

Bk. 61 Dr. 12A

OFFICE OF COUNTY ENGINEER
RAMSEY CO. MINN.

Stadia.....Survey

Wakefield Lake

X-Sec. Ball Field 1930

From West Traverse Co. 1949

Road Acc't. No.

Date Filed 6-13-49

File

Wakefield Lake

Lake elevations

June 21 - July 7 "49"

GB

AM

MB

BC.

Date Lake elev.

June 21 - 882.60

June 28 - 882.46

June 30 - 882.41

July 5 - 882.21

July 7 - 882.17

July 18 881.93

July 22 881.78

July 29 882.21

Aug 9 881.99

DIST.

VERT
ANGLE

ROD
LOU

Stadia Survey

Wakefield Lake

5-24-48

GB

AM

MB

Rec 5-25-49

Completed Survey 5-27-49
C.B.

17.15
3.22
78

OBJECT

AZ

STADI

π @ Ctr. Sec 15		
To SE ^{5/4} cor. Sec 15	(From Dr. 12 A Bk 41)	180°00'
BM To Spk in Arc LTP SE cor Frost & Prosp.		
To Pt #1	T 4.0	151°46' (151°46' per Brown) 152°25'
℄ Frost		270°20'
N Toe		252°40'
T Back Slope		258°42'
"		249°18'
"		237°45'
Fe. cor.		183°30'
		180°00'
		180°00'
℄ Frost		90°22'
Shoulder		97°
Toe S		102°30'
		90°22'
Fe & Toe of slope		78°15'
Shoulder		94°50'
T B. Slope		97°00'
	T 4.0	95°00'
℄ Frost	T 0.2	90°28'
	T 1.3	93°25'
	T 1.20	95°00'
	* 0.7	98°40'

5-24-49

①

DIST.	VERT. ANGLE	ROD EQUIV.	ROD	DIFF.	ELEV.
		$H.I. = 904.70$ ✓	$H.I. = 902.45$		
			5.25		(899.45) ✓
	$+0^{\circ}30'$		1.19		^{0.1} 902.80
7.45 ✓			0.78	903.92	903.92 902.20
92.			5.24		899.46 ✓
100			8.5		96.2 ✓
99			5.68		99.0 ✓
102			7.63		97.1 ✓
60			5.18		99.5 ✓
33			4.55		00.2 ✓
20			5.4		99.3 ✓
28'			8.2		96.5 ✓
185'			4.3		00.4 ✓
180			5.1		99.6 ✓
185			11.0		93.7 ✓
265			2.5		02.2 ✓
300			8.2		96.5 ✓
280'			2.8		01.9 ✓
280			0.3		04.4 ✓
360			+2.2		06.9 ✓
433			+2.0		06.7 ✓
400			+0.7		05.4 ✓
415			+0.9		05.6 ✓
445			+1.5		06.2 ✓

OBJECT

AZI

ST-DIA

T 3.10

95°35'

T/slope Fe Cor.

96°35'

4

T 0.0

116°40'

Shoulder.

T 0.6

116°40'

Toe slope

102°00'

117°35'

107°25'

106°50'

124°20'

105°20'

Fe Cor.

137°26'

Fe Cor

138°30'

Fe Cor.

144°30'

Fe Cor.

144°40'

end Fe

157°05'

115°15'

117°20'

B 11.6

101°27'

J end 34" cone

104°20'

B 11.72

110°07'

B 10.9

134°20'

135°20'

(2)

DIST.	VERT. ANGLE	ROD EQUIV.	ROD	DIFF.	ELEV.
H.I. = 904.70 HI = 907.5					
420			370		
	+ 0°30'				
420	+ 0°50'	+ 3.8	1.1	+ 2.7	07.4 ✓
530			+ 2.65		07.4 ✓
510			+ 2.0		06.7 ✓
430			4.9		99.8 ✓
500			2.40		02.3 ✓
440			7.10		97.6 ✓
440			7.9		96.8 ✓
410			10.8		93.9 ✓
340			3.80		00.9 ✓
410			11.0		93.7 ✓
450			10.2		94.5 ✓
450			11.7		93.0 ✓
400			10.9		93.8 ✓
400			10.7		94.0 ✓
370			5.7		99.0 ✓
280			11.2		93.5 ✓
270			12.9		91.8 ✓
215	- 1°00'	- 3.7	10.87	14.6	901 ✓
175	- 1°00'	- 3.1	12.6	15.7	89.0 ✓
370			12.7		92.0 ✓
370	- 1°00'	- 6.5	7.80	14.3	904 ✓
370	- 1°00'	- 6.5	5.50	12.1	92.6 ✓

OBJECT

AZI

STADIA

Ditch

142°55'

TBS 10/120

144°30'

125°35'

132°40'

156°20'

162°40'

Fe

180°10'

178°25'

169°15'

173°10'

B

11.50

169°00'

B

11.50

176°05'

B

11.00

180°14'

Fe

173°00'

B

11.0

171°00'

168°40'

163°40'

138°10'

143°35'

150°45'

154°20'

159°30'

166°00'

220.35

DIST.	VERT. ANGLE	ROD EQUIV.	ROD	DIFF.	ELEV.
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H.I. = 904.70

~~HI = 907.5~~

3.20	-1°00'	-6.5	9.00	15.5	89.2 ✓
3.70	-1°00'	-6.5	7.6	14.1	90.6 ✓
2.10	-2°00'	-7.4	9.70	17.1	87.6 ✓
1.40	-2°00'	-4.9	6.50	11.4	93.3 ✓
.73	-2°00'	-2.5	5.50	8.0	96.7 ✓
.60			10.0		94.7 ✓
.70			5.5		99.2 ✓
1.60			9.5		95.2 ✓
1.45			9.50		95.2 ✓
2.10			11.0		93.7 ✓
2.30			12.6		92.1 ✓
2.20			12.6		92.1 ✓
2.80			12.9		91.8 ✓
1.90			11.60		93.1 ✓
1.90			11.9		92.8 ✓
1.90			11.30		93.4 ✓
2.00			11.40		93.3 ✓
2.20			12.60		92.1 ✓
2.10	-1°30'	-5.5	10.7	16.2	88.5 ✓
2.75	-1°30'	-7.2	8.9	16.1	88.6 ✓
3.70	-1°30'	-9.7	4.30	14.0	90.7 ✓
4.30			5.60		99.1 ✓
4.40			7.0		97.7 ✓
2.15			10.7		94.0 ✓

OBJECT

AZI

STADIA

209°10'

207°00'

174°20'

201°00'

174°20'

196°40'

F₄

180°00'

194°30'

F₁

180°15'

192°20'

175°30'

190°20'

171°40'

F₂

180°00'

T 1.30

168°20'

+ 0.7

166°20'

161°40'

155°00'

146°40'

142°10'

141°30'

140°00'

137°00'

136°20'

DIST.	VERT. ANGLE	ROD EQUIV.	ROD	DIFF.	LEV.
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H.I: 904.70 H.E: 907.5

310		9.50			952 ✓
380		3.90			00.8 ✓
440		10.1			94.6 ✓
480		7.5			97.2 ✓
520		10.1			94.6 ✓
540		3.60			01.1 ✓
550		9.90			95.7 ✓
6.40		9.70			00.0 ✓
700		4.70			00.0 ✓
740		1.50			03.2 ✓
650		5.0			99.7 ✓
810		5.6			99.1 ✓
710		3.0			01.7 ✓
770		8.40			96.3 ✓
650		1.90			02.8 ✓
560		1.50			03.2 ✓
590		9.70			00.0 ✓
590		8.0			96.7 ✓
510		9.8			94.9 ✓
480		10.5			94.2 ✓
480		11.4			93.3 ✓
480		9.10			95.6 ✓
480		9.30			95.4 ✓
480		7.70			97.0 ✓

OBJECT

AZI

STADIA

127°15'

129°00'

141°20'

140°20'

139°40'

139°10'

138°10'

137°40'

139°10'

130°00'

T/B slope Fe.

129°20'

Shoulder

129°10'

Q

128°20'

Q

123°

Shoulder

123°10'

Fe T/B slope

123°50'

@ PT #1

To ctr sec 15

332°25'

To BM spk in Ark L & P. Frost & Prosperity

11°20'

To pt # 2,

10.20

177°36'

To pt # 3

163°20'

Group 3 20' oak

12.60

326°30'

Group 2 20' oak ← 20' Apart

317°10'

To Hub 2A

197°21½'

DIST.	VERT. ANGLE	ROD EQUIV.	ROD	DIFF.	DIAG.
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$H.I. = 904.70 \pm 4 = 907.3$

470			6.70		98.0 ✓
530			5.30		99.4 ✓
560			5.50		99.2 ✓
570			5.50		99.2 ✓
570			6.30		98.4 ✓
580			5.30		99.4 ✓
570			6.4		98.3 ✓
570			5.3		99.4 ✓
590			4.2		00.4 ✓
610	+0°40'	+ 7.1	3.0	+4.1	08.8 ✓
620'	+0°40'	+ 7.3	4.3	+4.0	08.7 ✓
625'	+0°40'	+ 7.3	3.1	+4.2	08.9 ✓
630'	+0°40'	+ 7.4	2.7	+3.7	08.4 ✓
580'	+0°40'	+ 6.8	2.2	+4.6	09.3 ✓
570'	+0°40'	+ 6.6	2.4	+3.7	08.4 ✓
550'	+0°40'	+ 6.4	5.3	+1.1	05.8 ✓

$H.I. = 909.88$

~~907.40~~
H.I. 5.20

747			10.25		
640'	+0°30'	+ 5.6	7.60		
380 ✓			12.10		
540' ✓			1.91		
333			14.20	95.7 ✓	
320			10.80	99.1 ✓	
389					

904.69

Branch
Lands

897.70

3907.86

OBJECT

AZI

STADIA

GE

309°55'

268°00'

240°10'

224°50'

190°20'

Fe

247°00'

238°00'

246°40'

237°30'

243°00'

270°10'

1°20'

33°20'

Fe Toe of slope

60°30'

Toe Rd. slope Fe T/ditch Bank

94°50'

95°50'

95°50'

222°35'

217°20'

208°30'

194°00'

186°50'

150°46'

STATION	VERT. ANGLE	ROD EQUIV.	ROD	DIFF.	ELEV.
H.I. = 909.88		HI = 907.4			
120			8.86		01.5 ✓
135			7.00		02.9 ✓
165			8.8		01.1 ✓
120			10.75		99.1 ✓
90			7.15		02.7 ✓
390	-1°00'	- 6.8	9.35	16.2	93.7 ✓
440	-1°00'	- 7.7	9.0	16.7	93.2 ✓
295			10.9		99.0 ✓
230			8.30		01.6 ✓
20'			5.5		04.4 ✓
60'			8.4		01.5 ✓
110			7.9		02.0 ✓
125			9.75		00.1 ✓
170			7.70		02.2 ✓
160			10.7		99.2 ✓
85			6.5		03.4 ✓
43			7.40		02.5 ✓
285	-1°00'	- 5.0	9.20	14.2	95.7 ✓
250	-1°00'	- 4.4	9.30	13.7	96.2 ✓
180	-1°00'	- 3.1	10.7	13.8	96.1 ✓
190	-1°00'	- 3.3	10.20	13.5	96.4 ✓
70	-1°00'	- 1.2	6.0	7.2	02.7 ✓
87			8.63		01.3 ✓

OBJECT

AZI

STADIA

Top of Bank	1240 ⁹⁹	99°20'
Top Rd. B Slope	1.1	39°20'
ditch	420 ¹⁰⁵⁰	39°50'
edge of Rd.	275 ¹¹²	41°00'
		42°55'
ctr. inters. Road E		97°05'
Shoal Idem.		98°05'
Toe of slope		119°50'
q Rd.		128°40'
q Rd.		142°10'
Shoal Idem.		130°45'
		144°00'
Toe Slope		131°40'
Toe B Slope		144°35'
Top B. Slope		133°40'
		146°00'
GE		149°40'
"		147°00'
"		159°30'
"		158°00'
"		175°00'
E Bank ditch		104°40'
"		118°00'
Bott. Ditch		143°50'

DIST.	VERT. ANGLE	ROD EQUIV.	ROD	DIFF.	ELEV.
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$$H.I. = 909.88$$

160			13.20		96.7 ✓
220			+ 1.0		10.9 ✓
230			3.0		06.9 ✓
232			1.5		08.4 ✓
240			1.1		08.8 ✓
200			4.0		05.8 ✓
185			4.8		05.1 ✓
215			6.20		03.7 ✓
280			2.90		07.0 ✓
392			2.70		07.2 ✓
270			3.15		06.8 ✓
380			1.90		08.0 ✓
270			4.45		05.5 ✓
375			3.70		06.2 ✓
260			1.9		08.0 ✓
380			2.1		07.8 ✓
215			5.7		04.2 ✓
320			1.6		08.3 ✓
265			5.5		04.4 ✓
310			8.7		01.2 ✓
270			11.3		98.6 ✓
165			11.0		98.9 ✓
155			11.6		98.3 ✓
150	-1°20'	-3.5	7.8	13.3	96.6 ✓

OBJECTION

AZI

STADIA

4' Bottom	W Bank Ditch	142°50'	
4' Bottom	W " "	115°00'	
	Bot ditch	115°45'	✓
	Bottom	142°40'	2
	Top	163°20'	✓
	Top	162°20'	
	Top	163°10'	
6' Bottom	Q Bottom	173°10'	✓
		173°40'	
		174°20'	
		190°45'	
12' Bottom	Q in ditch	191°45'	✓
	L in ditch	200°00'	✓
	T/W Bank	193°00'	
	T/E "	190°20'	
		193°20'	
		188°50'	
		202°40'	
		198°00'	
FL. 30" CM	E end.	81°40'	✓
FL 30" CM	W end	99°13'	✓
FL 12" CM	S end.	15°07'	✓
18" Oak		143°40'	
BM	Frost & Prosp.		

DIST.	VERT. ANGLE	ROD EQUIV.	ROD	DIFF.	ELEV.
$H.I. = 909.88$					
140	-1°20'	-3.3	8.70	12.0	977.9 ✓
140	-1°20'	-3.3	7.30	11.0	989.9 ✓
140	-1°20'	-3.3	12.0	15.3	94.6 ✓
150	-1°20'	-3.5	13.25	16.6	93.3 ✓
173	-3°30'	-10.6	8.10	18.7	91.2 ✓
180	-3°30'	-11.3	5.0	16.3	93.6 ✓
145	-3°30'	-10.1	4.3	14.4	95.5 ✓
210	-3°30'	-12.7	8.2	20.9	89.0 ✓
210	-3°30'	-12.7	4.3	17.0	92.9 ✓
195	-3°30'	-11.9	3.8	15.7	94.2 ✓
245	-3°30'	-15.0	8.4	23.4	86.5 ✓
270	-3°30'	-16.5	8.6	25.1	84.8 ✓
330'	-3°30'	-20.2	5.0	25.2	84.7 ✓
230	-3°30'	-14.0	4.8	18.8	91.1 ✓
250	-3°30'	-15.2	5.35	20.5	89.4 ✓
270	-3°30'	-16.5	3.70	20.2	89.7 ✓
270	-3°19'	-15.6	3.0	18.6	91.3 ✓
323	-3°19'	-18.9	3.6	22.5	87.4 ✓
328'	-3°19'	-19.0	2.7	21.7	88.2 ✓
227			15.6		94.3 ✓
162	-1°08'	-3.2	12.5	157	94.2 ✓
550			9.3		00.6 ✓
216			5.0		04.9 ✓
			1.92		07.96 ✓

OBJECT

AZI

STADIA

DIST

VERT.
ANGLEROD
EQUIV.

ROD

DIFF.

ELEV.

Rec. 5-26-49

$$\begin{array}{r} 535 \\ 140 \\ \hline 395 \\ 395 \\ \hline 790 \end{array}$$

OBJECT

AZ

STADIA

PT @ PT 2A

To PT # 1

17° 21' 1/2 ✓

Lake elev

To PT # 2B

169° 42' ✓ ✓

GE

Lake Shore

177° 20'

"

"

179° 50'

"

"

178° 50'

"

"

179° 05'

Break in B Slope

1.5

168° 10'

" " " "

0.9

167° 30'

Lake Shore

171° 10'

Break in B Slope

1.3

163° 05'

Lake Shore

164° 50'

0.0

156° 50'

0.1

151° 30'

0.5

147° 20'

Lake Shore

155° 40'

"

152° 00'

"

151° 30'

GE

4.6

147° 40'

144° 50'

141° 40'

Lake Shore

155° 50'

5-25-49

GR
AM
MB

10

DIST.	VERT. ANGLE	ROD EQUIV.
-------	----------------	---------------

HI = 890.15

HI, 5.00

Bench Level

387 ✓

885.15

6.81

883.34 ✓

790 ✓

1.39

888.76 ✓

840'

6.8

83.4 ✓

785'

6.8

83.4 ✓

785'

6.8

83.4 ✓

750'

6.8

83.4 ✓

740'

+2.2

92.4 ✓

710

+2.6

92.8 ✓

635

6.8

83.4 ✓

625'

+1.8

92.0 ✓

550

6.8

83.4 ✓

550'

+2.7

92.9 ✓

500'

+2.4

92.6 ✓

470'

+1.9

92.1 ✓

450'

6.8

83.4 ✓

385'

6.8

83.4 ✓

340'

6.8

83.4 ✓

320'

3.0

87.2 ✓

270'

+1°

+4.7

3.3

+1.4

91.6 ✓

205'

+1°

+3.6

1.7

+1.9

92.1 ✓

255'

6.8

83.4 ✓

OBJECT

AZ

STADIA

@ A # 2 A

GE

Lake Shore

157°00'

"

" "

148°40'

"

125°50'

"

82°50'

60°50'

Lake Shore

145°50'

E side ^{4'} Ditch Ent

264°30'

D Ditch Ent.

264°30'

W side " "

269°30'

Lake Shore

269°30'

338°30'

315°20'

Lake Shore

295°10'

" "

291°50'

Fe

1/2

" "

287°20'

302°20'

To P4 # 3

119°03' ✓

To PT # 1

AZ Check

17°21 1/2' ✓

@ A # 3

To A # 1

343°20 1/2' ✓

To A # 2 A

299°03' ✓

check AZ T/Water Tank

280°08 1/2'

To A # 4

185°59' ✓

(11)

VERT.
ANGLEROD
EQUIV.

ROD

DIFF.

ELEV.

HI = 890.15

178'			6.8		83.4 ✓
105'			6.8		83.4 ✓
135'	+100'	+ 2.4	0.6	+ 1.8	92.0 ✓
95'	+200'	+ 3.3	0.6	+ 2.7	92.9 ✓
65'	+200'	+ 2.3	8.3	- 1.0	89.2 ✓
70'			6.8		83.4 ✓
30'			6.2		84.0 ✓
33'			7.0		83.2 ✓
35'			6.3		83.9 ✓
50'			6.8		83.4 ✓
110'			1.3		88.9 ✓
190			0.7		89.5 ✓
130'			6.8		83.4 ✓
190'			6.8		83.4 ✓
250'			6.8		83.4 ✓
290'			1.1		89.1 ✓
310' ✓					#3 907.86
3.87'					

HI = 912.98
5.11

540'			8.30		907.87 907.97 Bench Level. 904.68
310'					

858'

4.52

908.46

OBJECT

AZ

STADT

④ A #3

To Turn P.#1

GE E Prospect y 41°00'

" Shoulder 37°40'

" Fr & Toe/slope 31°45'

" FL 12"cm W end 11.60 20°40' ✓

" " E end 39°35' ✓

" 15" oak 06°30'

" 24" oak 12°12'

355°20'

355°20'

345°50'

326°00'

308°40'

310°30'

315°20'

13°20'

50°00'

83°00'

249°00'

236°00'

206°30'

Ctr. Group 7-10 "willow 20' apart. 184°30'

93°15'

Ctr. Group 25" oaks 16' 131°00'

DIST	VERT. ANGLE	ROD EQUIV.	ROD	DIFF.	EV.
			HI = 912.98		
			1.5		911.48
150			3.73		09.25 ✓
142			4.07		08.91 ✓
130			9.28		03.70 ✓
155			12.37		00.61 ✓
205			10.40		02.58 ✓
160	-0°55'	- 2.5	11.0	-13.5	99.5 ✓
120	-0°55'	- 1.9	10.1	-12.0	01.0 ✓
130'	-2°55'	- 6.6	9.0	-15.6	97.4 ✓
174'	-2°55'	- 8.8	6.3	-15.1	97.9 ✓
200	-2°55'	- 10.2	4.8	-15.0	98.0 ✓
205	-2°55'	- 10.4	5.5	-15.9	97.1 ✓
190'	-2°55'	- 9.7	6.3	-16.0	97.0 ✓
170'	-2°55'	- 8.6	5.4	-14.0	99.0 ✓
70'	-2°55'	- 3.6	8.7	-12.3	00.7 ✓
54'			5.9		07.1 ✓
62'			3.0		10.0 ✓
28'			3.0		10.0 ✓
44'			10.4		02.6 ✓
108			10.7		02.3 ✓
124'	-8°00'	-17.4	6.4	-23.8	89.2 ✓
128	-8°00'	-17.8	8.0	-25.8	87.2 ✓
60'	-10°35'	-11.0	10.0	-21.0	92.0 ✓
64	-10°35'	-14.7	1.8	-13.5	99.5 ✓

OBJECT

AZ.

STADIA

② A "3

GE Toe Rd Slope

140°40'

" Fence

101°35'

"

47°40'

15" oak

63°00'

Toe Rd Slope

99°10'

Shoulder

99°10'

♂ Prosperity

99°10'

Fe Toe Rd Slope

-0.4 150°10'

" 12" oak

-0.4 147°30'

"

-0.3 161°45'

"

-0.0 158°25'

"

154°20'

"

168°20'

" 15" oak

158°40'

" 12" oak

168°20'

" 15" oak.

175°00'

" 18" oak

171°55'

" 165°20'

Top of Slope

178°00'

Toe R

153°00'

Shoulder

152°15'

♂ Road.

151°00'

DIST.	VERT. ANGLE	ROD EQUIV.	ROD	DIFF.	EV.
$H/I = 912.98$					
90'	-10°35'	-16.4	1.40	-17.8	95.2 ✓
88'	—		4.5		08.5 ✓
90'			3.5		09.5 ✓
90'			3.5		09.5 ✓
100'			3.1		09.9 ✓
110'			1.0		12.0 ✓
122'			0.6		12.4 ✓
230'			+0.7		13.7 ✓
220'			+0.7		13.7 ✓
314'			+1.3		14.3 ✓
250'			+1.3		14.3 ✓
150'	-4°00'	-10.4	7.7	18.1	94.9 ✓
170'	-4°00'	-11.8	7.7	19.5	93.5 ✓
205'			7.5		05.5 ✓
240'	+2°00'	+7.0	5.0	+2.0	15.0 ✓
270'	+2°00'	+9.4	3.0	+6.4	19.4 ✓
305'	+4°04'	+21.6	4.0	+17.6	30.6 ✓
265'	+4°04'	+18.7	7.9	+10.8	23.8 ✓
308'	+4°04'	+21.8	11.1	+10.7	23.7 ✓
300'	+1°41'	+8.8	5.0	+3.8	16.8 ✓
305'	+1°41'	+9.0	3.8	+5.2	18.2 ✓
328'	+1°41'	+9.5	4.1	+5.4	18.4 ✓

OBJECT

AZI

STADIA

@ APT #4

To Δ #3

5°59' ✓

T.P. #1

To Δ "4A"

139°23½' ✓

To A #5

201°48½' ✓

Check Az. T/water Tower.

291°47'

GE

10°40'

" Ctr. 3 12" oak

9°00'

" 1-18" oak

16°00'

" 1-15" oak

19°35'

" Top Back Slope

19°50'

" Fence

23°10'

" / 11.1 19°40'

" 16°00'

" 24°00'

" Fence 32°10'

" 29°50'

" 35°00'

" 44°50'

" 24°40'

" 20°20'

" 16°30'

" 11°50'

DIST.	VERT. ANGLE	ROD EQUIV.	Diff. ROD	Rod DIFF.	EV.
H.I. = 928.73					
H.E. = 5.00					
860 ✓	-0°49'	-12.3	21.3	9.00	923.73
					907.86
340'					914.79
498' ✓				11.05	917.67 ✓
500'				1.9	26.9 ✓
470				0.8	27.9 ✓
515				3.6	25.1 ✓
585'				3.2	25.5 ✓
590'				4.1	24.6 ✓
560'				10.5	18.2 ✓
490'				13.5	15.2 ✓
418'	-1°00'	-7.3	-18.2	10.9	10.5 ✓
410'	-1°00'	-7.1	-14.2	7.1	14.5 ✓
428'	-1°00'	-7.5	-16.1	8.6	12.6 ✓
375'	-2°00'	-13.1	-20.8	7.7	07.9 ✓
370'	-2°00'	-12.9	-14.9	2.0	13.8 ✓
328'	-2°00'	-11.4	-15.8	4.4	12.9 ✓
334'	-3°00'	-17.7	-26.4	8.7	02.3 ✓
360'	-3°00'	-18.8	-22.8	4.0	05.9 ✓
390'	-3°00'	-20.2	-21.8	1.6	06.9 ✓
310'	-4°30'	-24.3	-31.7	7.4	97.0 ✓

OBJECT

AZI

STADIA

© 4"4"

GE

0°00'

"

4°50'

"

347°40'

"

Top 15' Hogback

325°20'

"

" " " "

163°20'

"

" " " "

150°30'

"

" " " "

152°20'

"

" " " "

155°20'

"

1-12" oak

145°30'

"

1-12" oak

136°15'

"

1-12" oak

132°40'

"

1-12" oak

143°00'

"

1-24" oak

148°00'

"

166°30'

171°30'

~~Fe Con~~

178°50'

190°20'

1.0

200°45'

203°20'

216°20'

227°00'

214°55'

197°20'

190°15'

DIST.	VERT. ANGLE	ROD EQUIV.	ROD	DIFF.	EV.
H.I. = 928.73					928.73
310'	-1°30'	- 8.1	11.5	19.6	09.1 ✓
290'	-1°30'	- 7.6	6.0	13.6	15.1 ✓
125'	-6°46'	-14.7	8.0	22.7	06.0 ✓
38'	-		4.5		24.2 ✓
15'			5.7		23.0 ✓
52'			4.0		24.7 ✓
110			1.4		27.3 ✓
184	+2°28'	+7.9	5.0	+2.9	31.6 ✓
186'			1.4		27.3 ✓
165'			9.7		19.0 ✓
138'	-2°45'	-6.6	5.0	11.6	17.1 ✓
84'			3.2		25.5 ✓
250'	+0°38'	+2.6	6.0	-3.4	25.3 ✓
232'	+3°00'	+12.1	6.0	+6.1	34.8 ✓
290'	+3°00'	+15.2	9.4	+5.8	34.5 ✓
362	0°57'		3.0		
330'	-2°00'	-11.5	5.0	16.5	12.2 ✓
330'	-2°00'	-11.5	+0.6	10.9	17.8 ✓
270'			11.0		17.7 ✓
248'	-2°30'	-10.8	5.0	15.8	12.9 ✓
200'	-6°45'	-23.4	6.0	29.4	99.3 ✓
190'	-6°45'	-22.2	3.1	25.3	03.4 ✓
230'	-4°56'	-19.7	6.0	25.7	03.0 ✓
278'	-2°00'	-9.3	8.0	17.3	11.4 ✓

395
392
7.90

OBJECT

AZI

STADIA

@ A #4

GE

195°30'

"

183°15'

"

212°20'

"

243°14'

"

266°20'

"

231°15'

To A #2B

350°20 $\frac{1}{2}$ ' ✓

@ A 2B

To A 2A

3.95
4.8

349°42' ✓

To A #4

170°20 $\frac{1}{2}$ ' ✓

To A #2C

236°43' ✓

GE

17°20'

"

75°40'

"

104°20'

"

102°55'

"

Toe Rd Slope

4.1

147°40'

"

FL 5' Maserry - 2' Head Wall

146°40'

"

147°20'

"

Fence.

145°30'

"

145°40'

DIST.	VERT. ANGLE	ROD EQUIV.	ROD	TYPE
-------	----------------	---------------	-----	------

$$H.I. = 928.73$$

923.73

190'	-6°27'	-21.3	6.00	27.3	01.4✓
150'	-6°27'	-16.8	6.5	23.3	05.4✓
110'	-9°35'	-18.1	7.0	25.1	03.6✓
114'	-9°35'	-18.8	11.9	30.7	98.0✓
80'	-12°34'	-17.0	10.0	27.0	01.7✓
50'	-12°34'	-10.6	8.3	18.9	09.8✓
232'✓	-8°48'	-34.4	5.0	39.4	89.3✓

HI = 893.87

886.76

5.08

888.82

790

8.75

885.15

233 +8°40' +36.3

5.0

874

7.58

886.29

40'

1.9

92.0✓

62

1.5

92.4✓

92'

2.6

91.3✓

150

2.55

91.3✓

455' +1°00' +7.9

1.85

+6.0

99.9✓

455' +1°00' +7.9

5.0

+2.9

96.8✓

430' +1°00' +7.5

4.8

+2.7

96.6✓

430' +1°00' +7.5

4.5

+3.0

96.9✓

370

4.6

89.3✓

OBJECT

AZ.

STADIA

@ A 2-B

GE

140°20'

"

Fe & Toe Slope

132°30'

"

" " " "

125°20'

"

" " " "

115°00'

"

114°40'

"

117°30'

"

124°10'

"

131°10'

"

140°10'

"

148°50'

"

149°30'

"

⊕ Draw

134°30'

"

" "

125°50'

"

" "

117°30'

"

121°20'

"

145°20'

"

155°20'

"

147°40'

"

129°00'

"

⊕ Draw

121°50'

"

" "

209°40'

213°50'

256°00'

DIST.	VERT. ANGLE	ROD EQUIV.	ROD	DIFF.	ELEV.
$H.I. = 893.87$					
350	$+1^{\circ}00'$	+ 6.1	5.3	+ 0.8	94.7 ✓
365'	$+1^{\circ}00'$	+ 6.5	0.4	+ 6.1	00.0 ✓
330'	$+2^{\circ}00'$	+ 11.5	2.6	+ 8.9	02.8 ✓
310'	$+3^{\circ}00'$	+ 16.2	2.2	+ 14.0	07.9 ✓
250'	$+2^{\circ}00'$	+ 8.8	3.5	+ 5.3	99.2 ✓
190'	$+2^{\circ}00'$	+ 6.6	6.0	+ 0.6	94.5 ✓
230'	$+1^{\circ}00'$	+ 4.0	1.5	+ 2.5	96.4 ✓
270'	$+1^{\circ}00'$	+ 4.7	5.0	0.3	93.6 ✓
270'	$+1^{\circ}00'$	+ 4.7	5.0	0.3	93.6 ✓
260'	$+1^{\circ}00'$	+ 4.5	5.6	- 1.1	92.8 ✓
170'	$+1^{\circ}00'$	+ 2.8	5.5	2.7	91.2 ✓
225'	-		1.8		92.1 ✓
170'			4.1		89.8 ✓
120'			5.3		88.6 ✓
120'			3.9		90.0 ✓
115'			3.2		90.7 ✓
85'	$+2^{\circ}00'$	+ 3.0	0.2	+ 2.8	96.7 ✓
70'			2.3		91.6 ✓
55'			4.1		89.2 ✓
45'			6.3		87.6 ✓
30'			8.1		85.8 ✓
20			5.9		88.0 ✓
55'			7.1		86.8 ✓

OBJECT

AZ

STADT

GE

end Draw

249°00'

"

225°50'

"

204°50'

"

205°00'

"

194°10'

"

191°10'

"

185°40'

"

166°20'

" app 2

50-100 Back from Shore

Beg. Fringe Willows S

349°40'

B.M.

721.38

721.30

H/I = 899.57

$$\begin{array}{r} 899.57 \\ + 0.18 \\ \hline 899.69 \\ + 13.17 \\ \hline 906.86 \\ + 0.72 \\ \hline \end{array}$$

$$\begin{array}{r} 906.14 \\ + 10.32 \\ \hline 916.46 \\ + 5.14 \\ \hline \end{array}$$

911.32 = 911.48

T.B.M. =

DIST.	VERT. ANGLE	ROD EQUIV.	ROD	DIFF	ELEV
70			8.5		85.4 ✓
70			7.1		86.8 ✓
150'	-		8.3		85.6 ✓
230'	-0°45'	3.0	5.0	8.0	85.9 ✓
230'			0.3		93.6 ✓
155'			0.4		93.5 ✓
100'			1.2		92.7 ✓
75'			1.2		92.7 ✓
165'			10.1		83.8 ✓

SPK in scrub oak S.W. cor Larp. Ave
& prosperity Ave

OBJECT

AZI

STADIA

DIST.	VERT; ANGLE	ROD EQUIV.	ROD	DIFF.	V.
-------	----------------	---------------	-----	-------	----

rod 5/27/49

OBJECT

AZ

AD

T @ A' Ctr. Sec.

To S $\frac{1}{2}$ Cor.

GE

"

"

"

"

"

"

FL 12" CM E end.

180°00

153°

169°40'

165°00'

161°10'

156°20'

148°35'

107°20'

(ok to use this)
AZ
K.A.

@ A#5-

To A#4

GE 24" oak

GE 24" oak

"

"

"

"

"

"

"

"

"

Fe

Top Borrow Pit Cat

21°48'

1.44
1.68

21°48½'

35°10'

46°40'

41°40'

59°45'

68°50'

62°50'

39°50'

20°20'

23°50'

43°50'

22°00'

5-20-49

(19)

DIST.	VERT. ANGLE	ROD EQUIV.	ROD	DIFF.	V.
-------	----------------	---------------	-----	-------	----

H.I. = 904.50

HI = 5.00

899.51

200'	-1°29'	5.2	-10.0	-15.2	89.3 ✓
210'	-1°29'	5.4	-5.8	-11.2	93.3 ✓
270'	-1°29'	7.0	-5.0	-12.0	92.5 ✓
340'	-1°29'	8.8	-4.9	-13.7	90.8 ✓
350'	-1°29'	9.1	-5.9	-15.0	89.5 ✓
310'	-1°29'	8.0	-7.9	-15.9	88.6 ✓
432'			7.08		97.42 ✓

H.I. = 921.80

HI = 927.90

917.67

498 ✓			4.17		923.73
195'			9.9	-9.9	11.9 ✓
190'			7.6	-7.6	14.2 ✓
190'			10.5	-10.5	11.3 ✓
154'			4.2	-4.2	17.6 ✓
155'			0.8	-0.8	21.0 ✓
200'	+2°30'	+8.7	1.0	+7.7	29.5 ✓
210'			10.9		10.9 ✓
220'			5.0		16.8 ✓
165'			5.1		16.7 ✓
125'			9.7		12.1 ✓
125'			11.1		10.7 ✓

OBJECT

AZ

ADT

T @ Δ #5

GE

15°00'

"

32°40'

"

30" oak

51°40'

"

60°40'

"

66°20'

"

Fence

70°30'

"

20" oak

8°30'

"

2°20'

1°10'

359°50'

357°20'

20" oak

350°40'

344°30'

306°40'

293°10'

15" Pop.

270°00'

265°00'

254°20'

258°20'

Sec Line Fe

258°40'

Toe Rd slope & Fe.

250°20'

Burrid

N. end Top culvert

Toe Slope

248°20'

12.2

280°00'

DIST.	VERT. ANGLE	ROD EQUIV.	ROD	DIFF.	VI
		H.I. = 921.80	HI = 927.90		
90'				-5.5	16.3 ✓
105'				-4.6	17.2 ✓
95'				-4.0	17.8 ✓
115'				-6.7	15.1 ✓
120'				-3.6	18.2 ✓
145'				-2.3	19.5 ✓
135'	-3°00'	-7.1	-8.0	-15.1	06.7 ✓
170'	-3°00'	-8.9	-10.3	-19.2	02.6 ✓
210'	-3°00'	-11.0	-11.3	-22.3	99.5 ✓
225'	-3°00'	-11.8	-8.4	-20.2	01.6 ✓
210'	-4°00'	-14.6	-11.4	-26.0	95.8 ✓
132'	-4°00'	-9.2	-14.5	-23.7	98.1 ✓
125 130'	-11°00'	-23.4	-2.5	-25.9	95.9 ✓
70 75'	-15°00'	-17.5	-10.1	-27.6	94.2 ✓
112 120'	-15°00'	-28.0	-5.2	-33.2	88.6 ✓
103 110'	-15°00'	-25.8	-6.5	-32.3	89.5 ✓
128 135'	-13°00'	-28.0	-4.1	-32.1	89.7 ✓
160 165'	-10°00'	-27.4	-4.7	-32.1	89.7 ✓
223 225'	-6°00'	-23.2	-9.4	-32.6	89.2 ✓
267 270'	-6°00'	-27.8	-3.4	-31.2	90.6 ✓
273 275'	-5°00'	-23.7	-0.7	-24.4	97.4 ✓
218 220'	-5°00'	-18.9	-8.82	-27.72	94.1 ✓
164 165'	-5°00'	-14.3	-13.00	-27.3	94.5 ✓

OBJECT

AZI

STADIA

TODAS

GE

218°10'

"

240°10'

"

269°40'

"

1-24" oak

322°30'

1-20" oak

341°20'

1-20" oak

18°10'

358°00'

188°40'

Fe

183°30'

Fe Cor.

185°30'

Tree slope

158°10'

Fe

159°30'

edge Borrow Pit

132°10'

" " "

95°00'

Fe

87°00'

edge Borrow Pit

75°20'

Bott. " "

84°20'

ctr.

87°50'

ctr. " "

89°10'

89°10'

91°10'

Tope B slope

91°20'

99°30'

DIST.	VERT. ANGLE	ROD EQUIV.	ROD	DIFF.	ELEV.
		H.I. = 921.80			
			HI 927.90		
91					
94'	- 10°00'	15.6	5.9	- 21.5	900.3 ✓
87					
90'	- 10°00'	14.9	11.9	- 26.8	95.0 ✓
53					
55'	12°00'	10.8	11.8	- 22.6	99.2 ✓
55					
57'	12°00'	11.2	10.8	- 22.0	99.8 ✓
96					
100'	12°00'	19.5	4.6	- 24.1	97.7 ✓
55'	—		5.5		16.3 ✓
27'			5.4		16.4 ✓
65'			5.0		16.8 ✓
110'			4.6		17.2 ✓
120'			3.7		18.1 ✓
120'			3.1		18.7 ✓
75'			3.9		17.9 ✓
20'			4.1		17.7 ✓
100'			4.0		17.8 ✓
97'			3.5		18.3 ✓
150			2.5		19.3 ✓
135'			9.3		12.5 ✓
150'			8.2		13.6 ✓
155'			2.6		19.2 ✓
185'			2.9		13.9 ✓
215			4.0		17.8 ✓
230			3.7		18.1 ✓
220'			4.1		17.7 ✓

OBJECT

AZI

STADIA

T@ 4 5

GE

102°20'

"

Top B. Slope

83°20'

"

" " "

77°30'

"

30" oak

73°50'

"

Edge Borrow Pit

75°20'

"

" " "

79°50'

"

" " "

68°30'

"

"

" & Fe

65°00'

Toe

142°30'

Shoulder } Carpenter

143°50'

⊕

146°30'

⊕

170°00'

Shoulder

170°00'

Toe

174°00'

⊕

204°00'

Shoulder

200°50'

⊕

213°30'

Fe

221°20'

Shoulder.

225°20'

⊕

234°10'

Shoulder

237°10'

Fe

239°40'

Fe Cor

12.4

240°10'

Shoulder

245°00'

DIST.	VERT ANGLE	ROD EQUIV	ROD	DIST	ELEV
-------	---------------	--------------	-----	------	------

H.I. = 921.80

~~HI = 937.90~~

220'			5.5		16.3 ✓
250'			3.3		18.5 ✓
280'			4.9		16.9 ✓
285'			5.7		16.1 ✓
230'			0.9		20.9 ✓
220'			2.0		19.8 ✓
240	+2°00	+8.4	-4.4	+4.0	25.8 ✓
240'	+3°00'	+12.6	-7.0	+5.6	27.4 ✓
150'			2.4		19.4 ✓
160			1.3		20.5 ✓
170'			0.5		21.3 ✓
145'			1.3		20.5 ✓
125'			1.8		20.0 ✓
120'			3.5		18.3 ✓
130'	X		6.5		15.3 ✓
135'			3.7		18.1 ✓
170'			4.6		17.2 ✓
150'			8.1		13.7 ✓
175'			6.3		15.5 ✓
240'			8.2		13.6 ✓
230'			8.9		12.9 ✓
225'			11.1		10.7 ✓
285'			14.8		07.0 ✓
290					
390'			11.1		10.7 ✓

OBJECT

AZ

STADIA

Top Mont $5\frac{1}{4}$ Sec 15 $241^{\circ}48'$ $\angle$ $246^{\circ}20'$ Shoulder $249^{\circ}30'$ $\angle$ 11.0 $252^{\circ}10'$ Shoulder 11.2 253° Toe $254^{\circ}30'$ GE $256^{\circ}40'$ 12.4 $264^{\circ}10'$ $265^{\circ}10'$ Toe of slope $254^{\circ}20'$ $298^{\circ}27\frac{1}{2}'$ @ SE $\frac{1}{4}$ cor.To $\Delta^{\#}5$ $117^{\circ}27\frac{1}{2}'$ To ctr. Sec. $360^{\circ}39'$

@ A 4 A

To A 4 $319^{\circ}20\frac{1}{2}'$ ctr. Antenna KSTP $338^{\circ}3\frac{1}{2}'$ $\angle$ Road $6^{\circ}01'$ edge Black Top $40^{\circ}50'$ Shoulder $3^{\circ}40'$ Shoulder $4^{\circ}10'$ edge Bk Top $6^{\circ}40'$

DIST.

VERT
ANGLEROD
EQUIV.

H.I. = 921.80

~~HI = 927.90~~

290'

350'

11.3

10.5 ✓

350'

11.4

10.4 ✓

430'

13.1

08.7 ✓

400'

13.2

08.6 ✓

400'

-1°00'

-7.0

-10.5

-17.5

04.3 ✓

420'

-0°45'

-5.5

-4.0

-9.5

12.3 ✓

465'

14.4

07.4 ✓

320'

-2°40'

-17.2

-9.0

-26.2

95.6 ✓

360'

-2°40'

-16.7

-7.0

-23.7

98.1 ✓

246

~~246~~

HI = 920.09

914.79

340

339

Hi 5.30

510

3.0

17.1 ✓

490

3.1

17.0 ✓

500

3.9

16.2 ✓

410

4.2

15.9 ✓

400'

4.5

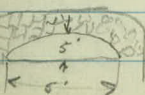
15.6 ✓

OBJECT

AZ

STADIA

⊥	8°20'
⊥	11°30'
edge Bk Top.	9°40'
shoulder	6°40'
shoulder.	6°10'
edge Bk Top	13°10'
⊥	16°40'
⊥	19°40'
edge Bk Top	14°30'
shoulder.	8°00'
"	3°40'
edge Bk Top	9°50'
⊥	22°10'
⊥	9°00'
edge Bk Top	314°10'
shoulder	295°00'
"	242°20'
edge Bk Top	226°40'
⊥	215°10'
Top of head wall (End)	72°50'
G.B. to FL 5' mas. Culv.	347°10'
Toe of slope	341°10'
Toe of slope	323°50'
"	299°10'



DIST.	VERT. ANGLE	ROD EQUIV.			
		HI =	920.09		
390			4.1		16.0 ✓
290			4.9		15.2 ✓
280'			5.5		14.6 ✓
270'			6.2		13.9 ✓
175'			7.7		12.4 ✓
175'			5.8		14.3
185'			5.2		14.9 ✓
130'			5.3		14.8 ✓
125'			6.6		13.5
125'			7.0		13.1 ✓
75'			6.7		13.4 ✓
65'			6.3		13.8
70'			5.5		14.6 ✓
15'			5.4		14.7 ✓
18'			5.5		14.6
30'			6.1		14.0 ✓
45'			5.5		14.6 ✓
60			5.1		15.0
72'			4.6		15.5 ✓
35'	-2°20'	-1.4	-11.0	-12.4	07.7 ✓
67	-3°02½'	-3.5	-15.0	-18.5	01.6 ✓
45'	-3°00½'	-2.4	-12.2	-14.6	05.5 ✓
40'			10.8	-10.8	09.3 ✓

OBJECT

AZI

STADIA

@A4A

GE	Toe of slope	272°10'
"	" " "	232°40'
"	Fence	249°30'
"	"	272°25'
	36" oak	297°20'
		270°10'
	15" oak	321°40'
	Fence	326°10'
	Fence	340°10'
	-18" oak Top B. Slope	226°50'
	Fe, Top B. Slope	235°10'
	Fe Cor.	226°20'
	Fe	225°30'
		237°50'
	24" oak	297°10'
		248°40'
		254°10'
	Top Back Slope	223°40'
	Bot " "	220°10'
	Shoulder	217°20'
	⊥	213°50'
	⊥	213°30'
	Shoulder	216°10'

DIST.	VERT ANGLE	ROD EQUIV.	ROD	DIFF.	ELEV.
HI = 920°09					
42'			8.3		11.8 ✓
75'			6.7		13.4 ✓
85'	+2°35'	+3.8	-2.0	+1.8	21.9 ✓
65'	+5°50'	+6.6	-4.0	+2.6	22.7 ✓
100'	+5°50'	+10.0	4.7	15.3	^{25.2} 15.4 ✓
120'			3.5		16.6 ✓
85'			3.0		17.1 ✓
70'			8.1		12.0 ✓
90'	-3°2½'	-4.8	-15.3	-20.1	00.0 ✓
150'			2.5	-2.5	17.6 ✓
115'	-1°15''	+2.5	-2.0	+0.5	20.6 ✓
160'			3.2		16.9 ✓
135'			3.2		16.9 ✓
180'	+1°12'	+3.8	-2.0	+1.8	21.9 ✓
200'	+3°30'	+12.2	-3.0	+9.2	29.3 ✓
175'	+3°30'	+10.7	-1.2	+9.5	29.6 ✓
154'	+4°25'	+11.8	-2.0	+9.8	29.9 ✓
200'	-		2.2		17.9 ✓
190'			5.3		14.8 ✓
210'			4.0		16.1 ✓
205'			3.4		16.7 ✓
290'			1.9		18.2 ✓
290'			2.3		17.8 ✓

OBJECT

AZI

STADIA

B. H. Back Slope		217°30'
⊥		213.10
Beg Rad		214°40'
Ctr. Rad	1.5	216°00'
edge Black	0.7	214°20'
end Rod	0.9	218°10'
⊥ Larpintur.	0.2	218°30'
Beg Rad	0.0	219°20'
Ctr. Rad	0.0	216°20'
edge BIK Top	0.5	214°10'
FL S end 18"cm	3.2	216°10'
FL N " " "		216°50'
		224°00'

@ Ctr. Sec 15

To S $\frac{1}{4}$ cor

180°

To Δ #1

151°46'

DIST.	VERT. ANGLE	ROD EQUIV	ROD	DIFF.	ELEV.
-------	----------------	--------------	-----	-------	-------

$$HI = 920^{\circ}09'$$

290'				3.2	16.9 ✓
365'				0.0	20.1 ✓
375'				0.0	20.1 ✓
400'				+0.5	20.6 ✓
410'				+1.4	21.5 ✓
430'				+1.2	21.3 ✓
440'				+2.0	22.1 ✓
465				+2.3	22.4 ✓
468'				+2.3	22.4 ✓
430'				+1.6	21.7 ✓
480'				0.8	20.9 ✓
400'				-1.1	19.0 ✓
405' ± 0°-55'		+6.5		7.0	19.6 ✓

OBJECT

TIME

STATION

T@A2C

To A2B

56°43' ✓

Shore Line

52°30'

" "

51°00'

" "

60°10'

Shore Line

64°40'

GE

65°30'

"

71°30'

"

Shore Line

67°30'

"

" "

71°50'

GE

 $\frac{1}{2} = 290$

77°00'

"

85°40'

"

Shore Line

82°40'

"

 $\frac{1}{2} = 1.8$

92°20'

"

Shore Line

98°00'

"

106°10'

"

 $\frac{1}{2} = 255$

105°00'

"

108°40'

"

112°50'

"

Fe, Sec Line

 $\frac{2.6}{1.5}$ ~~192°20'~~
~~222°20'~~

"

8

118°10'

"

112°30'

"

100°20'

"

Fe, Sec. line, Lake Shore

106°30'

DIST.	VERT. ANGLE	ROL EQUIV.	ROD	DIFF.	ELEV.
		HZ	891.31 HI = 5.08		886.23
874'			2.60	2.60	888.71
740'			8.2		83.1 ✓
720'			"		83.1 ✓
740'			"		83.1 ✓
675			"		83.1 ✓
730'			4.5		86.8 ✓
665'			2.0		89.3 ✓
615'			8.2		83.1 ✓
535'			"		83.1 ✓
580'			1.7		89.6 ✓
550'			0.2		91.1 ✓
480'			8.2		83.1 ✓
530'			+ 0.8		92.1 ✓
410			8.2		83.1 ✓
455'			6.1		85.2 ✓
510			2.1		89.2 ✓
485'			5.4		85.9 ✓
450'			5.3		86.0 ✓
390			0.8		90.5 ✓
385			0.8		90.5 ✓
360'			5.2		86.1 ✓
400'			8.2		83.1 ✓
350'			8.2		83.1 ✓

20 2C

G.E.

$\frac{1}{2} = 165'$

125° 40'

225° 40'

" Shore Line

112° 30'

" "

114° 40'

" "

111° 50'

" ———

127° 50'

" 137° 18'

" 141° 30'

" 132° 10'

" 133° 40'

" end Fringe of willows
Shore Line

107° 00'

" 168° 30'

" 150° 20'

" 167° 10'

" 179° 00'

" 161° 20'

" 159° 30'

" 140° 00'

" 134° 30'

" 5-27-49
Water Elev

" Shore 61° 10'

" 25° 00'

" 11° 20'

" 4 cottonwoods
~~600~~ 12 "

354° 20'

" end of Fl 358° 20'

DIST.	VERT. ANGLE	ROD DOWN	ROD	DIFF.	ELEV.
-------	----------------	-------------	-----	-------	-------

HI = 891.31

330	+0°32'	+3.1	-3.0	+0.1	91.4 ✓
265'				8.2	83.1 ✓
190'				8.2	83.1 ✓
120'				8.2	83.1 ✓
195'				4.9	86.4 ✓
210'	+1°30'	+5.5	-4.0	+1.5	92.8 ✓
160'	+1°30'	+4.2	-4.1	+0.1	91.4 ✓
140'	-			4.5	86.8 ✓
95'				4.0	87.3 ✓
98'				8.2	83.1 ✓
123					
125'	+7°00'	+14.9	-10.0	+14.9	96.2 ✓
182					
185'	+7°00'	+22.0	-8.0	+14.0	05.3 ✓
227					
236'	+7°00'	+27.5	-3.0	+24.5	15.8 ✓
207					
210'	+7°00'	+25.0	-2.8	+22.2	13.5 ✓
236					
240'	+7°00'	+28.6	-6.7	+21.9	13.2 ✓
250'	+7°45'	+20.6	-9.0	+11.6	02.9 ✓
245'	+2°15'	+9.6	-3.0	+6.6	97.9 ✓
245'	+0°50'	+3.6	-2.0	+1.6	92.9 ✓
				8.18	883.13
45'				8.2	83.1 ✓
60'				8.2	83.1 ✓
175'				8.2	83.1 ✓
190'				5.3	86.0 ✓
185'				6.3	85.0 ✓

OBJECT

AZI

STADIA

④ A 2C

	336°50'
	328°30'
	318°10'
ℓ Road	317°30'
	307°30'
	301°10'
	284°20'
	280°00'
	289°10'
Top Rd slope	303°30'
" " "	294°50'
" " "	289°50'
	279°40'
1.7	273°30'
	257°10'
Top Back slope	252°20'
Shoulder	252°50'
ints. Price Golden & Barclay.	254°00'
ℓ Road	273°30'
ℓ Road	290°00'
	299°00'
	283°50'
end Fe.	267°00'

DIST.	VERT. ANGLE	ROD EQUIV.	ROD	DIFF.	ELEV.
HI 891.31					
215'	+2°10'	+8.1	-2.5	+5.6	96.9 ✓
235'	+3°10'	+13.0	-6.0	+7.0	98.3 ✓
285'	+3°10'	+15.7	-10.2	+5.5	96.8 ✓
310'	+3°10'	+17.1	-10.3	+6.8	98.1 ✓
250'	+1°15'	+5.5	-9.0	-3.5	87.8 ✓
205'	+1°15'	+4.5	-8.7	-4.2	87.1 ✓
190'	+1°15'	+4.1	-7.2	-3.1	88.2 ✓
250'	+1°15'	+5.5	-5.0	+0.5	91.8 ✓
290'	+1°15'	+6.3	-8.7	-2.4	88.9 ✓
310'	+1°15'	+6.8	-9.7	-2.9	88.4 ✓
370'	+1°15'	+8.1	-10.5	-2.4	88.9 ✓
420'	+1°15'	+9.2	-9.0	+0.2	91.5 ✓
360'	+1°15'	+7.8	-7.3	+0.5	91.8 ✓
260'	+1°15'	+5.7	-0.4	+5.3	96.6 ✓
200'	+2°44'	+9.5	-2.0	+7.5	98.8 ✓
290'	+2°44'	+13.8	-5.5	+8.3	99.6 ✓
310'	+2°44'	+14.8	-9.0	+5.8	97.1 ✓
330'	+2°44'	+15.7	-8.9	+6.8	98.1 ✓
335'	+1°40'	+10.3	-5.0	+5.3	96.6 ✓
450'	+1°40'	+13.1	-9.7	+3.4	94.7 ✓
190'	—			-4.0	87.3 ✓
140'				-5.0	86.3 ✓
130'				-3.5	87.8 ✓

OBJECT

AZI

STADIA

T@A2C

GE

283°10'

6

289°30'

11

313°30'

4

324°50'

11

329°00'

11

324°10'

11

319°10'

A

Fe

353°20'

4

Fe Cor.

247°50'

4

242°30'

0.5

200°50'

197°40'

197°10'

211°30'

226°00'

246°00'

253°50'

233°10'

209°00'

196°20'

183°40'

182°40'

DIST.	VERT. ANGLE	ROD EQUIV.	ROD	DIFF.	ELEV.
-------	----------------	---------------	-----	-------	-------

$$HI = 891.31$$

95'				- 5.0	86.3 ✓
100'				- 3.3	88.0 ✓
130'	+3°20'	+7.5	-4.6	+2.9	94.2 ✓
110'	+3°20'	+6.4	-5.0	+1.4	92.7 ✓
145'	+3°20'	+8.4	-3.3	+5.1	96.4 ✓
155'	+3°20'	+9.0	-2.6	+6.4	97.7 ✓
170	+3°20'	+9.9	-4.1	+5.8	97.1 ✓
105'	—			- 5.0	86.3 ✓
22'	—			- 4.7	86.6 ✓
2 115'				- 1.4	89.9 ✓
95'				- 0.0	91.3 ✓
150'	+4°33'	+11.9	-7.0	+4.9	96.2 ✓
230'	+4°33'	+18.2	-0.8	+17.4	08.7 ✓
185'	+4°33'	+14.6	-2.0	+12.6	03.9 ✓
170'	+4°33'	+13.4	-3.6	+9.8	01.1 ✓
180'	+4°33'	+14.2	-6.3	+7.9	99.2 ✓
220'	+4°33'	+17.4	-8.4	+9.0	00.3 ✓
240	+4°33'	+19.0	-9.8	+9.2	00.5 ✓
230'	+4°33'	+18.2	-3.1	+15.1	06.4 ✓
235'	+4°33'	+18.6	-0.6	+18.0	09.3 ✓
240'	+6°30'	+27.0	-2.0	+25.0	16.3 ✓
185'	+6°30'	+20.8	-3.9	+16.9	08.2 ✓

OBJECT

AZI

STADIA

To Δ 2C

GE Lake shore

10°20'

" 4°00'

" Lake shore 17°20'

" Group 3 Pine - 2 Birch 11°40'

" 359°40'

" 1/2 220 359°40'

" 1/2 210 350°50'

" 1/2 190 351°00'

" 1.8 350°00'

" 387°00'

" Δ Rd. 333°30'

To Δ #2A

25°06 1/2

To Δ #2A

To Δ 2C

205°06 1/2

GE Lake shore

212°20'

" " 219°50'

220°20'

1/2 = 53° 222°00'

Δ Road, 1/2 = 57 224°50'

620

138.6

(81)

DIST.	VERT. ANGLE	ROD EQUIV.	ROD	DIFF.	ELEV.
-------	----------------	---------------	-----	-------	-------

HI = 891.31

260'			8.2	8.2	83.1 ✓
------	--	--	-----	-----	--------

290'			5.9	5.9	85.4 ✓
------	--	--	-----	-----	--------

450'			8.2	8.2	83.1 ✓
------	--	--	-----	-----	--------

430'			1.8	1.8	89.5 ✓
------	--	--	-----	-----	--------

390'	+1°00'	+6.8	-5.0	+1.8	93.1 ✓
------	--------	------	------	------	--------

440'	+1°00'	+7.7	-11.1	-3.4	87.9 ✓
------	--------	------	-------	------	--------

420'	+1°00'	+7.3	-9.7	-2.4	88.9 ✓
------	--------	------	------	------	--------

380'	+1°00'	+6.6	-8.3	+3.3	94.6 ✓
------	--------	------	------	------	--------

300'	—		0.3	-0.3	91.0 ✓
------	---	--	-----	------	--------

300'	+2°00'	+10.5	-5.8	+4.7	96.0 ✓
------	--------	-------	------	------	--------

350'	+2°00'	+12.2	-6.5	+5.7	97.0 ✓
------	--------	-------	------	------	--------

1398'			6.20	6.20	885.11 ✓
-------	--	--	------	------	----------

HI = 889.75

HI = 460

885.15

1390			3.60		86.2
------	--	--	------	--	------

852'			6.7		83.1 ✓
------	--	--	-----	--	--------

868'			6.7		83.1 ✓
------	--	--	-----	--	--------

940'			2.0		87.8 ✓
------	--	--	-----	--	--------

1060'	+0°30'	+9.2	-10.4	-1.2	88.6 ✓
-------	--------	------	-------	------	--------

1142'	+0°30'	+9.9	-3.4	+6.5	96.3 ✓
-------	--------	------	------	------	--------

OBJECT

AZI

STADIA

T@ A 2A.

E Rd.

230°55'

GE

 $\frac{1}{2} = 522$

230°20'

"

7.3

227°30'

 $\frac{1}{2} = 472$

"

226°20'

"

Lake shore

226°00'

"

" "

231°30'

"

233°20'

1/2

236°15'

"

Intersection
E Road

243°25'

"

E

 $\frac{1}{2} = 524'$

243°10'

"

247°45'

"

243°00'

"

Lake shore

245°40'

"

" "

252°00'

"

253°45'

"

 $\frac{1}{2} = 520$

251°20'

"

261°30'

"

 $\frac{1}{2} = 460$

264°00'

"

262°20'

"

Lake shore

257°26'

" "

261°20'

1.0

269°00'

0.7

274°00'

DIST.	VERT. ANGLE	ROD EQUIV.	ROD	DIFF.	ELEV.
			H.I. = 889.75		
			HI = 880.15		
1150'	+0°30'	+10.0	-7.1	+2.9	92.7 ✓
1044'	+0°30'	+9.1	-11.8	-2.7	87.1 ✓
944'	—		2.6	-2.6	87.2 ✓
880'			3.1	-3.1	86.7 ✓
830'			6.7	-6.7	83.1 ✓
792'			6.7	-6.7	83.1 ✓
900'	+0°30'	+7.8	-3.5	+4.3	94.1 ✓
1030'	+0°30'	+9.0	-3.5	+5.5	95.3 ✓
1150'	+0°30'	+10.0	-5.0	+5.0	94.8 ✓
1048'	+0°30'	+9.1	-9.0	+0.1	89.9 ✓
1052'	+0°30'	+9.2	-0.7	+8.5	98.3 ✓
915'	—		2.9	-2.9	86.9 ✓
954'			6.7	-6.7	83.1 ✓
990'			6.7	-6.7	83.1 ✓
980'			3.0	-3.0	86.8 ✓
1040'	+1°00'	+18.1	-11.9	+6.2	96.0 ✓
1030'	+0°30'	+9.0	-9.7	-0.7	89.1 ✓
920'	+0°30'	+8.0	-8.2	-0.2	89.6 ✓
820'	+0°30'	+7.1	-9.1	-2.0	87.8 ✓
790'	—		6.7	-6.7	83.1 ✓
670'	—		6.7	-6.7	83.1 ✓
³⁵ 710'			+2.5	+2.5	92.3 ✓
620'					

OBJECT

AZI

STADIA

T @ A 2A

Lake shore

274°10'

Lake shore

280°40'

GE

0.9

298°10'

$\frac{1}{2} = 320$

To A #1

17°22½

T A # 2

96°03½

180

276

DIST.	VERT. ANGLE	ROD EQUIV.	ROD	DIFF.	ELEV.
-------	----------------	---------------	-----	-------	-------

$$H.I. = 889.75$$

$$H.I. = \cancel{885.15}$$

500'

6.7

83.1 ✓

410'

6.7

83.1 ✓

440

+ 1.3

91.1 ✓

132'

132'

OBJECT

AZ

STADIA

WAKEFIELD LAKE
Bench Levels

Sta	+	π	-	Elev
BM	1.55	909.35		907.80
Ctr. Sec. 15			9.84	899.51
$\Delta^{\#} 1$			4.67	904.68
$\Delta^{\#} 2$	0.47	898.17	11.65	897.70
$\Delta^{\#} 2A$			13.02	885.15
BM	10.85	908.55		897.70
$\Delta^{\#} 3$	+12.78	920.64	-0.69	907.86
TP	+8.35	925.47	-3.52	917.12
$\Delta^{\#} 4A$			-10.68	914.79
$\Delta^{\#} 4$			-1.74	923.73
$\Delta^{\#} 4A$	10.16	924.95		914.79
BM			3.57	921.38
$\Delta^{\#} 5$	1.81	919.48	7.28	917.67
	1.61	908.08	13.01	906.47
	2.93	898.63	12.38	895.70
$\Delta^{\#} 2C$			12.40	886.23

921.39

5-25-49

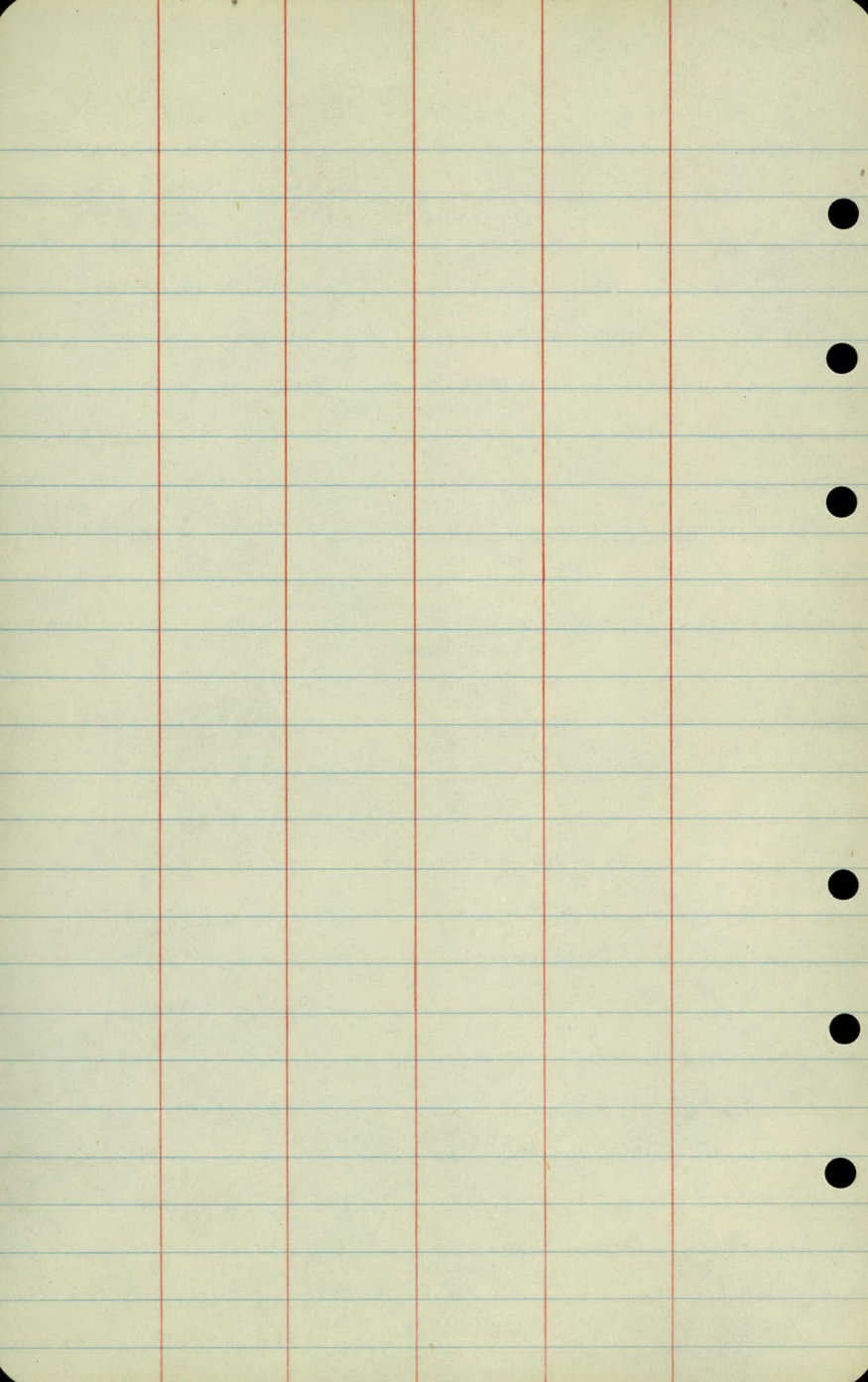
35

Spk in Arc Light Pole SE Cor. Frost & Prosperity
Top Mont Ctr. Sec 13

5-26-49

A # 2A

Spk in 15" Scrub Oak SW Cor. Larpenteur & Prosperity



36

DIST.

VERT.
ANGLE

ROD.
EQUIV.

ROD

DIFF.

ELEV.

OBJECT

AZI

STADIA

π @ H Ctr. Sec

To $S\frac{1}{4}$ cor.

180°00'

174°

131°00'

121°20'

121°30'

123°40'

DIST.	VERT. ANGLE	ROD EQUIV.	ROD	DIFF.	ELEV.
-------	----------------	---------------	-----	-------	-------

$$H.I. = 904.95$$

$$H.I. = 5.49$$

$$899.51$$

320'

- 12.1

217'

- 2°00

- 7.6

- 8.9

- 16.5

88.5 ✓

213'

- 2°00

- 7.4

- 9.4

- 16.8

88.2 ✓

270

- 2°00

- 9.4

- 3.9

- 12.8

92.2 ✓

147'

- 2°00'

- 5.1

- 8.2

- 13.3

91.7 ✓

OBJECT

AZI

STADIA

DIST.	VERT. ANGLE	ROD EQUIV.	ROD	DIFF.	ELEV.
-------	----------------	---------------	-----	-------	-------

OBJECT

AZI

STADIA

T @ A2B

To A2A

349°42'

To A4

170°20½' ✓

GE

7°40'

"

22°50'

"

52°30'

"

47°20'

"

47°10'

"

26°00'

"

6°30'

"

26°50'

"

65°20'

"

94°20'

"

87°40'

"

83°50'

1

T @ Ctr. Sec

To P4°1

151°46' ✓

GE

191°50'

1/2 = 450

201°40'

205°00'

204°40'

191°30'

189°30'

DIST	H.I. =	893.90	ROD	DIFF	ELEV
			HI = 5.1		888.80
795'					
115'	+1°30'	+ 3.0	4.1	- 1.1	92.8 ✓
120'	+10°10'	+ 20.5	3.7	+ 16.8	10.7 ✓
120'	+ 4°55'	+ 10.7	7.0	+ 3.7	97.6 ✓
95'	+5°55'	+ 9.7	3.0	+ 6.7	00.6 ✓
75'	+5°55'	+ 7.7	1.5	+ 6.2	00.1 ✓
85'	+9°30'	+ 13.8	1.0	+ 12.8	06.7 ✓
75'	—		1.1		92.8 ✓
40'	—		2.0		91.9 ✓
54'	—		1.6		92.3 ✓
70'	—		2.9		91.0 ✓
85'	+2°10'	+ 3.2	1.0	+ 2.2	96.1 ✓
110'	+2°10'	+ 4.2	3.7	+ 0.5	94.4 ✓

$$H.I. = 905.02$$

			HI = 5.52		899.5
820'	—		6.7		98.3
820'	—	HI 5.52	6.7		98.3 ✓
960			7.2		97.8 ✓
1060			8.0		97.0 ✓
1160			15.0		90.0 ✓
750			2.0		03.0 ✓
820			9.5		95.5

OBJECT

AZI

STADIA

H.I. = 905.02

T@ A Ctr. Sec.

G.F. Cor. Cult. Land.

180°40'

DIST.	ANGLE	ROD EQUIV.	ROD	DIFF.	ELEV.
-------	-------	---------------	-----	-------	-------

770

7.9

✓
97.1

OBJECT

AZI

STADIA

DIST.	VERT. ANGLE	ROD EQUIV.	ROD	DIFF.	ELEV.
-------	----------------	---------------	-----	-------	-------

Pac 6-6-49

OBJECT

AZI

STADIA

N @ $\Delta^{\#}2$ To $\Delta^{\#}1$

357°36'

To $\Delta^{\#}2A$

276°02'

To $\Delta^{\#}2D$

251°08'

N @ $\Delta^{\#}2D$ To $\Delta^{\#}2$

71°08'

Shoulder

179°00'

Toe of slope

171°35'

Top of B Slope

162°00'

GE

38°40'

Toe

161°20'

Shoulder

159°40'

edge of cult. Land

30°35'

shoulder

152°40'

Toe

152°15'

edge Cult Land

21°20'

Shoulder

152°40'

Toe

151°00'

, 11.0

29°45'

Shoulder

158°20'

Toe

157°10'

DIST.	VERT. ANGLE	ROD EQUIV.	ROD	DIFF.	ELEV.
			<u>HI = 902.70</u>		
			HI = 5.00		897.70
384'					
132'					
1200	—		7.28		895.42
					900.42, 91 900.33
			<u>HI = 900.47</u>		
			HI = 5.00		895.42
1200'			2.83		897.59
144			6.9		93.6 ✓
155'			8.5		92.0 ✓
204'			5.1		95.4 ✓
430'			12.0		88.5 ✓
290'			9.5		91.0 ✓
332'			6.9		93.6 ✓
500'			5.1		95.4 ✓
490'			5.2		95.3 ✓
452'			10.3		90.2 ✓
410'			6.4		94.1 ✓
554'			3.9		96.6 ✓
545'			5.3		95.2 ✓
334			12.7		87.8 ✓
650'			3.1		97.4 ✓
652'			4.1		96.4 ✓

OBJECT

AZI

STADIA

T@ A 2 D

GE	cor. Cult Land	11°40'
"		16°40'
"		10°45'
"	Fe Cor	10°00'
"	Fe	339°10'
"	Fe Cor.	312°20'
"		327°00'
	Top B Slope	301°45'
	Toe	298°10'
	Shoulder	296°00'
	⊥	292°00'
	Toe Slope	203°35'
	Shoulder	222°00'
	⊥	240°20'
	Inters. Ripley & Gulden ^{Pl.}	301°40'
	Top B Slope	265°45'
To S 1/2 cor.	1/2 698	148°29 1/2'

DIST.	VERT. ANGLE	ROD EQUIV.	ROD	DIFF.	ELEV.
		- 141 = 700.47			
342'			7.2		93.3 ✓
242'			12.3		88.2 ✓
163'	-1°00'	-2.8	10.5	-13.3	87.2 ✓
342			7.2		93.3 ✓
270'			6.4		94.1 ✓
290'			0.3		00.2 ✓
172'			7.8		92.7 ✓
155'			0.2		00.3 ✓
164'			1.3		99.2 ✓
152'			0.4		00.1 ✓
155'			0.0		00.5 ✓
76'			8.1		92.4 ✓
73'			7.2		96.3 ✓
82'			3.3		97.2 ✓
284'	+1°00'	+4.9	2.5	+2.4	02.9 ✓
60'	-		1.7		98.8 ✓
1396'					

OBJECT

AZI

STADIA

DIST.

VERT.
ANGLEROD
EQUIV.

ROD

DIFF.

ELEV.

OBJECT

AZI

STADIA

At $\Delta 5$ To $\Delta 4$ $21^{\circ}48\frac{1}{2}$ To S $\frac{1}{4}$ Cor. Sec. $241^{\circ}46'$ To $\Delta 2\frac{1}{2}$ $289^{\circ}33\frac{1}{2}$ At S $\frac{1}{4}$ Cor. Sec.To $\Delta 5$ $61^{\circ}46'$ To $\Delta 20$ $316^{\circ}07\frac{1}{2}$

To Cen. Sec.

 $0^{\circ}37'$ At $\Delta 20$ $136^{\circ}07\frac{1}{2}$ To S $\frac{1}{4}$ Cor. Sec. $136^{\circ}07\frac{1}{2}$ To $\Delta 5$ $109^{\circ}32\frac{1}{2}$ To $\Delta 28$ $56^{\circ}40\frac{1}{2}$ To $\Delta 1$ $23^{\circ}24'$ At $\Delta 1$ To $\Delta 20$ $203^{\circ}24'$

To Cen. Sec.

 $332^{\circ}23'$

DIST.

VERT.
ANGLEROD
EQUIV.

ROD

DIFF.

ELEV.

498

296

625

292

480

478

623

880

1774

887

2

1774

1774

746

OBJECT

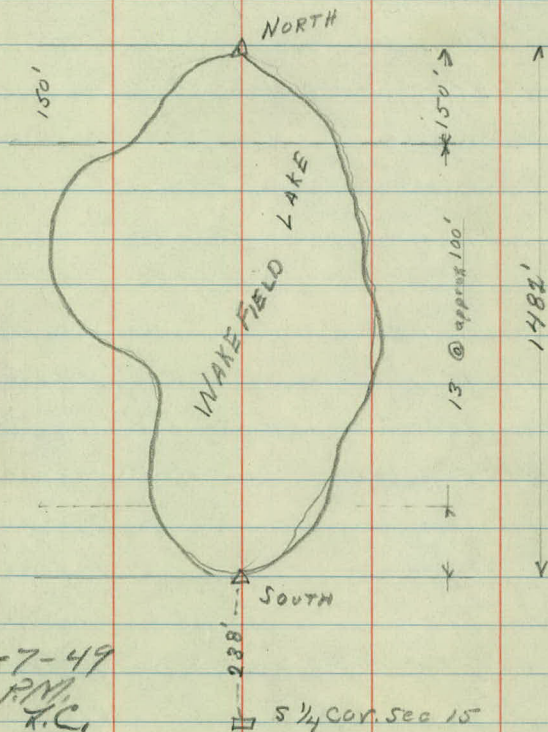
AZI

STADIA

DIST.	VERT. ANGLE	ROD EQUIV.	ROD	DIFF.	ELEV.
-------	-------------	------------	-----	-------	-------

Lake Bottom Topog Sounding & Stadia

Ctr. Sec. 15



Rec 6-7-49
P.M.
K.C.

OBJECT

AZI

STADIA

Δ North - 1720' N of S $\frac{1}{4}$ cor §

Δ South - 238' N " " "

X @ Δ North

To Δ South

180°00'

To Δ 2A

131°31 $\frac{1}{2}$ '

Lake elev

Line, 150' S of Δ North (approx)

Shore W

240°50'

221°05'

177°00'

130°00'

Shore E

119°25'

Line, 250' S of Δ North

Shore E

129°20'

135°40'

155°05'

176°40'

197°00'

219°25'

232°50'

238°40'

Shore W

6-6-49 X47

DIST.	VERT. ANGLE	ROD EQUIV.	ROD	DIFF.	ELEV.
-------	----------------	---------------	-----	-------	-------

25' Not N end of Lake

" 5 of 5 " " "

HI=890.35

283'

5.20

Bench Elev.
885.15

7.51

882.84

410

7.5

82.9

360

10.5

79.9 ✓

210

12.5

77.9 ✓

160

12.4

78.0 ✓

210

10.6

79.8 ✓

304

7.5

82.9 ✓

396

7.5

82.9 ✓

340

12.0

78.4 ✓

300

14.5

75.9 ✓

260

14.5

75.9 ✓

270

14.5

75.9 ✓

330

14.5

75.9 ✓

430

11.5

78.9 ✓

500

9.5

80.9 ✓

610

7.5

82.9

OBJECT

AZI

STADIA

A@ Δ North

To A #2A (BM)

Lake

Line 350 E to W

138°50'

149°50'

165°00'

181°40'

202°05'

222°10'

230°20'

237°20'

Line 450 W to E

225°00'

218°50'

211°20'

202°45'

194°50'

178°20'

165°30'

156°25'

145°30'

C-7-49 2 48

DIST.	VERT. ANGLE	ROD EQUIV.	ROD	DIFF.	ELEV.
-------	----------------	---------------	-----	-------	-------

HI = 890.40

			5.25		885.15
6-7-49			7.56	water	882.84

470			11.0		79.4 ✓
415			14.5		75.9 ✓
400'			15.5		74.9 ✓
370			15.5		74.9 ✓
390			15.0		75.4 ✓
480			13.5		76.9 ✓
585 [?]			10.5		79.9 ✓
680 [?]			8.5		81.9 ✓

660			9.5		80.9 ✓
590			11.5		78.9 ✓
530			14.5		75.9 ✓
505			15.0		75.4 ✓
470			15.5		74.9 ✓
450			15.5		74.9 ✓
460			15.5		74.9 ✓
495			15.0		75.4 ✓
550			12.5		77.9 ✓

OBJECT

Az

Stadia

Line 550 E-W

140°

~~146°25'~~

146°25'

157°40'

169°25'

182°20'

191°15'

205°20'

215°00'

Line 650 W-E

207°00'

220°00'

196°00'

191°20'

184°00'

178°20'

173°40'

168°40'

158°00'

150°40'

148°00'

DIST.	VERT. ANGLE	ROD EQUIV.	ROD	DIFF.	ELEV.
-------	----------------	---------------	-----	-------	-------

$$H.I. = 890.40$$

590			11.0		79.4✓
660			11.9		78.5✓
600			14.5		75.9✓
550			18.6		74.8✓
540			15.6		74.8✓
570			15.5		74.9✓
600			13.5		76.9✓
665			8.5		81.9✓
700			9.6		80.8✓
680			10.6		79.8✓
660			11.0		79.4✓
640			14.5		75.9✓
640			18.0		75.4✓
610			14.5		75.9✓
640			15.5		74.9✓
650			15.5		74.9✓
670			14.5		75.9✓
700			11.5		78.9✓
720			9.0		81.4✓

OBJECT

AZI

STADIA

Line 750 E to W

158°40'

172°20'

182°20'

193°40'

200°30'

202°25'

T @ A South

To A North

0°00'

To A 2C

287°24'

Line 850 (850' South of A North) W to E

347°00'

355°20'

0°20'

8°20'

14°40'

19°40'

Line 950 E to W

20°20'

11°45'

357°15'

379°40'

343°50'

DIST.	VERT. ANGLE	ROD EQUIV.	ROD	DIFF.	ELEV.
-------	----------------	---------------	-----	-------	-------

H.I. = 890.40

780			11.5		78.9✓
740			15.0		75.4✓
740			13.5		76.9✓
750			12.5		77.9✓
790			9.5		80.9✓
800			8.5		81.9✓

H.I. = 888.61

350'			2.32		888.29 ^{2 3 2}
670			8.8		79.8✓
650			10.8		77.8✓
650			11.3		77.3✓
670			11.8		76.8✓
680			10.3		78.3✓
700			8.8		79.8✓
600'			7.8		80.8✓
575			11.3		77.3✓
560			11.8		76.8✓
570			9.8		78.8✓
580			7.3		81.3✓

OBJECT

AZI

STADIA

Line 1050

W-E

336°20'

341°40'

352°00'

359°00'

7°00'

13°50'

21°50'

27°35'

Line 1150 E-W

25°40'

14°40'

0°00'

346°20'

332°40'

326°50'

Line 1250 W to E

318°25'

326°20'

337°56'

354°20'

8°40'

23°20'

DIST.	VERT. ANGLE	ROD EQUIV.	ROD	DIFF.	ELEV.
-------	----------------	---------------	-----	-------	-------

$$H.I. = 888.61$$

510			7.3		81.3 ✓
490			9.3		79.3 ✓
465			11.3		77.3 ✓
450			11.8		76.8 ✓
420			11.8		76.8 ✓
470			10.8		77.8 ✓
495			9.8		78.8 ✓
513			8.3		80.3 ✓

405			8.8		79.8 ✓
385			9.8		78.8 ✓
370			10.8		77.8 ✓
390			10.8		77.8 ✓
415			9.3		79.3 ✓
445			7.7		80.9 ✓

380			7.8		80.8 ✓
340'			9.8		78.8 ✓
195	295?		11.3		77.3 ✓
270			10.8		77.8 ✓
270			10.3		78.3 ✓
278			8.3		80.3 ✓

OBJECT

AZI

STADIA

Line 1350 E to W

24°00'

359°45'

326°30'

313°20'

304°46'

Line 1450 W to E

293°15'

300°00'

313°30'

349°46'

24°15'

Lake elev.

DIST.	VERT. ANGLE	ROD EQUIV.	ROD	DIFF.	ELEV.
-------	----------------	---------------	-----	-------	-------

$H.I. = 888.61$

173			8.3		80.3 ✓
165			9.8		78.8 ✓
200			10.3		78.3 ✓
270			9.3		79.3 ✓
320			7.3		81.3 ✓

225			6.8		81.8 ✓
175			8.3		80.3 ✓
132			8.3		80.3 ✓
80			7.8		80.8 ✓
90'			7.3		81.3 ✓

			5.77		882.84 ✓
--	--	--	------	--	----------

OBJECT

AZI

STADIA

DIST.

VERT
ANGLE

ROD

DIFF.

ELEV.

OBJECT

AZI

STADIA

K @ $\Delta^{\#} 2A$ To $\Delta^{\#} 1$. $17^{\circ} 21\frac{1}{2}'$ To Δ North $294^{\circ} 10'$ K @ Δ North $116^{\circ} 10'$ To $\Delta^{\#} 2A$ $114^{\circ} 10'$ To Δ South. $\frac{1}{2} = 738$ $180^{\circ} 37\frac{1}{2}'$ To $\Delta^{\#} 2$ $108^{\circ} 07\frac{1}{2}'$

6-9-44

GB
AM
MB
BC

(119-50)

54

VERT
ANGLE

ROD
EQUIV.

ROD

DIFF.

ELEV.

HI = 4.95 ✓

885'15"

387'

265'

—

4.51

265'

—

5.34

1476'

391

OBJECT

AZI

STADIA

West Traverse

WAKEFIELD LAKE

GB

AM

BC

July 8 & 11, 1949

Sta Pt L L A Rt.

19+64.02

18+15.25

$56^{\circ}07\frac{1}{2}'$

15+96.57

$39^{\circ}30'$

14+11.57

$46^{\circ}10'$

10+63.64

$36^{\circ}45'$

6+00.29

$72^{\circ}46'$

2+89.82

$62^{\circ}41'$

1+15.32

Thence N parallel with $\frac{1}{4}$ Sec Line

0+00

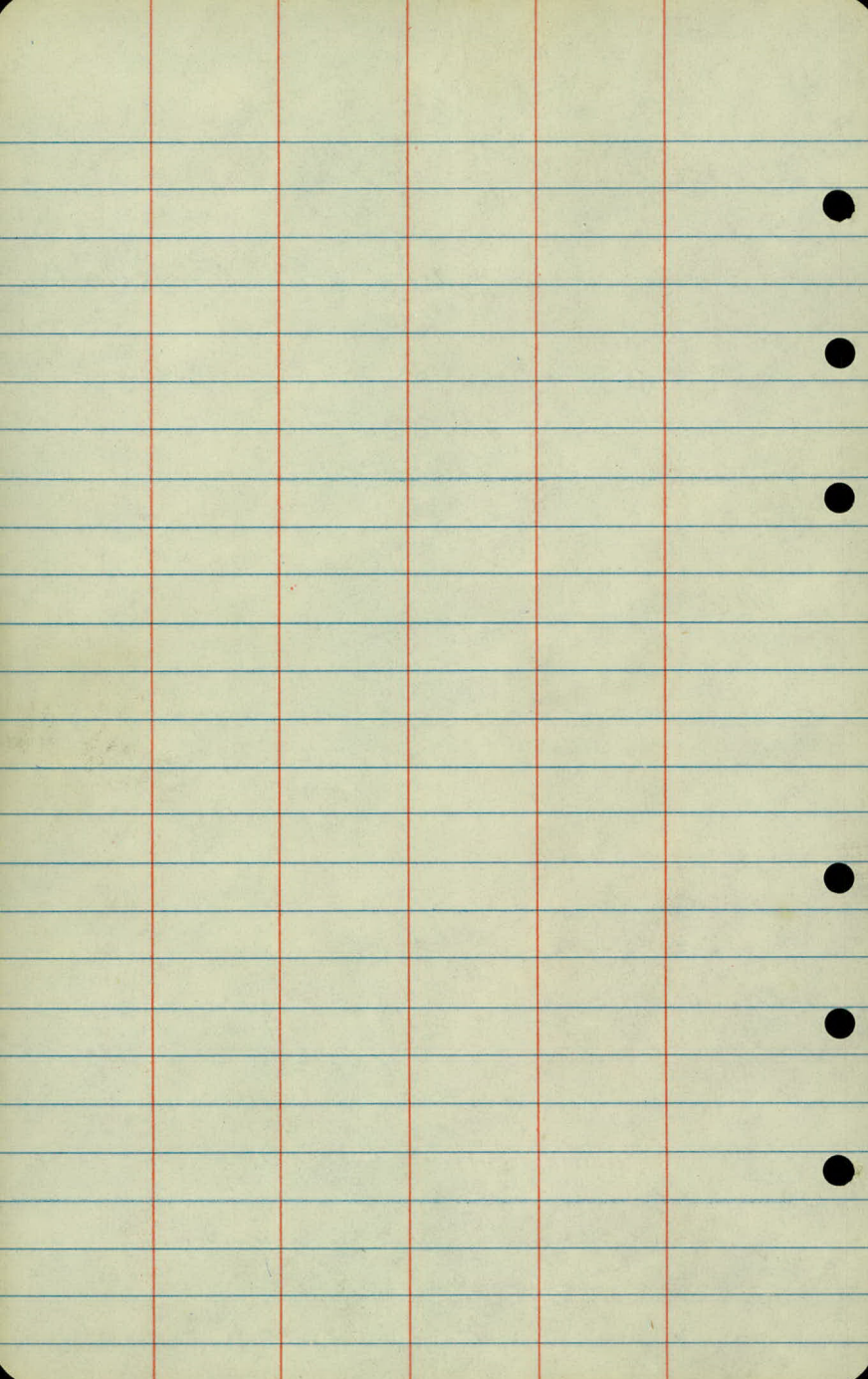
S $\frac{1}{4}$ cor sec 15

Cor. Iron on $\frac{1}{16}$ line, SE Cor. Ripley & Goulden^{P.}

$\frac{1}{16}$ Line

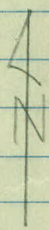
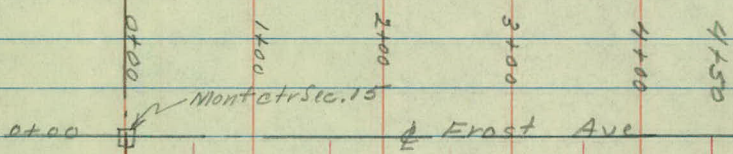
2 Carpenter's 115.32' W of Mont.

□ Stone Mont.



WAKEFIELD PARK

X Section of
Ball field



Hazelwood Ave

4-28-50

G.B.

A.M.

M.B.

K.R.

Wakefield
Lake

Rec. 4-30-50
T.G.

Sta	+	π	-	Elev
BM	5.24	904.80		899.56

0+00

899.51

2

Painted Sq. (□) @ Ctr Sec 15

99.6	99.5	99.5	96.9	96.9	00.3	99.9	97.9
5.24	5.3	5.3	7.9	7.9	4.5	4.9	6.9
2	10	20	26	29	34	64	100

94.4	94.7	94.2	93.2	92.5	92.6	93.0	93.7	94.0	95.6
9.9	10.1	10.6	11.6	12.3	12.2	11.8	11.1	10.8	9.2
542	500	450	400	351	300	248	200	178	146

97.1	98.6	99.6	00.5	00.3	98.2	98.1	97.5	95.4
7.7	6.2	5.2	4.3	4.5	6.6	6.7	7.3	9.4
571	600	633	664	700	721	738	761	800

86.7	89.7	94.5
18.1	15.1	10.3
900	866	820

Sta	+	π	-	Elev
-----	---	-------	---	------

		904.80		
--	--	--------	--	--

0+50				
------	--	--	--	--

2

99.6	99.4	99.1	97.7	97.0	96.7
5.17	5.35	5.7	7.1	7.8	8.1
2	10	20	25	31	48

93.0	92.9	93.1	93.0	93.8	95.3
11.8	11.9	11.7	11.8	11.0	9.5
356	300	256	200	148	100

94.7	95.1	94.7	94.4	94.9	97.0	99.0	900.0	00.7
10.1	9.7	10.1	10.4	9.9	7.8	5.8	4.8	4.1
400	414	448	500	533	559	600	650	700

87.4	91.3	95.2	97.0	97.7	99.1	99.9
17.4	13.5	9.6	7.8	7.1	5.7	4.9
900	864	833	800	770	743	725

✓

Sta	+	π	-	Elev
-----	---	-------	---	------

		904.80		
--	--	--------	--	--

1+00				
------	--	--	--	--

7

99.8	99.6	99.4	95.0	94.2	93.4	92.8
4.95	5.15	5.4	9.8	10.6	11.4	11.9
4	10	20	37	74	100	100

98.1	97.3	96.6	96.0	94.0	92.4	92.3	92.4
6.7	7.5	8.2	8.8	10.8	12.4	12.5	12.4
500	415	445	400	350	300	250	200

98.8	99.3	99.8	00.8	01.5	00.8	99.8
6.0	5.5	5.0	4.0	3.3	4.0	5.0
550	600	650	700	717	741	768

88.4	95.0	98.2
16.4	9.8	6.6
900	847	800

✓

Sta	+	π	-	Elev
-----	---	-------	---	------

		904.80		
--	--	--------	--	--

1+50				
------	--	--	--	--

£

✓	00.2		900.0	99.7	94.5	94.3
	4.60		4.79	5.1	10.8	10.5
	2		10	21	37	100
✓	95.6	93.7	93.0	93.0	93.4	93.8
	9.2	11.1	11.8	11.8	11.4	11.0
	400	340	300	242	200	142
✓	97.4	98.9	99.9	00.3	00.3	01.4
	7.4	5.9	4.9	4.5	4.5	3.4
	445	500	543	600	653	700
✓	89.9	95.8	99.8	02.0	02.9	03.9
	14.9	9.0	5.0	2.8	1.9	0.9
	900	858	800	866	831	807

✓

Sta + π - Elev

904.80 ✓

2+00

5.25 899.55

ϕ
 ϕ

01.0	00.7	00.2	95.1	95.0	94.7
3.82	4.10	4.6	9.7	9.8	10.1
2	10	21	46	80	100

94.2	93.7	93.8	94.1	94.5
10.6	11.1	11.0	10.7	10.3
357	300	262	200	145

95.4	97.1	98.8	99.7	00.5
9.4	7.7	6.0	5.1	4.3
400	451	500	546	600

91.8	96.2	97.2	98.0	00.4	01.5	01.8	01.2
130	8.6	7.6	6.8	4.4	3.3	3.0	3.6
900	871	832	800	766	734	700	644

Sta	+	π	-	Elev
-----	---	-------	---	------

2+50		904.80		
------	--	--------	--	--

02.2	02.2	01.2	96.4	95.8	95.6
258	2.63	3.60	8.4	9.0	9.2
2	10	22	39	85	100
	94.4	94.3	94.1	94.5	95.0
10.4	10.5	10.7	10.3	9.8	
346	300	251	200	152	
94.6	95.8	97.4	98.7	90.4	
10.2	9.0	7.4	6.1	4.4	
400	447	476	500	545	
99.8	01.4	02.4	02.1	01.5	
5.0	3.4	2.4	2.7	3.3	
740	700	675	646	600	
97.9	96.3	94.8	93.8	92.0	
6.9	8.5	10.0	11.0	12.8	
768	800	854	883	900	



Sta + π - Elev

904.80

3+00

TP 5.03 908.78 1.05 903.75

1.15	13.2	1.5	2.2	6.1	7.8	8.2
2	10	20	24	36	47	100
03.6	03.5	03.3	02.6	98.7	97.0	96.6

9.4	9.5	9.6	9.3	8.5
341	300	244	200	147
95.4	95.3	95.2	95.5	96.3

89	8.7	58	4.00	4.00
400	458	500	554	600
95.9	96.1	99.0	00.8	00.8

6.7	4.6	2.7	2.4	3.00
800	748	700	668	634
98.1	00.2	02.1	02.4	01.8

10.1	13.3	18.1	18.1
857	834	891	900
94.7	91.5	86.7	86.7

Sta	+	x	-	Elev
-----	---	---	---	------

		908.78		
--	--	--------	--	--

3+50				
------	--	--	--	--

05.0
3.80
£

05.8
2.97
10

04.4
4.4
20

£
03.9
4.9
24

01.5
7.3
36

97.3
11.5
46

96.6
12.2
300

04.4
4.4
256

96.3
12.5
200

96.8
12.0
61

97.3
11.5
100

97.3
11.5
358

97.2
11.6
400

97.4
11.4
463

98.4
10.4
500

01.2
7.6
532

4.03.9
4.9
685

04.7
4.1
665

04.5
4.3
639

02.7
6.1
600

02.7
6.1
561

5.03.1
5.7
700

02.4
6.4
746

01.7
7.1
779

99.8
9.0
800

98.2
10.6
815

91.6
17.2
876

88.2
20.6
868

91.9
16.9
866

93.6
15.2
857

96.8
12.0
821

Sta	+	π	-	Elev
		908.78		

3495

2

= Toe of cut

For other shots See 4+00

	97.4	97.4	97.1	97.7
	11.4	11.4	11.7	11.1
	300	262	213	200
	97.1	97.1	97.6	98.0
	11.7	11.7	11.2	10.8
	346	400	435	475

246	254	32	4.3	4.6	9.3	10.6	11.5	11.9
246	10	25	28	33	47	67	100	128
06.4	06.3	05.6	04.5	04.2	99.5	98.2	97.3	96.9

800	262	213	200	171
900.0	99.7	98.1	97.7	96.9
8.8	9.1	10.7	11.1	11.9

346	400	435	475
9.5	9.5	9.2	8.6
99.3	99.3	99.6	99.2

600	572	523	500
5.4	6.2	9.1	10.1
03.4	02.6	99.1	98.7

642	675	700	725	755
6.2	6.4	6.8	7.7	8.6
02.6	02.4	02.0	01.1	00.2

837	834	826	815	800
14.6	18.1	18.1	13.5	12.1
94.2	90.7	90.7	95.3	96.7

853	900
14.7	10.2
94.1	98.6

Sta	+	π	-	Elev
-----	---	-------	---	------

908.78

4+50

BM

9.20 899.58

C

07.2
154
L

07.2
1.6.2
10

07.2
1.6
34

06.1
2.7
100

05.6
3.2
160

03.6
5.2
200

04.6
4.2
400

04.8
4.0
376

04.7
4.1
380

05.6
3.2
320

05.2
3.6
300

03.9
4.9
277

03.5
5.3
283

04.1
4.7
451

05.0
3.8
494

03.7
5.1
500

02.0
6.8
510

01.7
7.1
535

00.1
8.7
558

08.1
10.7
744

00.1
8.7
700

02.9
5.9
663

02.8
6.0
634

00.4
8.4
600

08.9
14.9
756

08.9
14.9
758

08.9
12.9
760

08.7
12.1
767

08.6
13.2
777

04.5
4.3
900

04.4
4.4
868

02.7
6.1
843

08.5
10.3
800

06.6
12.2
791

✓

Sta

+

π

-

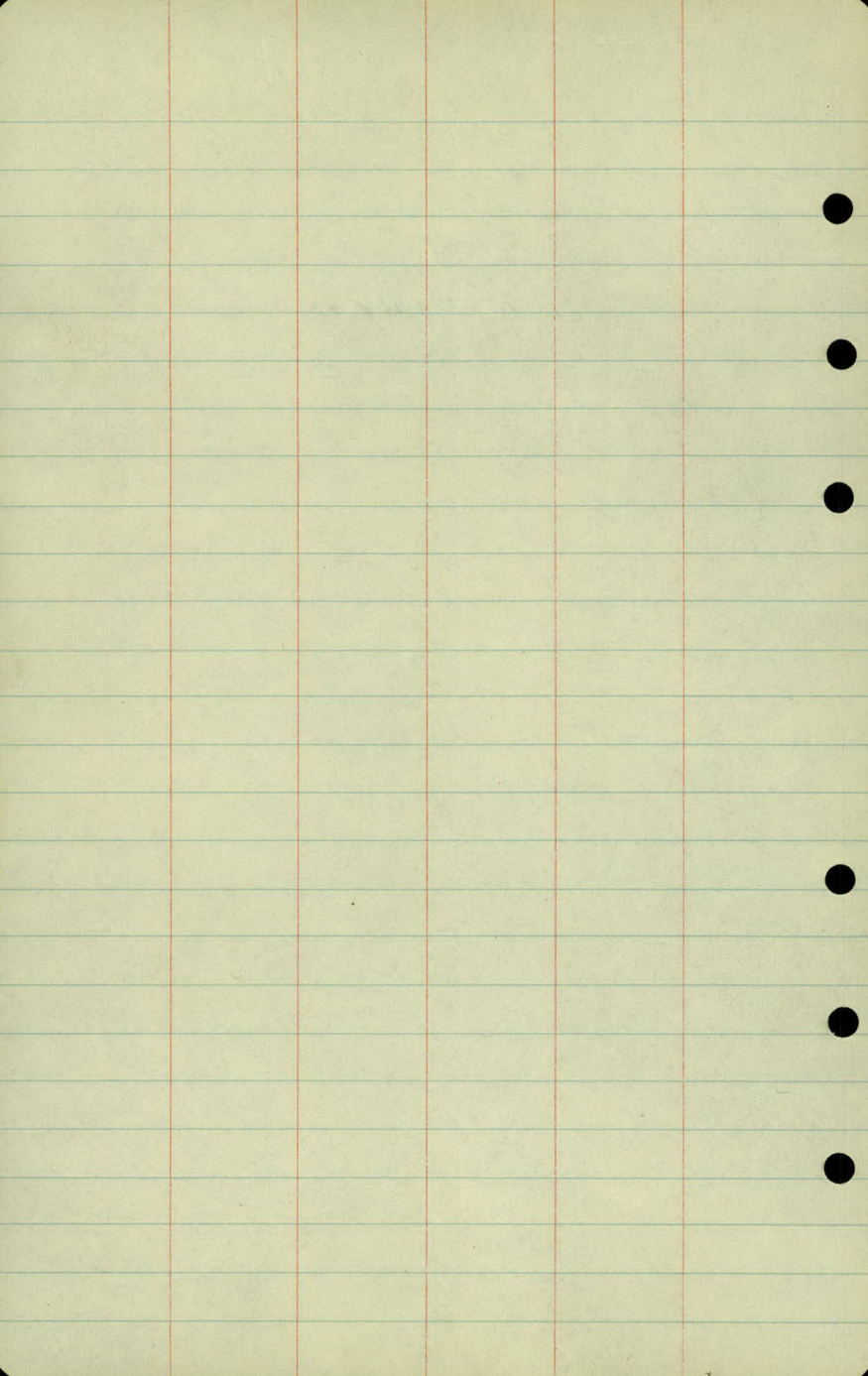
Elev

1
Wakefield Park

Contours

West Side

12 pages



8 May 1953
FH
AM
M Mc

2

Alignment

Sta Point ΔL ΔR

13+67.60 P.I. $83^{\circ}12\frac{1}{2}'$

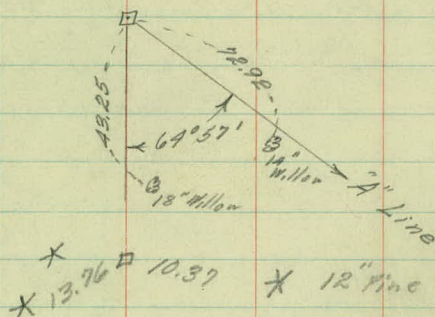
9+22.95 P.I. $42^{\circ}05\frac{1}{2}'$

2+28.13 P.I. $56^{\circ}09'$

2+19

1+62.33 POT Property iron

0+00 Property Iron SE Cor Golden Pl & Ripley



$\square$ 60.42 OPP
 PPO 48.27

Sta Point ΔL ΔR

19+49.30 P.I. $\pm$ Larpeur

19+18.58 P.O.T. Property Iron

17+57.92 P.I. $79^{\circ}40'$

Cor. Foundation

117.00

Post Sp in Mont.

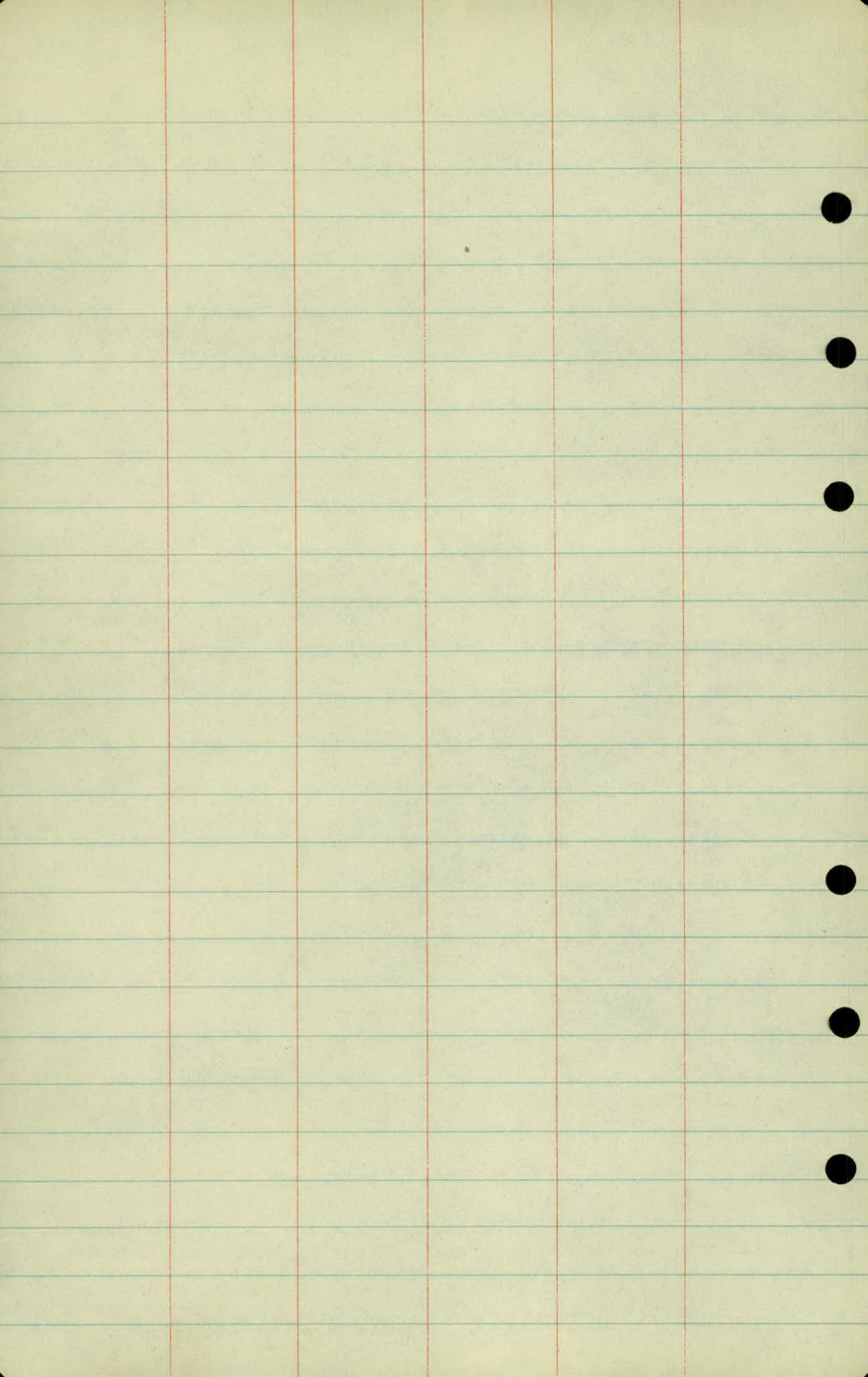
26.08

opp

34.95 0 PP

14.31

12" Willow



Contours

Note:

Contour 887.0 Established
with Hand Level

Sta	PG	PGR	-	Elev
BM	2.03	894.61		892.58
W.S	7.35	891.49	10.47	884.14

888.00 3.5

890.00 1.5

1+63

1+87

2+14

3

4

5

6

7

L

E

R

1.5

3.5

887.0

887.0

4

4.1

3.5 ✓

1.5 ✓

7

46

887.0

21

3.5 ✓

1.5 ✓

47

887.0

101

3.5 ✓

47

3.1

1.5 ✓

37 ✓

887.0

89

3.5 ✓

79

2.8

1.6 ✓

24

887.0

20

40

3.5 ✓

12

1.5 ✓

32

Wall

Sta	PG	PGR	-	Elev
	888.00	3.5		
	890.00	1.5		

8

W.S.	9.60	893.74		884.14
	888.00	5.74		
	890.00	3.74		

9

+30

10

11

12

+78

13

W.S.	7.02	891.16		884.14
	888.00	3.16		
	890.00	1.16		

L

L

R

$$\begin{array}{r} 887.0 \\ 65 \end{array}$$

$$3.5 \checkmark$$

$$1.5 \checkmark$$

$$32$$

$$\begin{array}{r} 887.0 \\ 85 \end{array}$$

$$5.74 \checkmark$$

$$76$$

$$3.74 \checkmark$$

$$2$$

3.6

$$\begin{array}{r} 887.0 \\ 34 \end{array}$$

$$5.75 \checkmark$$

$$28$$

$$3.75 \checkmark$$

$$13$$

2.5

$$\begin{array}{r} 887.0 \\ 4 \end{array}$$

6.2

$$5.75 \checkmark$$

$$5$$

$$3.75 \checkmark$$

$$16$$

$$\begin{array}{r} 887.0 \\ 9.0 \\ 22 \end{array}$$

$$5.75 \checkmark$$

$$29$$

$$3.75 \checkmark$$

$$35$$

$$\begin{array}{r} 887.0 \\ 7.0 \\ 3 \end{array}$$

$$5.75 \checkmark$$

$$12$$

$$3.75 \checkmark$$

$$24$$

$$\begin{array}{r} 887.0 \\ 8.6 \\ 46 \end{array}$$

$$5.75 \checkmark$$

$$6.2$$

$$3.75 \checkmark$$

$$74$$

$$887.0$$

$$10$$

Sta	PG	PGR	-	Elev
	888.00	3.16		
	890.00	1.16		

14

15

16

WS	9.75	893.89		884.14
	888.00	5.89		
	890.00	3.89		

17

+25

+63

+84

18

+30

L

L

R

887.0 ✓ ✓
 10 3.16 2.6 1.16
 9 19

887.0 ✓ ✓
 3 3.7 3.16 1.16
 6 21

887.0 ✓ ✓
 6.6 3.16 1.16
 25 31 47

887.0 ✓ ✓
 8.2 5.9 3.9
 10 20 34

887.0
 47

5.9 ✓

3.9 ✓

887.0 ✓ ✓
 75 5.9 3.9 3.1
 49 16

3.9 3.7
 7

Sta	PG	PCR	-	Elev
	888.00	5.9		
	890.00	3.9		

18+50

W.S.	11.79	895.93		884.14
	888.00	7.93		
	890.00	5.93		

0+00 A

1 A

+15

2 A

2+45 A

TP	6.15	894.79	7.29	888.64
	890.00	4.79		

3

+50

+62

L

E

R

✓
3.9 3.0
29

5.9 7.9 8.0 887.0
33 3 15

5.9 6.2 7.9 887.0 887.0 7.9 5.9 887.0
3 18 22 25 26 34 25

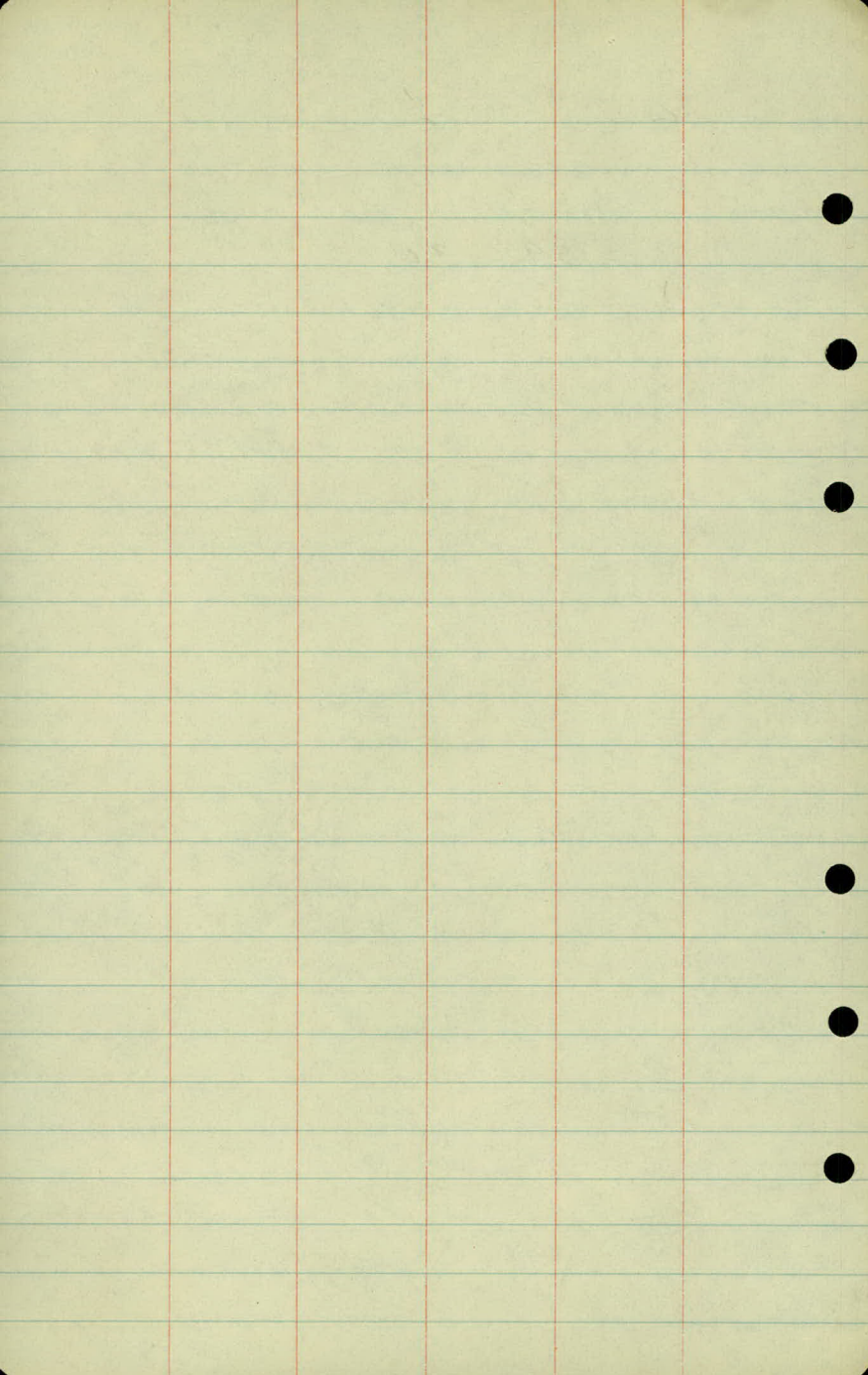
5.9 7.0 7.9 7.9 5.9
5 9 46 54

1.8 5.9 7.4 5.9
13 Lowest 74

4.8 6.6 4.8
28 68

4.8 5.4 4.8
20 12

4.8



Irons

Tied out

Sta

7+00

6+00

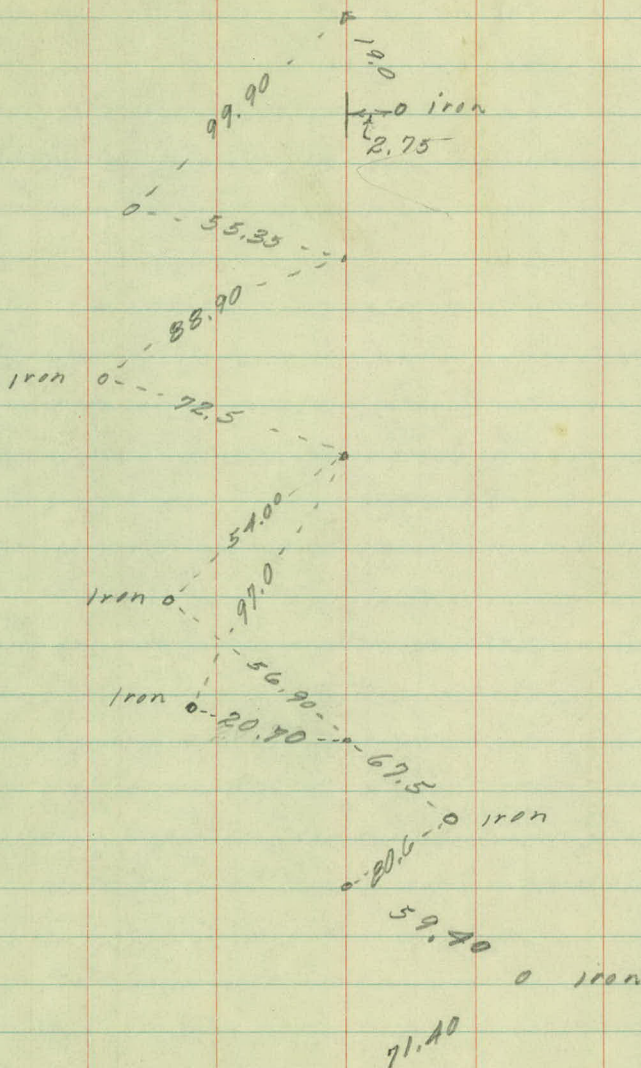
6+00

5+00

4+00

3+00

2+23.13 P.I.



Sta

12+00

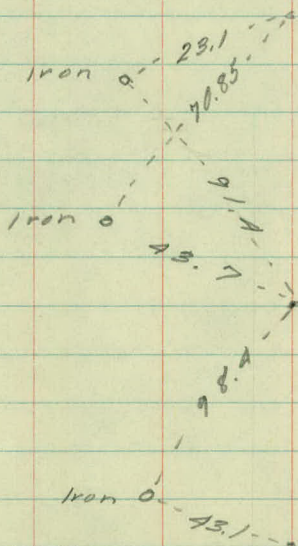
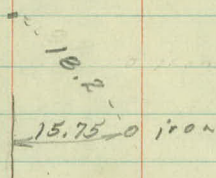
9+00

8+00

7+00

£

12



Soundings

Wakefield Park

7/22/53

2+90 Water

Sta 3+50 on Line 0+00 Beyond 2+23.13

0-1

1-1 $\frac{1}{2}$

1 $\frac{1}{2}$ -2

2-3

3-4

4-

Water

Mud

Sand

Sta 4+00 on Line 0+00 to 2+23.13 Extended

0-1

1-2

2-2 $\frac{1}{2}$

2 $\frac{1}{2}$ -3

3-4

4-5

5-6

6-

Water

Mud

Sand

(1) of (8)

Sta 4 180' Ft Lt

90' Lt Water
Edge

Feet	Material
0-1	Water
1-2	
2-3½	
3½-4	
4-5	
5-6	Mud
6-7	
7-7½	✓
7½-	
	sand

Sta 5 202 Ft Lt

Water 145'

0-4	Water
4-4½	Mud
4½-	Sand

Sta 5 190 ft Lt

0-2	Water
2-	Sand

Sta 6 206' Lt

146' Water

59	0-3	Water
59	3-4	Mud
146	4-	Sand

Sta 7 182' Lt

Water 105'

97	0-3	Water
105	3-4½	Mud
182	4½-	Sand

Sta 7 155'

Water 105'

50	0-3	Water
	3-4	Mud
	4-	Sand

Sta 8 205' Lt

Water 128'

0-3½ Water

3½-4½ Mud

4½- Sand

Sta 9 180' Lt

Water 127'

0-3 Water

3-4 Mud

4- Sand

Sta 9+30 130' Lt

73' Water

0-3 Water

3-4½ Mud

4½- Sand

Sta 9+30 112' Lt

28

0-2½ Water

2½-3 Mud

3- Sand

(4)

16

DIST.

VERT.
ANGLEROD
EQUIV.

ROD

DIFF.

ELEV.

OBJECT

AZ.

STADIA

Sta 10 105' Lt Water 42'

0-2 Water

3-4½ Mud

4½— Sand

Sta 10 78' Lt

0-2½ Water

2½-4 Mud

4— Sand

Sta 11 92' Lt Water 19'

0-3' Water

3-6' Mud

6— Sand

Sta 11 60' Lt

0-2 Water

2-8 Mud

8— Sand

(5)

DIST.	VERT. ANGLE	ROD EQUIV.	ROD	DIFF.	ELEV
-------	----------------	---------------	-----	-------	------

OBJECT

AZ.

STADIA

Sta 12 73' Lt Water 27'

0-2 Water

2-4 Mud

4- Sand

Sta 12 100' Lt

0-3 Water

3-6 Mud

6- Sand

Sta 15 110' Lt 41' Water

0-3 Water

3-5 Mud

5- Sand

Sta 15 75' Lt

0-2½ Water

2½-3 Mud

3- Sand

18

VERT:
ANGLE

OBJECT

AZ.

STADIA

Sta 16 75' Lt 13' Water

0-2½ Water

2½-9 Mud

9- Sand

Sta 16 50' Lt

0-2 Water

2-10 Mud

10- Sand

Sta 17 87' Lt Water 22'

0-3 Water

3-11 Mud

11- Sand

Sta 17 57' Lt

0-1½ Water

1½-4½ Mud

4½- Sand

DIST.

VERT.
ANGLEROD
EQUIV.

ROD

DIFF.

ELEV

OBJECT

AZ.

STADIA

Sta 17+57.92

100'

Water 44

0-2½

Water

2½-6

Mud

6-

Sand

Sta 17+57.92

130'

0-3½

Water

3½-8

Mud

8-

Sand

Sta 17+57.92

80' Lt

0-1½

Water

1½-5

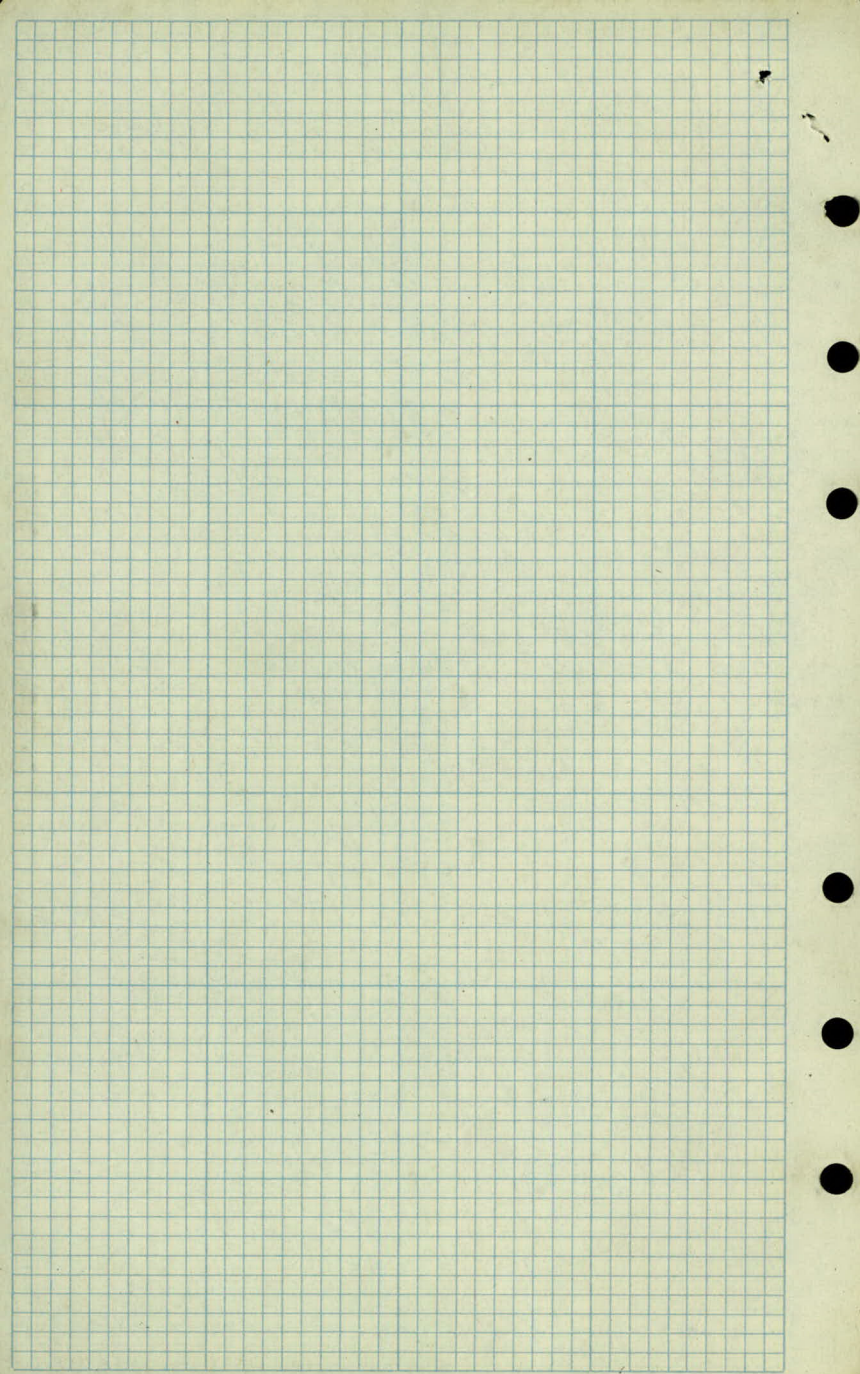
Mud

5-

Sand

Locations

Wakefield Park



E Frost Ave.

14 Aug 1952
Krisera
Clark
Banister

Backstop { + 47 62'
+ 65 71' & 79'

+ 62 Beg Parking Rail 41.5

7720 Backing Lot Fe P.L. 43'

8+20 End Parking Area Pests 95

8+54 Swings 93' to 117'

8+57 Fire place 129'

8+50 Climbing Bars 152'

8+40 6.55 Slide 1.79

8+40 6.50 Textoter 200-214

8+64 Fire place 170

+ 19 Beg 29" SCP Ent Cul. 24' 83' long

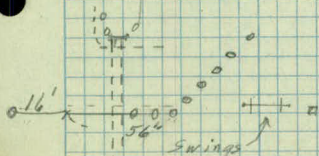
+ 20 End Parking Area Fe 24'

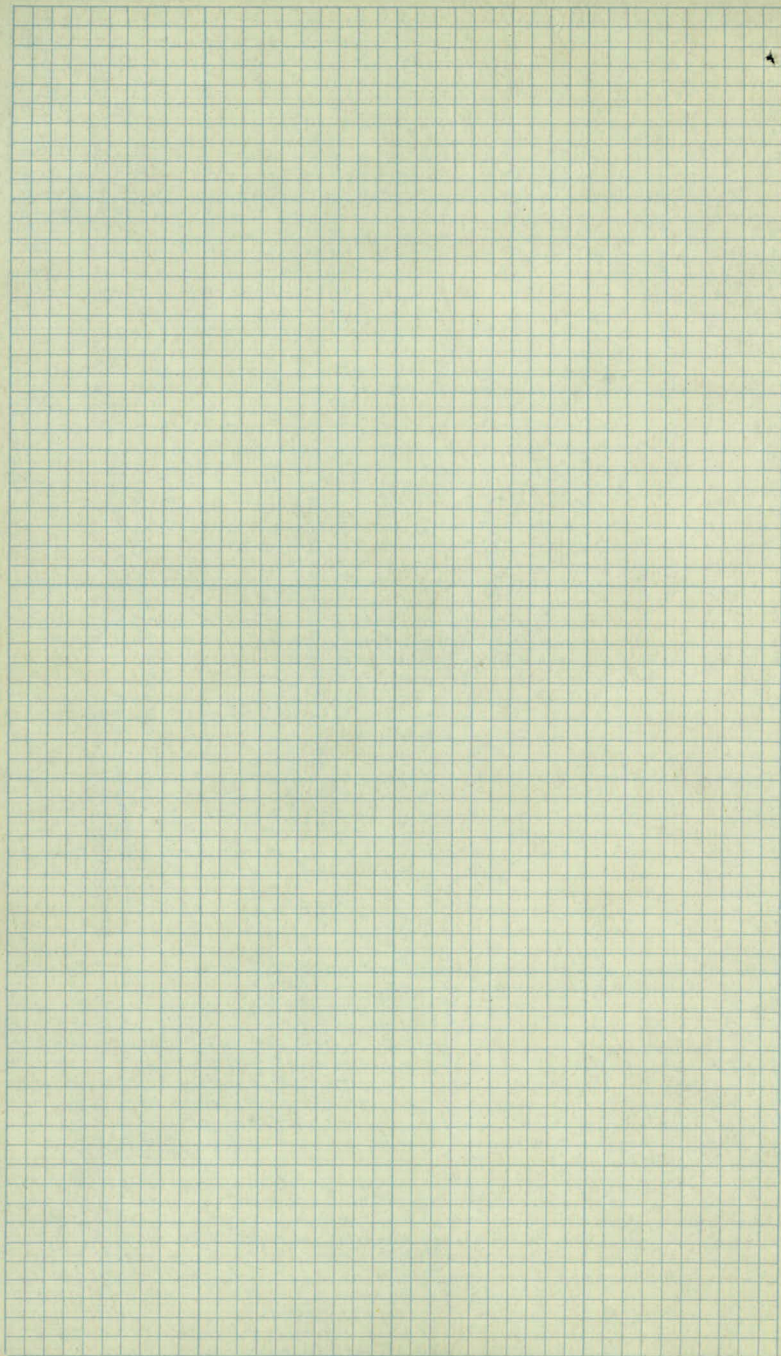
+ 25 Beg Ent

+ 55 End Ent

+ 61 X Guard Rail

Hazelnut





Bench for Lake Elev.

Wakefield Lake.

Sta	+	-	Elev.	
BM	0.24	908.04	907.80	
BM		8.48	899.56	
BM	2.35	923.65	921.30	
TP	0.65	910.88	13.42	910.23
TP	2.56	901.87	11.57	899.31
	1.56	894.07	9.36	892.51
BM		5.49	888.58	
Lake elev.		11.47	882.66	June 21
A "C"		7.91	886.16	
TP	12.27	906.25	0.09	893.98
	10.69	914.47	2.47	903.78
	8.70	922.88	0.29	914.18
BM		1.58	921.30	
BM	1.97	890.55	888.58	
Lake Elev.		8.09	882.46	June 28
BM	1.58	890.16	888.58	
Lake		7.75	882.41	June 30

Spk in P.P. S.E. cor. Frost & Prosperity
painted 4 @ Mont. Ctr. Sec 15

200' E W of Prosperity
Spk in 15" Scrub oak, SW Cor. Prosperity & Larpenteur

} Spk in 10" cot. 60' S. of Lake, 40' west of sec line

Spk in 15' scrub oak SW. Cor. Prosp. & Larpenteur

Sta	+	π	-	Elev
BM	1.18	889.76		888.58
Lake Elev.			7.55	882.21
LAKE. ELEV	1.12	889.70	7.53	882.17
Lake Elev	2.93	891.51	9.58	881.93
"	4.12	892.70	10.92	881.78
Lake Elev.	7.41	889.99	7.73	882.21
Lake Elev	2.34	890.92	8.93	881.99
Lake Elev	1.60	890.18	8.49	881.69

July-5

July-7

July-18

July-22

July-29

Aug-9

Aug-24.

Note 3.3" rain
7-27-49

