

Book #9 Dr. 12-A

OFFICE OF COUNTY ENGINEER
RAMSEY CO. MINN.

Plan Survey

DEEBACH ROAD

From Relocation of 84" C.M. Culvert

Road Acc't. No.

Date Filed 6-11-35

File

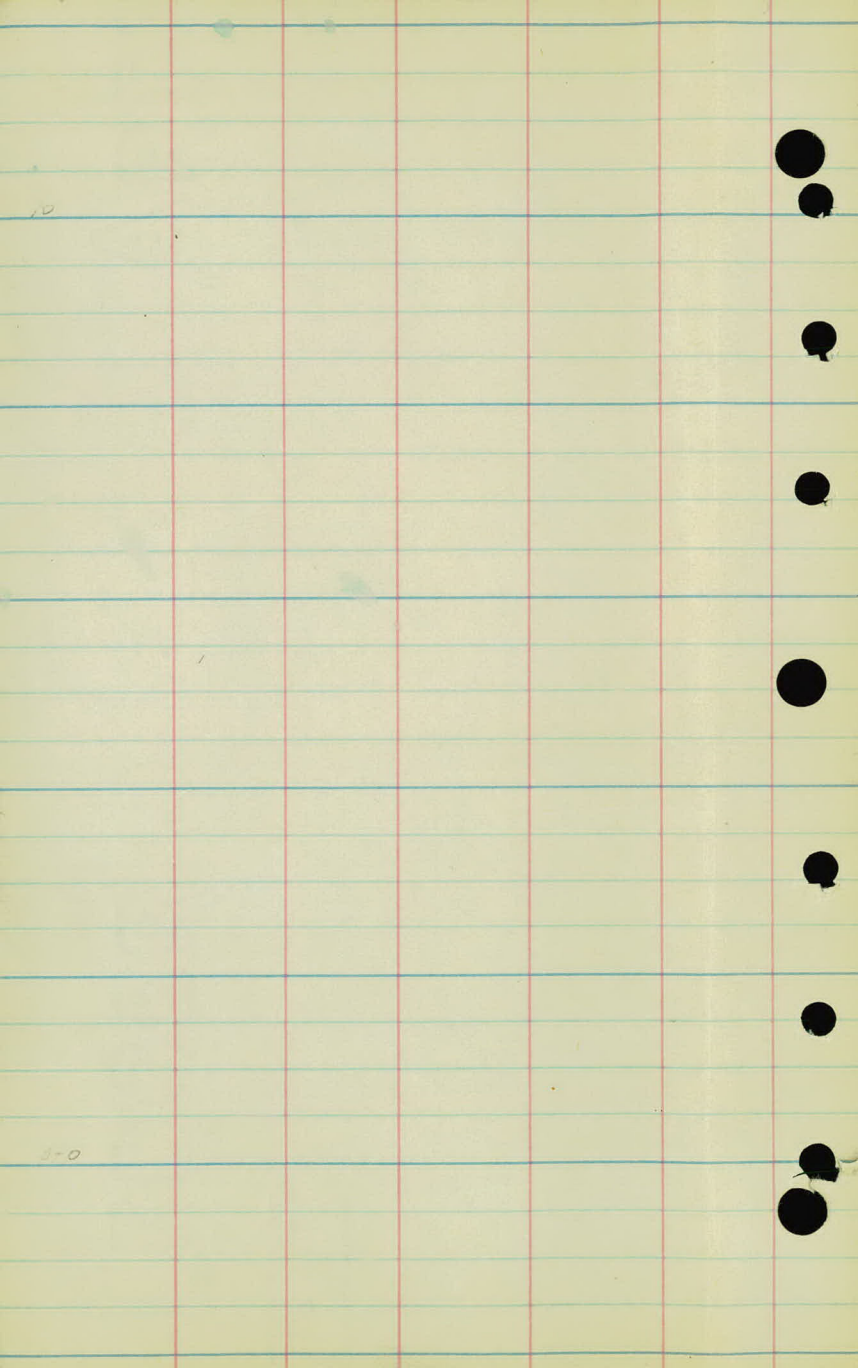
Plan Survey
DEEBACH ROAD
CULVERT
34-N-22

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Mo/ 23, 1935

W. H. Carlson
A. D. Crombuto
L. D. Goldberg



Alignment

Sta.

Point.

13+22.35

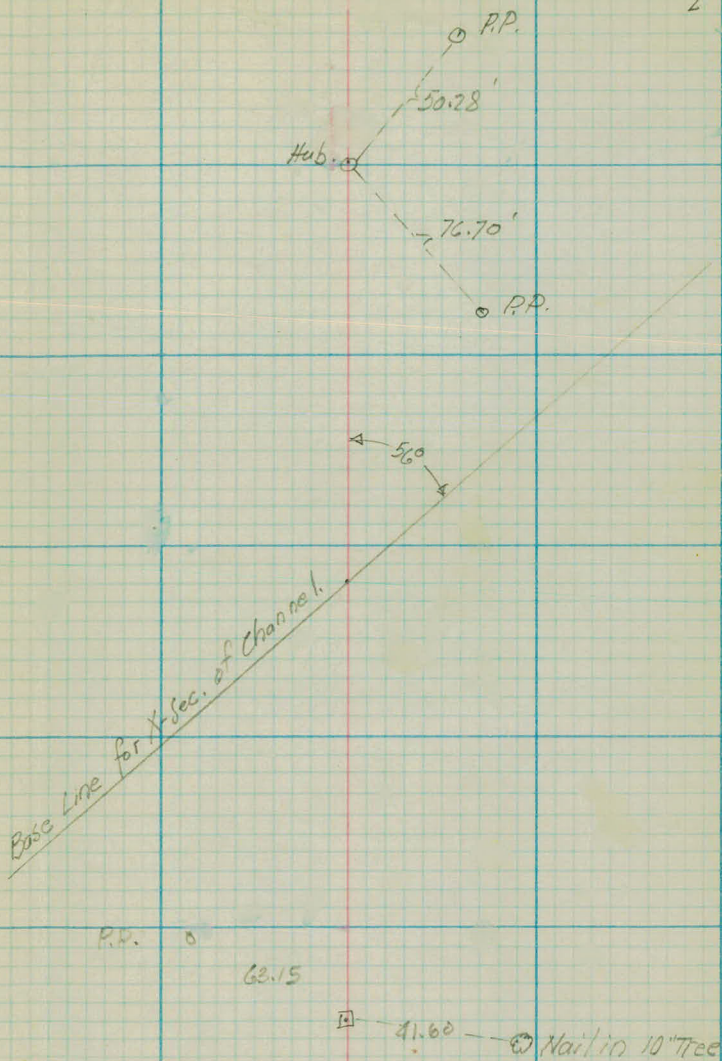
P.O.T.

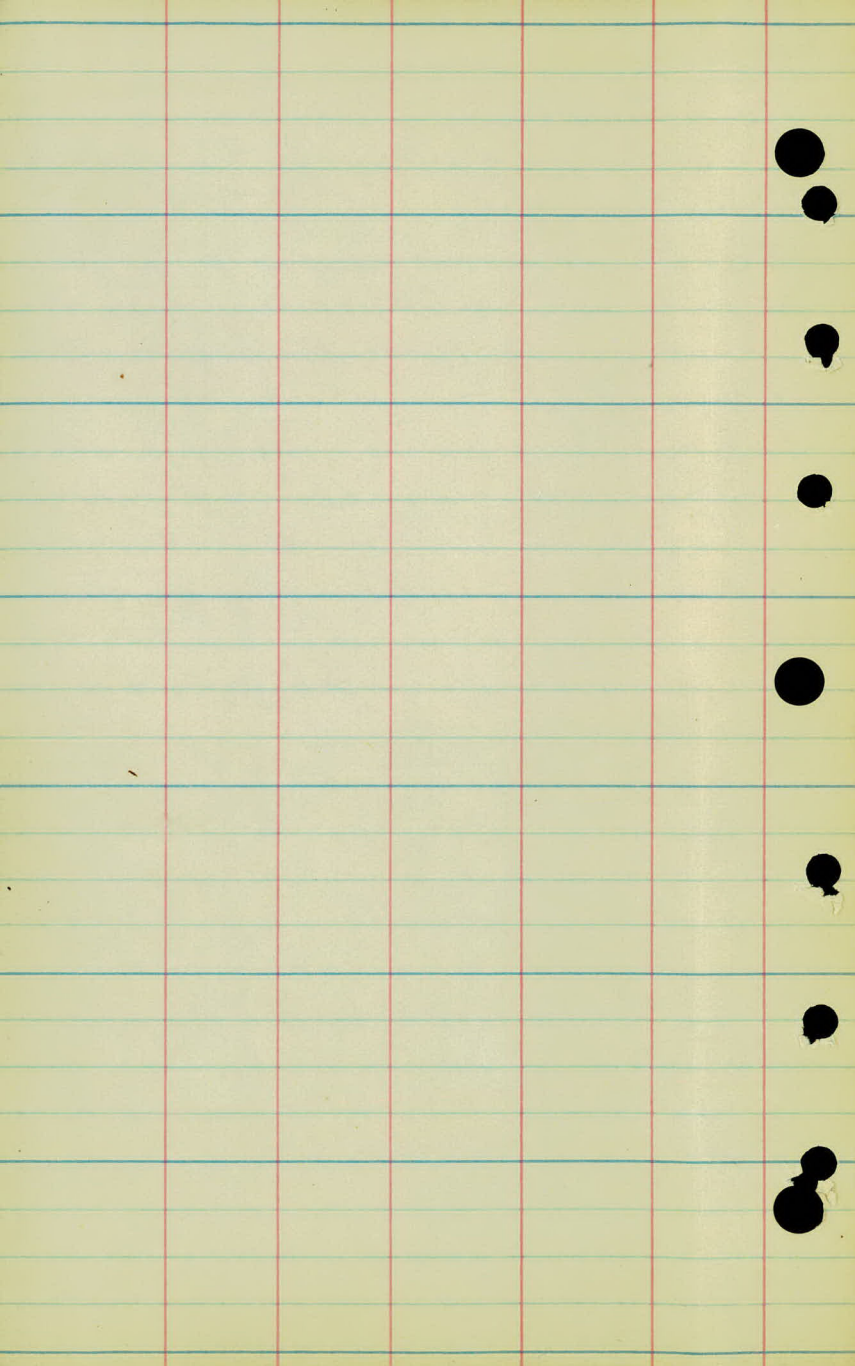
7+00

P.O.T.

4+00

Mod. P.O.T.





Topography
Deebach Road
Culvert.

8+0

7+50

7+0

6+50

84" X 70.6' c.m. cu/v.

Sag



S/B. 7.0

Sec A-A

6+0

5+50

5+0

W.H.C.

A.D.C. May 23, 38

L.D.G.

4

+14-F. Cot. 76

F-76

F-31

+73-P.P. 18

+73-14' oak & Fern ^{B. 44}
32'

F-27

+50-20" Tree 53

(7 Large Boulder
1/2 c. each)

+73-10' Tree 52

F-27

Note:
see +500
for Loc. 42 Chan.
Base Line for
X-sec.

+81-E. 84' C.M. 25

+84-E.W.W. 38

+78-E. C.M. 29

+63-8' Branch 22

24' X 30' C.M.

+55-E. C.M. 33

+50-E. C.M. 38

+50-F-33

+37-P.P.
191

F-32

F-32

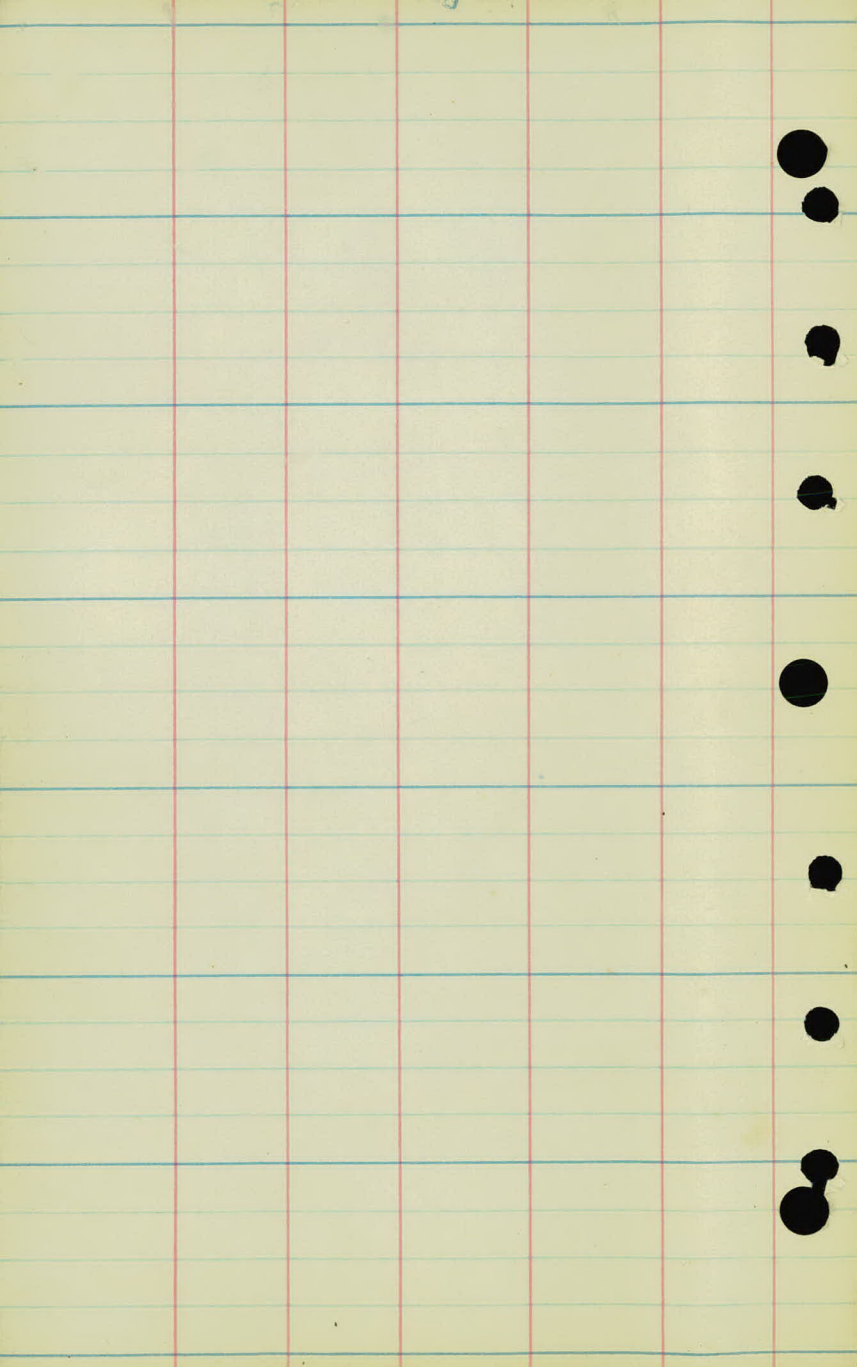
+72-F. 29

F-29

Scale 1" = 50'

F-20

+12-Tree 14, rpp
171



Levels +
Cross-sections.

Sta.	+	Σ	-	Elev.
	0.68	894.94		894.26
5+50				94.0
+77				91.9
6+0				90.3
+22				89.1
+50				87.9
+65				87.4
7+0				88.5
+25				88.9
+80				90.2
+65				91.1
8+0				93.5
T.P.	2.89	884.16	13.67	881.27

47.

£

Pl.

6

Spike in 15" Oak 30' Rt. Sta. 7470

$$\begin{array}{ccccccc} 10.6 & 10.6 & 3.3 & 3.2 & 1.4 & 0.9 & 1.0 & 2.5 & 2.5 \\ \hline 33 & 26 & 21 & 17 & 13 & - & 13 & 17 & 21 \end{array}$$

955 955 91.6 91.7 93.5 94.2 93.9 92.4 92.4

3.9	3.9	5.8	5.3	3.3	3.0	2.8	4.2	4.1	1.6
<u>4.0</u>	<u>2.8</u>	<u>2.3</u>	<u>1.9</u>	<u>1.3</u>		<u>1.2</u>	<u>1.7</u>	<u>2.2</u>	<u>2.5</u>

91.0 91.0 89.1 89.6 91.6 91.9 92.1 90.7 90.8 93.3

— — — $\frac{4.7}{12}$ $\frac{4.6}{11}$ $\frac{4.5}{13}$ $\frac{6.2}{18}$ $\frac{6.4}{23}$ $\frac{4.2}{26}$ $\frac{1.6}{28}$ $\frac{7.0}{46}$ $\frac{7.0}{50}$

90.2 90.3 90.4 88.7 88.5 90.7 93.9 97.9 97.9

$$\frac{62}{11} \quad \frac{58}{12} \quad \frac{64}{13} \quad \frac{84}{26} \quad \frac{89}{34} \quad \frac{439}{34}$$

88.7 89.1 88.8 86.5 86.0 98.8

$$- \quad - \quad - \quad \frac{7.7}{12} \quad \frac{7.0}{12} \quad \frac{7.0}{12} \quad - \quad - \quad -$$

87.2 87.9 87.9

$\frac{79}{11}$ $\frac{7.5}{1}$ $\frac{76}{12}$ - - -

87.0 87.4 87.3

$$\begin{array}{r} 12.9 \\ \underline{40} \end{array} \quad \begin{array}{r} 12.9 \\ \underline{29} \end{array} \quad \begin{array}{r} 13.8 \\ \underline{27} \end{array} \quad \begin{array}{r} 13.7 \\ \underline{23} \end{array} \quad \begin{array}{r} 7.1 \\ \underline{13} \end{array} \quad \begin{array}{r} 6.4 \\ \underline{\quad} \end{array} \quad \begin{array}{r} 6.6 \\ \underline{8} \end{array} \quad - \quad - \quad -$$

82.0 82.0 81.1 81.2 87.8 88.5 88.3

$\frac{11.5}{40}$	$\frac{11.5}{28}$	$\frac{10.6}{24}$	$\frac{9.7}{19}$	$\frac{6.2}{13}$	$\frac{6.0}{9}$			
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83.4 83.4 84.3 85.2 88.7 88.9 88.9

$\frac{8.7}{40}$	$\frac{7.6}{27}$	$\frac{7.0}{22}$	$\frac{7.1}{18}$	$\frac{5.0}{14}$	$\frac{4.7}{12}$	$\frac{4.9}{12}$	$\frac{6.6}{17}$	—	—	—
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86.2 87.3 87.9 87.8 89.9 90.2 90.0 88.3

$\frac{7.6}{40} \quad \frac{6.4}{27} \quad \frac{5.5}{23} \quad \frac{6.2}{22} \quad \frac{6.2}{18} \quad \frac{4.4}{14} \quad \frac{3.8}{13} \quad \frac{4.0}{13} \quad \frac{4.4}{16} \quad \frac{5.0}{17} \quad \frac{5.7}{24} \quad \frac{4.7}{29} \quad \frac{5.2}{38} = T_{60}$
 1306

87.3 88.5 89.4 88.7 88.7 90.5 91.1 90.9 90.5 89.9 89.2 90.2 89.7

$\frac{20}{40}$	$\frac{20}{29}$	$\frac{14}{25}$	$\frac{34}{22}$	$\frac{34}{18}$	$\frac{18}{14}$	1.4	$\frac{2.1}{13}$	$\frac{3.2}{16}$	$\frac{34}{20}$	$\frac{0.4}{26}$	$\frac{0.0}{32}$
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72.9 72.9 73.5 91.5 91.5 93.1 93.5 92.8 91.7 91.5 94.5 94.9

Sta.	+	π	-	Elev.
6+50		884.16		

6+65

7+0

+25

+50

T.P.	8.38	881.81	10.73	873.43
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at 100 = 56° Rt. at Sta. 7+00

1+00

1+50

T.P.	2.05	871.01	12.85	868.96
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Lt. 2 Rt. 7

-3.7 $\frac{2.5}{75}$ $\frac{6.3}{83}$ $\frac{6.0}{86}$ $\frac{0.0}{43}$
 81.7 77.9 78.2 84.2

Inlet of 30" Culv. 7.70 76.5

-3.2 $\frac{4.0}{75}$ $\frac{5.0}{79}$ $\frac{5.0}{89}$ $\frac{0.0}{49}$
 80.2 79.2 78.8 84.2

Outlet 30" Culv. $\frac{10.70}{72.5}$

Inlet 84" Culv. $\frac{15.2}{69.0}$

-4.3 $\frac{7.1}{75}$ $\frac{10.8}{84}$ $\frac{11.2}{38}$ $\frac{6.5}{47}$ $\frac{1.5}{55}$
 77.1 73.4 73.0 77.7 82.7

-4.7 $\frac{6.1}{75}$ $\frac{13.0}{87}$ $\frac{13.6 = \text{chan} = 13.5}{39}$ $\frac{8.2}{44}$ $\frac{8.2}{51}$
 78.1 71.2 70.6 70.7 76.0
 $\frac{0.0}{72}$ $\frac{4.0}{62}$
 84.2 80.2

-6.0 $\frac{1.0}{75}$ $\frac{8.0}{87}$ $\frac{10.2}{46}$ $\frac{12.7 = \text{chan} = 13.0}{54}$ $\frac{13.0}{59}$
 83.2 76.2 74.0 71.5 71.2
 $\frac{0.0}{82}$ $\frac{4.0}{75}$ $\frac{6.5}{70}$ $\frac{8.7}{67}$
 84.2 80.2 77.7 75.5

Lt. 2 Rt.

S.S. $\frac{1.8}{33}$ $\frac{5.4}{27}$ $\frac{9.4}{79}$ $\frac{10.1}{13}$ $\frac{9.4}{7}$ $\frac{5.1}{0}$
 80.0 76.4 72.4 71.7 72.4 76.1

S.S. $\frac{0.0}{42}$ $\frac{3.6}{40}$ $\frac{8.7}{33}$ $\frac{7.0}{27}$ $\frac{6.6}{5}$ $\frac{0}{0}$
 81.8 74.2 73.1 72.8 75.2

Sta.	+	π	-	Elev.
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871.01

0+0 = 124°-Lt. of Sta. 7+0

1+0

1+50

Flow Line 84" Culvert Outlet 4.08

6+22

6+50

6+65

T.P.	12.24	881.14	2.11	868.90
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6+0

T.P.	13.18	894.11	0.21	880.93
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B.M.			40.13	894.24
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Lt.

E

Rt.

8

$$45^\circ \text{ slope } \frac{28}{32} \frac{28}{27} \frac{54}{22} \xrightarrow{\text{Echan}} \frac{58}{18} \frac{47}{10} \frac{15}{0}$$

$$70.4 \ 68.5 \ 65.6 \ 65.2 \ 66.3 \ 69.5$$

$$45^\circ \text{ slope } \frac{17}{16} \frac{58}{11} \xrightarrow{\text{Echan}} \frac{59}{0} \frac{64}{11} \frac{35}{15} \frac{30}{35}$$

$$69.3 \ 65.2 \ 65.1 \ 64.6 \ 67.5 \ 68.0$$

$$66.9$$

$$\frac{1.0}{60} \frac{0.0}{48} \frac{1.3}{44} \frac{0.2}{40} -18.1$$

$$70.0 \ 71.0 \ 69.7 \ 70.8$$

$$\xrightarrow{\text{Echan}} \frac{5.0}{65} \frac{4.1}{39} -16.9$$

$$66.0 \ 66.9$$

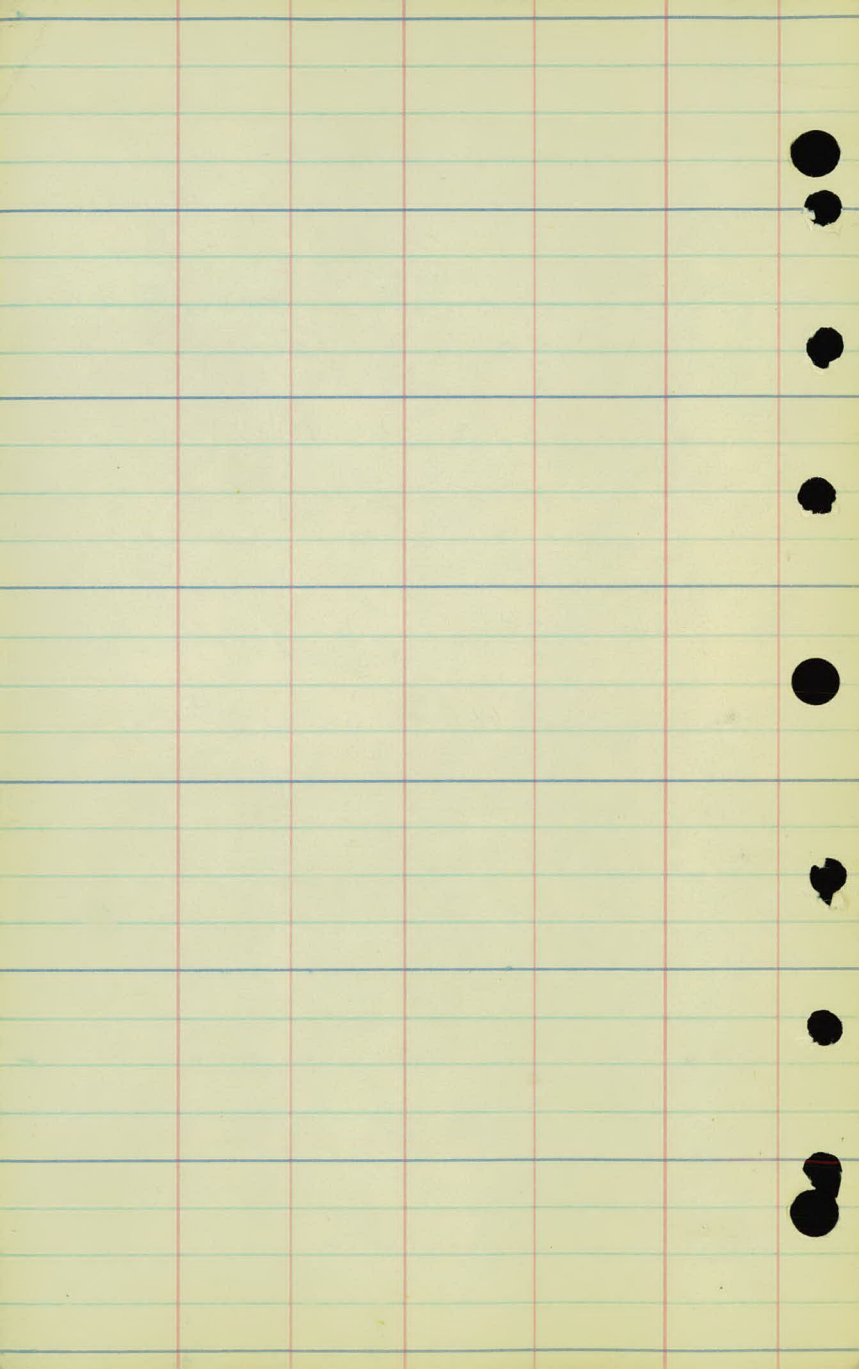
$$\frac{13.0}{60} \frac{0.0}{52} \frac{1.7}{43} \frac{0.3}{40} -16.4$$

$$74.0 \ 71.0 \ 69.3 \ 70.7$$

$$-9.2$$

$$\frac{6.0}{52} \frac{4.7}{44} \frac{3.0}{33} \frac{0.5}{28}$$

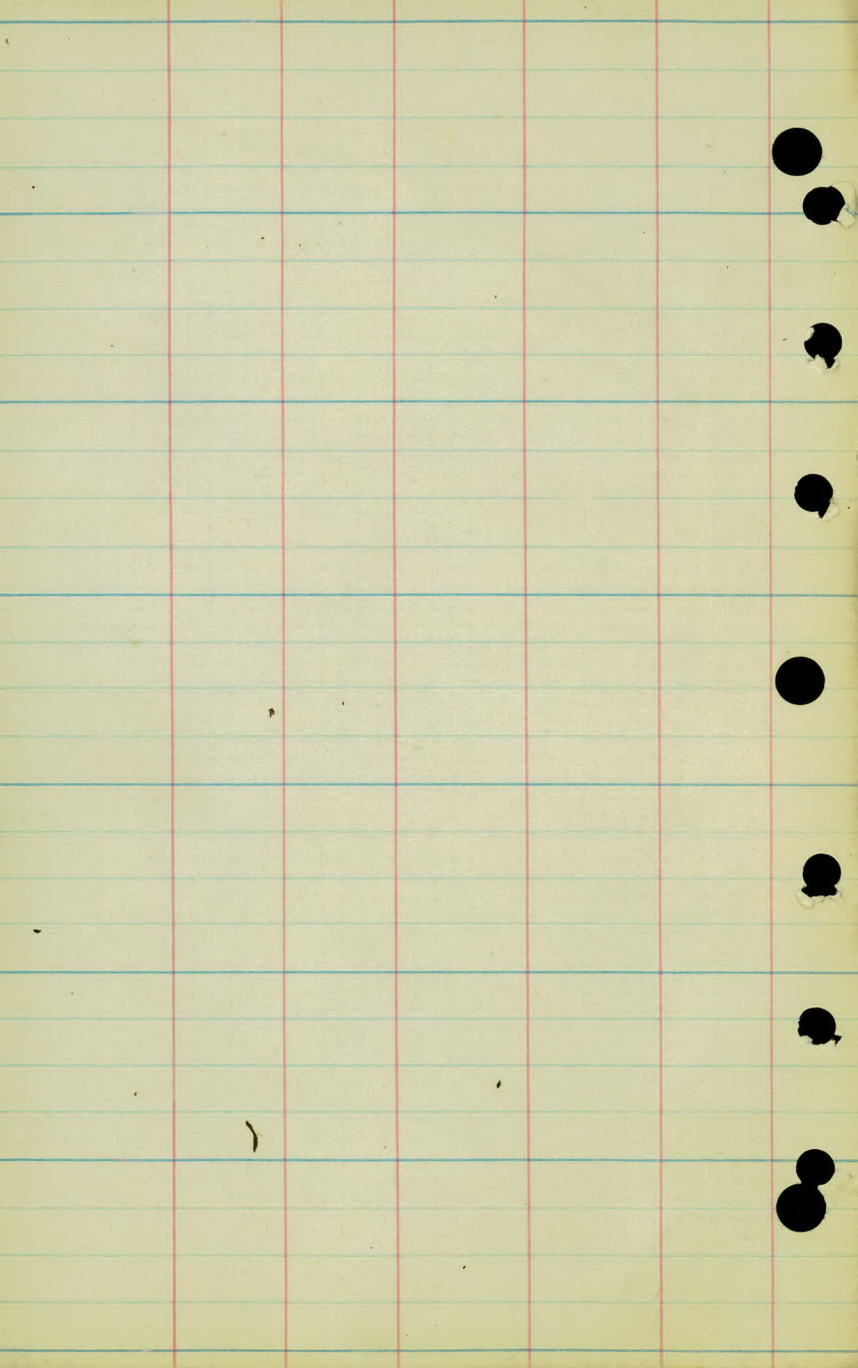
$$75.1 \ 76.4 \ 78.1 \ 80.6$$



Check on
Proposed Location
of Culvert
Deebach Road.

B.M.	0.60	✓ 894.86		894.26	
6+50					
6+65					
6+80					
0+00 = 6+92			6.5		88.4
0+11 - Rt.			6.4		88.5
0+16 Lt.			7.5		87.4
T.P.	1.59	✓ 884.25	12.20	✓ 882.66	
{ 0+50 Rt. = Toe of Slope.			12.3		72.0
{ 6'-Rt. of 0+50 Rt. = $\frac{1}{2}$ channel.			14.0		70.3
{ 0+59 - Rt.			13.0		71.3
{ 4'-Rt. of 0+59 Rt. = $\frac{1}{2}$ channel			13.6		70.7
{ 0+70 Rt.			12.8		71.5
{ 3'-Rt. of 0+70 = $\frac{1}{2}$ channel			13.3		71.0
T.P.	0.36	✓ 871.34	13.27	✓ 870.98	
0+55 Lt. = Toe Slope			3.8		67.5
0+61 - Lt.			4.7		66.6
0+70 - Lt.			4.6		66.7
4' N. of 0+70 Lt. = $\frac{1}{2}$ channel			5.0		66.3
T.P.	12.01	✓ 882.88	0.47	✓ 870.87	
B.M.			11.42		
T.P.	12.73	✓ 894.91	0.70	✓ 882.18	
B.M.			0.66	✓ 894.25	

Top large Rock Lt. G+30



Deebach Road
Extension to Culvert

W. H. Carlson
April 20, 1937

Lt

Rt.

(101)

2 to $\pm$ than angle to left.

0+75

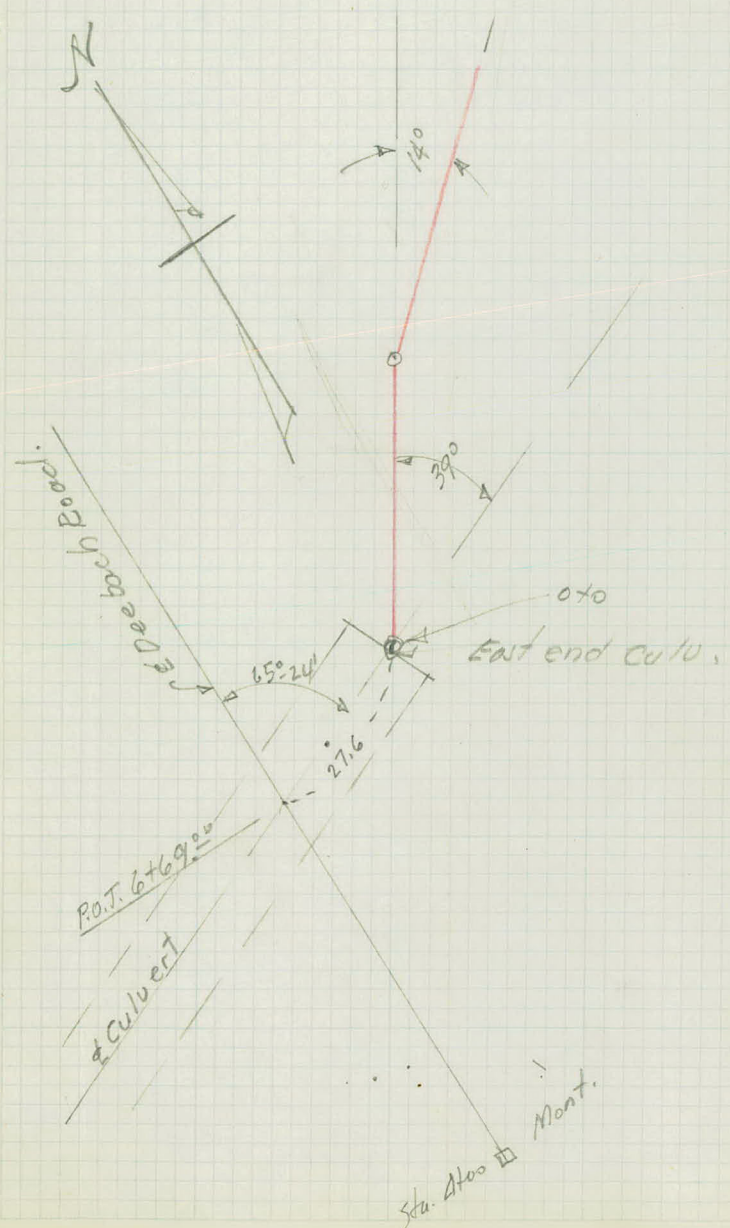
14° 00' 12"

$$\begin{cases} 0+00 \\ 0+27.6 \end{cases}$$

39° 00' 12"

0+0 = 6+69°

65° 24'





Levels +
Cross Sections

Deebach Rd.

Culv. Extension

W. H. Carlson
April 20, 1937

Sta.	+	π	-	Elev.
	0.67	894.93		894.26

± Levels Over Cula.

0			4.4	90.5
+35			6.3	88.6
+69 ± Cula			8.4	86.5
7+0			6.3	88.6
T.P.	0.97	882.18	13.72	881.21

0+97 226 Flow Line			13.30	868.88
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0+00 = End Cula.

0+15				71.5
------	--	--	--	------

0+30				71.0
------	--	--	--	------

0+53				71.5
------	--	--	--	------

0+75 = (P1)	X-Sec. Tunn ahead.			71.8
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Spike in 15" oak 30" Rt. Sta. 7+70

Lt. E Rt.

13.30 = Flow 84" Cu/U.

$\frac{6.5}{7}$ $\frac{9.2}{6}$ $\frac{10.7}{5}$ $\frac{12.3}{4}$ $\frac{12.3}{9}$ $\frac{7.4}{19}$ $\frac{+2.0}{21}$ $\frac{+5.0}{26}$ $\frac{+13.0}{39}$ $\frac{+17.0}{47}$

$\frac{5.2}{14}$ $\frac{9.4}{9}$ $\frac{11.4}{5}$ $\frac{11.2}{5}$ $\frac{11.2}{2}$ $\frac{8.2}{5}$ $\frac{0.5}{17}$ $\frac{+3.0}{25}$ $\frac{+18.3}{49}$ L.O.

$\frac{3.5}{24}$ $\frac{7.0}{18}$ $\frac{10.1}{10}$ $\frac{10.7}{2}$ $\frac{10.7}{2}$ $\frac{5.6}{7}$ $\frac{2.8}{15}$ $\frac{0.0}{22}$ $\frac{+10.0}{35}$ $\frac{+17.0}{49}$ L.O.

$\frac{6.0}{20}$ $\frac{8.2}{10}$ $\frac{10.4}{6}$ $\frac{10.4}{4}$ $\frac{10.4}{4}$ $\frac{5.3}{9}$ $\frac{0.0}{20}$ $\frac{+10.5}{37}$ $\frac{+16.0}{50}$

Sta. + - Elev.

882.18

1400

72.5

1425

72.5

1450

72.8

1475

73.0

B.M.

13.62

✓
894.83

0.97

0.59

✓
881.21
893.24
894.24

Lt

t

Rt

Up $\frac{0.0}{22}$ $\frac{6.1}{12}$ $\frac{9.6}{6}$ $\frac{9.7}{-}$ $\frac{9.5}{5}$ $\frac{6.5}{11}$ $\frac{4.1}{18}$ Up

$\frac{0.0}{17}$ $\frac{3.8}{7}$ $\frac{9.3}{2}$ $\frac{9.7}{-}$ $\frac{9.4}{9}$ $\frac{2.5}{17}$ Up

$\frac{0.0}{18}$ $\frac{7.0}{11}$ $\frac{9.5}{6}$ $\frac{9.4}{-}$ $\frac{9.0}{5}$ $\frac{7.5}{8}$ $\frac{6.8}{13}$ $\frac{1.7}{20}$

9.2

0+72- 30' 10.1/0.10
6' Lt.

0+48- 18' back top off.
7' 1/2'.

B.M.

1.54

875.80

891.26

Sub Grade

9.2

866

T

R+

7.7

8.1

12.6

83.2

C-5.0

C-2.5

9.1

1.1

C-9.1

C-14.1

15.8

77.0

78 C-11.0
C-16.0

C-14.1

9.8

23.8

72.0

9.7 C-14.1
C-9.1

C-9.1

W A - E

10.3

10.3

C-2.5

C-2.5

1.02

883.54

13.28

882.52

1.23

872.60

12.17

871.37

Top Layer
Base

0.6

720

7.7

873.57

6.20

866.40

1.6

720