

Drawer 13 104

OFFICE OF COUNTY ENGINEER
RAMSEY COUNTY, MINN.

PLAN

Survey

Co. Rd. "B"

From Cleveland To Snelling

Road Acc't. No.

25
Dr 13

Date Filed 11-1976

File 104

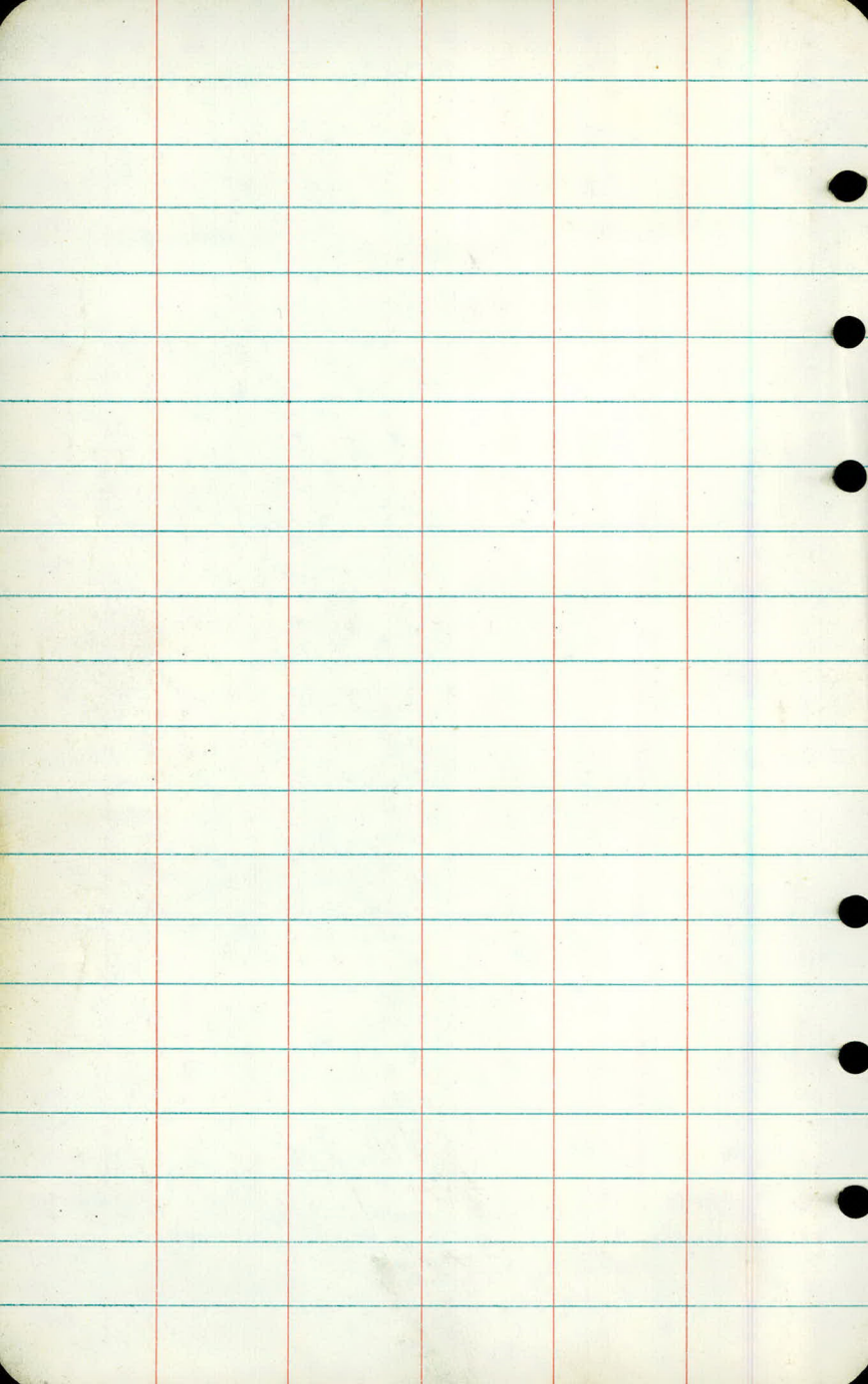
Co. Rd. "B"

Cleveland to Snelling

PLAN SURVEY

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X-Sections	32-



July 31, 1969

2

Alinement

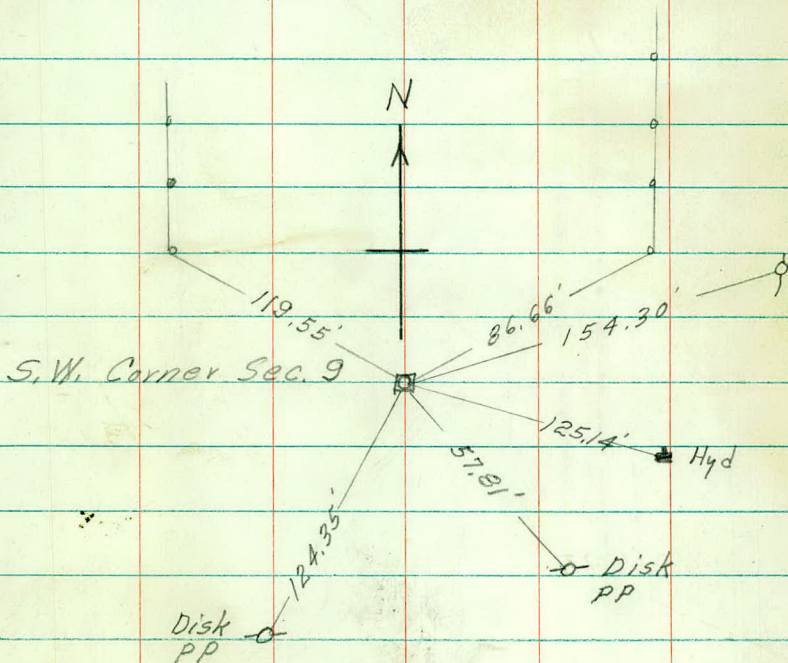
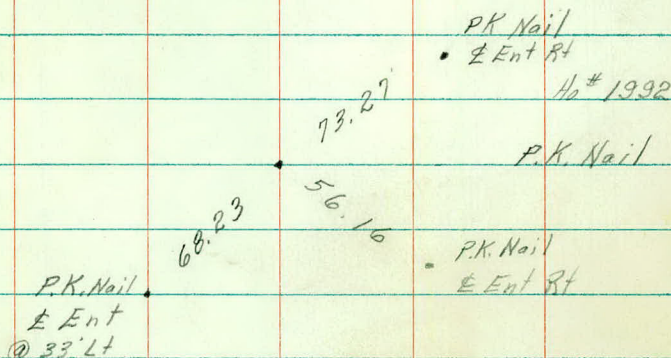
Sta Point Δ Lt Δ Rt

7+28.85 P.O.T

0+00

Oct. 27, 1969

3



Sta	Point	ΔL	ΔR
-----	-------	------------	------------

26+32.66 P.I.

23+20.18 P.O.T.

August 5, 1969

4

Disk
Side Tie

R.R. Spike
24" Cut

PK in
Curb

55.68
73.10
101

59.67' Stub pole
MHD-SRP

FAIRVIEW

Disk
PP

PK in
Curb

Hqd

12" Disk

PP

Iron

85.83'
74.30'
61.10'
67.04'
52.22'
61.22'

60.55' Iron
99.10' Granite
76.70' P.K. Nails

65.28

3N
10" E/m

3N
PP

29.41

37.58
37.5

53.12

P.K. Nail
W. Side Ent

Sta Point Δ Lt. Δ Rt.

3.5
31.2
2.0

52+63.52 Section Corner!

36+68.50 P.O.T.

34+00 P.O.T.

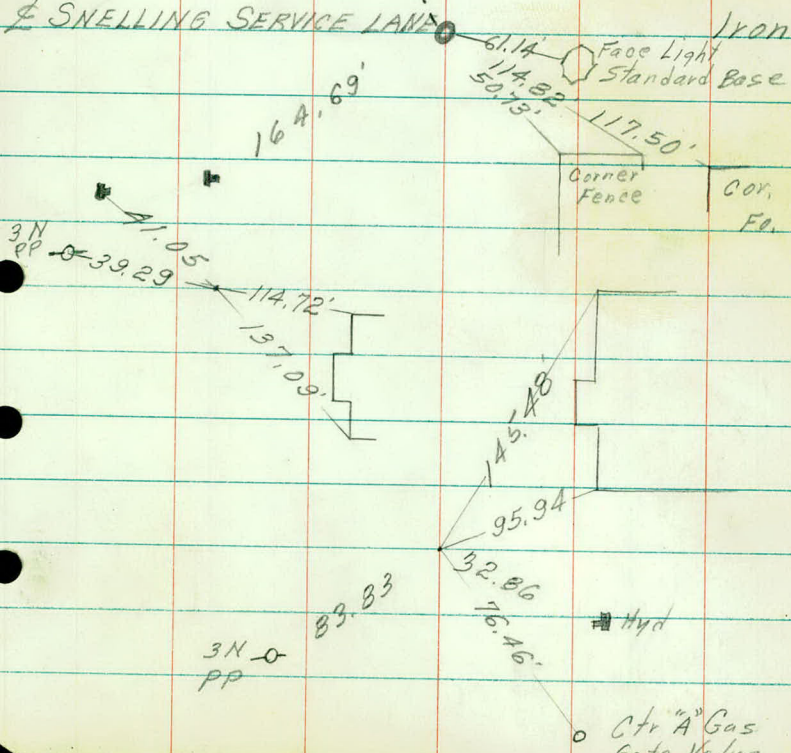
Oct. 27, 1969

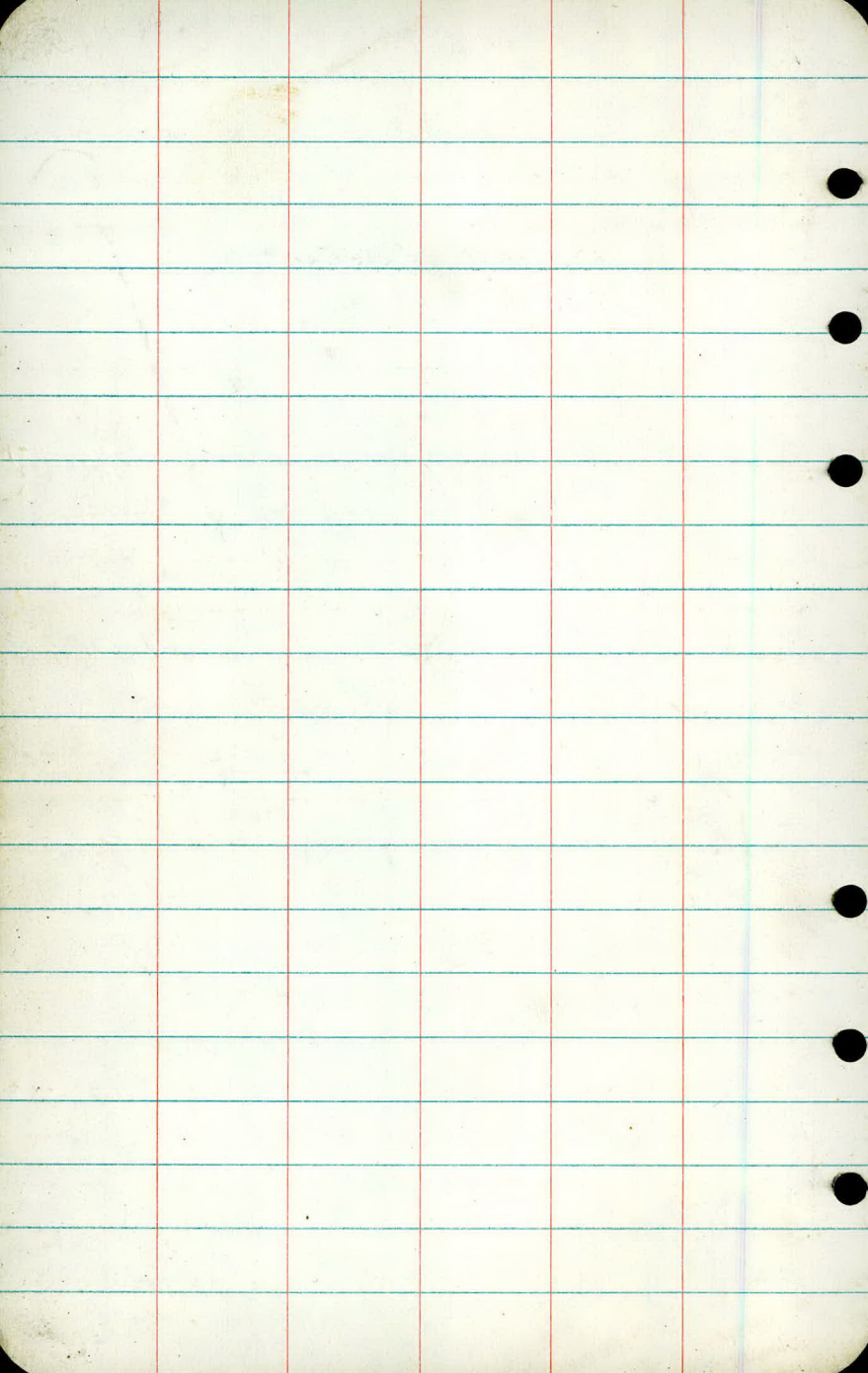
5

± S.B.L.

T.H. No. 51

± SNELLING SERVICE LANE





FK
WJ
KG
JA

Dec. 2, 1969

6

TOPOGRAPHY

Road
12

+85 ER
48

+77 POR
29

+71 E, Fe
49

+62 R Tie
Fe

+63 POR
19

+73 ER
12

+27 POR
33

+42 POR
21

+49 POR
18

+22 MH
21

+45 PP
38

+19 Cor. B, +
46

+22 Arc LT
54

+22 MH
23

+29 POR
30

+12 Cor Conc
60

+13 BR
88

0

-16 SE 4' Med -16 N. End 4' Median Tapered
56 55

-45 Cor Conc
58

-44 BR
72

-54 ER
40

-42 G. GV
22

Road
-65 26 26

-61 MH
37

-80 MH
13

-63 Arc LT
72

Road
-85 19-17

-1

Road
20 14

-12 E, Fe
42

-23 BR
66

-16 POR
35

-48 ER
51

-56 POR
25

-72 BR
15

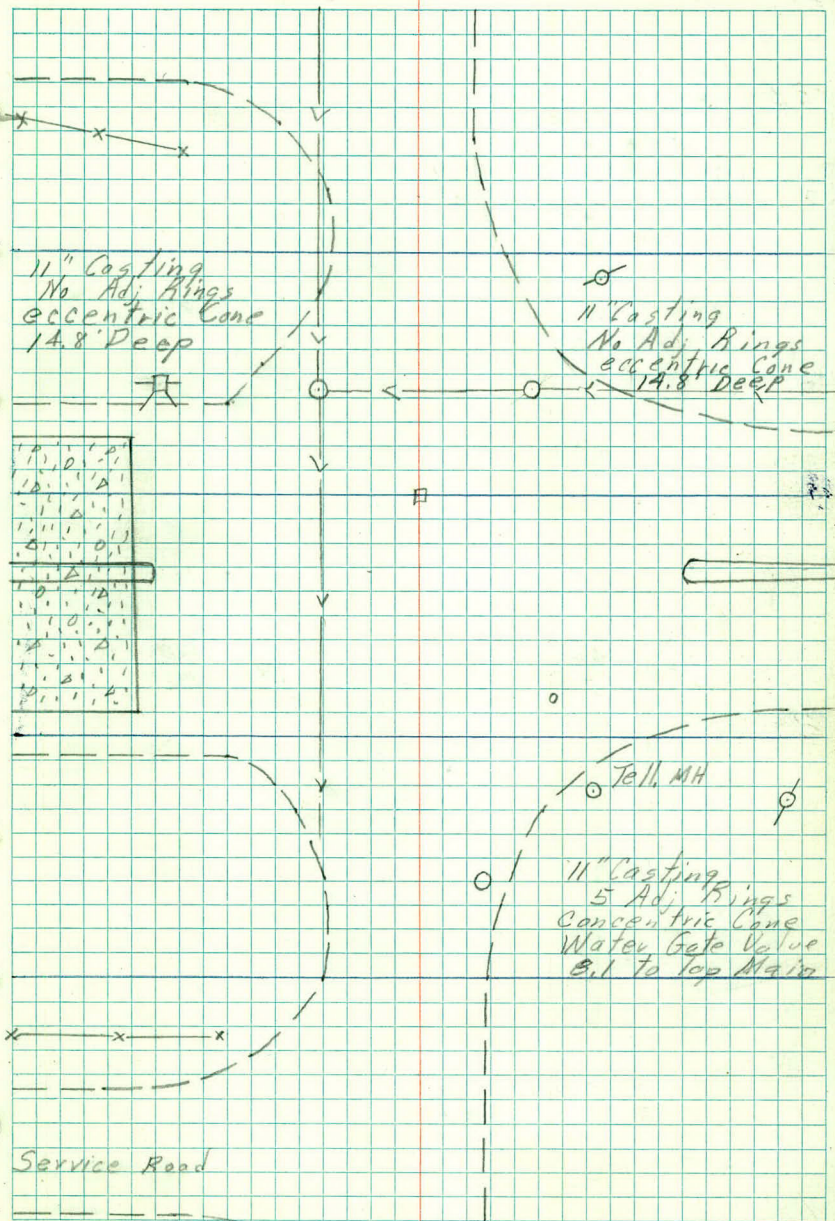
-2

-98 PP
28

Road
12 13

Dec. 2, 1969

7



KTWN

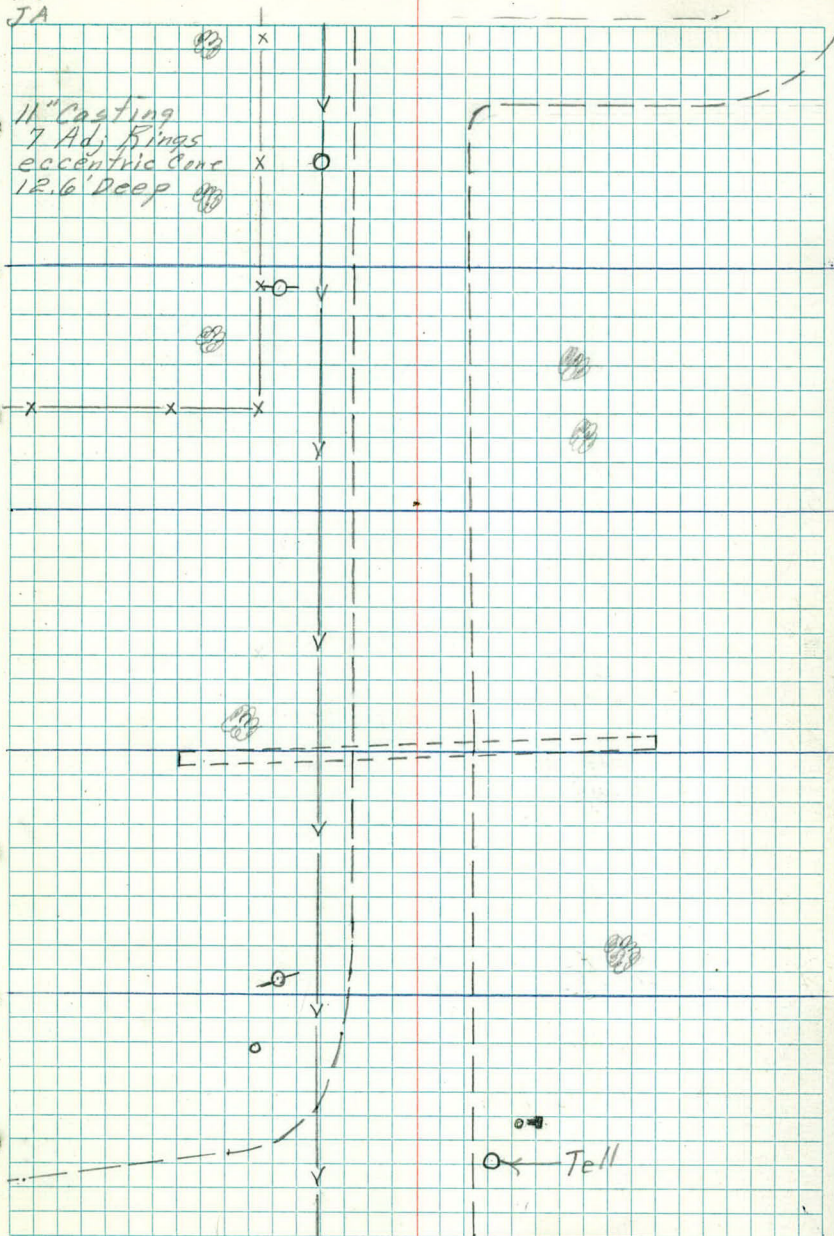
	$+47 \frac{10" \text{ Apple}}{43}$	$+43 \frac{E 18' \text{ Eht}}{C.R.}$
$+23 \frac{MH}{19}$	$+14 \frac{10" \text{ Apple}}{43}$	
3	$+96 \frac{PP}{29}$	$\frac{\text{Road}}{13 \ 11}$
	$+85 \frac{10" \text{ Apple}}{43}$	$+79 \frac{Tw 4" \text{ Elm}}{33}$
	$+71 \frac{Fe Cor}{33}$	$+65 \frac{4" \text{ Tw Elm}}{35}$
	$+05 \frac{4" \text{ CE}}{36}$	$+02 \frac{SE 24" \text{ SCP}}{50}$
2	$+93 \frac{NE 24" \text{ SCP}}{49}$	$\frac{\text{Road}}{13 \ 12}$
	$+65 \frac{ER}{13}$	
$+42 \frac{POR}{16}$	$+53 \frac{PP}{29}$	$+58 \frac{Tw 8" \text{ Coll}}{43}$
	$+39 \frac{WGV}{34}$	
$+17 \frac{POR}{39}$	$+27 \frac{POR}{21}$	$+23 \frac{Hyd}{25}$
	$+12 \frac{BR}{82}$	$+11 \frac{MT}{16}$
1		$+23 \frac{WGV}{22}$

FX
HG
WJ
JA

Dec. 5, 1969

8

11" Casting
7 Adj. Rings
eccentric Cent
12.6' Deep



6

$$\begin{array}{r} \text{Fe} \\ 37 \end{array}$$

$$\begin{array}{r} \text{Road} \\ 11 \quad 11 \end{array}$$

$$\begin{array}{r} \downarrow 6" \text{Maple} \\ +68 \quad 45 \end{array}$$

$$\begin{array}{r} \downarrow \text{Trip } 4" \text{ Birch} \\ +92 \quad 62 \end{array}$$

$$\begin{array}{r} \downarrow 14" O \\ +90 \quad 57 \end{array}$$

$$\begin{array}{r} \downarrow BR \\ +39 \quad 47 \end{array}$$

$$\begin{array}{r} \downarrow \text{Yard Lt} \\ +62 \quad 71 \end{array}$$

$$\begin{array}{r} \downarrow 218" \text{Ent} \\ +49 \quad B.F \end{array}$$

$$\begin{array}{r} \downarrow \text{Mugo P} \\ +34 \quad 44 \end{array}$$

$$\begin{array}{r} \downarrow \text{Mugo P} \\ +31 \quad 37 \end{array}$$

$$\begin{array}{r} \downarrow \text{NWC Co. Ho} \\ +61 \quad 119 \end{array}$$

$$\begin{array}{r} \downarrow \text{Cor Ent} \\ +19 \quad 66-77 \end{array}$$

$$\begin{array}{r} \downarrow 6" \text{Maple} \\ +23 \quad 53 \end{array}$$

$$\begin{array}{r} \downarrow 18" \text{Oak} \\ +54 \quad 51 \end{array}$$

$$\begin{array}{r} \downarrow 6" P \\ +11 \quad 50 \end{array}$$

$$\begin{array}{r} \downarrow \text{Mugo P} \\ +23 \quad 37 \end{array}$$

$$\begin{array}{r} \downarrow \text{Fe Cor} \\ +22 \quad 40 \end{array}$$

$$\begin{array}{r} \downarrow 26" \text{Oak} \\ +24 \quad 46 \end{array}$$

$$\begin{array}{r} \downarrow \text{MH Tell} \\ +11 \quad 18 \end{array}$$

$$\begin{array}{r} \downarrow \text{Gate P} \\ +03 \quad 65 \end{array}$$

$$\begin{array}{r} \text{Road} \\ 12 \quad 12 \end{array}$$

$$\begin{array}{r} \downarrow 8" P \\ +00 \quad 41 \end{array}$$

$$\begin{array}{r} 5 \\ +95 \quad 212" \text{Ent} \\ \text{C.R} \end{array}$$

$$\begin{array}{r} \downarrow \text{Gate P (13')} \\ +90 \quad 65 \end{array}$$

$$\begin{array}{r} +66 \quad \text{Fe} \\ 40 \end{array}$$

$$\begin{array}{r} +77 \quad \text{ER Fe} \\ 65 \end{array}$$

$$\begin{array}{r} +99 \quad 8" P \\ 57 \end{array}$$

$$\begin{array}{r} +55 \quad \text{PP} \\ 29 \end{array}$$

$$\begin{array}{r} +93 \quad \text{Hyd} \\ 26 \end{array}$$

$$\begin{array}{r} +58 \quad 10" \text{CE} \\ 56 \end{array}$$

$$\begin{array}{r} +72 \quad 4" P \\ 56 \end{array}$$

$$\begin{array}{r} +38 \quad \text{BR Fe} \\ 33 \end{array}$$

$$\begin{array}{r} +58 \quad \text{Trip } 6" \text{ Ash} \\ 38 \end{array}$$

$$\begin{array}{r} +56 \quad \text{PP} \\ 25 \end{array}$$

$$\begin{array}{r} +48 \quad \text{NE Cor Ho} \\ 85 \end{array}$$

$$\begin{array}{r} +34 \quad 10" \text{Apple} \\ 43 \end{array}$$

$$\begin{array}{r} +47 \quad \text{Honeysuckle} \\ 31 \end{array}$$

$$\begin{array}{r} +38 \quad 14" \text{CE} \\ 43 \end{array}$$

4

$$\begin{array}{r} +00 \quad \text{Fe} \\ 33 \end{array}$$

$$\begin{array}{r} \text{Road} \\ 12 \quad 11 \end{array}$$

$$\begin{array}{r} +02 \quad 4" \text{Maple} \\ 24 \end{array}$$

$$\begin{array}{r} +94 \quad \text{EE } 12" X \\ 22 \end{array}$$

$$\begin{array}{r} +99 \quad 3" P \\ 35 \end{array}$$

$$\begin{array}{r} +81 \quad 218" \text{Ent} \\ \text{C.R} \end{array}$$

$$\begin{array}{r} +75 \quad 10" \text{Apple} \\ 43 \end{array}$$

$$\begin{array}{r} +67 \quad 2" \text{MT Ash} \\ 28 \end{array}$$

$$\begin{array}{r} +71 \quad \text{ER} \\ 56 \end{array}$$

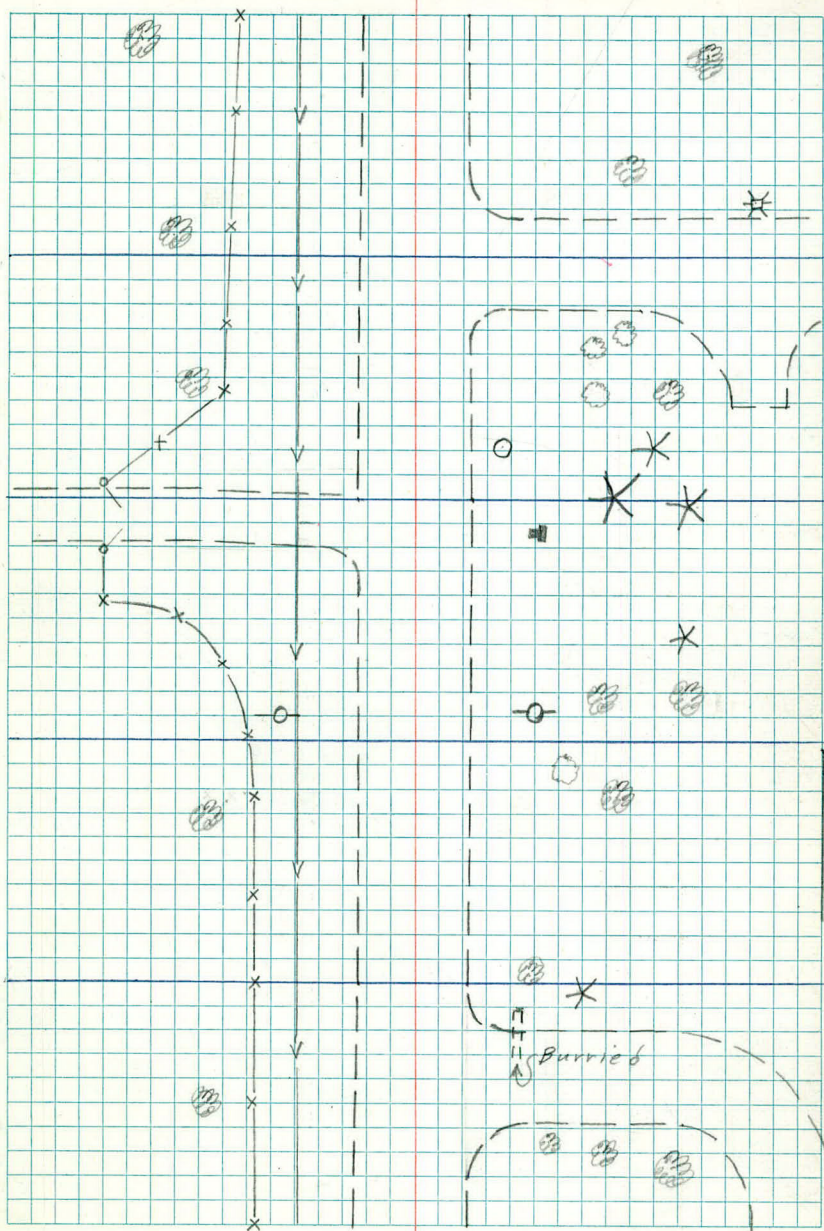
$$\begin{array}{r} +64 \quad 6" \text{Em} \\ 40 \end{array}$$

$$\begin{array}{r} +51 \quad \text{BR} \\ 58 \end{array}$$

$$\begin{array}{r} +62 \quad 18" \text{CE} \\ 54 \end{array}$$

Dec. 5, 1969

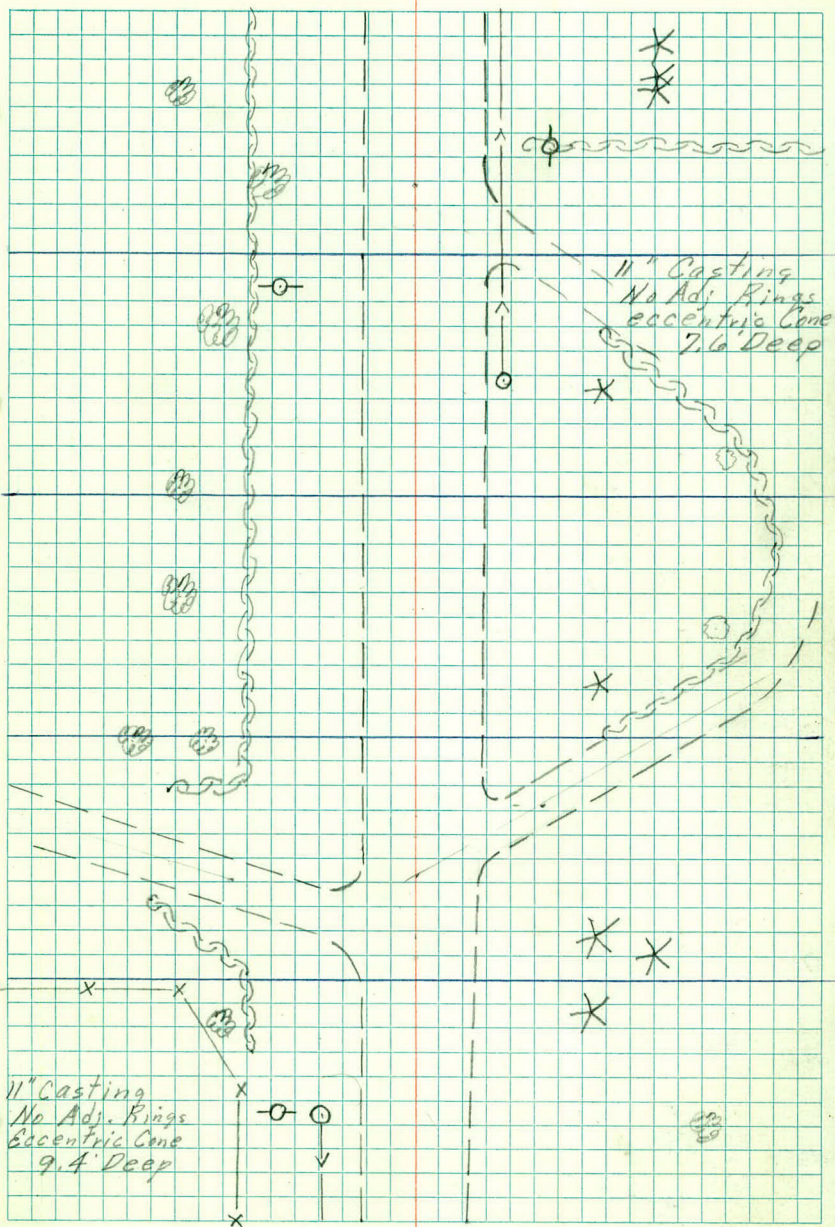
9



			$+44 \frac{6^{\circ}P}{51}$	
			$+36 \frac{4^{\circ}P}{51}$	
	$+33 \frac{10^{\circ}Apple}{49}$		$+22 \frac{N.E. Hedge}{40}$	$+34 \frac{6^{\circ}P}{51}$
$+14 \frac{24^{\circ}Oak}{32}$			$+22 \frac{PP}{28}$	
5	$Hedge \frac{33}{33}$	$Road \frac{11}{15}$		$+14 \frac{R.Tie Ent}{Ent}$
			$+79 \frac{NE Cor Ho}{109}$	$+84 \frac{E Hedge}{39}$
	$+93 \frac{PP}{28}$		$+74 \frac{MH}{18}$	
	$+85 \frac{30^{\circ}O}{41}$		$+73 \frac{2^{\circ}P}{39}$	
	$+52 \frac{6^{\circ}Apple}{49}$		$+58 \frac{3^{\circ}Arbovide}{64}$	$+58 \frac{Hedge}{70}$
			$+40 \frac{Hedge}{75}$	
	$+29 \frac{12^{\circ}Oak}{48}$		$+23 \frac{4^{\circ}Arbov}{63}$	$+23 \frac{Hedge}{70}$
7		$Road \frac{11}{14}$	$+12 \frac{3^{\circ}P}{38}$	
$+90 \frac{Cor Hedge}{35}$			$+100 \frac{B. Hedge}{39}$	
	$+98 \frac{6^{\circ}Cedar}{43}$		$+71 \frac{R.Tie Ent}{Ent}$	$+86 \frac{E 14' Ent}{27}$
$+89 \frac{N. End Hedge}{53}$		$+98 \frac{14^{\circ}CE}{58}$	$+59 \frac{8^{\circ}P}{37}$	
	$+71 \frac{E 14' Ent}{38}$			
$+67 \frac{E. Hedge}{55}$		$+58 \frac{R.Tie Ent}{Ent}$	$+56 \frac{8^{\circ}P}{50}$	
	$+51 \frac{Cor Hedge}{35}$			
$+41 \frac{8^{\circ}Cedar}{41}$		$+48 \frac{Fe C}{49}$	$+44 \frac{8^{\circ}P}{37}$	
	$+35 \frac{B. Hedge}{34}$			
$+23 \frac{PP}{29}$		$+27 \frac{Fe.C}{36}$	$+20 \frac{Trip 4^{\circ} Birch}{62}$	
6	$+22 \frac{MH}{19}$	$Road \frac{11}{11}$		$+17 \frac{NE Cor Ho}{94}$

Dec 5, 1969

10



11

$\frac{Fe}{35}$	$\frac{Road}{14}$	12	$\frac{W.E. 15" CM}{20}$
$\frac{MH}{8}$	$\frac{Apple}{66}$	89	$\frac{12" P}{44}$
$\frac{4" O}{57}$	$\frac{4" Coll}{60}$	85	
$\frac{10" O}{46}$	$\frac{4" O}{40}$		
$\frac{6" O}{43}$	$\frac{8" O}{35}$	$\frac{CB}{21}$	
$\frac{2-10" Coll}{58}$	$\frac{MH}{17}$	$\frac{30" Maple}{56}$	
$\frac{CB}{21}$			

10

$\frac{Fe}{33}$	$\frac{Road}{13}$	13	$\frac{6" P}{60}$
$\frac{12" O}{41}$	$\frac{Hyd}{27}$	90	$\frac{6" P}{57}$
$\frac{Tw CE}{50}$	$\frac{WGV}{25}$	92	
$\frac{Fe Cor}{33}$	$\frac{E.E. Culv}{20}$	87	$\frac{E 17" Ent}{28}$
$\frac{PP}{29}$	$\frac{Maple}{57}$	75	
$\frac{6" Elm}{43}$	$\frac{WE 12" Culv}{20}$	59	$\frac{R.Tie}{}$
$\frac{E 10" Ent}{Gravel}$	$\frac{3" P}{37}$	48	
$\frac{WE 15" x Culv}{23 E.E. Buried}$	$\frac{18" CE}{49}$	29	

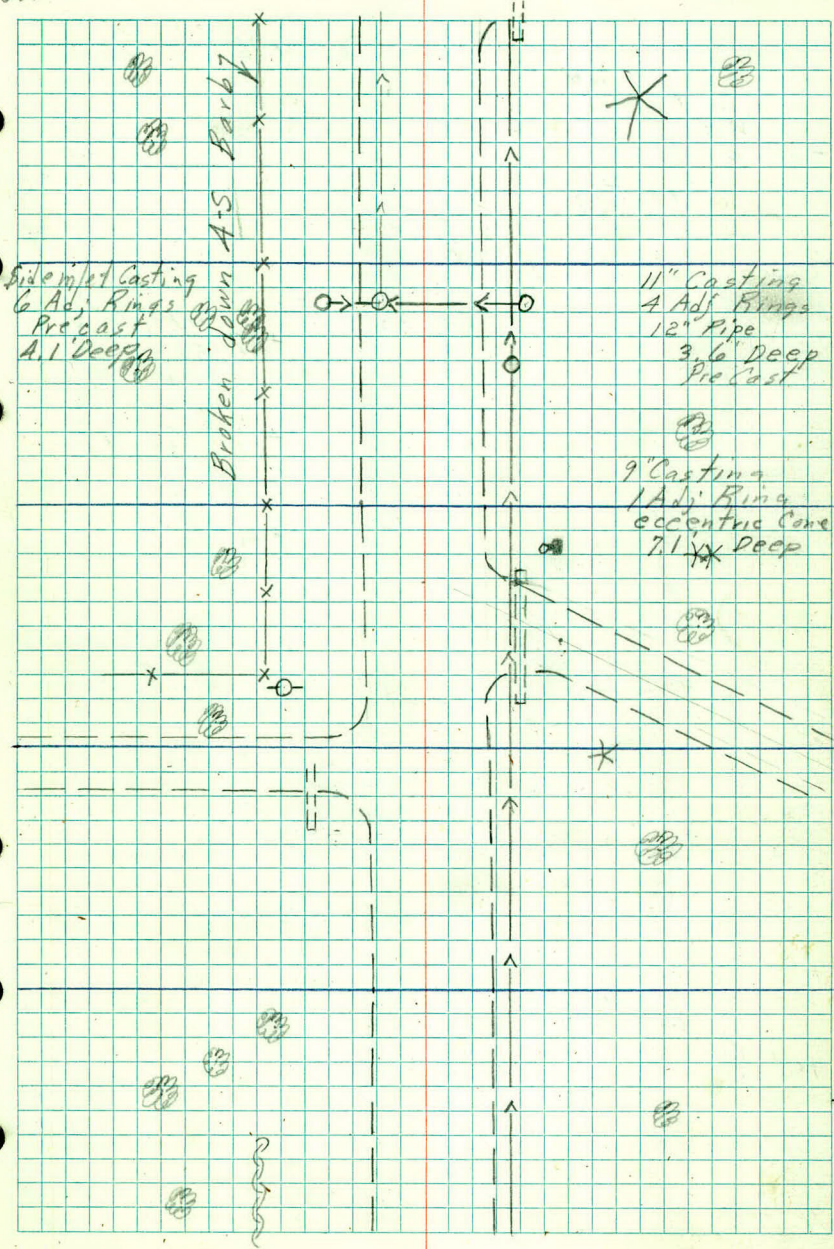
9

$\frac{Road}{11}$	14	$\frac{18" O}{32}$	$\frac{NW Cor. Ho}{118}$
$\frac{14" Coll}{43}$	$\frac{18" Coll}{55}$	78	
$\frac{E End Hedge}{34}$	$\frac{8" Apple}{51}$	56	$\frac{6" Maple}{50}$
		74	

FK
KG
JA

Dec 11, 1969
overcast 18°

11



$$+18 \frac{\text{MH}}{13}$$

$$+17 \frac{\text{MH}}{19}$$

$$+11 \frac{\text{PP}}{29}$$

13

$$\text{Road} \\ 13 \frac{12}{12}$$

$$+11 \frac{\text{MH}}{17}$$

$$+46 \frac{\text{G.R.P.}}{24}$$

$$+39 \frac{\text{BR}}{13}$$

$$+101 \frac{\text{CB}}{21}$$

$$+27 \frac{\text{WGV}}{28}$$

$$+23 \frac{\text{Hyd}}{28}$$

$$+77 \frac{\text{Cor Hedge}}{36}$$

$$+63 \frac{8" \text{P}}{76}$$

$$+49 \frac{\text{NE Cor Ho}}{110}$$

$$+12 \frac{4" \text{Calt}}{46}$$

12

$$\text{Road} \\ 15 \frac{12}{12}$$

$$+94 \frac{\text{EE 15" CM}}{20}$$

$$+85 \frac{10' \text{ Conc Ent}}{32}$$

$$+54 \frac{\text{Cor Hedge}}{36}$$

$$+74 \frac{\text{WE 15" CM}}{19}$$

$$+52 \frac{\text{Fe Cor}}{35}$$

$$+52 \frac{\text{PP}}{61}$$

$$53 \frac{\text{PP}}{40}$$

$$+41 \frac{8" \text{ Apple}}{61}$$

$$+44 \frac{10" \text{ LF}}{41}$$

$$+44 \frac{\text{MH}}{8}$$

$$+27 \frac{\text{PP}}{28}$$

$$+30 \frac{10" \text{ P}}{44}$$

$$+25 \frac{\text{Mugor P}}{39}$$

$$+22 \frac{\text{Mugor P}}{45}$$

$$+21 \frac{\text{EE 15" CM}}{20}$$

$$+04 \frac{\text{R.Tie Ent}}{Ent}$$

$$+09 \frac{\text{E Ent}}{45}$$

11

Dec 11, 1969

12

11 Casting

4 Adj. Rings

Max. Hat

6, 8' to Top Main

Side Inlet Casting
Precast Section
4.0' Deep

Spirea
Buckthorn
Honeysuckle
& Rose

16

13 20

$$+11 \overset{\vee}{\text{B. Row P}} \frac{53}{\quad}$$

$$+04 \overset{\vee}{\text{B. Row}} \frac{47}{\quad}$$

$$+94 \overset{\vee}{\text{MH}} \frac{8}{\quad}$$

$$+90 \overset{\vee}{\text{PP}} \frac{28}{\quad}$$

$$+98 \overset{\vee}{\text{PP}} \frac{69}{\quad}$$

$$\text{Road} \frac{13}{22}$$

$$+96 \overset{\vee}{\text{SD}} \frac{31}{\quad}$$

$$+82 \overset{\vee}{\text{NH}} \frac{35}{\quad}$$

$$+54 \overset{\vee}{\text{MH}} \frac{8}{\quad}$$

$$+54 \overset{\vee}{\text{CB}} \frac{21}{\quad}$$

$$+54 \overset{\vee}{\text{CB}} \frac{21}{\quad}$$

$$+41 \overset{\vee}{5" \text{ Coll}} \frac{33}{\quad}$$

$$+10 \overset{\vee}{2" \text{ Ash}} \frac{34}{\quad}$$

$$+07 \overset{\vee}{\text{ER}} \frac{22}{\quad}$$

14

$$\text{Road} \frac{13}{26}$$

$$+95 \overset{\vee}{\text{Curb Line BR}} \frac{35}{\quad}$$

$$+64 \overset{\vee}{\text{POR}} \frac{26}{\quad}$$

$$+70 \overset{\vee}{\text{ERC}} \frac{36}{\quad}$$

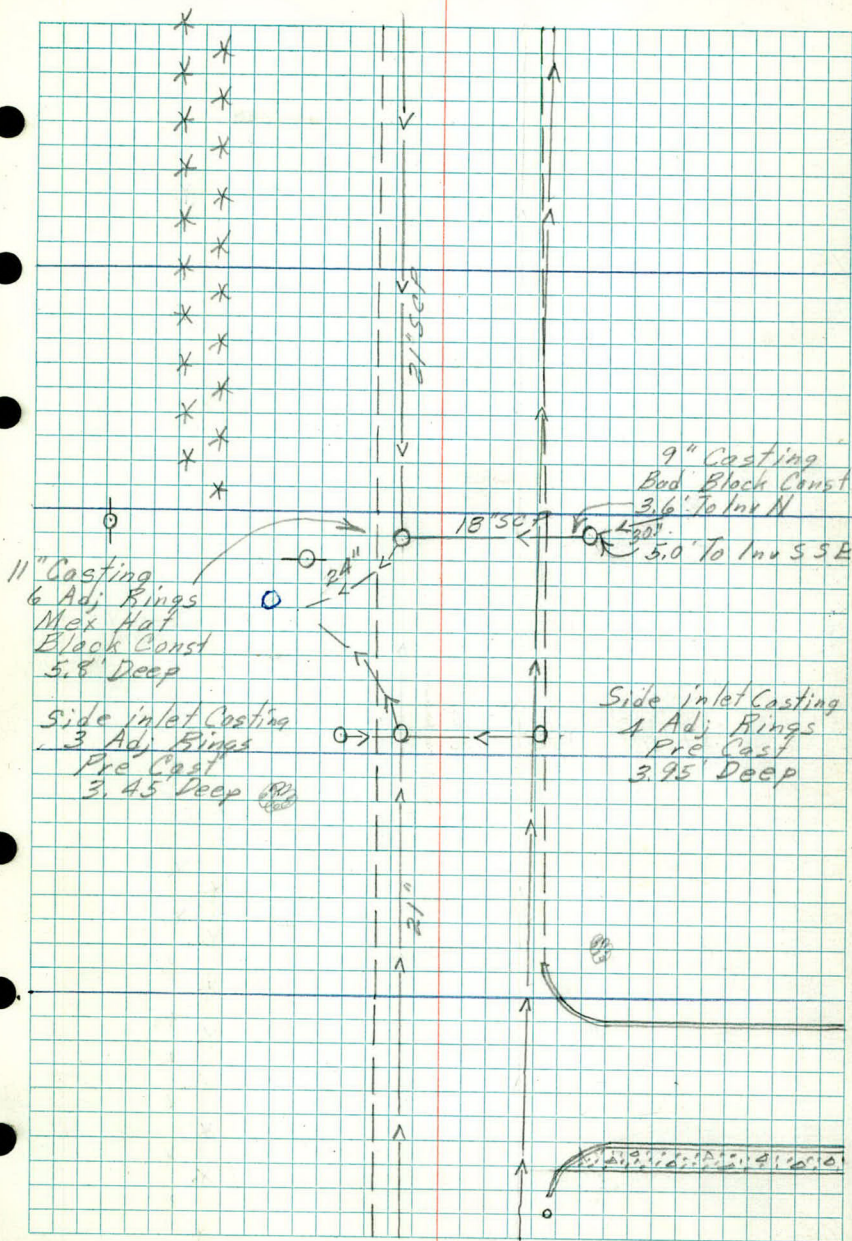
$$+64 \overset{\vee}{\text{W Edge Walk}}$$

$$+55 \overset{\vee}{\text{GRP}} \frac{23}{\quad}$$

$$+59 \overset{\vee}{\text{BRG}} \frac{23}{\quad}$$

Dec. 11, 1969

13



$$+45 \frac{\sqrt{B. Row P}}{56}$$

$$+45 \frac{\sqrt{B. Row P}}{48}$$

$$+44 \frac{\sqrt{PP}}{28}$$

$$+22 \frac{\sqrt{PP}}{28}$$

18

$$\frac{Road}{13\checkmark}$$

$$+101 \frac{CB}{21}$$

$$+99 \frac{\sqrt{E. Curb}}{24}$$

$$+85 \frac{\sqrt{Cor Curb}}{33}$$

$$+90 \frac{\sqrt{POR}}{26}$$

$$+85 \frac{\sqrt{ER}}{44}$$

$$+82 \frac{\sqrt{POR}}{48}$$

$$+82 \frac{\sqrt{POR}}{33}$$

$$+78 \frac{\sqrt{POR}}{44}$$

$$+35 \frac{\sqrt{CB}}{21}$$

$$+49 \frac{\sqrt{POR}}{29}$$

$$+43 \frac{\sqrt{E. Curb}}{23}$$

$$+35 \frac{\sqrt{MH}}{8}$$

$$+52 \frac{\sqrt{POR}}{38}$$

$$+43 \frac{\sqrt{R. Tie}}{Curb}$$

$$+46 \frac{\sqrt{BR}}{41}$$

$$+32 \frac{\sqrt{Cor Curb}}{37}$$

$$+35 \frac{CB}{21}$$

17

$$+100 \frac{\sqrt{End Row P}}{47}$$

$$\frac{Road}{14\checkmark 21\checkmark}$$

$$+28 \frac{\sqrt{Light Pole}}{40}$$

$$+99 \frac{\sqrt{MH}}{24}$$

$$+98 \frac{\sqrt{MH}}{42}$$

$$+93 \frac{\sqrt{E. Row P}}{54}$$

$$+88 \frac{\sqrt{Hyd}}{28}$$

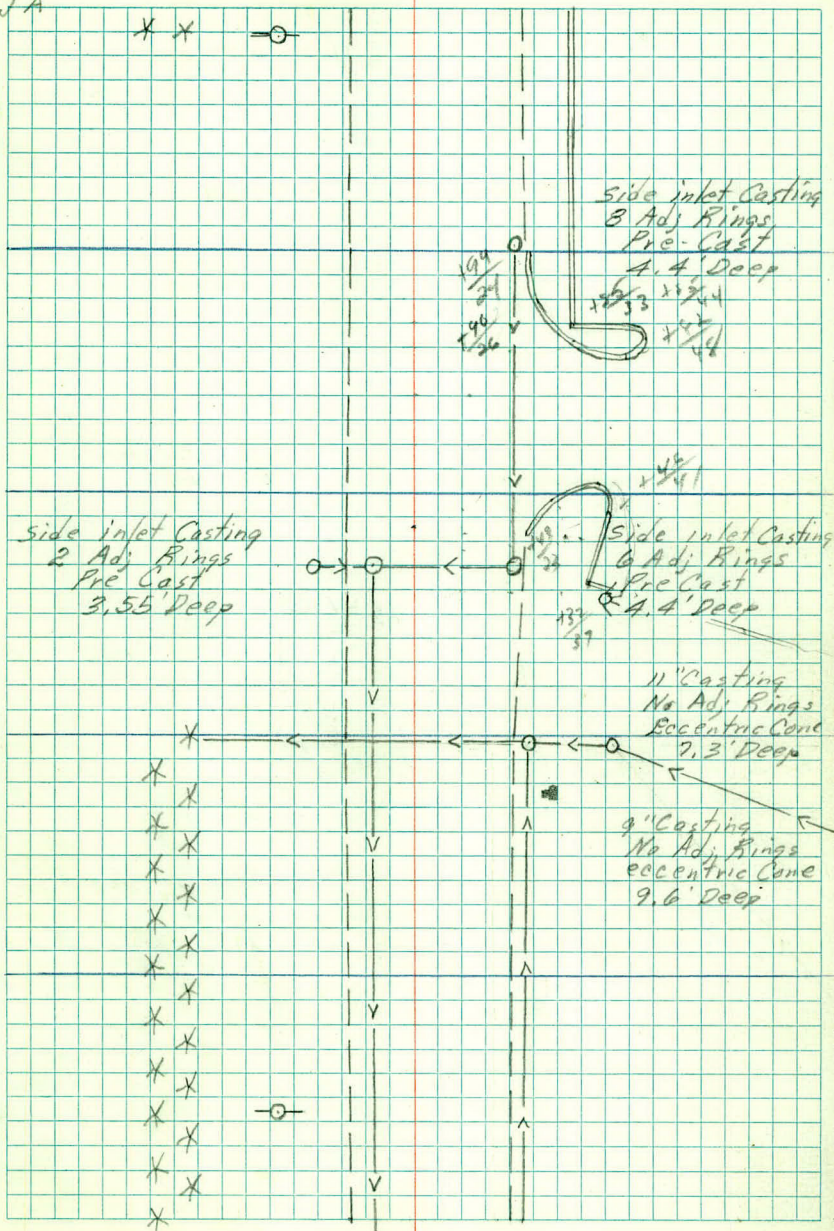
16

$$+22 \frac{\sqrt{PP}}{28}$$

FK
KG
WJ
JA

Dec 11, 1969
Dec. 12, 1969

14



21

✓
Road
13 16

20

✓
PP
+84 28

✓
Road
14 16

✓
PP
+83 43

✓
ERC
+75 24

✓
BR
+59 39

✓
R-Tie
+75 37

✓
POR
+24 51

✓
BR
+13 44

✓
POR
+18 24

✓
Road
13 22

✓
R-Tie
+00 Ent
+98 56

✓
Hyd
+79 26

✓
POR
+63 29

✓
L.L. Pole
+69 38

✓
POR
+30 37

✓
E. Edge Walk
+66 35

✓
POR
+29 45

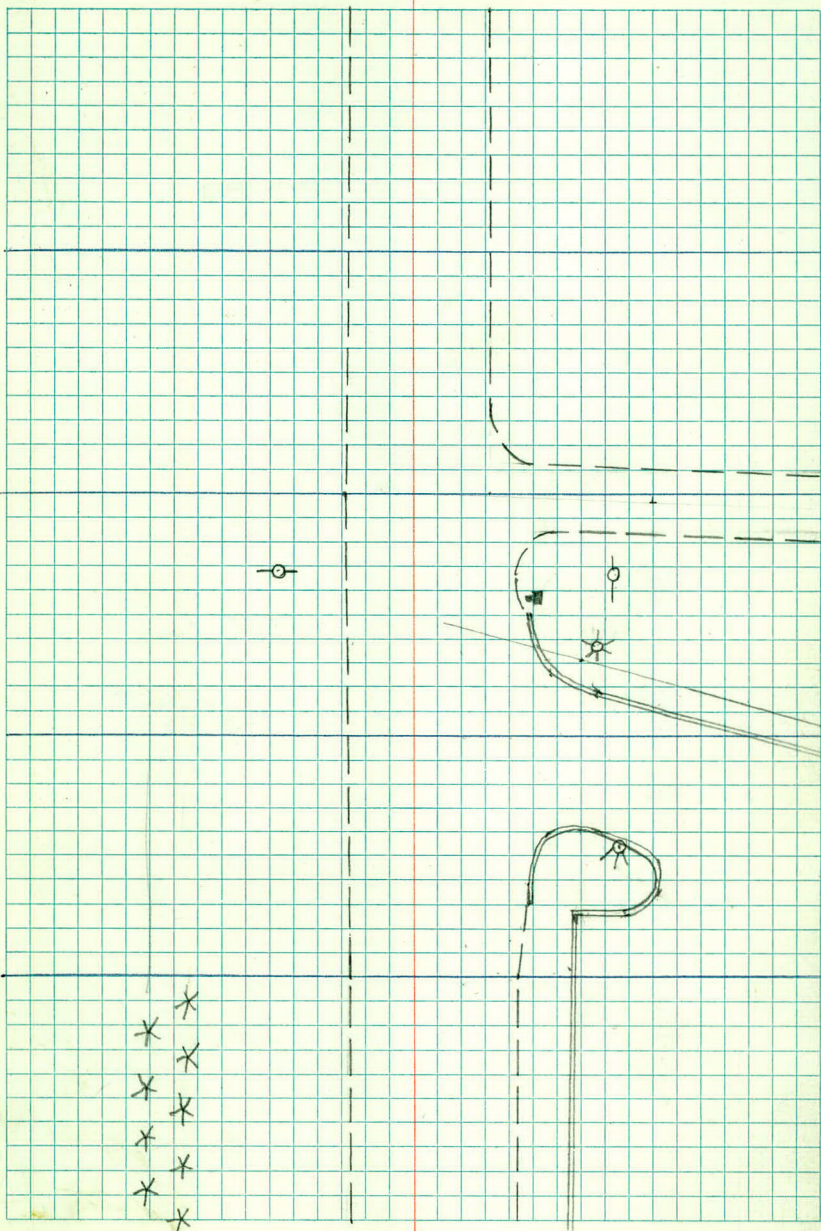
✓
L.L. Pole
+27 43

✓
End C
+15 24

✓
Cor Curb
+13 33

19

15



$$\begin{array}{r}
 \checkmark 2'' \text{LP} \\
 +34 \quad 61 \\
 \hline
 \end{array}
 \quad
 \begin{array}{r}
 \checkmark 2'' \text{LP} \\
 +40 \quad 49 \\
 \hline
 \end{array}
 \quad
 \begin{array}{r}
 \checkmark 2'' \text{LP} \\
 +47 \quad 49 \\
 \hline
 \end{array}$$

$$\begin{array}{r}
 \checkmark \text{Hyd} \\
 +48 \quad 27 \\
 \hline
 \end{array}$$

$$\begin{array}{r}
 +17 \\
 \text{End Row 1P} \\
 \hline
 +30 \quad 49 \\
 \hline
 \end{array}
 \quad
 \begin{array}{r}
 \checkmark \\
 \text{PP} \\
 +16 \quad 30 \\
 \hline
 \end{array}$$

$$\begin{array}{r}
 \checkmark \\
 \text{ENT} \\
 +19 \quad 60 \\
 \hline
 \end{array}
 \quad
 \begin{array}{r}
 \checkmark \\
 \text{Road} \\
 12 \quad 17 \\
 \hline
 \end{array}$$

$$\begin{array}{r}
 \checkmark \text{R.Tic} \\
 +31 \quad \text{ENT} \\
 \hline
 \end{array}$$

$$\begin{array}{r}
 \checkmark \text{MH} \\
 +22 \quad 19 \\
 \hline
 \end{array}$$

23

$$\begin{array}{r}
 \checkmark \text{stp} \\
 +30 \quad 36 \\
 \hline
 \end{array}$$

$$\begin{array}{r}
 \checkmark \\
 \text{Road} \\
 14 \quad 17 \\
 \hline
 \end{array}$$

$$\begin{array}{r}
 \checkmark 26'' \text{Elm} \\
 +03 \quad 35 \\
 \hline
 \end{array}$$

22

$$\begin{array}{r}
 \checkmark 28'' \text{Elm} \\
 +75 \quad 35 \\
 \hline
 \end{array}$$

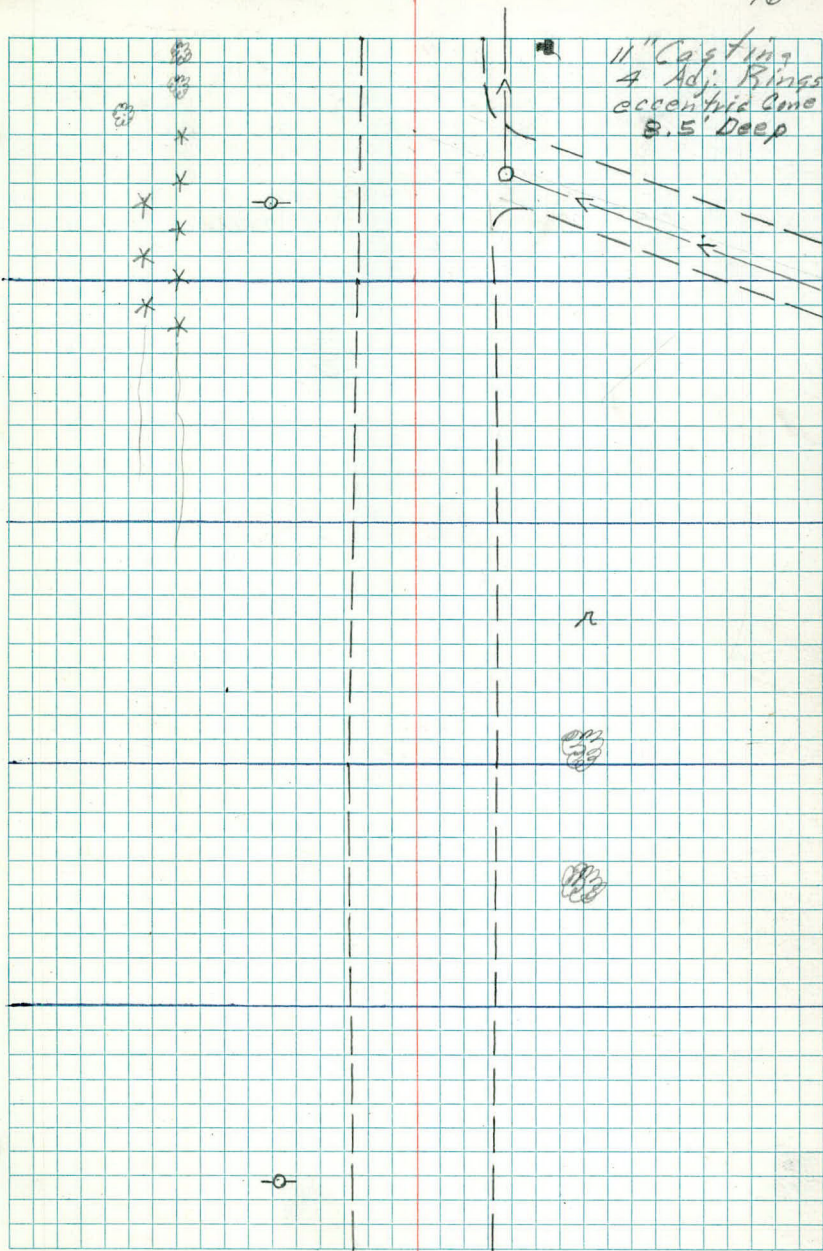
$$\begin{array}{r}
 \checkmark \text{PP} \\
 +14 \quad 29 \\
 \hline
 \end{array}$$

21

$$\begin{array}{r}
 \checkmark \\
 13 \quad 16 \\
 \hline
 \end{array}$$

Dec. 15, 1969

16



+94	$\frac{100}{33}$	$\frac{160}{54}$	+95	$\frac{Hyd}{28}$	
26	$\frac{100}{22}$	$\frac{160}{54}$	+95	$\frac{MH}{19}$	
+81	$\frac{22}{52}$	$\frac{160}{54}$	+90	$\frac{19}{51}$	
+72	$\frac{22}{52}$	$\frac{160}{54}$	+80	$\frac{31}{59}$	
+53	$\frac{31}{53}$	$\frac{160}{54}$	+60	$\frac{59}{59}$	
	$\frac{31}{53}$	$\frac{160}{54}$			
+34	$\frac{41}{57}$	$\frac{160}{54}$	+41	$\frac{180}{40}$	
+17	$\frac{41}{57}$	$\frac{160}{54}$	+20	$\frac{31}{57}$	
	$\frac{41}{57}$	$\frac{160}{54}$	+109	$\frac{21}{57}$	
+102	$\frac{31}{61}$	$\frac{160}{54}$	+06	$\frac{61}{34}$	
23	$\frac{31}{61}$	$\frac{160}{54}$	+104	$\frac{Road}{17}$	
+87	$\frac{41}{70}$	$\frac{160}{54}$	+77	$\frac{Road}{12}$	
+73	$\frac{41}{70}$	$\frac{160}{54}$	+98	$\frac{21}{57}$	
+59	$\frac{29}{29}$	$\frac{160}{54}$	+61	$\frac{57}{57}$	
+28	$\frac{21}{54}$	$\frac{160}{54}$	+37	$\frac{240}{43}$	
+12	$\frac{52}{52}$	$\frac{160}{54}$	+13	$\frac{47}{47}$	
24	$\frac{52}{52}$	$\frac{160}{54}$	+06	$\frac{59}{59}$	
+86	$\frac{58}{58}$	$\frac{160}{54}$	+81	$\frac{57}{57}$	
+67	$\frac{59}{59}$	$\frac{160}{54}$	+73	$\frac{56}{56}$	
+55	$\frac{49}{49}$	$\frac{160}{54}$	+52	$\frac{67}{67}$	

Dec. 15, 1969

17

9" Casting
13 Adj. Rings
Mex Hat

8.7 to top Main

Side Inlet Cast

7 Adj. Rings

No Cast

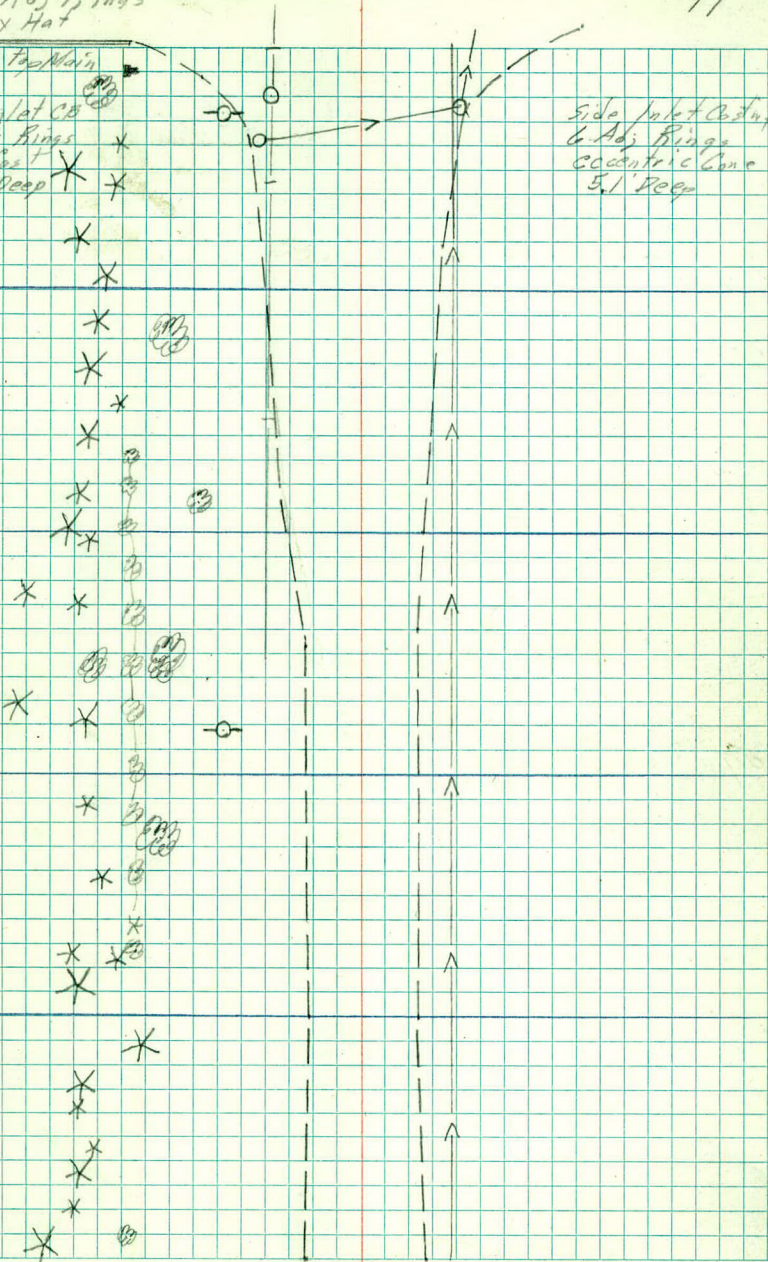
4.3' Deep

Side Inlet Cast

6 Adj. Rings

eccentric Cone

5.1' Deep



$$+50 \frac{\sqrt{\text{Cedar}}}{55}$$

$$+34 \frac{\sqrt{\text{Cedar}}}{55}$$

$$\frac{\text{Road}}{11 \sqrt{11} \sqrt{11}}$$

$$+91 \frac{\sqrt{\text{Road}}}{11}$$

$$+50 \frac{\sqrt{\text{Road}}}{15}$$

$$+79 \frac{\sqrt{\text{Road}}}{12}$$

$$+34 \frac{\sqrt{\text{Cedar}}}{53}$$

$$+41 \frac{\sqrt{\text{Road}}}{17}$$

$$+19 \frac{\sqrt{\text{Cedar}}}{53}$$

$$+100 \frac{\sqrt{\text{MH}}}{20}$$

$$\frac{\text{Road}}{23 \sqrt{20}}$$

$$+96 \frac{\sqrt{\text{Sign}}}{51}$$

$$+98 \frac{\sqrt{\text{Sign}}}{49}$$

$$+88 \frac{\sqrt{\text{POR}}}{24}$$

$$+74 \frac{\sqrt{\text{MH}}}{20}$$

$$+92 \frac{\sqrt{\text{POR}}}{21}$$

$$+82 \frac{\sqrt{\text{Cott}}}{57}$$

$$+67 \frac{\sqrt{\text{POR}}}{32}$$

$$+80 \frac{\sqrt{\text{POR}}}{25}$$

$$+78 \frac{\sqrt{\text{Cott}}}{39}$$

$$+81 \frac{\sqrt{\text{PP}}}{28}$$

$$+63 \frac{\sqrt{\text{MH}}}{28}$$

$$+71 \frac{\sqrt{\text{POR}}}{31}$$

$$+57 \frac{\sqrt{\text{POR}}}{42}$$

$$+63 \frac{\sqrt{\text{stab P.}}}{45}$$

$$+33 \frac{\sqrt{\text{5.E 6 Median}}}{50}$$

$$+62 \frac{\sqrt{\text{Curb}}}{51}$$

$$+53 \frac{\sqrt{\text{POR}}}{56}$$

$$+15 \frac{\sqrt{\text{MH}}}{43}$$

$$+106 \frac{\sqrt{\text{POR}}}{46}$$

$$+107 \frac{\sqrt{\text{MH}}}{26}$$

$$+11 \frac{\sqrt{\text{POR}}}{87}$$

$$+101 \frac{\sqrt{\text{End Curb}}}{48}$$

26

FK
KG
WJ

Dec. 16, 1969
Dec. 17, 1969 18

11" Casting
12 Adj. Rings
Mex Hat
B. 35 to Top Main

MA Buried

Tell

11" Casting
9 Adj. Rings
Mex Hat
B. 0 to Top Main

11" Casting
2 Adj. Rings
Mex Hat
13.7 Deep

31

Road
11 11

+22 $\frac{PP}{27}$

30

Road
11 11

+96 $\frac{Hyd}{31}$
 +77 $\frac{Bench}{114-126}$
 +13 $\frac{Backstop}{94}$
 +57 $\frac{Backstop}{71}$ +72 $\frac{Backstop}{83}$
 +47 $\frac{Backstop}{70}$ +35 $\frac{Cedar}{52}$
 +35 $\frac{Cedar}{57}$ +27 $\frac{Bench}{66}$
 +13 $\frac{Cedar}{46}$ +14 $\frac{Bench}{66}$
 +12 $\frac{Cedar}{58}$ +106 $\frac{Cedar}{53}$
 +96 $\frac{E. Fe}{49}$

29

Road
11 11

+53 $\frac{PP}{27}$

+51 $\frac{B. Broken down Snow Fe}{49}$

FH
KG
WJ

Dec. 18, 1969

19

—○—

GU

4

—○—

—○—

—○—

—○—

—○—

—○—

—○—

$$+20 \frac{PP}{27}$$

$$+30 \frac{ER}{10}$$

$$+18 \frac{POR}{22}$$

Road
11 11

$$+07 \frac{BR}{42}$$

33

$$+72 \frac{ER}{29}$$

$$+44 \frac{BR}{11}$$

$$+05 \frac{Backstop}{82}$$

$$+11 \frac{Road}{11}$$

$$+04 \frac{Backstop}{73}$$

32

$$+73 \frac{PP}{28} \text{ Arc Lt.}$$

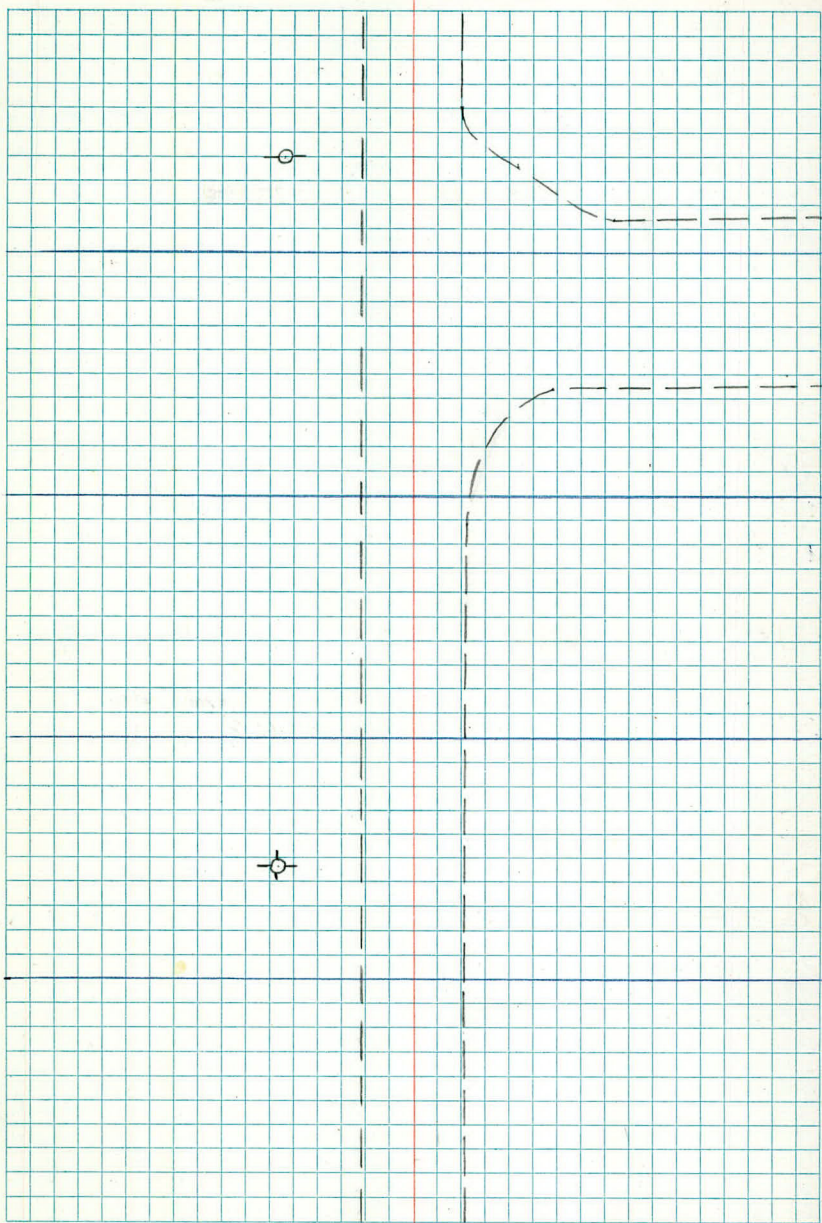
$$+91 \frac{Backstop}{39}$$

$$+81 \frac{Backstop}{58}$$

31

Dec. 18, 1969

20



36

Road
11 11

+93 NW Cor School
114

+86 8" CEH
49

+60 6" Coll
35

+47 5" Coll
40

+24 4" Coll
37

+31 5" Coll
30

+20 4" Coll
37

+1A 6" Coll
30

+16 4" Coll
31

+20 NE Cor School

+05 PP
29

35

Road
11 11

+95 School

+77 School
75

+50 N.W. Corner BRIMHALL
83 School

34

Road
11 11

+90 Hyd
32

Dec. 18, 1969

21



GV



+15 $\frac{PP}{32}$ ✓

38

Road
" "

+72 $\frac{Tw 6" CE}{67}$ ✓

37

Road
" "

+99 $\frac{Hyd}{27}$ ✓

+74 $\frac{16" CE}{37}$ ✓

+92 $\frac{PP}{32}$ ✓

+73 $\frac{8" CE}{56}$ ✓

+63 $\frac{NE Cor}{School}$

+41 $\frac{4" Ash}{46}$ ✓

+58 $\frac{Abandon}{Ent}$ ✓

+40 $\frac{12" Elm}{45}$

+24 $\frac{Lilac}{38}$ ✓

+34 $\frac{6" Ash}{38}$ ✓

36

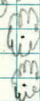
+04 $\frac{5" CE}{A7}$ ✓

Road
" " " "

Dec 18, 1969 22



GV



E

41

+92 $\frac{EK}{34}$

+85 $\frac{Hyd}{44}$

+73 $\frac{10"CE}{50}$

+93 $\frac{EK}{21}$

+70 $\frac{BR}{11}$

+80 $\frac{BR}{12}$

+63 $\frac{4"Cell}{37}$

+76 $\frac{Quint 4 "Birc}{69}$

+49 $\frac{4"MTash}{41}$

+50 $\frac{8"P}{58}$

+42 $\frac{8"P}{59}$

+36 $\frac{8"P}{63}$

+19 $\frac{NW Cor Ho}{75}$

+27 $\frac{3SE Cor Ho \checkmark}{61}$

+19 $\frac{Lilac}{58}$

+09 $\frac{EFc}{56}$

+16 $\frac{Lilac}{56}$

+19 $\frac{Mugo P \checkmark}{57}$

+00 $\frac{BFc}{56}$

$\frac{Road}{11 \ 11}$

40

+95 $\frac{12"CR}{54}$

+93 $\frac{EFc}{56}$

+92 $\frac{S.E. Cor Ga \checkmark}{61}$

+83 $\frac{Quad 8" Maple}{36}$

+84 $\frac{B. Fc}{56}$

+85 $\frac{E Ent \checkmark}{}$

+67 $\frac{E Ent}{56}$

+73 $\frac{10"Plum}{29}$

+60 $\frac{NW Cor Ga}{59}$

+50 $\frac{FC}{37}$

+55 $\frac{10"Plum \checkmark}{29}$

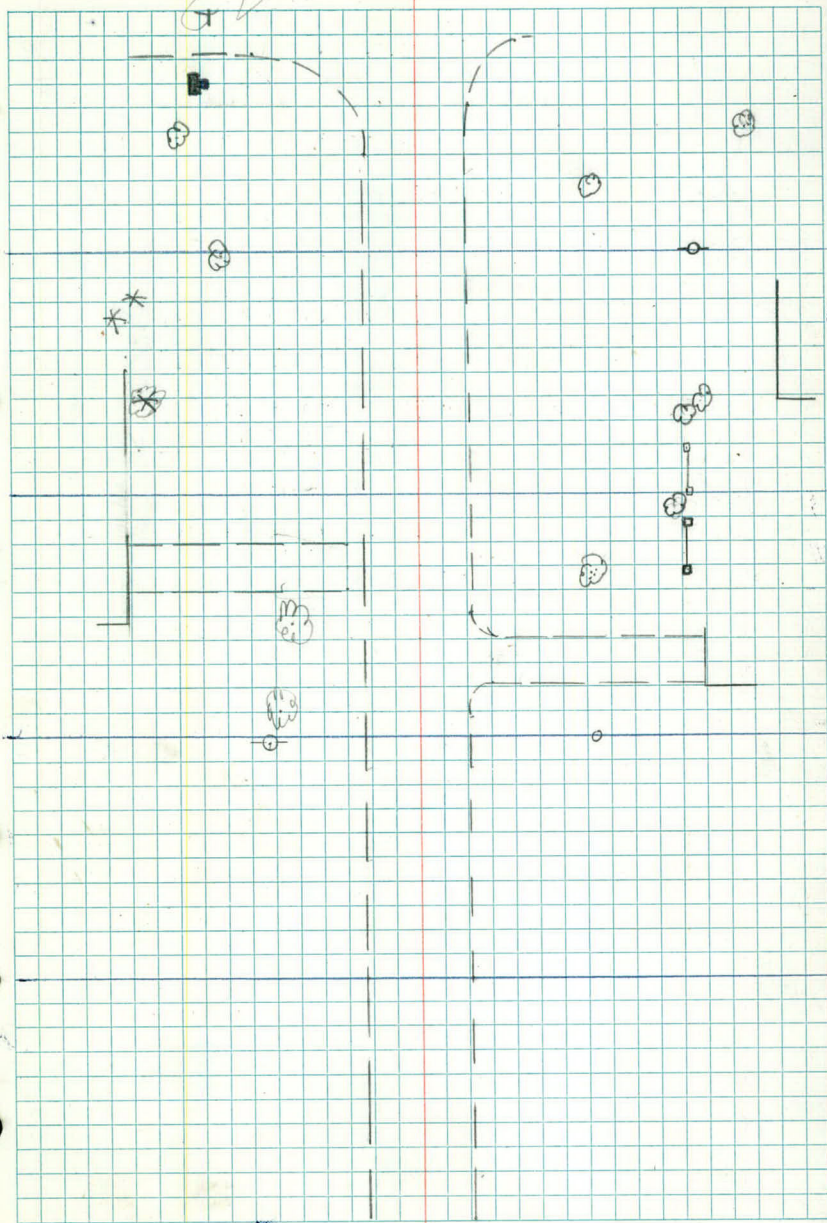
+48 $\frac{PP \checkmark}{32}$

$\frac{Road}{11 \ 11}$

39

Dec. 18, 1969

23



$$\begin{array}{r}
 +10 \quad \checkmark 12" \text{Maple} \\
 \hline
 68 \\
 43
 \end{array}
 \quad
 \begin{array}{r}
 +45 \quad \checkmark 14" \text{CEH} \\
 \hline
 52 \\
 +01 \quad \checkmark 6" \text{Birch} \\
 \hline
 42
 \end{array}
 \quad
 \begin{array}{r}
 +24 \quad \checkmark 14" \text{CEH} \\
 \hline
 58 \\
 \text{Road} \\
 \hline
 11 \quad 11
 \end{array}$$

$$\begin{array}{r}
 +94 \quad \checkmark \text{Pitch} \\
 \hline
 31
 \end{array}$$

$$\begin{array}{r}
 +71 \quad \checkmark \text{SW Cor Ga} \\
 \hline
 81 \\
 +66 \quad \checkmark \text{WE } 12" \times 33 \text{ CM} \\
 \hline
 25 \\
 +17 \quad \checkmark \text{WE } 15" \times 24 \text{ CM} \\
 \hline
 25
 \end{array}
 \quad
 \begin{array}{r}
 +82 \quad \checkmark 18" \text{Ent} \\
 \hline
 \text{Bit} \\
 +53 \quad \checkmark 2" \text{Birch} \\
 \hline
 51 \\
 +15 \quad \checkmark \text{Light} \\
 \hline
 39
 \end{array}
 \quad
 \begin{array}{r}
 +95 \quad \checkmark 4" \text{Flum} \\
 \hline
 52 \\
 +69 \quad \checkmark \text{PP} \\
 \hline
 33 \\
 +29 \quad \checkmark 17" \text{Ent} \\
 \hline
 \text{Bit}
 \end{array}$$

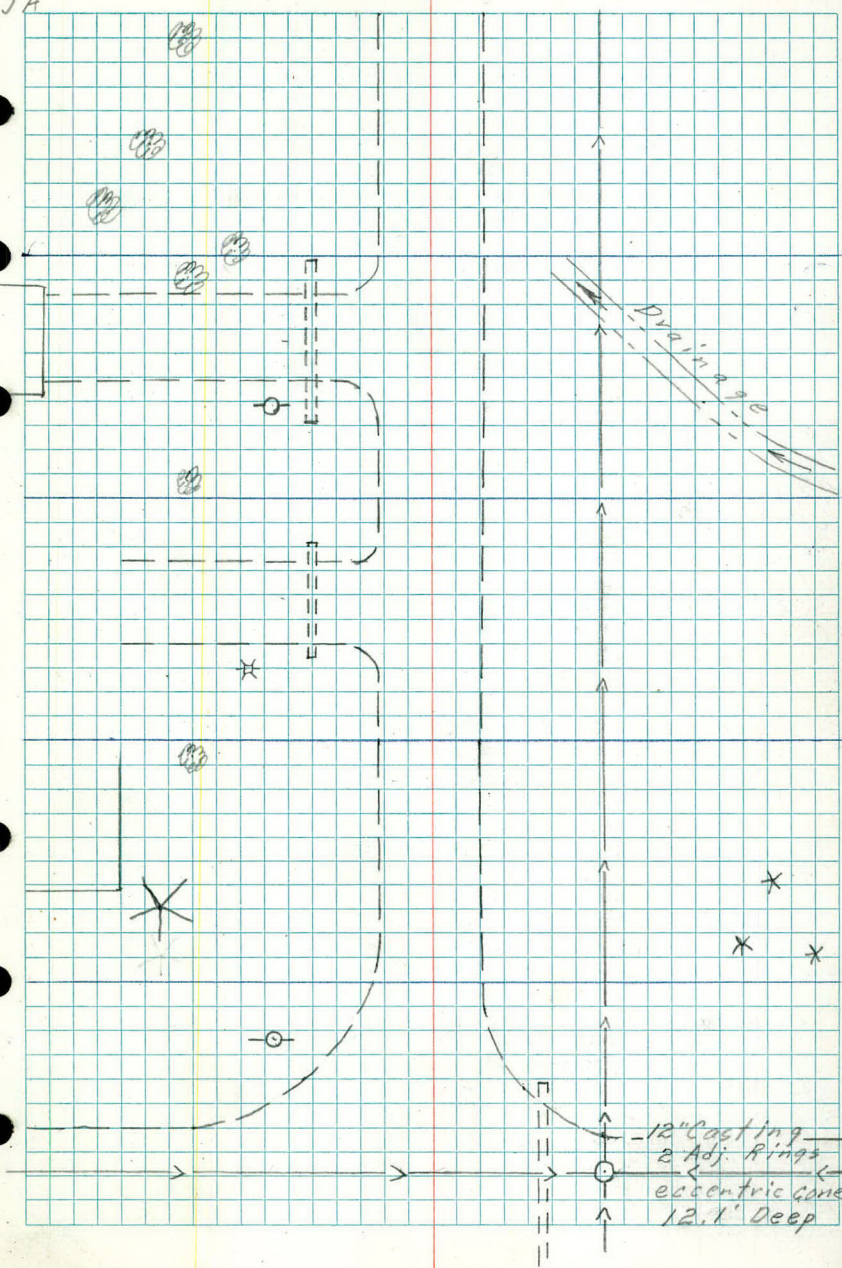
$$\begin{array}{r}
 +70 \quad \checkmark \text{Ditch} \\
 \hline
 57
 \end{array}$$

$$\begin{array}{r}
 42 \\
 \text{Road} \\
 \hline
 11 \quad 10
 \end{array}$$

$$\begin{array}{r}
 +97 \quad \checkmark \text{B" Ash} \\
 \hline
 50 \\
 +65 \quad \checkmark 10" \text{P} \\
 \hline
 57 \\
 +30 \quad \checkmark \text{POR} \\
 \hline
 27 \\
 +20 \quad \checkmark \text{BR} \\
 \hline
 50
 \end{array}
 \quad
 \begin{array}{r}
 +79 \quad \checkmark \text{SW Cor Ho} \\
 \hline
 65 \\
 +58 \quad \checkmark \text{ER} \\
 \hline
 11 \\
 +38 \quad \checkmark \text{PP} \\
 \hline
 33 \\
 +18 \quad \checkmark \text{BR} \\
 \hline
 36
 \end{array}
 \quad
 \begin{array}{r}
 +71 \quad \checkmark 1" \text{P} \\
 \hline
 71 \\
 +45 \quad \checkmark \text{ER} \\
 \hline
 11 \\
 +11 \quad \checkmark \text{MH} \\
 \hline
 36
 \end{array}
 \quad
 \begin{array}{r}
 +56 \quad \checkmark 1" \text{P} \\
 \hline
 80 \\
 +28 \quad \checkmark \text{POR} \\
 \hline
 19 \\
 +28 \quad \checkmark \text{EE. Q. 1/2} \\
 \hline
 23
 \end{array}
 \quad
 \begin{array}{r}
 +57 \quad \checkmark 1" \text{P} \\
 \hline
 64
 \end{array}$$

41

24



46

192 Car Apt

191 Ent
43-62188 12"CE
41185 10"BR
44166 WE 19" Arch
28176 8" Ash
47124 1" P
72129 1" P
62167 GV
43112 2" P
66110 2" P
80195 BR
40174 Ent
56-67160 ER
50177 MH
34123 SW Car Apt
83155 Ent
57-67155 WGV
45105 34" Will
42149 POR
23153 Hyd
43125 BR
13

15

Ent
64-54Road
11 1169 ER
13158 Arc Lt
33151 E.E 12" CM
28149 SE 12" CM
45-65147 POR
27144 10" Ent
56-67139 BR
44174 SD
23117 WGV
32112 ER
35107 S.E 12" CM
53-71129 MH
35104 W.E 12" CM
28112 Sign
51-59

44

16 11

186 2-6" Birch
51186 BR
11158 12" P
71152 SE Car Ho
73

FK
KG
WJ
JA

Dec. 4, 1969

25

Apt.

9" Casting
2 Adj. Rings
eccentric C
8.0' Deep

11" Casting
Brick Const
2.1' Deep

12" CAP

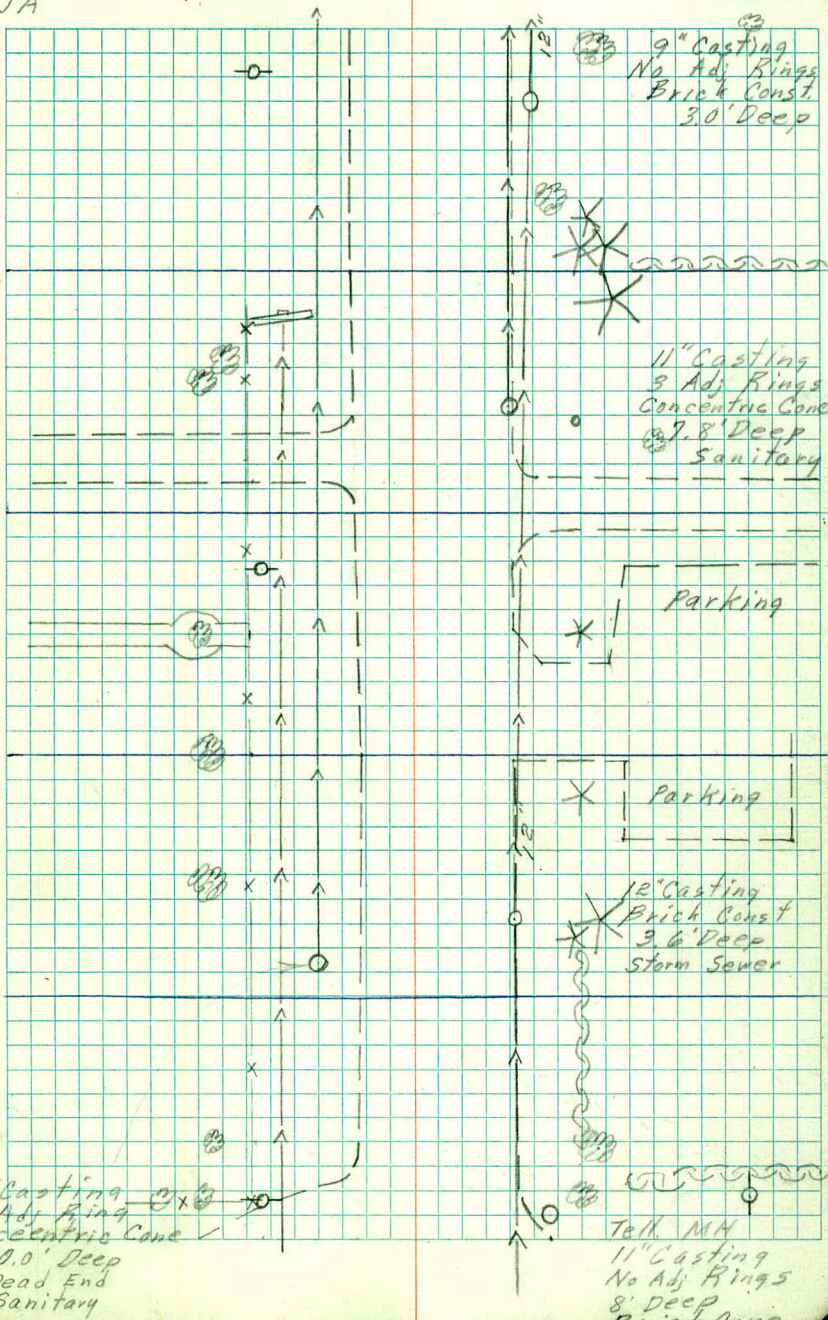
10" Casting
No Adj. Rings
eccentric Cone
9.3' Deep

			$\sqrt{8''E/m}$ $+50 \frac{71}{}$	$+49 \sqrt{NE Cor H.}$ $\frac{123}{}$
				$\sqrt{Tw 20'' Ash}$ $+46 \frac{38}{}$
	$\frac{PP}{}$ $+41 \frac{33}{}$		$\sqrt{Tw 10'' Ash}$ $+15 \frac{29}{}$	$\sqrt{S.D.}$ $+35 \frac{25}{}$
			$\sqrt{8''P}$ $+12 \frac{41}{}$	
		$\sqrt{8''P}$ $+05 \frac{45}{}$		$\sqrt{8''P}$ $+05 \frac{40}{}$
$48 \sqrt{E.E. 18'' CM}$ $+90 \frac{27}{}$		$\frac{Road}{}$ $\sqrt{13 \frac{21}{}}$	$\sqrt{B. Hedge}$ $+02 \frac{50}{}$	
		$\sqrt{Row 4'' Ash}$ $+89 \frac{38}{}$		
	$\sqrt{End Wall}$ $+91 \frac{21}{}$		$\sqrt{16''P}$ $+94 \frac{42}{}$	
$\sqrt{Fe Cor}$ $+88 \frac{35}{}$	$\sqrt{End Wall}$ $+88 \frac{35}{}$		$\sqrt{NW Cor H.}$ $+54 \frac{12015}{}$	
	$\sqrt{22'' LP}$ $+81 \frac{39}{}$		$\sqrt{Tw 2'' Birch}$ $+64 \frac{51}{}$	$\sqrt{3'' Maple}$ $+64 \frac{44}{}$
$\sqrt{\pm Ent 10' CR.}$ $+62 \frac{32}{}$	$\sqrt{22'' LP}$ $+78 \frac{43}{}$		$\sqrt{MH}$ $+72 \frac{20}{}$	
	$\sqrt{NE Cor School}$ $+55 \frac{84}{}$	$\sqrt{\pm 11' C.R.}$ $+52 \frac{Ent}{}$		$\sqrt{W.S.O.}$ $+69 \frac{34}{}$
$\sqrt{28'' Ash}$ $+25 \frac{43}{}$	$\sqrt{PP}$ $+38 \frac{32}{}$	$\sqrt{Cor. Ent}$ $+26 \frac{21}{}$	$\sqrt{Cor. Parking}$ $+89 \frac{44}{}$	
	$\sqrt{\pm 5' Walk}$ $+25 \frac{34}{}$		$\sqrt{3''P}$ $+25 \frac{35}{}$	
			$\sqrt{Ent B.t}$ $+18 \frac{29-41}{}$	
47	$\sqrt{24'' Ash}$ $+00 \frac{42}{}$	$\sqrt{Fe Road}$ $+34 \frac{11}{}$		
			$\sqrt{B. Ent}$ $+99 \frac{21-44}{}$	$\sqrt{4''P}$ $+92 \frac{35}{}$
		$\sqrt{Cor. Parking}$ $+82 \frac{44-79}{}$		
			$\sqrt{S.D.}$ $+66 \frac{21}{}$	
		$\sqrt{8'' Pine}$ $+61 \frac{34}{}$		$\sqrt{10'' Pine}$ $+67 \frac{39}{}$
			$\sqrt{End Hedge}$ $+58 \frac{34}{}$	
	$\sqrt{28'' Ash}$ $+73 \frac{42}{}$	$\sqrt{B. Hedge}$ $+19 \frac{35}{}$		$\sqrt{NW Cor Apt}$ $+32 \frac{92}{}$
$\sqrt{16'' Ash}$ $+18 \frac{42}{}$	$\sqrt{MH}$ $+57 \frac{20}{}$		$\sqrt{16'' Elm}$ $+18 \frac{38}{}$	
	$\sqrt{PP}$ $+07 \frac{33}{}$	$\sqrt{PP}$ $+08 \frac{70}{}$	$\sqrt{ER}$ $+11 \frac{22}{}$	$\sqrt{N.E. Hedge}$ $+11 \frac{44}{}$
$\sqrt{Row 4'' Ash}$ $+05 \frac{44}{}$	$\sqrt{Fe Cor}$ $+07 \frac{34}{}$		$\sqrt{Tw 8'' Maple}$ $+08 \frac{35}{}$	
46	$\sqrt{\pm Ent}$ $+00 \frac{32}{}$	$\frac{Road}{}$ $+12 \frac{28}{}$		$\sqrt{MH}$ $+05 \frac{28}{}$

FK
HG
JA

Dec. 3, 1969

26



Road
13 20

51

+77 Cor Parking
45 CR

+73 E.E 15' CM
27

+62 24" Ash
52

+46 PP
33

+19 8" Ash
42

+61 E, Fe
29

+51 12" Ash
30

+26 2" Ent
Dirt

+143 12" Ash
30

+154 20" Ash
57

+63 12" Elm
34

+55 Tw 8" Ash
44

+16 12" Maple
35

+14 6" Ash
35

+143 12" Ash
30

+140 26" Maple
55

+101 18" Elm
67

50

Road
12 18

+77 22" Elm
39

+91 4" P
33

+86 3" P
32

+74 3" P
31

+56 33 Ash
58

+62 10" BFE
33

+55 BFE
29

+45 PP
34

+39 WGV
22

+29 2" 10' Ent
CR

+50 WGV
20

+53 Tw 6" Ash
41

+45 12" Elm
55

+44 Hyd
31

+14 26" E
55

+11 SW Cor Stand
46 6x8

+47 S.D
23

+46 WGV
33

+33 Edge
Parking

49

Road
13 21

+79 NW Cor Ho
100+

+84 14" Ash
55

+73 Edge
Parking

+73 NW Cor Apt
126

+70 6" P
42

+65 6" P
42

+57 MH
20

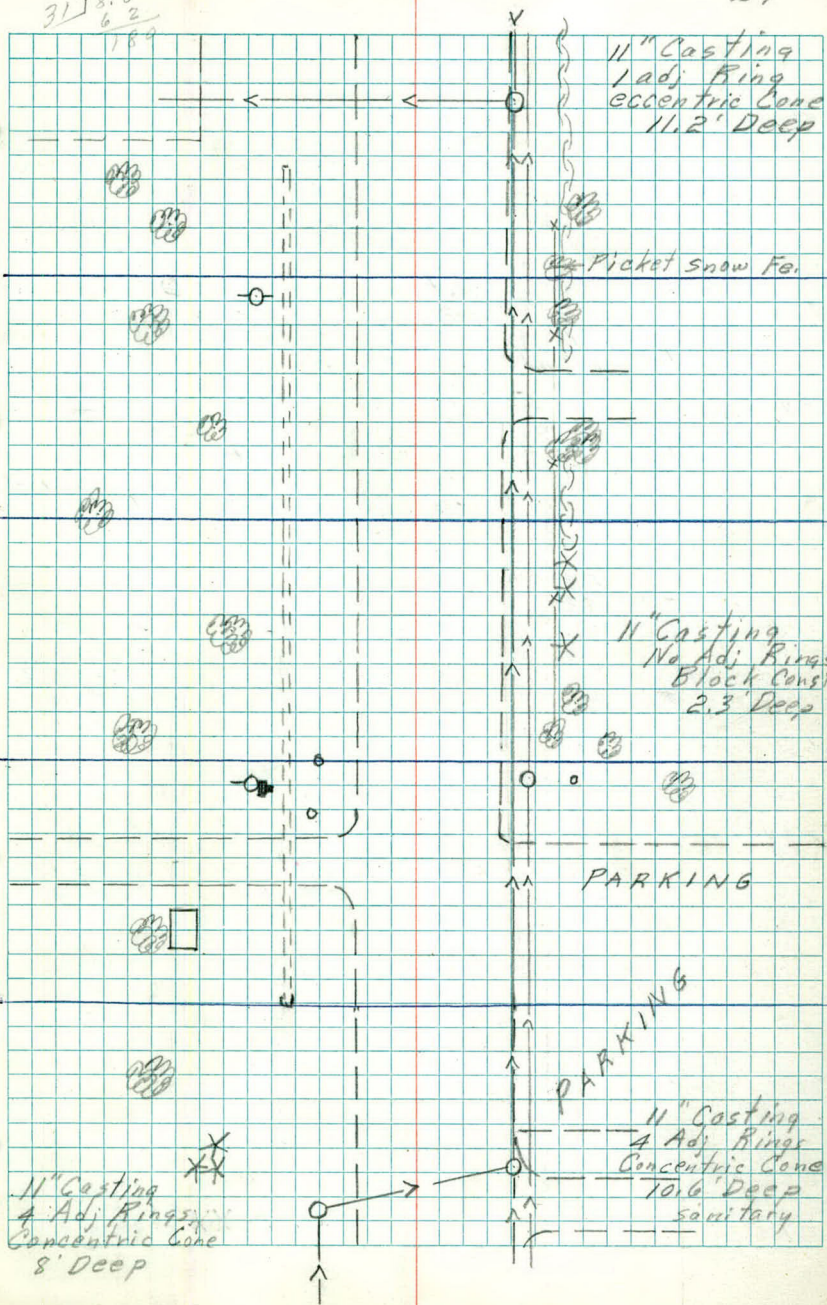
+66 MH
21

+58 2" 11' CR
Ent

Dec. 3, 1969

27

2.6
31) 8.0
6 2
180



+04 W. Edge
SBL

+01 E. Med
E

53
+90 POR 34 +95 ER 43-45 +88 GP 45 +82 C.C. 30 +83 SD 109 +89 CC 30
+64 BRC 67 +68 POR 35 +80 POR 29 +86 Pullbox 5, GKP 52 +90 PP 45
+27 R. He +52 MH 13 +62 POR 45 +94 CC 17 +81 SwCo. Control 51 - 57.5 x 4'
+27 ER 45 +28 BR 69 +32 ER 73 +87 POR 39 +94 CC 57 +93 F.R 46
+23 POR 24 +32 POR 32 +33 POR 42 +74 Bois M 1 +73 POR 51 +94 PP 45
+22 Arclt 39 +24 Arclt 41 +24 Sign 38 +37 ER 83 +69 BR 68
+19 BRC 28 +76 E.E. 18" SPAN 43 +19 PP 36 +40 BR 77
+83 CC 30 +18 CorC 34-24 +95 CC 60 +27 FeCor 34 +36 ER 40
+14 SD 28 +194 CC 18 +109 Pumps 80-108 +21 Pull Box 28 +12 CB 26 old Notes
52 +82 S.E. Cor Sta 86 +92 ER 21 +21 Fe 34 +21 BR 24
+96 Cor Conc 22 +96 ER 26 +96 Cor Conc 33 +85 BRC 26
+58 W.E. 18" 55 +81 Cor Conc 33 +93 BR 22 +69 MH 20 +77 E 12' Em Bit
+45 B. Bit 18 +54 Cor Conc 33 +57 Cor Conc 34 +65 Cor Ent 21
+22 Cor Conc 33 +43 Cor Conc 16 +34 STP 33 +40 14' EW Conc Slab 36-52
+20 Sign 35 +20 Cor Park 46 +33 6" Ash 45 +33 Fe Cor 34
+06 W.E. 18" SPAN CM 27 +108 Cor Conc 16 +26 3" P 50 +28 6" Ash 40
+102 Hyd 31 +102 WGV 28 +403 Trip 8" Apple 69

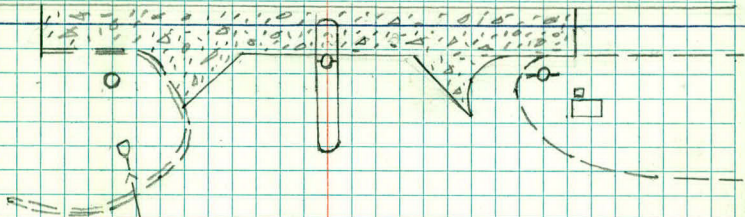
FK
AG
WJ
JA

Dec. 4, 1969

28

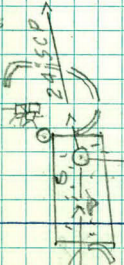
S. B. L.

T.H. No 51

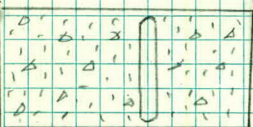


○ Tell

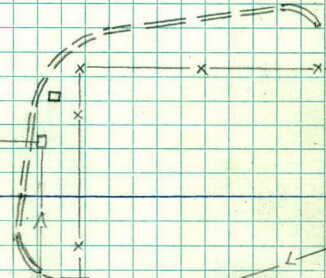
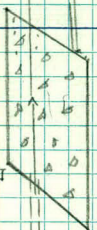
6" Casting
No Adj. Rings
Poured Conc
3.5' Deep



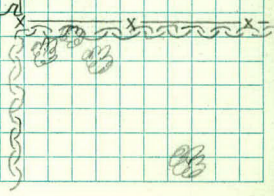
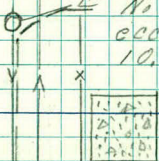
12" DEEP



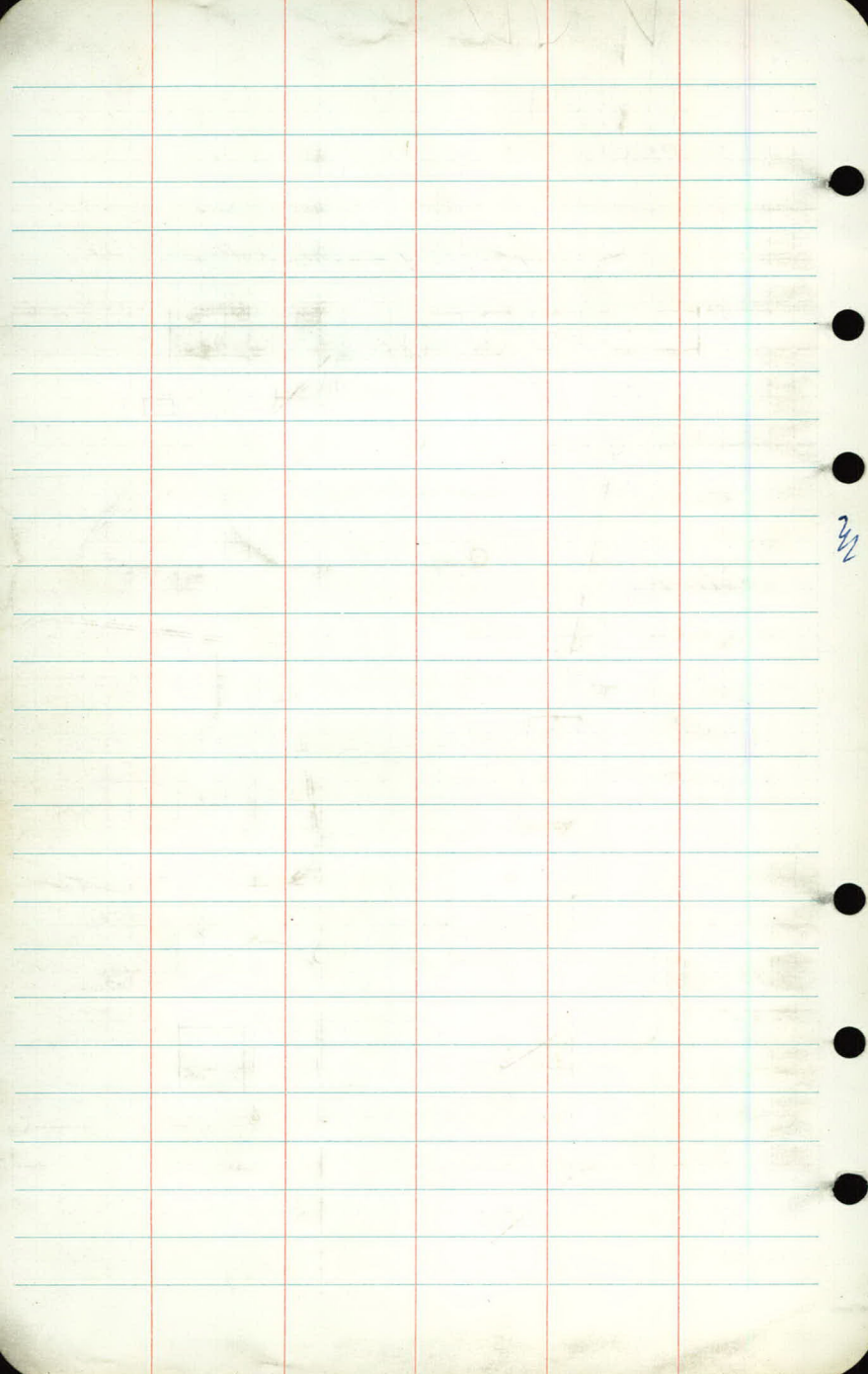
serv. Sta



12" Casting
No Adj. Rings
eccentric Cone
10.5' Deep



BB



FK
DS
CM

Oct. 29, 1969

29

BENCH LEVELS

Sta	+	π	-	Elev.	Corrected Elevations
BM	4.72	970.26			(965.54)
BM			1.72	968.54	53
BM	5.69	974.75	1.20	969.06	06
BM	10.15	984.83	0.07	974.68	66 ✓
BM	0.71	984.90	0.64	984.19	17 ✓
BM	5.72	980.35	10.27	974.63	60 ✓
BM	5.00	983.97	1.38	978.97	94 ✓
BM	3.35	982.27	5.05	978.92	88
BM	1.05	979.05	4.27	978.00	96
BM	2.85	971.56	10.34	968.71	67
BM	3.94	971.51	3.94	967.62	(967.57)
TP	2.48	967.95	6.04	965.47	
BM	0.93	965.54	3.34	964.61	(964.61) ✓
BM	1.56	962.37	4.73	960.81	✓
BM	4.92	962.36	4.93	957.44	(957.44)
BM	4.71	965.52	1.55	960.81	(960.81) ✓
BM	3.25	967.87	0.90	964.62	
TP	5.19	970.67	2.39	965.48	
BM			3.10	967.57	(967.57)
BM			2.00	968.67	

Oct 29, 1969

30

FK H
DS T
CM +

Roseville B.M. # 140 at School 623

Top Hyd by West Ent. to FAIRVIEW Junior High

Top Hyd N.W. Corner Parking Lot " " "

Top Hyd by East Ent. to FAIRVIEW JUNIOR HIGH

Top Hyd by Ent. to Corpus Christi School

Top Hyd N.W. Corner Fairview & "B"

Top Hyd by West backstop

Top Hyd S.E. Corner Ent to BRIMHALL SCHOOL

Top Hyd Left Sta 37+00

Top Hyd NW Corner Midlothian Rd

Roseville B.M. # 142 SW Corner " " & "B"

Rock E. Side Ent. North

Top Hyd S.W. Corner Fry & Co. Rd. "B"

Top Hyd Lt. Sta 49+50±

Top Hyd N.W. Corner Snelling & "B"

Top Hyd Lt Sta 49+50±

Top Hyd S.W. Corner Fry & Co Rd "B"

Rock E. Side Ent North

Roseville BM # 142 SW Cor. Midlothian

Top Hyd NW Corner Midlothian Road

Sta	+	-	Elev	Corrected Elevations
BM	11.24	978.81		(967.57)
BM			10.14	968.67 (968.67)
BM	3.84	981.80	0.85	977.96 (977.96)
BM	5.75	984.64	2.91	978.89 (978.88)
BM	1.65	980.60	5.69	978.95 (978.94)
BM	10.39	985.00	5.99	974.61 (974.60)
BM	0.20	984.38	0.82	984.18 (984.17) 11-10-69
BM	0.04	974.72	9.70	974.68 (974.66)
BM	1.52	970.61	5.63	969.09 (969.06)
BM	9.82	5	2.04	968.57 (968.53)
BM	12.81	978.35	5.05	965.56 (965.54)
T.P.	11.18	989.01	0.52	977.83
BM		96	7.42	981.59
BM	0.16	979.80	9.37	979.64
BM	6.34	979.76	6.38	973.42 (973.41)
BM	9.35	989.00	0.11	979.65 (979.64)
BM			7.37	981.63 (981.60)
TP	0.42	978.27	11.15	977.85 (977.83) 3.72 984.60
BM		977	9.72	968.55 (968.53)
BM		978	12.71	965.56 (965.54)

FK 121
DS π
CM $\dagger$

26

Nov. 7, 1969

31

also Nov. 10, 1969

Midlothian

Top Roseville BM #142 S.W. Corner

Top Hyd NW Corner Midlothian & B

Top Hyd Lt. Sta 37+00

Top Hyd SE corner Ent. to BRIMHALL School

Top Hyd by West Backstop

Top Hyd NW Corner Fairview & "B"

Top Hyd by Ent. to Corpus Christi School

Top Hyd by East Ent. to FAIRVIEW JUNIOR HIGH

Top Hyd by N.W. Corner Parking Lot " " "

Top Hyd by West Entrance to " " "

Roseville B.M. # 140

Sta 10 £

Top Hyd Rt Sta 9+90±

Top Hyd by Ho # 2008

Top Hyd S.E. Corner Cleveland & "B"

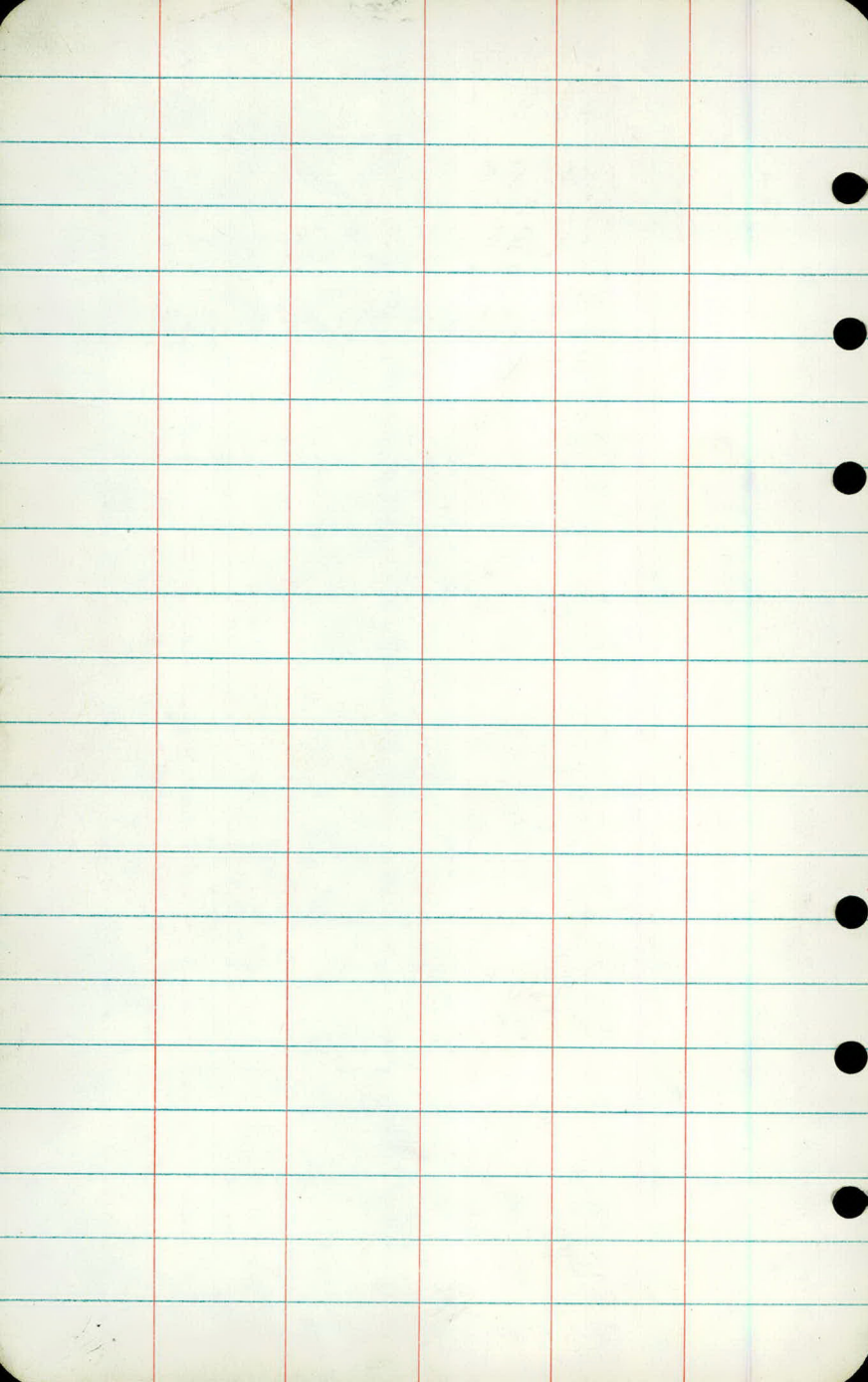
Top Hyd by Ho # 2008

Top Hyd Rt Sta 9+90±

Sta 10 £

Top Hyd by West Ent. to FAIRVIEW JUNIOR HIGH

Roseville B.M. # 140



FK
KG

Dec. 22, 1969

32

X-Sections

Sta	+	π	-	Elev.
BM	1.99	975.40		973.41

0+12

+22

0+00

+40

BM	1.79	975.20	1.99	973.41
----	------	--------	------	--------

+60

+85

FKW
KGT
KPT

LT

Dec. 22, 1969
Dec. 23, 1970

33

Top Hyd S.E. Corner Cleveland + "B"

70.77	71.0	70.7	71.4	71.5	71.75	71.8	72.1	72.1	72.2
4.63	4.40	4.17	4.0	3.9	3.65	3.6	3.3	3.3	3.2
100	80	60	50	25		25	50	75	100

conc

69.9	70.7	71.3	71.3	71.31	71.6	71.75	71.9	72.0	72.1
5.5	4.7	4.1	4.1	4.09	3.8	3.65	3.5	3.4	3.3
100	75	50	25	21	MH	MH	50	75	75

MH 24

71.0	71.20	71.44	71.7	71.9	72.1	72.3	72.3	72.4
4.4+	4.20	3.96	3.7	3.5	3.3	3.1	3.1	3.0
100	80	60	30		25	50	75	100

69.1	70.3	70.9	71.2	71.4	71.6	71.4	71.3	71.1	70.3	69.9
6.3	5.1	4.5	4.2	4.0	3.8	4.0	4.1	4.3	5.1	5.5
75	45	31	21	14		12	21	29	42	58

69.3	70.1	70.6	71.1	71.2	71.5	71.2	71.0	69.6	69.6
5.9	5.1	4.6	4.1	4.0	3.7	4.0	4.2	5.7	5.6
75	53	39	30	18		15	25	38	62

69.3	70.3	70.8	71.1	71.3	70.9	70.8	69.1	69.0	69.6
5.7	4.9	4.4	4.1	3.9	4.3	4.4	6.1	6.2	5.6
90	59	38	17		15	22	34	45	52

Sta + π - Elev.

975.20

1 ϕ Service Lane Lt.

+12

✓

+42

✓

+62

TP 5.28 975.63 4.85 970.35 2+00

Lt

Dec. 23, 1969

BT 34

69.3	69.8	70.4	70.9	71.2	70.8	70.8	69.4	68.6	67.9	66.1
5.9	5.4	4.8	4.3	4.0	4.4	4.4	5.8	6.6	7.9	8.8
100	77	49	23		14	20	32	43	60	79

69.3	69.8	70.5	70.8	71.0	70.67	70.7	69.7	67.7
5.9	5.4	4.7	4.4	4.2	4.53	4.5	5.5	7.5
91	64	26	20		16	21	28	42

MM

64.7	65.1
10.5	10.1
29	59

66.1	67.7	69.5	70.4	70.5	70.7	70.5	70.4	68.8	66.9	64.2
9.1	7.5	5.7	4.8	4.7	4.5	4.7	4.8	6.4	8.3	11.0
75	49	34	22	15		15	19	27	36	45

62.2	62.8
130	124
76	56

67.3	66.1	67.5	67.7	69.3	70.3	70.6	70.2	70.2	69.5	67.3	63.2	61.5
7.9	9.1	7.7	7.5	5.9	4.9	4.6	5.0	5.0	5.7	7.9	12.0	13.7
67	60	47	28	17			13	20	25	32	45	62

61.5
13.7
83

Sta + π - Elev.

975.63

2+00

✓ 1493 Top 24" SCP 51' 24 12.74

2+23

✓ +60

FX
KG
CM

LT

✓

Dec. 23, 1969

RT

35

68.5 69.8 70.0 70.2 70.3 70.2 70.0 70.0 66.1
7.1 5.8 5.6 5.4 5.3 5.4 5.6 5.6 9.5
33 24 21 13 13 17 21 30

66.7 68.3 69.6 68.4 68.4 68.1 68.5 62.39 Top
8.9 11.3 12.0 11.2 14.2 14.5 13.1 13.24
40 46 55 75 75 51 46 50
Top 24
Sep

68.7 68.1 69.4 69.9 70.2 70.3 70.2 69.8 69.8 68.4
6.9 7.5 6.2 5.7 5.4 5.3 5.4 5.8 5.8 10.2
34 30 21 18 10 11 18 21 32

67.2 68.6 67.9 68.3 68.5 62.4
8.4 7.0 7.7 14.3 14.1 13.2
46 55 75 75 58 46

69.4 69.9 69.9 70.1 70.4 70.5 70.2 70.0 69.8 66.5 63.9
6.2 5.7 5.7 5.5 5.2 5.1 5.4 5.6 5.8 9.1 11.7
32 26 21 19 11 12 18 25 31 45

66.9 68.7 68.5 68.5 68.5 68.5 68.5 68.5 68.5 68.5
6.7 6.9 7.1 14.1 13.6
49 67 75 75 58

Sta + π - Elev

975.63

2+90

✓

T.P. 5.95 976.96 4.62 971.01 \$ 3+00

3

30

60

65

✓

+30

✓

L.T.

L

R.T.

36

69.9 70.4 70.7 70.8 70.8 70.7 70.6 69.5 69.7

5.7 5.2 4.9 4.8 4.8 4.9 5.0 6.1 9.9
30 25 19 12 ✓ 12 18 23 36

70.1 70.2 70.3

5.5 5.4 5.3
32 51 75

72.1 73.3

13.2 12.3
75 51

70.8 70.9 70.9 71.0 71.0 71.0 70.9 69.6 67.6 66.0

6.2 6.1 6.1 6.0 6.0 6.0 6.1 7.4 9.4 11.0
32 25 20 11 ✓ 12 17 24 31 44

70.8 70.8 70.7

6.2 6.2 6.3
42 63 75

63.3 64.1

13.7 12.9
75 58

72.0 72.1 71.7 71.7 71.8 71.8 71.8 71.7 72.1 72.2

5.0 4.9 5.3 5.3 5.2 5.2 5.2 5.3 4.9 4.8
32 28 23 20 11 ✓ 12 18 26 31

71.9 71.5

5.1 5.5
48 75

72.9 73.0 72.7

4.1 4.0 4.3
75 66 52

Sta + π - Elev

976.96

3+60

✓

+88

✓

4

✓

TP 8.59 983.05 2.50 974.46 sta 42

Dec. 23, 1969

37

Lt

L

Rt

71.9	72.3	72.5	72.8	72.9	72.8	72.7	72.7	72.5
5.1	4.7	4.5	4.2	4.1	4.2	4.3	4.3	4.5
32	23	20	11	✓	12	20	25	45

72.2	71.8	73.0	72.6
4.8	5.2	4.0	4.4
51	75	75	68

71.9	73.2	73.9	73.9	74.0	73.9	74.1	73.3	73.1	73.6
5.1	3.8	3.1	3.1	3.0	3.1	2.9	3.7	3.9	3.4
29	23	16	11	✓	12	18	29	51	75

71.7	71.6	71.5
5.3	5.4	5.5
33	57	75

74.02
294
Garage
Floor 82

73.1	74.1	74.4	74.5	74.4	74.6	72.4	72.1
3.9	2.9	2.6	2.50	2.6	2.4	4.6	4.9
27	19	11	✓	10	16	21	27

71.8	71.6	71.1	70.9	73.9	73.7	73.0	72.5
5.2	5.4	5.9	6.1	3.1	3.3	4.0	4.5
31	38	62	75	75	69	52	31

Ho

Sta	+	π	-	Elev.
-----	---	-------	---	-------

		983.05		
--	--	--------	--	--

4+50				
------	--	--	--	--

✓				
---	--	--	--	--

+80				
-----	--	--	--	--

✓				
---	--	--	--	--

5	Ent	Lt.		
---	-----	-----	--	--

✓				
---	--	--	--	--

BM	676	986.40	3.41	979.64 (979.64)
----	-----	--------	------	-----------------

Dec. 23, 1969

38

Lt.

Lt.

Rt.

75.7

75.9

76.2

76.5

76.7

76.6

76.6

75.4

74.1

7.3

7.1

6.8

6.5

6.3

6.4

6.4

7.6

8.9

25

23

17

12

✓

12

18

21

27

72.7

70.9

70.3

73.8

73.9

73.7

10.3

12.1

12.7

9.2

9.1

9.3

34

52

75

75

65

46

77.4

77.3

77.6

77.6

77.8

77.9

77.9

76.7

76.1

75.2

5.6

5.7

5.4

5.4

5.2

5.1

5.1

6.3

6.9

7.8

27

20

16

11

✓

12

16

21

23

34

74.5

72.2

72.2

71.2

73.6

74.1

8.5

9.8

10.8

11.8

9.4

8.9

46

52

65

77

75

53

77.7

76.6

78.6

78.8

78.8

78.8

78.7

78.3

78.2

78.3

5.3

4.6

4.4

4.2

4.2

4.2

4.3

4.7

4.8

4.7

42

20

17

12

✓

12

15

18

21

28

77.2

76.6

74.8

76.2

78.1

5.8

6.4

8.2

6.8

4.9

65

100

75

52

38

Top Hyd Rt.

Sta + π - Elev.

986.40

5+39

✓

+57

39

57

✓

6

✓

Dec. 23, 1969

39

Lt

♀

R1

80.4	79.8	80.1	80.3	80.3	80.2	80.2	80.0	81.1
6.0	6.6	6.3	6.1	6.1	6.2	6.2	6.4	5.3
25	22	18	13	✓	11	15	20	36

80.7	80.6	82.3	82.1	82.2		82.5	82.0
5.7	1.8	3.1	3.3	3.2		3.9	4.4
27	37	48	64	75		79	56

80.6	80.7	80.8	80.9	80.8	80.8	80.5	81.1
5.8	5.7	5.6	5.5	5.6	5.6	5.9	5.3
22	17	13	✓	12	16	21	33

81.1	83.9	83.8	82.2	82.3		82.5	82.0
5.3	2.5	2.6	3.2	3.1		3.9	4.4
26	35	38	58	75		75	52

82.1	81.6	81.8	81.9	82.0	81.8	81.6	81.3	81.5
4.3	4.8	4.6	4.5	4.4	4.6	4.8	5.1	4.9
24	19	15	11	✓	12	15	18	24

85.1	84.9	82.9	81.7	82.87	82.7	82.6	82.0
1.3	1.5	3.5	4.7	2.53	3.7	3.8	4.4
33	36	55	75	House walk	75	66	42

Sta + π - Elev.

986.40

6+37

27

65

85

✓
T.P. 7.94 992.46 1.88 984.52

+65 Ent Lt

✓

+85 Ent Ry

✓

PK
PK
KG
CM

Lt.

Dec 23, 1969

Dec 24, 1969

40

82.9	82.6	82.9	82.9	83.0	82.7	82.7	82.5	82.1
3.5	3.8	3.5	3.5	3.4	3.7	3.7	3.9	4.3
26	20	16	12	✓	11	15	17	24

84.9	84.9	82.4	80.4		82.6	82.3	82.2
1.5	1.5	4.0	6.0		3.8	4.1	4.2
34	40	57	75		75	53	35

Spike in Arc Light Pole Lt.

85.5	84.3	84.0	83.9	83.9	83.9	83.9	83.6	84.1
7.0	8.2	8.5	8.6	8.6	8.6	8.6	8.9	8.4
42	25	20	12	✓	12	16	26	48

86.5	86.8	87.4					84.6
6.0	5.7	5.1					2.9
59	78	100					75

86.7	84.9	84.2	84.3	84.2	84.2	84.1	84.6	85.1	85.7
5.8	7.6	8.3	8.2	8.3	8.3	8.4	7.9	7.4	6.1
31	25	18	12	✓	12	19	40	57	75

86.7	87.2	86.9	87.2
5.8	5.3	5.6	5.3
35	48	64	75

Sta + π - Elev.

992.46

7+00

✓

+38

✓

+74

✓

TP 0.58 988.43 4.57 987.89 (987.85)

Dec. 24, 1969

11

2

PH

41

84.2	84.1	84.3	84.4	84.4	84.4	84.4	84.2	84.5
83	84	82	81	81	81	81	83	80
22	20	16	11	✓	12	16	26	39

87.3	87.9	87.8	87.8		85.7	85.8
52	46	47	47		6.8	6.7
32	51	67	75		75	65

Ent

87.8	84.4	83.7	84.3	84.5	84.5	84.5	84.3	84.2	84.0	84.6
47	8.1	8.8	8.2	8.0	8.0	8.0	8.2	8.3	8.5	7.9
32	23	20	17	11	✓	12	16	20	27	46

88.9	90.4	89.3	89.2		85.6
36	21	32	33		6.9
37	49	65	75		75

87.7	84.6	83.7	84.2	84.3	84.1	83.73	83.7	84.0
48	79	8.8	8.3	8.3	8.4	8.73	8.8	8.5
33	24	21	11	✓	12	20	26	36

MH

88.2	84.3	86.9	87.3		85.1	84.9	84.3
43	42	56	52		7.4	7.6	8.2
39	46	58	75		75	62	49

Ent

stake

Sta + π - Elev

988.43

8+00 Ent Rt.

✓

+28

✓

+68

✓

BM	2.97	984.57	6.82	981.61	(981.60)
BM	8.21	987.85		979.64	Hyd
TP			3.33	984.52	Ave Lt.
TP	0.92	988.77	0.00	987.85	Stage
			10.91	977.86	10 E
BM			7.14	981.63	981.60 Hyd

FK
KG
CM

Dec. 29, 1969

FK	KG	CM	FK	KG	CM	FK	KG	CM
84.7	83.6	83.0	83.6	83.7	83.6	83.2	83.5	83.8
37	48	54	48	4.7	48	5.2	4.9	4.6
33	25	20	12	✓	12	19	28	46

84.6	84.5	83.1	83.9	84.2
38	39	33	45	42
44	61	75	75	67

82.4	82.3	82.1	82.9	83.1	83.0	82.6	82.6	81.8
6.0	6.1	6.3	5.5	5.3	5.4	5.8	5.8	6.6
25	23	19	11	✓	10	16	19	29

82.7	82.8	83.2	83.7	81.2	81.4	81.6	82.0	81.9
5.7	5.6	5.2	4.7	7.2	7.0	6.8	6.4	6.5
31	40	65	75	75	69	54	43	37

81.3	81.1	81.1	82.0	82.1	81.9	81.7	81.1	81.4
7.1	7.3	7.3	6.4	6.3	6.5	6.7	7.3	7.0
25	22	18	11	✓	9	14	18	23

81.5	82.0	82.5	83.3	83.9	83.0	83.0	82.6
6.9	6.4	5.9	5.1	4.9	5.4	5.4	5.8
34	46	64	75	75	56	49	35

Top Hyd St Sta 9+90 =

{ check

Sta + π - Elev.

984.57

9+00

✓
+45 Ent Lt

✓
+65 Ent Rt

Dec 29 1969

43

LT	LT	LT	LT	LT	LT	LT	LT	LT
80.8	80.2	80.6	81.2	81.3	81.1	80.9	80.5	80.4
3.8	4.4	4.0	3.4	3.3	3.5	3.7	4.1	4.2
25	21	18	11	✓	10	15	19	23

81.2	81.2	80.9	81.2	82.0	83.8	82.8	82.7	81.3	80.6
3.6	3.4	3.7	3.4	2.6	0.8	1.8	1.9	3.3	4.0
31	36	45	65	75	75	51	43	28	25

79.4	79.5	79.7	79.8	79.8	79.8	79.6	79.5	79.1	79.6
5.2	5.1	4.9	4.8	4.8	4.8	5.0	5.1	5.5	5.0
29	20	15	11	✓	11	15	17	19	24

79.8	80.3	81.5	82.1	81.9	82.1	81.8	81.1
4.8	4.3	3.1	2.5	2.7	2.5	2.8	3.5
41	58	75	75	63	51	41	32

Ent

78.9	78.3	78.7	79.0	79.1	79.0	79.0	79.5	80.4
5.7	6.3	5.9	5.6	5.5	5.6	5.6	5.1	4.2
25	21	17	11	✓	10	16	24	37

79.7	79.8	80.9	80.9	80.6	81.5	81.3	81.3	80.9
4.9	4.8	4.6	3.7	4.0	3.1	3.3	3.3	3.7
30	38	46	54	60	75	75	62	51

Sta + π - Elev.

984.57

10

✓

BM 0.15 981.75 2.97 981.60

+50

✓

11

Ent Rt.

✓

TP 4.57 976.32 10.00 971.75

Dec. 23, 1969

44

78.0	76.7	77.3	77.6	77.9	77.8	77.7	77.2	76.8
66	79	73	70	6.7	6.8	6.9	74	7.8
26	21	17	11	✓	9	14	18	23
78.4	77.9	77.4	77.1	76.7	77.8	77.3	77.3	77.2
62	6.7	72	75	79	6.8	21	21	74
35	46	56	67	78	75	60	46	33
76.3	75.4	75.3	75.5	75.8	76.1	76.0	75.9	75.1
55	64	65	63	60	5.7	58	5.9	6.7
28	24	22	18	12	✓	10	15	18
75.4	74.6	73.5	71.4		77.0	76.3	75.7	
64	72	8.3	10.4		4.8	5.3	6.1	
34	43	55	75		75	61	44	
73.5	73.4	73.6	74.2	74.3	74.1	74.1	74.0	74.1
8.3	8.4	8.2	76	7.5	7.7	7.7	7.8	7.7
25	21	19	13	✓	10	14	19	32
73.5	72.7	71.3	69.5					76.3
8.3	9.1	10.5	12.3					5.5
33	44	58	75					78

White stake

Sta + π - Elev

976.32

11 + 50

✓

+85

Ent Rt.

✓

12

✓

Dec. 29, 1969 RT. 45

Lt.

70.8	70.9	71.3	72.0	72.3	72.1	71.9	71.0	71.2
5.5	5.4	5.0	4.3	4.0	4.2	4.4	5.3	5.1
24	21	18	12	✓	12	15	20	26

70.5	69.9	68.5	68.1	73.8	73.3	72.3	71.6
5.8	6.4	7.8	8.2	2.5	3.0	4.0	4.7
32	46	62	75	75	56	43	33

69.6	69.8	70.0	70.6	70.9	70.8	70.8	71.1	71.8
6.7	6.5	6.3	5.7	5.4	5.5	5.5	5.2	4.5
25	21	19	13	✓	10	16	23	41

69.0	68.5	68.9	73.4	73.2	72.7
7.3	2.8	7.4	0.90	3.1	3.6
39	54	75	Garage	75	64

68.0	69.2	69.1	69.5	70.1	70.3	70.3	70.2	69.6	69.0	69.3
7.3	7.1	7.2	6.8	6.2	6.0	6.0	6.1	6.7	7.3	7.0
28	24	22	19	12	✓	10	13	17	20	22

68.4	67.9	68.4	69.4	72.9	72.1	71.7	71.2	70.2
7.9	8.4	2.9	7.3	3.4	4.2	4.6	5.1	6.1
37	49	60	75	75	56	43	32	27

Sta + π - Elev.

976.32

12+50

✓

+70

✓

+85

✓

BM 1.86 970.39 7.76 968.56 (968.53)

Dec. 29, 1969

46

Lt.

L

Rt.

66.9	67.9	67.8	68.2	68.4	68.1	67.7	68.3	67.1	67.6
94	84	85	81	79	82	86	80	92	87
26	22	19	13	✓	10	15	19	22	26

66.6	66.3	66.0	67.5	67.6	72.2	70.9	70.1	69.0
9.7	10.0	10.3	8.8	8.7	41	54	62	73
30	41	49	59	75	75	53	40	32

66.1	66.3	66.5	67.0	67.5	67.7	67.3	67.0	66.6	67.2	66.5
10.2	10.0	9.8	9.3	8.8	8.6	9.0	9.3	9.7	9.1	9.8
31	26	22	18	12	✓	11	15	19	22	24

65.9	66.4	67.5	67.4	67.5	70.5	70.4	69.4	68.9	68.0	67.0
10.4	9.9	8.8	8.9	8.8	5.8	5.9	6.9	7.4	8.3	9.3
41	48	58	70	75	75	63	50	43	34	28

66.1	67.2	66.7	67.0	66.9	67.2	66.9	66.7	66.2	66.1	66.2
10.2	9.1	9.6	9.3	9.4	9.1	9.4	9.6	10.1	10.2	10.1
25	21	18	12	15	✓	13	17	20	25	30

65.9	65.8	66.5	67.1	67.1	69.5	68.7	67.2
10.4	10.5	9.8	9.2	9.2	6.8	7.6	9.1
30	41	49	63	75	75	58	42

Top Hyd W. Ent Fairview Junior High

Sta + π - Elev

970.39

13+00

✓

+11

Buried

+18

✓

+40

✓

Dec. 29, 1969

47

51

63.9	66.7	66.2	66.6	66.8	66.5	66.3	65.4	66.1
4.5	3.7	4.2	3.8	3.6	3.9	4.1	4.96	4.3
23	21	18	12	✓	10	16	21	28

CB

65.7	65.4	66.8	66.5	68.2	67.4	66.8
4.7	5.0	3.6	3.9	2.2	3.0	3.6
27	40	57	75	75	59	43

65.9	65.85	66.1	66.2	66.3	66.1	65.9	65.6	65.5
4.5	4.54	4.3	4.2	4.1	4.3	4.5	4.8	4.9
21	18	12	9	✓	11	16	21	28

MH

66.5	65.2	66.1	66.0	66.1	66.4	66.0	65.5
3.9	5.2	5.2	4.3	4.4	4.3	4.0	4.9
24	32	39	55	68	75	75	64

64.8	65.0	65.2	65.4	65.7	65.9	65.7	65.6	65.1	65.4
5.6	5.4	5.2	5.0	4.7	4.5	4.7	4.8	5.3	5.0
33	25	22	18	12	✓	13	18	22	33

65.0	65.9	65.8	66.2	66.1	65.7
5.4	4.5	4.6	4.2	4.3	4.7
37	57	75	75	65	49

Sta + π - Elev.

970.39

13+70 Curb Line Rt

✓

BM 2.56 971.09 1.86 968.53 (968.53)

+95 Curb Line Rt

✓

14

29

54

✓

FX
KG
CM

LT

Dec. 30, 1969

RT

48

65.1	64.6	64.9	65.3	65.3	65.4	65.2	64.9	65.37
5.3	5.8	5.5	5.1	4.9	5.0	5.2	5.5	5.02
27	23	19	13	✓	10	17	27	36

Curb

64.4	65.4	66.2	66.4	66.36	66.09	65.86	65.58
6.0	5.0	4.2	4.0	4.03	4.30	4.53	4.81
34	50	69	75	100	83	69	52

Top Hyd by W. Ent

Curb

64.5	64.2	64.3	65.0	65.3	65.2	64.8	65.28	65.37
6.5	6.9	6.8	6.1	5.8	5.9	6.3	5.81	5.72
35	28	23	13	✓	12	21	34	42

Curb

65.3	66.2	66.3		66.30	65.83	65.60
5.8	4.9	4.8		4.79	5.26	5.49
50	65	75		100	69	56

64.7	64.1	64.3	65.0	65.3	65.1	64.9	65.4	65.6
6.7	7.0	6.8	6.1	5.8	6.0	6.2	5.7	5.5
36	29	23	13	✓	12	21	31	49

65.3	66.1	66.2		66.1	65.9
5.8	5.0	4.9		5.0	5.2
51	64	75		75	62

Sta + π - Elev.

971.09

14+27

✓

+54

✓

BM 1.42 969.95 2.55 968.54 (968.53)

+94 MH 8' Lt 5.19 964.76

+96 S.D. 31' Rt 5.76 964.19

15

FX
DS
CM

Dec. 30, 1969
Jan 13, 1970
RT.

49

Lt.

6 ^{3.7}	6 ^{4.0}	6 ^{4.1}	6 ^{4.7}	6 ^{5.1}	6 ^{4.9}	6 ^{4.7}	6 ^{4.8}	6 ^{4.8}
7.4	7.1	7.0	6.4	6.0	6.2	6.4	6.3	6.3
32	26	22	12	✓	12	19	24	29

6 ^{4.6}	6 ^{5.9}	6 ^{6.2}	6 ^{5.8}	6 ^{5.4}	6 ^{5.1}	6 ^{4.8}
6.5	5.2	4.9	5.3	5.7	6.0	6.3
48	62	75	75	59	47	36

6 ^{3.9}	6 ^{3.2}	6 ^{4.0}	6 ^{4.7}	6 ^{5.1}	6 ^{4.8}	6 ^{3.9}	6 ^{4.6}	6 ^{4.7}
7.2	7.7	7.1	6.4	6.1	6.3	7.6	6.5	6.4
28	21	18	12	✓	12	21	23	27
CB						CB		

6 ^{3.8}	6 ^{5.1}	6 ^{5.8}	6 ^{5.4}	6 ^{4.8}	6 ^{4.7}
7.3	6.0	5.3	5.7	6.3	6.4
36	53	75	75	54	38

Top Hyd By West Ent to Fairview J. High

6 ^{3.4}	6 ^{3.8}	6 ^{4.5}	6 ^{4.8}	6 ^{5.1}	6 ^{5.0}	6 ^{4.8}	6 ^{4.6}	6 ^{4.1}
6.5	6.1	5.4	5.1	4.8	4.9	5.1	5.3	5.8
52	35	21	12	✓	10	18	27	32

6 ^{3.6}	6 ^{5.2}	6 ^{5.1}	6 ^{4.9}
6.3	4.7	4.8	5.0
75	75	66	45

Sta + π - Elev.

969.95

15 + 50

✓

16

16

✓

+50

✓

B.M. 5.79 974.85 0.91 969.04 (969.06)

Jan. 13, 1970 50

LT

RT

6 ^{4.2}	6 ^{4.2}	6 ^{4.6}	6 ^{5.1}	6 ^{5.3}	6 ^{5.3}	6 ^{5.0}	6 ^{5.4}	6 ^{5.1}
5.7	5.7	5.3	4.8	4.6	4.6	4.9	4.5	4.5
36	28	20	13		10	18	31	56

6 ^{4.2}	6 ^{4.6}
5.7	5.3
54	75

6 ^{5.5}
4.4
75

6 ^{4.6}	6 ^{4.8}	6 ^{4.7}	6 ^{4.9}	6 ^{5.3}	6 ^{5.3}	6 ^{5.2}	6 ^{4.8}	6 ^{5.2}
5.3	5.1	5.2	5.0	4.6	4.6	4.7	5.1	4.7
36	29	22	13		10	17	26	34

6 ^{4.6}	6 ^{5.3}
5.3	4.6
50	75

6 ^{5.6}	6 ^{5.4}
4.3	4.5
75	59

6 ^{4.5}	6 ^{4.9}	6 ^{5.0}	6 ^{5.1}	6 ^{5.4}	6 ^{5.4}	6 ^{5.3}	6 ^{5.3}	6 ^{5.7}
5.1	5.0	4.9	4.8	4.5	4.5	4.6	4.6	4.2
46	31	23	13		10	19	28	44

6 ^{5.3}	6 ^{5.4}
4.4	3.5
62	75

6 ^{5.9}
4.0
75

Top Hyd N.W. Corner Parking Lot

Sta + π - Elev.

974.85

17

16+99 MH 24' Rt. 9.42 965.43

16+98 MH 42' Rt. 8.02 66.83

✓

17+35 CB 21' Lt. 10.22 964.63

+35 CB 21' Rt. 9.44 965.41

+50

✓

+76

✓

17+99 Top Curb 24' Rt. 7.60 967.25

Jan. 13, 1970

51

LT

2

RT

6 ^{5.3}	6 ^{5.3}	6 ^{5.4}	6 ^{5.6}	6 ^{5.6}	6 ^{5.5}	6 ^{5.2}	6 ^{5.8}
9.5	9.3	9.4	9.2	9.2	9.3	8.6	8.0
32	23	13		10	19	28	44

6 ^{5.9}	6 ^{7.0}
8.9	7.8
48	75

6 ^{6.9}
7.9
75

6 ^{6.4}	6 ^{5.9}	6 ^{5.4}	6 ^{5.8}	6 ^{6.1}	6 ^{6.0}	6 ^{5.7}	6 ^{5.9}	6 ^{6.8}
8.4	8.9	9.4	9.0	8.7	8.8	9.1	8.9	7.9
42	31	22	14		10	20	6	0
								32

6 ^{6.9}	6 ^{7.3}
7.9	7.5
59	75

6 ^{6.4}	6 ^{6.3}	6 ^{6.3}	6 ^{7.1}
8.4	8.5	8.5	7.6
75	52	6	0
41			

6 ^{6.6}	6 ^{7.0}	6 ^{5.7}	6 ^{6.1}	6 ^{6.3}	6 ^{6.2}	6 ^{5.8}	6 ^{6.1}	6 ^{6.6}
8.2	7.8	9.1	8.7	8.5	8.6	9.0	8.7	8.2
47	33	23	13		9	20	30	39
								6

6 ^{7.0}	6 ^{7.1}
7.8	7.7
62	75

6 ^{6.7}	6 ^{6.5}	6 ^{6.6}	6 ^{7.2}	6 ^{7.8}
8.1	8.3	8.2	7.5	7.6
75	56	6	0	0
45				39

Sta + π - Elev.

974.85

18

+01 C.B 21' RT 8.76 966.09

✓

BM 2.19 976.85 0.17 974.68 (974.66)

+50

✓

19

✓

+15 Top Carb 6.11 970.74
24' RT.

Jan 13, 1970 52
RT.

11.

66.5	66.4	66.2	66.3	66.5	66.5	66.5	67.5	67.5
8.4	8.5	8.7	8.6	8.4	8.4	8.4	2.4	2.4
37	31	21	13	10	19	40	59	

66.9	67.1	67.4
8.0	7.8	7.5
59	75	75

Tap Hyd. by East Entrance

66.2	67.5	67.0	67.3	67.6	67.6	67.5	67.4	67.4
10.7	9.4	9.9	9.6	9.3	9.3	9.4	9.5	8.5
35	27	21	13	10	17	23	34	

66.4	66.4	67.7	67.7	67.7
10.5	10.5	8.2	8.2	8.2
57	75	75	63	43

67.2	67.0	68.6	69.1	69.3	69.3	69.2	70.1	70.1
9.7	8.9	8.3	7.8	7.6	7.6	7.7	6.8	6.8
29	23	19	13	10	18	27	41	

67.0	67.3	67.3	70.9	70.55	70.0	70.1
9.9	9.6	9.6	6.0	6.30	6.9	6.8
38	57	75	75	6	6	58

71

Sta + π - Elev.

976.85

19+31

✓

+46 Ent Rt

✓

+67

✓

BM 5.37 980.03 2.19 974.66

Jan. 13, 1970

53

11.

RT

68.2	68.4	70.0	70.2	70.5	70.5	70.3	70.6	71.20
8.7	8.0	6.9	6.7	6.4	6.4	6.6	6.3	5.65
30	23	18	13	✓	10	27	G	C
								33

67.6	68.4	67.4	66.5	71.1	71.0	70.9	71.33	71.31
9.3	8.5	9.5	10.4	5.8	5.9	6.0	5.53	5.54
39	45	68	75	75	66	G	C	43
							49	C

68.3	68.1	70.4	70.7	71.0	71.0	70.6	70.6	71.1
8.6	7.8	6.5	6.2	5.9	5.9	6.3	6.3	5.8
35	25	18	13	✓	10	25	37	54

68.1	67.8	66.8					71.13
7.8	9.1	10.1					5.6
45	71	75					75

67.9	71.1	70.5	71.6	71.4	71.9	71.4	71.5	71.64
7.0	5.8	6.4	5.3	5.0	5.0	5.5	5.4	5.21
42	29	22	13	✓	10	21	27	C
							G	27

68.0	68.1	66.3		72.8	72.9	72.1
8.9	8.8	10.6		3.1	4.0	4.8
60	68	75		75	59	42

Top Hyd by East Ent to Fairview Junior High School

Sta + π - Elev

980.03

20

✓

+50

✓

21

✓

TP

8.73 985.77 2.99 977.04

FX
DS
WT
CM

Jan. 13, 1970

54

11

2

RT

71.3

71.1

72.3

72.9

73.1

72.0

72.7

72.8

73.6

8.7

8.9

7.7

7.1

6.9

7.0

7.3

7.2

6.4

39

27

18

12

9

17

29

50

69.0

68.6

66.0

76.8

74.3

11.0

11.4

14.0

4.2

5.7

52

65

75

100

67

73.4

73.9

74.4

74.9

75.1

75.1

74.8

75.0

76.0

6.6

6.1

5.6

5.1

4.9

4.9

5.2

5.0

4.0

32

24

19

13

10

17

25

29

73.0

70.2

69.8

65.9

76.3

76.9

76.6

7.0

7.8

10.2

14.1

1.7

3.1

3.4

43

53

61

75

100

67

51

76.1

76.0

76.4

77.1

77.0

77.0

76.8

76.3

78.0

3.9

4.0

3.3

2.9

3.0

3.0

3.2

3.7

2.0

42

29

18

12

9

16

23

33

74.2

71.3

67.9

74.2

78.6

78.5

78.3

5.8

8.7

12.1

0.8

1.4

1.5

1.7

48

59

75

100

77

67

49

Sta 21 2

Sta + π - Elev

985.77

21 + 50

✓

22

✓

+50

FK
DS
LPO
WJ
CM

Jan 15, 1970

5.5

Lt

2

Rt

77.6	77.5	78.0	77.9	78.6	78.7	78.7	78.5	78.5	78.5	80.6
8.2	8.3	7.8	7.9	7.2	7.1	7.1	7.3	7.3	7.3	5.3
45	35	28	20	12		9	15	23	26	30

→ 12.8
13.0 14.8
65 75

✓

80.6 80.7 81.2 81.0
5.2 5.1 4.6 3.8
100 75 59 42

78.5	78.8	79.5	79.7	79.8	79.8	79.4	79.0	81.0	83.5
7.3	7.0	6.3	6.1	6.0	6.0	6.4	6.8	4.8	2.3
34	24	19	13		9	15	23	28	36

→ 78.8 77.1 73.7
7.0 8.7 12.1
49 61 75

✓

82.6 82.6 83.9
3.2 3.2 1.9
100 82 57

79.8	79.4	80.1	80.2	80.2	80.4	80.4	80.2	80.3	83.1
6.0	6.4	5.7	5.6	5.6	5.4	5.4	5.6	5.5	2.7
52	33	23	18	12		10	15	23	37

→ 78.9 77.8
6.9 8.0
66 75

✓

83.4 83.3 83.0
2.4 2.5 2.8
100 82 64

Sta.

+

π

-

Elev.

985.77

23+00

+22'

+50

Jan 15, 1970

56

L7

R7

80.5	80.4	80.9	80.9	80.6	80.6	80.7	81.0 ¹²	81.4	81.5
5.3	5.4	5.4	5.4	5.2	5.2	5.1	4.8	3.1	3.3
29	23	19	12		10	17	25	49	80

80.1	79.6	78.6
5.7	6.2	7.3
39	62	75

82.8
3.0
100

79.8	79.6	80.2	80.4	80.5	80.7	80.7	80.6 ¹⁴	80.7	Profile	81.3	82.3
6.0	6.2	5.6	5.4	5.3	5.1	5.1	5.13	ENT.	→	4.5	3.5
39	28	22	18	11		10	19	M.H.		39	89

79.3	79.1
6.5	6.7
59	75

84.5	83.4	82.4
1.3	2.4	3.4
200	150	110

79.2	79.2	79.9	80.2	80.3	80.6	80.6	80.6	81.3	82.7	83.0
6.6	6.6	5.9	5.6	5.5	5.2	5.2	5.2	4.5	3.1	2.8
42	30	23	19	11		10	16	23	47	68

78.1	75.5
7.7	10.3
57	75

84.0	83.5
1.8	2.3
100	85

Sta.	+	π	-	Elev.
------	---	-------	---	-------

		985.77		
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24+00				
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+50				
-----	--	--	--	--

25+00				
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✓ BM	1.57	985.74	1.57	984.20	984.17
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T.P.	2.73	982.69	5.81	979.96	
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Jan 15, 1970

LT

♂

Rt

57

74.9 ^{15.4}	75.8	78.1	79.4	79.6	80.0	80.1	80.1	80.7	81.6	82.5
11.4	10.0	7.7	6.4	6.2	5.8	5.7	5.7	5.1	4.2	3.3
53	39	28	19	12		11	18	27	44	68

12.4
13.4
75

83.3
82.9
2.5 2.9
100 86

73.8	75.8	77.4	78.0	78.6	78.8	78.9	78.4	79.2	80.1	80.5
12.0	10.0	8.4	7.8	7.2	7.0	6.9	7.4	6.6	5.7	5.3
41	31	24	18	10		12	19	29	50	71

12.5
12.0
13.3 13.8
60 75

81.0
4.8
100

72.4	75.5	76.0	76.4	76.6	76.9	78.0	76.6	75.1	77.9	78.2
13.4	10.3	9.8	9.4	9.2	8.9	8.8	9.2	10.7	7.9	7.6
34	27	23	18	14		11	19	33	55	84

71.0
71.2
70.0
14.8 14.6 15.8
44 64 75

78.5
7.3
100

24+00 ♂

Sta + π - Elev.

982.69

25+40

✓

+81

✓

+88

✓

B.M. 4.82 979.42 8.06 974.63 (974.60)

FX
DS
WJ
CM

Jan. 26, 1970

58

11.8	14.8	15.4	15.4	15.6	15.7	15.8	14.8	14.0	15.6
109	79	73	73	71	20	23	8.3	8.7	71
32	25	19	14		12	20	26	33	49

10.0	19.6	18.3
12.7	13.2	14.4
46	66	75

16.3
6.4
75

11.8	12.1	13.2	13.6	13.9	14.4	14.2	14.2	13.7	13.5
10.9	10.0	9.42	9.1	8.8	8.3	8.5	8.5	9.0	9.2
48	30	23	20	14		12	16	23	37
		CB							

19.9	19.9
12.8	13.3
67	75

14.2	13.9
8.5	8.8
75	64

12.7	13.4	13.8	13.4	13.7	14.3	14.0	13.9	13.14	13.6	14.2
10.0	9.3	9.3	9.28	9.0	8.4	8.7	8.8	8.95	9.1	8.5
46	30	22	MH	14		11	17	23	28	49
			19					CB		

10.3
12.4
75

13.4
8.9
75

Top Hyd N.W. Corner Fairview & B"

Sta + π - Elev

979.42

26+00

+07[?]

MH 25' RT

5.88 973.54

+15

+33

$\pm$ Fairview

+50

+62

✓

Jan. 26, 1970

59

LT

RT

12.79	13.10	13.2	13.1	13.6	13.9	3.8	13.1	13.6	14.2	14.0
6.63	6.32	6.2	6.3	5.8	5.5	5.6	5.7	5.8	5.2	5.4
75	48	39	27	14		12	23	33	53	75
Curb										

12.5	12.7	12.91	13.1	13.6	13.8	13.1	13.1	13.5	13.4
6.9	6.7	6.51	6.3	5.8	5.6	5.7	5.7	5.9	6.0
75	62	MH	30	13		12	29	59	75
41									

13.31	13.02	13.1	13.3	13.1	13.6	13.7	13.1	13.6	13.6	13.4
6.06	5.80	6.3	6.1	5.7	5.8	5.7	5.7	5.8	5.8	6.0
75	50	50	36	12		12	33	62	75	100
Median										

12.8	12.8	12.9	13.6	13.6	13.6	13.7	13.9	13.3	13.2
6.6	6.6	6.5	5.8	5.8	5.8	5.7	6.1	6.1	6.2
75	62	36	12		11	27	52		75

13.11	12.6	12.7	13.0	13.4	13.7	13.6	13.5	13.24	13.2
6.31	6.8	6.7	6.4	6.0	5.7	5.8	5.9	6.18	6.2
51	50	39	25	12		12	25	28	38
Curb									
								MH	

12.53
6.59
75

13.0
6.4
75

13.6
5.8
60

Sta	+	π	-	Elev
-----	---	-------	---	------

		979.42		
--	--	--------	--	--

26+75				
-------	--	--	--	--

✓				
---	--	--	--	--

27				
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✓				
---	--	--	--	--

+50				
-----	--	--	--	--

✓				
---	--	--	--	--

TP	5.97	981.09	4.30	975.12
----	------	--------	------	--------

Jan 26, 1970

Lt.

A

At

60

^{12.1} 6.7	^{13.0} 6.4	^{13.3} 6.1	^{13.6} 5.8	^{13.6} 5.8	¹⁴ 5.6	^{13.6} 5.8	^{13.5} 5.9	^{13.4} 6.0	^{12.4} 7.0	^{13.2} 6.2
33	27	20	12	65		11	22	27	36	45

^{11.9} 7.5	^{11.2} 8.2	^{10.6} 8.8		^{13.1} 5.7	^{13.6} 5.8
48	64	75		75	65

^{12.9} 6.5	^{14.1} 5.3	^{13.6} 5.77	^{13.9} 5.5	^{14.1} 5.3	^{13.9} 5.5	^{13.7} 5.7	^{12.4} 7.0	^{12.3} 7.1
27	23	21	10		10	20	26	32
		MH						

^{10.5} 8.9	^{10.9} 8.5		^{14.3} 5.1	^{14.2} 5.2	^{13.5} 5.9
42	75		75	51	40

^{11.1} 7.7	^{12.1} 6.7	^{13.6} 5.8	^{14.3} 5.1	^{14.4} 5.0	^{14.6} 4.8	^{14.5} 4.9	^{14.4} 5.0	^{13.1} 6.3	^{12.7} 6.7
37	28	24	17	10		10	14	23	28

^{11.5} 7.9	^{11.4} 8.0		^{15.1} 4.3	^{14.9} 4.6	^{13.4} 6.0
60	75		75	57	39

~~28100~~

Sta + π - Elev

981.09

28+00

✓

+50

✓

29

✓

LT

Jan 26, 1970

RT

61

12.4	14.2	14.5	14.7	14.9	13.1	14.9	14.5	15.0	13.4	13.4
8.7	6.9	6.6	6.4	6.2	6.0	6.2	6.6	6.1	7.7	6.8
28	24	18	12	10		10	16	23	34	43

11.4	11.1	11.6
9.5	10.0	9.5
42	59	75

15.4	15.4
5.7	5.7
75	61

11.5	12.0	12.6	14.4	15.2	15.1	15.4	15.1	15.3	14.1	14.0
9.6	9.1	8.5	6.7	5.9	5.4	5.7	6.0	5.8	7.0	7.1
75	49	34	26	13		9	16	21	25	32

15.4	15.6	15.1
5.3	5.5	6.0
75	66	46

12.0	13.2	12.3	15.8	16.2	16.0	15.4	15.1	14.6	16.1
9.1	7.9	6.8	5.3	4.9	5.1	5.7	5.4	6.5	5.0
46	31	21	10		12	22	33	36	51

11.9	11.9
9.2	9.3
63	75

16.3
4.6
75

Sta + π - Elev.

981.09

29+50

30

✓

BM 3.69 982.66 2.16 978.93 (978.97)

+50

✓

31

EX
DS
LPD
GA
CM

LT

Jan. 26, 1970
March 5, 1970 Rt 62

11.1	13.3	14.0	14.1	16.4	16.9	16.6	16.1	16.9	17.0	17.1
94	78	71	64	47	43	46	50	52	41	34
75	45	30	22	11		11	22	35	49	75

12.2	13.4	15.6	15.4	16.8	17.2	17.0	16.4	16.9	17.3	17.1
89	77	55	57	43	39	41	47	42	38	34
47	34	26	21	12		11	21	29	43	65

12.1	12.5	17.9
8.5	8.6	3.2
65	75	75

Top Hyd by backstop (West)

14.4	15.4	16.3	17.0	17.4	17.6	17.5	17.4	17.0	18.0	18.5
83	73	64	57	53	51	52	53	57	47	42
37	26	20	15	10		10	14	18	33	36

13.8	12.4	11.9	18.5	17.5
8.9	10.3	10.8	42	42
50	63	75	75	62

17.1	16.7	16.8	17.3	17.8	17.9	17.7	17.7	17.5	18.4	18.6
56	60	59	54	49	48	50	50	52	43	41
38	28	21	17	10		10	15	18	32	48

16.9	15.2	13.4	19.0	19.0
58	75	93	37	37
48	60	75	75	68

Sta + π - Elev.

982.66

31+50

✓

32

✓

+35

✓

March 5, 1970

Lt

E

Rt 63

77.6	77.2	77.7	77.8	79.1	78.0	78.0	77.8	78.1
5.1	5.5	5.0	4.9	4.6	4.7	4.7	4.9	4.0
29	22	15	10		10	15	18	31

78.5	78.3	76.5	72.8	80.4	80.3	79.7	78.8
4.2	4.4	6.2	9.9	2.3	2.4	3.0	3.9
39	46	57	75	75	72	55	42

77.2	77.3	77.7	77.9	78.1	77.9	77.9	77.7	78.7
5.4	5.4	5.0	4.8	4.6	4.8	4.8	5.0	4.0
28	21	16	10		10	15	19	35

78.4	79.1	78.0	75.5	80.5	80.4	79.5
4.3	3.6	4.7	7.2	2.2	2.3	3.2
37	45	57	75	75	66	49

77.7	77.8	77.2	77.7	77.9	77.8	77.6	77.6	78.0
5.0	4.9	5.5	5.0	4.8	4.9	5.1	5.1	4.7
43	30	21	10		10	19	32	40

77.0	75.3
5.7	7.4
56	75

79.1	78.4
3.6	4.3
75	55

Sta + π ~ Elev

982.66

32+72 W. Edge Ent

✓

33

+13 E. Edge Ent

+43

✓

BM 1.99 980.87 3.76 978.90 (978.88)

March 5, 1970

LT

Z

RT

64

77.8	78.1	77.3	77.7	77.9	77.8	77.5	77.3	77.6
4.9	4.6	5.4	5.0	4.8	4.9	5.2	5.4	5.1
42	33	21	10		10	21	30	40

75.5	73.2
7.2	9.5
60	75

77.6	77.6
5.1	5.1
75	58

69.6	70.9	73.3	77.0	77.2	77.6	77.7	77.5	77.5	77.6	77.8	77.0
13.1	11.8	9.4	5.7	5.5	5.1	5.0	5.2	5.2	5.1	4.9	4.7
75	64	48	30	21	10		10	20	32	59	75

65.2	69.7	71.9	76.5	77.1	77.4	77.5	77.3	77.3	77.3	77.5	77.9
14.5	13.0	10.8	6.2	5.6	5.3	5.2	5.4	5.4	5.4	5.2	4.8
75	59	45	28	23	10		10	20	33	54	75

70.2	70.6	77.1	77.1	77.2	77.4	77.2	76.5	75.6	76.8
12.5	6.1	5.6	5.6	5.5	5.3	5.5	6.2	7.1	5.9
40	29	23	19	10		9	18	28	35

69.2	68.0	67.5
13.5	14.7	15.2
45	58	75

78.3	77.9
4.4	4.8
75	54

Top Hyd S.E. Corner Ent. to Brimhall School

Sta	+	π	-	Elev.
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		980.87		
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33+75				
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✓				
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34				
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✓				
---	--	--	--	--

+50				
-----	--	--	--	--

✓				
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March 5, 1970

Lt

BT 65

68.3	76.1	76.5	76.8	77.2	76.9	76.3	75.6	76.7	79.1
12.6	4.8	4.4	4.1	3.7	4.0	4.6	5.3	4.2	2.1
41	24	19	10		10	19	29	40	60

67.8	67.3
13.1	13.6
52	75

78.5
2.4
75

68.1	75.7	76.2	76.5	76.9	76.7	75.9	75.5	76.6	79.1
12.8	5.2	4.7	4.4	4.0	4.2	5.0	5.4	4.3	3.3
43	27	20	10		10	19	30	40	53

67.0	66.8	66.7
13.9	14.1	14.2
50	65	75

78.7	78.6
2.2	2.3
75	67

66.5	67.0	75.2	75.7	76.2	76.6	76.5	75.4	74.6	77.9	79.1
14.4	13.9	5.7	5.2	4.7	4.3	4.4	5.5	6.3	3.0	1.5
63	48	26	20	10		12	21	30	50	6.2

66.5
14.4
75

79.2
1.7
75

Sta + π - Elev

980.87

35

+30

+59 $\angle$ Drainage Rt from School
Buildings

97796

March 5, 1970

66

LT

+

RT

66.4	66.7	74.6	75.4	75.9	76.3	76.1	75.3	73.2	76.5	78.9
14.5	14.2	6.3	5.5	5.0	4.6	4.8	5.6	7.7	4.4	2.0
75	50	28	20	10		10	19	26	40	53

80.5	79.8
0.4	11
75	63

66.5	66.8	74.9	75.2	75.8	76.1	76.0	75.3	73.7	75.8
14.4	14.0	6.0	5.7	5.1	4.8	4.9	5.6	7.2	5.1
64	46	26	21	10		10	20	26	38

66.9
14.0
75

79.4	79.1	78.2
1.5	1.8	2.7
75	70	53

67.5	75.1	75.2	75.7	75.9	75.8	75.2	73.5	76.3	77.4
13.4	5.8	5.9	5.2	5.0	5.1	5.7	7.4	4.6	3.5
50	29	21	10		10	19	37	44	59

67.6
13.3
75

77.6
3.3
75

Sta + π - Elev.

980.89

36

✓

+35

✓

+55

BM 2.45 980.41 2.90 977.97 (977.96)

March 5, 1970

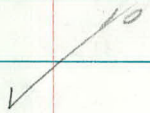
Lt.

£

Rt.

67

70.4	74.9	75.0	75.6	75.9	75.8	75.1	73.2	76.2
10.5	6.0	5.9	5.3	5.0	5.1	5.8	7.7	4.7
42	27	21	10		10	19	26	41



69.5	69.6
11.4	11.3
57	75

79.4	77.3	78.5
1.5	1.6	2.4
75	68	59

72.4	72.5	74.7	75.2	75.5	75.6	75.5	74.9	72.9	76.2
8.5	8.4	6.2	5.7	5.4	5.3	5.4	6.0	8.0	4.7
75	52	29	22	10		10	19	27	44



79.2	78.5
1.7	2.4
75	61

75.8	75.5	75.4	75.1	75.3	75.5	75.4	74.9	73.1	75.8
5.1	5.4	5.5	5.8	5.6	5.4	5.5	6.0	7.8	5.1
54	40	28	21	10		11	18	26	42



76.1
4.8
75

79.1	78.6
1.8	2.3
75	62

Top Hyd Lt Sta 37+00±

Sta	+	π	-	Elev.
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		980.41		
--	--	--------	--	--

37				
----	--	--	--	--

✓				
---	--	--	--	--

+50				
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✓				
---	--	--	--	--

38				
----	--	--	--	--

✓				
---	--	--	--	--

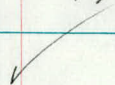
March 5, 1970 68

Lt.

E

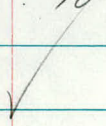
Rt.

76.1	74.9	74.6	74.9	75.1	75.1	74.7	74.6	76.1
4.3	5.5	5.8	5.5	5.3	5.3	5.7	7.8	4.3
41	27	21	10.		11	19	26	47



76.3	75.5	76.0			76.8	76.7
4.1	4.9	4.4			3.6	3.7
55	70	75			75	70

77.3	75.9	74.0	74.0	74.5	74.7	74.6	73.9	72.0	75.1	75.8
31	4.5	6.4	6.4	5.9	5.7	5.8	6.5	8.4	5.3	4.6
57	40	26	20	10		10	19	25	46	75



77.8	77.5
2.6	2.9
69	75

77.2	75.4	73.1	73.1	73.9	73.9	73.9	73.1	71.3	74.1
32	50	73	73	6.5	6.5	6.5	7.3	9.1	6.3
56	41	27	20	10		10	20	25	43



77.9
23
75

74.5	74.4
5.9	6.0
75	60

Sta + π - Elev,

980.41

38+50

✓

TP

8.29 972.12 5/6 39 ~~2~~

TP

1.27 973.39

972.12

39+00

✓

Lt. £ March 5, 1970 69
RT

^{15.0}	^{12.3}	^{12.3}	^{12.8}	^{13.0}	^{12.9}	^{12.6}	^{10.8}	^{11.9}
5.4	8.1	8.1	7.6	7.4	7.5	7.8	9.6	8.5
44	28	19	10		10	20	25	36

^{11.2}
 → 3.2
 63

^{11.1}
 3.3
 75

^{13.7}
 6.7
 75

^{13.7}
 6.7
 62

^{13.5}
 6.9
 46

RG
 WT
 CM

March 10, 1970
 PC 150

Sta 39+00 £

^{13.2}	^{11.7}	^{11.3}	^{11.9}	^{12.1}	^{12.0}	^{11.4}	^{10.6}	^{10.9}	^{12.5}
0.2	1.7	2.1	1.5	1.3	1.4	2.0	2.8	2.5	0.9
40	29	25	10		10	20	25	31	43

^{13.8}
 → +0.4
 52

^{12.0}
 +0.6
 42

^{13.4}
 0.0
 75

^{12.9}
 0.5
 75

^{13.0}
 0.4
 66

^{12.5}
 0.9
 60

Sta

+

π

-

EIV

973.39

39+50

✓

+69

Ent. Rt.

✓

+86

Ent. Lt.

✓

Left

2

Right

70.6	69.8	70.5	70.7	70.8	70.7	70.5	69.8	70.7	69.9
2.8	3.6	2.9	2.7	2.6	2.7	2.9	3.6	2.7	3.5
27	23	19	10		10	16	26	37	53

69.9	70.5	70.0		69.2	69.5
3.5	2.9	3.4		4.2	3.9
45	61	75		75	65

69.1	69.5	70.0	70.3	70.5	70.4	70.0	70.1	70.2	69.7
4.3	3.9	3.4	3.1	2.9	3.0	3.4	3.29	3.2	3.7
41	23	17	10		10	16	18	22	34
							B.T	BT	BT

68.9	68.8	68.8		69.0
4.5	4.6	4.6		4.40
57	63	75		58
				Garage

69.1	69.4	69.5	69.9	70.1	70.0	69.6	69.6	68.7	68.7
4.3	4.04	3.9	3.5	3.3	3.4	3.8	3.8	4.7	4.7
40	23	20	10		10	18	26	37	51
BT	BT								

68.9		68.7	68.7
4.51		4.7	4.7
61		75	66
Garage			

Sta + π - E/V

973.39

40+00

✓

+50

✓

BM 3.07 971.74 4.73 968.66 (968.67)

+87

ditch

✓

L4

L

R4

71

68.7	68.4	69.3	69.4	69.7	69.5	69.0	69.3	68.3	68.5
4.7	5.0	4.1	4.0	3.7	3.9	4.4	4.1	5.1	4.9
27	21	15	10	10	17	28	40	49	

68.2
~~68.4~~

68.1	68.1
5.2	5.3
39	70

68.8
4.6
75

67.2	67.2	67.7	68.2	68.6	68.4	68.0	67.7	67.9	67.8
6.2	6.2	5.7	5.2	4.8	5.0	5.4	5.7	5.5	5.6
29	23	19	10	10	16	17	22	30	

67.1

67.4

6.3	6.0
46	67

68.6

68.1

67.3

67.4

4.8	5.3	6.1	6.0
66	57	43	37

Top Hyd NW Cor "B" ≠ Midlothian Rd.

65.5	65.7	66.8	67.2	67.6	67.9	67.6	67.3	67.0	67.4	67.7
6.2	6.0	4.9	4.5	4.1	3.8	4.1	4.4	4.7	4.3	4.0
57	40	29	20	10	10	19	22	31	52	

65.1

6.6
75

66.9

4.8
75

Sta + π - EN

971.74

40+92

shoulder

41+07

Midlothian Rd

+11

4.54 967.20 MH rim

+21

shoulder

+25

ditch

+50

✓

LT

Q.

RT

72

65.9	66.0	66.6	67.0	67.5	67.8	67.6	67.3	67.1	66.9	66.9
5.8	5.7	5.1	4.7	4.2	3.9	4.1	4.4	4.6	4.8	4.8
75	53	34	24	10		10	23	44	60	75

66.0	66.1	66.2	66.5	67.1	67.3	67.6	67.3	67.3	67.0	66.9	66.9	66.9
5.7	5.6	5.5	5.2	4.6	4.4	4.1	4.4	4.4	4.7	4.8	4.8	4.8
150	100	68	43	22	10		10	25	50	75	100	150

RT 36'

65.7	65.8	66.2	66.8	67.1	67.3	67.1	67.0	67.1	66.9	66.8
6.0	5.9	5.5	4.9	4.6	4.4	4.6	4.7	4.6	4.8	4.9
80	60	40	25	10	✓	10	23	44	62	80

64.5	64.5	64.8	66.2	66.6	67.0	67.2	67.0	66.8	66.1	65.5	65.4	65.5
7.2	7.2	6.9	5.5	5.1	4.7	4.5	4.7	4.9	5.6	6.2	6.3	6.2
85	69	54	34	26	10	✓	10	23	34	43	58	75

65.5	64.0	64.4	66.2	66.5	66.8	66.6	66.1	65.3	66.7	66.4	66.2
6.2	7.7	7.3	5.5	5.2	4.9	5.1	5.6	6.4	5.0	5.3	5.5
39	29	23	18	10	✓	10	19	28	39	59	75

65.7	65.9
6.0	5.8
60	75

Sta + π - E/V

971.74

42+00

✓

TP 0.61 966.77 5.58 966.16 & Sta. 42

+30 & Ent 24

✓

+55

FK
GA
CM

March 13, 1970

LT

R

RT

73

65.3 63.5 65.7 65.9 66.1 65.8 65.5 64.3 65.3
6.4 8.2 6.0 5.8 5.6 5.9 4.2 7.4 6.4
36 25 17 10 ✓ 10 19 26 32

66.3 66.2
5.4 5.5
53 61
Ho.

64.8 65.3
6.9 6.4
75 51

66.7 65.7 65.4 65.6 65.7 65.4 65.3 64.1 64.8
0.1 1.1 1.4 1.2 1.1 1.4 1.5 2.7 2.0
Ga 37 23 11 10 20 25 35
64

64.4 64.6
2.4 2.2
75 51

63.1 63.1 65.0 65.2 65.4 65.2 65.1 63.7 63.7
3.7 3.7 1.8 1.6 1.4 1.6 1.7 3.1 3.1
29 26 19 11 ✓ 10 19 25 30

64.7 65.3 65.9 65.4
2.1 1.5 0.9 1.4
36 45 63 75

63.5 63.9 64.1
3.3 2.9 2.7
75 59 41

Sta + π - Elev.

966.77

42+80

✓

43

✓

+50

✓

BM

2.12 964.65 (964.61)

Lt.

March 13, 1970

51

74

65.5

65.2

64.8

65.0

65.1

64.9

64.4

62.6

62.1

1.3	1.6	2.0	1.8	1.7	1.9	2.4	4.2	4.7
34	32	21	11		10	20	27	38

65.8

63.4

61.9

61.8

→ 1.0
81
Ga

Pick up Drainage

3.4 4.9 5.0
75 52 46
→ Ditch

64.2

63.4

64.5

64.8

64.9

64.5

64.1

61.9

61.7

2.6	4.4	2.3	2.0	1.9	2.3	2.7	4.9	5.1
36	27	20	11		11	21	27	33

Ditch

65.0

65.7

65.9

63.7

63.6

63.3

→ 1.8 1.1 0.9
44 62 75

3.1 3.2 3.5
75 60 44

63.5

61.7

63.8

64.1

64.3

64.0

63.3

62.9

62.8

3.3	5.1	3.0	2.7	2.5	2.8	3.5	5.9	4.0
37	28	17	11		10	19	27	39

65.1

65.8

63.5

63.2

→ 1.7 1.0
48 73
Ho

3.3 3.6
75 56

Top Hyd S.W. Corner Fry & "B"

Sta + π - Elev.

BM

Linker

Rod

964.61

Top Hyd at Fry

44

✓

+13

✓

+25^t £ Haddington ⁺

+28 MH 38' Rt 63. 963.03

✓ March 13, 1970

1t

RT

75

✓
61.8 61.3 63.5 63.4 63.7 63.3 62.7 60.8 62.3
33 28 21 10 10 19 25 38

→ 63.6 64.3 64.5 63.2 62.9
42 61 75 75 53

✓
64.4 64.0 63.6 63.4 63.5 63.2 62.6 60.5 62.3
75 57 32 11 11 19 27 39

→ 64.9 63.2 62.9
100 75 52

✓
64.6 64.1 63.6 63.3 63.4 63.0 62.5 60.6
80 56 29 11 10 18 25

→ 65.1 63.1 62.8 62.3
100 75 54 36

Sta	+	π	-	Elev.
-----	---	-------	---	-------

44+38				
-------	--	--	--	--

✓				
---	--	--	--	--

+55				
-----	--	--	--	--

✓				
---	--	--	--	--

45				
----	--	--	--	--

✓				
---	--	--	--	--

44+76 S.D. 23'±Rt				
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59.56				
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March 13, 1970

Lt

Rt

76

633 632 63.1 63.3 62.9 62.1 60.6
52 31 11 10 19 24

64.2 64.7
75 100

63.0 62.7 62.2 60.8
75 53 36 28

60.3 62.4 62.5 62.8 63.1 62.8 62.0 60.5 60.3
30 24 21 11 10 18 22 27

61.7 62.8 63.8 64.0 63.6 / 62.8 62.6 62.4 62.0
41 47 52 66 75 / 75 57 43 37

60.1 60.0 62.0 62.5 96^{2.66} 62.4 61.7 60.3 60.7
32 28 18 11 10 20 26 31

61.8 64.0 64.1 64.2
40 54 65 75

62.8 62.7 62.1
75 58 37

Sta + π - Elev

45+32

✓

+64 Gutter Rd

✓

+78 $\pm$ Fry

✓

March 13, 1970

Lt.

£

At.

77

59.7 59.9 61.6 62.0 62.2 62.0 61.7 61.0
32 27 19 12 10 18 27

61.7 64.2 64.3 64.4 64.6 / 62.6 62.6 62.4 61.4
40 51 57 67 75 75 60 40 33

58.8 60.9 61.4 61.7 61.9 61.8 61.8 61.7 61.6
27 23 19 12 10 19 32 47

59.5 61.4 64.0 64.3 64.6 64.6 / 62.1 61.9 61.8
30 40 50 57 67 75 100 84 68

59.6 59.7 60.9 61.3 61.6 61.8 61.6 61.6 61.58 61.8
34 30 25 21 11 10 25 MH 59
33

61.6 63.8 64.0 64.5 / 62.7 62.6 62.4 62.1 62.0
41 50 56 67 200 170 137 100 81

64.6
75

Sta + π - Elev

45+93

✓

46 $\pm$ Ent Lt

✓

+20

✓

11.

March 13, 1970

At.

78

61.5 61.3 61.5 61.6 61.4 61.3 61.3 61.4
31 23 11 10 23 36 58

62.4 63.5 63.9 64.5
42 56 65 75

61.9 61.7
100 77

62.4 61.5 61.3 61.4 61.5 61.3 61.2 61.0 61.9
44 30 22 10 11 19 27 39

63.7 64.2
60 75

62.5 62.3
75 63

60.4 61.1 61.1 61.2 61.3 61.1 60.9 61.7 62.4
44 35 23 11 10 18 31 43

60.4 60.4
65 75

63.6 63.3 63.1
75 68 57

Sta + π - Elev.

46 + 57

✓

47 Ent Rt

✓

+27 Walk Lt.

✓

March 13, 1970

Lt

RY

79

60.8 60.8 60.8 60.9 60.8 60.8 61.8
32 23 12 9 15 27

60.4 60.4 60.4 63.7 63.6 62.6 61.7
37 52 75 75 70 52 38
Low Spot

60.8 60.5 60.4 60.3 60.5 60.3 60.0 60.4 61.0
40 34 21 11 10 18 28 45

60.8 61.1 61.6 61.3
58 75 81 63

60.29 60.4 60.1 60.1 60.2 60.0 59.6 60.5 60.9
34 33 22 11 10 19 27 41
walk

60.74 60.74 60.88 61.3 61.1
44 61 75 56

Sta + π - Elev.

47+52 $\pm$ Ent Rt

✓

+65 $\pm$ Ent Lt

✓

48

✓

2+

March 13, 1970
Rt 80

✓
60.4 59.9 59.6 59.8 59.9 59.8 59.3 59.4 59.1
(36 27 17 10 10 22 38 60

→ 60.8 60.97
55 75
walk

60.0
75

60.5 59.9 59.6 59.6 59.8 59.6 59.3 59.2 59.1
61 41 21 10 10 18 30 50

→ 60.7
75

60.0 59.8
75 68

✓
58.2 56.7 59.1 59.4 59.4 59.1 59.7 58.2 58.1
(39 ~~39~~ 18 12 10 79 30 41
29%

→ 57.8 58.6
54 75

59.4 59.0
75 62

Sta + π - Elev.

48+34

✓

+55 Ent Rt,

✓

+66

Checked Bench

(960.81)

Lt

L M

R

81

57.6 56.8 58.6 58.9 59.0 58.7 58.2 57.58
 32 28 17 10 10 18 26
 50

58.3 58.7 58.7 59.4 58.1 57.9
 48 68 75 100 60 37

57.7 56.4 58.3 58.7 58.7 58.5 57.6 57.6
 44 29 17 11 10 23 41

58.3 58.8 57.9 57.9 57.9
 65 75 82 70 62

59.4 56.1 58.2 58.5 58.6 58.3 57.71 57.6
 38 28 16 10 10 MH 36
 22

60.1 60.6 61.1 57.8 57.7 57.6
 54 69 75 75 71 58

Top Hyd Lt Sta 49+50

Sta + π - Elev.

960.81

49+00

✓

47+73 MH 19' RT

958.97

+30 ± EH + RT

✓

+47

✓

BM

✓

957.44

March 13, 1970

Lt.

Rt.

82

54.7 57.0 57.8 58.2 58.3 58.0 57.6 57.4
28 23 19 11 10 21 41

57.3 59.2 59.9 61.4 62.2 / 57.7 57.5
34 40 51 68 75 75 63

59.8 58.5 58.0 57.9 58.0 57.7 57.0 57.2
15 39 22 11 10 22 30

61.3 57.6 57.5 57.2
75 75 64 49

60.5 58.8 57.6 57.7 57.8 57.6 57.3 55.90
37 34 22 11 10 17 23
MH

61.2 62.4 55.7 55.8 56.0 56.0
64 86 75 56 49 34

Top Hyd

Sta + π - Elev.

BM

960.81

49 +67

✓

50

✓

+27 $\neq$ Abandon Ent Rt

✓

57.44

FK
RG
WJ
GA

Lt.

March 16, 1970

83

Rt

✓

58.4 57.6 57.6 57.64 57.4 57.3 57.1
26 18 10 10 17 18

→ 60.3 61.8 62.0 56.5 56.4 56.0
49 70 75 75 51 28

✓

60.3 57.9 57.3 57.3 57.3 57.1 56.9 56.9
49 28 16 10 9 17 29

→ 61.7 62.3 57.1 56.7 56.2
63 75 75 51 30

✓

58.8 57.3 56.9 57.0 57.0 56.9 56.8 56.6
45 28 19 11 10 21 30

→ 60.7 61.0 57.0 56.7
69 75 75 55

Sta	+	π	-	Elev.
-----	---	-------	---	-------

50+60				
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✓				
---	--	--	--	--

+81				
-----	--	--	--	--

✓				
---	--	--	--	--

+88	MH 22' BT	956.18		
-----	-----------	--------	--	--

51				
----	--	--	--	--

✓				
---	--	--	--	--

				57.14
--	--	--	--	-------

£ March 16, 1970

Lt.

84

56.5 56.4 56.6 56.7 56.5 56.6 56.3
29 20 10 10 21 32

→ 57.0 58.1 59.0 59.7 57.7 56.5
41 60 75 75 50 37

53.0 53.0 56.1 56.4 56.5 56.3 56.1 56.0
30 27 18 13 10 21 28

→ 55.0 55.7 55.4 55.2 60.2 58.9 57.4
33 40 57 78 75 63 46
Parking

55.6 52.7 56.0 56.1 56.2 56.1 56.2 55.9
35 27 20 11 9 19 25

→ 55.8 55.6 55.3 55.1 59.3 58.4 56.2
40 45 58 75 75 52 35

Sta	+	π	-	Elev
-----	---	-------	---	------

51+20				
-------	--	--	--	--

✓				
---	--	--	--	--

+57				
-----	--	--	--	--

+67 ⁺ MH 19 ⁺ Rt				
--	--	--	--	--

				955.73
--	--	--	--	--------

✓				
---	--	--	--	--

+81 Good for Ent Rt				
---------------------	--	--	--	--

✓				
---	--	--	--	--

March 16, 1970

Lt.

RT

85

56.2 55.95 55.81 55.9 56.1 56.0 56.3 56.9
32 28 16 11 20 25 36
conc Ent

55.9 55.5 55.0 55. 59.3 58.7 57.3
43 47 75 67 58 44
Parking

55.7 55.8 55.3 55.5 55.8 55.7 55.9 56.9
24 19 18 11 10 20 33
C G

55.10 54.96 54.71 58.8 57.72 57.37
34 55 75 75 53 36
conc conc

55.3 55.5 55.0 55.4 55.6 55.5 55.5 56.3
35 21 20 10 9 20 33
conc C G

54.62 54.53 54.35 57.6 57.1 56.6
37 54 77 75 63 46
conc

Sta	+	-	Elev.
-----	---	---	-------

52+00			
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✓			
---	--	--	--

+15	SD	Lt	954.51
-----	----	----	--------

+29			
-----	--	--	--

✓			
---	--	--	--

+33	W. Edg	Service Lane	
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✓			
---	--	--	--

Lt.

March 16, 1970

Rt.

86

54.6 54.6 55.1 55.5 55.4 55.1 55.7
34 23 10 9 21 22

54.5 54.3 54.2 55.8 56.2
46 58 75 39 33

55.4 54.8 55.0 55.2 55.4 55.3 55.2 55.7
26 25 11 8 10 27 28
C G G C

55.0 54.9 54.3 54.0 53.7 / 56.1 56.0 55.5
39 47 48 70 80 75 65 45

54.7 54.8 55.2 55.4 55.2 55.1 55.1 55.3
54 29 9 10 22 33 57
Gutter Line

54.5
75

55.6
75

Sta	+	π	-	Elev
-----	---	-------	---	------

52+53				Service Lane
-------	--	--	--	--------------

✓

+64				Section Line
-----	--	--	--	--------------

✓

+75				
-----	--	--	--	--

✓

lt.

E

March 16, 1970

At

87

54.6 54.9 55.04 55.2 55.1 55.0 55.0
 56 28 MH 11 26 52
 13

54.4 54.2
 79 100

55.8 55.4
 100 79

55.0 54.5 55.0 55.1 55.1 55.0 55.1 55.1
 41 40 14 14 34 67 100
 C 6

54.9 54.1 54.0
 58 74 100

54.9 54.4 54.7 55.1 55.2 55.1 54.9 54.9
 32 31 17 3 C 3 25 45
 C

54.9 50.25 52.3
 37 44 46
 inv.

55.0 54.9
 75 56

51.3 51.5
 75 62

Sta	+	π	-	Elev.
-----	---	-------	---	-------

52+86				
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✓				
---	--	--	--	--

+96				
-----	--	--	--	--

53				
----	--	--	--	--

✓				
---	--	--	--	--

BM				
----	--	--	--	--

			957.44	
--	--	--	--------	--

Lt.

March 16, 1970 88
Rt.

54.4 54.5 55.1 55.7 55.1 54.9 54.9 55.3
30 18 3 3 22 39 45

54.9 54.6 51.9 51.7 51.5 / 55.0 55.0 54.9
32 36 44 58 75 75 69 63

54.13 54.49 54.95 55.6 55.7 55.6 54.97 54.88
39 20 3 3 3 3 21
conc 55 conc

54.11 53.77 55.48 55.38 55.07
cor 58 bit 75 57 40
conc. 75 bit conc

Top Hyd.

Sta	+	π	-	Elev
BM	2.15	975.56		973.41

0-80	MH 13' Rt	2.82	972.74	
------	-----------	------	--------	--

0-60	MH 37' Rt	3.28	972.28	
------	-----------	------	--------	--

3+23		4.31	971.25	70.67
------	--	------	--------	-------

✓		4.88	970.68	
---	--	------	--------	--

BM	6.81	986.45		979.64
----	------	--------	--	--------

5+11	MH 18' Rt	2.57	978.88	
------	-----------	------	--------	--

6+22	MH 19' Lt	3.98	982.47	
------	-----------	------	--------	--

6	Σ	4.25	82.2	82.0
---	----------	------	------	------

7+70	Rt 18	2.79	83.66	983.73
------	-------	------	-------	--------

5+00	Σ	2.61	78.84	78.8
------	----------	------	-------	------

BN	0.99	982.59		981.60
----	------	--------	--	--------

10+29	MH 17' Rt	6.59	976.-	
-------	-----------	------	-------	--

10+42	CB 21' Rt	7.77	974.82	
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+42	CB 21' Lt	7.41	973.18	
-----	-----------	------	--------	--

+42	MH 8' Lt	6.92	973.67	
-----	----------	------	--------	--

11		9.06	73.53	74.25
10		4.95	77.64	72.9

FK
LPD
CM

March 19, 1970

89

Top Hyd SE Corner Cleveland & "B"

Top Hyd R1

Top Hyd R1 9+90

730
651

.79

6.13
79

6.92

Sta	+	π	-	Elev.
BM	0.90	982.50		981.60
TP		685	10.66	971.84 971.75
BM	2.05	970.58		968.53
13+11	MH 17' Lt		4.67	965.91
MH			5.80	964.78 964.76
BM	1.79	966.40		964.61
46+05	MH 28' Rt		5.03	961.37
+56	MH 20' Lt		5.81	960.59
27	$\neq$ $\checkmark$		5.92	60.5 60.5
BM	2.93	963.74		960.81
48+57			6.57	957.17
+66			6.01	37.73 $\checkmark$ 957.71
TP MH	5.12	960.16		955.04
52+83	SD 109' Rt		6.41	953.75
+86	$\neq$		4.49	55.7 55.7

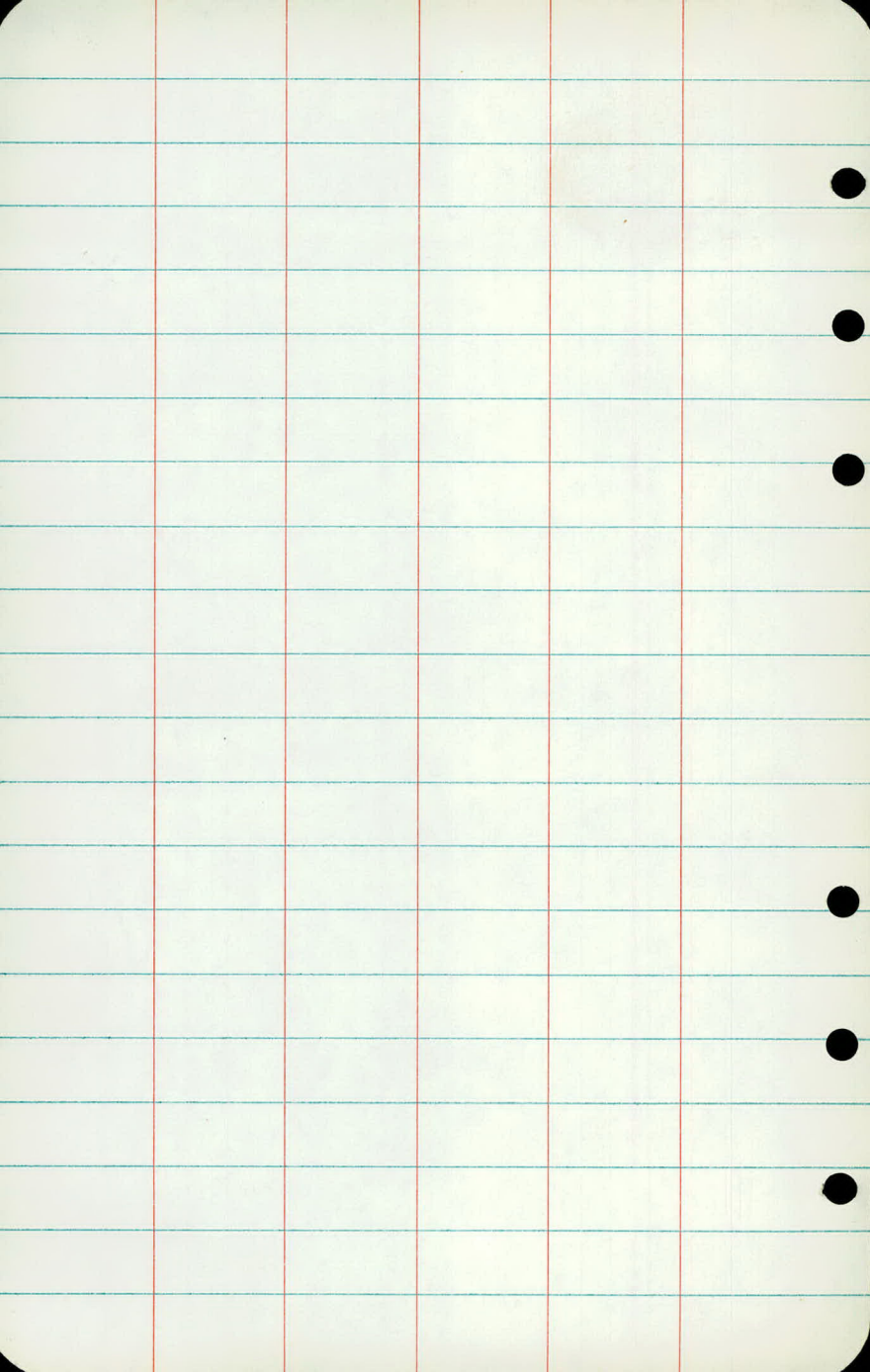
March 19, 1970
£

90

Top Hyd
White Stake

Top Hyd By West Ent To Fairview Junior High

Top Hyd at F. y



FK
RG
CM

May 22, 1970

91

Additional x-sections

Sta	+	π	-	Elev.
BM	8.12	981.53		973.41

0-61

✓

-80

✓

-1

✓

May 22, 1970 92
 Lt North Rt South

Top Hyd. SE Corner Cleveland & B

9.9 9.5 9.2 9.1 9.0 9.1 9.3 9.35 9.8
 64 45 28 11 13 31 37 47
 MH

92.18

→ 10.4
 81

10.4 10.2
 75 64

9.4 9.0 9.0 8.7 8.6 8.84 9.0 9.2 10.0
 41 26 19 11 14 18 28 41
 MH

92.69

→ 10.3
 79

11.4 10.9
 77 55

9.5 8.8 8.5 8.3 8.2 8.5 8.7 8.9 10.0
 56 34 21 11 14 25 30 36

→ 9.9
 75

9.7 9.1
 75 55

Sta + π - Elev

981.53

- 133 $\angle$ Service Lane Left (North)

✓

- 163

✓

- 200

✓

£

93

8.9 8.4 7.8 7.3 7.1 7.3 7.7 8.2 5.4
100 70 40 12 12 24 30 34

→ 9.4
125

5.9
53

8.9 8.0 7.3 6.5 6.2 6.3 6.7 6.9 5.6
61 82 33 19 12 22 28 31

→ 10.5
78

0.4 3.1
39 33

3.8 6.2 6.0 5.6 5.4 5.5 6.0 5.7 3.0
43 31 24 13 12 22 27 32

→ 2.1 4.4 6.7
54 63 75

0.1
38

Sta + π - Elev

981.53

-250'

✓

-300'

BM 11.52 987.44 5.61 975.92

-133

-163

-200

0.24

-250

BM

14.04 973.40 (973.41)

North

May 22, 1970

South

94

5.7	5.6	5.0	4.9	5.2	5.4	0.4
32	24	11		13	24	37

61

→ 1.5 4.9
51 73

10.5	8.5	6.3	6.4	5.0	5.0	5.2	5.5	1.2	0.6
75	57	40	32	11		13	23	36	41
									Fe

Spike in Transformer P.P. NW Corner Cleveland 4B

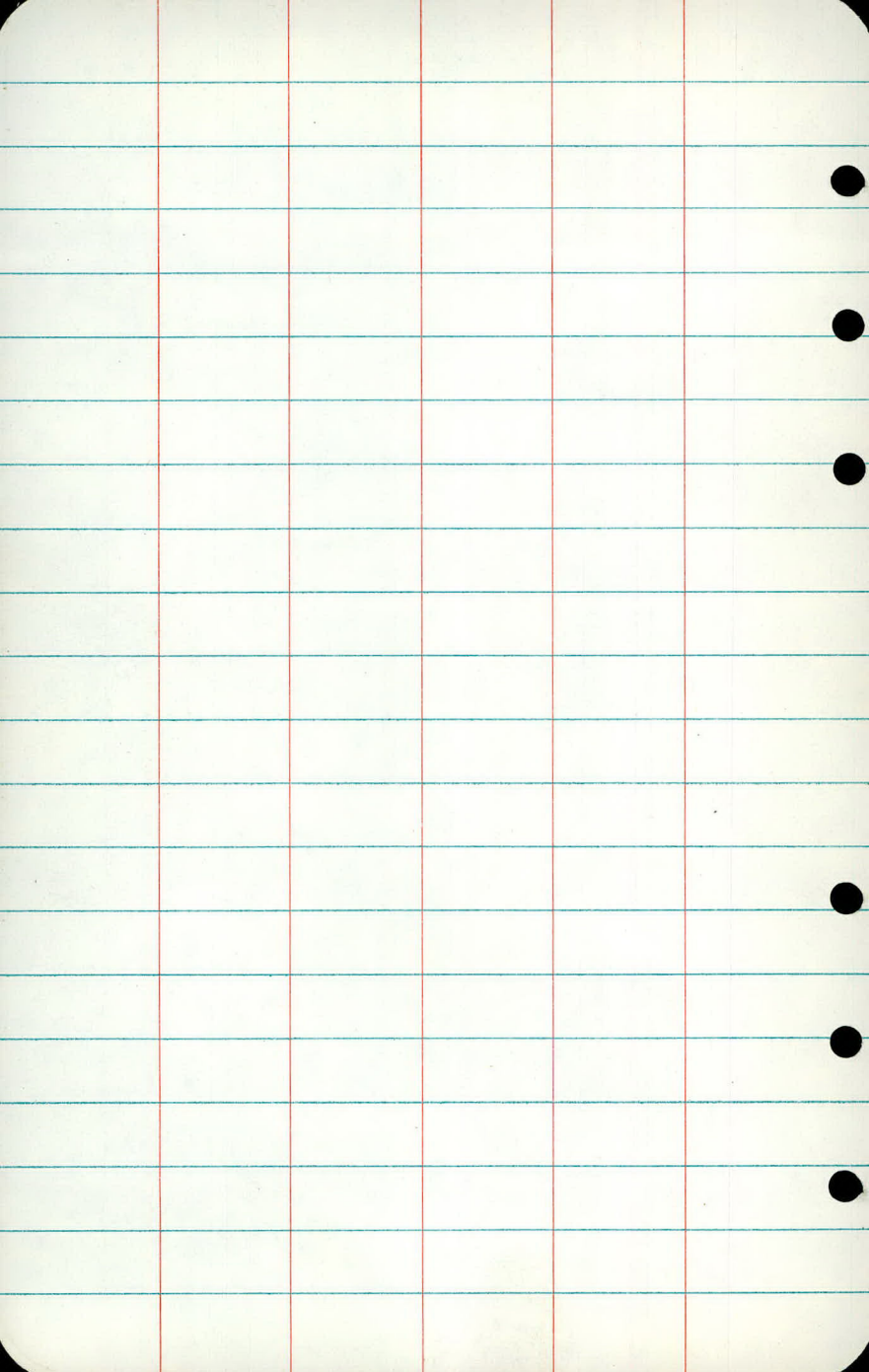
12.9
75

5.1	5.5	8.7
41	58	78

0.6	1.7
49	68
Fe	

88.2
52

Top Hyd S.E. Corner Cleveland + "B"



KP
DS
CP

26 MAY 1910
SUNNY & WINDY
50°

CLEVELAND AVE
AT CO. RD B

X- SECTIONS

0+00 = 300' S. OF CO. RD B
ON SECTION LINE

STA + π - ELEV

BM 4.57 977.98

973.41

0+00

✓

+50

✓

1+00

✓

LT

26 MAY 1970

RT

TOP HYD S.E. COR CLEVELAND CO. RD B

10.0	10.9	11.1	11.6	11.7	11.5	11.5	10.9	11.3
8.0	7.1	6.9	6.4	6.3	6.5	6.5	7.6	6.7
60	43	32	11		11	17	33	39
FE								

DITCH

11.6
6.4
50

10.2	11.1	11.4	11.9	12.1	11.9	11.2	11.5	11.5
7.8	6.9	6.6	6.1	5.9	6.1	6.8	6.5	6.5
66	48	35	12		11	24	42	50
FE								

19.6	11.5	11.8	12.3	12.3	12.0	11.0	11.0	11.8
8.4	6.5	6.2	5.7	5.7	6.0	7.0	3.6	3.2
64	51	39	14		12	26	39	50

11.6
6.4
76
FE

✓

LT

26 MAY 1970
RT

72.2	72.53	73.14	72.50	72.5	72.2	71.8	71.2	71.7
5.8	5.45	4.84	5.48	5.5	5.8	6.2	6.8	3.3
42	17 6	15	14 6		12	21	26	35

71.8	70.0	72.1
6.2	8.0	5.9
53	69	90

FE

73.4
4.6
50

71.8	72.2	72.60	73.30	72.56	72.4	72.2	71.8	71.2	71.2	72.7	72.7
6.2	5.8	5.38	4.68	5.42	5.6	5.8	6.2	6.8	4.8	5.7	
55	44	18 6	15	14 6		12	23	29	38	50	

70.2
7.8
65

70.5
7.5
93

70.5	71.5	72.2	72.5	72.3	72.0	71.3	70.0	69.5
7.5	6.5	5.8	5.5	5.7	6.0	6.7	8.0	8.5
78	62	47	20		15	30	39	50

STA

+

 π

—

ELEV.

977.98

300

$$= \mathcal{L}$$

Co. RD B

750

400

6.22

871.76

971.75

LT

E

26

MAY
RT

1970

13.4

4.6

100

12.8

5.2

75

12.4

5.6

50

12.2

5.8

25

11.9

6.1

11.6

6.4

25

11.5

6.5

50

11.4

6.6

75

11.2

6.8

100

12.3

5.7

95

11.9

6.1

75

12.1

5.9

52

11.9

6.1

19

11.6

6.4

11.3

6.7

12

11.3

6.7

23

10.3

7.7

37

10.0

8.0

50

11.8

6.20

35

11.25

6.73

19

12.06

5.92

16

11.30

6.68

14

11.03

6.95

6

12.08

7.17

12

12.04

7.6

25

12.4

9.6

37

12.8

10.2

50

11.4

6.6

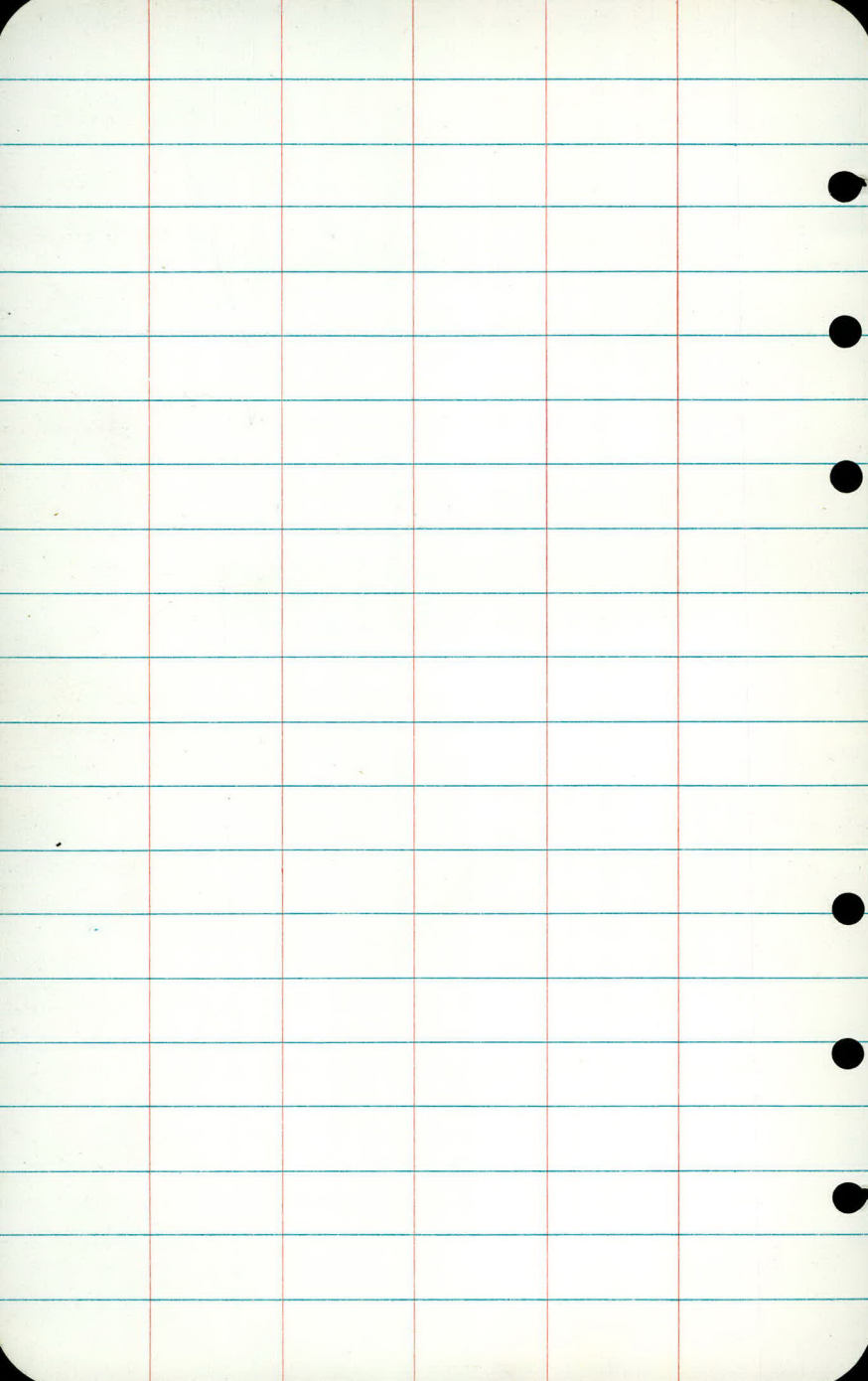
53

12.7

7.3

70

TOP MH 22' RT 2+77



26 MAY 1970

CLEVELAND AVE.

AT CORD B

0+00 = 300' S. OF CORD B

ON SECTION LINE

+50

BR

49

PP

56

+46 END Median

16

BR

16

+39 PP

16

+30 Arc Lite

60

2+00

MEDIAN

14-17

RD

44

RD

12

+94 PP

67

+50

+46 BEGIN MED

14-16

1+00

RD

40

RD

12

+57 PP

55

+59 PP

25

+50

+45 3" M

37

+23 3" M

37

+03 4" M

47

0+00

RD

33

RD

11

26 MAY 1970

LT

E

RT



4+00

+50

3+00

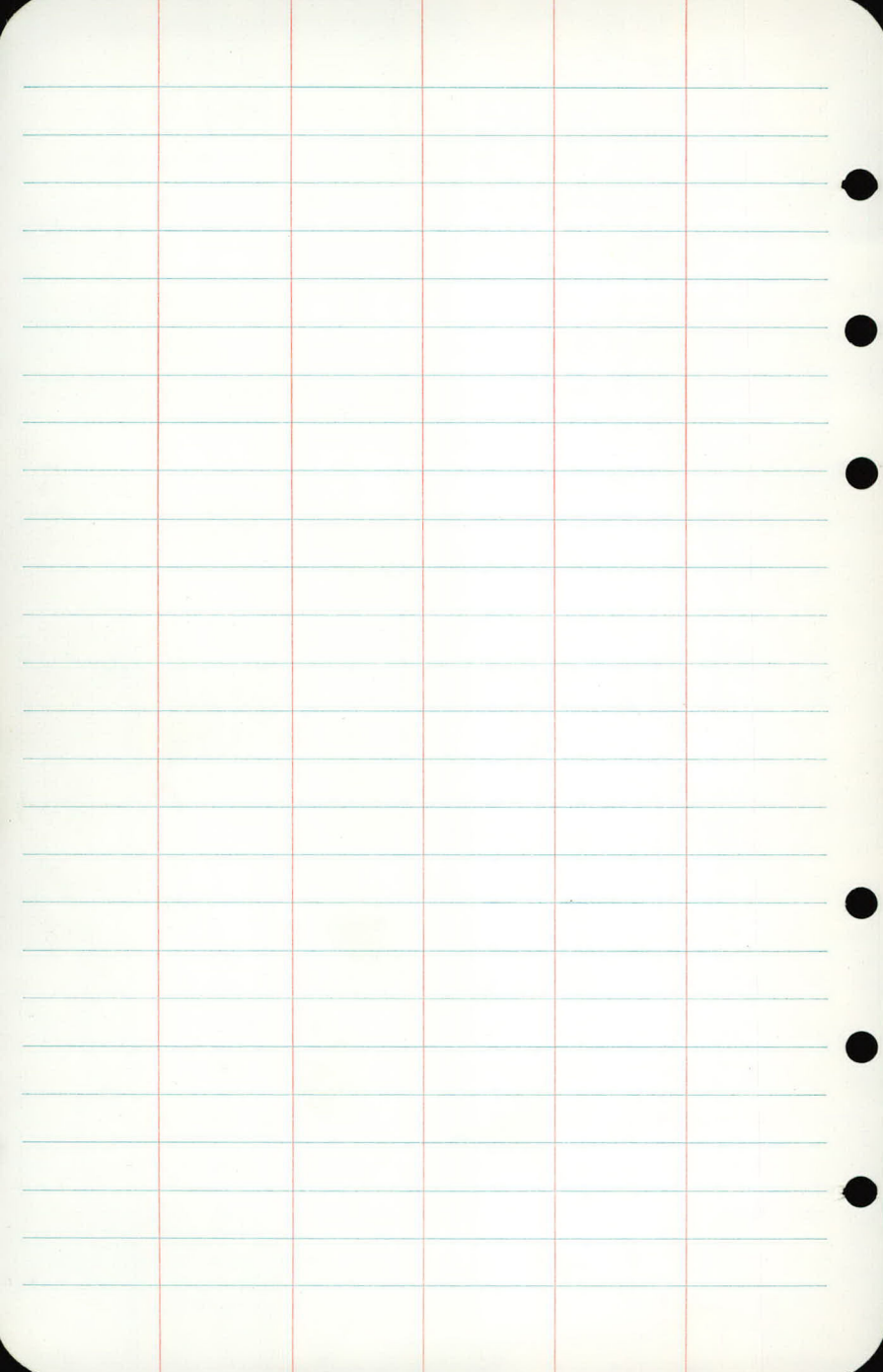
+77 MH
22

2+50

LT

~~E~~

RT



TOPOGRAPHY

LT ~~R~~ RT RT

$$\begin{array}{r} +49 \text{ BR} \\ \hline 24 \end{array}$$

$$\begin{array}{r} +43 \text{ 8" ELM} \\ \hline 39 \end{array}$$

$$\begin{array}{r} +196 \text{ ELM} \\ \hline 42 \end{array}$$

$$\begin{array}{r} +32 \text{ BR} \\ \hline 22 \end{array}$$

$$\begin{array}{r} +31 \text{ BUSH} \\ \hline 56 \end{array}$$

$$\begin{array}{r} +171 \text{ PINE} \\ \hline 50 \end{array}$$

$$\begin{array}{r} +001 \text{ ELM} \\ \hline 50 \end{array}$$

2+00

RD 21 RD 22

$$\begin{array}{r} +50 \text{ ROAD} \\ \hline 19 \quad 19 \end{array}$$

$$\begin{array}{r} +491 \text{ PINE} \\ \hline 53 \end{array}$$

$$\begin{array}{r} +361 \text{ ELM} \\ \hline 53 \end{array}$$

1+00

RD 15 RD 13

$$\begin{array}{r} +89 \text{ CB} \\ \hline 31 \end{array}$$

$$\begin{array}{r} +89 \text{ CB} \\ \hline 19 \end{array}$$

$$\begin{array}{r} +50 \text{ ROAD} \\ \hline 16 \quad 12 \end{array}$$

$$\begin{array}{r} +831 \text{ PINE BUSH} \\ \hline 54 \end{array}$$

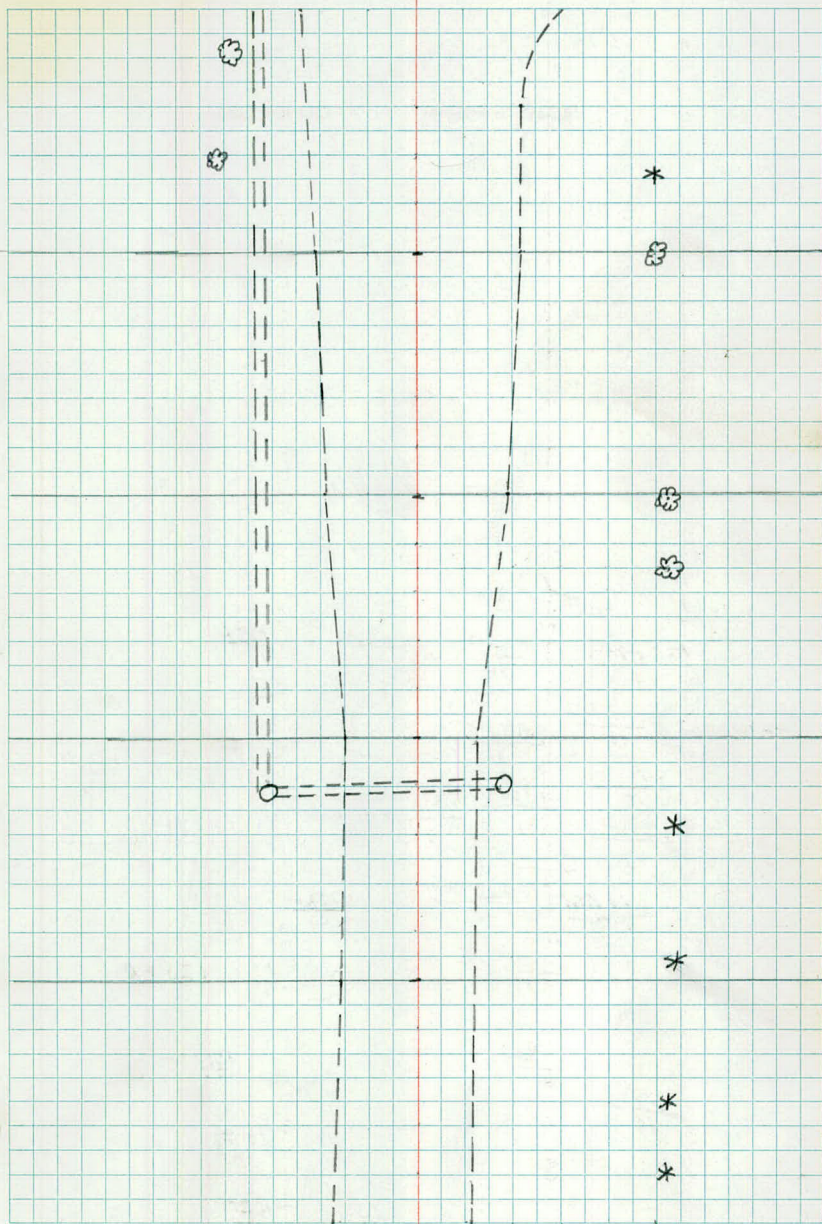
$$\begin{array}{r} +541 \text{ PINE BUSH} \\ \hline 54 \end{array}$$

$$\begin{array}{r} +251 \text{ PINE BUSH} \\ \hline 53 \end{array}$$

$$\begin{array}{r} +131 \text{ PINE BUSH} \\ \hline 52 \end{array}$$

0+00

RD 17 RD 12



4+00

RD RD
31 31

$$\begin{array}{r} +76 PP \\ \hline 38 \end{array}$$

$$\begin{array}{r} +83 14" OAK \\ \hline 47 \end{array}$$

$$\begin{array}{r} +53 14" OAK \\ \hline 41 \end{array}$$

$$\begin{array}{r} +65 HA \\ \hline 39 \end{array}$$

$$\begin{array}{r} +65 HA \\ \hline 1 \end{array}$$

$$\begin{array}{r} +65 HA \\ \hline 34 \end{array}$$

$$\begin{array}{r} +58 4" COTTONWOOD \\ \hline 50 \end{array}$$

$$\begin{array}{r} +48 BEG B624 \\ \hline 37 \end{array}$$

$$\begin{array}{r} +48 ER \\ \hline 31 \end{array}$$

$$\begin{array}{r} +43 MH \\ \hline 18 \end{array}$$

$$\begin{array}{r} +33 WSO \\ \hline 39 \end{array}$$

$$\begin{array}{r} +99 BEG MEDIAN \\ \hline 33 \end{array}$$

$$\begin{array}{r} +51 ER \\ \hline 31 \end{array}$$

$$\begin{array}{r} +51 BEG B624 \\ \hline \end{array}$$

$$\begin{array}{r} +29 PP \\ \hline 45 \end{array}$$

$$\begin{array}{r} +22 POR \\ \hline 43 \end{array}$$

$$\begin{array}{r} +39 24" COTTONWOOD \\ \hline 47 \end{array}$$

$$\begin{array}{r} +19 MH \\ \hline 43 \end{array}$$

$$\begin{array}{r} +22 CB \\ \hline 51 \end{array}$$

$$\begin{array}{r} +28 PP \\ \hline 49 \end{array}$$

$$\begin{array}{r} +28 POR \\ \hline 42 \end{array}$$

$$\begin{array}{r} +16 BR \\ \hline 67 \end{array}$$

$$\begin{array}{r} +20 MH \\ \hline 68 \end{array}$$

$$\begin{array}{r} +20 BR \\ \hline 76 \end{array}$$

3+00

$$\begin{array}{r} +85 ER \\ \hline 69 \end{array}$$

$$\begin{array}{r} +81 MH \\ \hline 41 \end{array}$$

$$\begin{array}{r} +83 ER \\ \hline 67 \end{array}$$

$$\begin{array}{r} +79 CB \\ \hline 45 \end{array}$$

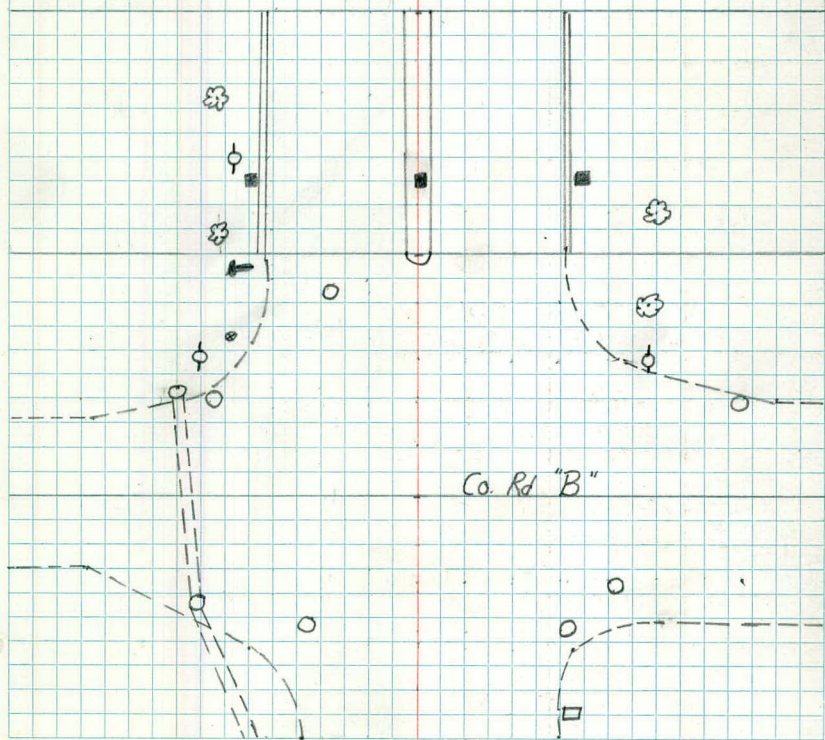
$$\begin{array}{r} +74 MH \\ \hline 27 \end{array}$$

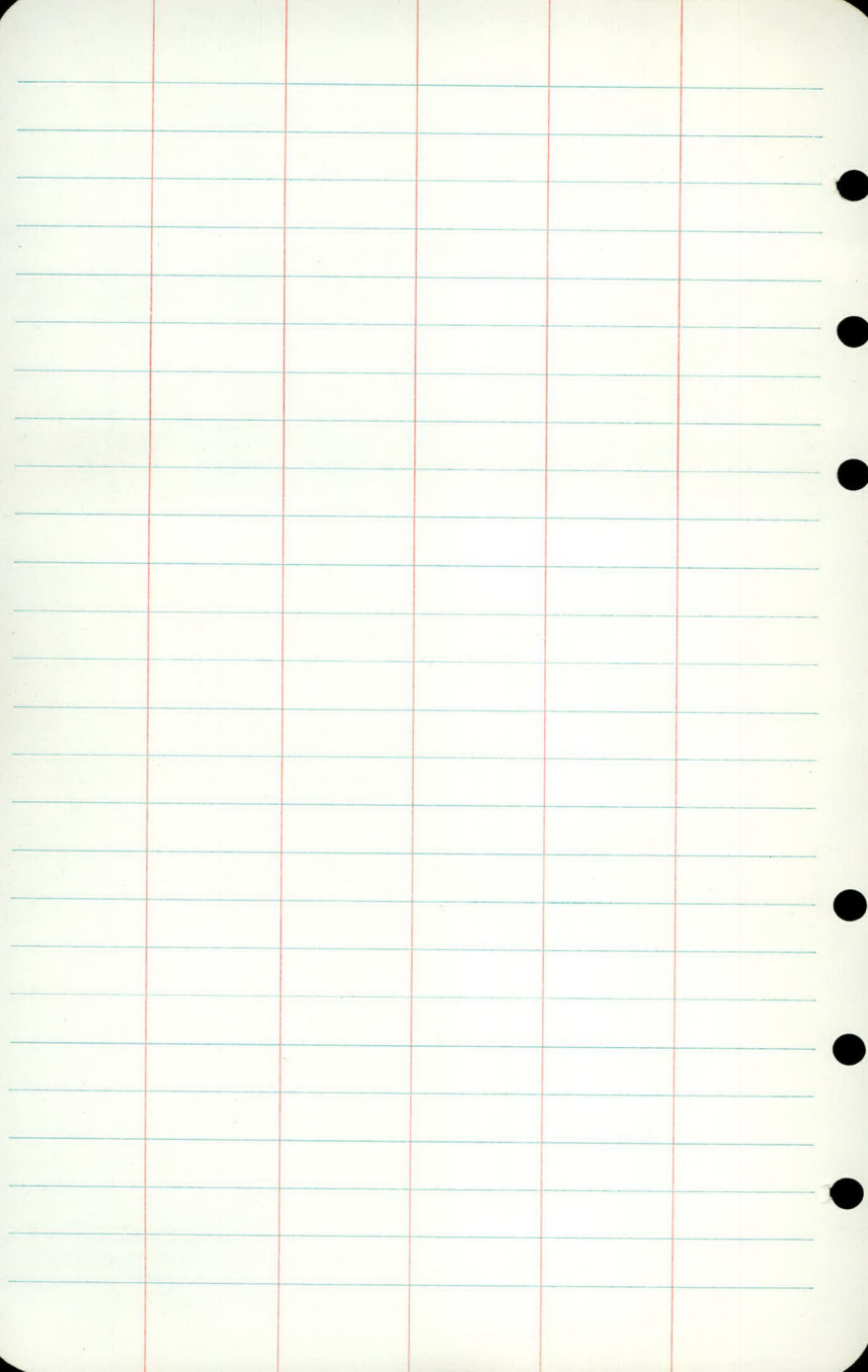
$$\begin{array}{r} +72 TELE MH \\ \hline 31 \end{array}$$

$$\begin{array}{r} +68 POR \\ \hline 35 \end{array}$$

$$\begin{array}{r} +68 POR \\ \hline 33 \end{array}$$

$$\begin{array}{r} +55 CONTROL BOX \\ \hline 31 \end{array}$$





KP
DS
CP

25 MAY 1970
P. Cloudy, Cool
55°

FAIRVIEW AVE

62-625-04

X- SECTIONS

Q+00 = 300' S. Co. Rd B

STA	+	π	-	ELEV.
BM	3.42	978.02		974.60

0+00

✓

+50

+89

6.70 71.32

+89

6.35 71.67

1+00

+50

✓

25 MAY 1970.

LT

E

RT

TOP HYD NW COR. CO. RD B & FAIRVIEW

73.2	72.3	71.7	72.4	72.0	73.0	72.6	72.2	72.8	74.4
4.8	5.7	6.3	5.6	5.2	5.0	5.4	5.8	5.2	3.6
50	38	28	22	16		12	15	29	50

73.1	72.5	71.9	72.3	72.8	72.9	72.5	72.0	72.4	74.4
4.9	5.5	6.1	5.7	5.2	5.1	5.5	6.0	5.6	3.6
50	32	27	22	14		12	18	36	50

FL CB 19' RT

FL CB 31' LT

73.0	72.4	72.3	72.6	72.9	72.4	71.8	72.2	73.0	74.2
5.0	5.6	5.7	5.4	5.1	5.6	6.2	5.8	5.0	3.8
50	39	19	14		13	21	36	46	50

STA

+

π

-

ELEV.

978.02

1+50

✓

2+00

+50

+66 = 1/2 DITCH RT

LT

£

25 MAY 1970

RT

13.1	12.8	12.1	13.1	15.6	12.2	12.6	13.0
4.9	5.2	5.3	4.9	5.4	5.8	5.5	5.0
50	30	19		19	24	37	45

13.6	13.4	13.1	13.3	13.0	13.1	13.8
4.4	4.6	4.9	4.7	5.0	4.9	4.2
50	32	19		21	33	50

13.4	14.0	13.2	13.6	13.1	12.1	13.2	13.3
4.6	4.0	4.8	4.4	4.9	5.3	4.8	4.5
50	34	22		21	25	39	50

13.1	13.2	13.6	13.6	13.4	13.1	12.5	12.0
4.3	4.8	4.4	4.4	4.6	4.9	5.5	6.0
50	32	16		17	31	36	50

STA + π - ELEV.

978.02

+72 TOP MH 31' RT

+74 TOP MH 27' LT

+79 TOP CB 45' LT

+81 TOP MH 41' RT

+84

3+00 $\neq$ Co. RD B

+19 TOP MH 43' LT

LT

E

25 MAY 1970
RT
 $\begin{array}{r} \cdot \\ 13.18 \\ 4.84 \end{array}$
 $\begin{array}{r} \cdot \\ 13.51 \\ 4.51 \end{array}$
 $\begin{array}{r} \cdot \\ 13.10 \\ 4.32 \end{array}$
 $\begin{array}{r} \cdot \\ 13.41 \\ 4.61 \end{array}$
 $\begin{array}{r} \cdot \\ 13.9 \\ 4.1 \\ 50 \end{array}$
 $\begin{array}{r} \cdot \\ 13.8 \\ 4.2 \\ 42 \end{array}$
 $\begin{array}{r} \cdot \\ 13.6 \\ 4.4 \\ 21 \end{array}$
 $\begin{array}{r} \cdot \\ 13.6 \\ 4.4 \end{array}$
 $\begin{array}{r} \cdot \\ 13.6 \\ 4.4 \\ 23 \end{array}$
 $\begin{array}{r} \cdot \\ 13.6 \\ 4.4 \\ 50 \end{array}$
 $\begin{array}{r} \cdot \\ 15.8 \\ 2.2 \\ 100 \end{array}$
 $\begin{array}{r} \cdot \\ 14.9 \\ 3.1 \\ 75 \end{array}$
 $\begin{array}{r} \cdot \\ 14.3 \\ 3.7 \\ 50 \end{array}$
 $\begin{array}{r} \cdot \\ 13.8 \\ 4.2 \\ 25 \end{array}$
 $\begin{array}{r} \cdot \\ 13.6 \\ 4.4 \end{array}$
 $\begin{array}{r} \cdot \\ 13.6 \\ 4.4 \\ 25 \end{array}$
 $\begin{array}{r} \cdot \\ 13.8 \\ 4.2 \\ 50 \end{array}$
 $\begin{array}{r} \cdot \\ 14.1 \\ 3.9 \\ 75 \end{array}$
 $\begin{array}{r} \cdot \\ 14.2 \\ 3.8 \\ 100 \end{array}$
 $\begin{array}{r} \cdot \\ 13.32 \\ 4.70 \end{array}$

STA + π - ELEV

978.02

+20 TOP MH 68' RT

+22 TOP CB 51' LT

+43 TOP MH 18' LT

+49

+49

1.80 976.38 3.44 974.58 974.6

LT

£

25 MAY 1970

RT

73.60
4.42

73.22
4.80

72.87
5.15

72.59
5.43
31
G

73.12
4.90
G

72.64
5.38
31
G

73.57
4.45
TOP

PK £ STA 27 ⁺⁵⁰ CO. RDB

STA	+	π	-	ELEV
-----	---	-------	---	------

		976.38		
--	--	--------	--	--

4+00				
------	--	--	--	--

BM				
----	--	--	--	--

+74				
-----	--	--	--	--

BM				
----	--	--	--	--

	1.86			
--	------	--	--	--

		974.52		
--	--	--------	--	--

			974.60	
--	--	--	--------	--

LT

E

25 MAY 1970
RT

71.94
444
31
6

72.45
3.93
3
6

72.88
3.50

72.48
3.90
3
6

71.95
4.43
31
6

TOP HYD NW Cor Fairview & Co RD B

70.82
5.56
31
CB

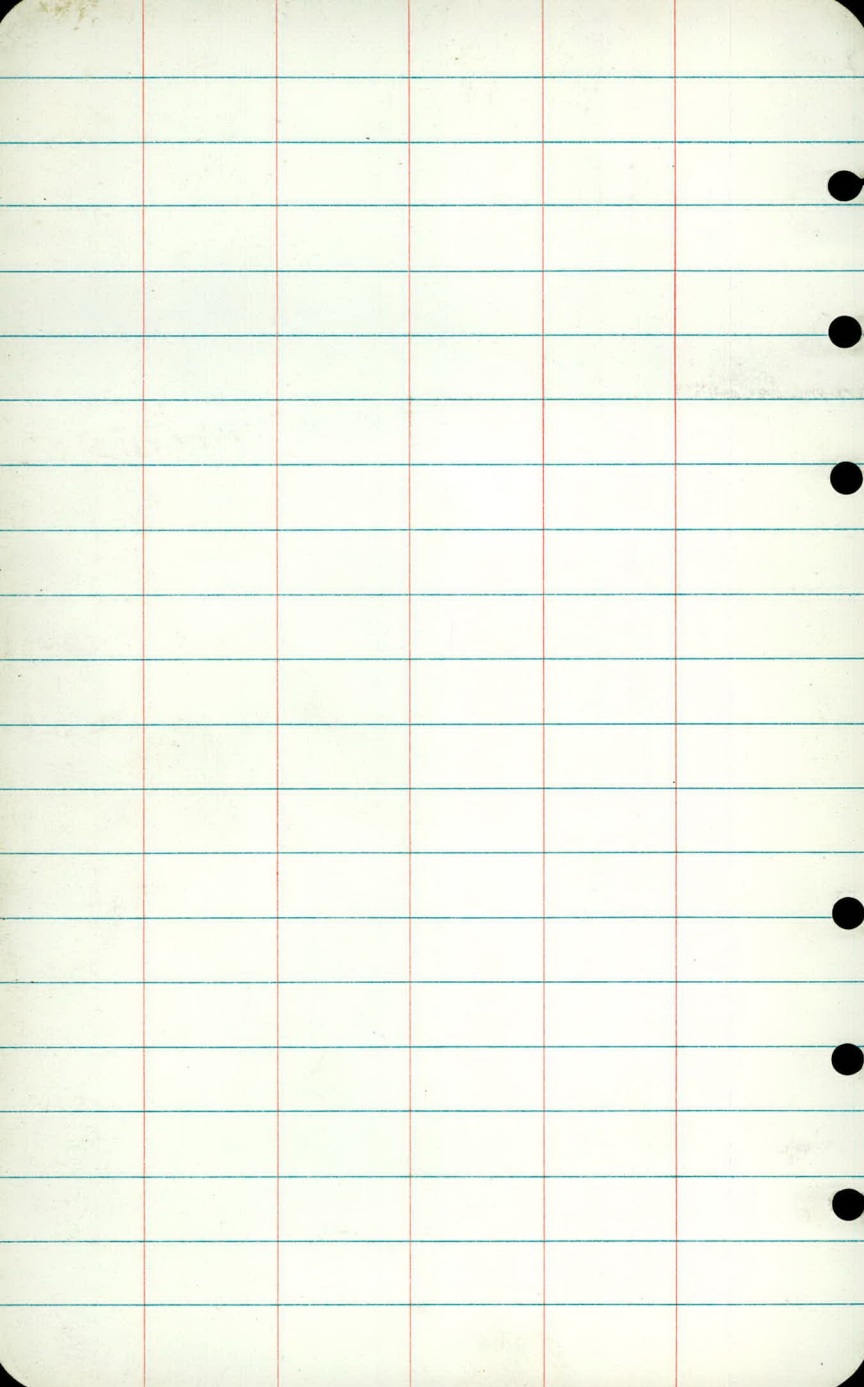
71.53
4.85
3
6

72.03
4.35

71.55
4.83
3
6

71.02
5.36
31
CB

TOP HYD NW Cor B & FAIRVIEW



MANHOLE
LOCATION
AND
ELEVATIONS

STA + π - ELEV

3.13 7.654
32

973.41

5.32 71.22

6.19 70.35 (70.35)

PK
CM
CP
BP

LT

E

June 19 1970

RT

ATC 1

Top Hyd

MH STA 3+23 LT 19'

11" casting

6 Rings

Eccentric cone streight side

To the south

Top of casting

PK STA 2+00

FL to Top = 13.02'

STA	+	π	-	ELEV
-----	---	-------	---	------

BM	0.83	8.242		981.59 ₈₃
----	------	-------	--	----------------------

			6.42	976.00
--	--	--	------	--------

			10.02	72.40
--	--	--	-------	-------

TP	0.06	72.46	10.02	72.40
----	------	-------	-------	-------

LT - E RT 2

Top Hyd STA 9+90± RT

MH STA 10+42 LT B'

11" CASTING

5 RINGS

No Cone

Conc Block Construction

FL To TOP 5.40

Top of Casting

MH STA 11+44 LT B'

11" CASTING

5 RINGS

No Cone Block const

FL To TOP = 9.38

Top of CASTING

STA	+	π	-	Elev
-----	---	-------	---	------

		72.46		
--	--	-------	--	--

MH				
----	--	--	--	--

		6.68		
--	--	------	--	--

		9.80		
--	--	------	--	--

MH				
----	--	--	--	--

		6.58		
--	--	------	--	--

BM	1.87	70.40	3.93	68.53	968.53
----	------	-------	------	-------	--------

1.87

LT

E

RT

3

MH STA 13+11 RT 17'

10" CASTING

1 RING

Eccentric cone straight

side North

FL to Top 8.04'

Top of CASTING

MH STA 13+18 LT 18'

11" CASTING

4 RINGS

WATER MAIN GATE VALVE

Top of GATE VALVE

FL to Top 9.14

Top of CASTING

Top Hyd by West Ent To School

STA	+	π	-	Elev
-----	---	-------	---	------

		70.46		
--	--	-------	--	--

MH		7.11		7.11
----	--	------	--	------

MH		6.83		
----	--	------	--	--

BM		1.33	69.07	(969.06)
----	--	------	-------	----------

CB STA 14+54 LT 21'

11" CASTING

3 RINGS

NO CONE

FL To Top 3.44

Top of Casting

MH STA 14+82 LT 35'

11" CASTING

3 RINGS

NO CONE Block const

FL To Top = 4.90

Top of Casting

TOP Hyd East Ent Fairview Jr High

STA	+	π	-	Elev
BM	2.89	71.95		969.06

MH			6.31	65.64
BM			2.89	69.06

BM	5.43	80.06		974.63
		$\begin{array}{r} 109 \\ 897 \end{array}$		$\begin{array}{r} 597 \\ 8006 \end{array}$

MH			6.79	
----	--	--	------	--

BM			1.09	78.97
----	--	--	------	-------

TOP HYD by East ENT Fairview Jr Hi

MH STA 17+35 LT 8'

11" casting

4 RINGS

No Cone conc block const

FL To Top = 5.30

Top of casting

Top Hyd NW cor Fairview EB

MH STA 26+7.4 RT 20'

11" casting

No Rings

ECC. CONE STreight side North

FL To Top = 10.20

Top of casting

Top Hyd by West Backstop

STA	+	π	-	Elev
BM.	0.48	61.29		960.81 <u>138</u> 962.19

MH			6.24	
----	--	--	------	--

BM			3.86	57.43	957.44
----	--	--	------	-------	---

	62.19	
	<u>56.81</u>	62.19
		<u>11.96</u>
10.02	5.38	50.23
<u>5.38</u>		
4.64		

Top Hyd STA 49+50 Left

MH STA 52+12

4" casting conc rectangular

No Rings

No cone Brick construct

Very poor condition

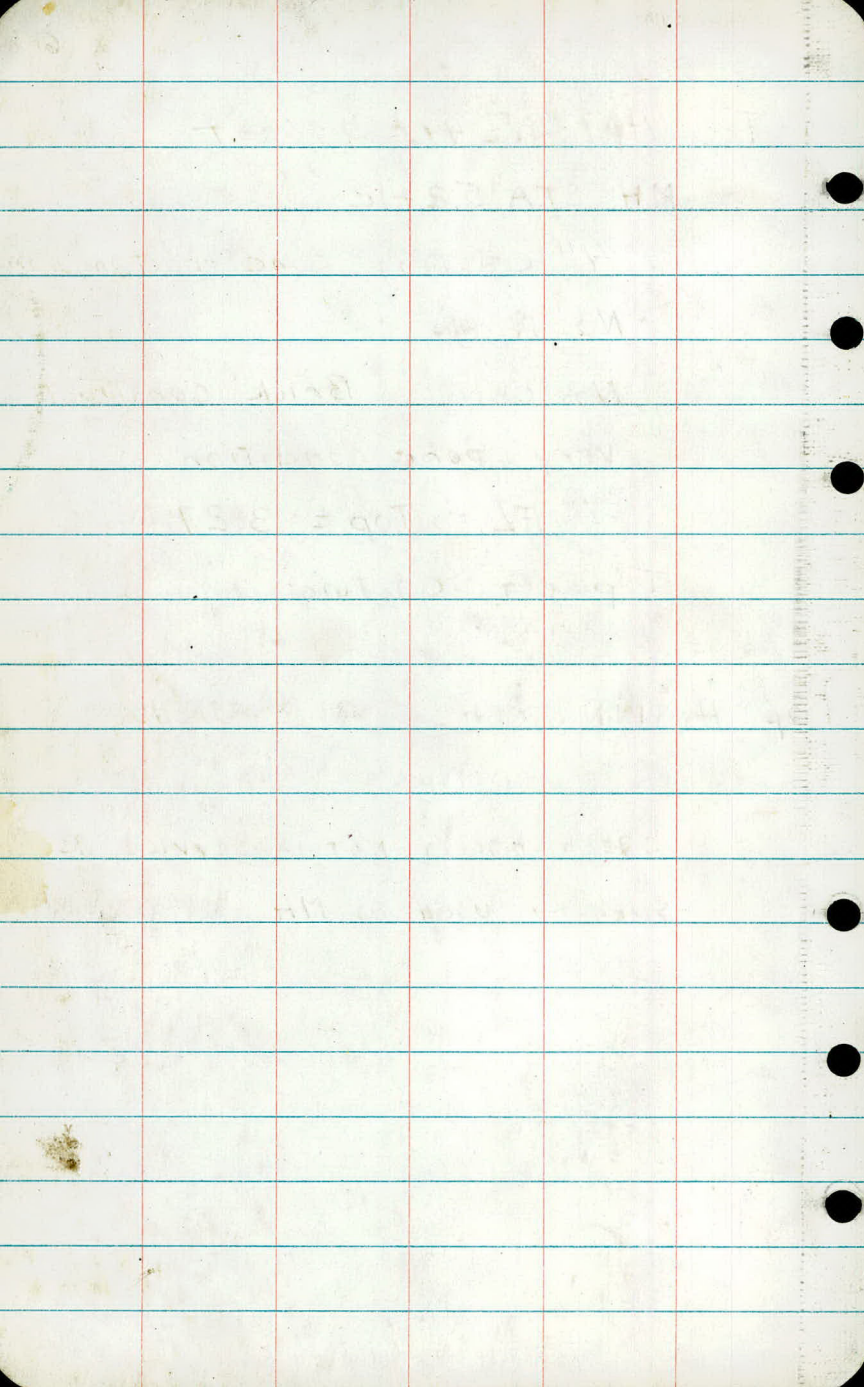
FL to Top = 3.27

Top of casting

Top Hyd NW cor Co Rd B & Snelling

catch basin NOT in service as

such → used as MH



25 62-625-04

water main

Elevations

20 +50

60

26 +50

STA	+	$\bar{A}$	-	Elev
BM	2.00	78.48		976.48
20+50		6.99 11.28	10.50	5.1 4.99
+75				
21				
+25				
+50			7.71 2.73	4.5 2.73
+75			5.0 45	5.5 4.23
22			6.93	~
+25				
+50			6.07 1.84	3.7 1.84
+75			4.23	
23				
+25				
+50			6.06	76.99
+75				
TP				
24			6.00 1.85	3.7 76.40
+25			4.15	
+50			7.07 2.56	4.0 2.56
			451 4.0	

50141 '91

PK
BP
BR
JC

Sta + π - Elev

24+75

4.9

25

8.90 3.48

3.48

+25

5.42

+50

+75

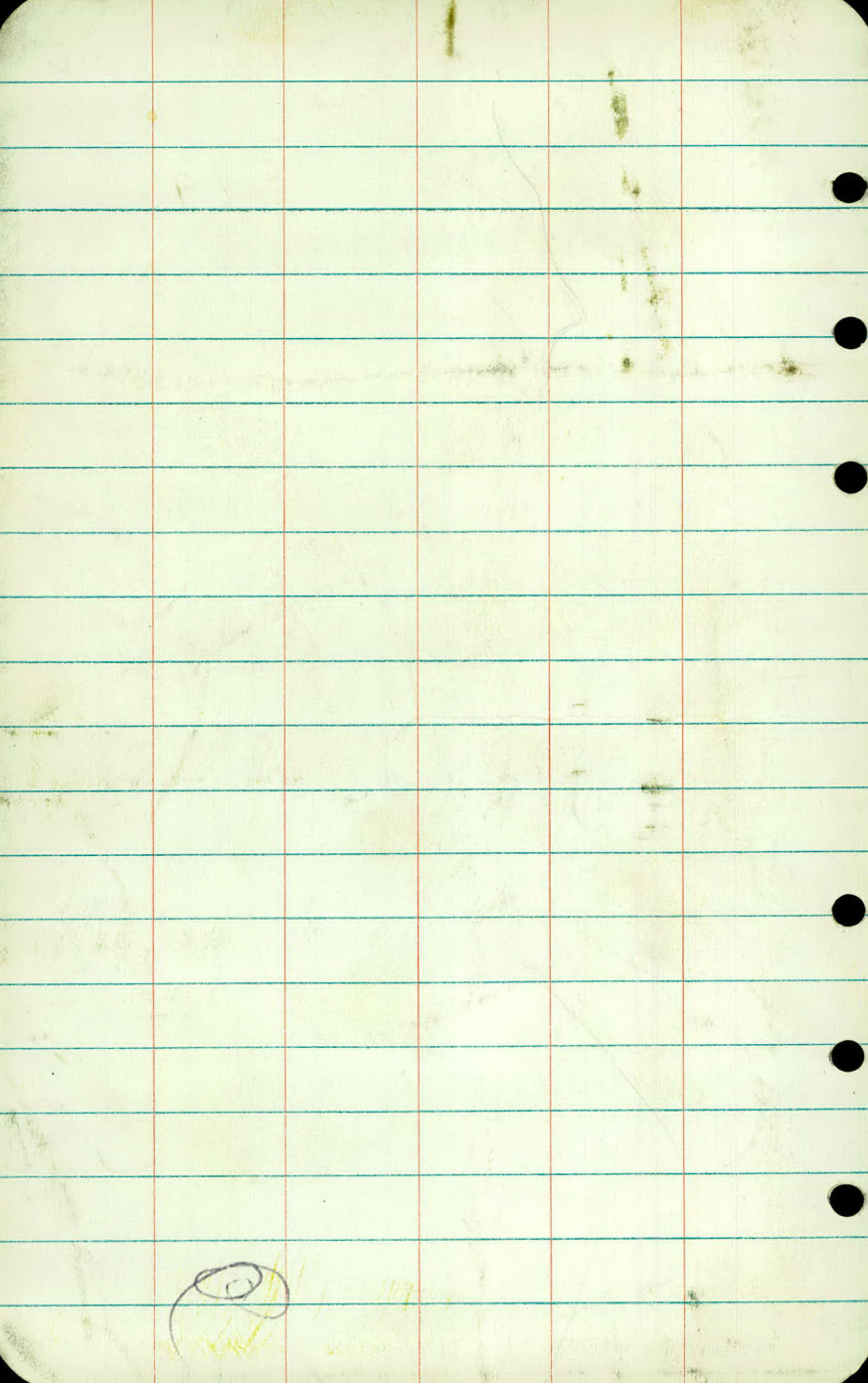
26

+25

+50

974.60

BM



62-625-04

Storm Sewer MH

Staking

Sec. Corner at Snelling

52+63.52

STA	PG	PGR	Rod	CUT
BM	1.38	962.19		960.81

MH85	956.81	5.38		
------	--------	------	--	--

2.5
7.88
2.6

10.02 4.64

533
788
255

1.34

5.38 -

6.63 on Block

* MH MOVED 15' EAST TO FIT
over watermain

11.96 950.23

BM	2.80	967.41		
----	------	--------	--	--

964.61

45 ±

4.88 62.53 62.6

+30

8.48

44+37 962.52

4.89

6.89 F2.0

+45

11.08

45+44 961.29

6.13

5.13 C1.0

4.91

+50

12.01

+38

11.86

July 17 1970 2

PK
CP
BP
DB
DT

Top HYD STA 49+50 LT

Top Pipe E. Side of MH 85

Top of Casting

FL Pipe West of MH

Top Hyd SW Cor Fry

Top 30" SCP West

Top 30" SCP East

Top pipe East 36" SCP

Top pipe West 30" SCP

Sta	PG	PGR	Red	Elev	
BM	3.18	971.85			968.67
+02	Top 24"SCP		8.50		
41+17	966.35	5.50	4.77		60.73
+20	Top 30"SCP		10.64		
BM			4.27	967.58	967.57
BM	2.34	980.30		972.96	Hyd Lt 37+00±
35 R			4.11	76.17	76.3
			5.24	75.04	75.1
BM			1.41	978.89	
					F 2.0 2.00
35+84	75.30	5.00			
+86	Top 12"SCP		10.36		
+54	Top 12"SCP		13.08		
37+55	73.72	6.58			F 1.0 t. 7.58
+56	Top 18"SCP		13.08		
+25	Top 18"SCP		12.14		
39+26	70.01	10.29			Grade
+27	Top 24"SCP		12.20		
+37	Tell MH 17'RT	10.56		969.74	

30' Down Grade
Blocks

July 24, 1970

Sta	PG	PGR	-	E/cv.
BM	7.24	975.91		968.67

39+26	70.01	5.90		Grade
-------	-------	------	--	-------

MH		6.20	969.71	969.74
----	--	------	--------	--------

Feb 16, 1971

FK + HL along with Bob Glasgow
 Located Newly built C.B on Proj.
 49+42± C.B. Clearly on R.W as
 back of C.B is 32.65' from £.

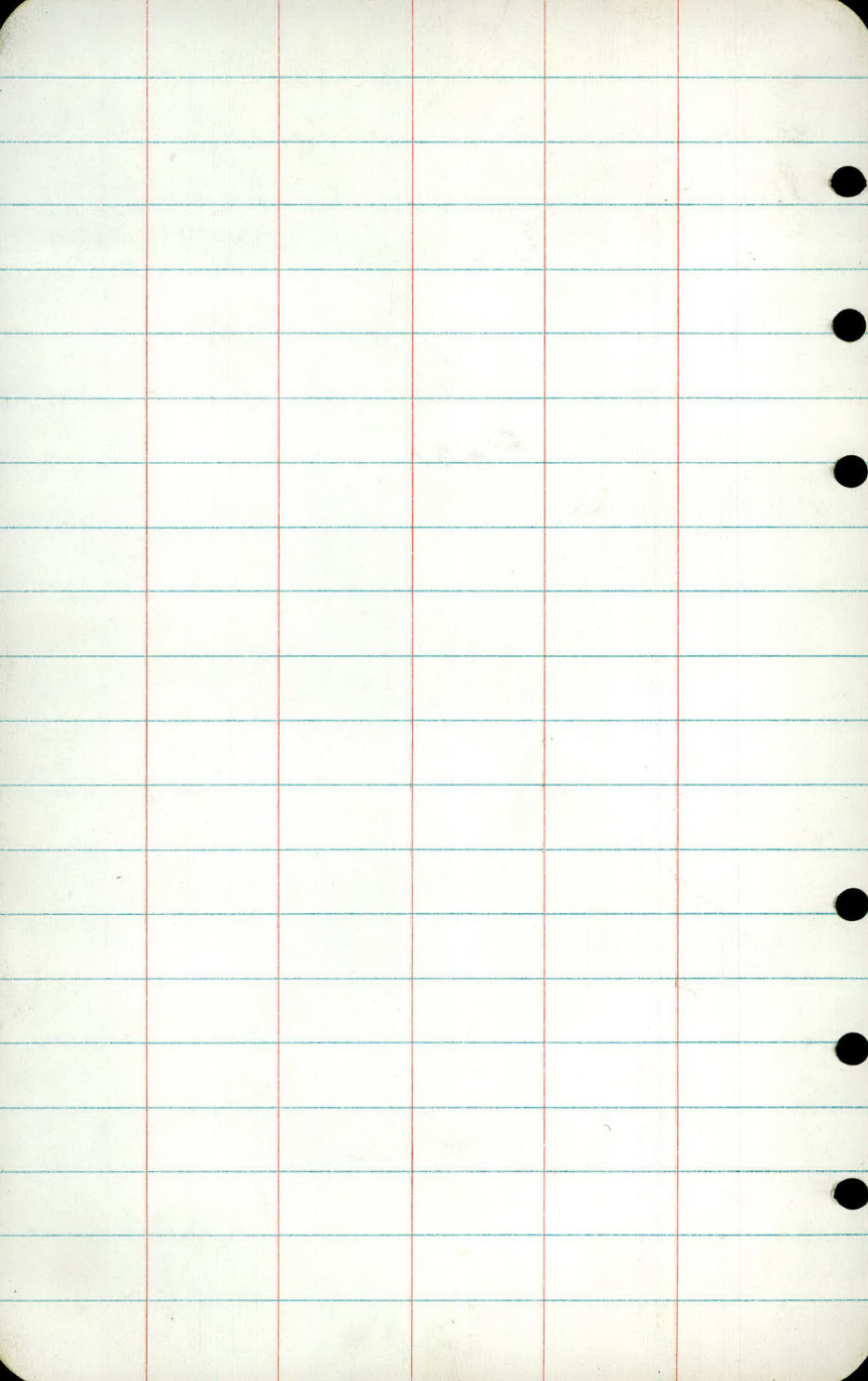
50+95± C.B Ctr is 31.3' R to £

The Back plate will still be
 within the R-W. The stub
 to E.N.E. however is somewhat
 South of £ necessitating the
 Construction of catchbasin
 to be somewhat beyond the
 33' R-W Line

JK

Top Hyd NW Corner Middleton Rd + B

2



62-625-04

Sta PG PGR - Elev.

BM 2.68 967.29

964.61

423 3.06 963.05 ✓

45+24.75 61.67 5.62
+ 37 61.47
+ 94 61.39

45+44.75 61.38 5.91
29

146
12
492
146
1732

BM 3.81 972.41

968.60 Top Hnd
Mid/Bottom

4.78 67.63 67.62

41+10.30
31
40+79
20

475
593
15.7

40+59.3 67.44 4.97
28

41+75 67.16
8

40+79.3 67.08 5.33 ✓

August 7, 1970

2

Top Hyd S.W. Cor Fry & ^BC

45 + 75.75

41

45 + 34.75

- 10

24.75

20

4

5.40
5.70

5.50
5.60

5.28
+ 0.6% Grade to S

5.40
6.00

.018
4.3
54
72
0774

13.7
.018
1256
157
2826

Curb Grade

Sta	+	π	-	Elev.
BM	1.59	962.40		960.81

49+10	57.20	5.20		
-------	-------	------	--	--

+30	57.09	5.31		
-----	-------	------	--	--

+32	57.07	5.33		
-----	-------	------	--	--

+52	56.96	5.44		
-----	-------	------	--	--

BM	0.34	961.15		960.81
----	------	--------	--	--------

Sta 51 ±

4.96	56.2	56.2		
------	------	------	--	--

50+85	56.17	4.98		
-------	-------	------	--	--

50+95	56.18			
-------	-------	--	--	--

51+05	56.05	5.10		
-------	-------	------	--	--

M14	56.03	5.12		
-----	-------	------	--	--

August 12, 1970

3

Top Hyd 31' Lt Sta 49+44

✓

34.5' Lt

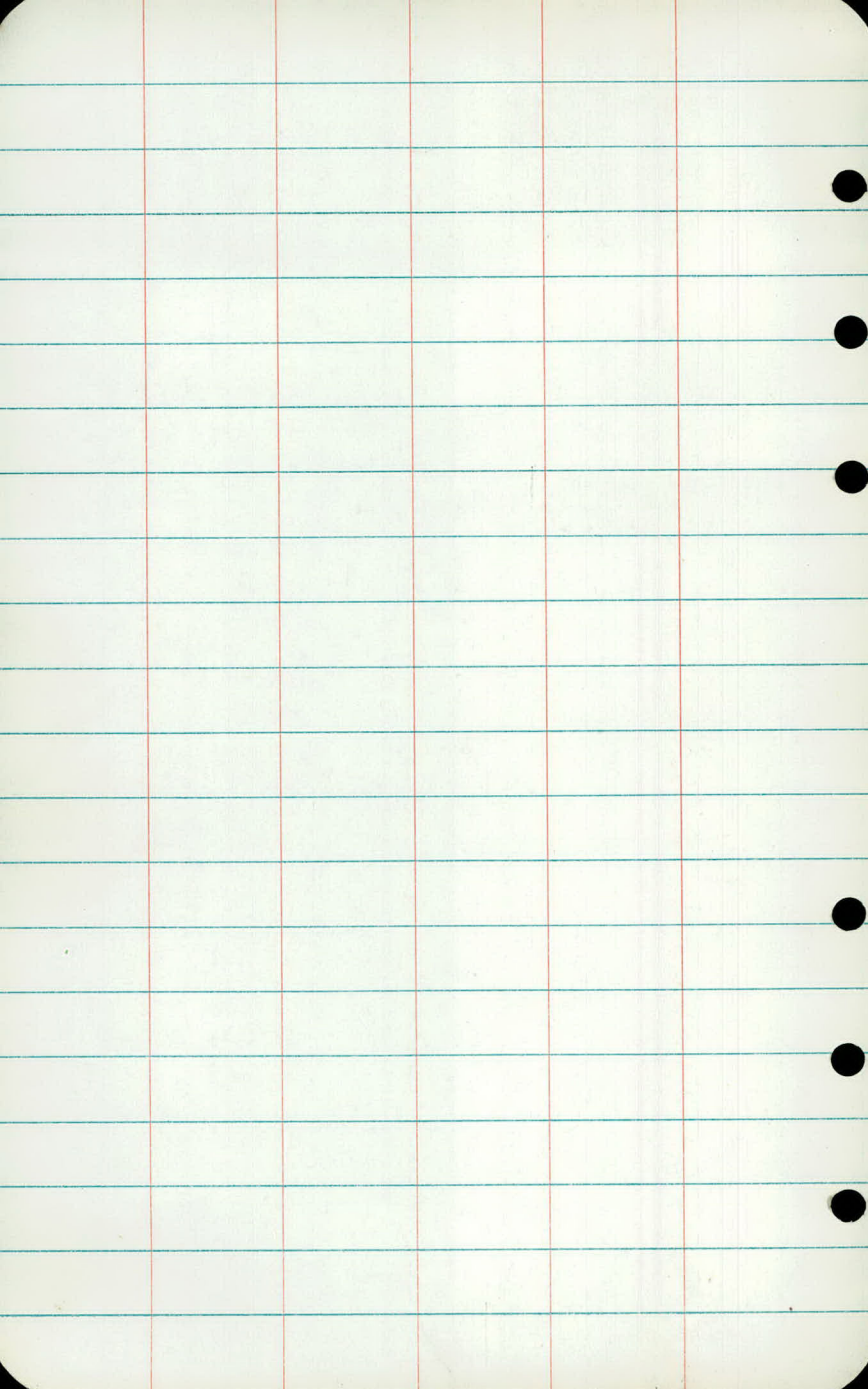
✓

✓

Rt 31'

✓

August 13, 1970



Co Rd "B"

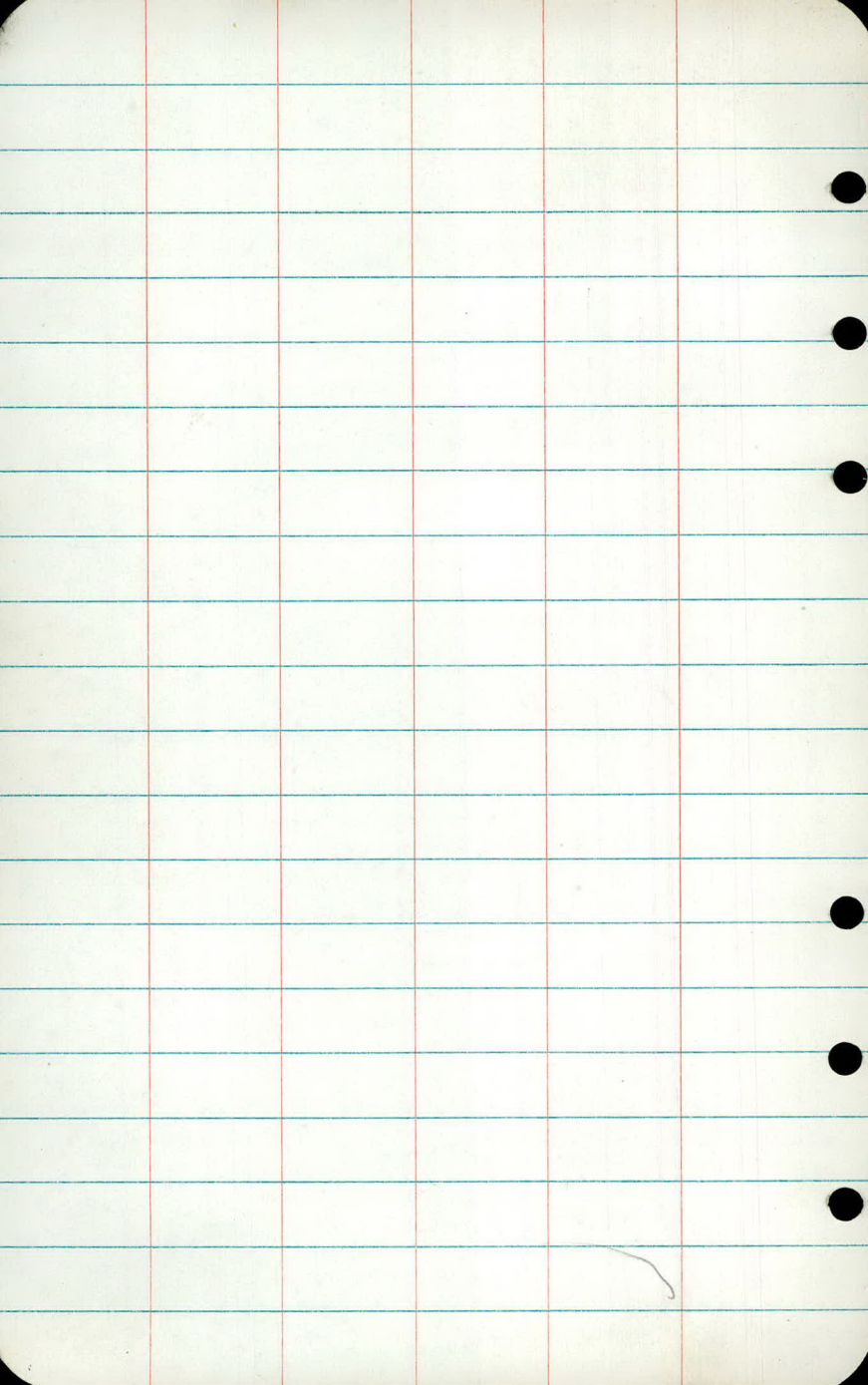
41+10.307

30'

90'

81'

30'



HADDINGTON RR

60'

Brick
Apt
Bldg

154.38'

131.21'

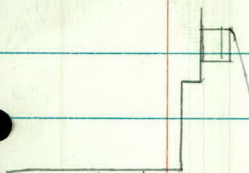
30'

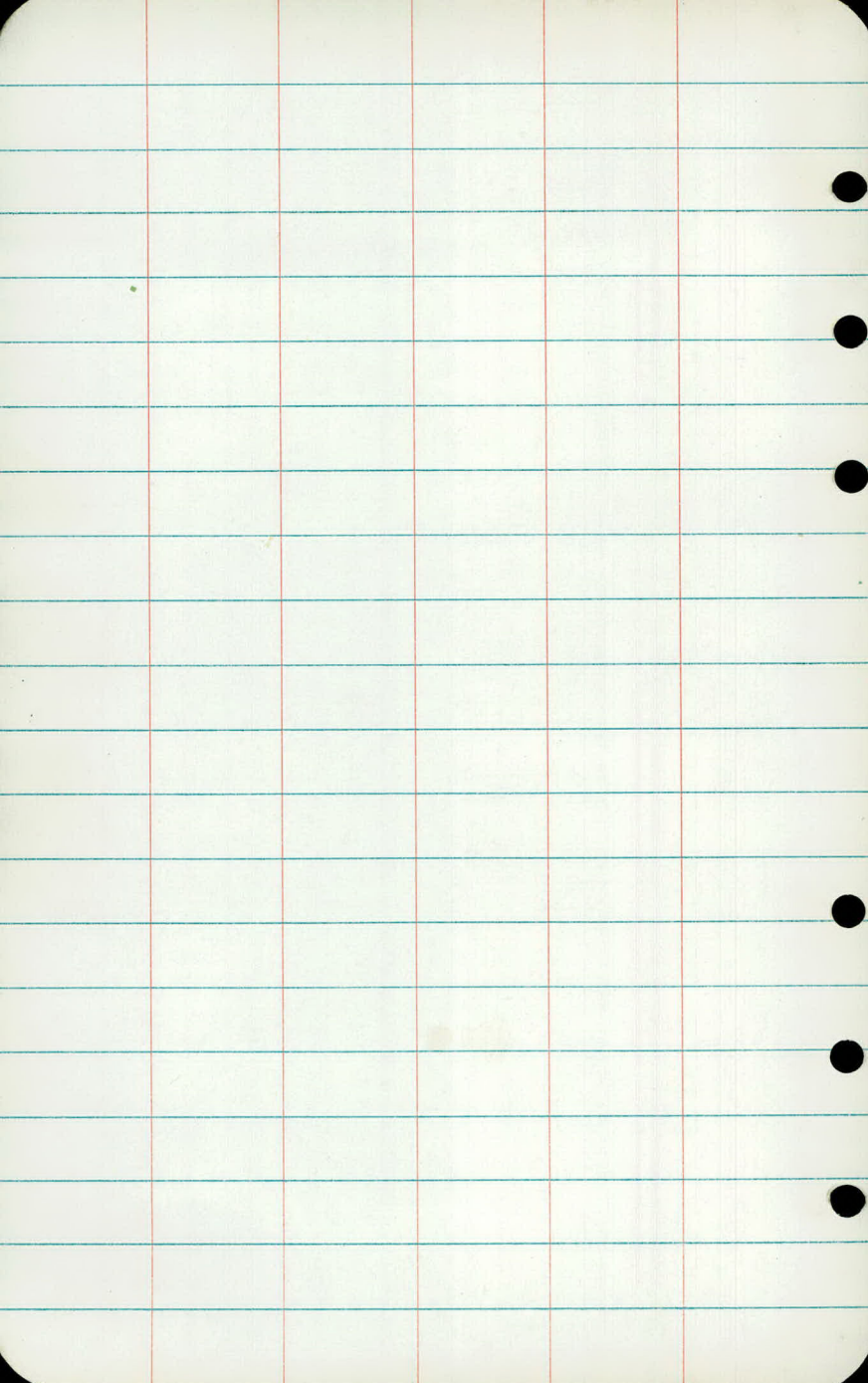
PK

found
iron

64.28'

60.28





Apt Bldg

8' 8" 8"

8' 4" 13"

50' 44"

4' 4" 57"

30'

Found Iron

0 3N
PP

Fry St.

Iron tipped

Eldridge

30'

Found Iron

$$\begin{array}{r}
 1245 \\
 348 \\
 \hline
 99.60
 \end{array}$$

$$1245$$

$$1345$$

$$1245.$$

$$\begin{array}{r}
 12 \overline{) 14939.60} \\
 \underline{12} \\
 29 \\
 \underline{24} \\
 53 \\
 \underline{48} \\
 59
 \end{array}$$

$$\begin{array}{r}
 3 \\
 577.60 \\
 4220 \\
 \hline
 12 \overline{) 34760} \\
 90 \\
 \underline{96} \\
 114920 \\
 \underline{114937.60}
 \end{array}$$

FK
DS
RG
BW

June 10, 1974
Rain 55°

1

Co. Rd. "B"

at

Snelling

+63.2 Mon

+33

+30.2

+20

+12

52

L

Curb Rt

2

40.62

36.6

32.54

Pac CB

32.65

32.08

886.00

BM

SE Cor
883.82 Outlet Street
are
Owasso

Elev 886.19