

Book 7-A, Dr 12-A 7

ENGINEERS'
LEVEL BOOK
No. 10410

EUGENE DIETZGEN CO.

DRAWING MATERIALS, MATHEMATICAL and
SURVEYING INSTRUMENTS

Chicago New York San Francisco New Orleans Pittsburg Toronto

Distances from Center of Roadway for Cross-Sectioning
Roadway 16 feet wide. Side Slopes 1 on 1.
For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.1	8.2	8.3	8.4	8.5	8.6	8.7	8.8	8.9	0
1	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	1
2	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	2
3	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	3
4	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	4
5	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	5
6	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	6
7	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	7
8	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	8
9	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	9
10	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	10
11	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	11
12	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	12
13	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	13
14	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	14
15	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	15
16	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	16
17	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	17
18	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	18
19	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	19
20	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	20
21	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	21
22	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	22
23	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	23
24	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	24
25	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	25
26	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	26
27	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	27
28	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	28
29	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	29
30	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	30
31	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	31
32	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	32
33	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	33
34	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	34
35	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	35
36	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	36
37	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	37
38	46.0	46.1	46.2	46.3	46.4	46.5	46.6	46.7	46.8	46.9	38
39	47.0	47.1	47.2	47.3	47.4	47.5	47.6	47.7	47.8	47.9	39
40	48.0	48.1	48.2	48.3	48.4	48.5	48.6	48.7	48.8	48.9	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 30.6. For same slopes but other widths of roadbed, correct above figures by one-half difference in width of roadbed; thus in example above, for 20 ft. roadbed distance will be $30.6 + (20 - 16) \div 2$ or 2 ft. added to 30.6 = 32.6. For slopes of 1 on $1\frac{1}{2}$ see inside of back cover.

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733.29- B.M. Geological Survey
90767- C.O. water Gauge Bald Eagle Lake

Return to: Paul H. Coates,
County Surveyor,
920- Guardian Life Bldg.,
St. Paul,
Minn.

911.14
910.67
27

7

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Description	Page	Page
Alignment	1	3
X-Sec. Slope Stakes	4	19
Final X-Sec	21	35
" " " for Wash Out	36	

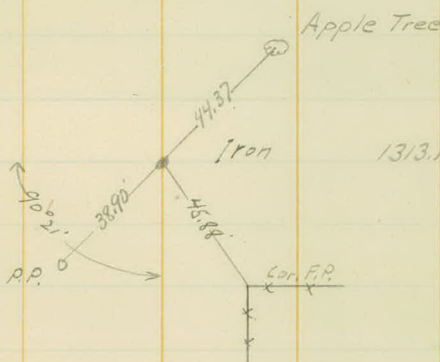
Sta.	Point	A-Lt.	A-Rt.
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32+23.85	P.O.T.		
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26+02.45	P.I.	0°17'	
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0+00			
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 1313.10
 N. 1/4 Cor. Sec.
 24-28-22



1313.10 
 Ctr. Sec.
 24-28-22

Mont.

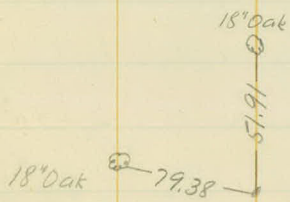
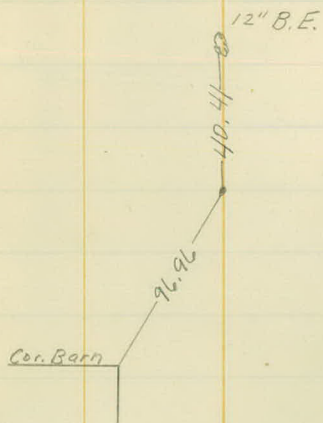

1303.40

40'

R.R. Spc. in 8" Oak



Sta	Point	Δ -Lt	Δ -Pt.
47+00.98	P.T.	28°15'	
+75		23°19'	Δ -56°30'
+50		18°34'	D-38°L
46+34.82	P.I.	56°30'	T-82.52
+25		13°49'	L-148.68
46		9°04'	R-153.58
+75		4°19'	
45+52.30	P.C.	0°00'	
40+30.16	P.T.		19°39 ⁵
40			16°38 ⁵ Δ -39°19'
+50			11°38 ⁵ D-20°R
39+36.45	P.I.		39°19' T-102.87
39			6°38 ⁵ L-196.58
+50			1°38 ⁵ R-287.94
38+33.58	P.C.		0°00'



Sta.	Point	Δ -Lt.	Δ -Rt.
------	-------	---------------	---------------

53+70.85	Int East Co. Line		
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32

38

52+13.51	P.T.		
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7°05'

52

6°36'E

Δ -14°10'

+50

4°51'E

D-7°R

51+12.90	P.I.		
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14°10'

T-101.77

51

3°06'E

L-202.38

+50

1°21'E

R-819.02

50+11.13	P.C.		
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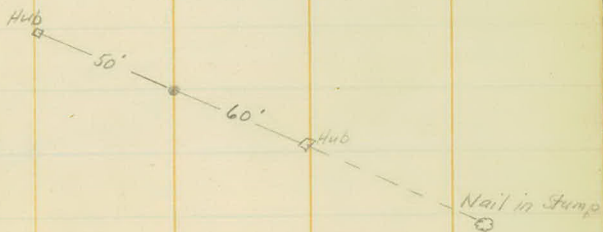
0°00'

0400 E. Co. Line Proj.

3" Apple Tree

4" Apple Tree

44.57
79.2
93.55
33.57



B.M.	11.78	866.78 ✓	855.00	
B.M.		6.99	859.79 ✓	
0+00			54.1 ✓	12.7

+50			54.9 ✓	11.9
-----	--	--	--------	------

1			54.0 ✓	10.8
---	--	--	--------	------

+50			57.3 ✓	9.5
-----	--	--	--------	-----

2			59.1 ✓	7.7
---	--	--	--------	-----

+50			61.2 ✓	5.6
T.P.	11.31	875.04 ✓	0.68 3.05	863.73 ✓

3			63.4 ✓	11.6
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+25			64.3 ✓	10.7
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Spk. in P.P. 19.5' N.E. 0400

Spk. in 8" Oak 120 Rt D-10

DC1.1	13.3	13.6	13.0	(12.7)	11.8	12.0	10.9	10.3	10.4	C1.8
22.7	33	22.7	16	40.2	12	21	26.7	31	33	26.7

DC1.0	12.7	12.9	13.0	(11.9)	11.9	11.5	11.7	12.1	12.8	12.6	DC1.8
22.5	33	22.5	11	-0.6	2	12	22	23.7	28	33	23.7
	-8	-1.0	-1.1		0	+4	+2	-2	-9	-7	

DC0.0	12.9	12.8	12.7	(10.8)	11.6	11.7	12.2	13.0	12.7	DC0.6
21.0	33	24.0	11	-1.2	1	20	21.9	28	33	21.9
	-2.1	-2.0	-1.9		-8	-9	-1.4	-2.2	-1.9	

F2.6	12.4	12.1	11.3	10.7	(9.5)	9.9	10.2	11.0	11.6	11.4	DC0.5
18.2	33	18.2	3	1	-1.2	9	20	21.8	24	33	21.8
	-2.9	-2.6	-1.8	-1.2		-4	-7	-1.5			

F3.3	11.6	11.0	10.5	8.8	8.7	8.0	8.1	8.7	8.5	7.6	DC1.0
19.6	33	19.6	7	3	-1.0	8	19	22.5	28	33	22.5

F3.0	9.1	8.6	6.1	5.6	5.3	5.7	6.3	6.3	2.4	2.2	DC1.3
<u>19.0</u>	<u>33</u>	<u>19</u>	<u>6</u>	<u>0.0</u>	<u>6</u>	<u>17</u>	<u>23</u>	<u>24</u>	<u>31</u>	<u>33</u>	<u>23.0</u>

DC1.1	10.6	12.4	12.5	11.5	12.0	(11.6)	11.2	11.6	11.9	11.1	10.7	9.3	4.9	4.9	0.5
22.7	33	24	22.7	11	3	+0.1	4	15	18	24.8	28	31	33	35	24.8
							+4	0	-3	+5	+9	+23	+6.7	+6.7	

C8.2	3.1	2.5	1.3	8.4	9.8	10.7	(10.7)	10.2	10.3	10.6	9.7	9.5	4.1	4.8	C1.2
36.3	40	36.3	22	12	7	5	+0.5	14	16	20	25.8	33	36	25.8	

875.04

3+50.

65.3 - 9.7

+80

66.3 - 8.7

4

67.0 - 8.0

T.P.

6.23

874.36 - 6.91

868.13 -

+40

68.1 - 6.3

+70

68.9 - 5.5

5

69.5 - 4.9

+50

70.5 - 3.9

T.P.

6.53

878.50 - 2.39

871.97 -

6

71.3 - 7.2

+50

72.1 - 6.4

(9.7)													C5.8
<u>C5.8</u>	<u>6.0</u>	<u>3.9</u>	<u>1.9</u>	<u>1.4</u>	<u>8.5</u>	<u>9.5</u>	<u>8.9</u>	<u>9.3</u>	<u>9.0</u>	<u>3.5</u>	<u>3.9</u>	<u>4.7</u>	<u>C5.8</u>
32.7	40	32.7	27	20	9	5	10.8	15	18	29	32.7	40	32.7

(8.7)													C1.0
<u>C1.0</u>	<u>7.6</u>	<u>7.7</u>	<u>7.8</u>	<u>8.2</u>	<u>8.0</u>	<u>7.9</u>	<u>8.2</u>	<u>7.2</u>	<u>7.7</u>	<u>8.7</u>			<u>C1.0</u>
25.5	33	25.5	11	8	10.7	12	18	23	25.5	33			25.5
	+1.1	+1.0	+1.9	+5		+1.8	+5	+1.5	+1.0	0			

(8.0)													DC0.0
<u>C0.3</u>	<u>7.9</u>	<u>7.7</u>	<u>7.6</u>	<u>7.5</u>	<u>7.9</u>	<u>10.0</u>	<u>13.2</u>						<u>DC0.0</u>
24.5	33	24.5	11	10.5	12	18.5	33						18.5
	+1	+3	+4		+1	-2.0	-5.2						

(6.3)													F4.9
<u>DC0.8</u>	<u>6.9</u>	<u>7.5</u>	<u>7.3</u>	<u>6.3</u>	<u>6.4</u>	<u>6.8</u>	<u>11.1</u>	<u>13.2</u>	<u>14.6</u>				<u>F4.9</u>
22.2	33	22.2	16	13	10.1	8	16	26.8	33				26.8
	-1.6	-1.2	-1.0	0		-1.5	-4.8	-6.9	-8.3				

(5.5)													DC0.1
<u>DC1.2</u>	<u>5.8</u>	<u>6.3</u>	<u>6.3</u>	<u>6.8</u>	<u>5.6</u>	<u>5.6</u>	<u>5.9</u>	<u>7.1</u>	<u>7.1</u>	<u>6.3</u>	<u>7.4</u>	<u>10.2</u>	<u>DC0.1</u>
22.8	33	22.8	20	18	14	-0.1	8	11	14	17	21.2	33	21.2
	-1.3	-1.8	-1.8	-1.3	-1.1		-4	-1.6	-1.6	-8	-1.9	-4.7	

(4.9)													DC1.0
<u>DC0.9</u>	<u>6.1</u>	<u>6.0</u>	<u>5.9</u>	<u>5.2</u>	<u>5.0</u>	<u>5.2</u>	<u>5.2</u>	<u>5.0</u>	<u>5.9</u>	<u>6.1</u>			<u>DC1.0</u>
22.4	33	22.4	17	13	3	-0.3	8	13	22.5	33			22.5
	-1.2	-1.1	-1.0	-1.3	-1.1		-1.3	-1.1	-1.0	-1.2			

(3.9)													DC1.8
<u>DC0.9</u>	<u>5.1</u>	<u>5.0</u>	<u>4.8</u>	<u>4.5</u>	<u>4.5</u>	<u>4.8</u>	<u>4.0</u>	<u>4.1</u>	<u>4.3</u>				<u>DC1.8</u>
22.4	33	22.4	16	13	-0.6	9	15	23.7	33				23.7
	-1.2	-1.1	-1.9	-1.6		-1.9	-1.1	-1.2	-1.4				

(7.7)													DC0.2
<u>C0.3</u>	<u>6.4</u>	<u>6.9</u>	<u>7.4</u>	<u>7.8</u>	<u>7.3</u>	<u>7.5</u>	<u>8.2</u>	<u>9.1</u>	<u>9.0</u>	<u>9.8</u>			<u>DC0.2</u>
24.5	33	24.5	14	11	7	-0.3	9	20	21.3	33			21.3
	+8	+3	-2	-1.6	-1		-1.0	-1.9	-1.8	-2.6			

(6.4)													DC0.0
<u>C1.8</u>	<u>4.5</u>	<u>4.6</u>	<u>6.0</u>	<u>6.6</u>	<u>6.3</u>	<u>6.5</u>	<u>7.1</u>	<u>7.9</u>	<u>8.4</u>	<u>8.9</u>	<u>8.6</u>		<u>DC0.0</u>
26.7	33	26.7	18	10	3	-0.1	8	10	19.0	28	33		19
	+1.9	+1.8	+4	-2	+1		-7.7	-1.5	-2.0	-2.5	-2.2		

878.50

7

72.9 ✓ 5.6

+50

73.7 ✓ 4.8

8

74.5 ✓ 4.0

+50

75.3 ✓ 3.2

9

76.1 ✓ 2.4

B.M. 8.59 886.17 ✓ 0.93

877.57 ✓ 877.58

+50

76.9 ✓ 4.3

10

77.7 ✓ 8.5

+50

78.5 ✓ 7.7

11

79.2 ✓ 7.0

(5.6)

<u>C1.8</u>	<u>3.9</u>	<u>3.8</u>	<u>3.9</u>	<u>6.2</u>	<u>5.6</u>	<u>6.0</u>	<u>6.3</u>	<u>6.6</u>	<u>6.4</u>	<u>6.2</u>	<u>DC1.2</u>
<u>26.7</u>	<u>33</u>	<u>26.7</u>	<u>25</u>	<u>19</u>	<u>13</u>	<u>-0.4</u>	<u>10</u>	<u>17</u>	<u>22.8</u>	<u>33</u>	<u>22.8</u>
	+1.7	+1.8	+1.7	-6	0		-7	-1.0	-8	-6	

(4.8)

<u>C1.6</u>	<u>3.1</u>	<u>3.2</u>	<u>3.2</u>	<u>4.8</u>	<u>4.7</u>	<u>5.2</u>	<u>5.3</u>	<u>5.8</u>	<u>5.3</u>	<u>5.2</u>	<u>5.1</u>	<u>DC1.6</u>
<u>26.4</u>	<u>33</u>	<u>26.4</u>	<u>25</u>	<u>21</u>	<u>13</u>	<u>10</u>	<u>-0.5</u>	<u>16</u>	<u>19</u>	<u>23.4</u>	<u>33</u>	<u>23.4</u>
	+1.7	+1.6	+1.6	-1	-9	-4		-1.0	-5	-4	-3	

(4.0)

<u>C1.8</u>	<u>2.3</u>	<u>2.2</u>	<u>2.8</u>	<u>4.5</u>	<u>4.0</u>	<u>4.0</u>	<u>4.0</u>	<u>3.7</u>	<u>3.6</u>	<u>CO.3</u>
<u>25.7</u>	<u>33</u>	<u>25.7</u>	<u>23</u>	<u>18</u>	<u>12</u>	<u>0.0</u>	<u>8</u>	<u>24.5</u>	<u>33</u>	<u>24.5</u>
	+1.7	+1.8	+1.7	-5	0		0	+3	+4	

(3.2)

<u>C1.2</u>	<u>1.6</u>	<u>2.0</u>	<u>4.0</u>	<u>3.3</u>	<u>3.3</u>	<u>3.7</u>	<u>4.7</u>	<u>4.8</u>	<u>4.7</u>	<u>3.7</u>	<u>3.0</u>	<u>DC0.4</u>
<u>25.8</u>	<u>33</u>	<u>25.8</u>	<u>19</u>	<u>10</u>	<u>-0.1</u>	<u>7</u>	<u>16</u>	<u>24.6</u>	<u>23</u>	<u>26</u>	<u>33</u>	<u>21.6</u>
	+1.6	+1.7	-8	-1		-5	-1.5	-1.6	-1.5	-5	+2	

(2.4)

<u>C1.2</u>	<u>0.3</u>	<u>1.2</u>	<u>1.0</u>	<u>2.9</u>	<u>2.5</u>	<u>2.4</u>	<u>2.8</u>	<u>3.9</u>	<u>4.7</u>	<u>4.4</u>	<u>2.8</u>	<u>F2.3</u>
<u>25.8</u>	<u>33</u>	<u>25.8</u>	<u>25</u>	<u>21</u>	<u>12</u>	<u>0.0</u>	<u>7</u>	<u>11</u>	<u>17.6</u>	<u>25</u>	<u>33</u>	<u>17.6</u>
	+1.1	+1.2	+1.4	-5	-1		-4	-1.5	-2.3	-2.0	-2	

Spt. in 20" Elm 10 Rt. 9+48 (9.3) Will Be Moved

<u>C2.4</u>	<u>6.4</u>	<u>6.9</u>	<u>7.0</u>	<u>9.8</u>	<u>8.9</u>	<u>8.9</u>	<u>9.2</u>	<u>10.2</u>	<u>10.0</u>	<u>9.4</u>	<u>9.1</u>	<u>DC1.3</u>
<u>27.6</u>	<u>33</u>	<u>27.6</u>	<u>25</u>	<u>20</u>	<u>12</u>	<u>10.4</u>	<u>9</u>	<u>19</u>	<u>23.0</u>	<u>27</u>	<u>33</u>	<u>23</u>
	+2.9	+2.4	+2.3	-5	+4		+1	-9	-7	-1	+2	

(8.5)

<u>C3.9</u>	<u>4.4</u>	<u>4.6</u>	<u>4.7</u>	<u>8.6</u>	<u>8.6</u>	<u>7.7</u>	<u>7.7</u>	<u>8.1</u>	<u>8.4</u>	<u>8.8</u>	<u>8.2</u>	<u>8.1</u>	<u>CO.3</u>
<u>29.9</u>	<u>33</u>	<u>29.9</u>	<u>25</u>	<u>18</u>	<u>14</u>	<u>11</u>	<u>10.8</u>	<u>11</u>	<u>14</u>	<u>21</u>	<u>24.5</u>	<u>33</u>	<u>24.5</u>
	+4.1	+3.9	+3.8	-1	-1	+8		+4	-1	-3	+3	+4	

(7.7)

<u>C2.8</u>	<u>4.5</u>	<u>4.9</u>	<u>5.1</u>	<u>7.7</u>	<u>7.9</u>	<u>7.1</u>	<u>6.8</u>	<u>7.1</u>	<u>8.5</u>	<u>7.9</u>	<u>8.0</u>	<u>DC1.8</u>
<u>28.2</u>	<u>33</u>	<u>28.2</u>	<u>25</u>	<u>20</u>	<u>14</u>	<u>11</u>	<u>10.9</u>	<u>12</u>	<u>20</u>	<u>23.7</u>	<u>33</u>	<u>23.7</u>
	+2.6	0	-2	+6		+6	-8	-7	-7	-3		

(7.0)

<u>C1.2</u>	<u>5.6</u>	<u>5.8</u>	<u>5.9</u>	<u>7.2</u>	<u>6.3</u>	<u>5.9</u>	<u>6.3</u>	<u>7.6</u>	<u>7.5</u>	<u>7.0</u>	<u>DC1.5</u>
<u>25.8</u>	<u>33</u>	<u>25.8</u>	<u>23</u>	<u>19</u>	<u>13</u>	<u>11</u>	<u>11</u>	<u>19</u>	<u>23.3</u>	<u>33</u>	<u>23.3</u>

886.17

11+50

79.8 ✓ 6.4

+82

79.9 ✓ 6.3

T.P.

9.46

890.72 ✓ 4.91

881.26 ✓

12

80.1 ✓ 10.6

+50

80.4 ✓ 10.3

+75

80.4 ✓ 10.3

B.M.

1.32

884.52 ✓ 7.52

883.20 ✓ 883.24

13

80.4 ✓ 4.1

+50

80.3 ✓ 4.2

14

80.1 ✓ 4.4

+50

79.9 ✓ 4.6

6.4

<u>CO.7</u>	<u>6.3</u>	<u>5.7</u>	<u>5.8</u>	<u>6.0</u>	<u>5.2</u>	<u>5.2</u>	<u>5.3</u>	<u>6.3</u>	<u>6.5</u>	<u>6.5</u>	<u>3.9</u>	<u>DC.19</u>
25.1	33	25.1	23	20	11	+1.2	11	20	23.9	28	35	23.9

6.3

<u>CO.8</u>	<u>6.4</u>	<u>5.5</u>	<u>5.3</u>	<u>4.8</u>	<u>5.2</u>	<u>4.7</u>	<u>5.5</u>	<u>6.7</u>	<u>5.5</u>	<u>1.4</u>	<u>CO.8</u>
25.2	33	25.2	23	12	10	+1.6	10	17	25.2	3.9	25.2

10.6

<u>CO.4</u>	<u>10.1</u>	<u>10.2</u>	<u>10.1</u>	<u>9.7</u>	<u>9.1</u>	<u>9.8</u>	<u>10.4</u>	<u>9.0</u>	<u>2.4</u>	<u>3.2</u>	<u>4.2</u>	<u>C7.4</u>
24.6	33	24.6	23	12	+1.5	10	15	20	27	35.1	40	35.1

10.8

<u>CO.5</u>	<u>13.4</u>	<u>11.1</u>	<u>9.8</u>	<u>10.1</u>	<u>9.6</u>	<u>9.3</u>	<u>9.8</u>	<u>9.6</u>	<u>8.6</u>	<u>4.2</u>	<u>3.3</u>	<u>4.4</u>	<u>C7.0</u>
24.8	30	29	24.8	21	11	+1.0	8	13	17	21	34.5	40	34.5

10.3

<u>DC1.5</u>	<u>12.1</u>	<u>12.1</u>	<u>13.7</u>	<u>13.6</u>	<u>10.8</u>	<u>9.7</u>	<u>9.6</u>	<u>10.0</u>	<u>9.8</u>	<u>9.6</u>	<u>8.0</u>	<u>CO.5</u>
23.3	33	31	30	28	23.3	13	+0.7	16	24.8	27	33	24.8

Spk. in 12" Dak 125' Rt. 13+20

4.1

<u>DC0.7</u>	<u>6.5</u>	<u>7.9</u>	<u>7.9</u>	<u>5.4</u>	<u>4.9</u>	<u>4.3</u>	<u>4.2</u>	<u>4.0</u>	<u>4.4</u>	<u>4.3</u>	<u>3.5</u>	<u>DC1.8</u>
22.1	30	28	26	22.1	20	15	10	+0.1	13	23.7	33	23.7

4.2

<u>F4.2</u>	<u>8.0</u>	<u>8.4</u>	<u>8.3</u>	<u>5.8</u>	<u>5.3</u>	<u>5.2</u>	<u>5.2</u>	<u>7.2</u>	<u>7.5</u>	<u>7.5</u>	<u>F3.3</u>
21.4	33	21.4	20	15	12	-1.0	7	11	18.6	33	19.6

4.4

<u>F4.0</u>	<u>8.6</u>	<u>8.4</u>	<u>8.0</u>	<u>6.2</u>	<u>6.0</u>	<u>6.2</u>	<u>8.2</u>	<u>8.4</u>	<u>8.2</u>	<u>F4.0</u>
21	33	24.0	16	13	-1.6	6	10	24.0	33	21

4.6

<u>F3.5</u>	<u>8.7</u>	<u>8.1</u>	<u>8.0</u>	<u>6.2</u>	<u>6.2</u>	<u>6.8</u>	<u>8.1</u>	<u>8.7</u>	<u>8.7</u>	<u>F4.1</u>
20	33	20.0	15	12	-1.6	6	11	21.2	33	21.2

884.52

15

79.7 ✓ 4.8

+50

79.6 ✓ 4.9

16

79.8 ✓ 4.7

+50

80.1 ✓ 4.4

T.P.

8.53

887.29 ✓ 5.76

878.76 ✓

17

80.7 ✓ 6.6

+50

81.4 ✓ 5.9

18

82.1 ✓ 5.2

+50

82.8 ✓ 4.5

19

83.5 ✓ 3.8

T.P.

13.72

900.85 ✓ 0.16

887.13 ✓

$\frac{F3.7}{20.4}$	$\frac{8.5}{33}$	$\frac{8.5}{20.4}$	$\frac{8.5}{16}$	$\frac{6.2}{12}$	$\frac{4.8}{-1.5}$	$\frac{6.3}{6}$	$\frac{6.8}{9}$	$\frac{8.4}{20.8}$	$\frac{8.7}{33}$	$\frac{8.8}{33}$	$\frac{F3.9}{20.8}$
$\frac{F3.4}{19.8}$	$\frac{8.3}{33}$	$\frac{8.3}{19.8}$	$\frac{8.2}{17}$	$\frac{6.2}{12}$	$\frac{4.9}{-1.2}$	$\frac{6.1}{6}$	$\frac{6.4}{10}$	$\frac{8.6}{24.0}$	$\frac{8.9}{24.0}$	$\frac{9.0}{33}$	$\frac{F4.0}{21}$
$\frac{F3.6}{20.2}$	$\frac{8.3}{33}$	$\frac{8.3}{20.2}$	$\frac{8.2}{16}$	$\frac{6.2}{12}$	$\frac{4.7}{-1.3}$	$\frac{6.0}{6}$	$\frac{6.3}{10}$	$\frac{8.5}{24.0}$	$\frac{8.7}{24.0}$	$\frac{8.7}{33}$	$\frac{F4.0}{21}$
$\frac{F3.4}{20.2}$	$\frac{8.0}{33}$	$\frac{8.0}{20.2}$	$\frac{8.0}{17}$	$\frac{6.1}{12}$	$\frac{4.4}{-1.6}$	$\frac{6.0}{5}$	$\frac{6.1}{8}$	$\frac{8.2}{24.2}$	$\frac{8.5}{24.2}$	$\frac{8.6}{33}$	$\frac{F4.1}{21.2}$
$\frac{F3.9}{20.8}$	$\frac{10.5}{33}$	$\frac{10.5}{20.8}$	$\frac{10.5}{17}$	$\frac{8.8}{12}$	$\frac{6.6}{-2.0}$	$\frac{8.6}{5}$	$\frac{8.6}{10}$	$\frac{11.0}{24.4}$	$\frac{10.8}{24.4}$	$\frac{10.9}{33}$	$\frac{F4.2}{21.4}$
$\frac{F4.3}{21.6}$	$\frac{10.2}{33}$	$\frac{10.2}{21.6}$	$\frac{10.2}{15}$	$\frac{8.5}{12}$	$\frac{5.9}{-2.3}$	$\frac{8.2}{5}$	$\frac{8.5}{8}$	$\frac{10.5}{22.0}$	$\frac{10.4}{22.0}$	$\frac{10.5}{33}$	$\frac{F4.5}{22}$
$\frac{F4.8}{22.6}$	$\frac{9.9}{33}$	$\frac{10.0}{22.6}$	$\frac{9.7}{15}$	$\frac{7.9}{11}$	$\frac{5.2}{-2.4}$	$\frac{7.6}{6}$	$\frac{7.8}{9}$	$\frac{10.0}{22.6}$	$\frac{10.0}{22.6}$	$\frac{9.9}{33}$	$\frac{F4.8}{22.6}$
$\frac{F5.0}{23}$	$\frac{9.6}{33}$	$\frac{9.5}{23}$	$\frac{8.9}{15}$	$\frac{6.6}{12}$	$\frac{4.5}{-1.6}$	$\frac{6.1}{6}$	$\frac{6.4}{9}$	$\frac{8.1}{19.4}$	$\frac{7.7}{24}$	$\frac{5.8}{33}$	$\frac{F3.2}{19.4}$
$\frac{F4.1}{21.2}$	$\frac{8.7}{33}$	$\frac{7.9}{21.2}$	$\frac{7.7}{19}$	$\frac{4.1}{12}$	$\frac{3.8}{-0.1}$	$\frac{3.9}{13}$	$\frac{4.3}{13}$				

900.85

19

83.5 ✓ 17.4

+30

83.9 ✓ 17.0

+70

84.5 ✓ 16.4

20

84.9 ✓ 16.0

T.P.

4.64

891.77 ✓ 13.72

887.13 ✓

19+30

83.9 ✓ 7.9

+70

84.5 ✓ 7.3

20

84.9 ✓ 6.9

+50

85.6 ✓ 6.2

21

86.3 ✓ 5.5

17.4

$$\frac{11.6}{25} \quad \frac{2.1}{40} \quad \frac{1.6}{45}$$

$$\frac{C15.3}{40}$$

17.0

$$\frac{11.1}{18} \quad \frac{0.1}{25} \quad \frac{0.9}{31} \quad \frac{0.8}{40} \quad \frac{0.9}{45}$$

$$\frac{C16.2}{40}$$

16.4

$$\frac{11.9}{17} \quad \frac{3.6}{25} \quad \frac{4.7}{29} \quad \frac{5.3}{40} \quad \frac{5.4}{45}$$

$$\frac{C11.1}{40}$$

16.0

$$\frac{14.0}{14} \quad \frac{9.2}{21} \quad \frac{9.7}{33.5} \quad \frac{9.8}{40}$$

$$\frac{C6.3}{33.5}$$

$$\frac{C0.0}{24} \quad \frac{7.2}{33} \quad \frac{7.9}{24} \quad \frac{7.7}{22} \quad \frac{7.8}{15} \quad \frac{7.3}{11} \quad \frac{7.9}{10.6} \quad \frac{7.4}{5} \quad \frac{5.4}{12}$$

$$\frac{C0.0}{24} \quad \frac{7.3}{33} \quad \frac{7.3}{24} \quad \frac{7.1}{16} \quad \frac{6.6}{9} \quad \frac{6.1}{11.2} \quad \frac{6.4}{5} \quad \frac{5.5}{11}$$

$$\frac{D04.6}{23.4} \quad \frac{6.8}{33} \quad \frac{7.3}{23.4} \quad \frac{6.3}{10} \quad \frac{5.8}{11.1} \quad \frac{6.1}{10}$$

$$\frac{F5.3}{23.6} \quad \frac{12.3}{33} \quad \frac{11.5}{23.6} \quad \frac{9.7}{16} \quad \frac{6.6}{8} \quad \frac{6.1}{10.1} \quad \frac{6.3}{10} \quad \frac{6.7}{15} \quad \frac{5.2}{21} \quad \frac{4.8}{24.1} \quad \frac{4.6}{33} \quad \frac{C1.4}{26.1}$$

$$\frac{F6.4}{25.8} \quad \frac{12.4}{33} \quad \frac{11.9}{25.8} \quad \frac{11.1}{18} \quad \frac{9.9}{13} \quad \frac{6.4}{6} \quad \frac{5.5}{-0.4} \quad \frac{5.9}{11} \quad \frac{6.8}{17} \quad \frac{6.5}{20} \quad \frac{5.2}{24.5} \quad \frac{5.2}{33} \quad \frac{C0.3}{24.5}$$

891.77

21 +50

87.2 ✓ 4.6

22

88.5 ✓ 3.3

+25

89.4 ✓ 2.4

T.P.

8.30

899.19 ✓ 0.88

890.89 ✓

+75

91.2 ✓ 8.0

23

92.3 ✓ 6.9

+50

94.6 ✓ 4.6

T.P.

10.20

906.83 ✓ 2.56

896.63 ✓

24

96.9 ✓ 9.9

+50

99.2 ✓ 7.6

25

01.5 ✓ 5.3

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 6.7 \\
 \hline
 28
 \end{array}
 \quad
 \begin{array}{r}
 6.7 \\
 \hline
 28.8
 \end{array}
 \quad
 \begin{array}{r}
 6.7 \\
 \hline
 33
 \end{array}
 \quad
 \begin{array}{r}
 C3.2 \\
 \hline
 28.8
 \end{array}$$

$$\begin{array}{r}
 \text{C0.8} \\
 \hline
 25.2
 \end{array}
 \quad
 \begin{array}{r}
 8.1 \\
 \hline
 33
 \end{array}
 \quad
 \begin{array}{r}
 6.8 \\
 \hline
 25.2
 \end{array}
 \quad
 \begin{array}{r}
 7.0 \\
 \hline
 18
 \end{array}
 \quad
 \begin{array}{r}
 8.2 \\
 \hline
 15
 \end{array}
 \quad
 \begin{array}{r}
 7.7 \\
 \hline
 -0.1
 \end{array}
 \quad
 \begin{array}{r}
 8.3 \\
 \hline
 16
 \end{array}
 \quad
 \begin{array}{r}
 9.3 \\
 \hline
 21
 \end{array}
 \quad
 \begin{array}{r}
 5.8 \\
 \hline
 26.7
 \end{array}
 \quad
 \begin{array}{r}
 5.1 \\
 \hline
 29
 \end{array}
 \quad
 \begin{array}{r}
 5.0 \\
 \hline
 33
 \end{array}
 \quad
 \begin{array}{r}
 C1.8 \\
 \hline
 26.7
 \end{array}$$

$$\begin{array}{r}
 \text{F2.1} \\
 \hline
 17.2
 \end{array}
 \quad
 \begin{array}{r}
 8.9 \\
 \hline
 33
 \end{array}
 \quad
 \begin{array}{r}
 8.3 \\
 \hline
 22
 \end{array}
 \quad
 \begin{array}{r}
 7.4 \\
 \hline
 17.2
 \end{array}
 \quad
 \begin{array}{r}
 6.4 \\
 \hline
 12
 \end{array}
 \quad
 \begin{array}{r}
 5.8 \\
 \hline
 -0.5
 \end{array}
 \quad
 \begin{array}{r}
 6.3 \\
 \hline
 9
 \end{array}
 \quad
 \begin{array}{r}
 5.0 \\
 \hline
 24.5
 \end{array}
 \quad
 \begin{array}{r}
 4.5 \\
 \hline
 33
 \end{array}
 \quad
 \begin{array}{r}
 C0.3 \\
 \hline
 24.5
 \end{array}$$

906.83

25+50

03.8 ✓ 3.0

+77

05.0 ✓ 1.8

+80

05.2 ✓ 1.6

26

06.0 ✓ 0.8

+16

06.6 ✓ 0.2

B.M.

7.14

913.81 ✓ 0.21

906.62 ✓ 906.67

+20

06.7 ✓ 7.1

+60

07.6 ✓ 6.2

27

08.6 ✓ 5.2

+50

08.9 ✓ 4.9

	30												
DC1.4	3.1	3.6	3.5	4.8	4.1	3.8	4.3	4.3	5.1	4.3	3.7	3.7	DC0.7
23.1	33	23.1	20	16	10	-0.8	9	19	20	22.1	24	33	22.1

	1.8										
CO.6	0.8	1.2	1.1	2.9	2.4	2.7	2.7	3.4			DC1.1
24.9	33	24.9	20	15	-0.6	13	22.7	33			22.7

	1.6					
	2.4	2.6	2.2	2.4	2.3	2.7
	33	17	-0.6	12	29	33

	0.8				
	1.5	1.5	1.1	1.1	0.8
	33	11	-0.3	15	33

	0.2				
	1.5	1.1	0.4	0.5	0.6
	33	14	-0.2	15	33

Spk. in P.P.-N.W. Cor. Carver Ave + Polander Rd.

	2.1										
C1.2	5.9	5.9	5.9	7.8	7.1	7.4	7.4	8.0	6.6	6.3	DC1.1
25.8	33	25.8	18	11	0.0	10	17	22.7	24	33	22.7

	6.2										
CO.5	6.0	5.7	5.4	6.4	5.7	6.3	5.7	5.7	4.2	3.2	C2.0
24.8	33	24.8	16	14	+0.5	10	15	19	27	29	27

	32								
DC1.4	6.9	5.8	5.1	5.4	4.2	4.6	4.0	2.0	C1.2
25.8	33	23.1	17	15	+1.0	13	25.8	35	25.8

	4.9								
F1.9	9.2	6.8	5.5	4.6	5.1	3.8	3.9	4.3	C1.0
16.8	33	16.8	13	+0.3	10	21	25.5	33	25.5

913.81

28

08.6 ✓ 5.2.

+50

08.2 ✓ 5.6

+75

08.1 ✓ 5.7

29

08.1 ✓ 5.7

+15

08.1 ✓ 5.7

T.P.

4.85

910.17 ✓

8.49

905.32 ✓

+35

08.2 ✓ 2.0

+70

08.5 ✓ 1.7

30

09.0 ✓ 1.2

+35

09.8 ✓ 0.4

T.P.

13.64

922.99 ✓ 0.82

909.35 ✓

$$\begin{array}{r}
 \text{F4.5} \\
 \hline
 22
 \end{array}
 \quad
 \begin{array}{cccccccccc}
 & 10.2 & 9.7 & 8.8 & 5.9 & 5.2 & 5.2 & 5.6 & 5.7 & 5.6 \\
 & \hline
 33 & 22 & 16 & 9 & 0.0 & 7 & 17 & 233 & 33
 \end{array}
 \quad
 \begin{array}{r}
 \text{DC1.5} \\
 \hline
 23.3
 \end{array}$$

$$\begin{array}{r}
 \text{DC0.8} \\
 \hline
 22.2
 \end{array}
 \quad
 \begin{array}{cccccccccc}
 & 7.4 & 6.8 & 6.6 & 7.0 & 6.5 & 5.8 & 5.9 & 5.3 & 3.8 & 3.1 & 2.5 \\
 & \hline
 33 & 22.2 & 18 & 14 & 12 & -0.2 & 9 & 19 & 22 & 27.8 & 33
 \end{array}
 \quad
 \begin{array}{r}
 \text{C2.5} \\
 \hline
 27.8
 \end{array}$$

$$\begin{array}{r}
 \text{DC1.7} \\
 \hline
 23.6
 \end{array}
 \quad
 \begin{array}{cccccccccc}
 & 6.6 & 6.0 & 5.9 & 7.1 & 6.7 & 7.1 & 6.6 & 3.4 & 3.0 & 3.1 \\
 & \hline
 33 & 23.6 & 16 & 12 & -1.0 & 9 & 14 & 23 & 28.1 & 33
 \end{array}
 \quad
 \begin{array}{r}
 \text{C2.7} \\
 \hline
 28.1
 \end{array}$$

$$\begin{array}{r}
 \text{F2.3} \\
 \hline
 17.6
 \end{array}
 \quad
 \begin{array}{cccccccccc}
 & 9.0 & 8.0 & 8.8 & 8.0 & 7.8 & 8.2 & 8.4 & 3.5 & 2.4 & 2.1 \\
 & \hline
 33 & 17.6 & 14 & 8 & -2.1 & 10 & 18 & 24 & 28 & 33
 \end{array}
 \quad
 \begin{array}{r}
 \text{C3.3} \\
 \hline
 28
 \end{array}$$

$$\begin{array}{r}
 \text{F5.6} \\
 \hline
 24.2
 \end{array}
 \quad
 \begin{array}{cccccccccc}
 & 11.9 & 11.3 & 10.0 & 8.5 & 8.3 & 9.6 & 7.4 & 2.8 & 2.8 \\
 & \hline
 33 & 24.2 & 13 & 7 & -2.6 & 19 & 24.5 & 31 & 33
 \end{array}
 \quad
 \begin{array}{r}
 \text{DC0.3} \\
 \hline
 21.5
 \end{array}$$

$$\begin{array}{r}
 \text{F8.6} \\
 \hline
 30.2
 \end{array}
 \quad
 \begin{array}{cccccccccc}
 & 10.7 & 10.6 & 8.8 & 7.0 & 5.3 & 5.1 & 5.3 & 6.6 & 7.5 & 7.8 \\
 & \hline
 33 & 30.2 & 14 & 10 & 6 & -3.1 & 12 & 15 & 24 & 33
 \end{array}
 \quad
 \begin{array}{r}
 \text{F5.5} \\
 \hline
 24
 \end{array}$$

$$\begin{array}{r}
 \text{F9.0} \\
 \hline
 31
 \end{array}
 \quad
 \begin{array}{cccccccccc}
 & 10.7 & 10.7 & 8.7 & 5.3 & 4.9 & 5.1 & 11.3 & 11.8 & 12.5 \\
 & \hline
 33 & 31 & 13 & 7 & -3.2 & 13 & 24 & 33 & 40
 \end{array}
 \quad
 \begin{array}{r}
 \text{F10.1} \\
 \hline
 33
 \end{array}$$

$$\begin{array}{r}
 \text{F7.5} \\
 \hline
 28
 \end{array}
 \quad
 \begin{array}{cccccccccc}
 & 9.2 & 8.7 & 8.2 & 4.2 & 4.1 & 4.3 & 9.2 & 11.7 & 12.0 \\
 & \hline
 33 & 28 & 17 & 6 & -2.9 & 14 & 23 & 33 & 40
 \end{array}
 \quad
 \begin{array}{r}
 \text{F10.5} \\
 \hline
 33
 \end{array}$$

$$\begin{array}{r}
 \text{F4.7} \\
 \hline
 22.4
 \end{array}
 \quad
 \begin{array}{cccccccccc}
 & 5.4 & 5.1 & 4.3 & 2.9 & 2.5 & 2.5 & 3.4 & 3.7 & 5.7 \\
 & \hline
 33 & 22.4 & 16 & 10 & -3.1 & 13 & 17 & 19.6 & 33
 \end{array}
 \quad
 \begin{array}{r}
 \text{F3.3} \\
 \hline
 19.6
 \end{array}$$

922.99

30+65

10.6 ✓ 12.4

31

11.7 ✓ 11.3

+25

12.4 ✓ 10.6

+75

13.7 ✓ 9.3

32

14.2 ✓ 9.8

+50

14.5 ✓ 8.5

33

14.3 ✓ 8.7

T.P.

1.79

918.08 ✓

6.70

916.29 ✓

+50

13.2 ✓ 4.9

34

11.9 ✓ 6.2

$$\begin{array}{r}
 \frac{C1.2}{25.8} \quad \frac{11.8}{33} \quad \frac{11.2}{25.8} \quad \frac{11.3}{21} \quad \frac{14.0}{15} \quad \frac{13.6}{-1.2} \quad \frac{14.0}{10} \quad \frac{10.3}{27.2} \quad \frac{9.1}{33} \quad \frac{C2.1}{27.2}
 \end{array}$$

$$\begin{array}{r}
 \frac{C2.9}{28.4} \quad \frac{6.1}{33} \quad \frac{8.4}{28.4} \quad \frac{9.1}{25} \quad \frac{11.6}{14} \quad \frac{11.3}{0.0} \quad \frac{11.8}{9} \quad \frac{10.3}{14} \quad \frac{6.4}{31.4} \quad \frac{6.2}{33} \quad \frac{C4.9}{31.4}
 \end{array}$$

$$\begin{array}{r}
 \frac{C10.3}{33} \quad \frac{0.8}{40} \quad \frac{0.3}{33} \quad \frac{0.1}{26} \quad \frac{9.3}{13} \quad \frac{9.8}{9} \quad \frac{9.2}{+1.4} \quad \frac{9.8}{10} \quad \frac{8.6}{13} \quad \frac{4.8}{32.7} \quad \frac{4.8}{30} \quad \frac{C5.8}{32.7}
 \end{array}$$

$$\begin{array}{r}
 \frac{C7.3}{33} \quad \frac{2.7}{40} \quad \frac{2.0}{33} \quad \frac{1.9}{19} \quad \frac{7.4}{11} \quad \frac{7.5}{7} \quad \frac{6.7}{+2.6} \quad \frac{6.9}{9} \quad \frac{3.5}{32.7} \quad \frac{2.9}{40} \quad \frac{C5.8}{32.7}
 \end{array}$$

$$\begin{array}{r}
 \frac{C4.8}{31.2} \quad \frac{4.0}{33} \quad \frac{4.0}{31.2} \quad \frac{3.7}{20} \quad \frac{5.9}{17} \quad \frac{7.1}{12} \quad \frac{6.1}{+2.7} \quad \frac{6.2}{8} \quad \frac{3.5}{32} \quad \frac{3.0}{40} \quad \frac{C5.3}{32}
 \end{array}$$

$$\begin{array}{r}
 \frac{DC0.8}{22.2} \quad \frac{10.5}{33} \quad \frac{9.7}{22.2} \quad \frac{9.2}{19} \quad \frac{7.9}{13} \quad \frac{6.9}{+1.6} \quad \frac{7.1}{13} \quad \frac{6.1}{27.6} \quad \frac{5.5}{33} \quad \frac{C2.4}{27.6}
 \end{array}$$

$$\begin{array}{r}
 \frac{F3.1}{19.2} \quad \frac{13.0}{33} \quad \frac{11.8}{19.2} \quad \frac{11.5}{15} \quad \frac{8.9}{7} \quad \frac{8.3}{+0.4} \quad \frac{8.3}{13} \quad \frac{7.2}{26.3} \quad \frac{6.5}{33} \quad \frac{C1.5}{26.3}
 \end{array}$$

$$\begin{array}{r}
 \frac{F2.4}{17.8} \quad \frac{8.3}{33} \quad \frac{7.3}{17.8} \quad \frac{6.6}{12} \quad \frac{5.1}{6} \quad \frac{4.6}{+0.3} \quad \frac{4.7}{12} \quad \frac{4.0}{25.4} \quad \frac{3.1}{33} \quad \frac{C0.9}{25.4}
 \end{array}$$

$$\begin{array}{r}
 \frac{DC0.6}{21.9} \quad \frac{8.0}{33} \quad \frac{7.6}{21.9} \quad \frac{6.9}{13} \quad \frac{6.1}{8} \quad \frac{5.9}{+0.3} \quad \frac{5.9}{11} \quad \frac{5.5}{25.1} \quad \frac{4.9}{33} \quad \frac{C0.7}{25.1}
 \end{array}$$

918.08

34+50

10.6 ✓ 7.5

35

09.3 ✓ 8.8

B.M.

7.36

918.05 ✓ 7.36

910.72 ✓ 910.69

+50

08.0 ✓ 10.1

36

06.7 ✓ 11.4

T.P.

0.99

905.58 ✓

13.46

904.59 ✓

+50

05.4 ✓ 0.2

37

Super.
0.2 0.2

04.4 ✓ 1.0 1.4
1.2

+50

0.4 0.4 03.9 ✓ 1.3 2.1
1.7

38

Widen H.
0.0

0.6 0.6

04.0 ✓ 1.0 2.2
1.6

+50

3.0

0.9 1.1

04.7 ✓ 0.0 2.0
0.9

				7.5						
DC1.9		<u>7.5</u>	<u>7.4</u>	<u>8.2</u>	<u>7.1</u>	<u>7.5</u>	<u>6.7</u>	<u>6.2</u>		<u>C0.8</u>
23.9		33	23.9	12	10.4	14	25.2	33		25.2

					8.8					
DC1.0		<u>9.9</u>	<u>9.8</u>	<u>9.7</u>	<u>10.5</u>	<u>9.6</u>	<u>9.1</u>	<u>9.7</u>	<u>9.3</u>	<u>8.6</u>
22.5		33	22.5	16	14	8	-0.3	15	23.3	33

Spt. in Triple Elm 60 Lt. 35+07

DC1.9		<u>9.2</u>	<u>10.2</u>	<u>10.7</u>	<u>12.5</u>	<u>11.9</u>	<u>11.4</u>	<u>12.1</u>	<u>11.0</u>	<u>9.3</u>
23.9		33	23.9	15	12	8	-1.3	13	22.7	33

						11.4				
C0.3		<u>10.7</u>	<u>11.1</u>	<u>12.1</u>	<u>14.7</u>	<u>14.1</u>	<u>13.6</u>	<u>14.2</u>	<u>14.2</u>	<u>13.7</u>
24.5		33	24.5	16	12	9	-2.2	16	18.6	33

						0.2				
F2.3		<u>0.8</u>	<u>2.5</u>	<u>3.4</u>	<u>3.1</u>	<u>2.8</u>	<u>3.3</u>	<u>4.6</u>	<u>5.5</u>	
17.6		33	17.6	15	9	-2.6	11	21.8	33	

						1.2				
F5.0		<u>6.5</u>	<u>6.0</u>	<u>5.6</u>	<u>4.0</u>	<u>3.8</u>	<u>4.5</u>	<u>5.4</u>	<u>6.2</u>	<u>6.2</u>
2.3		33	23	15	10	-2.6	12	14	22.6	33

						1.7				
F6.6		<u>7.2</u>	<u>7.9</u>	<u>8.0</u>	<u>6.7</u>	<u>5.0</u>	<u>4.5</u>	<u>4.7</u>	<u>5.6</u>	<u>5.6</u>
26.2		33	26.2	19	12	9	-2.8	9	12	20.0

						1.6				
F5.9		<u>7.0</u>	<u>6.9</u>	<u>6.4</u>	<u>5.2</u>	<u>4.6</u>	<u>5.1</u>	<u>6.0</u>	<u>6.2</u>	<u>6.2</u>
24.8		33	24.8	13	9	-3.0	10	12	21.0	33

						0.9				
F6.5		<u>6.5</u>	<u>6.5</u>	<u>6.2</u>	<u>5.2</u>	<u>4.8</u>	<u>4.9</u>	<u>6.0</u>	<u>6.3</u>	<u>6.4</u>
26.0		33	26.0	12	8	-3.9	9	12	24.6	33

		905.58					
39		3.5	1.1	1.3	05.9 ✓	+1.4 +0.3	1.0
+50		3.5	1.1	1.3	07.6 ✓	+3.1 +2.0	+0.7
T.P.	13.31	916.46 ✓	2.43		903.15 ✓		
40		3.0	1.0	1.2	09.7 ✓	5.8 6.8	8.0
B.M.			3.14		913.32	913.32	
T.P.	13.70	928.16 ✓	2.00		914.46 ✓		
+50		1.0	0.7	0.8	11.7 ✓	15.8 16.5	17.3
+80		0.0	0.5	0.5	12.9 ✓	14.8 15.3	15.8
41			0.4	0.4	13.7 ✓	14.1 14.5	14.9
+20			0.3	0.3	14.4 ✓	13.5 13.8	14.1
T.P.	9.50	937.66 ✓	0.00		928.16 ✓		
40+50		1.0	0.7	0.8	11.7 ✓	25.3 26.0	
+80		0.0	0.5	0.5	12.9 ✓	24.3 24.8	

$$\begin{array}{r}
 F7.3 \\
 \hline
 27.6
 \end{array}
 \qquad
 \begin{array}{r}
 +0.3 \\
 \hline
 \begin{array}{r}
 5.9 \\
 33
 \end{array}
 \quad
 \begin{array}{r}
 5.9 \\
 27.6
 \end{array}
 \quad
 \begin{array}{r}
 5.5 \\
 20
 \end{array}
 \quad
 \begin{array}{r}
 4.7 \\
 14
 \end{array}
 \quad
 \begin{array}{r}
 3.8 \\
 7
 \end{array}
 \quad
 \begin{array}{r}
 3.6 \\
 -3.9
 \end{array}
 \quad
 \begin{array}{r}
 4.2 \\
 11
 \end{array}
 \quad
 \begin{array}{r}
 5.4 \\
 15
 \end{array}
 \quad
 \begin{array}{r}
 5.8 \\
 24.1
 \end{array}
 \quad
 \begin{array}{r}
 5.9 \\
 33
 \end{array}
 \end{array}
 \qquad
 \begin{array}{r}
 F4.8 \\
 \hline
 26.1
 \end{array}$$

$$\begin{array}{r}
 F8.4 \\
 \hline
 29.8
 \end{array}
 \qquad
 \begin{array}{r}
 +2.0 \\
 \hline
 \begin{array}{r}
 5.6 \\
 33
 \end{array}
 \quad
 \begin{array}{r}
 5.3 \\
 29.8
 \end{array}
 \quad
 \begin{array}{r}
 5.2 \\
 21
 \end{array}
 \quad
 \begin{array}{r}
 1.0 \\
 12
 \end{array}
 \quad
 \begin{array}{r}
 0.3 \\
 -2.3
 \end{array}
 \quad
 \begin{array}{r}
 1.0 \\
 13
 \end{array}
 \quad
 \begin{array}{r}
 4.7 \\
 20
 \end{array}
 \quad
 \begin{array}{r}
 4.9 \\
 27.7
 \end{array}
 \quad
 \begin{array}{r}
 4.9 \\
 33
 \end{array}
 \end{array}
 \qquad
 \begin{array}{r}
 F5.6 \\
 \hline
 27.7
 \end{array}$$

$$\begin{array}{r}
 C1.9 \\
 \hline
 26.
 \end{array}
 \qquad
 \begin{array}{r}
 6.8 \\
 \hline
 \begin{array}{r}
 3.1 \\
 33
 \end{array}
 \quad
 \begin{array}{r}
 4.5 \\
 26
 \end{array}
 \quad
 \begin{array}{r}
 6.0 \\
 16
 \end{array}
 \quad
 \begin{array}{r}
 6.3 \\
 11
 \end{array}
 \quad
 \begin{array}{r}
 6.0 \\
 +0.8
 \end{array}
 \quad
 \begin{array}{r}
 6.0 \\
 6
 \end{array}
 \quad
 \begin{array}{r}
 6.8 \\
 16
 \end{array}
 \quad
 \begin{array}{r}
 10.0 \\
 24
 \end{array}
 \quad
 \begin{array}{r}
 10.8 \\
 33
 \end{array}
 \end{array}
 \qquad
 \begin{array}{r}
 DC0.0 \\
 \hline
 24
 \end{array}$$

Sok in 12" Oak 50' L+ 39+90

$$\begin{array}{r}
 16.5 \\
 \hline
 \begin{array}{r}
 2.9 \\
 17
 \end{array}
 \quad
 \begin{array}{r}
 5.5 \\
 17
 \end{array}
 \quad
 \begin{array}{r}
 11.2 \\
 12
 \end{array}
 \quad
 \begin{array}{r}
 13.8 \\
 7
 \end{array}
 \quad
 \begin{array}{r}
 13.4 \\
 +3.1
 \end{array}
 \quad
 \begin{array}{r}
 13.1 \\
 4
 \end{array}
 \quad
 \begin{array}{r}
 13.9 \\
 14
 \end{array}
 \quad
 \begin{array}{r}
 8.1 \\
 18
 \end{array}
 \quad
 \begin{array}{r}
 9.8 \\
 33
 \end{array}
 \quad
 \begin{array}{r}
 10.0 \\
 36
 \end{array}
 \end{array}
 \qquad
 \begin{array}{r}
 C7.5 \\
 \hline
 33
 \end{array}$$

$$\begin{array}{r}
 15.3 \\
 \hline
 \begin{array}{r}
 4.6 \\
 33
 \end{array}
 \quad
 \begin{array}{r}
 9.0 \\
 21
 \end{array}
 \quad
 \begin{array}{r}
 11.7 \\
 8
 \end{array}
 \quad
 \begin{array}{r}
 11.0 \\
 +4.3
 \end{array}
 \quad
 \begin{array}{r}
 10.7 \\
 4
 \end{array}
 \quad
 \begin{array}{r}
 11.3 \\
 11
 \end{array}
 \quad
 \begin{array}{r}
 8.3 \\
 20
 \end{array}
 \quad
 \begin{array}{r}
 3.8 \\
 22
 \end{array}
 \quad
 \begin{array}{r}
 5.9 \\
 33
 \end{array}
 \quad
 \begin{array}{r}
 6.4 \\
 40
 \end{array}
 \end{array}
 \qquad
 \begin{array}{r}
 C9.9 \\
 \hline
 33
 \end{array}$$

$$\begin{array}{r}
 14.5 \\
 \hline
 \begin{array}{r}
 2.5 \\
 21
 \end{array}
 \quad
 \begin{array}{r}
 7.4 \\
 17
 \end{array}
 \quad
 \begin{array}{r}
 10.1 \\
 9
 \end{array}
 \quad
 \begin{array}{r}
 9.6 \\
 +4.9
 \end{array}
 \quad
 \begin{array}{r}
 9.4 \\
 3
 \end{array}
 \quad
 \begin{array}{r}
 10.0 \\
 13
 \end{array}
 \quad
 \begin{array}{r}
 4.0 \\
 20
 \end{array}
 \quad
 \begin{array}{r}
 6.1 \\
 30
 \end{array}
 \quad
 \begin{array}{r}
 6.1 \\
 32.8
 \end{array}
 \quad
 \begin{array}{r}
 7.3 \\
 40
 \end{array}
 \end{array}
 \qquad
 \begin{array}{r}
 C8.8 \\
 \hline
 32.8
 \end{array}$$

$$\begin{array}{r}
 13.8 \\
 \hline
 \begin{array}{r}
 0.0 \\
 19
 \end{array}
 \quad
 \begin{array}{r}
 6.6 \\
 10
 \end{array}
 \quad
 \begin{array}{r}
 8.5 \\
 7
 \end{array}
 \quad
 \begin{array}{r}
 8.5 \\
 +5.3
 \end{array}
 \quad
 \begin{array}{r}
 8.6 \\
 13
 \end{array}
 \quad
 \begin{array}{r}
 5.9 \\
 18
 \end{array}
 \quad
 \begin{array}{r}
 8.4 \\
 26
 \end{array}
 \quad
 \begin{array}{r}
 8.5 \\
 29.6
 \end{array}
 \quad
 \begin{array}{r}
 9.3 \\
 33
 \end{array}
 \end{array}
 \qquad
 \begin{array}{r}
 C5.4 \\
 \hline
 29.6
 \end{array}$$

$$\begin{array}{r}
 C18.3 \\
 \hline
 42.3
 \end{array}
 \qquad
 \begin{array}{r}
 6.5 \\
 45
 \end{array}
 \quad
 \begin{array}{r}
 2.0 \\
 42.3
 \end{array}
 \quad
 \begin{array}{r}
 11.1 \\
 25
 \end{array}
 \quad
 26.0$$

$$\begin{array}{r}
 C19.8 \\
 \hline
 43.8
 \end{array}
 \qquad
 \begin{array}{r}
 3.7 \\
 45
 \end{array}
 \quad
 \begin{array}{r}
 4.5 \\
 43.8
 \end{array}
 \quad
 24.8$$

937.66

41

0.4 0.4

13.7 ✓

23.6

24.0

+20

0.3 0.3

14.4 ✓

23.0

23.3

+50

0.2 0.2

15.3 ✓

22.2

22.4

42

14.5 ✓

21.2

+50

17.2 ✓

20.7

20.5

T.P.

0.08

924.31 ✓

13.43

924.23 ✓

41+50

0.2 0.2

15.3 ✓

9.0

9.2

42

14.5 ✓

7.8

+50

17.2 ✓

7.1

T.P.

4.58

921.37 ✓

7.52

916.79 ✓

43

17.4 ✓

4.0

$$\begin{array}{r} \underline{C22.6} \\ 45 \end{array} \quad \begin{array}{r} \underline{0.0} \\ 50 \end{array} \quad \begin{array}{r} \underline{1.0} \\ 45 \end{array} \quad \begin{array}{r} \underline{1.7} \\ 41 \end{array} \quad \begin{array}{r} \underline{3.4} \\ 41 \end{array} \quad \begin{array}{r} \underline{9.9} \\ 30 \end{array} \quad 24.0$$

$$\begin{array}{r} \underline{C21.9} \\ 45 \end{array} \quad \begin{array}{r} \underline{0.1} \\ 49 \end{array} \quad \begin{array}{r} \underline{1.1} \\ 45 \end{array} \quad \begin{array}{r} \underline{4.7} \\ 20 \end{array} \quad 23.3$$

$$\begin{array}{r} \underline{C18.7} \\ 42.7 \end{array} \quad \begin{array}{r} \underline{2.8} \\ 45 \end{array} \quad \begin{array}{r} \underline{3.5} \\ 42.7 \end{array} \quad \begin{array}{r} \underline{9.6} \\ 18 \end{array} \quad \begin{array}{r} \underline{12.5} \\ 17 \end{array} \quad 22.4$$

$$\begin{array}{r} \underline{C12.7} \\ 36.7 \end{array} \quad \begin{array}{r} \underline{6.3} \\ 45 \end{array} \quad \begin{array}{r} \underline{8.5} \\ 36.7 \end{array} \quad \begin{array}{r} \underline{11.7} \\ 24 \end{array} \quad 21.2$$

$$\begin{array}{r} \underline{10.6} \\ 45 \end{array} \quad \begin{array}{r} \underline{12.6} \\ 39 \end{array} \quad 20.5$$

$$\begin{array}{r} \underline{2.8} \\ 12 \end{array} \quad \begin{array}{r} \underline{4.0} \\ 8 \end{array} \quad \begin{array}{r} \underline{9.0} \\ 3.8 \\ +5.2 \end{array} \quad \begin{array}{r} \underline{4.1} \\ 15 \end{array} \quad \begin{array}{r} \underline{7.7} \\ 21 \end{array} \quad \begin{array}{r} \underline{8.7} \\ 24.8 \end{array} \quad \begin{array}{r} \underline{10.0} \\ 33 \end{array} \quad \begin{array}{r} \underline{C0.5} \\ 24.8 \end{array}$$

$$\begin{array}{r} \underline{3.0} \\ 19 \end{array} \quad \begin{array}{r} \underline{4.9} \\ 14 \end{array} \quad \begin{array}{r} \underline{4.6} \\ 6 \end{array} \quad \begin{array}{r} \underline{7.8} \\ 4.9 \\ +2.9 \end{array} \quad \begin{array}{r} \underline{5.5} \\ 7 \end{array} \quad \begin{array}{r} \underline{9.4} \\ 14 \end{array} \quad \begin{array}{r} \underline{9.8} \\ 19.5 \end{array} \quad \begin{array}{r} \underline{12.0} \\ 33 \end{array} \quad \begin{array}{r} \underline{DC0.0} \\ 19.5 \end{array}$$

$$\begin{array}{r} \underline{C5.0} \\ 29 \end{array} \quad \begin{array}{r} \underline{2.1} \\ 29 \end{array} \quad \begin{array}{r} \underline{4.5} \\ 27 \end{array} \quad \begin{array}{r} \underline{5.4} \\ 23 \end{array} \quad \begin{array}{r} \underline{5.6} \\ 10 \end{array} \quad \begin{array}{r} \underline{7.1} \\ 6.5 \\ +0.6 \end{array} \quad \begin{array}{r} \underline{11.6} \\ 9 \end{array} \quad \begin{array}{r} \underline{13.3} \\ 25.4 \end{array} \quad \begin{array}{r} \underline{13.7} \\ 33 \end{array} \quad \begin{array}{r} \underline{F6.2} \\ 25.4 \end{array}$$

$$\begin{array}{r} \underline{C0.9} \\ 25.4 \end{array} \quad \begin{array}{r} \underline{0.7} \\ 33 \end{array} \quad \begin{array}{r} \underline{0.9} \\ 29 \end{array} \quad \begin{array}{r} \underline{3.1} \\ 25.4 \end{array} \quad \begin{array}{r} \underline{3.4} \\ 24 \end{array} \quad \begin{array}{r} \underline{3.4} \\ 14 \end{array} \quad \begin{array}{r} \underline{4.3} \\ 5 \end{array} \quad \begin{array}{r} \underline{4.0} \\ 6.9 \\ -2.9 \end{array} \quad \begin{array}{r} \underline{9.0} \\ 4 \end{array} \quad \begin{array}{r} \underline{11.1} \\ 27.2 \end{array} \quad \begin{array}{r} \underline{11.3} \\ 33 \end{array} \quad \begin{array}{r} \underline{F7.1} \\ 27.2 \end{array}$$

921.37

43+50

17.8 ✓ 3.6

44

18.5 ✓ 2.9

+50

super
0.2 0.2 19.5 ✓ 2.1 1.7
1.9

45

Wid. Lt.
1.0 0.6 0.5 20.8 ✓ 1.2 0.1
0.6

T.P. 9.80 928.87 ✓ 2.30 919.07 ✓

+25 2.0 0.8 0.7 21.7 ✓ 8.0 6.5
7.2

B.M. 8.51 931.62 ✓ 5.77 923.10 ✓ 923.11

+75 4.0 1.2 0.9 23.8 ✓ 9.0 6.9
7.8

46

930.49 5.0 1.5 1.1 25.0 ✓ 8.1 5.5
6.6

1339

943.88

+50 5.0 1.5 1.1 27.9 ✓ 5.2 2.6
3.7

47

2.5 1.0 0.8 31.5 ✓ 1.1 40.7
0.1

T.P. 13.77 944.60 ✓ 0.79 930.83 ✓

								29						
DCO.2	<u>2.5</u>	<u>4.1</u>	<u>4.7</u>	<u>4.8</u>	<u>5.6</u>	<u>8.1</u>	<u>9.4</u>	<u>9.4</u>	<u>10.9</u>	<u>11.2</u>				F 8.0
21.3	33	30	21.3	19	10	6	3	-6.5	29	33				29

<u>C3.3</u>	<u>4.5</u>	<u>4.7</u>	<u>5.8</u>	<u>9.1</u>	<u>9.2</u>	<u>9.7</u>	<u>9.0</u>	<u>13.2</u>	<u>14.2</u>	<u>14.6</u>	<u>14.9</u>	<u>F8.1</u>
31	30	31	23	17	3	1	-1.8	9	15	29.2	33	29.2

Spk. in 12" B.E. 40' Bt. 46+60 7.8

$\frac{C4.3}{33}$	$\frac{4.2}{40}$	$\frac{4.7}{33}$	$\frac{5.9}{20}$	$\frac{9.0}{16}$	$\frac{8.1}{8}$	$\frac{8.1}{-0.3}$	$\frac{8.1}{4}$	$\frac{7.8}{6}$	$\frac{8.7}{13}$	$\frac{9.1}{17.4}$	$\frac{10.6}{24}$	$\frac{11.7}{33}$	$\frac{F2.2}{17.4}$
-------------------	------------------	------------------	------------------	------------------	-----------------	--------------------	-----------------	-----------------	------------------	--------------------	-------------------	-------------------	---------------------

944.60

47+50

1.0

0.6 0.5

35.4 ✓

9.6 8.5
9.0

48

0.0

0.2 0.2

40.3 ✓

4.5 4.1
4.3

T.P.

11.36

955.46 ✓

0.50

944.10 ✓

+50

0.0

45.3 ✓

10.2

49

0.2 0.2

50.3 ✓

5.2

T.P.

12.11

967.37 ✓

0.20

955.26 ✓

+50

0.4 0.4

55.3 ✓

12.1

T.P.

11.96

974.37 ✓

4.96

962.41 ✓

50

Wid. RT.

1.0

0.7 0.8

60.3 ✓

13.4 14.9
14.1

T.P.

6.01

978.74 ✓

1.64

972.73 ✓

+50

2.0

1.0 1.2

65.3 ✓

12.4 14.6
13.4

51

2.0

1.0 1.2

70.1 ✓

7.6 9.8
8.6

+50

2.0

1.0 1.2

74.0 ✓

3.7 5.9
4.7

T.P.

5.18

982.96 ✓

0.96

977.78 ✓

$$\begin{array}{r}
 \text{DC0.5} \\
 \hline
 22.8
 \end{array}
 \quad
 \begin{array}{cccccccc}
 9.0 \\
 \frac{11.7}{28} \quad \frac{11.1}{22.8} \quad \frac{10.0}{5} \quad \frac{10.2}{-1.2} \quad \frac{10.7}{9} \quad \frac{12.3}{12} \quad \frac{13.0}{2.2} \quad \frac{13.0}{33}
 \end{array}
 \quad
 \begin{array}{r}
 F4.5 \\
 \hline
 22
 \end{array}$$

$$\begin{array}{r}
 F2.8 \\
 \hline
 18.6
 \end{array}
 \quad
 \begin{array}{cccccccc}
 4.3 \\
 \frac{7.1}{29} \quad \frac{6.7}{23} \quad \frac{7.4}{22} \quad \frac{7.3}{18.6} \quad \frac{6.2}{13} \quad \frac{5.9}{-1.6} \quad \frac{6.1}{7} \quad \frac{6.9}{10} \quad \frac{8.1}{11} \quad \frac{6.6}{13} \quad \frac{6.6}{18} \quad \frac{6.3}{24} \quad \frac{5.0}{33}
 \end{array}
 \quad
 \begin{array}{r}
 F2.5 \\
 \hline
 18
 \end{array}$$

$$\begin{array}{r}
 F2.7 \\
 \hline
 18.4
 \end{array}
 \quad
 \begin{array}{cccccccc}
 10.2 \\
 \frac{12.2}{26} \quad \frac{12.9}{18.4} \quad \frac{12.1}{14} \quad \frac{11.3}{-1.1} \quad \frac{11.5}{9} \quad \frac{13.6}{15} \quad \frac{16.1}{18} \quad \frac{10.7}{23.3} \quad \frac{9.1}{33}
 \end{array}
 \quad
 \begin{array}{r}
 DC1.5 \\
 \hline
 23.3
 \end{array}$$

$$\begin{array}{r}
 C4.6 \\
 \hline
 30.9
 \end{array}
 \quad
 \begin{array}{cccccccc}
 5.2 \\
 \frac{0.2}{33} \quad \frac{0.6}{30.9} \quad \frac{1.6}{20} \quad \frac{6.2}{17} \quad \frac{5.7}{12} \quad \frac{5.6}{-0.4} \quad \frac{6.0}{10} \quad \frac{6.8}{15} \quad \frac{8.1}{15} \quad \frac{8.1}{17} \quad \frac{4.6}{19} \quad \frac{3.5}{26.6} \quad \frac{2.3}{33}
 \end{array}
 \quad
 \begin{array}{r}
 C1.7 \\
 \hline
 26.6
 \end{array}$$

$$\begin{array}{r}
 C10.3 \\
 \hline
 39.5
 \end{array}
 \quad
 \begin{array}{cccccccc}
 12.1 \\
 \frac{1.3}{45} \quad \frac{1.8}{39.5} \quad \frac{2.9}{32} \quad \frac{3.8}{24} \quad \frac{12.2}{16} \quad \frac{11.7}{13} \quad \frac{11.4}{-0.7} \quad \frac{11.8}{9} \quad \frac{13.6}{11} \quad \frac{13.6}{13} \quad \frac{7.9}{19} \quad \frac{7.8}{25} \quad \frac{9.1}{29.5} \quad \frac{6.3}{33}
 \end{array}
 \quad
 \begin{array}{r}
 C3.0 \\
 \hline
 29.5
 \end{array}$$

$$\begin{array}{r}
 C11.4 \\
 \hline
 40
 \end{array}
 \quad
 \begin{array}{cccccccc}
 14.1 \\
 \frac{1.0}{45} \quad \frac{2.0}{40} \quad \frac{4.5}{24} \quad \frac{13.1}{15} \quad \frac{12.7}{-1.4} \quad \frac{12.9}{9} \quad \frac{14.2}{15} \quad \frac{7.6}{20} \quad \frac{6.4}{26} \quad \frac{6.0}{33} \quad \frac{4.9}{40} \quad \frac{4.0}{45}
 \end{array}
 \quad
 \begin{array}{r}
 C10.0 \\
 \hline
 40
 \end{array}$$

$$\begin{array}{r}
 C6.2 \\
 \hline
 33.3
 \end{array}
 \quad
 \begin{array}{cccccccc}
 13.4 \\
 \frac{5.5}{40} \quad \frac{6.2}{33.3} \quad \frac{7.3}{22} \quad \frac{12.3}{16} \quad \frac{11.8}{11} \quad \frac{11.6}{-1.8} \quad \frac{12.1}{10} \quad \frac{13.1}{12} \quad \frac{12.8}{15} \quad \frac{5.6}{23} \quad \frac{2.9}{40} \quad \frac{2.3}{45}
 \end{array}
 \quad
 \begin{array}{r}
 C11.7 \\
 \hline
 40
 \end{array}$$

$$\begin{array}{r}
 C0.4 \\
 \hline
 24.6
 \end{array}
 \quad
 \begin{array}{cccccccc}
 8.6 \\
 \frac{7.2}{33} \quad \frac{7.2}{24.6} \quad \frac{7.0}{17} \quad \frac{8.3}{15} \quad \frac{7.6}{10} \quad \frac{7.0}{-1.6} \quad \frac{7.4}{11} \quad \frac{7.7}{17} \quad \frac{4.8}{22} \quad \frac{3.6}{35.3} \quad \frac{3.0}{40}
 \end{array}
 \quad
 \begin{array}{r}
 C6.2 \\
 \hline
 35.3
 \end{array}$$

$$\begin{array}{r}
 C0.6 \\
 \hline
 24.9
 \end{array}
 \quad
 \begin{array}{cccccccc}
 4.7 \\
 \frac{2.8}{33} \quad \frac{3.1}{24.9} \quad \frac{3.2}{14} \quad \frac{4.3}{12} \quad \frac{3.9}{8} \quad \frac{3.6}{-1.1} \quad \frac{4.0}{12} \quad \frac{4.0}{18} \quad \frac{2.7}{22} \quad \frac{2.3}{31.4} \quad \frac{2.0}{33}
 \end{array}
 \quad
 \begin{array}{r}
 C2.6 \\
 \hline
 31.4
 \end{array}$$

982.96

52

1.0

0.8

0.9

76.7 ✓

5.5

7.2

6.3

+50

0.0

0.4

0.4

78.2 ✓

4.4

5.2

4.8

53

0.0

78.6 ✓

4.4

B.M.

3.97

978.99 ✓

979.00

B.M.

987.67

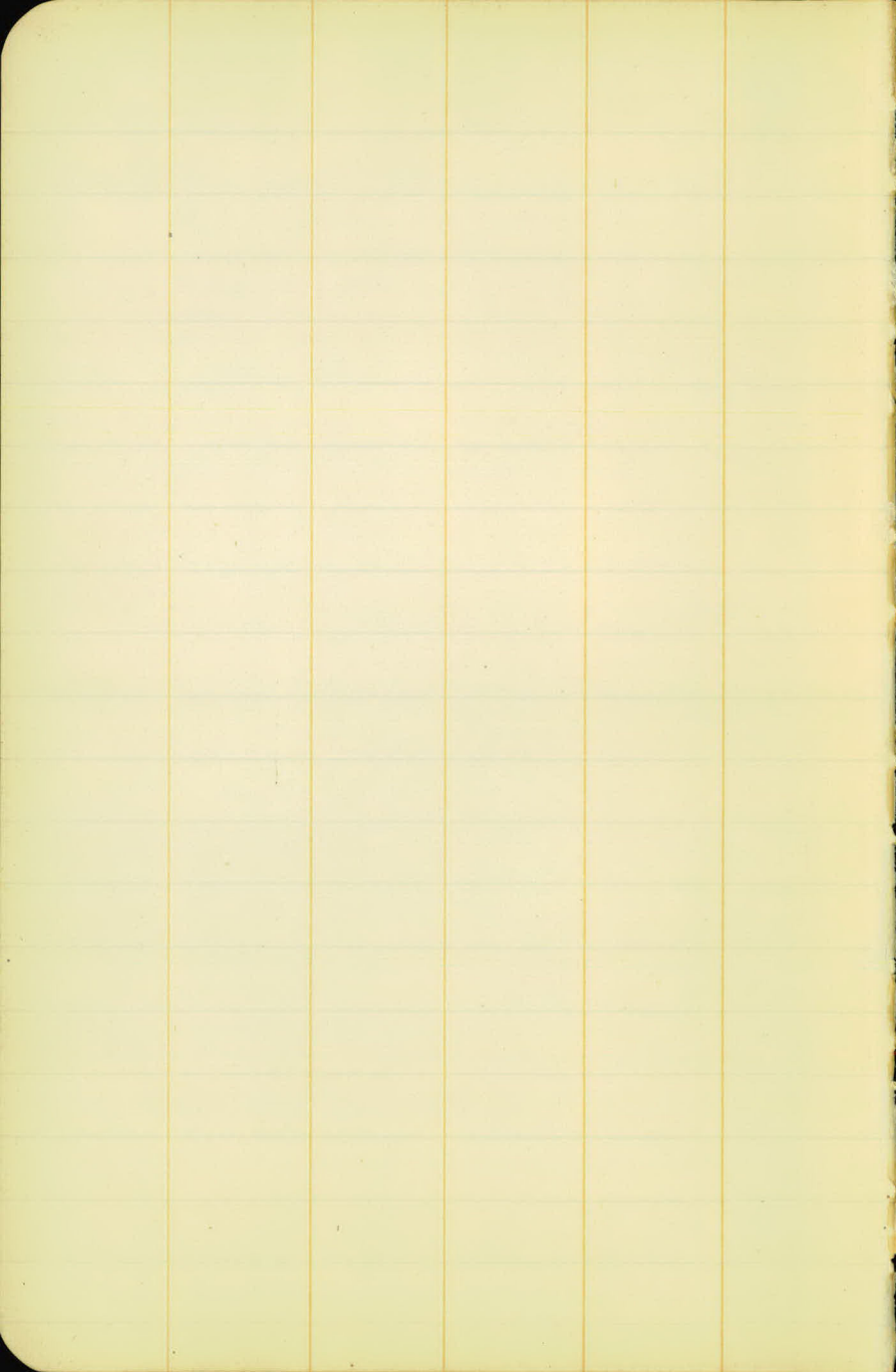
<u>C3.0</u>	<u>2.2</u>	<u>2.5</u>	<u>3.9</u>	<u>5.5</u>	<u>5.3</u>	<u>5.2</u>	<u>5.7</u>	<u>6.2</u>	<u>4.5</u>	<u>4.2</u>	<u>3.8</u>	<u>C3.0</u>
28.5	33	28.5	13	10	11.0	7	16	18	20	29.5	33	29.5

<u>DC0.5</u>	<u>5.9</u>	<u>5.9</u>	<u>5.9</u>	<u>5.2</u>	<u>4.5</u>	<u>4.9</u>	<u>5.7</u>	<u>5.6</u>	<u>5.5</u>	<u>DC1.6</u>
21.8	33	21.8	14	9	10.3	10	16	23.4	33	23.4

<u>5.6</u>	<u>5.1</u>	<u>4.3</u>	<u>4.2</u>	<u>5.2</u>	<u>5.2</u>
33	13	10.1	10	14	33

Spt. in P.P. N.W. Cor. Carver Ave & E. Co. Line

Spt. in Tree Stumps at E. Cor. 300 Lt 53+38'



B.M.

4.98

864.77 ✓

859.79

0-100

0+00

+50

1

+50

2

+50

T.P.

13.29

874.47 ✓

3.59

861.18 ✓

3

+25

O.O. Section

$\frac{11.2}{23}$	$\frac{12.4}{21}$	$\frac{12.5}{17}$	$\frac{10.5}{13}$	10.7 10.6	$\frac{10.7}{13}$	$\frac{12.5}{17}$	$\frac{12.4}{21}$	$\frac{9.0}{27}$
-------------------	-------------------	-------------------	-------------------	--------------	-------------------	-------------------	-------------------	------------------

$\frac{10.6}{23}$	$\frac{11.8}{20}$	$\frac{11.9}{17}$	$\frac{10.0}{13}$	9.9 9.4	$\frac{9.5}{13}$	$\frac{11.7}{18}$	$\frac{11.7}{22}$	$\frac{10.0}{24}$
-------------------	-------------------	-------------------	-------------------	------------	------------------	-------------------	-------------------	-------------------

$\frac{10.8}{18}$	$\frac{8.9}{13}$	8.8 8.6	$\frac{8.8}{13}$	$\frac{10.9}{18}$	$\frac{10.9}{21}$	$\frac{10.2}{22}$
-------------------	------------------	------------	------------------	-------------------	-------------------	-------------------

$\frac{10.0}{19}$	$\frac{7.5}{13}$	1.5 7.2	$\frac{7.7}{13}$	$\frac{9.7}{17}$	$\frac{9.7}{21}$	$\frac{8.9}{22}$
-------------------	------------------	------------	------------------	------------------	------------------	------------------

$\frac{9.1}{20}$	$\frac{5.7}{13}$	5.7 5.6	$\frac{5.6}{13}$	$\frac{7.9}{17}$	$\frac{7.8}{21}$	$\frac{6.4}{23}$
------------------	------------------	------------	------------------	------------------	------------------	------------------

$\frac{6.6}{18}$	$\frac{3.8}{13}$	3.6 3.4	$\frac{3.5}{13}$	$\frac{5.5}{17}$	$\frac{5.5}{21}$	$\frac{4.3}{23}$
------------------	------------------	------------	------------------	------------------	------------------	------------------

$\frac{11.9}{40}$	$\frac{10.6}{27}$	$\frac{13.3}{22}$	$\frac{13.3}{17}$	$\frac{11.3}{13}$	11.1 11.0	$\frac{11.2}{13}$	$\frac{13.2}{17}$	$\frac{13.3}{21}$	$\frac{9.3}{27}$	$\frac{8.6}{30}$
-------------------	-------------------	-------------------	-------------------	-------------------	--------------	-------------------	-------------------	-------------------	------------------	------------------

$\frac{1.9}{36}$	$\frac{11.6}{21}$	$\frac{11.8}{16}$	$\frac{10.3}{13}$	10.2 10.0	$\frac{10.0}{13}$	$\frac{11.8}{17}$	$\frac{11.8}{21}$	$\frac{8.5}{26}$
------------------	-------------------	-------------------	-------------------	--------------	-------------------	-------------------	-------------------	------------------

✓
874.47

3+50

+80

4

+40

+70

5

+50

6

T.P.

10.12

✓
882.23

2.36

✓
872.11

+50

$$\begin{array}{r} 3.4 \\ \hline 33 \end{array} \quad \begin{array}{r} 10.6 \\ \hline 21 \end{array} \quad \begin{array}{r} 10.6 \\ \hline 17 \end{array} \quad \begin{array}{r} 9.1 \\ \hline 13 \end{array} \quad 9.2 \quad \begin{array}{r} 9.1 \\ \hline 13 \end{array} \quad \begin{array}{r} 11.1 \\ \hline 17 \end{array} \quad \begin{array}{r} 10.8 \\ \hline 20 \end{array} \quad \begin{array}{r} 3.3 \\ \hline 33 \end{array}$$

$$\begin{array}{r} 7.0 \\ \hline 26 \end{array} \quad \begin{array}{r} 9.5 \\ \hline 21 \end{array} \quad \begin{array}{r} 9.5 \\ \hline 17 \end{array} \quad \begin{array}{r} 7.9 \\ \hline 13 \end{array} \quad 8.2 \quad \begin{array}{r} 7.9 \\ \hline 13 \end{array} \quad \begin{array}{r} 9.8 \\ \hline 17 \end{array} \quad \begin{array}{r} 9.8 \\ \hline 20 \end{array} \quad \begin{array}{r} 6.9 \\ \hline 26 \end{array}$$

$$\begin{array}{r} 7.2 \\ \hline 25 \end{array} \quad \begin{array}{r} 9.2 \\ \hline 21 \end{array} \quad \begin{array}{r} 9.3 \\ \hline 17 \end{array} \quad \begin{array}{r} 7.6 \\ \hline 13 \end{array} \quad 1.1 \quad \begin{array}{r} 7.5 \\ \hline 13 \end{array} \quad \begin{array}{r} 9.4 \\ \hline 18 \end{array} \quad \begin{array}{r} 9.7 \\ \hline 21 \end{array}$$

$$\begin{array}{r} 7.5 \\ \hline 22 \end{array} \quad \begin{array}{r} 8.3 \\ \hline 21 \end{array} \quad \begin{array}{r} 8.5 \\ \hline 17 \end{array} \quad \begin{array}{r} 6.4 \\ \hline 13 \end{array} \quad 6.8 \quad \begin{array}{r} 6.4 \\ \hline 13 \end{array} \quad \begin{array}{r} 13.3 \\ \hline 27 \end{array}$$

$$\begin{array}{r} 6.4 \\ \hline 23 \end{array} \quad \begin{array}{r} 7.5 \\ \hline 21 \end{array} \quad \begin{array}{r} 7.5 \\ \hline 17 \end{array} \quad \begin{array}{r} 5.8 \\ \hline 13 \end{array} \quad 5.6 \quad \begin{array}{r} 5.7 \\ \hline 13 \end{array} \quad \begin{array}{r} 7.7 \\ \hline 17 \end{array} \quad \begin{array}{r} 7.7 \\ \hline 21 \end{array} \quad \begin{array}{r} 7.3 \\ \hline 22 \end{array}$$

$$\begin{array}{r} 6.0 \\ \hline 23 \end{array} \quad \begin{array}{r} 7.0 \\ \hline 21 \end{array} \quad \begin{array}{r} 7.1 \\ \hline 17 \end{array} \quad \begin{array}{r} 5.1 \\ \hline 13 \end{array} \quad 5.0 \quad \begin{array}{r} 5.1 \\ \hline 13 \end{array} \quad \begin{array}{r} 6.9 \\ \hline 17 \end{array} \quad \begin{array}{r} 6.9 \\ \hline 20 \end{array} \quad \begin{array}{r} 5.9 \\ \hline 23 \end{array}$$

$$\begin{array}{r} 5.2 \\ \hline 23 \end{array} \quad \begin{array}{r} 5.9 \\ \hline 21 \end{array} \quad \begin{array}{r} 6.0 \\ \hline 17 \end{array} \quad \begin{array}{r} 4.0 \\ \hline 13 \end{array} \quad 4.0 \quad \begin{array}{r} 4.1 \\ \hline 13 \end{array} \quad \begin{array}{r} 6.1 \\ \hline 17 \end{array} \quad \begin{array}{r} 6.1 \\ \hline 21 \end{array} \quad \begin{array}{r} 4.4 \\ \hline 24 \end{array}$$

$$\begin{array}{r} 2.6 \\ \hline 25 \end{array} \quad \begin{array}{r} 5.0 \\ \hline 21 \end{array} \quad \begin{array}{r} 5.0 \\ \hline 17 \end{array} \quad \begin{array}{r} 3.2 \\ \hline 13 \end{array} \quad 3.2 \quad \begin{array}{r} 3.4 \\ \hline 13 \end{array} \quad \begin{array}{r} 5.1 \\ \hline 17 \end{array} \quad \begin{array}{r} 5.2 \\ \hline 21 \end{array} \quad \begin{array}{r} 4.9 \\ \hline 21 \end{array}$$

$$\begin{array}{r} 8.2 \\ \hline 27 \end{array} \quad \begin{array}{r} 11.9 \\ \hline 21 \end{array} \quad \begin{array}{r} 12.0 \\ \hline 18 \end{array} \quad \begin{array}{r} 10.1 \\ \hline 13 \end{array} \quad 10.1 \quad \begin{array}{r} 10.1 \\ \hline 13 \end{array} \quad \begin{array}{r} 12.0 \\ \hline 17 \end{array}$$

✓
182.23

7

+50

8

+50

9

+50

10

+50

11

$$\begin{array}{r} 2.7 \\ 27 \end{array} \quad \begin{array}{r} 11.1 \\ 21 \end{array} \quad \begin{array}{r} 11.2 \\ 17 \end{array} \quad \begin{array}{r} 9.3 \\ 13 \end{array} \quad \begin{array}{r} 9.7 \\ 9.2 \end{array} \quad \begin{array}{r} 8.3 \\ 13 \end{array} \quad \begin{array}{r} 11.3 \\ 17 \end{array} \quad \begin{array}{r} 11.3 \\ 21 \end{array} \quad \begin{array}{r} 10.0 \\ 23 \end{array}$$

$$\begin{array}{r} 7.1 \\ 26 \end{array} \quad \begin{array}{r} 10.5 \\ 21 \end{array} \quad \begin{array}{r} 10.5 \\ 17 \end{array} \quad \begin{array}{r} 8.5 \\ 13 \end{array} \quad \begin{array}{r} 8.5 \\ 8.4 \end{array} \quad \begin{array}{r} 8.7 \\ 13 \end{array} \quad \begin{array}{r} 10.5 \\ 17 \end{array} \quad \begin{array}{r} 10.4 \\ 21 \end{array} \quad \begin{array}{r} 8.9 \\ 23 \end{array}$$

$$\begin{array}{r} 6.0 \\ 26 \end{array} \quad \begin{array}{r} 9.8 \\ 21 \end{array} \quad \begin{array}{r} 9.7 \\ 17 \end{array} \quad \begin{array}{r} 7.7 \\ 13 \end{array} \quad \begin{array}{r} 7.7 \\ 7.5 \end{array} \quad \begin{array}{r} 7.7 \\ 13 \end{array} \quad \begin{array}{r} 9.8 \\ 17 \end{array} \quad \begin{array}{r} 9.8 \\ 21 \end{array} \quad \begin{array}{r} 7.4 \\ 25 \end{array}$$

$$\begin{array}{r} 5.8 \\ 26 \end{array} \quad \begin{array}{r} 8.9 \\ 21 \end{array} \quad \begin{array}{r} 8.9 \\ 17 \end{array} \quad \begin{array}{r} 6.9 \\ 13 \end{array} \quad \begin{array}{r} 6.9 \\ 6.8 \end{array} \quad \begin{array}{r} 6.9 \\ 13 \end{array} \quad \begin{array}{r} 9.0 \\ 17 \end{array} \quad \begin{array}{r} 9.1 \\ 21 \end{array} \quad \begin{array}{r} 8.6 \\ 22 \end{array}$$

$$\begin{array}{r} 5.0 \\ 26 \end{array} \quad \begin{array}{r} 8.2 \\ 21 \end{array} \quad \begin{array}{r} 8.2 \\ 17 \end{array} \quad \begin{array}{r} 6.3 \\ 13 \end{array} \quad \begin{array}{r} 6.1 \\ 6.0 \end{array} \quad \begin{array}{r} 6.1 \\ 13 \end{array} \quad \begin{array}{r} 8.1 \\ 17 \end{array}$$

$$\begin{array}{r} 3.0 \\ 28 \end{array} \quad \begin{array}{r} 7.1 \\ 21 \end{array} \quad \begin{array}{r} 7.2 \\ 17 \end{array} \quad \begin{array}{r} 5.2 \\ 13 \end{array} \quad \begin{array}{r} 5.3 \\ 5.0 \end{array} \quad \begin{array}{r} 5.3 \\ 13 \end{array} \quad \begin{array}{r} 6.9 \\ 17 \end{array} \quad \begin{array}{r} 6.9 \\ 21 \end{array} \quad \begin{array}{r} 5.8 \\ 23 \end{array}$$

$$\begin{array}{r} 0.7 \\ 30 \end{array} \quad \begin{array}{r} 6.6 \\ 21 \end{array} \quad \begin{array}{r} 6.5 \\ 17 \end{array} \quad \begin{array}{r} 4.5 \\ 13 \end{array} \quad \begin{array}{r} 4.5 \\ 4.4 \end{array} \quad \begin{array}{r} 4.5 \\ 13 \end{array} \quad \begin{array}{r} 6.5 \\ 17 \end{array} \quad \begin{array}{r} 6.3 \\ 21 \end{array} \quad \begin{array}{r} 4.2 \\ 24 \end{array}$$

$$\begin{array}{r} 1.0 \\ 28 \end{array} \quad \begin{array}{r} 5.8 \\ 22 \end{array} \quad \begin{array}{r} 5.7 \\ 17 \end{array} \quad \begin{array}{r} 3.7 \\ 13 \end{array} \quad \begin{array}{r} 3.7 \\ 3.8 \end{array} \quad \begin{array}{r} 3.7 \\ 13 \end{array} \quad \begin{array}{r} 5.8 \\ 17 \end{array} \quad \begin{array}{r} 5.7 \\ 20 \end{array} \quad \begin{array}{r} 4.0 \\ 24 \end{array}$$

$$\begin{array}{r} 1.8 \\ 26 \end{array} \quad \begin{array}{r} 4.8 \\ 21 \end{array} \quad \begin{array}{r} 4.9 \\ 17 \end{array} \quad \begin{array}{r} 2.9 \\ 13 \end{array} \quad \begin{array}{r} 2.9 \\ 2.9 \end{array} \quad \begin{array}{r} 3.0 \\ 13 \end{array} \quad \begin{array}{r} 5.0 \\ 17 \end{array} \quad \begin{array}{r} 5.0 \\ 21 \end{array} \quad \begin{array}{r} 3.5 \\ 23 \end{array}$$

✓
882.23

11+50

+82

T.P.

10.52

✓
889.86

2.89

✓
879.34

12

+50

+75

B.M.

6.62

883.24

883.24

13

T.P.

7.85

✓
886.06

11.65

✓
878.21

+50

14

+80

✓
886.06

15

+50

16

+50

17

+50

18

+50

19

✓

T.P.

8.32

894.01

0.37

✓

885.69

$$\begin{array}{r} 9.9 \\ 20 \end{array} \quad \begin{array}{r} 6.4 \\ 13 \end{array} \quad \begin{array}{r} 6.4 \\ 6.1 \end{array} \quad \begin{array}{r} 6.4 \\ 13 \end{array} \quad \begin{array}{r} 9.9 \\ 21 \end{array}$$

$$\begin{array}{r} 9.8 \\ 20 \end{array} \quad \begin{array}{r} 6.5 \\ 13 \end{array} \quad \begin{array}{r} 6.5 \\ 6.1 \end{array} \quad \begin{array}{r} 6.5 \\ 13 \end{array} \quad \begin{array}{r} 10.3 \\ 21 \end{array}$$

$$\begin{array}{r} 9.8 \\ 20 \end{array} \quad \begin{array}{r} 6.3 \\ 13 \end{array} \quad \begin{array}{r} 6.3 \\ 5.9 \end{array} \quad \begin{array}{r} 6.3 \\ 13 \end{array} \quad \begin{array}{r} 10.1 \\ 21 \end{array}$$

$$\begin{array}{r} 9.2 \\ 20 \end{array} \quad \begin{array}{r} 6.0 \\ 13 \end{array} \quad \begin{array}{r} 6.0 \\ 5.7 \end{array} \quad \begin{array}{r} 6.0 \\ 13 \end{array} \quad \begin{array}{r} 9.8 \\ 21 \end{array}$$

$$\begin{array}{r} 9.1 \\ 21 \end{array} \quad \begin{array}{r} 5.4 \\ 13 \end{array} \quad \begin{array}{r} 5.4 \\ 5.1 \end{array} \quad \begin{array}{r} 5.4 \\ 13 \end{array} \quad \begin{array}{r} 8.9 \\ 22 \end{array}$$

$$\begin{array}{r} 8.7 \\ 22 \end{array} \quad \begin{array}{r} 4.7 \\ 13 \end{array} \quad \begin{array}{r} 4.7 \\ 4.6 \end{array} \quad \begin{array}{r} 4.8 \\ 13 \end{array} \quad \begin{array}{r} 9.2 \\ 22 \end{array}$$

$$\begin{array}{r} 8.7 \\ 23 \end{array} \quad \begin{array}{r} 4.0 \\ 13 \end{array} \quad \begin{array}{r} 4.0 \\ 3.8 \end{array} \quad \begin{array}{r} 4.1 \\ 13 \end{array} \quad \begin{array}{r} 8.6 \\ 23 \end{array}$$

$$\begin{array}{r} 8.3 \\ 23 \end{array} \quad \begin{array}{r} 3.3 \\ 13 \end{array} \quad \begin{array}{r} 3.3 \\ 3.0 \end{array} \quad \begin{array}{r} 3.3 \\ 13 \end{array} \quad \begin{array}{r} 6.5 \\ 22 \end{array}$$

$$\begin{array}{r} 6.6 \\ 21 \end{array} \quad \begin{array}{r} 2.6 \\ 13 \end{array} \quad \begin{array}{r} 2.6 \\ 2.5 \end{array} \quad \begin{array}{r} 2.7 \\ 13 \end{array} \quad \begin{array}{r} 4.4 \\ 16 \end{array} \quad \begin{array}{r} 4.5 \\ 20 \end{array} \quad \text{Cont. on Page 27}$$

✓
894.01

19+30

+70

20

+50

21

+50

22

+25

+75

$$\begin{array}{r} 10.6 \\ 25 \end{array} \quad \begin{array}{r} 11.8 \\ 21 \end{array} \quad \begin{array}{r} 11.9 \\ 18 \end{array} \quad \begin{array}{r} 10.0 \\ 13 \end{array} \quad \begin{array}{r} 10.1 \\ 9.8 \end{array} \quad \begin{array}{r} 10.1 \\ 13 \end{array} \quad \begin{array}{r} 11.8 \\ 17 \end{array} \quad \begin{array}{r} 11.8 \\ 21 \end{array}$$

$$\begin{array}{r} 9.5 \\ 24 \end{array} \quad \begin{array}{r} 11.4 \\ 21 \end{array} \quad \begin{array}{r} 11.4 \\ 17 \end{array} \quad \begin{array}{r} 9.6 \\ 13 \end{array} \quad \begin{array}{r} 9.7 \\ 9.3 \end{array} \quad \begin{array}{r} 9.5 \\ 13 \end{array} \quad \begin{array}{r} 11.5 \\ 17 \end{array} \quad \begin{array}{r} 11.6 \\ 21 \end{array}$$

$$\begin{array}{r} 9.5 \\ 24 \end{array} \quad \begin{array}{r} 10.9 \\ 21 \end{array} \quad \begin{array}{r} 10.8 \\ 17 \end{array} \quad \begin{array}{r} 9.2 \\ 13 \end{array} \quad \begin{array}{r} 9.2 \\ 8.9 \end{array} \quad \begin{array}{r} 9.1 \\ 13 \end{array} \quad \begin{array}{r} 10.9 \\ 17 \end{array} \quad \begin{array}{r} 11.4 \\ 21 \end{array} \quad \begin{array}{r} 3.0 \\ 34 \end{array}$$

$$\begin{array}{r} 13.5 \\ 24 \end{array} \quad \begin{array}{r} 8.4 \\ 13 \end{array} \quad \begin{array}{r} 8.4 \\ 8.2 \end{array} \quad \begin{array}{r} 8.4 \\ 13 \end{array} \quad \begin{array}{r} 10.4 \\ 17 \end{array} \quad \begin{array}{r} 10.5 \\ 21 \end{array} \quad \begin{array}{r} 6.8 \\ 26 \end{array}$$

$$\begin{array}{r} 14.1 \\ 26 \end{array} \quad \begin{array}{r} 7.7 \\ 13 \end{array} \quad \begin{array}{r} 7.7 \\ 7.8 \end{array} \quad \begin{array}{r} 7.7 \\ 13 \end{array} \quad \begin{array}{r} 9.8 \\ 17 \end{array} \quad \begin{array}{r} 9.8 \\ 21 \end{array} \quad \begin{array}{r} 7.7 \\ 25 \end{array}$$

$$\begin{array}{r} 10.2 \\ 20 \end{array} \quad \begin{array}{r} 6.8 \\ 13 \end{array} \quad \begin{array}{r} 6.8 \\ 6.9 \end{array} \quad \begin{array}{r} 6.8 \\ 13 \end{array} \quad \begin{array}{r} 8.6 \\ 17 \end{array} \quad \begin{array}{r} 8.5 \\ 21 \end{array} \quad \begin{array}{r} 4.2 \\ 28 \end{array}$$

$$\begin{array}{r} 5.4 \\ 24 \end{array} \quad \begin{array}{r} 7.2 \\ 21 \end{array} \quad \begin{array}{r} 7.2 \\ 17 \end{array} \quad \begin{array}{r} 5.5 \\ 13 \end{array} \quad \begin{array}{r} 5.5 \\ 5.5 \end{array} \quad \begin{array}{r} 5.5 \\ 13 \end{array} \quad \begin{array}{r} 7.3 \\ 17 \end{array} \quad \begin{array}{r} 7.3 \\ 21 \end{array} \quad \begin{array}{r} 4.4 \\ 26 \end{array}$$

$$\begin{array}{r} 4.6 \\ 24 \end{array} \quad \begin{array}{r} 6.3 \\ 21 \end{array} \quad \begin{array}{r} 6.4 \\ 17 \end{array} \quad \begin{array}{r} 4.7 \\ 13 \end{array} \quad \begin{array}{r} 4.6 \\ 4.3 \end{array} \quad \begin{array}{r} 4.6 \\ 13 \end{array} \quad \begin{array}{r} 6.7 \\ 17 \end{array} \quad \begin{array}{r} 6.6 \\ 21 \end{array} \quad \begin{array}{r} 4.7 \\ 25 \end{array}$$

$$\begin{array}{r} 6.1 \\ 20 \end{array} \quad \begin{array}{r} 2.7 \\ 13 \end{array} \quad \begin{array}{r} 2.8 \\ 2.7 \end{array} \quad \begin{array}{r} 2.8 \\ 13 \end{array} \quad \begin{array}{r} 5.3 \\ 17 \end{array} \quad \begin{array}{r} 5.4 \\ 21 \end{array} \quad \begin{array}{r} 3.8 \\ 24 \end{array}$$

✓
894.01

23

T.P.

9.76

✓
901.80

-1.97

✓
892.04

19 +00

+30

From Page 25 +24

+70

23 +50

24

+50

T.P.

8.85

✓
908.23

2.42

✓
899.38

25

+50

$$\frac{6.4}{22} \quad \frac{1.8}{13} \quad 1.1 \quad \frac{1.7}{13} \quad \frac{4.0}{16} \quad \frac{4.0}{20} \quad \frac{2.0}{24}$$

$$18.3 \quad \frac{3.1}{40}$$

$$17.9 \quad \frac{1.7}{40}$$

$$17.3 \quad \frac{6.2}{40}$$

$$\frac{11.2}{21} \quad \frac{7.2}{13} \quad 1.2 \quad \frac{7.2}{13} \quad \frac{9.2}{17} \quad \frac{9.2}{20} \quad \frac{5.0}{27}$$

$$\frac{5.3}{23} \quad \frac{6.8}{21} \quad \frac{6.8}{17} \quad \frac{4.9}{13} \quad 4.9 \quad \frac{4.9}{13} \quad \frac{6.7}{17} \quad \frac{6.7}{20} \quad \frac{1.7}{29}$$

$$\frac{1.8}{25} \quad \frac{4.9}{20} \quad \frac{4.9}{17} \quad \frac{2.6}{13} \quad 2.6 \quad \frac{2.6}{13} \quad \frac{4.6}{17} \quad \frac{4.7}{22} \quad \frac{0.3}{28}$$

$$\frac{8.7}{17} \quad \frac{6.7}{13} \quad 6.1 \quad \frac{6.6}{13} \quad \frac{8.6}{17} \quad \frac{8.6}{21} \quad \frac{6.4}{26}$$

$$\frac{4.9}{24} \quad \frac{6.6}{22} \quad \frac{6.6}{17} \quad \frac{4.4}{13} \quad 4.4 \quad \frac{4.4}{13} \quad \frac{6.5}{17} \quad \frac{6.5}{21} \quad \frac{5.4}{22}$$

✓
908.23

25+77

+80

26

B.M.

718

913.85✓

1.56

✓
906.67

906.67

+16

+20

+60

27

+50

28

+50

91385

+75

29

+15

+35

T.P.

4.47

912.57✓

5.75

908.10✓

+70

30

+35

+65

T.P.

13.58

923.82✓

2.33

910.24✓

31

+25

Cold 10°F

29

$$\frac{6.0}{23} \quad \frac{7.5}{21} \quad \frac{7.6}{17} \quad \frac{5.7}{13} \quad \frac{5.8}{5.2} \quad \frac{5.4}{13} \quad \frac{7.2}{17} \quad \frac{7.2}{21} \quad \frac{3.2}{2}$$

$$\frac{8.0}{19} \quad \frac{5.7}{13} \quad \frac{5.8}{5.2} \quad \frac{5.6}{13} \quad \frac{7.5}{17} \quad \frac{7.7}{21} \quad \frac{3.5}{2.4}$$

$$\frac{10.6}{23} \quad \frac{5.7}{13} \quad \frac{5.8}{5.2} \quad \frac{5.6}{13} \quad \frac{7.9}{18} \quad \frac{8.0}{20} \quad \frac{5.9}{2.3}$$

$$\frac{13.7}{30} \quad \frac{5.7}{13} \quad \frac{5.7}{5.2} \quad \frac{5.5}{13} \quad \frac{11.2}{2.4}$$

$$\frac{13.2}{32} \quad \frac{3.8}{13} \quad \frac{4.1}{3.6} \quad \frac{4.0}{13} \quad \frac{14.1}{33}$$

$$\frac{11.0}{28} \quad \frac{3.6}{13} \quad \frac{3.6}{3.2} \quad \frac{3.5}{13} \quad \frac{13.8}{32}$$

$$\frac{7.6}{23} \quad \frac{2.9}{13} \quad \frac{2.8}{2.6} \quad \frac{2.5}{13} \quad \frac{6.5}{20}$$

$$\frac{0.6}{27} \quad \frac{2.8}{21} \quad \frac{3.8}{17} \quad \frac{1.7}{13} \quad \frac{2.0}{1.7} \quad \frac{1.9}{13} \quad \frac{4.0}{17} \quad \frac{4.2}{21} \quad \frac{0.0}{2.7}$$

$$\frac{8.0}{32} \quad \frac{10.6}{27} \quad \frac{14.0}{21} \quad \frac{14.0}{17} \quad \frac{12.0}{13} \quad \frac{12.1}{12.0} \quad \frac{12.0}{13} \quad \frac{14.3}{17} \quad \frac{14.0}{21} \quad \frac{7.2}{31}$$

$$\frac{1.0}{33} \quad \frac{13.1}{21} \quad \frac{13.2}{17} \quad \frac{11.5}{13} \quad \frac{11.4}{11.3} \quad \frac{11.5}{13} \quad \frac{13.4}{17} \quad \frac{13.4}{21} \quad \frac{5.8}{33}$$

Station + H.I. - Elev.

923.82

+75

32

+50

33

+50

T.F.

1.63

914.88

10.57

913.25

913.20

34

+50

35

+50

B.M.

4.22

910.66

910.69

LEFT & RIGHT.

$\frac{28}{33}$	$\frac{120}{21}$	$\frac{120}{17}$	$\frac{100}{13}$	$\frac{100}{100}$	$\frac{100}{13}$	$\frac{11.7}{17}$	$\frac{11.9}{21}$	$\frac{4.1}{33}$
-----------------	------------------	------------------	------------------	-------------------	------------------	-------------------	-------------------	------------------

$\frac{4.7}{31}$	$\frac{11.4}{21}$	$\frac{11.5}{17}$	$\frac{9.5}{13}$	$\frac{9.5}{9.5}$	$\frac{9.7}{13}$	$\frac{11.2}{17}$	$\frac{11.5}{21}$	$\frac{4.3}{32}$
------------------	-------------------	-------------------	------------------	-------------------	------------------	-------------------	-------------------	------------------

$\frac{10.4}{22}$	$\frac{11.1}{21}$	$\frac{11.1}{17}$	$\frac{9.0}{13}$	$\frac{9.0}{9.0}$	$\frac{9.2}{13}$	$\frac{10.8}{17}$	$\frac{10.9}{21}$	$\frac{6.6}{28}$
-------------------	-------------------	-------------------	------------------	-------------------	------------------	-------------------	-------------------	------------------

$\frac{12.5}{20}$	$\frac{9.5}{13}$	$\frac{9.5}{9.5}$	$\frac{9.5}{13}$	$\frac{11.5}{17}$	$\frac{11.6}{21}$	$\frac{6.0}{26}$
-------------------	------------------	-------------------	------------------	-------------------	-------------------	------------------

$\frac{13.0}{18}$	$\frac{10.7}{13}$	$\frac{10.7}{10.6}$	$\frac{10.7}{13}$	$\frac{12.6}{17}$	$\frac{12.6}{21}$	$\frac{9.6}{26}$
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Top Blue Top Lt Sta. 33+50

$\frac{4.4}{23}$	$\frac{4.8}{21}$	$\frac{4.6}{17}$	$\frac{2.6}{13}$	$\frac{2.6}{2.7}$	$\frac{3.0}{13}$	$\frac{4.9}{17}$	$\frac{4.9}{21}$	$\frac{2.2}{25}$
------------------	------------------	------------------	------------------	-------------------	------------------	------------------	------------------	------------------

$\frac{4.2}{24}$	$\frac{6.0}{21}$	$\frac{6.0}{17}$	$\frac{4.2}{13}$	$\frac{4.2}{4.1}$	$\frac{6.2}{13}$	$\frac{6.4}{17}$	$\frac{3.1}{21}$	$\frac{2.5}{25}$
------------------	------------------	------------------	------------------	-------------------	------------------	------------------	------------------	------------------

$\frac{6.5}{23}$	$\frac{7.6}{21}$	$\frac{7.7}{17}$	$\frac{5.6}{13}$	$\frac{5.6}{5.5}$	$\frac{5.5}{13}$	$\frac{7.7}{17}$	$\frac{7.7}{21}$	$\frac{6.1}{23.5}$
------------------	------------------	------------------	------------------	-------------------	------------------	------------------	------------------	--------------------

$\frac{7.0}{24}$	$\frac{9.0}{21}$	$\frac{8.9}{17}$	$\frac{6.6}{13}$	$\frac{6.6}{6.4}$	$\frac{6.9}{13}$	$\frac{8.9}{17}$	$\frac{8.8}{21}$	$\frac{7.7}{23}$
------------------	------------------	------------------	------------------	-------------------	------------------	------------------	------------------	------------------

Spt in Trip. Elev 60' Lt 35+07

91486

36

+50

TP 8.67 913.72 ✓ 9.83 905.05 ✓

37

+50

38

B.M. 1.09 914.41 ✓ 0.41 913.31 ✓ 913.32

+50

39

+50

40

$$\frac{8.0}{25} \quad \frac{10.4}{21} \quad \frac{10.4}{17} \quad \frac{8.2}{13} \quad \overset{f^v}{7.6} \quad \frac{8.0}{13} \quad \frac{10.5}{18}$$

$$\frac{11.2}{17.5} \quad \frac{9.0}{13} \quad \overset{q^s}{8.9} \quad \frac{9.2}{13} \quad \frac{13.7}{22}$$

$$\frac{13.8}{23} \quad \frac{8.2}{13} \quad \overset{q^s}{8.3} \quad \frac{8.3}{13} \quad \frac{15.2}{24}$$

$$\frac{15.8}{27} \quad \frac{8.7}{13} \quad \overset{q^s}{8.8} \quad \frac{9.5}{13} \quad \frac{13.5}{21}$$

$$\frac{15.1}{24} \quad \frac{8.5}{13} \quad \overset{q^s}{8.9} \quad \frac{9.4}{13} \quad \frac{14.5}{23}$$

Spt. 11 12" Oak 50' Lt. 39+90.

$$\frac{15.2}{26} \quad \frac{8.5}{13} \quad \overset{q^s}{9.2} \quad \frac{10.0}{13} \quad \frac{10.7}{16} \quad \frac{15.3}{25}$$

$$\frac{14.5}{25} \quad \frac{7.5}{13} \quad \overset{q^s}{7.8} \quad \frac{9.2}{16} \quad \frac{9.8}{20} \quad \frac{14.8}{29}$$

$$\frac{14.4}{30} \quad \frac{5.6}{13} \quad \overset{q^s}{6.3} \quad \frac{7.7}{14} \quad \frac{8.1}{17} \quad \frac{13.6}{28}$$

$$\frac{24}{26} \quad \frac{5.7}{21} \quad \frac{5.8}{17} \quad \frac{3.7}{13} \quad \overset{q^s}{4.8} \quad \frac{5.9}{16} \quad \frac{7.8}{20} \quad \frac{7.8}{24} \quad \frac{7.3}{27}$$

914.41

40+50

+80

T.P. 9.53 923.59 ✓ 0.35 914.06 ✓

40+50

+80

41

+20

+50

42

+50

T.P. 13.59 936.88 ✓ 0.30 923.29 ✓

12/18/34

$$\begin{array}{r} 39 \\ 21 \end{array} \quad \begin{array}{r} 3.9 \\ 17 \end{array} \quad \begin{array}{r} 2.2 \\ 13 \end{array} \quad \begin{array}{r} 2.7 \\ 28 \end{array} \quad \begin{array}{r} 3.6 \\ 14 \end{array} \quad \begin{array}{r} 5.4 \\ 17 \end{array} \quad \begin{array}{r} 5.5 \\ 21 \end{array}$$

$$\begin{array}{r} 2.6 \\ 21 \end{array} \quad \begin{array}{r} 2.7 \\ 17 \end{array} \quad \begin{array}{r} 0.9 \\ 13 \end{array} \quad \begin{array}{r} 1.5 \\ 14 \end{array} \quad \begin{array}{r} 1.8 \\ 13 \end{array} \quad \begin{array}{r} 3.8 \\ 17 \end{array} \quad \begin{array}{r} 3.8 \\ 21 \end{array}$$

$$\begin{array}{r} 11.9 \\ 33 \end{array}$$

$$\begin{array}{r} 5.3 \\ 33 \end{array}$$

$$\begin{array}{r} 10.7 \\ 33 \end{array}$$

$$\begin{array}{r} 1.3 \\ 33 \end{array}$$

$$\begin{array}{r} 11.4 \\ 21 \end{array} \quad \begin{array}{r} 11.5 \\ 17 \end{array} \quad \begin{array}{r} 9.5 \\ 13 \end{array} \quad \begin{array}{r} 9.9 \\ 28 \end{array} \quad \begin{array}{r} 10.3 \\ 13 \end{array} \quad \begin{array}{r} 12.3 \\ 17 \end{array} \quad \begin{array}{r} 12.1 \\ 21 \end{array} \quad \begin{array}{r} 1.6 \\ 33 \end{array}$$

$$\begin{array}{r} 10.9 \\ 21 \end{array} \quad \begin{array}{r} 11.0 \\ 17 \end{array} \quad \begin{array}{r} 9.0 \\ 13 \end{array} \quad \begin{array}{r} 9.2 \\ 8.9 \end{array} \quad \begin{array}{r} 9.7 \\ 13 \end{array} \quad \begin{array}{r} 11.8 \\ 17 \end{array} \quad \begin{array}{r} 11.7 \\ 21 \end{array} \quad \begin{array}{r} 4.0 \\ 30 \end{array}$$

$$\begin{array}{r} 10.0 \\ 21 \end{array} \quad \begin{array}{r} 10.0 \\ 17 \end{array} \quad \begin{array}{r} 8.1 \\ 13 \end{array} \quad \begin{array}{r} 8.3 \\ 8.0 \end{array} \quad \begin{array}{r} 8.4 \\ 13 \end{array} \quad \begin{array}{r} 10.8 \\ 17 \end{array} \quad \begin{array}{r} 10.8 \\ 21 \end{array} \quad \begin{array}{r} 7.5 \\ 26 \end{array}$$

$$\begin{array}{r} 9.5 \\ 21 \end{array} \quad \begin{array}{r} 9.3 \\ 17 \end{array} \quad \begin{array}{r} 7.2 \\ 13 \end{array} \quad \begin{array}{r} 7.1 \\ 7.2 \end{array} \quad \begin{array}{r} 7.3 \\ 13 \end{array} \quad \begin{array}{r} 9.1 \\ 17 \end{array} \quad \begin{array}{r} 9.0 \\ 21 \end{array}$$

$$\begin{array}{r} 0.5 \\ 32 \end{array} \quad \begin{array}{r} 8.7 \\ 21 \end{array} \quad \begin{array}{r} 8.7 \\ 17 \end{array} \quad \begin{array}{r} 6.1 \\ 13 \end{array} \quad \begin{array}{r} 6.4 \\ 6.2 \end{array} \quad \begin{array}{r} 6.5 \\ 13 \end{array} \quad \begin{array}{r} 12.7 \\ 25 \end{array}$$

93688

40+50

+80

41

+20

+50

42

T.P.

0.29923.58¹ 1359 923.29¹

43

+50

44

+50

$$\frac{63}{42}$$

$$25.2$$

$$\frac{0.4}{50}$$

$$24.0$$

$$\frac{+0.6 \text{ over H.I.}}{49} \quad 23.2$$

$$\frac{+0.6}{48}$$

$$22.5$$

$$\frac{2.0}{45}$$

$$21.6$$

$$\frac{7.6}{37}$$

$$20.4$$

$$\frac{51}{26} \quad \frac{81}{21} \quad \frac{83}{17} \quad \frac{63}{13} \quad \frac{62}{58} \quad \frac{63}{13} \quad \frac{130}{26}$$

$$\frac{66}{23} \quad \frac{79}{21} \quad \frac{79}{17} \quad \frac{58}{13} \quad \frac{58}{58} \quad \frac{58}{13} \quad \frac{131}{28}$$

$$\frac{69}{2} \quad \frac{74}{21} \quad \frac{75}{18} \quad \frac{51}{13} \quad \frac{51}{50} \quad \frac{49}{19} \quad \frac{132}{28}$$

$$\frac{68}{22} \quad \frac{70}{18} \quad \frac{43}{13} \quad \frac{41}{40} \quad \frac{40}{13} \quad \frac{119}{28}$$

923.58

45

T.P. 8.33 928.52¹ 3.39 920.19¹
+25.

+75

46

B.M. 13.26 936.37¹ 5.42 923.10¹ 923.11¹
+50

47

+50

T.P. 11.64 946.44¹ 1.57 934.80¹

48

+50

T.P. 12.0 957²³ 43²³ 1.21 945²³ 43²³

49

12/18/34 (Last mile boys)

$$\begin{array}{r} 3.7 \\ 24 \end{array} \frac{53}{22} \begin{array}{r} 5.4 \\ 18 \end{array} \frac{3.4}{14} \frac{2.8}{26} \frac{2.7}{13} \frac{10.7}{27}$$

$$\begin{array}{r} 4.5 \\ 30 \end{array} \frac{9.4}{24} \frac{9.3}{20} \frac{7.3}{15} \frac{6.7}{6.5} \frac{6.1}{13} \frac{13.6}{29}$$

$$\begin{array}{r} 1.6 \\ 33 \end{array} \frac{7.7}{25} \frac{7.6}{21} \frac{6.0}{17} \frac{4.7}{4.3} \frac{3.9}{13} \frac{6.2}{19}$$

$$\begin{array}{r} 0.5 \\ 33 \end{array} \frac{6.6}{26} \frac{6.4}{22} \frac{4.1}{18} \frac{3.5}{28} \frac{2.5}{13} \frac{4.0}{17}$$

Spike in 12" B.E. 40 107 46 + 60

$$\begin{array}{r} 6.6 \\ 33 \end{array} \frac{11.4}{27} \frac{11.4}{22} \frac{9.6}{18} \frac{8.5}{7.6} \frac{7.2}{14} \frac{10.6}{20}$$

$$\begin{array}{r} 5.8 \\ 26 \end{array} \frac{7.6}{23} \frac{7.6}{20} \frac{5.1}{15} \frac{4.9}{4.4} \frac{4.0}{13} \frac{10.2}{25}$$

$$\begin{array}{r} 2.5 \\ 22 \end{array} \frac{3.2}{21} \frac{3.1}{18} \frac{1.0}{14} \frac{0.8}{0.2} \frac{0.0}{13} \frac{4.6}{22}$$

$$\begin{array}{r} 8.9 \\ 19 \end{array} \frac{6.0}{13} \frac{6.1}{5.7} \frac{6.0}{13} \frac{8.5}{18}$$

$$\begin{array}{r} 3.7 \\ 19 \end{array} \frac{0.9}{13} \frac{1.1}{0.7} \frac{0.8}{13} \frac{3.2}{17} \frac{3.2}{21} \frac{1.6}{23}$$

$$\begin{array}{r} 2.2 \\ 31 \end{array} \frac{8.5}{21} \frac{8.7}{17} \frac{6.8}{13} \frac{6.9}{6.2} \frac{7.2}{13} \frac{9.8}{18} \frac{8.7}{22} \frac{4.9}{27}$$

²³
957.43

+50

968.88

T.P. 13.23

969.08

1.58

⁶⁵
955.85

49+50

50

+50

T.P. 11.23

¹¹
980.31

0.0

968.88

969.08

50

+50

T.P. 9.45

⁰⁸
988.28

1.48

⁶³
978.83

B.M.

0.49

⁵⁹
987.79

987.67

$$\begin{array}{r} 4.5 \\ 22 \end{array} \quad \begin{array}{r} 4.5 \\ 18 \end{array} \quad \begin{array}{r} 1.6 \\ 13 \end{array} \quad \begin{array}{r} 1.9 \\ 14 \end{array} \quad \begin{array}{r} 2.0 \\ 13 \end{array} \quad \begin{array}{r} 3.9 \\ 17 \end{array} \quad \begin{array}{r} 4.2 \\ 21 \end{array} \quad \begin{array}{r} 1.3 \\ 29 \end{array} \quad \text{over H.}$$

$$\begin{array}{r} 3.2 \\ 39 \end{array} \quad \begin{array}{r} 10.2 \\ 22 \end{array} \quad \begin{array}{r} 10.1 \\ 19 \end{array} \quad \begin{array}{r} 7.9 \\ 13 \end{array} \quad \begin{array}{r} 8.6 \\ 8.2 \end{array} \quad \begin{array}{r} 9.4 \\ 14 \end{array} \quad \begin{array}{r} 11.5 \\ 17 \end{array} \quad \begin{array}{r} 11.4 \\ 21 \end{array}$$

$$\begin{array}{r} 5.2 \\ 22 \end{array} \quad \begin{array}{r} 4.9 \\ 18 \end{array} \quad \begin{array}{r} 2.6 \\ 13 \end{array} \quad \begin{array}{r} 3.6 \\ 2.9 \end{array} \quad \begin{array}{r} 4.7 \\ 15 \end{array} \quad \begin{array}{r} 6.7 \\ 19 \end{array} \quad \begin{array}{r} 6.7 \\ 23 \end{array} \quad \text{—}$$

$$\begin{array}{r} 7.6 \\ 40 \end{array}$$

$$19.8$$

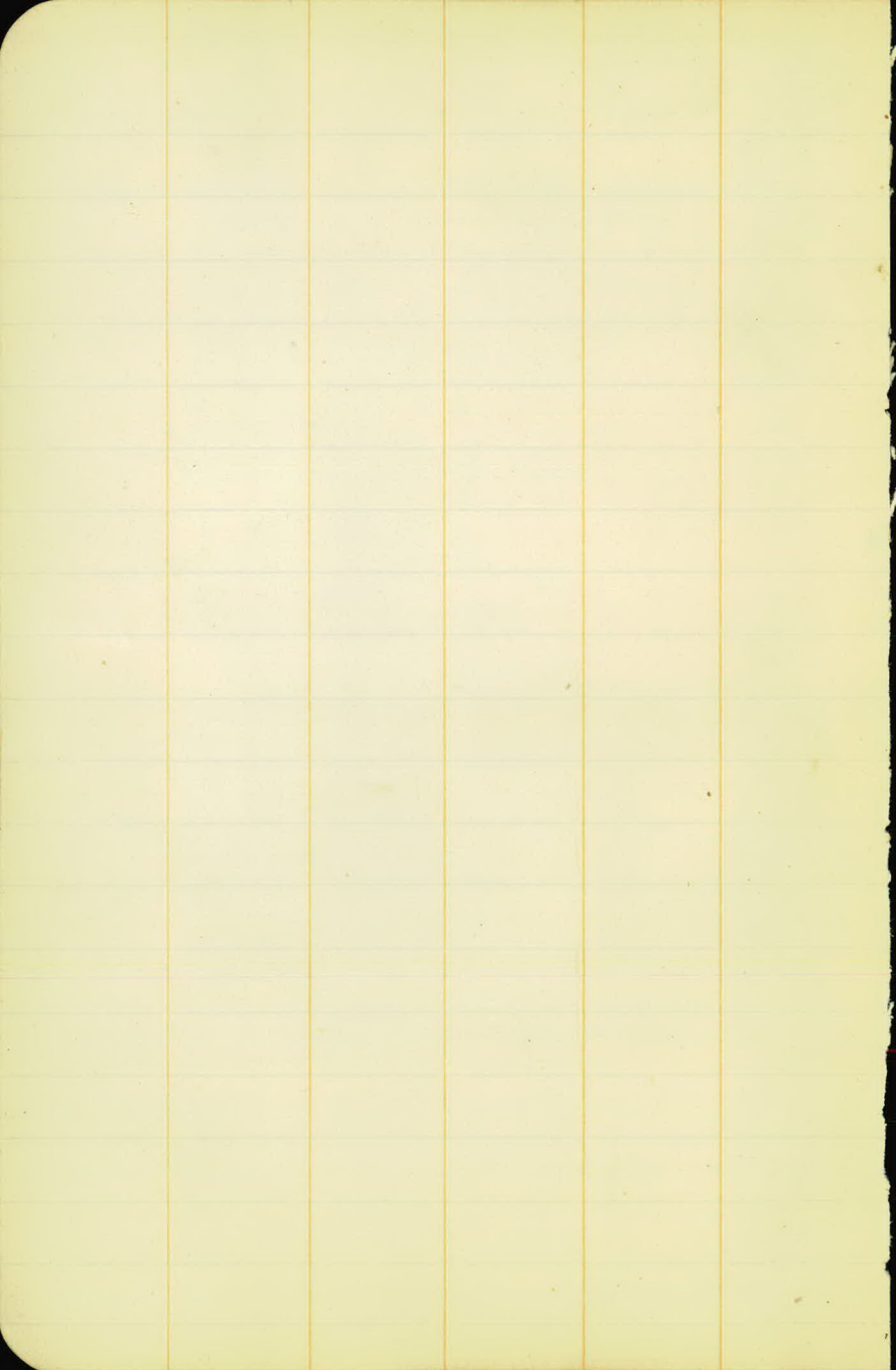
$$\begin{array}{r} 10.3 \\ 40 \end{array}$$

$$\begin{array}{r} 7.5 \\ 33 \end{array}$$

$$14.8$$

$$\begin{array}{r} 4.2 \\ 40 \end{array}$$

spl. in Stump at Floor 300 Lt 53 + 38



Final X-sections
of cut. Sta. 49 to 53
for Wash-Out

Sta.	+ -	π	-	Elev.
	2.54	990.21		987.67
52+50	0.0 Cut	Left.		
52+25				
52+0				
T.P.	408	981.11	13.18	977.03
51+50				
51+0				
50+50				
50+0				
49+50				
T.P.	249	968.28	13.32	967.69

Lt.

E

Rt.

W.H.C.

Anker

Kendrix

July 12,

Heine

1925

Spike in Sap @ F.C.R.

x Denotes natural Ground.

x						
$\frac{9.3}{53}$	$\frac{13.2}{45}$	$\frac{14.0}{31}$	$\frac{13.8}{18.5}$	$\frac{12.4}{14.5}$	$\frac{12.5}{15}$	$\frac{13.4}{15}$

x						
$\frac{7.0}{53}$	$\frac{9.0}{50}$	$\frac{14.4}{41}$	$\frac{15.0}{31}$	$\frac{14.7}{20}$	$\frac{13.0}{16}$	$\frac{13.5}{13.0}$
						$\frac{14.7}{19}$

x					
$\frac{5.3}{58}$	$\frac{7.4}{46}$	$\frac{8.4}{34}$	$\frac{8.3}{19}$	$\frac{6.2}{15}$	$\frac{7.1}{6.5}$
					$\frac{8.1}{20}$

x						
$\frac{9.2}{46}$	$\frac{11.7}{38}$	$\frac{12.2}{18}$	$\frac{10.3}{15}$	$\frac{11.0}{10.6}$	$\frac{11.4}{12}$	$\frac{12.5}{22}$

x
$\frac{7.0}{48}$

15.8

x
$\frac{7.9}{42}$

20.8

x
$\frac{15.0}{42}$

25.4

Sta.	+	π	-	Elev.
		968.28		

50+50 Cont'd

50+0

49+50

T.P.	1.45	956.27	13.46	954.82
------	------	--------	-------	--------

49+0

48+65 = 0.0 EXCAVATION.

T.P.	0.38	963.36	13.29	962.98
------	------	--------	-------	--------

T.P.	2.91	932.78	13.49	929.87
------	------	--------	-------	--------

B.M.			9.64	923.14
------	--	--	------	--------

Lt.

E

Rt.

$$\begin{array}{r}
 00 \\
 37
 \end{array}
 \begin{array}{r}
 3.0 \\
 32
 \end{array}
 \begin{array}{r}
 34 \\
 17
 \end{array}
 \begin{array}{r}
 24 \\
 15
 \end{array}
 \begin{array}{r}
 3.0 \\
 2.4
 \end{array}
 \begin{array}{r}
 29 \\
 8
 \end{array}
 \begin{array}{r}
 3.2 \\
 21
 \end{array}$$

$$\begin{array}{r}
 8.5 \\
 35
 \end{array}
 \begin{array}{r}
 89 \\
 18
 \end{array}
 \begin{array}{r}
 78 \\
 14
 \end{array}
 \begin{array}{r}
 8.0 \\
 7.7
 \end{array}
 \begin{array}{r}
 83 \\
 8
 \end{array}
 \begin{array}{r}
 85 \\
 20
 \end{array}$$

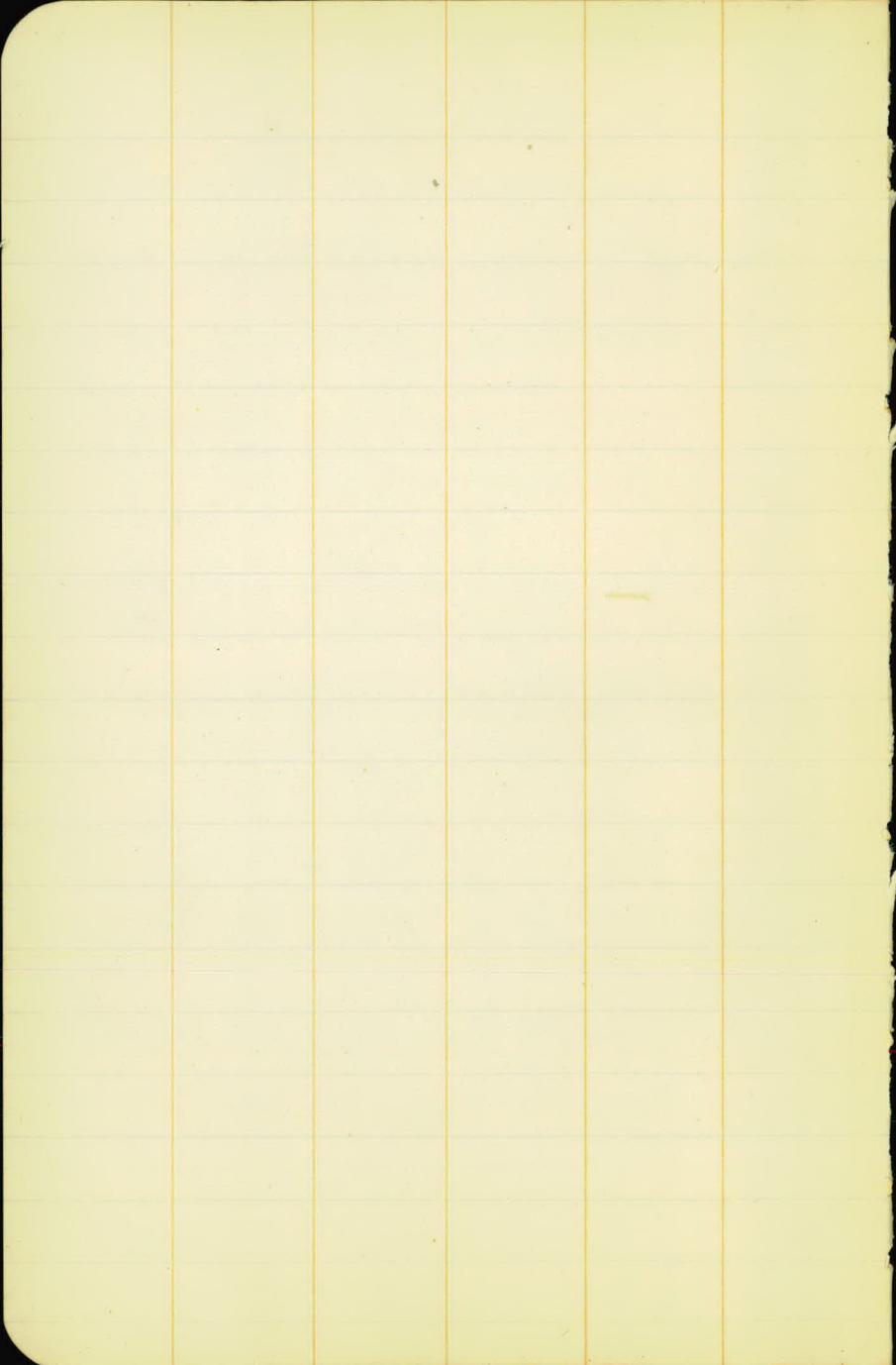
$$\begin{array}{r}
 139 \\
 37
 \end{array}
 \begin{array}{r}
 139 \\
 18
 \end{array}
 \begin{array}{r}
 127 \\
 15
 \end{array}
 \begin{array}{r}
 13.0 \\
 12.5
 \end{array}
 \begin{array}{r}
 13.2 \\
 20
 \end{array}$$

Parotes Matua/or.

$$\begin{array}{r}
 X \\
 0.0 \\
 41
 \end{array}
 \begin{array}{r}
 7.2 \\
 32
 \end{array}
 \begin{array}{r}
 68 \\
 17
 \end{array}
 \begin{array}{r}
 58 \\
 14
 \end{array}
 \begin{array}{r}
 6.0 \\
 5.7
 \end{array}
 \begin{array}{r}
 5.7 \\
 20
 \end{array}$$

O.O EXC.

923.11



B.M.	5.04	864.83	859.79	
0+00			54.1	10.73 ✓
+50			54.9	9.93 ✓
1			56.0	8.83 ✓
+50			57.3	7.53 ✓
2			59.1	5.73 ✓
+50			61.2	3.63 ✓
3			63.4	1.43 ✓
+50		877.07	65.3	11.77 ✓
4			67.0	10.07 ✓
+50			68.4	8.67 ✓
5			69.5	7.57 ✓
+50			70.5	6.57 ✓
6			71.3	5.77 ✓
+50			72.1	4.97 ✓
7			72.9	4.17 ✓
+50			73.7	3.37 ✓
8			74.5	2.57 ✓
+50			75.3	1.77 ✓

859.79

5.04

864.83

1.45

863.38

13.69

877.07

877.07

9 76.1 0.97✓

+50 884.91 76.9 0.17✓

10 77.7 7.21✓

+50 78.5 4.41✓

11 79.2 5.71✓

+50 79.8 5.11✓

12 80.1 4.81✓

+50 80.4 4.51✓

13 80.4 4.51✓

+50 80.3 4.61✓

14 80.1 4.81✓

+50 79.9 5.01✓

15 79.7 7.08✓

+50 79.6 7.18✓

16 79.8 6.98✓

+50 80.1 6.68✓

17 80.7 6.08✓

+50 81.4 5.38✓

$$\begin{array}{r} 884.91 \\ 1.67 \\ \hline \text{B.M. } 883.24 \end{array}$$
$$\begin{array}{r} 887.07 \\ .17 \\ \hline 886.90 \\ 8.01 \\ \hline 884.91 \end{array}$$
$$\begin{array}{r} 879.90 \\ 6.88 \\ \hline 886.78 \end{array}$$

886.78

18			82.1	4.68 ✓
+50			82.8	3.98 ✓
19			83.5	3.28 ✓
+50			84.2	2.58 ✓
20			84.9	1.88 ✓
+50			85.6	1.18 ✓
21			86.3	0.48 ✓
+50	898.23		87.2	11.03 ✓
22			88.5	9.73 ✓
+50			90.2	8.03 ✓
23			92.3	5.93 ✓
+50			94.6	3.63 ✓
24			96.9	1.33 ✓
+50	907.44		99.2	8.24 ✓
25			01.5	5.94 ✓
+50			03.8	3.64 ✓
26	912.39		06.0	6.39
+50			07.6	4.79 ✓

886.78

.48

886.30

11.93

898.23

1.33

896.90

10.54

907.44

0.77

906.67

5.72

912.39

912.39

27 08.6 3.79 ✓

+50 08.9 3.49 ✓

28 08.6 3.79 ✓

+50 08.2 4.19 ✓

29 08.1 4.29 ✓

+50 08.3 4.09 ✓

30 09.0 3.39 ✓

+50 10.2 2.19 ✓

31 11.7 0.69 ✓

+50 917.58 13.1 4.48 ✓

32 14.2 3.38 ✓

+50 14.5 3.08 ✓

33 14.3 3.28 ✓

+50 13.2 4.38 ✓

34 11.9 5.68 ✓

+50 10.6 6.98 ✓

35 09.3 8.28 ✓

+50 08.0 9.58 ✓

$$\begin{array}{r} 910.69 \\ 1.11 \\ \hline 911.80 \end{array}$$

$$\begin{array}{r} 912.39 \\ 0.69 \\ \hline 911.70 \\ 5.88 \\ \hline 917.58 \\ 6.90 \\ \hline 910.68 \text{ B.M.} \end{array}$$

9/11.80

36			06.7	5.1 ✓
+50			05.4	6.4 ✓
37		Super. 0.2	09.4	7.4
+50		0.4	03.9	7.9
38	Widen 0.0	0.6	04.0	7.8
+50			04.7	
39			05.9	
+50			07.6	
40			09.7	
+50			11.7	
41			13.7	
+50			15.3	
42			16.5	
+50			17.2	
43			17.4	
+50			17.8	
44			18.5	
+50			19.5	

7.2 ✓ 7.6 ✓

7.5 ✓ 8.3 ✓

7.2 ✓ 8.4 ✓

45

20.8

	5.20	83.70		78.50	
--	------	-------	--	-------	--

13+76	24" X 42' C.M.			75.7	8.0
-------	----------------	--	--	------	-----

B.M.	1.97	896.22		894.25	
------	------	--------	--	--------	--

T.P.	0.06	883.38	12.90	883.32	
------	------	--------	-------	--------	--

T.P.	4.19	874.54	13.03	870.35	
------	------	--------	-------	--------	--

E. End	Culv.			868.90	5.64
--------	-------	--	--	--------	------

W. "	"			866.90	7.64
------	---	--	--	--------	------

Down 1' Lt. & Rt. 10' O.S.

Spk. in 15" Oak 30' Rt. 7+70 On Deebach Rd.

Top of Rock

894.25

34979

49721

50278

94381

05612

 234977

74326

12345

87654

54321

45678

 274324

$$24865 = 25$$

$$\begin{array}{r} 25 \\ \hline 24840 = 10 \end{array}$$

$$24684 = 24$$

$$\begin{array}{r} 24 \\ \hline 24680 = 12 \end{array}$$

$$76431 = 21$$

$$\begin{array}{r} 21 \\ \hline \end{array}$$

$$78410 = 12$$

$$94147 = 25$$

$$25$$

$$74820 = 18$$

$$17$$

102.4

1030

1000

100.0

99.0

98

99.0

98.2

97

96

12.1.

10600

Grd.

6.0 1

7.0 2

8.0 3

9.0 4

10.0 5

12.6 - 2.4

3.0 40

6.0 20

$$\begin{array}{r} 912.28 \\ 3 \\ \hline 709.18 \end{array}$$

$$\begin{array}{r} 15.59 \\ 09.18 \\ \hline 6.41 \end{array}$$

$$\begin{array}{r} 6.51 \\ 8.16 \\ \hline \end{array}$$

$$6.41 \quad 6.76 - 7.31 - 8.16$$

$$\begin{array}{r} 15.59 \\ 912.28 \\ \hline 5.31 \end{array}$$

$$\begin{array}{r} 8M. \quad 933.29 \\ + 13.5 \quad 5.28 \\ \hline 938.57 \quad H.H. \\ - 13. \quad 4.50 \\ \hline 934.07 \end{array}$$

$$\begin{array}{r} 934.07 \\ 6.51 \\ \hline 927.56 \end{array}$$

5.48

934.07

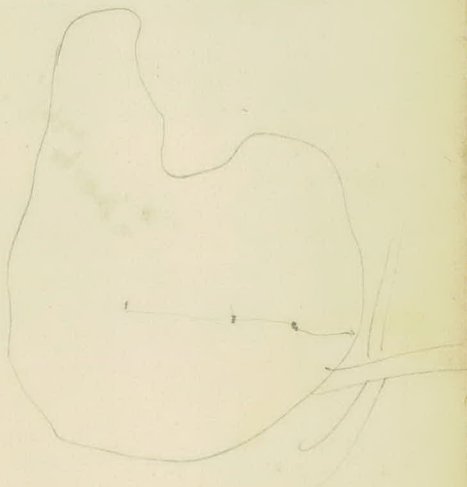


TABLE IX.—CALCULATION OF EARTHWORK.

Width	HEIGHT														
	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15
1	.02	.04	.06	.07	.09	.11	.13	.15	.17	.18	.20	.22	.24	.26	.28
2	.04	.07	.11	.15	.18	.22	.26	.30	.33	.37	.41	.44	.48	.52	.56
3	.06	.11	.17	.22	.28	.33	.39	.44	.50	.56	.61	.67	.72	.78	.83
4	.07	.15	.22	.30	.37	.44	.52	.59	.67	.74	.81	.89	.96	1.04	1.11
5	.09	.19	.28	.37	.46	.56	.65	.74	.83	.93	1.02	1.11	1.20	1.30	1.39
6	.11	.22	.33	.44	.56	.67	.78	.89	1.00	1.11	1.22	1.33	1.44	1.55	1.67
7	.13	.26	.39	.52	.65	.78	.91	1.04	1.16	1.30	1.42	1.55	1.68	1.81	1.94
8	.15	.30	.44	.59	.74	.89	1.04	1.19	1.33	1.48	1.63	1.78	1.92	2.08	2.22
9	.17	.33	.50	.67	.83	1.00	1.17	1.33	1.50	1.67	1.83	2.00	2.17	2.33	2.50
10	.18	.37	.56	.74	.93	1.11	1.30	1.48	1.67	1.85	2.04	2.22	2.41	2.59	2.78
11	.20	.41	.61	.82	1.02	1.22	1.43	1.63	1.83	2.04	2.24	2.44	2.65	2.85	3.06
12	.22	.44	.67	.89	1.11	1.33	1.56	1.78	2.00	2.22	2.44	2.67	2.89	3.11	3.33
13	.24	.48	.72	.96	1.20	1.44	1.68	1.92	2.16	2.41	2.65	2.89	3.13	3.37	3.61
14	.26	.52	.78	1.04	1.30	1.55	1.81	2.08	2.33	2.59	2.85	3.11	3.37	3.63	3.89
15	.28	.56	.83	1.11	1.39	1.67	1.94	2.22	2.50	2.78	3.06	3.33	3.61	3.89	4.17
16	.30	.59	.89	1.18	1.48	1.78	2.07	2.37	2.67	2.96	3.26	3.56	3.85	4.15	4.44
17	.31	.63	.94	1.26	1.57	1.89	2.20	2.52	2.83	3.15	3.46	3.78	4.09	4.41	4.72
18	.33	.67	1.00	1.33	1.67	2.00	2.33	2.67	3.00	3.33	3.67	4.00	4.33	4.67	5.00
19	.35	.70	1.06	1.41	1.76	2.11	2.46	2.82	3.17	3.52	3.87	4.22	4.57	4.92	5.28
20	.37	.74	1.11	1.48	1.85	2.22	2.59	2.96	3.33	3.70	4.07	4.44	4.81	5.18	5.56
21	.39	.78	1.17	1.55	1.94	2.33	2.72	3.11	3.50	3.89	4.28	4.67	5.06	5.44	5.83
22	.41	.81	1.22	1.63	2.04	2.44	2.85	3.26	3.67	4.07	4.48	4.89	5.30	5.70	6.11
23	.43	.85	1.28	1.70	2.13	2.56	2.98	3.41	3.83	4.26	4.68	5.11	5.54	5.96	6.39
24	.44	.89	1.33	1.78	2.22	2.67	3.11	3.56	4.00	4.44	4.89	5.33	5.78	6.22	6.67
25	.46	.92	1.39	1.85	2.31	2.78	3.24	3.70	4.17	4.63	5.09	5.56	6.02	6.48	6.94
26	.48	.96	1.44	1.92	2.41	2.89	3.37	3.85	4.33	4.82	5.30	5.78	6.26	6.74	7.24
27	.50	1.00	1.50	2.00	2.50	3.00	3.50	4.00	4.50	5.00	5.50	6.00	6.50	7.00	7.50
28	.52	1.04	1.55	2.07	2.59	3.11	3.63	4.15	4.67	5.18	5.70	6.22	6.74	7.26	7.78
29	.54	1.07	1.61	2.15	2.68	3.22	3.76	4.30	4.83	5.37	5.91	6.44	6.98	7.52	8.06
30	.56	1.11	1.67	2.22	2.78	3.33	3.89	4.44	5.00	5.55	6.11	6.67	7.22	7.78	8.33
31	.57	1.15	1.72	2.30	2.87	3.44	4.02	4.59	5.17	5.74	6.32	6.89	7.46	8.04	8.61
32	.59	1.18	1.78	2.37	2.96	3.56	4.15	4.74	5.33	5.92	6.52	7.11	7.70	8.30	8.89
33	.61	1.22	1.83	2.44	3.05	3.67	4.28	4.89	5.50	6.11	6.72	7.33	7.94	8.55	9.17
34	.63	1.26	1.89	2.52	3.15	3.78	4.40	5.04	5.67	6.29	6.93	7.56	8.18	8.81	9.44
35	.65	1.30	1.94	2.59	3.24	3.89	4.53	5.18	5.83	6.48	7.13	7.78	8.42	9.08	9.72
36	.67	1.33	2.00	2.67	3.33	4.00	4.66	5.33	6.00	6.67	7.33	8.00	8.67	9.33	10.00
37	.68	1.37	2.06	2.74	3.42	4.11	4.79	5.48	6.17	6.85	7.54	8.22	8.91	9.59	10.28
38	.70	1.41	2.11	2.82	3.52	4.22	4.92	5.63	6.33	7.03	7.74	8.44	9.15	9.85	10.56
39	.72	1.44	2.17	2.89	3.61	4.33	5.05	5.78	6.50	7.22	7.95	8.67	9.39	10.11	10.83
40	.74	1.48	2.22	2.96	3.70	4.44	5.18	5.92	6.67	7.41	8.15	8.89	9.63	10.37	11.11

Table gives cu. yds. in 1 ft. of a triangle of given width and height. Corrections for tenths of width are one tenth the values found under each height considering the widths from 1 to 9 as tenths and similarly the corrections for tenths of height are one tenth the figures opposite width considering the heights from 1 to 9 as tenths. Thus if $w = 16.2$ and $h = 5.3$, cu. yds. $= 1.48 + .028 + .089 = 1.597$ cu. yds. or practically 160 cu. yds. per 100 ft. If w exceeds 40 ft., use one half and multiply result by 2, if both w and h are large use one half of each and multiply result by 4. Any cross-section may be divided into triangles by the following rule. To the triangle of the sum of the outside cuts (or fills) $= h$, and $\frac{1}{2}$ the roadbed $= w$, add the triangles formed by taking the distance out to each break in turn ($= w$'s) by the difference between the cuts (or fills) on each side of it ($= h$'s) always subtracting the outer from the inner.

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.

Roadway 16 feet wide. Side Slopes 1 on 1½.
For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.2	8.3	8.5	8.6	8.8	8.9	9.1	9.2	9.4	0
1	9.5	9.7	9.8	10.0	10.1	10.3	10.4	10.6	10.7	10.9	1
2	11.0	11.2	11.3	11.5	11.6	11.8	11.9	12.1	12.2	12.4	2
3	12.5	12.7	12.8	13.0	13.1	13.3	13.4	13.6	13.7	13.9	3
4	14.0	14.2	14.3	14.5	14.6	14.8	14.9	15.1	15.2	15.4	4
5	15.5	15.7	15.8	16.0	16.1	16.3	16.4	16.6	16.7	16.9	5
6	17.0	17.2	17.3	17.5	17.6	17.8	17.9	18.1	18.2	18.4	6
7	18.5	18.7	18.8	19.0	19.1	19.3	19.4	19.6	19.7	19.9	7
8	20.0	20.2	20.3	20.5	20.6	20.8	20.9	21.1	21.2	21.4	8
9	21.5	21.7	21.8	22.0	22.1	22.3	22.4	22.6	22.7	22.9	9
10	23.0	23.2	23.3	23.5	23.6	23.8	23.9	24.1	24.2	24.4	10
11	24.5	24.7	24.8	25.0	25.1	25.3	25.4	25.6	25.7	25.9	11
12	26.0	26.2	26.3	26.5	26.6	26.8	26.9	27.1	27.2	27.4	12
13	27.5	27.7	27.8	28.0	28.1	28.3	28.4	28.6	28.7	28.9	13
14	29.0	29.2	29.3	29.5	29.6	29.8	29.9	30.1	30.2	30.4	14
15	30.5	30.7	30.8	31.0	31.1	31.3	31.4	31.6	31.7	31.9	15
16	32.0	32.2	32.3	32.5	32.6	32.8	32.9	33.1	33.2	33.4	16
17	33.5	33.7	33.8	34.0	34.1	34.3	34.4	34.6	34.7	34.9	17
18	35.0	35.2	35.3	35.5	35.6	35.8	35.9	36.1	36.2	36.4	18
19	36.5	36.7	36.8	37.0	37.1	37.3	37.4	37.6	37.7	37.9	19
20	38.0	38.2	38.3	38.5	38.6	38.8	38.9	39.1	39.2	39.4	20
21	39.5	39.7	39.8	40.0	40.1	40.3	40.4	40.6	40.7	40.9	21
22	41.0	41.2	41.3	41.5	41.6	41.8	41.9	42.1	42.2	42.4	22
23	42.5	42.7	42.8	43.0	43.1	43.3	43.4	43.6	43.7	43.9	23
24	44.0	44.2	44.3	44.5	44.6	44.8	44.9	45.1	45.2	45.4	24
25	45.5	45.7	45.8	46.0	46.1	46.3	46.4	46.6	46.7	46.9	25
26	47.0	47.2	47.3	47.5	47.6	47.8	47.9	48.1	48.2	48.4	26
27	48.5	48.7	48.8	49.0	49.1	49.3	49.4	49.6	49.7	49.9	27
28	50.0	50.2	50.3	50.5	50.6	50.8	50.9	51.1	51.2	51.4	28
29	51.5	51.7	51.8	52.0	52.1	52.3	52.4	52.6	52.7	52.9	29
30	53.0	53.2	53.3	53.5	53.6	53.8	53.9	54.1	54.2	54.4	30
31	54.5	54.7	54.8	55.0	55.1	55.3	55.4	55.6	55.7	55.9	31
32	56.0	56.2	56.3	56.5	56.6	56.8	56.9	57.1	57.2	57.4	32
33	57.5	57.7	57.8	58.0	58.1	58.3	58.4	58.6	58.7	58.9	33
34	59.0	59.2	59.3	59.5	59.6	59.8	59.9	60.1	60.2	60.4	34
35	60.5	60.7	60.8	61.0	61.1	61.3	61.4	61.6	61.7	61.9	35
36	62.0	62.2	62.3	62.5	62.6	62.8	62.9	63.1	63.2	63.4	36
37	63.5	63.7	63.8	64.0	64.1	64.3	64.4	64.6	64.7	64.9	37
38	65.0	65.2	65.3	65.5	65.6	65.8	65.9	66.1	66.2	66.4	38
39	66.5	66.7	66.8	67.0	67.1	67.3	67.4	67.6	67.7	67.9	39
40	68.0	68.2	68.3	68.5	68.6	68.8	68.9	69.1	69.2	69.4	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 41.9. For same slopes but other widths of roadbed correct above figures by one-half difference in width of roadbed; thus in example above for 20 ft. roadbed distance will be $41.9 + (20 - 16) \div 2$ or 2 ft. added to 41.9 = 43.9. For slopes of 1 on 1 see inside of front cover.