

BK. 57 Dr. 12 A

F COUNTY ENGINEER
RAMSEY CO. MINN.

Plan Survey

..... Jackson Street

From Larpenteur Av. To Co. Rd. "A2"

Road Acc't. No.

Filed 5-31-49

File

PLAN SURVEY

JACKSON STREET

LARPEUR TO COR A-2

3/2/49

Rec'd

Alignment

Bench levels page 2

X Sections " 3

Topography " 16

Stadia Topog. " 23

26+33.80

Ctn Sec 18 - T29 - R22W

7+79

Approx $\frac{1}{4}$ Dion St.

0+00 = $S\frac{1}{4}$ cor. Sec 18 T-29 R 22W

Cold-windy-Snowing

2/24/49

GB
AM
MB
DC

stone Mont.
center Sec 18



Co Rd A-2

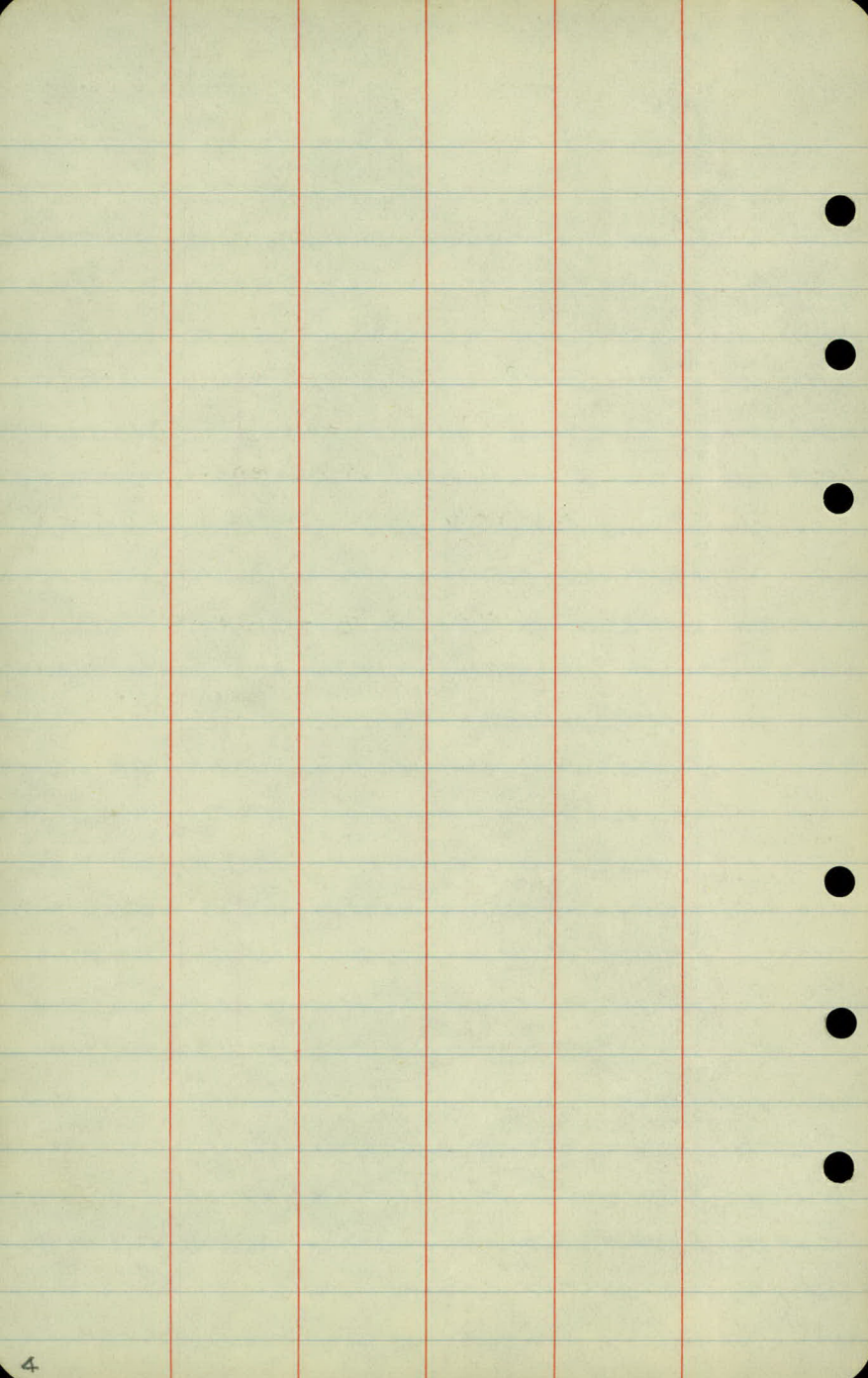
← 89° 11' 15" →



← 89° 10' →



Larpenteur Ave



Jackson St.

X Sections

Larpenteur to Co Rd A-2

Sta	+	π	-	Elev
BM	5.92	891.13		885.21
-0+05		approx $\frac{1}{2}$ Larpeur		88.0
-0+50				86.5
-1+00				85.7
-1+50				86.0
0+00				87.8
+08		shoulder		87.2
+13		ditch		86.7
+25				85.6

2-28-49
GB MB
AM B.C.

(3)

Lt

£

R.T.

NE cor. Bottom Step 1701 Jackson

-3.1

4.6

5.4

5.1

$\frac{13.4}{200}$ $\frac{10.8}{150}$ $\frac{7.8}{100}$ $\frac{5.3}{50}$ 3.3 $\frac{1.7}{50}$ $\frac{0.7}{700}$ $\frac{0.5}{150}$ $\frac{1.6}{200}$ ✓

5.6 $\frac{4.6}{25}$ $\frac{4.5}{16}$ 3.9 $\frac{3.3}{16}$ $\frac{2.4}{35}$ $\frac{2.0}{50}$ ✓

$\frac{5.2}{50}$ $\frac{4.7}{40}$ $\frac{4.3}{20}$ $\frac{5.1}{15}$ 4.4 $\frac{4.4}{14}$ $\frac{5.8}{22}$ $\frac{2.1}{29}$ $\frac{1.6}{50}$ ✓

$\frac{5.5}{50}$ $\frac{4.9}{28}$ $\frac{5.4}{20}$ $\frac{5.6}{13}$ 5.5 $\frac{5.7}{14}$ $\frac{5.6}{22}$ $\frac{2.5}{32}$ $\frac{1.7}{50}$ ✓

Sta + π - Elev

891.13

0 +30

85.0

+50

83.0

+81

80.2

+82

1 +00

78.9

TR 50 3.08 880.47 13.74 877.39

+ 50

76.1

2 +00

74.6

Lt

L

Rt

$$\begin{array}{r} 60 \\ 50 \end{array} \quad \begin{array}{r} 5.5 \\ 26 \end{array} \quad \begin{array}{r} 6.1 \\ 15 \end{array} \quad \begin{array}{r} 6.6 \\ 09 \end{array} \quad 41 \quad \begin{array}{r} 6.5 \\ 14 \end{array} \quad \begin{array}{r} 6.3 \\ 21 \end{array} \quad \begin{array}{r} 5.0 \\ 26 \end{array} \quad \begin{array}{r} 4.9 \\ 12 \end{array} \quad \begin{array}{r} 4.0 \\ 50 \end{array}$$

$$\begin{array}{r} 6.4 \\ 40.47 \end{array} \quad \begin{array}{r} 6.4 \\ 33 \end{array} \quad \begin{array}{r} 8.3 \\ 30 \end{array} \quad \begin{array}{r} 8.0 \\ 14 \end{array} \quad \begin{array}{r} 8.3 \\ 08 \end{array} \quad 8.1 \quad \begin{array}{r} 8.2 \\ 15 \end{array} \quad \begin{array}{r} 7.80 \\ 22 \end{array} \quad \begin{array}{r} 6.9 \\ 32 \end{array} \quad \begin{array}{r} 6.0 \\ 50 \end{array} \quad \begin{array}{r} 5.2 \\ 53 \end{array} \quad \begin{array}{r} 0.6 \\ 40 \end{array}$$

$$\begin{array}{r} 6.5 \\ 50 \end{array} \quad \begin{array}{r} 6.8 \\ 37 \end{array} \quad \begin{array}{r} 9.7 \\ 28 \end{array} \quad \begin{array}{r} 11.3 \\ 07 \end{array} \quad 10.9 \quad \begin{array}{r} 10.8 \\ 4 \end{array} \quad \begin{array}{r} 10.7 \\ 17 \end{array} \quad \begin{array}{r} 10.3 \\ 23 \end{array} \quad \begin{array}{r} 9.8 \\ 33 \end{array} \quad \begin{array}{r} 7.5 \\ 50 \end{array}$$

Gr

$$\begin{array}{r} 80.3 \\ 10.8 \\ \text{Gar Ent. } 37. \end{array} \quad \begin{array}{r} 11.7 \\ 28 \end{array}$$

$$\begin{array}{r} 11.6? \\ 12.5 \\ 50 \end{array} \quad \begin{array}{r} 11.6 \\ 37 \end{array} \quad \begin{array}{r} 11.8 \\ 13 \end{array}$$

$$12.2 \quad \begin{array}{r} 11.8 \\ 08 \end{array} \quad \begin{array}{r} 11.7 \\ 17 \end{array} \quad \begin{array}{r} 11.8 \\ 22 \end{array} \quad \begin{array}{r} 11.2 \\ 30 \end{array} \quad \begin{array}{r} 8.5 \\ 50 \end{array}$$

$$\begin{array}{r} 14.1 \\ 50 \end{array} \quad \begin{array}{r} 12.2 \\ 36 \end{array} \quad \begin{array}{r} 8.4 \\ 16 \end{array} \quad \begin{array}{r} 4.9 \\ 03 \end{array} \quad 4.4 \quad \begin{array}{r} 3.8 \\ 08 \end{array} \quad \begin{array}{r} 3.7 \\ 18 \end{array} \quad \begin{array}{r} 3.4 \\ 23 \end{array} \quad \begin{array}{r} 2.7 \\ 33 \end{array} \quad \begin{array}{r} 0.0 \\ 50 \end{array}$$

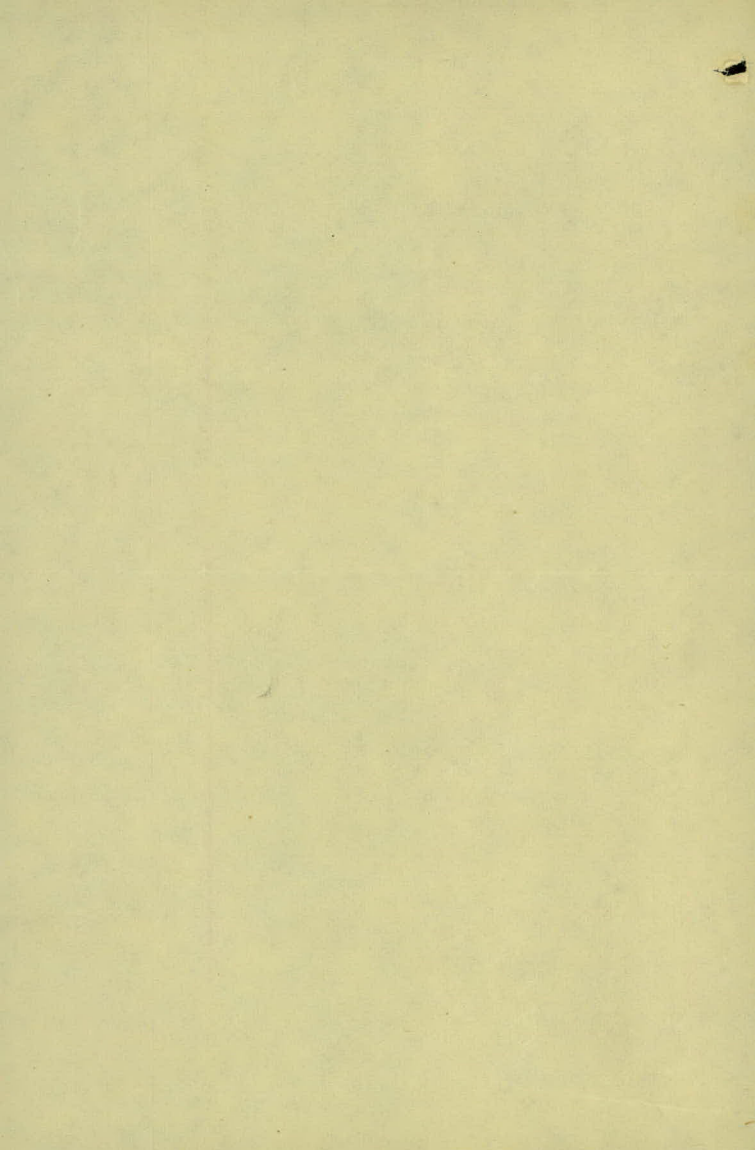
$$\begin{array}{r} 19.0 \\ 50 \end{array} \quad \begin{array}{r} 18.8 \\ 45 \end{array} \quad \begin{array}{r} 15.5 \\ 27 \end{array} \quad \begin{array}{r} 10.3 \\ 07 \end{array} \quad \begin{array}{r} 5.9 \\ 01 \end{array} \quad 5.9 \quad \begin{array}{r} 5.5 \\ 11 \end{array} \quad \begin{array}{r} 5.1 \\ 23 \end{array} \quad \begin{array}{r} 5.8 \\ 29 \end{array} \quad \begin{array}{r} 5.3 \\ 44 \end{array} \quad \begin{array}{r} 4.8 \\ 50 \end{array} \quad \checkmark$$

Sta	+	π	-	Elev
		880.47		
2+50				73.9
3+00				74.0
+ 47				75.1
+ 51				73.6
TP BM			0.00	880.47
+ 87				76.1

profile levels of sta 17+37

B.M. Door Sill on Ho. 2075 Jackson

EL 890.85



LT

Q

RT

$\frac{19.4}{50}$	$\frac{18.1}{35}$	$\frac{16.9}{32}$	$\frac{15.5}{18}$	$\frac{6.6}{01}$	$\frac{6.6}{12}$	$\frac{6.2}{25}$	$\frac{6.0}{30}$	$\frac{6.7}{50}$	$\frac{6.6}{50}$
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✓

$\frac{16.4}{50}$	$\frac{16.1}{34}$	$\frac{13.6}{28}$	$\frac{11.7}{12}$	$\frac{6.9}{03}$	$\frac{6.5}{10}$	$\frac{6.5}{24}$	$\frac{6.2}{30}$	$\frac{7.4}{50}$	$\frac{7.9}{50}$
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✓

$\frac{8.9}{50}$	$\frac{8.5}{32}$	$\frac{8.0}{19}$	$\frac{5.5}{0.1}$	$\frac{5.4}{08}$	$\frac{5.3}{12}$	$\frac{5.7}{24}$	$\frac{6.9}{43}$	$\frac{7.9}{43}$	$\frac{8.5}{43}$
------------------	------------------	------------------	-------------------	------------------	------------------	------------------	------------------	------------------	------------------

✓

$\frac{11.5}{50}$	$\frac{12.2}{35}$	$\frac{10.6}{30}$	$\frac{10.2}{21}$	$\frac{8.0}{9}$	$\frac{6.9}{1}$
-------------------	-------------------	-------------------	-------------------	-----------------	-----------------

✓

duplicate

✓

72.8

$\frac{7.7}{51 \& 40}$	$\frac{7.8}{22}$	$\frac{7.9}{17}$	$\frac{4.9}{07}$	$\frac{4.4}{08}$	$\frac{4.3}{21}$	$\frac{4.2}{29}$	$\frac{10.3}{45}$	$\frac{11.2}{50}$	$\frac{14.1}{50}$
------------------------	------------------	------------------	------------------	------------------	------------------	------------------	-------------------	-------------------	-------------------

Edge of Pot

$\frac{15.5}{15.5}$
Ctr. Pot hole

hole

2-28-49

B.

STA	+	π	-	ELEV
BM	7.19	887.66		880.47

4+00				76.6
------	--	--	--	------

+38				78.3
-----	--	--	--	------

+57				79.4
-----	--	--	--	------

+91				81.5
-----	--	--	--	------

5+00				82.1
------	--	--	--	------

+25				83.2
-----	--	--	--	------

+42				83.7
-----	--	--	--	------

+82				84.8
-----	--	--	--	------

Lt.

C

Rt.

12.15
50 12.9 37 14.0 14 11.4 7 11.1 11.0 8 11.5 20 15.9 29 18.6 42 58
edge P.H. ✓

9.8
1 9.8 50 10.6 30 10.0 20 11.1 17 11.1 14 9.3 10 9.3 7 10.0 21 14.8 29 18.8 43 59 edge
Pothole ✓

0.3 0.3 7.0 7.5 9.3 8.4 8.5 8.3 8.2 8.6 8.4 12.6 12.5
50 43 30 21 13 10 3 7 17 23 29 50 ✓

87.7
0.0 0.0 0.4 6.3 6.2 6.2 6.2 6.2 3.9 6.8 9.6
50 64 35 19 7 6 20 28 35 50
(Ho) ✓

+ 0.1 0.4 2.0 6.0 5.3 5.6 5.7 5.9 6.0 3.0 4.4 6.7
50 36 28 17 13 7 13 20 28 34 50 ✓

+0.8 +2.6 0.0 4.0 4.3 4.4 4.5 4.5 5.1 4.5 0.7 +0.3
50 40 29 17 6 10 16 19 28 50
? ✓

+6.4 +6.9 +9.0 3.9 4.2 4.2 4.0 3.9 4.6 3.7 +6.4 +5.4
50 38 19 13 7 06 17 26 42 50
R R ✓

+6.8 +6.8 +7.0 3.7 3.9 3.3 2.9 2.8 3.3 2.7 +9.6 +9.6
50 40 33 22 16 9 5 20 26 46 50
13 ✓

STA	+	π	-	Elev
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887.66

6+00

~~2.56~~ ~~885.10~~

T.P.

6+00

6.73

891.83

2.56

885.10

off

13 M

8.56

888.27

(888.29)

+50

85.9

+63

86.1

+67

86.1

+79

ϕ Dion

86.2

7+00

86.3

⑦

L+

Q

R+

(2.6)

+8.1 +7.0
46 50

$\frac{5.2}{6.4 \frac{1}{2} 10}$ $\frac{5.5}{50}$ $\frac{5.0}{28}$ $\frac{7.0}{25}$ $\frac{7.3}{15}$ $\frac{7.0}{8}$ $\frac{6.23}{6.7}$ $\frac{6.6}{7}$ $\frac{6.9}{20}$ $\frac{6.5}{27}$ $\frac{5.2}{32}$

?K

✓

$\frac{8.6}{50}$ $\frac{8.0}{28}$ $\frac{7.1}{16}$

5.9

$\frac{5.9}{7}$

$\frac{5.9}{19}$ $\frac{4.2}{30}$ $\frac{4.0}{50}$

$\frac{8.7}{50}$ $\frac{7.7}{33}$ $\frac{6.3}{14}$

5.7

$\frac{5.7}{08}$

$\frac{5.7}{20}$

$\frac{2.7}{30}$ $\frac{4.3}{50}$

$\frac{7.7}{50}$ $\frac{7.6}{39}$ $\frac{6.3}{17}$ 5.7

↑
Dupl. ?

✓

$\frac{10.8}{200}$ $\frac{9.5}{150}$ $\frac{8.5}{100}$ $\frac{7.4}{50}$

5.6

$\frac{5.5}{20}$

$\frac{4.8}{26}$

$\frac{4.1}{41}$

$\frac{4.0}{50}$

✓

$\frac{7.8}{50}$ $\frac{7.0}{28}$ $\frac{6.5}{12}$ 5.5 5.2 5.3 $\frac{4.9}{24}$ $\frac{4.3}{38}$ $\frac{7.1}{50}$

✓

STA	+	π	-	Elev
		89.83		
7+50				86.3
8+00				85.9
+35				86.0
+77				85.9
9+00				85.4
+23				85.4
+68				83.7

Lt

Q

Rt

$\frac{9.3}{114}$ $\frac{8.0}{50}$ $\frac{6.7}{21}$ $\frac{6.4}{12}$ 5 5.5 $\frac{5.1}{12}$ $\frac{4.9}{23}$ $\frac{4.5}{29}$ $\frac{3.8}{33}$ $\frac{3.9}{50}$ ✓

9.0
130 Garage

$\frac{7.6}{50}$ $\frac{7.3}{25}$ $\frac{6.8}{12}$ 5.9 $\frac{5.2}{11}$ $\frac{5.3}{23}$ $\frac{5.1}{26}$ $\frac{4.1}{30}$ $\frac{4.2}{50}$ ✓

$\frac{6.0}{50}$ $\frac{6.0}{26}$ $\frac{5.8}{06}$ 5.8 $\frac{5.6}{04}$ $\frac{5.2}{13}$ $\frac{5.5}{25}$ $\frac{4.4}{29}$ $\frac{3.9}{35}$ $\frac{4.4}{50}$ ✓

$\frac{0.3}{50}$ $\frac{1.4}{33}$ $\frac{2.4}{10}$ $\frac{4.1}{06}$ $\frac{6.0}{03}$ 5.9 $\frac{4.1}{4}$ $\frac{5.8}{13}$ $\frac{6.2}{25}$ $\frac{3.5}{35}$ $\frac{7.5}{50}$ ✓

$\frac{+4.0}{50}$ $\frac{0.7}{28}$ $\frac{1.3}{10}$ $\frac{6.4}{5}$ 6.4 $\frac{6.6}{04}$ $\frac{6.3}{14}$ $\frac{6.7}{23}$ $\frac{5.7}{31}$ $\frac{3.6}{35}$ $\frac{5.0}{50}$ ✓

$\frac{0.6}{50}$ $\frac{1.3}{25}$ $\frac{1.6}{13}$ $\frac{0.8}{10}$ $\frac{1.1}{5}$ 6.4 $\frac{7.3}{03}$ $\frac{6.4}{14}$ $\frac{7.3}{26}$ $\frac{6.5}{32}$ $\frac{4.9}{34}$ $\frac{6.1}{50}$ $\frac{6.7}{100}$ ✓

$\frac{6.1}{50}$ $\frac{6.7}{30}$ $\frac{6.1}{16}$ $\frac{6.0}{5}$ 8.1 $\frac{8.6}{8}$ $\frac{7.9}{16}$ $\frac{8.3}{29}$ $\frac{7.8}{37}$ $\frac{8.2}{50}$ ✓

Sta + π - Elev

891.83

10 83.0

+50 82.0

11 82.4

TP. 

11 + 50 8.53 891.03 9.33 882.50 83.6 ?

12 + 00 84.5

+50 84.9 

13 85.1

+50 84.8

L+

C

R+

$$\frac{9.3}{50} \frac{9.1}{30} \frac{8.5}{9} \frac{9.2}{5} 8.8$$

$$\frac{8.9}{4} \frac{8.6}{14} \frac{8.8}{21} \frac{8.4}{32} \frac{8.6}{50}$$

$$\frac{11.9}{50} \frac{11.5}{30} \frac{10.8}{11} \frac{10.2}{3} 9.8$$

$$\frac{9.6}{12} \frac{9.1}{21} \frac{8.4}{36} \frac{8.6}{50} \frac{8.6}{100}$$

882.43

$$\frac{11.8}{50} \frac{11.4}{33} \frac{10.3}{10} 9.4$$

$$\frac{8.5}{13} \frac{8.7}{24} \frac{8.1}{36} \frac{8.1}{50}$$

$$\frac{9.9}{50} \frac{9.1}{21} \frac{7.9}{8} 7.4$$

$$\frac{6.9}{13} \frac{7.2}{26} \frac{5.9}{33} \frac{6.2}{50}$$

884.53

$$\frac{9.8}{50} \frac{8.8}{32} \frac{7.7}{10} \frac{7.1}{5} 6.5$$

$$\frac{5.8}{13} \frac{6.2}{27} \frac{4.0}{32} \frac{4.1}{50}$$

$$\frac{10.5}{50} \frac{9.3}{29} \frac{7.7}{9}$$

$$6.1 \frac{5.3}{13} \frac{5.5}{27} \frac{3.6}{33} \frac{3.1}{50} \frac{0.0}{80}$$

$$\frac{10.3}{50} \frac{9.2}{30} \frac{8.2}{10} 5.9$$

$$\frac{5.0}{12} \frac{5.3}{25} \frac{5.0}{28} \frac{3.1}{34} \frac{2.4}{50}$$

$$\frac{9.7}{50} \frac{8.7}{29} \frac{10.3}{15} \frac{10.0}{0.8}$$

$$6.2 \frac{5.2}{13} \frac{5.6}{24} \frac{5.3}{30} \frac{3.6}{36} \frac{1.8}{50} \frac{0.0}{80}$$

Sta + π - Elev

891.03

14 83.6

+50

82.9

15 82.4

+50

82.2

16 82.4

+30

82.4

+50

82.4

B.M.

5.45

899.03

7.45

883.58

17 82.3

LT

C

RT

$$\begin{array}{r} 10.3 \\ 50 \end{array} \quad \begin{array}{r} 10.1 \\ 32 \end{array} \quad \begin{array}{r} 9.0 \\ 15 \end{array} \quad \begin{array}{r} 9.1 \\ 7 \end{array} \quad 7.4$$

$$\begin{array}{r} 6.5 \\ 12 \end{array} \quad \begin{array}{r} 6.8 \\ 24 \end{array} \quad \begin{array}{r} 5.5 \\ 30 \end{array} \quad \begin{array}{r} 3.8 \\ 35 \end{array} \quad \begin{array}{r} 3.1 \\ 50 \end{array} \quad \begin{array}{r} 0.0 \\ 60 \end{array}$$

$$\begin{array}{r} 10.1 \\ 50 \end{array} \quad \begin{array}{r} 10.9 \\ 25 \end{array} \quad \begin{array}{r} 9.8 \\ 14 \end{array}$$

$$8.1 \quad \begin{array}{r} 7.5 \\ 11 \end{array} \quad \begin{array}{r} 7.6 \\ 24 \end{array} \quad \begin{array}{r} 7.1 \\ 27 \end{array} \quad \begin{array}{r} 6.2 \\ 30 \end{array} \quad \begin{array}{r} 5.2 \\ 34 \end{array} \quad \begin{array}{r} 4.2 \\ 50 \end{array}$$

$$\begin{array}{r} 9.2 \\ 50 \end{array} \quad \begin{array}{r} 9.8 \\ 30 \end{array} \quad \begin{array}{r} 9.8 \\ 11 \end{array} \quad \begin{array}{r} 8.9 \\ 2 \end{array} \quad 8.6 \quad \begin{array}{r} 8.0 \\ 10 \end{array} \quad \begin{array}{r} 8.1 \\ 24 \end{array} \quad \begin{array}{r} 7.8 \\ 27 \end{array} \quad \begin{array}{r} 7.1 \\ 31 \end{array} \quad \begin{array}{r} 6.8 \\ 50 \end{array} \quad \begin{array}{r} 4.2 \\ 100 \end{array}$$

$$\begin{array}{r} 7.9 \\ 50 \end{array} \quad \begin{array}{r} 9.2 \\ 23 \end{array} \quad \begin{array}{r} 9.6 \\ 8 \end{array} \quad 8.8 \quad \begin{array}{r} 8.4 \\ 9 \end{array} \quad \begin{array}{r} 8.8 \\ 23 \end{array} \quad \begin{array}{r} 8.0 \\ 29 \end{array} \quad \begin{array}{r} 7.7 \\ 50 \end{array}$$

$$\begin{array}{r} 1.0 \\ 112 \end{array} \quad \begin{array}{r} 6.4 \\ 50 \end{array} \quad \begin{array}{r} 8.6 \\ 26 \end{array} \quad \begin{array}{r} 9.7 \\ 17 \end{array} \quad \begin{array}{r} 9.1 \\ 7 \end{array} \quad 8.6 \quad \begin{array}{r} 8.3 \\ 7 \end{array} \quad \begin{array}{r} 8.6 \\ 15 \end{array} \quad \begin{array}{r} 8.9 \\ 23 \end{array} \quad \begin{array}{r} 8.3 \\ 28 \end{array} \quad \begin{array}{r} 8.1 \\ 50 \end{array}$$

$$\begin{array}{r} 6.1 \\ 50 \end{array} \quad \begin{array}{r} 8.3 \\ 23 \end{array} \quad \begin{array}{r} 9.3 \\ 9 \end{array} \quad 8.6 \quad \begin{array}{r} 8.3 \\ 7 \end{array} \quad \begin{array}{r} 8.9 \\ 18 \end{array} \quad \begin{array}{r} 8.4 \\ 30 \end{array} \quad \begin{array}{r} 8.3 \\ 50 \end{array}$$

$$\begin{array}{r} 8.8 \\ 50 \end{array} \quad \begin{array}{r} 9.2 \\ 35 \end{array} \quad \begin{array}{r} 9.4 \\ 21 \end{array} \quad \begin{array}{r} 9.2 \\ 9 \end{array} \quad 8.6 \quad \begin{array}{r} 8.3 \\ 6 \end{array} \quad \begin{array}{r} 8.9 \\ 20 \end{array} \quad \begin{array}{r} 8.1 \\ 26 \end{array} \quad \begin{array}{r} 8.4 \\ 50 \end{array} \quad \begin{array}{r} 8.0 \\ 100 \end{array}$$

SpK PP # 3765 rt @ 17+20

$$\begin{array}{r} 7.7 \\ 50 \end{array} \quad \begin{array}{r} 7.3 \\ 34 \end{array} \quad \begin{array}{r} 7.2 \\ 18 \end{array} \quad \begin{array}{r} 7.0 \\ 9 \end{array} \quad 6.7 \quad \begin{array}{r} 6.6 \\ 06 \end{array} \quad \begin{array}{r} 6.9 \\ 17 \end{array} \quad \begin{array}{r} 6.5 \\ 21 \end{array} \quad \begin{array}{r} 6.7 \\ 38 \end{array} \quad \begin{array}{r} 6.7 \\ 50 \end{array}$$

Sta	+	π	-	Elev
-----	---	-------	---	------

		889.03		
--	--	--------	--	--

+ 50				
------	--	--	--	--

				82.3
--	--	--	--	------

18 + 00				
---------	--	--	--	--

				82.5
--	--	--	--	------

+ 50				
------	--	--	--	--

				82.7
--	--	--	--	------

19				
----	--	--	--	--

				82.8
--	--	--	--	------

+ 50				
------	--	--	--	--

				83.3
--	--	--	--	------

+ 69				
------	--	--	--	--

				83.4
--	--	--	--	------

+ 76				
------	--	--	--	--

		S Side Cattle lane		83.6
--	--	--------------------	--	------

+ 83				
------	--	--	--	--

		No. Side Cattle Lane		83.6
--	--	----------------------	--	------

Lt

C

Rt

$$\begin{array}{r} 6.7 \\ 50 \end{array} \quad \begin{array}{r} 6.8 \\ 38 \end{array} \quad \begin{array}{r} 6.8 \\ 18 \end{array} \quad \begin{array}{r} 6.9 \\ 9 \end{array} \quad 6.7 \quad \begin{array}{r} 6.6 \\ 5 \end{array} \quad \begin{array}{r} 6.9 \\ 17 \end{array} \quad \begin{array}{r} 6.7 \\ 24 \end{array} \quad \begin{array}{r} 6.9 \\ 33 \end{array} \quad \begin{array}{r} 7.0 \\ 50 \end{array} \quad \begin{array}{r} 7.1 \\ 100 \end{array}$$

$$\begin{array}{r} 7.1 \\ 50 \end{array} \quad \begin{array}{r} 6.9 \\ 31 \end{array} \quad \begin{array}{r} 6.8 \\ 18 \end{array} \quad \begin{array}{r} 6.8 \\ 11 \end{array} \quad 6.5 \quad \begin{array}{r} 6.8 \\ 14 \end{array} \quad \begin{array}{r} 6.4 \\ 21 \end{array} \quad \begin{array}{r} 6.8 \\ 28 \end{array} \quad \begin{array}{r} 6.7 \\ 50 \end{array}$$

$$\begin{array}{r} 6.2 \\ 50 \end{array} \quad \begin{array}{r} 6.2 \\ 39 \end{array} \quad \begin{array}{r} 6.1 \\ 21 \end{array} \quad \begin{array}{r} 6.6 \\ 10 \end{array} \quad 6.3 \quad \begin{array}{r} 6.6 \\ 15 \end{array} \quad \begin{array}{r} 6.0 \\ 18 \end{array} \quad \begin{array}{r} 6.3 \\ 23 \end{array} \quad \begin{array}{r} 6.5 \\ 28 \end{array} \quad \begin{array}{r} 6.8 \\ 50 \end{array}$$

882.83

$$\begin{array}{r} 7.0 \\ 50 \end{array} \quad \begin{array}{r} 6.7 \\ 32 \end{array} \quad \begin{array}{r} 6.3 \\ 20 \end{array} \quad \begin{array}{r} 6.3 \\ 12 \end{array} \quad 6.2 \quad \begin{array}{r} 6.2 \\ 14 \end{array} \quad \begin{array}{r} 6.0 \\ 15 \end{array} \quad \begin{array}{r} 6.2 \\ 23 \end{array} \quad \begin{array}{r} 6.6 \\ 40 \end{array} \quad \begin{array}{r} 6.7 \\ 50 \end{array}$$

$$\begin{array}{r} 6.3 \\ 50 \end{array} \quad \begin{array}{r} 6.1 \\ 30 \end{array} \quad \begin{array}{r} 5.6 \\ 21 \end{array} \quad \begin{array}{r} 6.0 \\ 12 \end{array} \quad 5.7 \quad \begin{array}{r} 5.8 \\ 9 \end{array} \quad \begin{array}{r} 5.4 \\ 14 \end{array} \quad \begin{array}{r} 5.8 \\ 20 \end{array} \quad \begin{array}{r} 6.2 \\ 26 \end{array} \quad \begin{array}{r} 6.5 \\ 50 \end{array}$$

$$\text{dupl. + 76} \quad 5.6 \quad \begin{array}{r} 5.7 \\ 12 \end{array} \quad \begin{array}{r} 5.3 \\ 14 \end{array} \quad \begin{array}{r} 5.3 \\ 16 \end{array} \quad \begin{array}{r} 5.5 \\ 22 \end{array} \quad \begin{array}{r} 5.9 \\ 50 \end{array}$$

$$\begin{array}{r} 5.6 \\ 50 \end{array} \quad \begin{array}{r} 5.5 \\ 33 \end{array} \quad \begin{array}{r} 5.0 \\ 21 \end{array} \quad \begin{array}{r} 5.7 \\ 14 \end{array} \quad 5.4 \quad \begin{array}{r} 5.4 \\ 13 \end{array} \quad \begin{array}{r} 4.8 \\ 15 \end{array} \quad \begin{array}{r} 4.8 \\ 18 \end{array} \quad \begin{array}{r} 4.6 \\ 50 \end{array}$$

dupl. + 76

dupl. + 76

Sta + π - Elev

889.03

19 + 88

83.7

20

83.9

+ 50

84.6

21

85.4

+ 50

86.3

TP 6.96 893.55 2.44 886.59

BM

2.71 890.84

890.85

(12)

Lx

E

$\frac{5.3}{50}$ $\frac{5.1}{30}$ $\frac{4.4}{24}$ $\frac{4.9}{18}$ $\frac{5.6}{11}$ 5.3 $\frac{5.3}{12}$ $\frac{5.6}{14}$ $\frac{4.7}{26}$ $\frac{5.9}{39}$ $\frac{5.7}{50}$

$\frac{4.8}{50}$ $\frac{4.9}{31}$ $\frac{4.4}{22}$ $\frac{5.1}{16}$ $\frac{5.3}{10}$ 5.1 $\frac{5.3}{11}$ $\frac{4.5}{14}$ $\frac{4.7}{24}$ $\frac{6.0}{32}$ $\frac{5.6}{50}$

$\frac{3.5}{50}$ $\frac{3.5}{21}$ $\frac{4.3}{16}$ $\frac{4.5}{10}$ 4.4

$\frac{4.4}{12}$ $\frac{4.6}{23}$ $\frac{5.4}{26}$ $\frac{5.7}{50}$

$\frac{2.8}{50}$ $\frac{3.1}{37}$ $\frac{2.7}{24}$ $\frac{3.1}{14}$ $\frac{3.6}{13}$ 3.6 $\frac{3.8}{11}$ $\frac{3.5}{13}$ $\frac{4.4}{15}$ $\frac{4.2}{24}$ $\frac{4.7}{33}$ $\frac{4.9}{50}$

$\frac{1.7}{50}$ $\frac{2.0}{42}$ $\frac{2.1}{28}$ $\frac{1.6}{23}$ $\frac{1.9}{20}$ $\frac{2.6}{14}$ 2.7 $\frac{3.1}{10}$ $\frac{2.7}{13}$ $\frac{3.4}{15}$ $\frac{2.9}{22}$ $\frac{3.5}{23}$ $\frac{4.2}{50}$

door Sill on house 2075 Jackson

2-2-49

JB.

Sta	+	$\bar{A}$	-	Elev
B.M.	8.47	899.32		890.85
22+00				87.4
+28				88.2
+31				88.3
+70		⊕ Driveway		89.5 or Rt.
23				90.3
+50				92.0
24				93.4
+50				94.7

RT

Q

LT

door Sill en house 2025 Jackson

$\frac{10.3}{50}$ $\frac{11.0}{27}$ $\frac{10.9}{20}$ $\frac{11.9}{13}$ 11.9 $\frac{12.1}{10}$ $\frac{11.9}{14}$ $\frac{13.4}{17}$ $\frac{13.1}{27}$ $\frac{12.3}{50}$ ✓

$\frac{9.3}{50}$ $\frac{10.4}{25}$ $\frac{10.6}{20}$ $\frac{11.3}{13}$ 11.1 ✗ $\frac{11.4}{10}$ $\frac{11.2}{16}$ $\frac{12.5}{25}$ $\frac{12.1}{50}$ ✓

$\frac{9.2}{50}$ $\frac{10.3}{26}$ $\frac{10.4}{20}$ $\frac{11.2}{13}$ 11.0 $\frac{11.1}{12}$ $\frac{10.7}{14}$ $\frac{11.3}{23}$ $\frac{10.9}{38}$ $\frac{10.7}{50}$ ✓

$\frac{8.0}{50}$ $\frac{9.2}{23}$ $\frac{9.6}{19}$ $\frac{10.2}{12}$ 9.8 $\frac{10.1}{12}$ $\frac{10.2}{32}$ $\frac{10.8}{50}$ ✓

$\frac{7.1}{50}$ $\frac{8.5}{24}$ $\frac{9.2}{17}$ $\frac{9.7}{13}$ 9.0 $\frac{9.9}{12}$ $\frac{9.2}{14}$ $\frac{9.6}{21}$ $\frac{9.7}{38}$ $\frac{9.9}{50 \frac{1}{2} Ho}$ 89.4 ✓

$\frac{5.6}{50}$ $\frac{6.8}{23}$ $\frac{7.5}{17}$ $\frac{8.0}{12}$ 7.3 $\frac{7.5}{12}$ $\frac{7.5}{17}$ $\frac{8.5}{22}$ $\frac{8.8}{30}$ $\frac{9.0}{50}$ ✓

$\frac{4.4}{50}$ $\frac{5.1}{25}$ $\frac{6.1}{17}$ $\frac{6.5}{11}$ 5.9 $\frac{6.6}{15}$ $\frac{6.9}{20}$ $\frac{7.7}{29}$ $\frac{8.2}{50}$ ✓

$\frac{3.3}{50}$ $\frac{4.1}{22}$ $\frac{4.7}{16}$ $\frac{4.9}{9}$ 4.6 $\frac{5.2}{10}$ $\frac{5.7}{16}$ $\frac{6.5}{26}$ $\frac{7.6}{50}$ 27 ✓

Sta	+	π	-	Elev
-----	---	-------	---	------

899.32

24+68

95.2

TP

15+00 TP

8.99

904.92

3.39

895.93

95.9

?

+50

96.2

+85

95.9

26

95.7

+09

95.8

+14

95.7

+18

95.6

Lt

C

Rt

~~1.8~~

$$\begin{array}{cccccccc} \frac{1.1}{50} & \frac{2.9}{55} & \frac{3.3}{22} & \frac{4.3}{16} & \frac{4.6}{11} & 4.1 & \frac{4.9}{13} & \frac{6.6}{25} & \frac{7.6}{50} \end{array}$$

$$\begin{array}{cccccccc} \frac{4.0}{50} & \frac{8.1}{21} & \frac{8.8}{18} & \frac{9.3}{10} & 9.0 & \frac{9.6}{11} & \frac{9.8}{16} & \frac{11.3}{23} & \frac{12.6}{50} \end{array}$$

$$\begin{array}{cccccccc} \frac{1.5}{68} & \frac{2.1}{50} & \frac{4.4}{34} & \frac{7.1}{19} & \frac{8.0}{15} & \frac{8.7}{10} & \frac{9.1}{14} & \frac{9.3}{20} & \frac{11.4}{50} \end{array}$$

$$\begin{array}{cccccccc} \frac{4.2}{50} & \frac{5.9}{31} & \frac{7.5}{18} & \frac{9.2}{10} & 9.0 & \frac{9.2}{11} & \frac{7.7}{19} & \frac{8.8}{38} & \frac{9.7}{50} \end{array}$$

$$\begin{array}{cccccccc} \frac{5.8}{50} & \frac{7.0}{32} & \frac{8.1}{18} & \frac{9.2}{14} & 9.2 & \frac{9.4}{11} & \frac{9.4}{17} & \frac{6.9}{23} & \frac{7.7}{32} & \frac{8.5}{56} \end{array}$$

$$\begin{array}{cccccccc} \frac{7.5}{50} & \frac{8.3}{30} & \frac{8.9}{18} & \frac{9.5}{16} & 9.1 & \frac{9.6}{14} & \frac{9.6}{21} & \frac{6.8}{30} & \frac{8.3}{50} \end{array}$$

$$\begin{array}{cccccccc} \frac{10.2}{50} & \frac{10.3}{43} & \frac{10.9}{33} & \frac{10.17}{23} & \frac{9.5}{17} & 9.2 & \frac{9.4}{12} & \frac{8.7}{23} & \frac{10.30}{24.5} & \frac{10.7}{31} & \frac{10.7}{50} \end{array}$$

Top 18" Conc. Culv. Top 18" Conc. C.

$$\begin{array}{cccccccc} \frac{9.0}{50} & \frac{9.2}{32} & \frac{9.5}{16} & 9.3 & \frac{9.5}{15} & \frac{10.1}{32} & \frac{10.3}{50} \end{array}$$

Sta + π - Elev
904.92

26 +25 S edge Blacktop 95.5

+34 $\frac{1}{2}$ Co Rd A-2 95.5

+41 N. edge Blacktop 95.4

+50 95.1

+51 $\frac{1}{2}$ 53 94.5

55 95.6

69 04.8

27+00 03.2

BM 7.82 897.10 (897.07)

Lt

Q

Rt

$$\frac{8.7}{50}$$

$$\frac{9.0}{31}$$

$$9.4$$

$$9$$

$$\frac{9.8}{27}$$

$$\frac{10.3}{50}$$

$$\frac{7.0}{200}$$

$$\frac{7.4}{150}$$

$$\frac{7.9}{100}$$

$$\frac{8.5}{50}$$

$$9.4$$

$$\frac{10.1}{50}$$

$$\frac{10.6}{100}$$

$$\frac{10.8}{150}$$

$$\frac{11.2}{200}$$

$$9.5$$

$$9.8$$

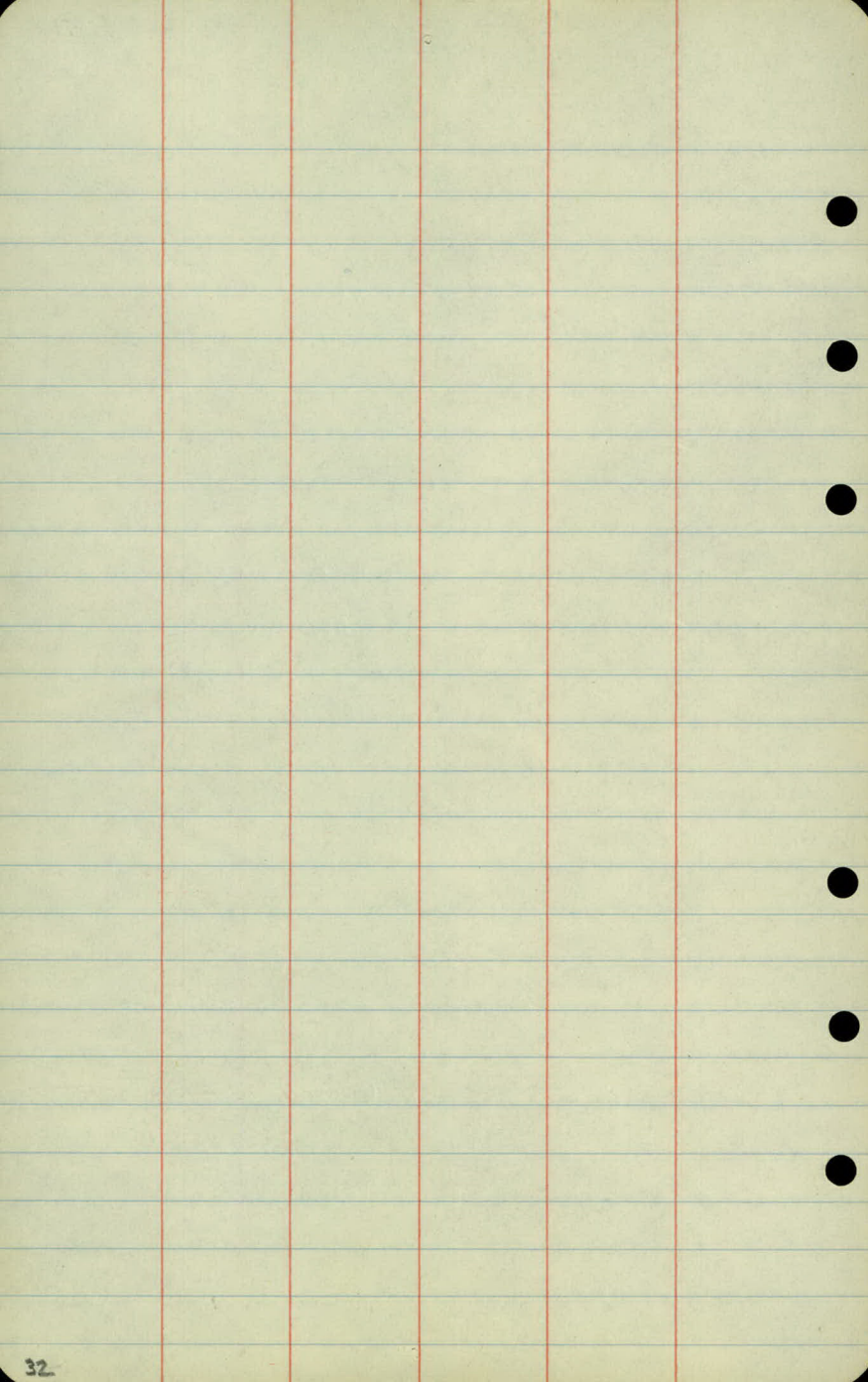
$$10.4$$

$$9.3$$

$$9.1$$

$$1.7$$

Spk in G pole North side of ~~Jackson~~ ^{A 2}
at Jackson st.



Topography

Jackson St
Lorpenieur to Co Rd. A-2

3+00

2 20

+70 End Low land Beg cult.

+69 Group of 42" BE 32'

+62 10" BE 36

+51 10" BE 42

+47 40" BE 32

+05 40" BE 30'

2+00

1 20

+98 end Pathole 170

+98 PP -24'

+80 Pathole 175-225

+86 TP -24'

+73 24" BE 30'

+40 24" BE

+09 24" BE 31'

+00 +08 Beg Pathole 175'

3' 18'

+15 cor. Cult. Field

+03 Apple T ?

+91 Q Ent Drive

+82 SE cor Gar 36

+82 ret wall -29

+45 BE 32

+42 SE cor H 46'

+33 lilac B -33'

+27 end rad 9'

+18 TP -26'

+05 Water Shut off -25'

+06 Shoulder Larpentur, Beg rad. 25'

0+00

+87 Top Rip Rap 66

+87 Toe + Cor Rip Rap 56

+79 pop 56

+63 pop 54

+61 SW cor H 72'

+48 pop 53

+37 Apple T -33

+33 PP -23'

+28 Top of Rip Rap 59

+28 Toe of Rip Rap 52'

+26 Picket E. 31'

+22 End Rad 15'

+06 Beg Rad. 28'

-15 S Shoulder Larpentur

2-25-49

G.B. M.B.
A.M. B.C.

(17)

Cult. Land.

Cult. Land

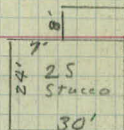
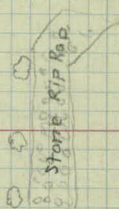
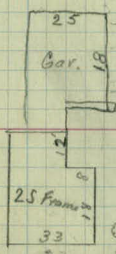
Low Land

O.P.P.

Cult. Land
high

Pot Hole

Apple



P.P.O.

white picket fence

Larpenfour

Stone M.

Ave

T.P.O.

+ 04 TP-22

+ 08 PP 29

9+00

6423

8+00

1' 21'

+ 83 2 Ent

+ 51 TP-23

+ 55 SE cor House 115'

+ 05 PP 61

+ 11 end rad. 4'

242 Field Ent

+ 05 PP 28

7+00

117 17

pt. on rad 11

+ 90 Beg rad. - 35'

+ 79 Approx E Dionst

+ 68 end Rad. - 46'

+ 38 Beg rad 4'

+ 16 TP 23

+ 11 SE cor Basement house 66'

+ 02 6-2" BE 28'

6+00

4 17

+ 99 7-2" BE 38'

+ 90 8-2" BE 30'

+ 77-P-2" scrub BE 29

+ 37 PP - 27

+ 13 2 Ent

+ 01 12" x 20 cm Culv. - 17'

+ 04 8" pop ?

3 15

5+00

+ 84 12" Elm 48 + 80 TP 14'

+ 65 15" Elm 47 + 82 SE cor

+ 41 Twin Pop 45 house 64'

+ 41 end Lilac hedge 34'

+ 24 Group 3" Elm 13 - 7

+ 12 Apple Tree 49

+ 06 Beg. Lilac hedge 34

+ 00 Bush - 43

+ 78 N Edge Pot + hole 136

+ 55 Pot hole 71 1/2 140

+ 00 Pot hole 60 1/2 160

4

+ 96 30" BE 33'

+ 70 SE cor House 51'

+ 65 12" CM 18' } Culvert

+ 41 12" CM 19' }

+ 58 Ctr Ent

+ 42 TP 24

+ 44 Ctr G.A. 39 Toe of rip rap

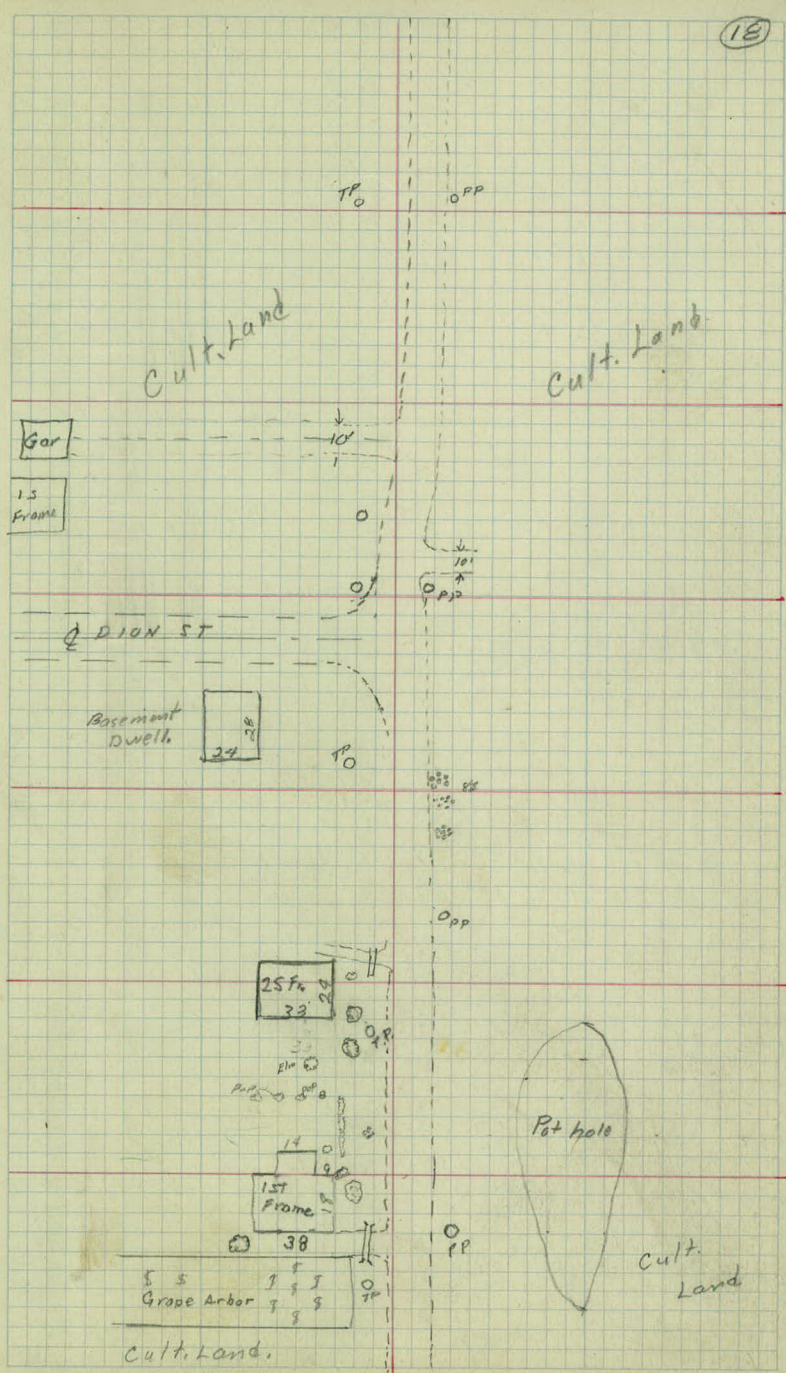
+ 20 Cor Grape A. 40

2 18 + 80 Pot hole 80 1/2 104

+ 68 PP 26

+ 45 S Edge Pot hole 100'

3+00



17 2' 16'

16 +98 PP 21' 2 & 19

+78 SE cor House 111

+60 $\frac{1}{2}$ Ent.

+05 end Cult. Land

+16 PP - 28

15 0 - 19

+05 - TP - 22

14 3 & 21

+70 End Boulder 10'

+28 TP 22

+13 PP - 28

+20 Beg Boulders - 10'

13 4 & 22

12 4 & 23

+87 TP 22'

+10 PP 29

11 4 & 22

+48 T.P. 23

5 - 24

1. S. M.
Frame

32

10'
Drive

Opp.

Cult. Land

1 doz Boulders
 $\frac{1}{4}$ - $\frac{3}{4}$ cu yd. ea.

TP O

Opp

TP O

Opp

TP O

24

10 10

+57 TP 23'

+38 30" RE 17'

+39 PP 28' Beg. cult.
+04 30" BE 47'

23

10 10

+94 L/loc 32'

+80 L/loc 33

+78 SW cor Ho 49

+70 E Ent

+47 end Fe

+42 Apple -50'

+40 10" Apple -26

+30 Tree 18 Cross Fe -16-E

+43 TP -23

22

10 10 Fe. 16

+98 Fe. cor. 26. to 88'

+89 end Op. Arbor 28' & 90'

+61 Beg. Op. Arbor -51 & 28

+60 end orchard 81 & 28

+17 TP 23'

+25 PP-28 - orchard @ 25 & 54

21

10 11 Fe @ 14 & 24

+98 Beg orchard 38

20

11 11 Fe. @ 15 & 26

+88 TP -23'

+85 Fe. cor. 36 ECH - Beg. cult.

+64 S.W. Cor. Ho. - 88
Ground at Ho. - 41. 85. 2

+76 Fe. cor. 15 - end. cult. land

+22 PP-28

19

9 13

+68 TP 23'

18

6 14

+60 Beg Cult

+31 TP 23'

+20 PP-28'

17

10

Cult. Land.

WEEDY Land

TP
O

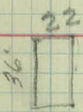
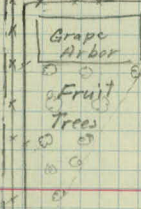
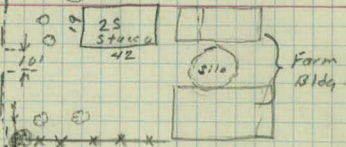
BE
O

TP
O

TP
O

TP
O

TP
O



Cattle lane

PP
O

Cult. Land.

Cult. Land

+42 Wedge Blk, Top

+26 edge Block Top

+23 end Rod 28'

+23 end rod - 33

+16 18" Conc. Culv. 23'

+16 18" Conc. C. 27'

+15 PP-29

+05 PP 29

26

+96 Beg Rod 10'

+96 Beg Rod 10'

+89 TP-21

+27 SE car Ho 69'

25

10 10 Stamp 16

+64 end weeds, Beg lawn

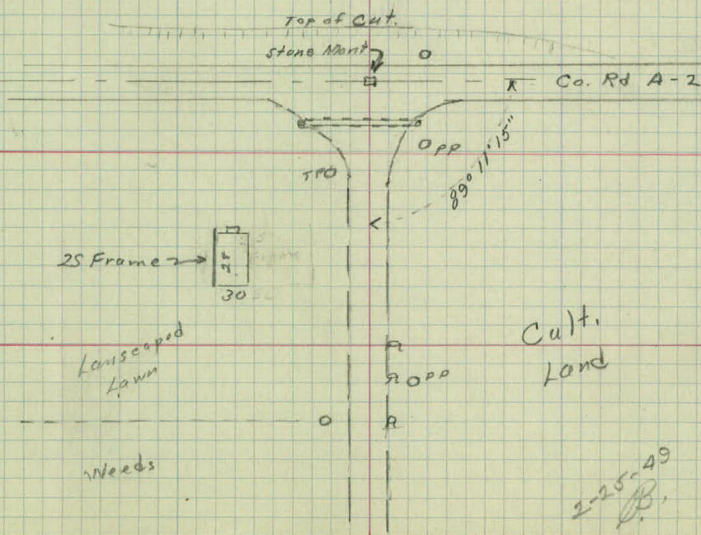
+85 stump 16

+64 TP-23'

+80 PP-28

+64 Stump 16

24



DIST.	VERTI ANGLE	ROD EQUIV.	ROD	DIFF.	ELEV.
-------	----------------	---------------	-----	-------	-------

Stadia topography
Jackson St.

Larpentour to Co Rd. A-2

OBJECT

AZ.

STADIA

@ Sta 11+00

to Mont. Ctr Sec 18

0°00'

G.E

262° 40'

"

271° 30'

1'

262° 20'

"

264° 30'

"

/ 9.3 252° 20'

"

314° 40'

"

343° 30'

AT STA 19+00

To MONT. CTR. SEC 18 =

0° 00'

G.E

/ 12.6 253° 20'

"

/ 11.8 257° 40'

"

/ 11.3 250°

"

/ 11.8 261°

1'

259° 20'

1'

269° 50'

3-3-79
GB
AM
MB
B.C.

23

DIST.	VERT. ANGLE	ROD EQUIV.	ROD	DIFF.	ELEV.
-------	----------------	---------------	-----	-------	-------

H.I. = 887.74 OK

H.I. 5.31

882.43

190'

9.9

877.8

276'

10.3

77.4

410

10.9

76.8

500

11.0

76.7

620

12.4

75.3

180

8.6

79.1

277

7.6

80.1

H.I. = 888.23 OK

H.I. 5.4

882.83

640

15.8

72.4

580

14.7

73.5

376

13.2

75.0

510

14.4

73.8

240

8.5

79.7

116

6.4

81.8

OBJECT

AZI

STADIA

BENCH LEVELS

Co. Rd A-2; McMenemy to
Jackson

Jackson; A-2 to Larpenteur.

STA	+	π	-	Elev.
BM	5.33	917.83		912.50
	1.62	908.70	10.75	907.08
	1.22	896.48	13.44	895.26
	0.52	883.33	13.67	882.81
	9.43	886.75	6.01	877.32
	7.86	894.50	0.11	886.64
	7.14	897.84	3.80	890.70
			0.67	897.17
				897.06
	0.09	895.23	2.60	895.14
BM			4.38	890.85
	2.63	887.57	10.29	884.94
	8.17	891.02	4.72	882.85
	5.48	891.08	5.42	885.60
BM			2.79	888.29
	2.70	882.07	11.71	879.37
	9.02	890.77	0.32	881.75
B.M.			5.56	885.21

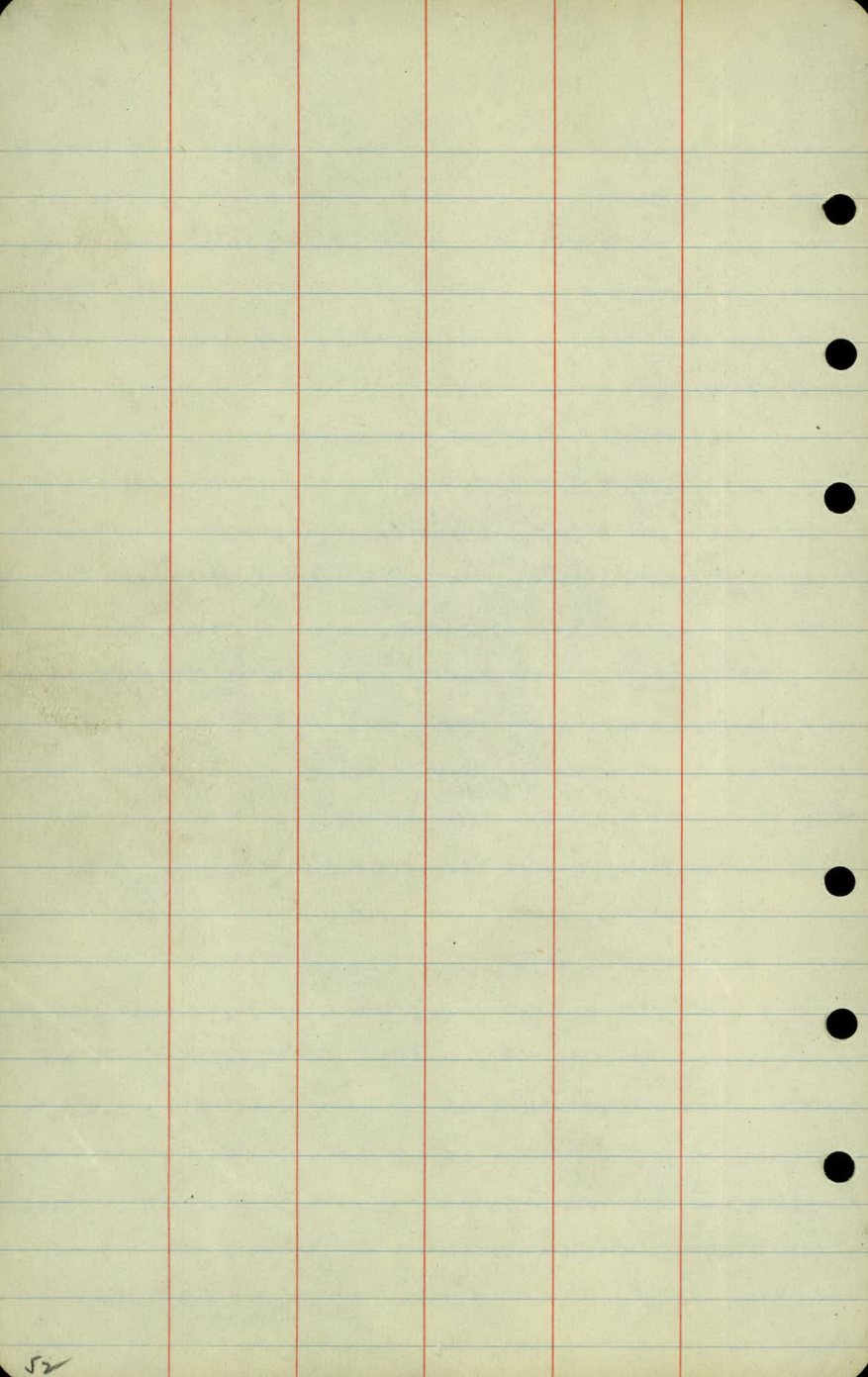
Corrected

{ Top N.W. Cor. Bottom Step of Church
center Entrance 400' E of McMenemy

Spt in G Pole N side of Jackson
to BM on Jackson (ABOVE)
Door sill on House. 2075 Jackson

Spt in P.P. NE Cor Dion St.

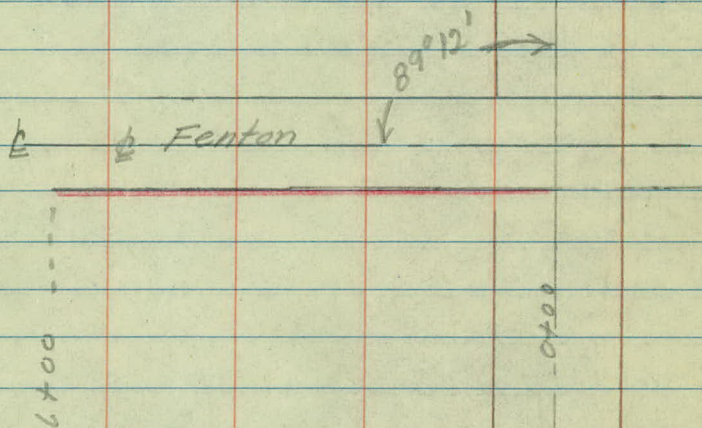
NE Cor Lower Step 1701 Jackson



Profile

Fenton St

Jackson St to 600' ϕ
along So. Prop. Line



4-25-50

GB
AM
MB
K.R.

Sta	+	$\bar{\pi}$	-	Elev
BM	4.55	888.13		883.58
0+00	=	Jackson St @		87.27+31

+06				81.9
-----	--	--	--	------

+08				82.0
-----	--	--	--	------

+24				81.9
-----	--	--	--	------

+50				82.1
-----	--	--	--	------

1				82.3
---	--	--	--	------

+50				82.7
-----	--	--	--	------

2				83.0
---	--	--	--	------

+50				82.3
-----	--	--	--	------

3				80.9
---	--	--	--	------

+50				79.4
-----	--	--	--	------

4				77.4
---	--	--	--	------

¢

Spk in PP #3765 rt @ Sta 17+20

5.9

6.2

6.1

6.2

6.0

5.8

5.4

5.1

5.8

7.2

8.7

10.7

Sta	+	π	-	Elev
-----	---	-------	---	------

888.13

4+50

75.4

5

73.9

+50

73.0

6 = Bottom of draw going into W.W. Prop. 72.5

Bm

4,54 883.59 (883.58)

②

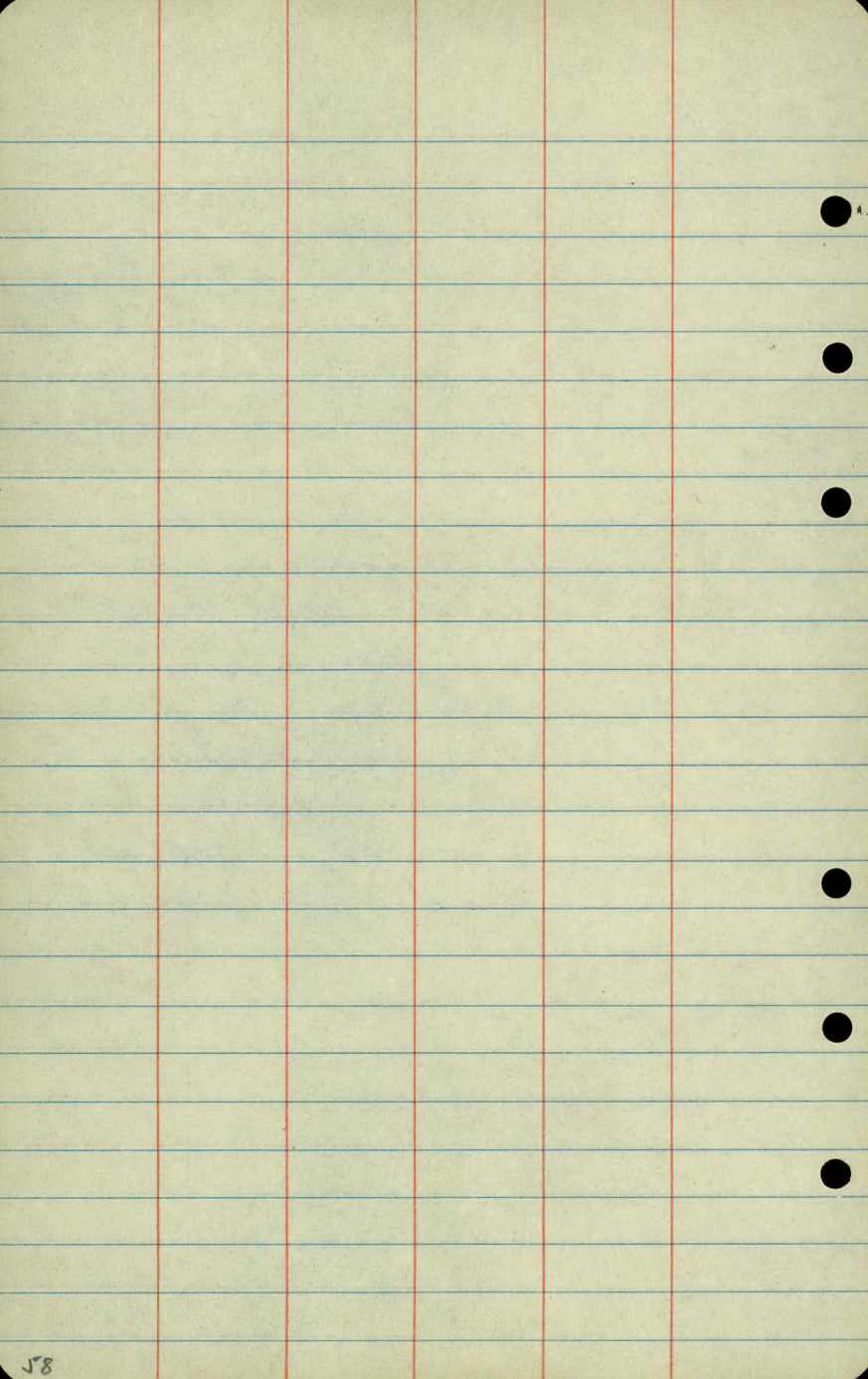
12.7

14.2

15.1

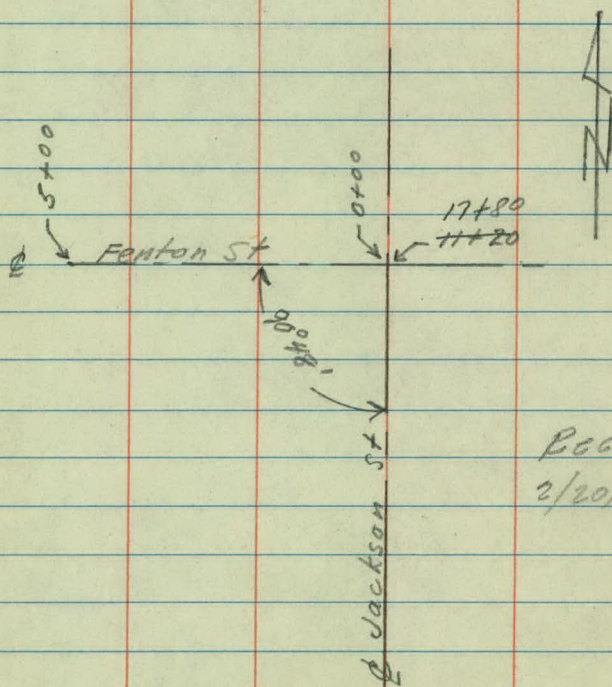
15.6

Spt in RPth 3765 rt@Sta 17+20



1

FENTON ST
Jackson St to 500' West
E Profile
X
Sections



Rec.
2/20/50

Sta	+	π	-	Elev
BM	3.40	886.98		883.58

0+00 = ϕ Jackson St (Sta 17+80) → 82.5

+17 82.3

+50 16 4 81.7

1 81.7

(Pulled up for Snow Plow)

2.60 886.18 883.58

1+50 81.0

2 80.5

+50 Aired oak -30 79.6

3 79.2

Lt

C

Rt

Spk in PP #3965, Rt @ 17+20

4.7
50

4.5

4.3 ✓
504.9
304.8
10

4.7

4.7
104.8 ✓
30

Road 16-4

4.0
305.2
21

5.3

5.4 ✓
10

Road 19-6

4.0
304.1
245.5
21

5.3

5.3 ✓
103.1
295.0
23

5.2

4.0 ✓
10

Road 22-10

3.3
305.5
24

5.7

4.3 ✓
103.9
306.1
23

6.6

5.7 ✓
9

Road 2029

6.0
306.9
23

7.0

8.2 ✓
10

Sta	+	π	-	Elev
		886.18 [✓]		

3+50

78.5

4

77.6

+21

24" cm

77.5

+40

5

77.4

+71

E Rd. Rt. 77.4

+85

24" cm Lt.

+89

77.1

+94

74.5

L4

F

R7

8.2	7.4	7.7	10.7	✓ L.O.
30	21		10	

19-7

9.8	8.4	8.6	11.3	✓ L.O.
30	21		10	

(74.20) ✓ FL 24" CM ✓

11.3	8.9	8.7	11.98	
30	20		11	

11.0	9.2	8.8	8.7	High
30	19		10	

Road - 19

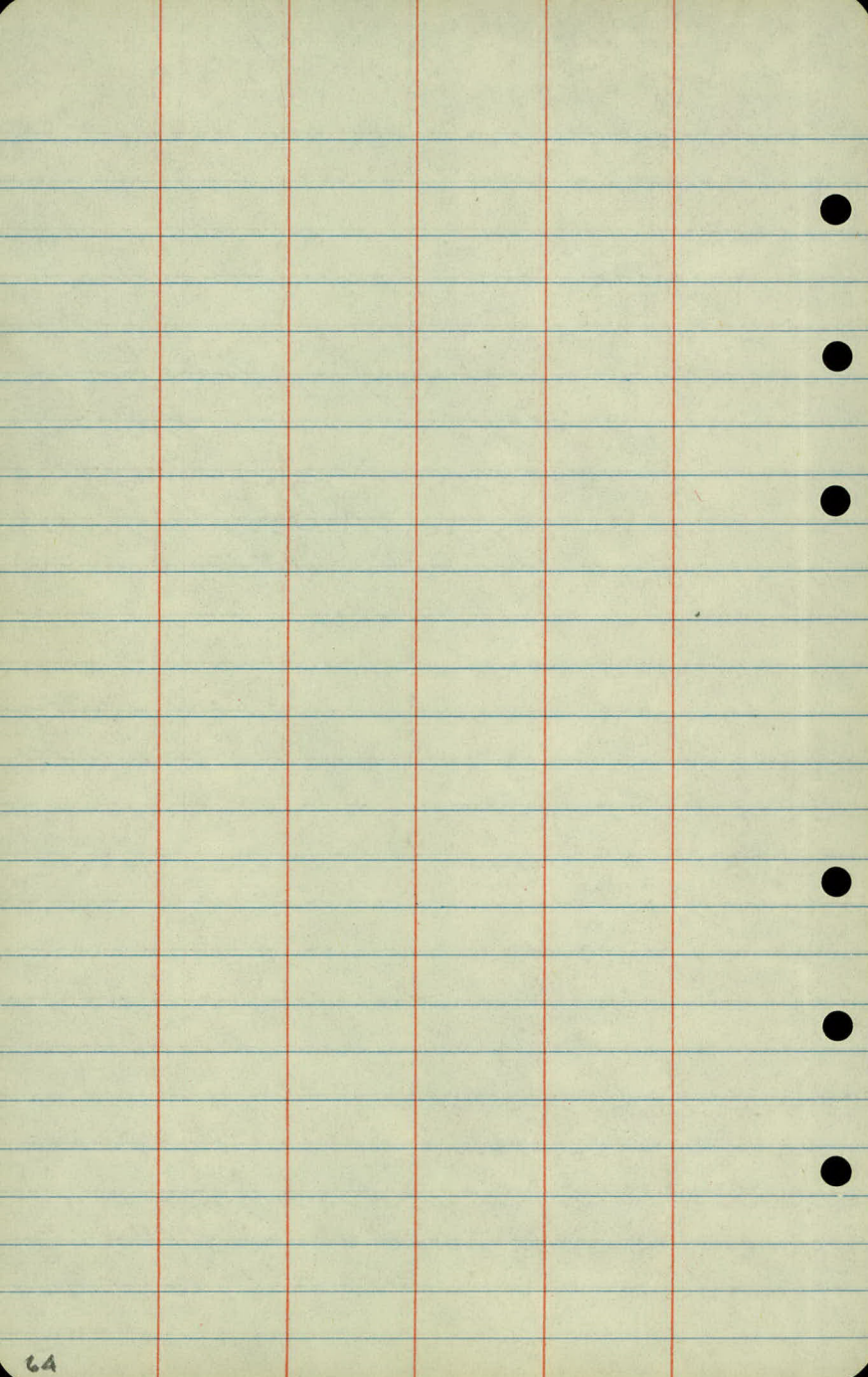
11.9	9.5	8.8	6.8	2.8
30	23		50	100

(13.51) FL-24" CM

12.67
29

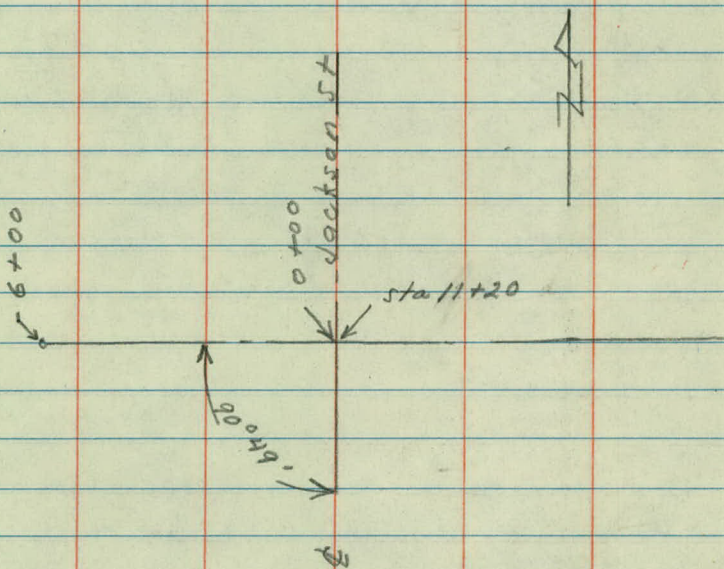
9.1

11.7



1

Profile
on Line
West of Jackson St @ Sta 11+20



Sta	+	π	-	Elev
BM	3.20	888 23		884.53
0+10		Approx Blacktop		83.6
- 3				83.2
0+00				82.9
0 + 7				82.1
+ 25				81.4
+ 53				80.7
1				79.7
+ 50				78.7
2				78.1
+ 50				78.0
3				77.9
+ 50				78.2
4				77.7

¢

Top SpK, Sta 12+00 (Jackson St)

4.6

5.0

5.3

6.1

6.8

7.5

8.5

9.5

10.1

10.2

10.3

10.0

10.5

Sta	+	T	-	Elev
-----	---	---	---	------

		888.23		
--	--	--------	--	--

4+50				
------	--	--	--	--

				77.7
--	--	--	--	------

5				
---	--	--	--	--

				77.9
--	--	--	--	------

4+50				
------	--	--	--	--

				78.3
--	--	--	--	------

6				
---	--	--	--	--

				78.6
--	--	--	--	------

$\frac{1}{2}$

10.5

10.3

9.9

9.6

Sta

+

π

-

Elev

10/12

A.M.

A.C.

K.R.

E.J.

FINAL - TOPOG + CULVERT - ELEV5

JACKSON - ST
LARP TO A2

18

+36.5 - C.B - 16

+36.5 18" CONC 15' .

+36.5 24" CONC 18' - 36' .

17 +36.5 HAND-DITCH 36' - 436'

+36.5 - C.B - 15'

+36.5 18" CONC 15' .

11

+48 - C.B - 15.5

+48 - 18" CONC 15' .

+48 18" CONC 18' - 118' .

+48 C.B 15.3

+48 18" CONC 15' .

10

3

+75 C.B - 15.4

+75 18" CONC 15.6 .

+75 18" CONC 17.5 - 29.5 .

+75 C.B - 15.20

+75 18" - 14.5 .

2

1

12

24" CONC X 18'

18" CONC X 30'

TYPE 1
C.B.

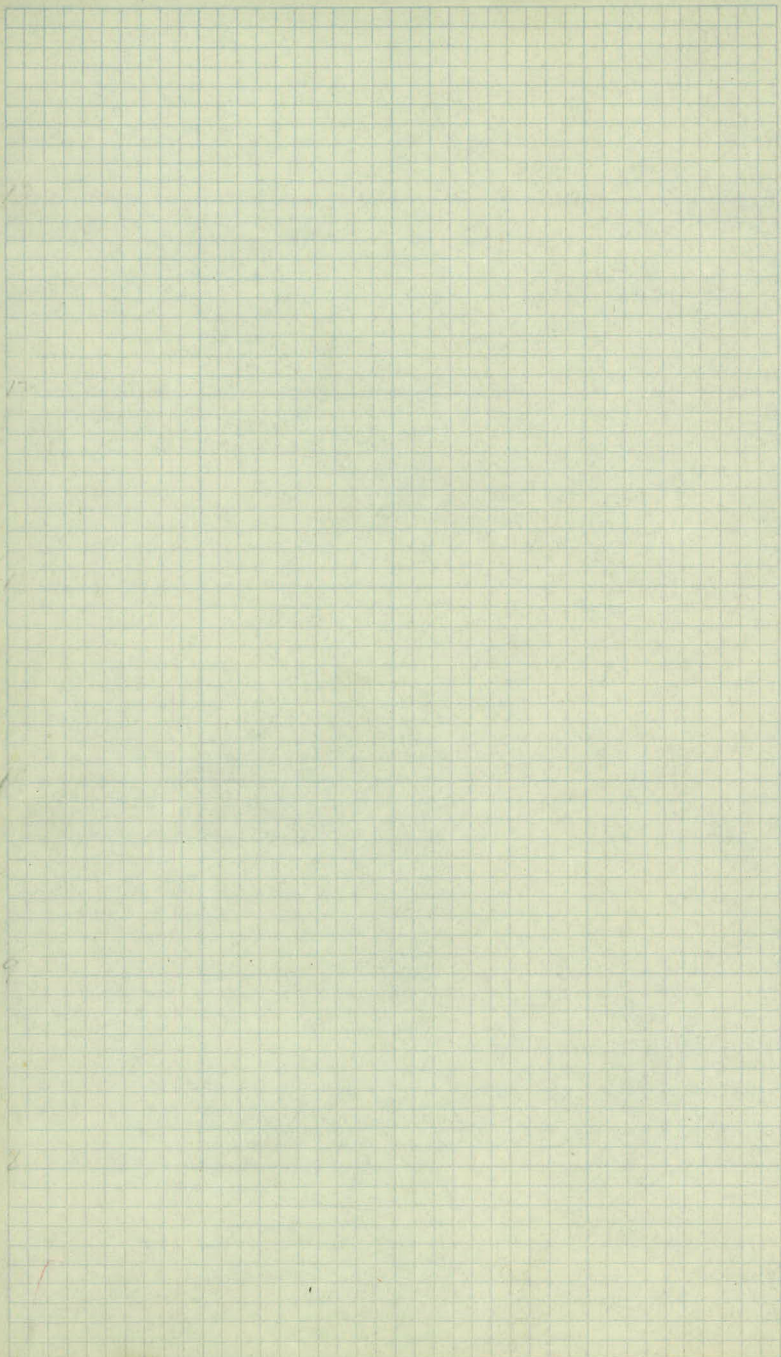
18" CONC X 100'

18" CONC X 30'

TYPE 1 - C.B.

18" CONC X 12'

18" CONC X 32'



67

15

475

1

515

5.0

6.0

7.1

515

515

515

STA	+	π	-	ELEV
B.M	1.22	886.43		885.21
	4.94	880.06	11.31	875.12

2+75

T.P.	11.64	889.64	2.06	878.00
B.M			1.35	888.29

10+48

T.P.	5.55	888.34	6.85	882.79
	4.81	887.48	5.73	882.61

17+36.5

T.P	6.28	891.07	2.69	884.79
B.M			0.25	890.82

890.85

LT & RT

N.E. COR. BOTTOM-STEP 1701-JACKSON

868.54	68.98	69.14	73.62	74.83	74.42	73.49	70.18
F.L.	F.L.	F.L.	F.L.	TOP.C.B.	TOP.C.B.	F.L.	F.L.
18" CONC	18" CONC	18" CONC	INLET			INLET	18" CONC
11.52	11.08	10.92	6.44	5.53	5.64	6.57	9.88
29.5	17.5	15.6	15.4	15.4	15.2	15.2	15

SPIKE-IN P. POLE N.E. COR. DION-ST

879.28	77.44	79.49	81.88	82.80	82.85	81.93	79.82
F.L.	F.L.	F.L.	F.L.	TOP.C.B.	TOP.C.B.	F.L.	F.L.
18" CONC	18" CONC	18" CONC	INLET			INLET	18" CONC
10.36	10.20	10.15	7.76	6.84	6.79	7.71	9.82
118	18	15	15.5	15.5	15.3	15.3	15.0

878.86	78.86	78.88	81.27	82.14	82.19	81.42	79.00
F.L.	F.L.	F.L.	F.L.	TOP.C.B.	TOP.C.B.	F.L.	F.L.
24" CONC	24" CONC	18" CONC	INLET-TO P.C.B.			INLET	18" CONC
8.62	8.62	8.60	6.21	5.34	5.29	6.06	8.48
36	18	15	16	16	15.0	15.0	15.0

DOOR-SILL ON-HOUSE 2075 JACKSON-ST

57

