

BK. 25 Dr. 13

OFFICE OF COUNTY ENGINEER
RAMSEY CO. MINN.

Plan Survey

Eighth St.

From 3rd Ave. To First Ave.

Also Curb & Slope stakes

Road Acc't. No.

Date Filed 7-25-47 File

Also New Align. June 1949

PLAN SURVEY

EIGHTH ST.

Third Ave to First Ave
First Ave. to Third Ave.

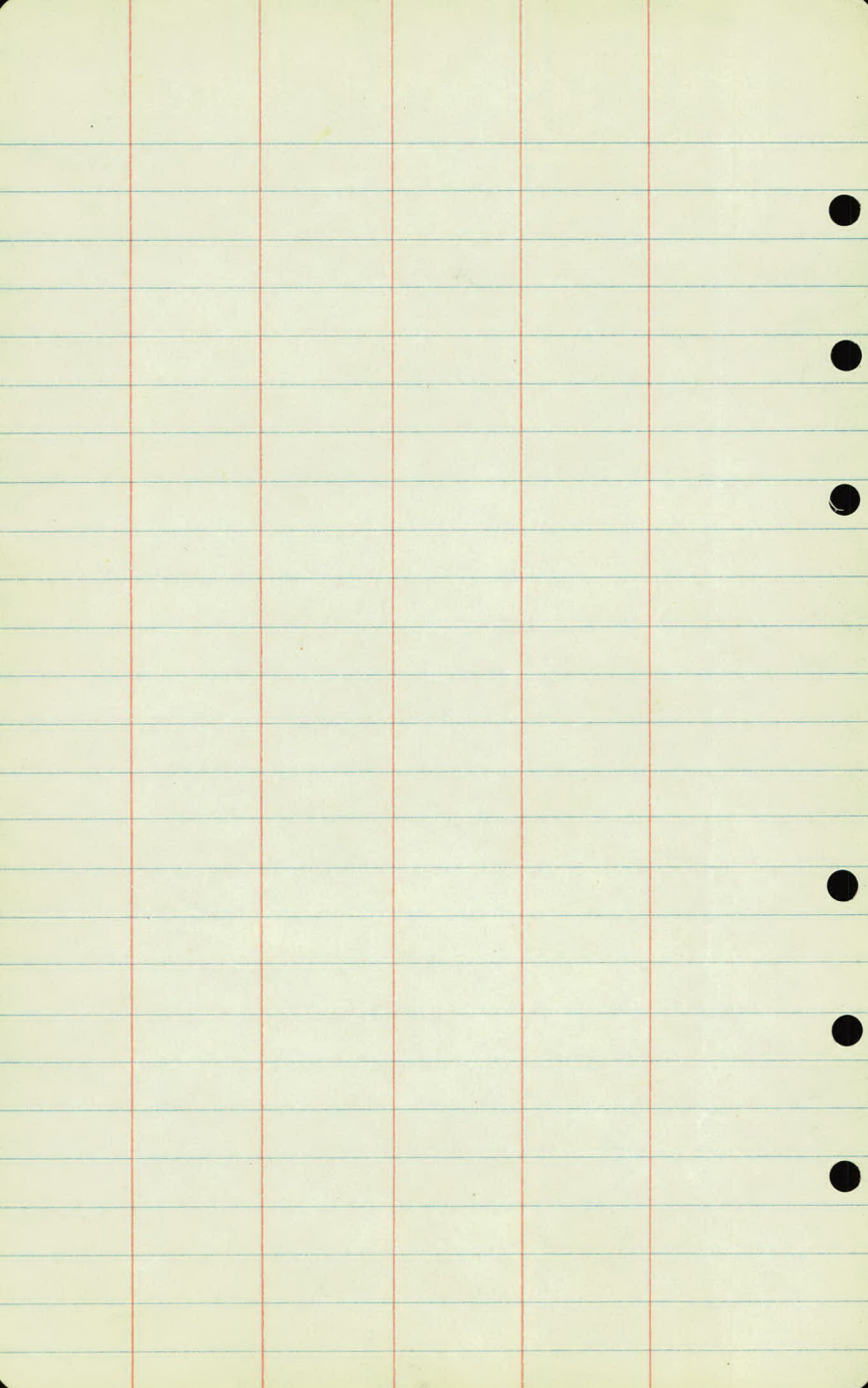
Village of New Brighton

(Grading)

Rev'd 3/25/47 WJB
Drawn up
4/22/47
L.P.C.
L.C.

INDEX

Align 1-2
Topog. 3-5
X Sections 6-10



Alignment.

Sta Point Δ Lt. Δ Pt

6 + 5085 = $\&$ 1st Ave.

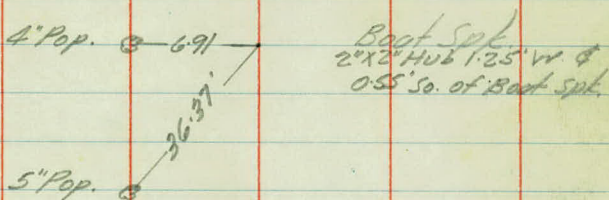
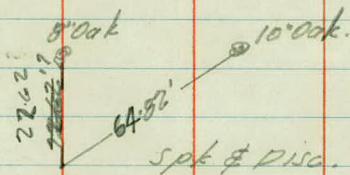
3 + 2763 P.O.T. = $\&$ 2nd Ave.

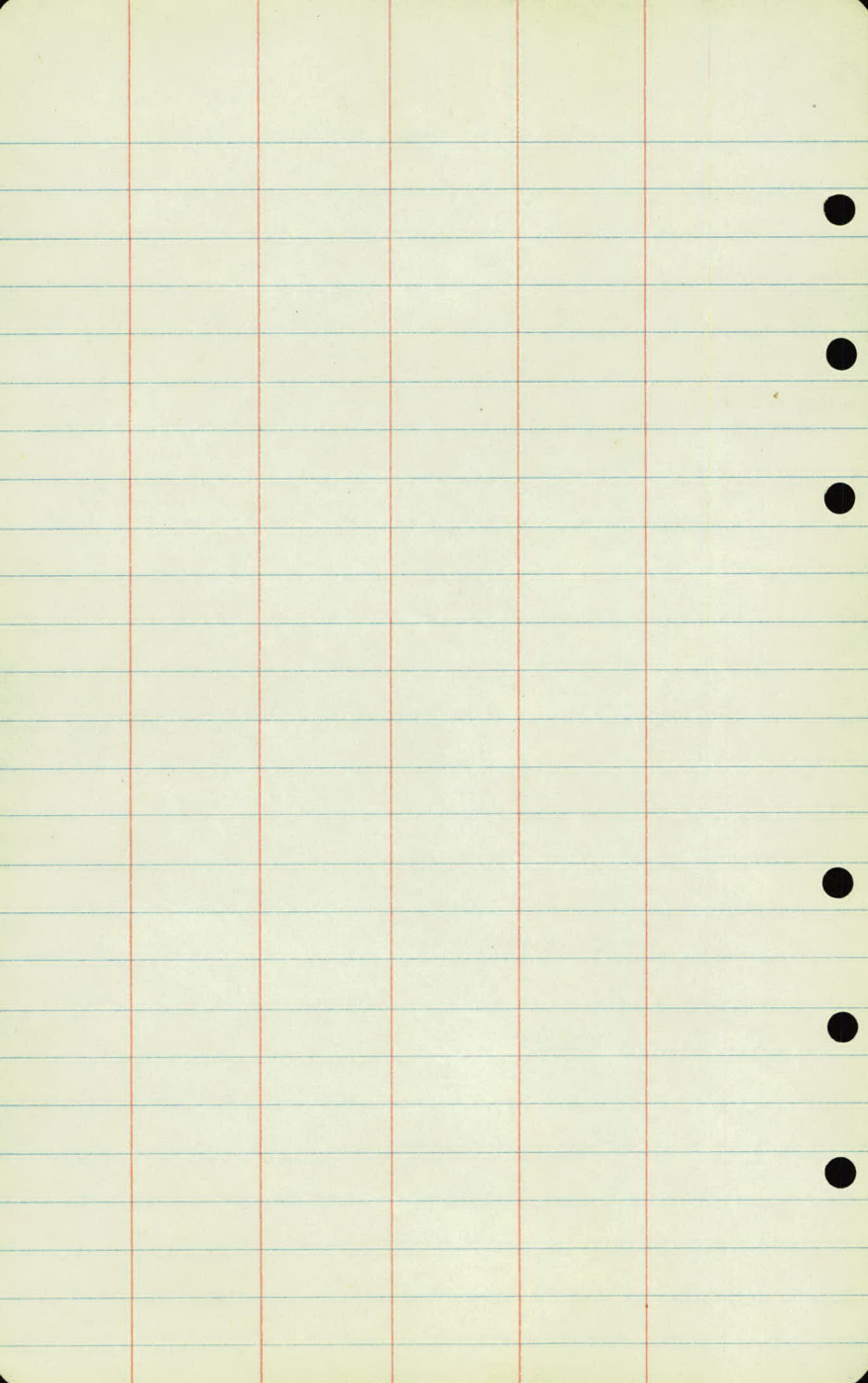
0 + 100 = $\&$ 3rd Ave.

L.A.
AM
M.B.
B.K.

3-24-41 Strong Winds

2





Topography

5

+08-NW Cor. Ho.-49'

+81 } Clothes Poles -32'-41'
+57 } 29'-39'

+53-NW Cor. Ho.-51'

4

Ent-37'

+26-6" Pop-7'
+24-6" Pop-9'
+05-4" Pop-16'
+01-2-9" Pop-15'

+44-6 Ent-30'
+45-End 18" C.M.-46'
50' = +36'
50' = +19'
+09-End 18" C.M.-46'
18'

3

3'

+95-4" Pop-15'
+73-4" Pop-16'
+71-10" Pop-16'

+80 = 6' 10'

+50 = 8' 7'

2

9' 8'

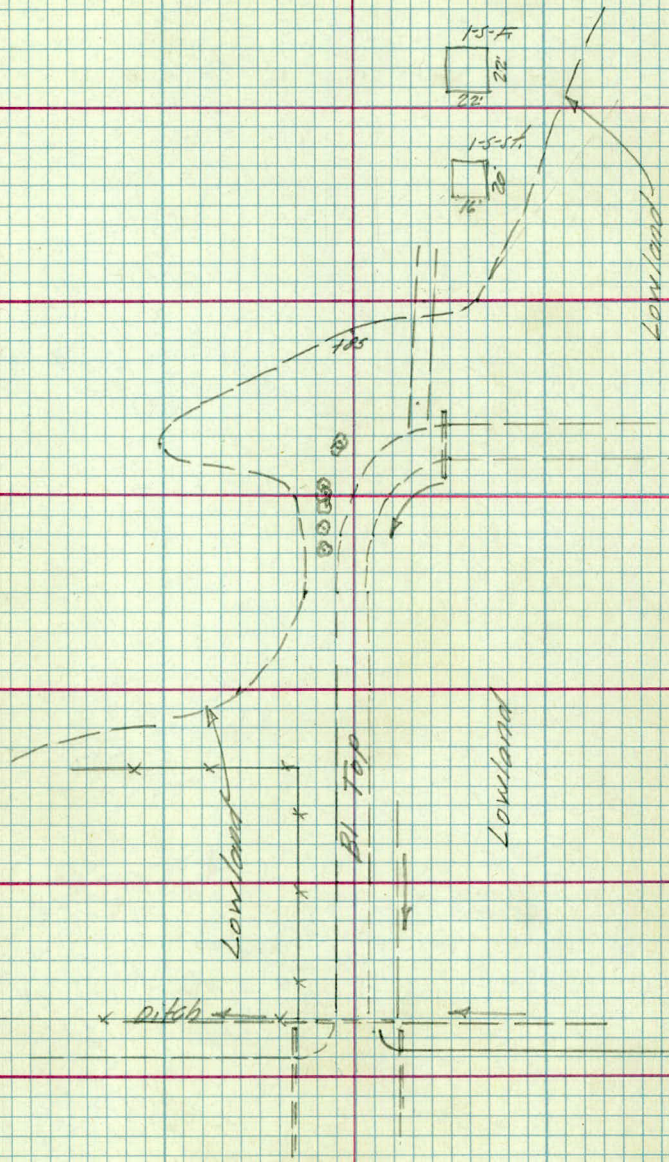
+60-Fc Cor-30'

1

9' 8'

+30-Fc Cor-30' +33-Rd-10'-7'
+28-18" C.M. Drain 20-20' +24-End 18" C.M.-24'
+25-End 18" C.M.-32' +10-32'
+23-End Curb-13'

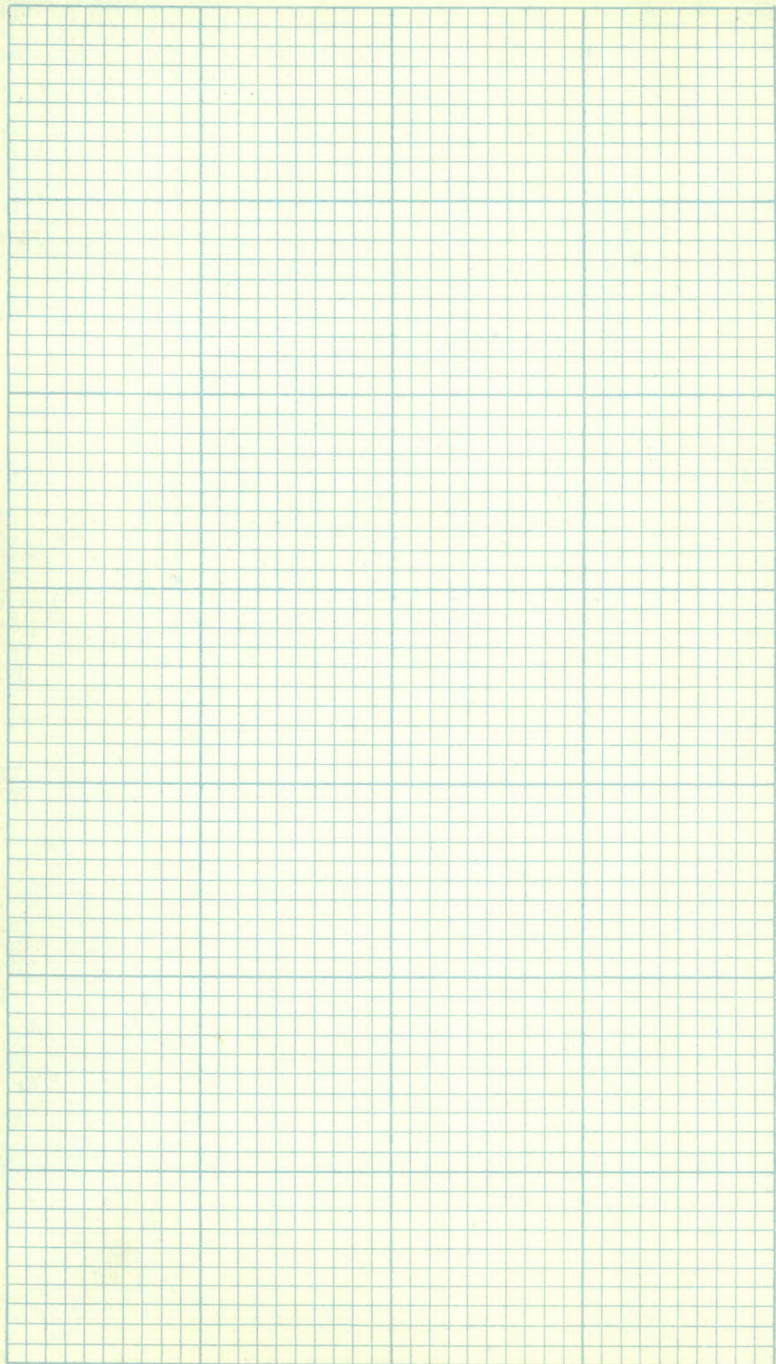
0



145- E Trail

6 110-6" Tw. Oak-25'

6" wide



X Sections

Sta	+	π	-	Elev.
B.M.	2.75	885.12		882.37

0 +00				81.2
-------	--	--	--	------

+13				81.0
-----	--	--	--	------

+23				80.6
-----	--	--	--	------

+24 - FL 18" CM.				
------------------	--	--	--	--

+25 FL 18" CM.				
----------------	--	--	--	--

+28				80.7
-----	--	--	--	------

+30				80.7
-----	--	--	--	------

+40				80.8
-----	--	--	--	------

K.A. 3-24-47 Strong Winds
A.M.
M.B.
R.K.

1

L E R
Spe in P.P.S.V. 8th St. + 3rd Ave.

46 46 39 40 38 ✓
50 34 27 50

48 46 49 45 41 42 44 44 ✓ 417 3.94
50 27 23 12 14 24 50 23-50
(Curbs)

55 48 52 48 45 47 42 43 8.1 66 ✓
50 19 14 9 13 13 18 24 50
(Curbs)

8.1
24

865
32'

9.7 91 835 49 49 45 44 47 48 55 802 78 44 52 58 ✓
100 50 20 15 12 6 9 12 17 20 25 29 42 50
FL. FL.

60 58 47 48 44 47 46 58 7.7 46 55 ✓
50 18 14 11 8 16 20 23-25 30 50

6.2 6.1 6.1 4.9 4.4 4.3 4.6 5.7 6.0 8.2 50 56 ✓
50 30 16 13 7 14 18 20 23-25 29 50

Sta	+	π	-	Elck
		885.12		
1				80.3
	+60			80.2
2				80.5
	+50			80.7
3				81.0
T.P.	530	886.04	4.35	880.74
	+02			81.0
	+05			81.0

+09 FL. 18" GM.

L E F ✓
 6.0 6.1 6.5 5.5 5.1 4.8 4.8 5.2 6.1 6.3 8.0 8.0 5.8 6.0
 50 28 16 14 11 5 13 16 20 23-25 28 50

6.0 6.1 6.1 50 49 49 5.1 6.1 6.6 7.7 6.5 6.3 ✓
 50 28 16 11 7 12 17 23 24-25 26 50

5.5 5.7 5.6 5.9 5.0 4.7 4.6 4.7 5.0 5.9 6.4 7.4 6.2 6.2 ✓
 50 30 20 17 13 9 5 11 16 22 23-25 27 50

4.7 5.4 5.3 4.6 4.4 4.6 5.6 6.0 6.8 5.7 5.7 ✓
 50-36 28 15 11 10 16 21 24-25 28 50

4.5 5.5 5.7 4.1 4.1 4.1 4.6 5.1 5.2 7.1 5.3 5.5 ✓
 50 30 15 9 4 11 14 21 23-25 29 50
 Top Boot Spk.

5.5 6.0 6.3 6.8 6.4 5.1 5.0 5.1 6.0 6.5 7.7 7.9 ✓
 50 30 18 14 8 7 18 25 27 50

5.5 6.3 6.8 6.4 5.1 5.0 5.1 5.8 6.3 6.4 8.0 6.6 ✓
 50 30 18 14 8 8 20 26 48 46-47 50

7.97

46

Sta.	+	π	-	Elev.
		886.04		
3	+19			81.0
	+27.63 = 2 nd Ave.			80.8
	+37			79.3
	+45			79.4
	+75			79.6
4				82.4
T.P.	12.52	896.05	2.51	883.53
	+30			86.4
	+95			91.8
5				92.4

L

E

R

63 65 68 64 54 50 51 53 55 ✓
50 41 22 12 8 15 27 50

65 69 63 55 52 51 51 52 50 ✓
50 30 8 4 12 34 50 100

66 68 67 63 55 52 54 ✓
50 25 4 14 25 50

67 68 66 63 53 51 80 798 ✓
50 29 25 26 96 47 ~~46~~ 498
CFL

67 55 64 65 66 51 50 ✓
50 29 11 28 30 50

23 28 36 49 55 47 45 ✓
50 29 12 27 30 50

66 82 97 ~~46~~ 115 136 131 130 ✓
50 25 22 25 41 50

02 22 43 67 110 112 104 ✓
50 29 25 30 41 50

103 1.7
50 26

37 60 76 75 ✓
25 29 50

Sta	+	π	-	Elev.
		896.05		
5	+50			(97.6)
T.P.	11.21	905.72	1.54	894.51

5	+50			97.6
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6				02.4
---	--	--	--	------

+08				02.9
-----	--	--	--	------

+14				03.7
-----	--	--	--	------

+20				00.9
-----	--	--	--	------

+31				97.6
-----	--	--	--	------

+5005 & 1 st Ave.				97.4
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B.M.		7.46	898.26	(898.24)
------	--	------	--------	----------

L

E

R

+1.5

-3.4 -7.4 -7.6

19.5.9 61
27 31 50

33 56 81 ✓
50 25

+05 1.2 33 64 76 105 110 ✓
50 22 28 33 37 50

+14 0.3 2.8 4.8 6.3 10.1 107 ✓
50 27 22 31 36 50

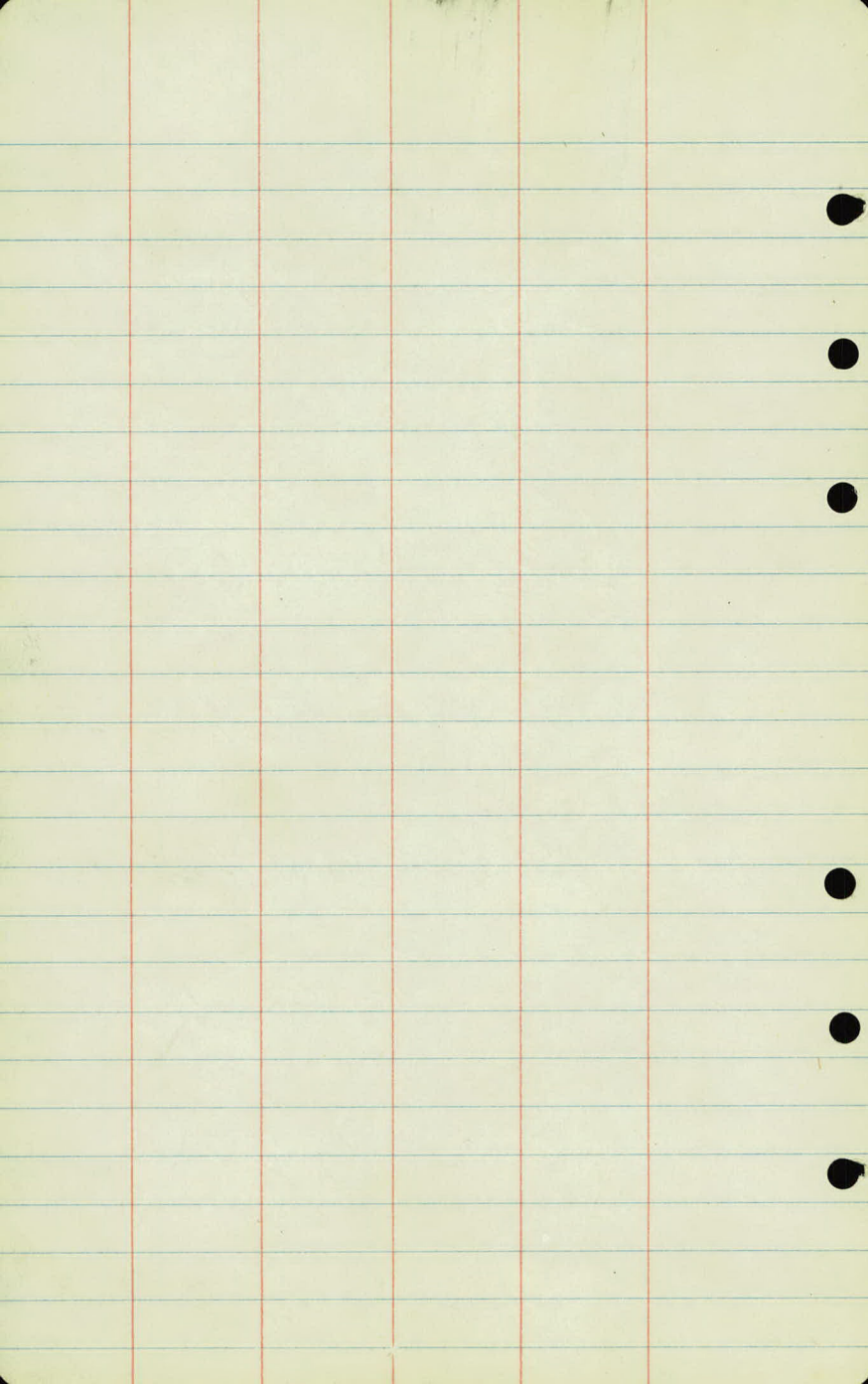
47 2.6 2.0 5.4 6.4 9.7 10.3 ✓
50 21 27 31 35 50

77 7.9 48 3.8 5.9 10.2 100 ✓
50 28 23 30 36 50

81 8.7 8.1 9.0 9.8 ✓
50 28 27 50

80 8.2 8.3 9.3 9.9 ✓
50 29 24 50

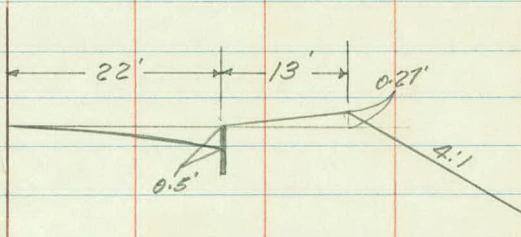
Spt in 8" Oak 125.50. E 31' E of 1st Ave. + 8th St



New Brighton

8th ST.

slope stakes



Sta	+	π	-	Grade
B.M.	0.15	896.57		(896.42)

0	+50			94.06
---	-----	--	--	-------

T.P.	1.17	889.03	8.71	887.86
------	------	--------	------	--------

	+60			93.62 4.9 ✓
--	-----	--	--	-------------

	+75			92.94
--	-----	--	--	-------

1				91.82 6.7 ✓
---	--	--	--	-------------

	+21			90.88
--	-----	--	--	-------

	+35			90.26
--	-----	--	--	-------

	+50			89.58 8.9 ✓
--	-----	--	--	-------------

	+70			88.69
--	-----	--	--	-------

6-6-46
K.A.
P.M.
M.B.
C.F.

2

Cor Rod Lt. E Bl

Spk in RR S.W. Cor 8th + 5th Ave.

$$\begin{array}{r} 251 \\ - 2 \\ \hline 252 \end{array}$$

$$\begin{array}{r} 670/102 \\ - 8.0 \end{array}$$

$$\begin{array}{r} + 4.6 \\ - 1.3 \\ \hline \end{array} - 4.9$$

$$\begin{array}{r} 83.0/71 \\ - 12.0 \end{array}$$

$$\begin{array}{r} 8.71 \\ 132 \\ 9049 \\ 7.3 \\ \hline 89.03 \end{array}$$

$$\begin{array}{r} 13.9 \\ - 2 \\ \hline \end{array} 4.2$$

$$\begin{array}{r} 28 \\ - 3 \\ \hline \end{array} - 3.1$$

$$\begin{array}{r} 81.6/23 \\ - 11.4 \end{array}$$

$$\begin{array}{r} 1.83 \\ - 2.1 \\ \hline \end{array}$$

$$\begin{array}{r} 123 \\ - 27 \\ \hline \end{array} + 1.5$$

$$\begin{array}{r} 25.4 \\ - 27 \\ \hline \end{array} - 0.8$$

$$\begin{array}{r} 73.0/87 \\ - 9.5 \end{array}$$

Sta	+	π	-	Grade
		989.03		
1	+80			88.24
2				87.34 11.2 ✓
	+50			85.32 13.2 ✓
3				83.79 5.8 ✓
	+34.46			82.82
	+54			82.56 67.0 ✓
4				81.95 7.6 ✓
T.P.	4.46	885.97	7.52	881.51
	+50			81.50 8.1

Gr Bod

lt

z

pt.

$$\begin{array}{r} 1.7 \\ - .3 \\ \hline \end{array} = 1.4$$

$$\begin{array}{r} 65.9 \\ - 7.7 \\ \hline \end{array}$$

$$\begin{array}{r} 3.7 \\ - .3 \\ \hline \end{array} = 3.4$$

$$\begin{array}{r} 68.4 \\ - 5.2 \\ \hline \end{array}$$

$$\begin{array}{r} 52.4 \\ - .2 \\ \hline \end{array} = 5.0$$

$$\begin{array}{r} 51.0 \\ - 4.0 \\ \hline \end{array}$$

$$\begin{array}{r} 6.21 \\ - .2 \\ \hline \end{array} = 5.9$$

$$\begin{array}{r} 47.0 \\ - 8.9 \\ \hline \end{array}$$

$$\begin{array}{r} 6.47 \\ - .2 \\ \hline \end{array} = 6.2$$

$$\begin{array}{r} 48.2 \\ - 9.5 \\ \hline \end{array}$$

$$\begin{array}{r} 70.8 \\ - 1.7 \\ \hline \end{array} = 6.8$$

$$\begin{array}{r} 45.4 \\ - 9.4 \\ \hline \end{array}$$

$$\begin{array}{r} 4.47 \\ - .2 \\ \hline \end{array} = 4.2$$

$$\begin{array}{r} 44.6 \\ - 2.4 \\ \hline \end{array}$$

Sta	+	π	-	Grade
		885.97		
5				81.31 8.3 ✓
	+50			81.12 8.5 ✓
6				80.93 8.7 ✓
	+26.18			80.82 8.8
	+39.18			80.73
B.M.		3.62	882.35	882.37

Gr. Rod

Lt

E

Et

$$\begin{array}{r} 4.65 \\ - .27 \\ \hline \end{array}$$

44

$$\begin{array}{r} 43.4/6.5 \\ -2.1 \\ \hline \end{array}$$

$$\begin{array}{r} 4.85 \\ - .21 \\ \hline \end{array}$$

45

$$\begin{array}{r} 43.0/6.5 \\ -2.0 \\ \hline \end{array}$$

$$\begin{array}{r} 5.04 \\ - .21 \\ \hline \end{array}$$

48

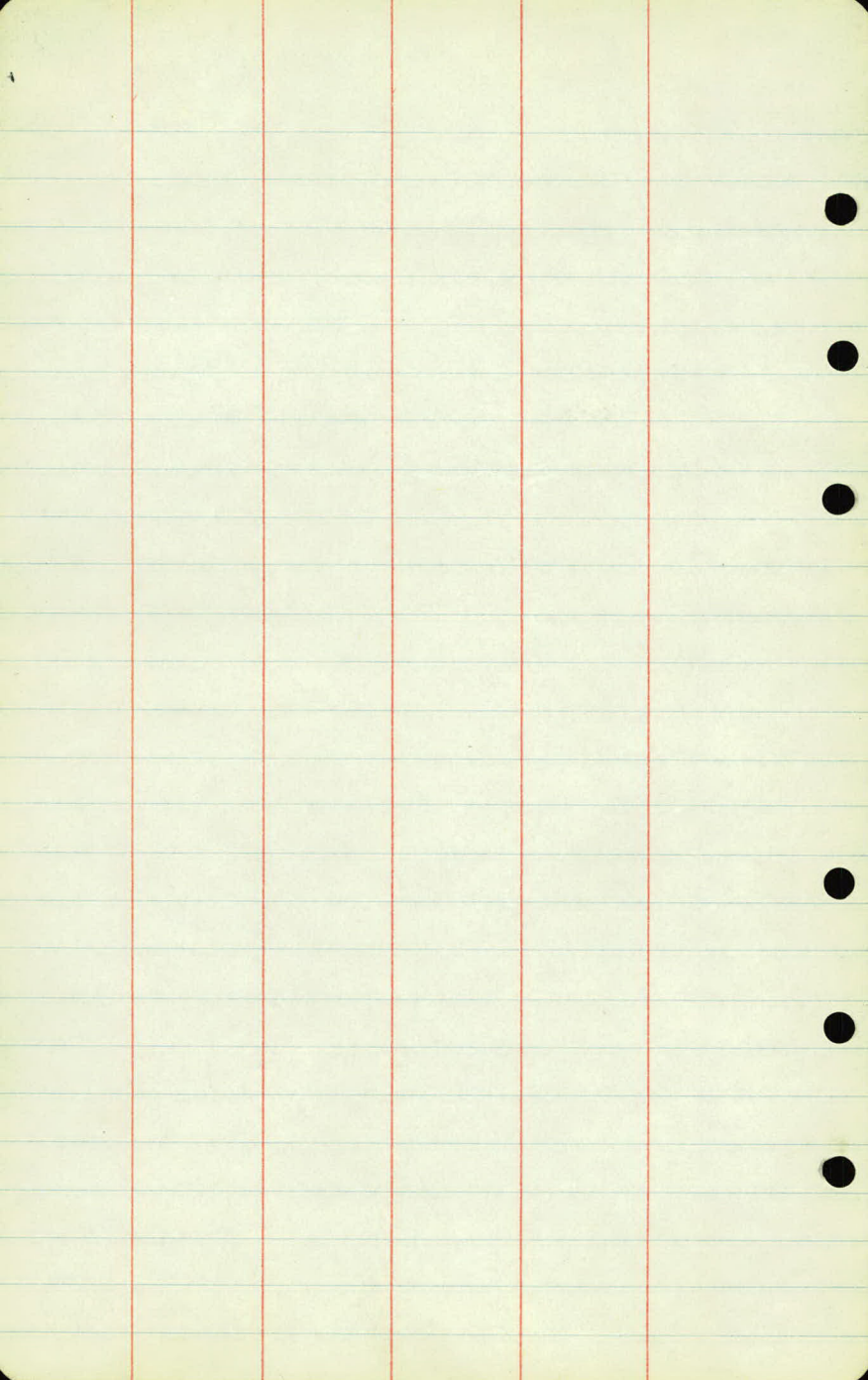
$$\begin{array}{r} 41.0/6.5 \\ -1.5 \\ \hline \end{array}$$

$$\begin{array}{r} 5.15 \\ - .21 \\ \hline \end{array}$$

49

$$\begin{array}{r} 41.0/6.4 \\ -1.5 \\ \hline \end{array}$$

sph. in P.P. of 3rd + 8th st.



8th St.
New Brighton

curb stakes

curb 20' lt. of E.
stakes set 4' o.s.

Rec. in office
1-3-47

Sto.	PG	PER	
B.M.	2.16	898.58	896.42

0	+38.2	94.53	4.20 ✓
---	-------	------------------	--------

+50	94.06	4.52 ✓
-----	-------	--------

+75	92.94	5.64 ✓
-----	-------	--------

1	91.82	6.76 ✓
---	-------	--------

+25	90.70	7.88 ✓
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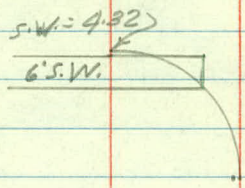
+50	89.58	9.0 ✓
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+75	88.46	10.12 ✓
-----	-------	---------

2

L E R

Spt. in P.P. S.W. cor. 8th St & 5th Ave.



4.48
 11.8
 3584
 448
 448
 52864

sta	PG	PCR
		89858

2	87.34	11.24 ✓
---	-------	---------

+25	86.28	12.30 ✓
-----	-------	---------

+50	85.32	13.26 ✓
-----	-------	---------

T.P.	1.06	886.37	13.27	885.31
------	------	--------	-------	--------

+75	84.48	1.89 ✓
-----	-------	--------

3	83.76	2.61 ✓
---	-------	--------

+25	83.13	3.24 ✓
-----	-------	--------

+50	82.02	3.75 ✓
-----	-------	--------

+75	82.24	4.13 ✓
-----	-------	--------

L

E

R

2102
87.27

 87.57

5'0.5.
 ————
 2'0.5.
 ————
 4
 ————

4'05.5.
 ————

Sto.	PG	PCR
		886.37

4	81.95	4.42 ✓
---	-------	--------

+25	81.72	4.65 ✓
-----	-------	--------

+50	81.50	4.87 ✓
-----	-------	--------

+75	81.40	4.97 ✓
-----	-------	--------

5	81.31	5.06 ✓
---	-------	--------

+25	81.21	5.16 ✓
-----	-------	--------

+50	81.12	5.25 ✓
-----	-------	--------

+75	81.02	5.35 ✓
-----	-------	--------

4

L

E

F

4

$$\begin{array}{r} 2 \frac{1}{2} \\ 1 \frac{3}{4} \\ \hline \end{array}$$

$$\begin{array}{r} 4.77 \\ 23 \\ \hline \end{array}$$

Alley

$$\begin{array}{r} 4.85 \\ 23 \\ \hline \end{array}$$

$$107 = \frac{509}{13}$$

sto.

PG

PCR

886.37

6

80.93

544 ✓

+2218 80.85

5.52 ✓

B.M.

4.01 88236

(882.37)

L

E

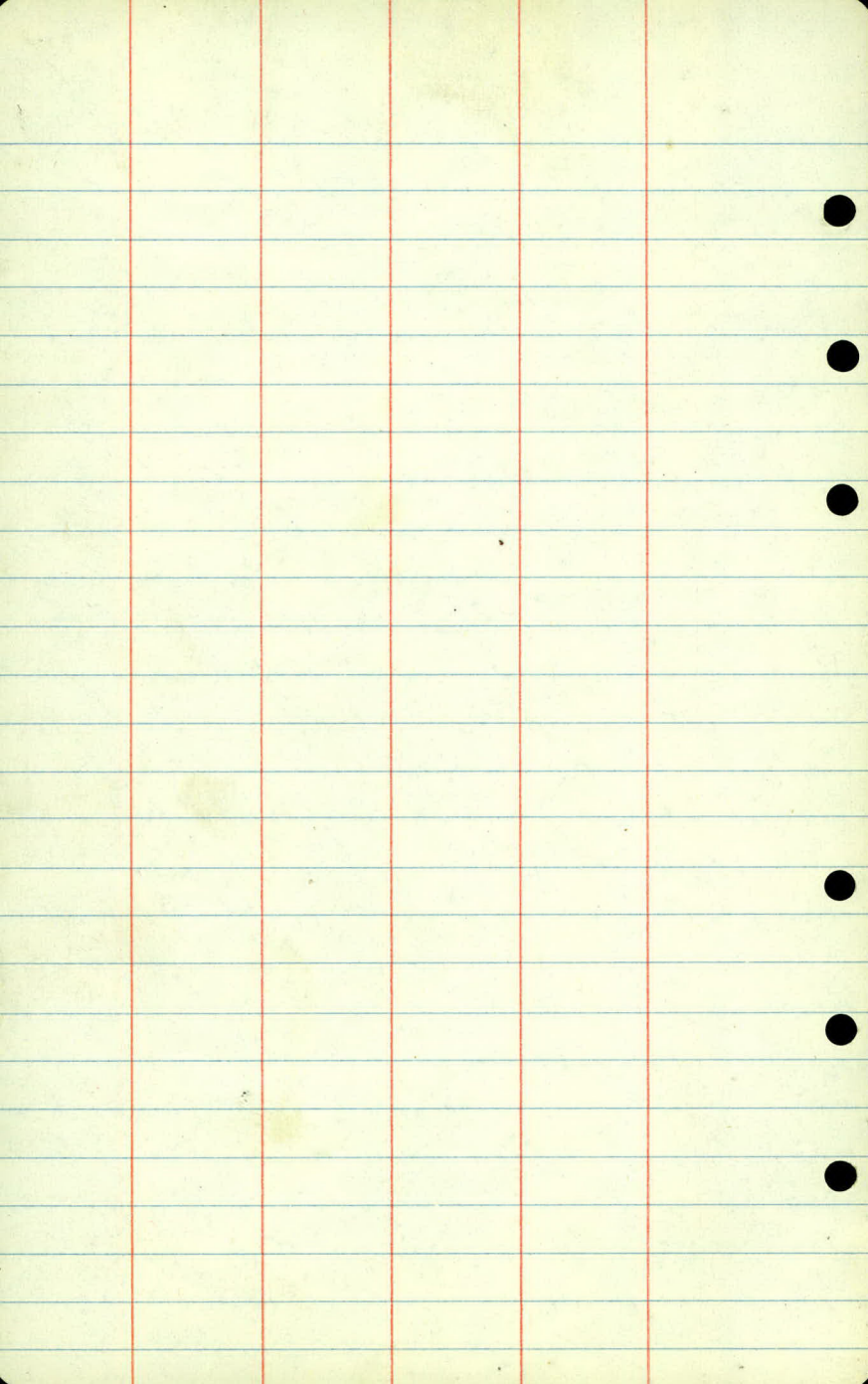
R

560

567

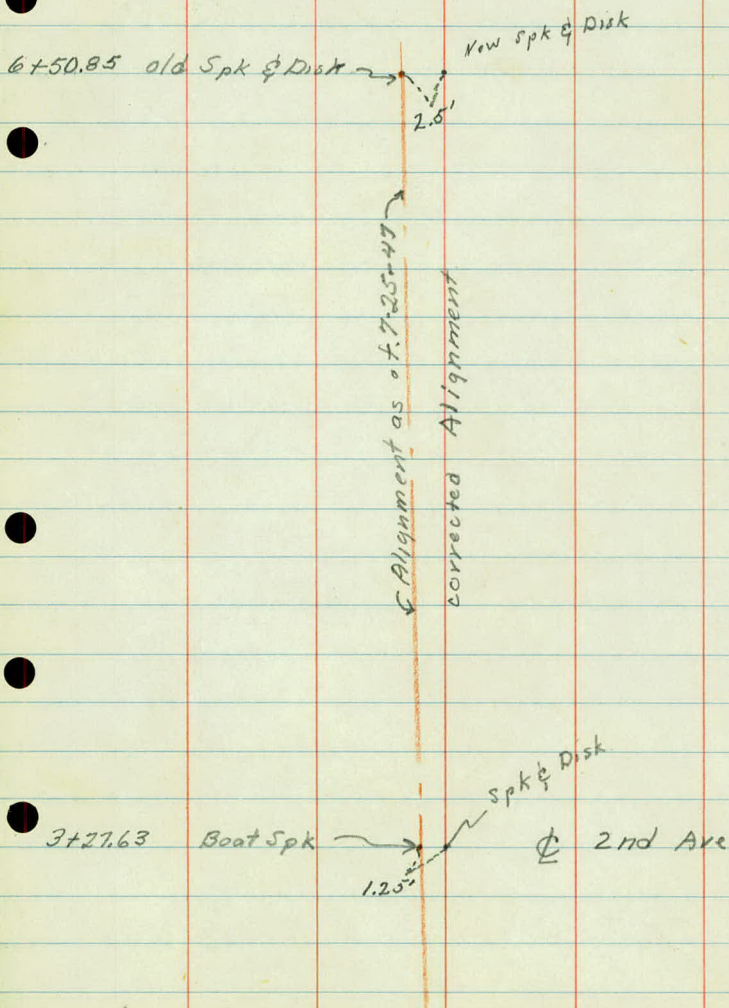
535
 +30-Beg old curb 13'

Spk. in P.P. SW. cor. 8th + 3rd Ave.



File with Dr. 13 BK, 25

Eight St
1st to 2nd Ave East.
X Sections
on New Alignment



Sta	+	π	-	Elev
-----	---	-------	---	------

B M	6.43	888.80		882.37
-----	------	--------	--	--------

3+27.63		¢ 2nd Ave		
---------	--	-----------	--	--

+ 37				79.1
------	--	--	--	------

+ 45				79.0
------	--	--	--	------

2' Bottom ditch Rt. 

+ 75				79.4
------	--	--	--	------

4				82.1
---	--	--	--	------

+ 50				85.9
------	--	--	--	------

T.P.	13.44	901.67	0.57	888.23
------	-------	--------	------	--------

6-20-49

G.B.
A.M.
M.B.
B.C.

Lt

E

Rt

Spk in PP S.W. Cor 8th & 3rd Ave

E. cont.

$$\frac{9.8}{50}$$

$$\frac{9.8}{25}$$

$$9.7$$

$$\frac{8.4}{12}$$

$$\frac{8.3}{22}$$

$$\frac{8.5}{33}$$

$$\frac{8.6}{50}$$

✓

$$\frac{9.9}{50} \quad \frac{9.8}{25}$$

$$9.8$$

$$\frac{9.5}{24}$$

$$\frac{8.4}{25}$$

$$\frac{8.6}{34}$$

$$\frac{8.4}{43}$$

$$\frac{11.02}{47}$$

$$\frac{10.2}{49}$$

$$\frac{8.4}{50}$$

$$\frac{8.5}{27}$$

$$9.4$$

$$\frac{9.6}{13}$$

$$\frac{9.5}{25}$$

$$\frac{8.3}{28}$$

$$\frac{8.2}{50}$$

$$\frac{5.4}{50}$$

$$\frac{5.7}{25}$$

$$\frac{6.7}{7}$$

$$\frac{7.2}{15}$$

$$\frac{8.3}{25}$$

$$\frac{8.7}{28}$$

$$\frac{7.9}{50}$$

$$\frac{7.7}{50}$$

Cor Ho

$$\frac{1.0}{50}$$

$$\frac{1.1}{26}$$

$$2.9$$

$$\frac{3.8}{16}$$

$$\frac{6.3}{23}$$

$$\frac{5.9}{48}$$

Sta	+	π	-	Elev
		901.61		
4	+95			91.3
5				92.2
	+40			96.0
	+61			98.6
	+68			99.2
T.P.	5.81	905.07	1.44	899.23
B.M.			6.89	898.15
	+95			01.4
6				01.9

898.24

Lt

Q

Rt

$$\frac{6.3}{50}$$

$$\frac{8.5}{24}$$

$$10.4$$

$$\frac{11.9}{18.5}$$

$$\frac{16.7}{24.5}$$

$$\frac{17.2}{50}$$

✓

$$\frac{8.1}{18}$$

$$\frac{5.6}{50}$$

$$9.5$$

$$\frac{11.8}{18}$$

$$\frac{12.9}{24}$$

$$\frac{12.1}{40}$$

$$\frac{12.0}{50}$$

✓

$$\frac{0.6}{50}$$

$$\frac{2.8}{25}$$

$$5.7$$

$$\frac{7.4}{16}$$

$$\frac{11.4}{23}$$

$$\frac{11.8}{46.5}$$

✓

HO.

$$\frac{+0.9}{50}$$

$$\frac{1.1}{23}$$

$$3.1$$

$$\frac{4.8}{14}$$

$$\frac{10.6}{24}$$

$$\frac{11.1}{50}$$

✓

$$+1.0$$

$$\frac{0.5}{25}$$

$$2.5$$

$$\frac{4.5}{16}$$

$$\frac{9.9}{23}$$

$$\frac{10.6}{27}$$

$$\frac{8.4}{31}$$

$$\frac{8.6}{50}$$

✓

$$\frac{+0.9}{50}$$

$$\frac{1.2}{26}$$

$$3.6$$

$$\frac{6.2}{26}$$

$$\frac{10.8}{32}$$

$$\frac{11.0}{50}$$

✓

✓

$$\frac{+3.9}{50}$$

$$\frac{+2.6}{25}$$

$$3.1$$

$$\frac{5.7}{25}$$

$$\frac{10.5}{32}$$

$$\frac{11.0}{50}$$

Sta	+	π	-	Elev
-----	---	-------	---	------

905.04

6 +08

02.7

+14

03.3

+20

00.7

+31

96.9

+50.85

96.6

L+

C

R+

$$\frac{1.7}{50} + \frac{0.4}{23}$$

$$2.3$$

$$\frac{4.9}{25}$$

$$\frac{10.6}{33}$$

$$\frac{10.7}{50}$$

✓

$$+ \frac{0.2}{50} \quad \frac{1.7}{22}$$

$$1.7$$

$$\frac{4.6}{24}$$

$$\frac{10.6}{33}$$

$$\frac{10.6}{50}$$

✓

$$\frac{7.3}{50}$$

$$\frac{7.3}{36}$$

$$\frac{4.7}{18}$$

$$4.3$$

$$\frac{4.1}{24}$$

$$\frac{10.1}{25}$$

$$\frac{10.1}{50}$$

✓

$$\frac{8.4}{50}$$

$$\frac{8.2}{20}$$

$$8.1$$

$$\frac{8.7}{31}$$

$$\frac{10.2}{38}$$

$$\frac{10.2}{50}$$

✓

$$\frac{7.7}{50}$$

$$\frac{8.0}{50}$$

$$8.4$$

$$\frac{9.6}{50}$$

$$\frac{11.2}{100}$$

✓

Sta

+

π

-

Elev