

BK. 23 Dr. 13

OFFICE OF COUNTY ENGINEER
RAMSEY CO. MINN.

47 N.B.2

Plan.....Survey

Eighth St.

From Long Lake Rd. To 6th Ave.

Road Acc't. No.....

Date Filed 7-25-47

File.....

PLAN SURVEY

EIGHTH ST.

Long Lake Rd. to 6th Ave.

Village of New Brighton

INDEX

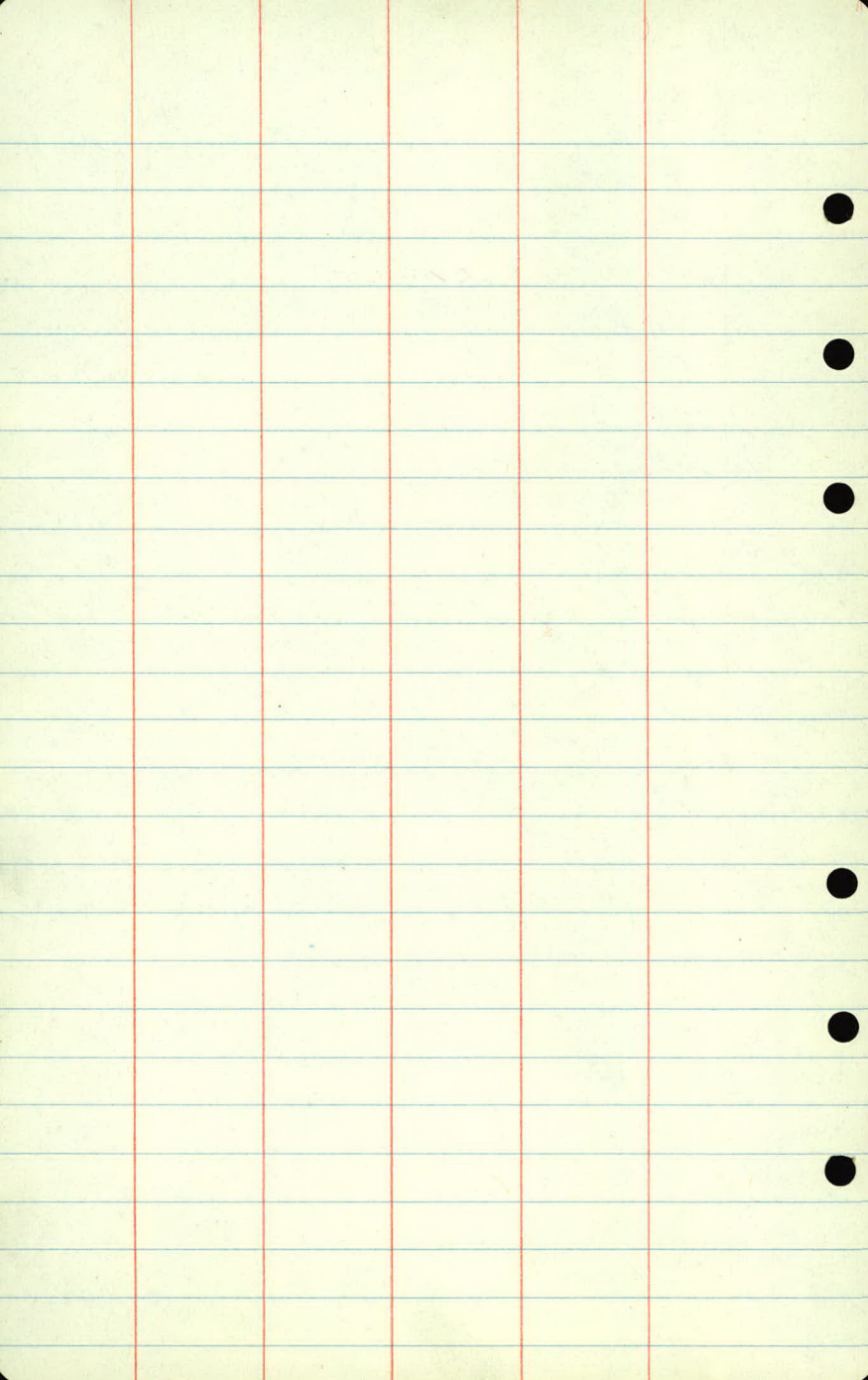
Align P. 1-2

Topog. P. 3-5

X Sections P. 6-12

Rec'd 6/1/47

Worked 90 6/10/47



1

Alignment

Sta Point

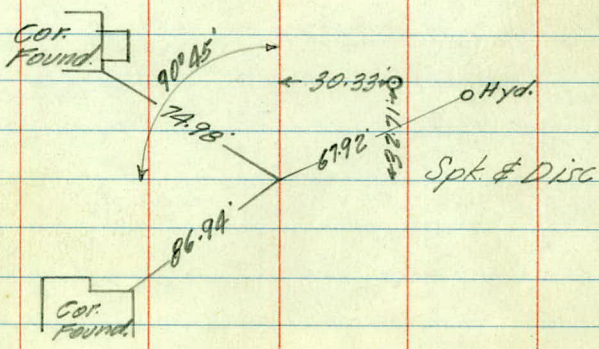
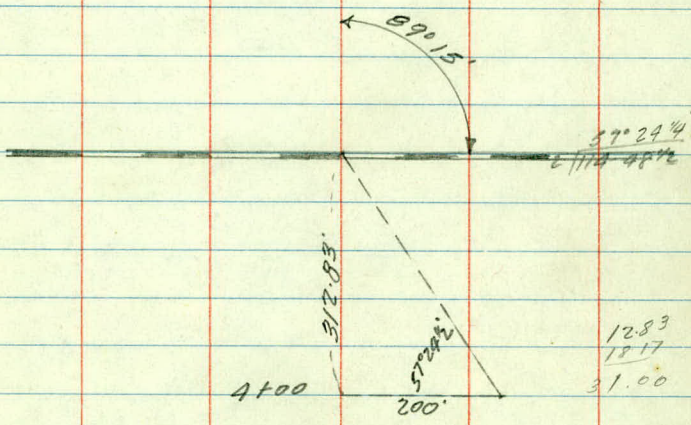
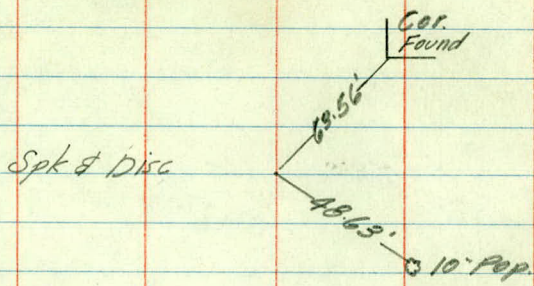
9 + 91.16 @ 6th Ave.

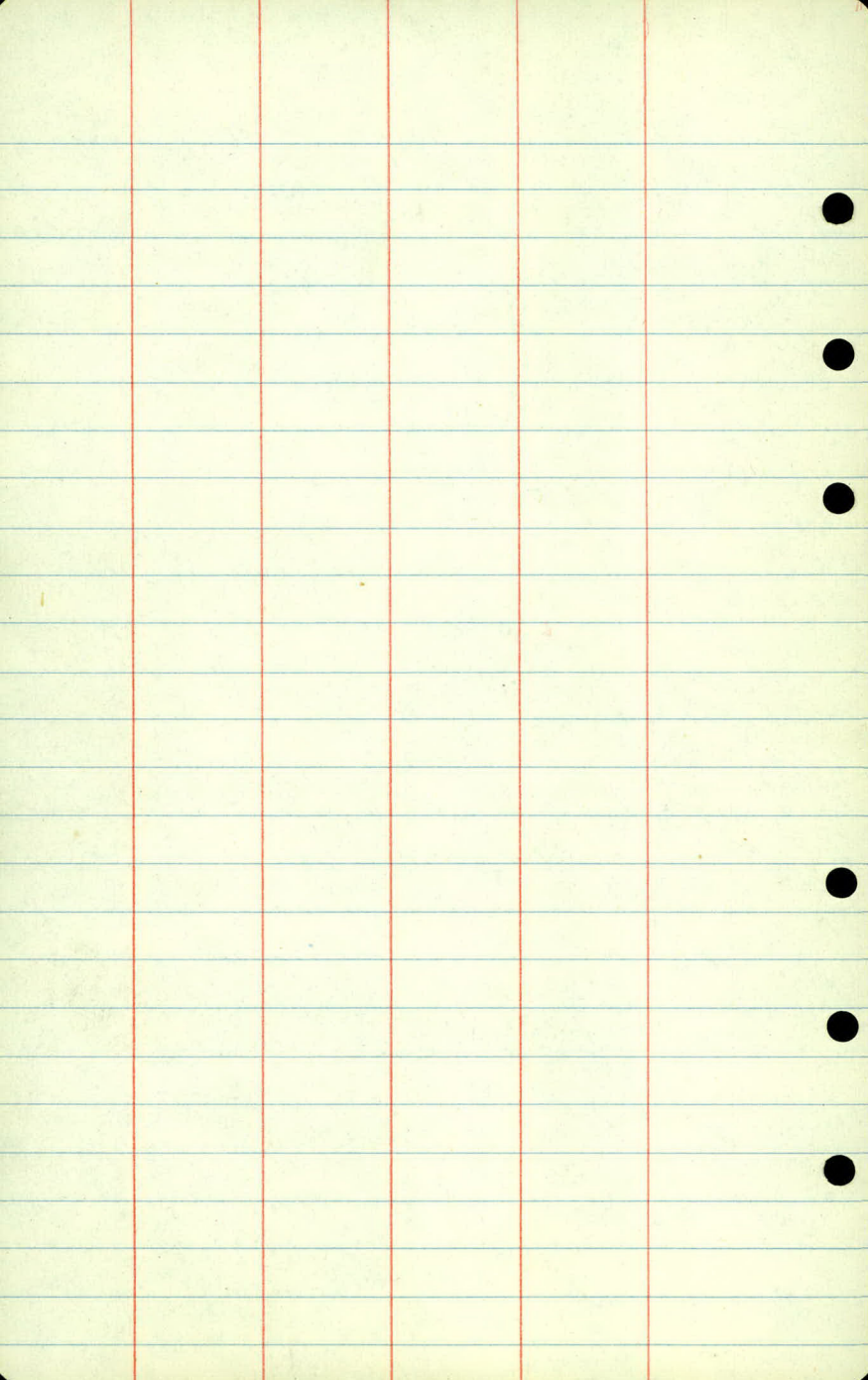
25

7 H2.93 - P.O.T. = @ Minn Transfer Track

(9 + 92.39 = @ 8th St.)

0 + 00 = @ Long Lake Rd.





Topography

5. Edge of Porch

+80-4"0-4'

+93-3"0-3' +51-Path X 5' +55-24"0-7'
 +39-5"0-19'
 +31-2-5"Oak-17'

4 +106-3-6"Pop-36' +12-8"Oak-7'
 +98-4"0-9'

+68-4"0-19'

3 +11-2-8"Oak-12'
 +108-2-2"Oak-32'

+12-8"0-31'

+56-24"Oak-10' 93-4"0-3' 5"0-29'
 +70-8"0-9'

+39-8"0-17'
 +109-4"0-11'

2

+71-5"0-5'
 +52-8"0-28-29'
 +48-5"0-0'
 +46-5"Tw.0-39'
 +38-4"0-23'
 +26-Swing/Pls-9-21'
 +11-4-8"0-32'
 80-11 8Tw.0-17 80-43'

1 +36-3-5"0-1'
 +10-5"Tw.0-25"
 10"0-31'

+82-12"0-26'

+97-2-8"Oak-35-38'
 +83-8"Tw.0-41' 5"0-22'
 +79-8"Tw.0-2 5"0-32'
 +11-10"0-27'
 +50-2-12"Oak-6-4'
 +43-4-8"Oak-40'
 +34-5"0-17'

+64-Cor Porch-35'

+90-2"Maple-31'

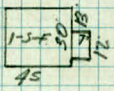
+13-Edge Black Top

0

Water

Garden

Garden



+35 = 11' 18' = +24'

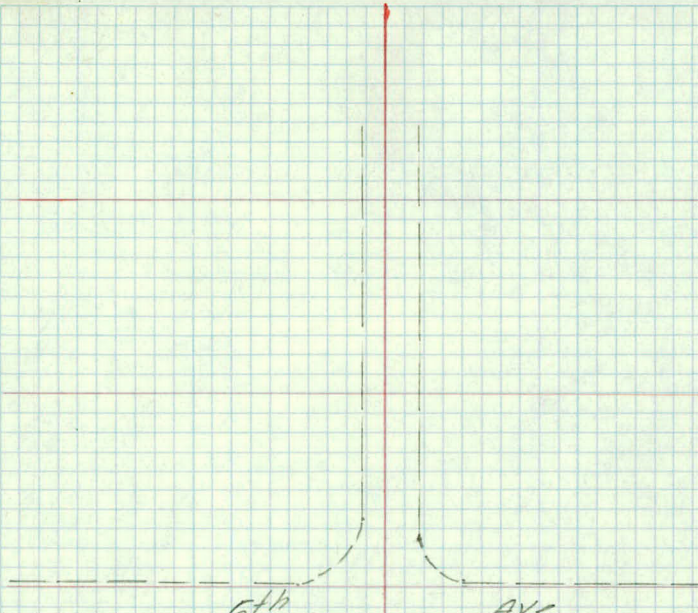
+01 = 46 41 = +02

+69/12" Pop - 45'
+77 - Edge of Bl. Top.
+60 - 8" T.H.P. B.E. 65

+94 - Edge of Water

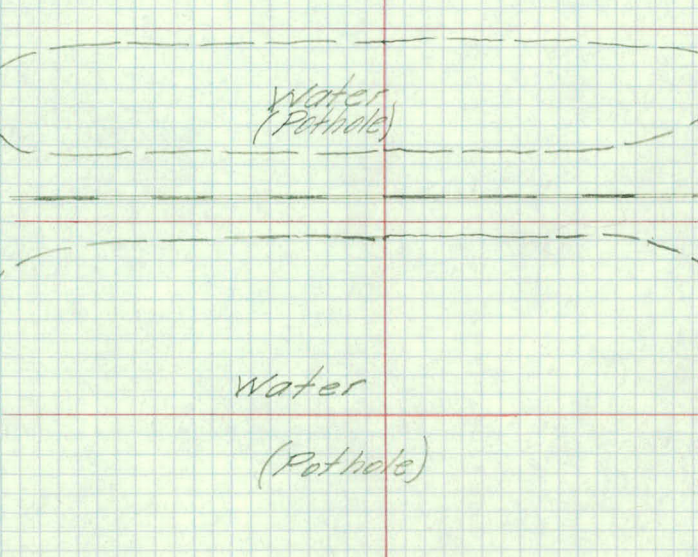
+38 - Edge of Water

+91 - Edge of Water



6th

Ave.



Water
(Pothole)

Water

(Pothole)

$$NE = 89-35\frac{1}{4}'$$

$$9 \overline{) 358-21}$$

$$141$$

$$35 \frac{1}{4}$$

X Sections

Sta	+	X	-	Elev
B.M.	4.67	901.09		(896.42)
T.P.	6.65	902.12	5.62	895.47
T.P.	12.79	911.23	3.68	898.44
B.M.			2.68	908.55
0 +00				06.8

+12 06.4

+21 05.2

+33 08.4

+64 06.6

1 04.0

+40 00.7

Spt. in P.P. S.W. Cor. 5th Ave & 8th St

Top Hyd. S.E. Cor. 8th St & Longlake Rd.

5.7	4.4	3.5	✓
50		50	

6.0	5.4	4.8	4.1	✓
50	25		50	

7.1	6.5	6.0	5.3	4.6	✓
50	25		26	22	
				50?	

5.9	5.5	3.5	2.8	1.6	1.3	1.0	✓
50	15	11		17	33	50	

6.2	5.9	5.5	4.6	3.1	1.8	✓
50	19	17		21	50	

7.9	8.3	8.9	8.2	7.2	6.4	5.7	4.6	4.2	✓
50	37	31	16		7	23	41	50	

12.8	12.6	11.6	10.5	9.3	8.2	7.7	✓
50	37	20		17	32	50	

Sta	+	π	-	Elev.
		911.23		
1 + 72				97.9
2				97.6
T.P.	3.04	909.07	11.20	900.03
+40				98.5
+78				99.4
3				99.2
+40				99.1
+79				98.6
4				98.2

L

E

E

15.1 15.2 14.9 13.3/21 11.3 11.1 ✓
 50 41 23 20 35 50

13.6 13.7 13.6 13.4 13.3 13.6 ✓
 50 28 19 28 50

3.2 3.4 4.6 5.5 6.8 7.3 ✓
 50 25 26 38 50

2.0 2.3 3.7 4.8 5.8 6.9 7.9 ✓
 50 25 14 27 38 50

2.2 2.8 3.9 4.8 5.9 7.7 ✓
 50 24 13 31 50

4.5 4.3 4.0 4.0 5.0 5.9 6.5 ✓
 50 39 19 23 38 50

5.4
 6.2 5.4 4.6 4.5 4.4 4.7 5.1 ✓
 50 30 15 16 40 50

6.4 6.3 5.5 4.9 4.7 4.9 ✓
 50 36 20 23 50

Sta	+	π	-	Elev
		903.07		

4	+30			95.8
---	-----	--	--	------

	+70			91.6
T.P.	331	894.39	12.00	891.07

5				87.1
---	--	--	--	------

	+50			85.5
--	-----	--	--	------

6				85.1
---	--	--	--	------

	+84			84.6
--	-----	--	--	------

	+90			86.8
T.P.	241	896.16	0.63	893.75

7	+03			94.4
---	-----	--	--	------

L

E

E

77 75 73 68 66 66 ✓
50 29 22 43 50

101 106 115 122 122 126 ✓
50 25 16 33 50

48 58 70 73 79 80 ✓
50 34 17 14 50

82 85 89 93 99
50 18 29 50

W.S. 2.27

07.11.

9.3

9.8

7.6 7.6 7.7 ✓
50 50

2.3 1.8 1.3 ✓
50 50

Sta	+	π	-	Elev
		896.16		

7 + 07				95.3
--------	--	--	--	------

+103 E Rail				95.96
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+115.3 E Rail				95.96
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+118				95.3
------	--	--	--	------

+125				94.6
------	--	--	--	------

+138				85.9
------	--	--	--	------

+150				84.5
------	--	--	--	------

+178				84.7
------	--	--	--	------

L

E

E

1.3
50

0.9

0.2
50

✓

0.20

0.20

1.4
50

0.9

0.4
50

✓

1.8
50

1.6

1.0
50

✓

103
50

103

103
50✓
85.78

W.S. = 10.38

L.O.

117

L.O.

✓

L.O.

115

L.O.

✓

Sto	+	π	-	Elev.
		896.16		

8				86.0
---	--	--	--	------

+26				86.4
-----	--	--	--	------

+31				87.5
-----	--	--	--	------

+57				89.6
-----	--	--	--	------

+83				93.4
-----	--	--	--	------

9				94.2
---	--	--	--	------

T.P.	4.73	899.74	1.15	895.01
------	------	--------	------	--------

+37				94.9
-----	--	--	--	------

+65				95.8
-----	--	--	--	------

L E E

10. 10.2 10. $\checkmark$

99 98 98 $\checkmark$
50 50

91 97 92 $\checkmark$
50 50

71 70 67 66 67 71 76 $\checkmark$
100 57 27 30 69 100

46 40 31 37 52 34 28 26 30 42 49 $\checkmark$
100 66 30 17 14-12 8 17 47 76 100

57
150
33 31 14 17 24 34 23 20 13 09 19 31 $\checkmark$
100 69 46 25 9 4 3 17 44 72 100

5.5 7.6 45 26 23 44 48 42 20 17 26 34 5.5 $\checkmark$
150 100 62 25 13 12 39 54 79 100 150

47
119 83 6.4 34 24 20 15 32 10 3.9 31 12 11 16 3.6 $\checkmark$
200 175 150 100 79 62 46 23 18 44 63 90 150

sto + K - E/cv
899.79

9 + 70

93.9

+91.16
B.M.

94.0

3.34

896.40

896.42

L

E

E

+

11.3	10.2	8.7	7.7	6.9	5.8	5.2	4.5	4.0	3.4
200	157	100	71	27		29	55	100	150

11.1	8.4	6.7
200	100	50

57	46	37
	50	100

X

