9
100

12.1
5.0
100

13.3	14.7	12.1	11.2	10.7	13.8	13.4	12.6	12.5
3.8	2.4	5.0	5.9	6.4	3.3	3.7	4.5	4.6
69	51	33	19		15	27	42	56

12.1	11.6
5.0	5.5
90	100

12.7	13.0
4.4	4.1
100	87

STA + π - ELEV.

917.07

35+94

✓

36

✓

+50

27 DEC. 1962

LT

F

RT

15

14.5	12.6	10.1	11.8	13.8	13.8	12.3	12.1	12.8
2.6	4.5	6.4	5.3	3.3	3.3	4.8	5.0	4.3
56	45	29	17		10	40	66	90

12.8 11.5
4.3 5.6
79 100

12.8
4.3
100

12.4	10.9	11.8	13.6	14.1	13.7	12.3	11.7	12.0
4.7	6.2	5.3	3.5	3.9	3.9	4.8	5.4	5.1
50	33	24	15		17	40	65	100

14.6 12.6 11.8
2.5 4.5 5.3
67 88 100

11.2	12.4	13.5	12.8	12.7	12.5	12.4	11.9	11.6
5.9	4.2	3.6	4.3	4.4	4.6	4.7	5.2	5.6
82	70	59	26		23	35	59	86

11.1 11.9
6.0 5.2
97 100

11.4
5.7
100

Sta + π - Elev

917.07

37+00

+50

38+00

+3

+32 Inv. 12" CM

+35 $\neq$ Ditch

✓

Dec. 23 1962

Lt

L

BT 16

11.1	11.2	11.8	12.2	12.1	11.8	11.4	11.2
6.0	5.9	5.3	4.9	5.0	5.3	5.7	5.9
100	65	29		23	51	83	100

9.7	9.8	10.6	11.0	11.4	11.5	11.5
7.4	7.3	6.5	6.1	5.7	5.6	5.6
100	75	36		30	73	100

1.1	8.1	8.1	9.8	10.6	11.2	10.9	10.5	10.4	10.2
9.4	9.0	8.4	7.3	6.5	5.9	6.2	6.6	6.7	6.9
100	81	54	25	13		19	43	74	100

9.29
8.78
22

8.36
8.21
17

1.2	1.6	8.2	8.6	10.9	11.0	10.9	8.1	8.1	8.9
9.9	9.5	8.9	8.5	6.2	6.1	6.2	8.4	8.4	8.2
100	76	48	22	18		14	17	42	70

9.1
8.0
100

Sta + π - Elev.

917.07

38+41 Shoulder Line

+49.7

+25

+65

✓

BM

9.36 907.71 (907.71)

Dec. 27, 1962

Lt.

Rt. 17

9.8	9.9	10.1	10.4	11.0	10.8	10.8	11.0	11.0
7.3	7.2	7.0	6.7	6.1	6.3	6.3	6.1	6.1
100	90	62	28	✓	18	49	79	100

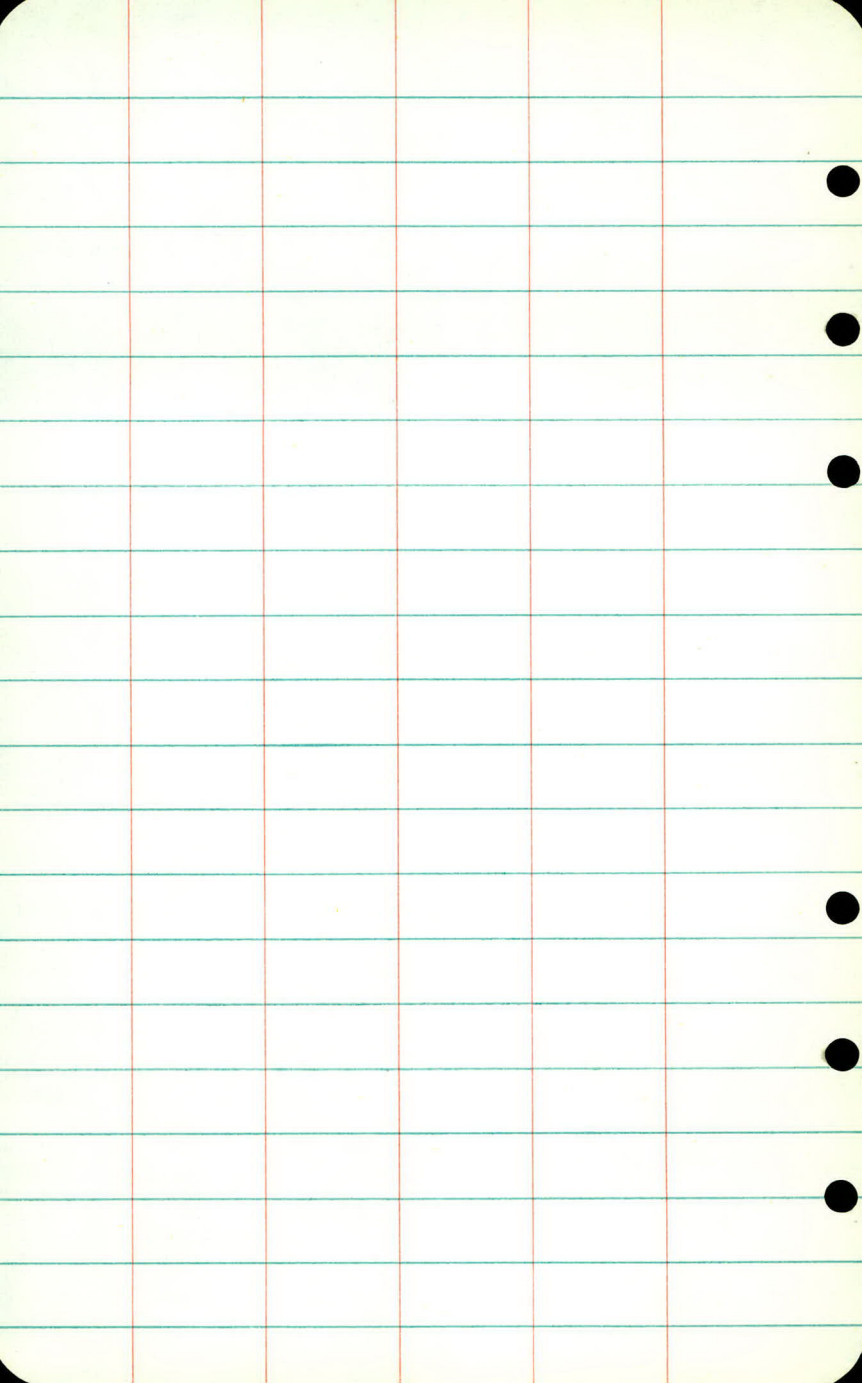
10.35	10.43	10.69	10.93	11.02	11.12	11.26
6.72	6.64	6.38	6.14	6.05	5.95	5.81
100	79	40	✓	24	50	77

11.35
5.72
100

10.54	10.61	10.79	10.95	11.07	11.17	11.27	11.40
6.55	6.40	6.28	6.12	6.00	5.90	5.80	5.67
100	75	50	25	✓	25	50	75

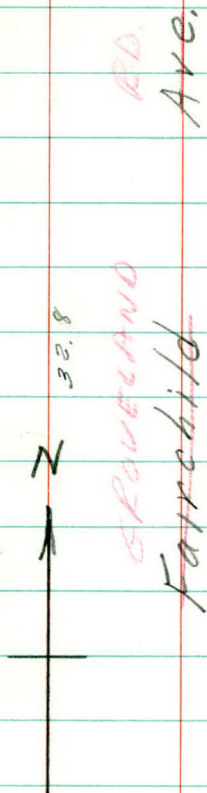
11.51
5.56
100

Spike in PP 200' N.W. of Proposed Intersection
Co Rd I + TH #10

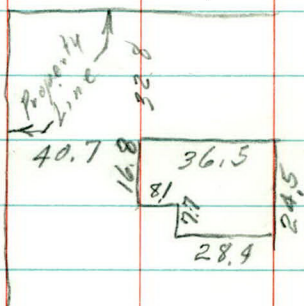


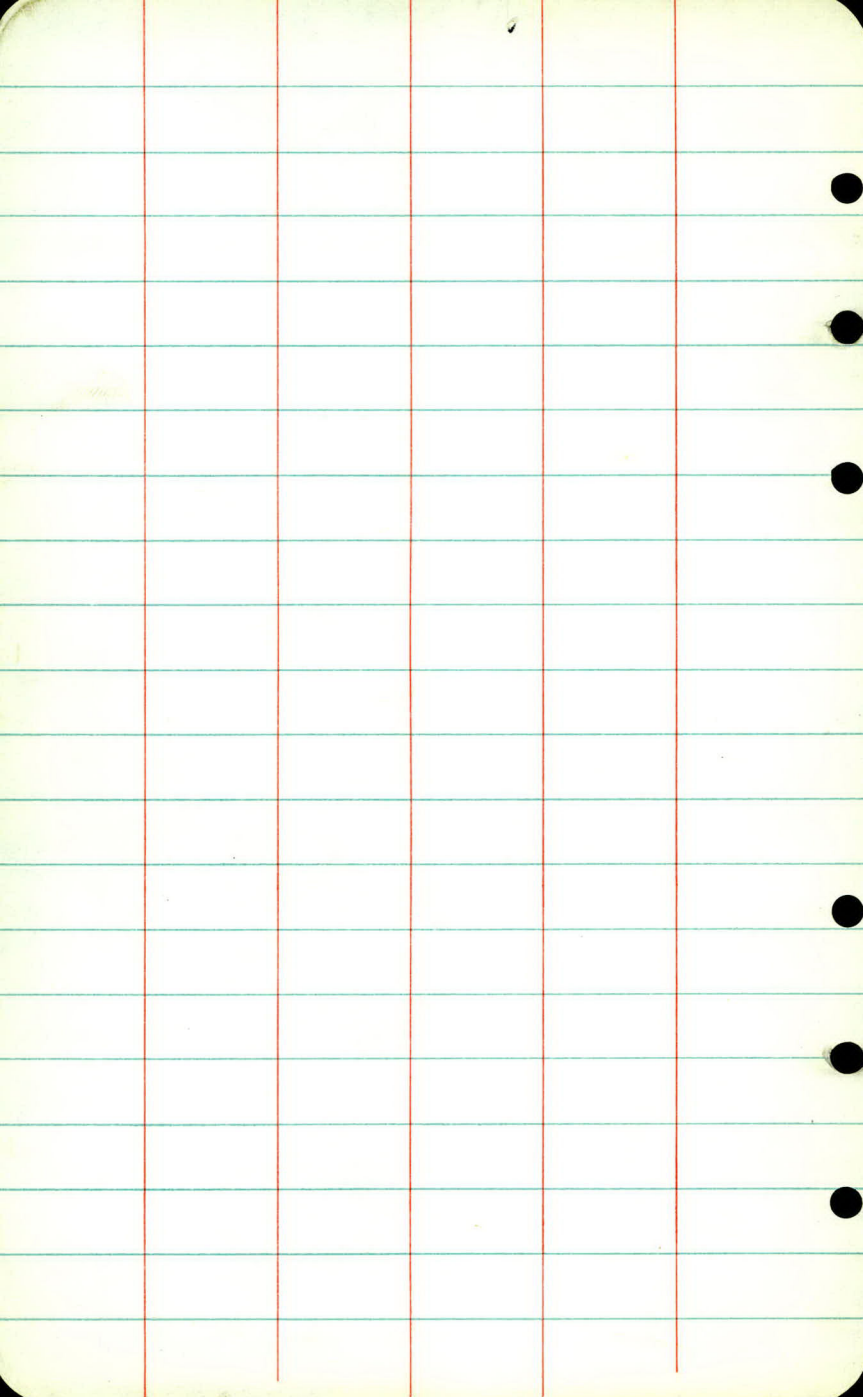
FX
RG
WM
LB

Oct. 9, 1962
Clear Cool 56°



Co. Rd "1"





1
Staking

Sta	PG	PGR	^{10.5} SGR	Elev	DGR
BM	0.11	916.09			(915.98)
18	13.14	2.95	3.45		3.95
+50	12.97	3.12	^{3.3} 3.62		
19	12.80 ₁₇	3.29	⁶ 3.79		
+50	12.63	3.46	^{7.12} 3.96		
20	12.46	3.63	4.13		
+50	12.29	3.80	4.3		
21	12.12	3.97	4.47		
T.P.	5.55	913.55	8.09	908.00	
+50	11.95	1.60	2.10		
22	11.78	1.77	2.27		

FK
JS
FS

Oct. 23, 1963

2

2

Top Arrow Point on Hyd SW Cor Groveland

3.35

2.65

CO.1

DO.1.3

2

33=19

5.35

4.52

F1.7

F0.9

15

15

6.9

6.0

F3.1

F2.2

15

15

7.56

7.8

F3.6

F3.8

15

15

7.93

8.4

F3.8

F4.3

15

15

7.5

8.8

F3.2

F4.5

15

15

8.2

8.7

F3.7

F4.2

15

15

5.5

5.9

F3.4

F3.8

15

15

5.17

5.07

F2.9

F2.8

15

Sta	PG	PGR	10.5 SGR	Elev.	+2.0 DGR
		913.55			
22+50	11.61	1.94	2.44		
23	11.44	2.11	2.61		
+50	11.27	2.28	2.78		
24	11.10	2.45	2.95		13.5
+50	10.88	2.67	3.17		
25	10.55	3.00	3.5		
T.P.	3.96	911.20	6.31	907.24	38
+50	10.17	1.03	1.53		152
			5.64	5.6	05.6
26	19.79	1.41	1.91		
+50	9.41	1.79	2.29		
T.P.	4.07	910.81	4.46	906.74	

Oct 23, 1963

3

(15)

3.44
F3.0
15.1

5.55
F3.1 34
19.3 15

(15)

6.4
F 3.8
17.9

6.2
F3.6
20.8

(11)

6.6
F 3.8
19.4

{ 6.78
F4.0
27.0 }

(7.5)

6.75
F 3.8
24.7

{ 6.75
F3.8
27.7 }

(3)

{ 6.67
F3.5
29.0 }

{ 6.87
F3.6
29.4 }

✓

25+00
slope stake Lt

{ 6.8
F3.3
28.2 }

{ 7.5
F4.0 32
31.0 29 }

{ 5.35
F3.8
30.2 }

{ 6.1
F4.6
33.4 }

{ 5.51
F3.6
29.4 }

{ 6.31
F4.4
32.6 }

{ 5.1
F2.8
26.2 }

{ 5.6
F3.3
28.2 }

5.6

Lt Sta 26+50
slope stake

Sta	PG	PCR	SGR	Elev.
		910.81		
27	09.16	1.65	2.15	
			4.3	6.5 ✓ (6.5)
	5			
+50	09.16	1.65	2.15	
	5.76	912.50	4.07	906.74
			6.90	05.6 05.6
28	09.28	3.22	3.72	
			3.3	
			6.5	
+50	9.40	3.10	3.6	12
			3.4	12.4
			2.9	15
			6.9	
29	9.53	2.97	3.47	12
			3.4	12.6
T.P.	5.51	912.36	5.51	906.99 (906.85)
			6.4	
+50	9.65	2.7	3.2	
				0

FK
JS
FS

17

Oct. 24, 1963 4
RT

06.16

$\left\{ \begin{array}{l} 4.75 \\ F2.6 \\ 25.4 \end{array} \right\}$

$\left\{ \begin{array}{l} 4.65 \\ F2.5 \\ 25.0 \end{array} \right\}$

$\left\{ \begin{array}{l} 4.95 \\ F2.8 \\ 26.2 \end{array} \right\}$

$\left\{ \begin{array}{l} 4.95 \\ F2.8 \\ 26.2 \end{array} \right\}$

$\left\{ \begin{array}{l} 6.9 \\ F3.2 \\ 27.8 \end{array} \right\}$

$\left\{ \begin{array}{l} 7.0 \\ F3.3 \\ 28.2 \end{array} \right\}$

$\left\{ \begin{array}{l} 7.0 \\ F3.4 \\ 28.6 \end{array} \right\}$

$\left\{ \begin{array}{l} 6.5 \\ F2.9 \\ 26.6 \end{array} \right\}$

$\left\{ \begin{array}{l} 6.9 \\ F3.4 \\ 28.6 \end{array} \right\}$

$\left\{ \begin{array}{l} 5.5 \\ F2.0 \\ 23.0 \end{array} \right\}$

$\left\{ \begin{array}{l} 6.4 \\ F3.2 \\ 27.8 \end{array} \right\}$

$\left\{ \begin{array}{l} 5.2 \\ F2.0 \\ 23.0 \end{array} \right\}$

Sta	PC	PER	10.5 SGR	Elev.	+2.0 DGR
		912.36			
30	9.28	2.6	^{5.3} 31 3		3.6
+50	9.90	2.46	^{4.9} 2.96		
31	10.03	2.33	2.83		4.33
+50	10.15	2.21	2.71		4.21 2.4 2
32	10.28	2.08			4.08 2.7 1.2
TP	5.68	917.02	1.02	911.34	^{16.3} (11.34)
+50	10.40	6.62			8.62 6.9

Lt

Oct. 24, 1963 5

E

Rt

$$\left\{ \begin{array}{l} 6.5 \\ F3.4 \\ 28.6 \end{array} \right\}$$

$$\left\{ \begin{array}{l} 5.2 \\ F2.1 \\ 23.4 \end{array} \right\}$$

$$\left\{ \begin{array}{l} 5.8 \\ F1.8 \\ 22.2 \end{array} \right\}$$

$$\left\{ \begin{array}{l} 4.9 \\ F1.9 \\ 22.6 \end{array} \right\}$$

$$\left\{ \begin{array}{l} 4.8 \\ F2.0 \\ 23.0 \end{array} \right\}$$

$$\left\{ \begin{array}{l} 4.22 \\ D0.1 \\ 27.4 \end{array} \right\}$$

$$\left\{ \begin{array}{l} 3.6 \\ D0.6 \\ 29.4 \end{array} \right\}$$

$$\left\{ \begin{array}{l} 2.6 \\ D1.6 \\ 33.4 \end{array} \right\}$$

$$\left\{ \begin{array}{l} 2.7 \\ D1.4 \\ 32.6 \end{array} \right\}$$

$$\left\{ \begin{array}{l} 1.1 \\ D3.0 \\ 39.0 \end{array} \right\}$$

$$\left\{ \begin{array}{l} 6.5 \\ D2.1 \\ 35.4 \end{array} \right\}$$

9/11/34

$$\left\{ \begin{array}{l} 5.0 \\ D3.6 \\ 40.0 \end{array} \right\}$$

Sta	PG	PCR	1-	Elev	+2.0 DGR
		917.02			
33	10.53	6.5			8.5
+50	10.65	6.37			8.37 5.8 5.5 5.2
34	10.78	6.24			8.24 5.8 2.34 0.224 0.6
+50	10.90	6.12			8.12 5.5 5.2
35	11.03	6.0			8.0 5.8 5.2
+50	11.15	5.87			7.9 5.8 1.7 2.8 1.2 1.3 1.2
T.P.	3.95	917.09	3.88	913.14	12.81 7.2

Oct. 24, 1963 6

$\begin{Bmatrix} 6.3 \\ 102.2 \\ 35.8 \end{Bmatrix}$

$\begin{Bmatrix} 4.4 \\ 104.1 \\ 40.0 \end{Bmatrix}$

$\begin{Bmatrix} 5.9 \\ 102.5 \\ 37.0 \end{Bmatrix}$

$\begin{Bmatrix} 4.1 \\ 104.3 \\ 40.0 \end{Bmatrix}$

$\begin{Bmatrix} 5.84 \\ 102.4 \\ 36.6 \end{Bmatrix}$

$\begin{Bmatrix} 5.09 \\ 103.2 \\ 39.8 \end{Bmatrix}$

$\begin{Bmatrix} 5.5 \\ 102.6 \\ 37.4 \end{Bmatrix}$

$\begin{matrix} 2.16 \\ 1.4 \\ 1.4 \\ 1.1 \end{matrix}$

$\begin{Bmatrix} 5.7 \\ 102.4 \\ 36.6 \end{Bmatrix}$

$\begin{Bmatrix} 5.3 \\ 102.7 \\ 37.8 \end{Bmatrix} \begin{Bmatrix} 5.4 \\ 102.6 \\ 37.4 \end{Bmatrix}$

$\begin{Bmatrix} 5.5 \\ 102.5 \\ 37.0 \end{Bmatrix}$

$\begin{Bmatrix} 4.9 \\ 102.0 \\ 40.0 \end{Bmatrix} \begin{Bmatrix} 4.1 \\ 103.5 \\ 40.0 \end{Bmatrix}$

$\begin{Bmatrix} 5.66 \\ 101.3 \\ 32.2 \end{Bmatrix} \begin{Bmatrix} 6.1 \\ 101.8 \\ 34.2 \end{Bmatrix}$

Top slope Stake Lt Sta 35+50

Sta	PG	PGR	DGR	Elev.
-----	----	-----	-----	-------

917.09

36	11.28	5.81	2.81	14.1
----	-------	------	------	------

+50	11.32	5.77	2.77	
-----	-------	------	------	--

37	11.21	5.88	7.88	
----	-------	------	------	--

+50	11.01	6.08	8.08	
-----	-------	------	------	--

38.	11.0	6.1	8.1	
-----	------	-----	-----	--

+49.7			6.18	910.91
-------	--	--	------	--------

10.93

FK
JS
FS
RB

Oct. 25, 1963
£

7

{
6.4
DC 1.4
32.6
}

{
5.0
DC 2.8
38.2
}

{
3.77
DC 4.0
4.0
}

{
4.97
DC 2.8
38.2
}

{
5.08
DC 2.8
38.2
}

{
4.98
DC 2.9
38.6
}

{
6.2
DC 1.9
34.6
}

{
5.78
DC 2.3
36.2
}

{
7.6
DC 0.8
29.0
}

{
6.8
DC 1.3
32.2
}

Edge Conc £

Sub Grade Stakes

Sta	PQ	PGR	SGR ^{+1.2}	Elev.
-----	----	-----	---------------------	-------

BM				908.78
----	--	--	--	--------

TP	5.15	911.89		906.74
----	------	--------	--	--------

27	09.16	2.73	3.93	
		6	6.35	05.54

+50	09.16	2.73	3.93	
		3	58	

28	09.28	2.61	3.81	
----	-------	------	------	--

+50	09.40	2.49	3.69	
-----	-------	------	------	--

29	09.53	2.36	3.56	
----	-------	------	------	--

+50	09.65	2.24	3.44	
		12		

30	09.78	2.11	3.31	
----	-------	------	------	--

TP	2.03	914.78	4.14	907.75
----	------	--------	------	--------

+50	09.90	4.88	6.08	
		12		

31	10.03	4.75	5.95	
----	-------	------	------	--

FK
FS
DS

Nov. 4, 1963
Clear Cool 50°

8

Top S. End 30" CM 250' ± E of MH #31

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Too Low

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Too Low

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Iron P.I.

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Sta	PG	PGR	SGR	Elev
		914.78		

31+50	10.15	4.63	5.83	
		5.1		

32	10.28	4.50	5.7	
----	-------	------	-----	--

+50	10.40	4.38	5.58	
-----	-------	------	------	--

33	10.53	4.25	5.45	
----	-------	------	------	--

+50	10.65	4.13	5.33	
-----	-------	------	------	--

34	10.78	4.-	5.2	
----	-------	-----	-----	--

+50	10.90	3.88	5.08	
		1.2		

35	11.03	3.75	4.95	
----	-------	------	------	--

T.P.	5.64	915.46	4.96	909.82
------	------	--------	------	--------

+50	11.15	4.31	5.51	
-----	-------	------	------	--

6.31
27
5.5

Nov. 4, 1963 9

Lt

Rt

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Sta	PG	PGR	SGR	Elev
-----	----	-----	-----	------

915.46

36	11.28	4.18	5.38	
----	-------	------	------	--

+50	11.32	4.14	5.34	
-----	-------	------	------	--

4.86

37	11.21	4.25	5.45	
----	-------	------	------	--

+50	11.01	4.45	5.65	
-----	-------	------	------	--

1.2

38	11.00	4.46	5.66	
----	-------	------	------	--

BM		2.74	907.72	907.71
----	--	------	--------	--------

Lt

Nov. 4, 1963

Rt

10

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Spike in PP 200'± West of Intersection
O. Rd I" & TH #10

0.7 to				
Sta	PG	PGR	SGR	Elev
BM	0.89	916.87		915.98
8	13.14	3.73	4.43	
+50	12.97	3.90	4.60	
9	12.80	4.07	4.77	
+50	12.63	4.24 4.4 4.7	4.94 (8)	
10	12.46	4.41	5.21 (8.5)	
+50	12.29	4.58	5.48	
T.P.	5.36	914.48	7.75	909.12
11	12.12	2.36	3.26	9.0
			5.40 (9.5)	909.09
+50	11.95	2.53	3.48	
12	11.78	2.70 1.1	3.80	

FK
FS
RB

Nov. 29, 1963 11
Overcast Snow

Top Arrow Point on Hyd S.W. Cor Groveland & "I"

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Top Slope State Lt Sta 20+50

Sta	PG	PGR	1588	Elev
		9/4.48		

22+50	11.61	2.87	4.07	
-------	-------	------	------	--

20	12.46	2.12	2.82	
----	-------	------	------	--

23	11.44	3.04	4.24	
----	-------	------	------	--

20+50	12.29	2.2	3.05	
-------	-------	-----	------	--

+50	11.27	3.21	4.41	
-----	-------	------	------	--

24	11.10	3.38	4.58	
----	-------	------	------	--

+50	10.88	3.60	4.80	
-----	-------	------	------	--

25	10.55	3.93	5.13	
----	-------	------	------	--

+50	10.17	4.31	5.51	
-----	-------	------	------	--

26	9.79	4.7	5.9	
----	------	-----	-----	--

+50	9.41	5.07	6.2	
-----	------	------	-----	--

FK
FS

Dec. 2, 1963
Snowing

12

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914.48

27 09.16 5.32 6.5

+50 09.16

28 09.28

+50 09.40

29 09.53

+50 09.65

30 09.78

+50 09.90

31 10.03

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Top Class 5

Sta	PG	PGR	SGR	Elev
BM	0.20	916.18		915.98
			10.2	
18	13.14	3.02	3.22	
+50	12.97	3.21	3.41	
19	12.80	3.38	3.58	
+50	12.63	3.55	3.75	
			0.3	
20	12.46	3.72	4.02	
			0.35	
+50	12.29	3.89	4.24	
			0.40	
21	12.12	4.06	4.46	
			708 45	909.10
+50	11.95	4.23	4.68	
			1	
22	11.78	4.40	5.0	

FK
TL
FK
HL

June 25, 1964

Hot

14
4'1"

Top Arrow Point on Hyd SW Cor Groveland

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Sta	PG	PGR	1.20.7	
			SGR	
		916.18		
22+50	11.61	4.57	5.27	
T.P.	3.49	914.39	5.28	910.90
23	11.44	2.95	3.65	
+50	11.27	3.12	3.82	
24	11.10	3.29	3.99	
+50	10.88	3.51	4.21	
25	10.55	3.84	4.54	
+50	10.17	4.22	4.92	
26	9.79	4.60	5.30	
+50	9.41	4.98	5.68	
T.P.	6.50	913.43	7.46	906.93

L+

June 25, 1964
 L

R+

15

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Top S. End Culvert sta 26 +20 R+

Sta	PG	PGR	SGR	Elev.	
		913.43			
27	09.16	4.27	4.97		
+50	09.16	4.27	4.97		
28	09.28	4.15	4.85		
+50	09.40	4.03	4.73		
29	09.53	3.90	4.60		
+50	09.65	3.78	4.48		
30	09.78	3.65	4.35		
+50	09.90	3.53	4.23	325 ✓	3.73
31	10.03	3.40	4.10		
TP	4.79	914.13	4.09	909.34	913.14

Lt

£

June 25, 1964

Rt

16

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Sta	PG	PCR	SGR	+0.7
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9/14.13

31+50	10.15	3.98	4.68	
-------	-------	------	------	--

32	10.28	3.85	4.55	
----	-------	------	------	--

+50	10.40	3.73	4.43	
-----	-------	------	------	--

33	10.53	3.60	4.30	
----	-------	------	------	--

+50	10.65	3.48	4.18	
-----	-------	------	------	--

34	10.78	3.35	4.05	
----	-------	------	------	--

+50	10.90	3.23	3.93	
-----	-------	------	------	--

35	11.03	3.10	3.80	
----	-------	------	------	--

TP	4.51	9/14.84	3.80	9/10.33
----	------	---------	------	---------

+50	11.15	3.89	4.39	92 4.89
-----	-------	------	------	------------

Lt

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Rt

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Sta	PG	PGR	SGR	Elev.
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		9/4.84		
--	--	--------	--	--

34	11.28	3.56	4.26	
----	-------	------	------	--

+50	11.32	3.52	4.22	
-----	-------	------	------	--

37	11.21	3.63	4.33	
----	-------	------	------	--

+50	11.01	3.83	4.53	
-----	-------	------	------	--

38	11.0	3.84	4.54	
----	------	------	------	--

Conc	£	3.97	9/10.97	10.93
------	---	------	---------	-------

June 25, 1964

Lt.

L

Rt

18

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Reset Grade Stakes

Sta	+	-	Elev.
BM	1.53	917.53	915.98
		0.2	
18	13.14	4.39	4.59
+50	12.97	4.56	4.76
19	12.80	4.73	4.93
+50	12.63	4.90	5.1
		0.3	
20	12.46	5.07	5.37
		0.35	
+50	12.29	5.24	5.59
		0.4	
21	12.12	5.41	5.81
			5.79
	3.91	915.65	911.74
		0.45	
+50	11.95	3.70	4.15
		0.6	
22	11.78	3.87	4.47

EX
TL
FR
HL

July 1, 1964

19
Ft. T

Lt

Tap Arrow Point on Hwy SW Cor Groveland

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Sta	+	π	$\frac{0.7}{-}$	Elev
-----	---	-------	-----------------	------

915.65

22+50	11.61	4.04	4.74	
-------	-------	------	------	--

23	11.44	4.21	4.91	
----	-------	------	------	--

+50	11.27	4.38	5.08	
-----	-------	------	------	--

24	11.10	4.55	5.25	
----	-------	------	------	--

+50	10.88	4.77	5.47	
-----	-------	------	------	--

25	10.55	5.10		
----	-------	------	--	--

+50	10.17			
-----	-------	--	--	--

26	9.79			
----	------	--	--	--

+50	9.41			
-----	------	--	--	--

July 1, 1964

Lt

L

Rt 20

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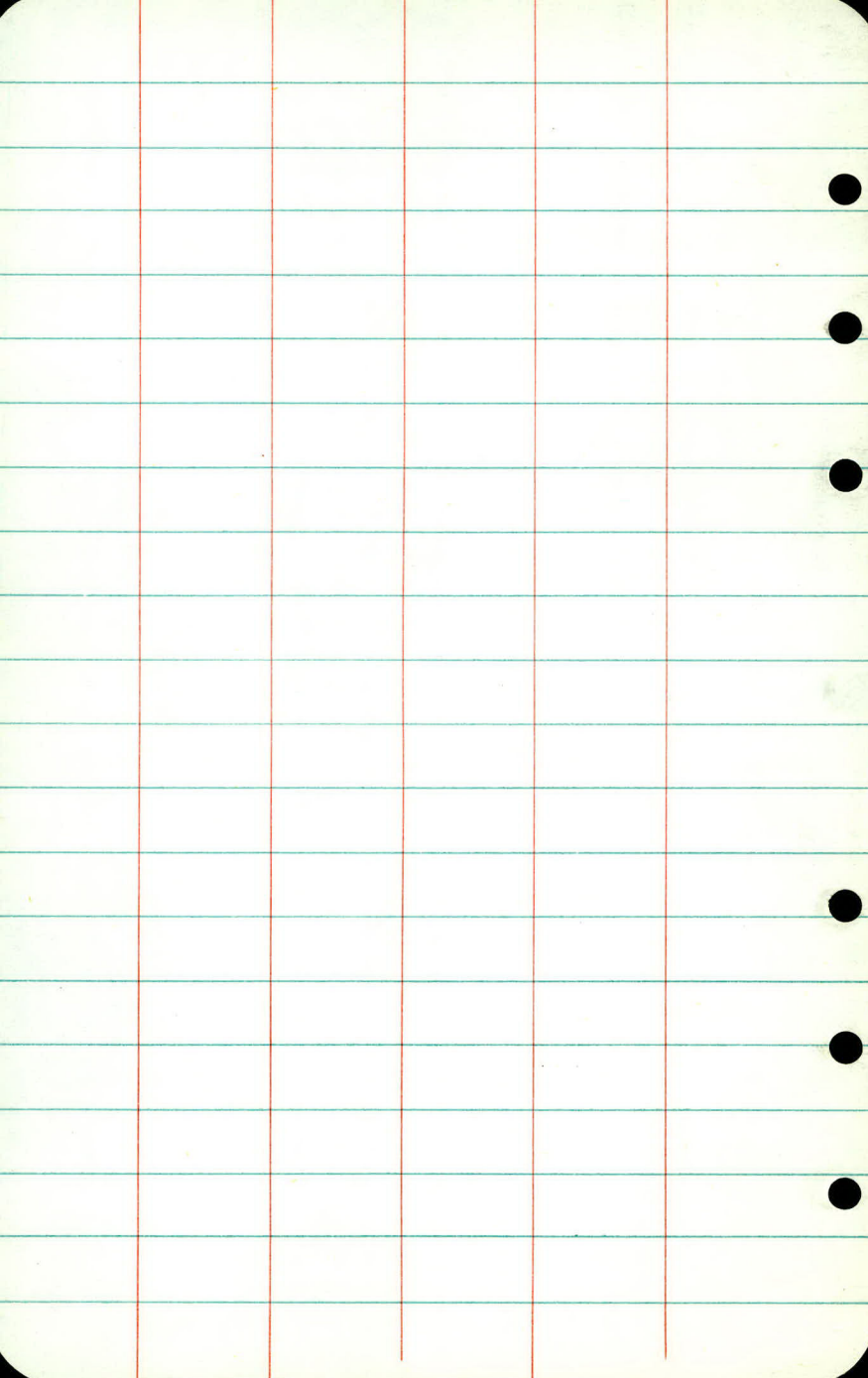
✓

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Co. Rd I

M. H. LOCATIONS

#1
150' E of Eastwood Dr

#2 460± East of #1

0+00 = E Long Lake Road

0+98 #3

Oct 30, 1968

2

7775

Eastwood Dr

Twin 8" Oak

88

34'

39'

167'

Co. Rd I
10' 50' N.H.

Hyd

88.5

127'

Hyd

Line
P.P.
P.P.

Sta

M.H.No.

15+96

6

10+96

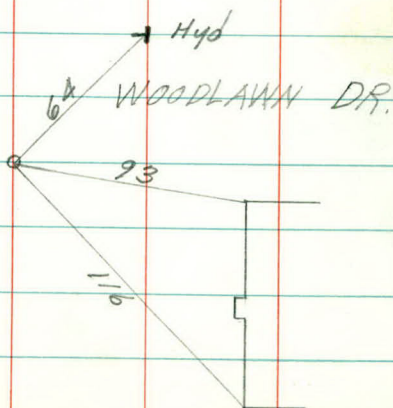
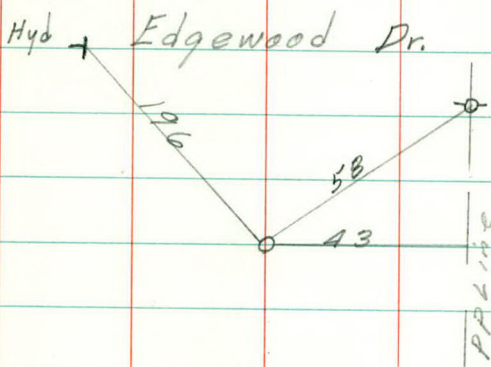
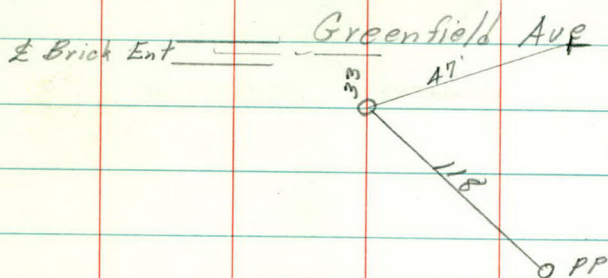
5

5+97

4

Oct. 30, 1962

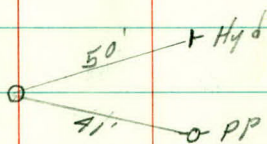
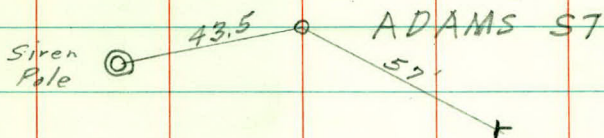
3



Sta	M.H. No.
30+92	#9
26+05	#8
20+96	#7

Oct. 30, 1962

4



20" Cott.



Sta M.H. No.

130

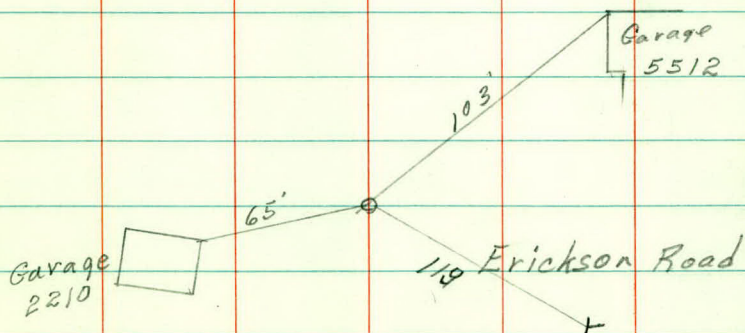
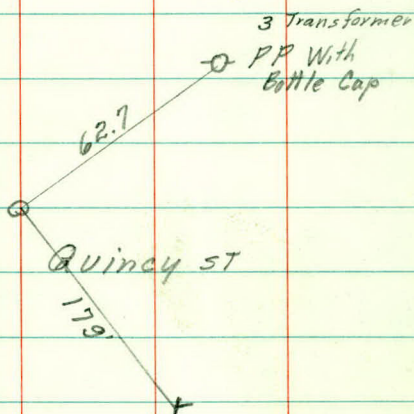
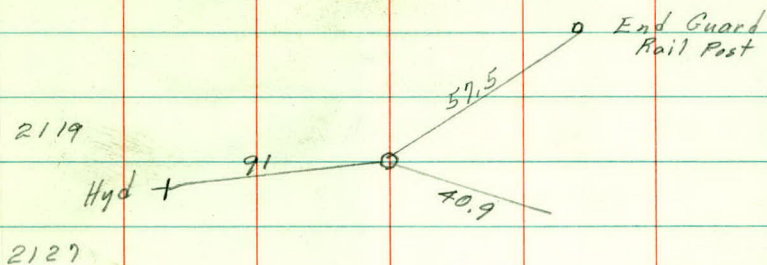
45+97 #12

40+98 #11

35+97 #10

Oct. 30, 1962

5



Sta M.H. No.

West Edge of Conc T.H. #8

50+83 #13

47+27 Storm Sewer M.H.

