

BK BK. 54 DA. 12 A

Payne Ave. N.C.

OFFICE ENGINEER
RAMSEY CO. MINN.

Plan Survey

Payne Ave.

From Co. Rd. "B" To S.T.H. "36"

Road Acc't. No.

Date Filed 8-3-48 File

11/8/47

Plan Survey
Payne Ave
Co. Rd. "B." to S.H. #36

Sta

Pt

Alt

As

12+02

App. ~~E~~ STA 36

10+52

P.O.T. South Prop Line

0+33

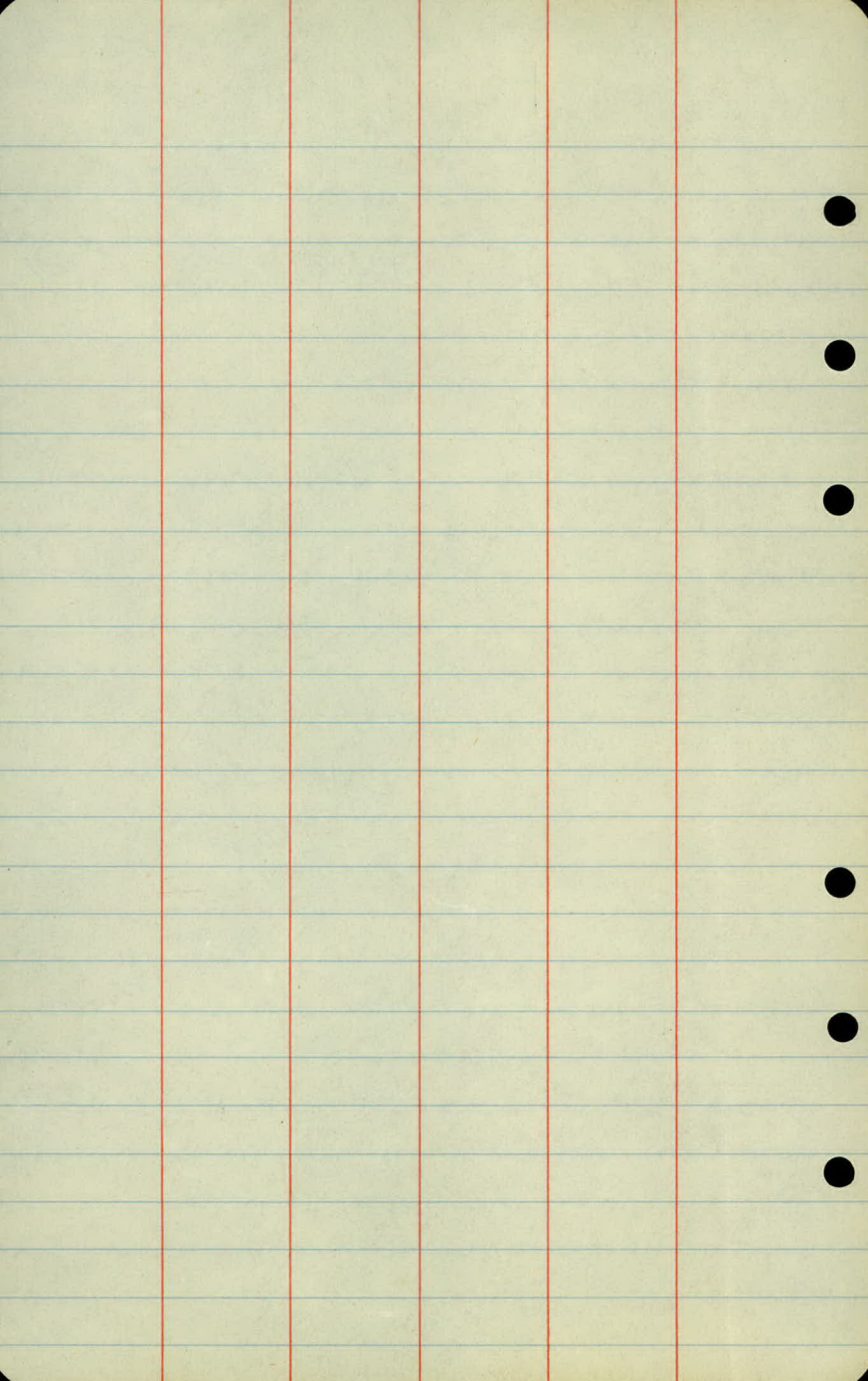
0+00

H.W.
W.B. 2
L.C.

Nail

Fron

Nail



11/8/47

3

X sections

Sta	+	Δ	-	Elev
B.M.	4.90	913.42		908.52
	3.91	914.03	3.30	910.12 ✓
B.M.	4.15	914.03	4.15	909.88 ✓

0+00 07.5 ✓

0+24 06.5 ✓

0+32 07.9 ✓

0+65 05.8 ✓

1+00 05.9 ✓

+50 08.5 ✓

2+00 10.4 ✓

+50 13.2 ✓

T.P. 8.61 922.02 0.62 913.41 ✓

3+00 14.5 ✓

+30 16.9

LT

R

RT

Top Men & Co Rd B & Edgerton

Spk in 18" Oak SW Cor Payne Ave & B.

$$\frac{5.7}{50}$$

$$6.5$$

$$\frac{7.6}{50}$$

$$\frac{6.4}{50}$$

$$7.4$$

$$8.7 \frac{8.7}{50}$$

$$\frac{7.5}{50}$$

$$\frac{7.6}{50} 6.1 \frac{5.1}{16} \frac{4.4}{30} \frac{4.2}{50}$$

$$\frac{9.3}{50}$$

$$\frac{8.8}{21}$$

$$8.2$$

$$\frac{7.7}{19}$$

$$\frac{6.8}{35}$$

$$\frac{5.1}{50}$$

$$\frac{8.4}{50}$$

$$\frac{8.4}{22}$$

$$8.1$$

$$\frac{7.5}{15}$$

$$\frac{6.5}{33}$$

$$\frac{6.0}{50}$$

$$\frac{5.9}{50}$$

$$\frac{5.8}{25}$$

$$5.5$$

$$\frac{4.6}{22}$$

$$\frac{2.8}{50}$$

$$\frac{4.0}{50}$$

$$\frac{3.9}{25}$$

$$3.6$$

$$\frac{3.1}{15}$$

$$\frac{1.4}{35}$$

$$\frac{1.2}{50}$$

$$\frac{0.7}{50}$$

$$\frac{0.5}{25}$$

$$0.8$$

$$\frac{1.4}{20}$$

$$\frac{2.1}{32}$$

$$\frac{2.9}{50}$$

$$\frac{7.7}{50}$$

$$\frac{7.7}{18}$$

$$7.4$$

$$\frac{6.9}{12}$$

$$\frac{7.3}{35}$$

$$\frac{8.8}{50}$$

$$\frac{7.2}{50}$$

$$\frac{6.1}{30}$$

$$\frac{6.1}{12}$$

$$5.1$$

$$\frac{4.7}{17}$$

$$\frac{5.9}{30}$$

$$\frac{8.4}{50}$$

Sta	+	π	-	Elev
		922.02 ✓		

3760				17.4 ✓
------	--	--	--	--------

4				19.4 ✓
---	--	--	--	--------

T.P.	453	926.41 ✓	0.14	921.88 ✓
+28				20.0

+68				20.4
-----	--	--	--	------

5				22.4
---	--	--	--	------

+50				22.2
-----	--	--	--	------

6				21.1
---	--	--	--	------

+50				22.7
-----	--	--	--	------

7				23.7
---	--	--	--	------

+50				24.5
-----	--	--	--	------

8				24.3
---	--	--	--	------

T.P.	4.44	930.59.	0.26	926.15 ✓
+13				26.3

LT

R

RT

$$\frac{5.3}{50} \quad \frac{4.4}{20} \quad 4.6 \quad \frac{5.1}{18} \quad \frac{7.7}{32} \quad \frac{10.8}{50}$$

$$\frac{1.5}{50} \quad \frac{1.8}{22} \quad 2.6 \quad \frac{3.5}{14} \quad \frac{6.4}{30} \quad \frac{9.3}{50}$$

$$\frac{4.9}{50} \quad \frac{4.1}{32} \quad \frac{5.9}{17} \quad 6.4 \quad \frac{7.4}{15} \quad \frac{9.8}{30} \quad \frac{11.3}{50}$$

$$\frac{6.4}{50} \quad \frac{6.0}{30} \quad 6.0 \quad \frac{6.0}{22} \quad \frac{6.9}{41} \quad \frac{7.7}{50}$$

$$\frac{5.0}{50} \quad \frac{4.5}{25} \quad 4.0 \quad \frac{4.3}{20} \quad \frac{4.8}{35} \quad \frac{4.8}{50}$$

$$\frac{6.4}{50} \quad \frac{5.1}{25} \quad 4.2 \quad \frac{4.1}{22} \quad \frac{4.4}{50}$$

$$\frac{8.0}{50} \quad \frac{6.3}{22} \quad 5.3 \quad \frac{4.8}{18} \quad \frac{4.7}{32} \quad \frac{5.3}{50}$$

$$\frac{7.0}{50} \quad \frac{4.8}{20} \quad 3.7 \quad \frac{3.0}{25} \quad \frac{2.9}{50}$$

$$\frac{4.5}{50} \quad \frac{3.8}{24} \quad 2.7 \quad \frac{2.7}{22} \quad \frac{2.5}{50}$$

$$\frac{4.2}{50} \quad \frac{3.7}{30} \quad \frac{2.8}{10} \quad 1.9 \quad \frac{2.0}{25} \quad \frac{2.0}{50}$$

$$\frac{2.0}{50} \quad \frac{2.4}{25} \quad 2.1 \quad \frac{1.7}{15} \quad \frac{2.1}{30} \quad \frac{2.7}{50}$$

$$\frac{4.0}{50} \quad \frac{4.2}{25} \quad 4.3 \quad \frac{5.0}{25} \quad \frac{6.4}{50}$$

Sta + π - Elev

930.59 ✓

8+33 26.7

+58 27.9

9 27.0

+50 26.7

+80 25.7

10 23.5

+52 21.5

+65 21.6

T.P. 1.91 92416 ✓ 834 922.25 ✓

11 16.6

+71 15.3

+80 Shoulder Rd 17.1

12+02 17.2

B.M 0.73 923.43 ✓

Lt

2

Rt

$$\frac{3.6}{50} \quad \frac{3.8}{25} \quad 3.9 \quad \frac{4.9}{30} \quad \frac{6.2}{50}$$

$$\frac{3.6}{50} \quad \frac{3.1}{20} \quad 2.7 \quad \frac{2.9}{24} \quad \frac{3.9}{40} \quad \frac{4.6}{50}$$

$$\frac{4.0}{50} \quad \frac{3.9}{25} \quad 3.6 \quad \frac{3.8}{25} \quad \frac{4.5}{50}$$

$$\frac{3.2}{50} \quad \frac{3.3}{25} \quad 3.9 \quad \frac{4.7}{25} \quad \frac{5.8}{50}$$

$$\frac{4.0}{50} \quad \frac{4.1}{25} \quad 4.9 \quad \frac{5.0}{25} \quad \frac{5.9}{50}$$

$$\frac{5.6}{50} \quad \frac{7.0}{24} \quad 7.1 \quad \frac{6.3}{17} \quad \frac{5.6}{33} \quad \frac{5.9}{50}$$

$$\frac{9.6}{30} \quad \frac{9.9}{20} \quad 9.1 \quad \frac{7.2}{30} \quad \frac{6.5}{50}$$

$$\frac{10.4}{50} \quad \frac{10.2}{30} \quad \frac{9.9}{15} \quad 9.0 \quad \frac{7.8}{30} \quad \frac{7.2}{50}$$

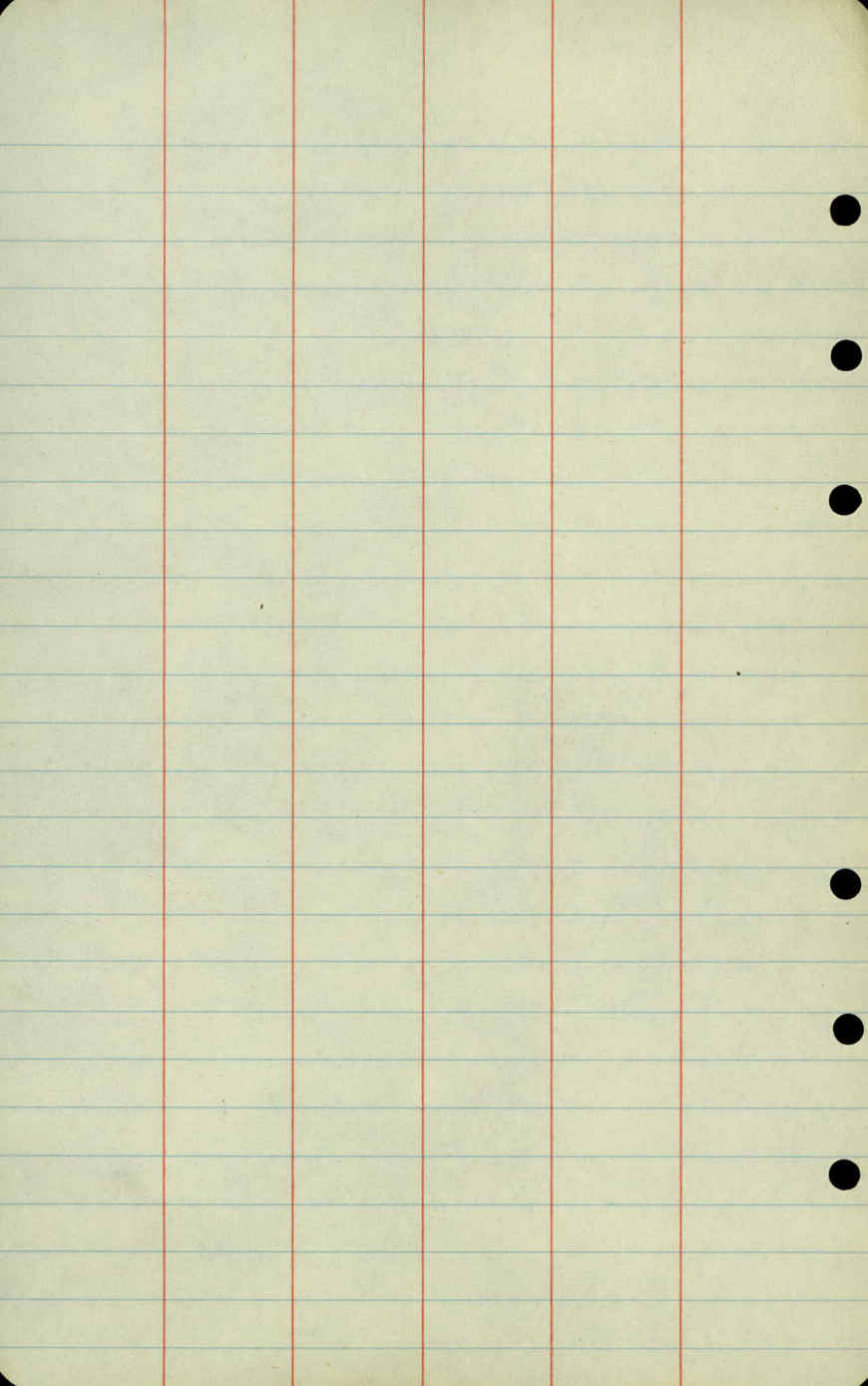
$$\frac{5.6}{50} \quad \frac{6.7}{25} \quad 7.4 \quad \frac{8.2}{25} \quad \frac{9.3}{50}$$

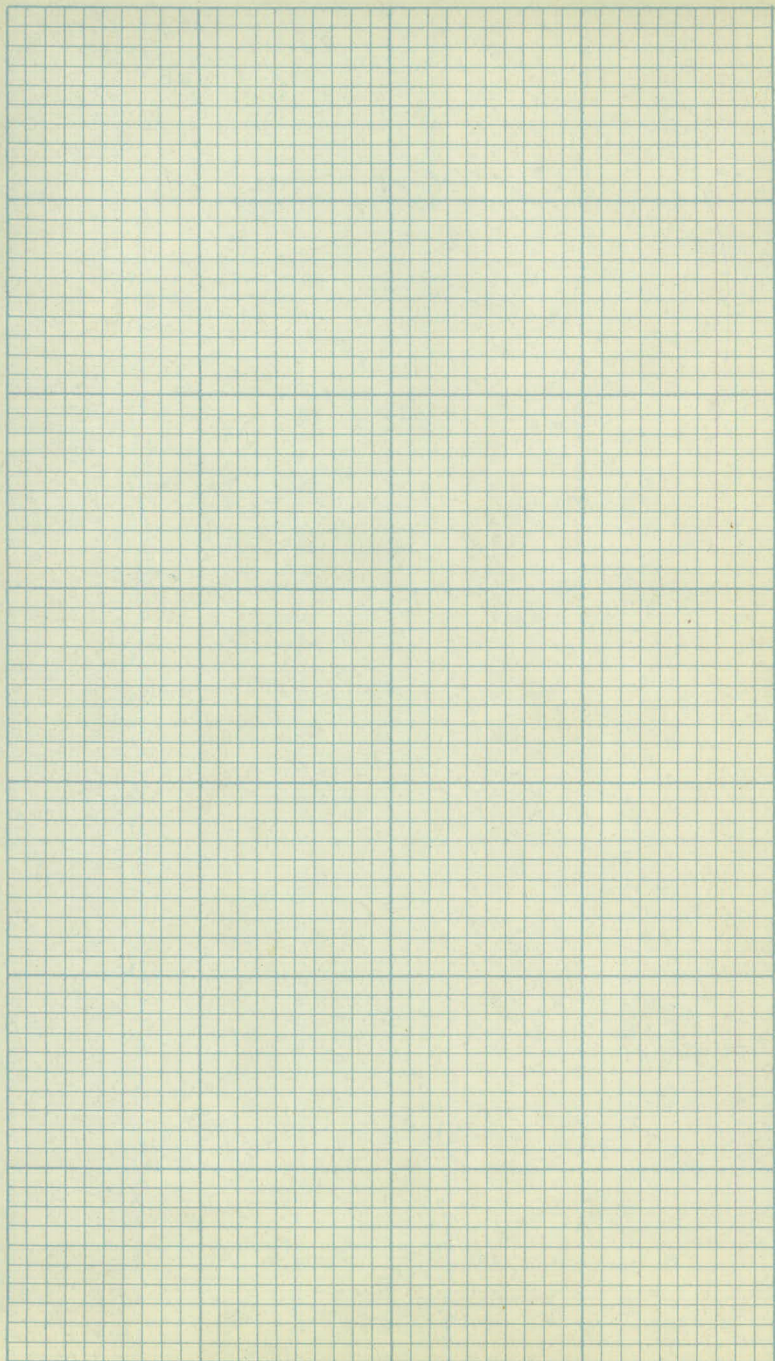
$$\frac{6.3}{50} \quad \frac{7.6}{25} \quad 8.9 \quad \frac{9.9}{25} \quad \frac{10.8}{50}$$

$$\frac{4.4}{50} \quad 7.1 \quad \frac{9.3}{50}$$

6.6

Top Iron 30' R1 1075V





Topog

Payne Ave

+81 Stn 18'

+29 Stn 1'

5

+65 Stn 12'

+48 Stn 12'

+23 Stn 27'

4

+94 Stn 43'

3

+70 Stn 6'

+30 18" Oak 35'

2

+10 Δ in Fe 47'

1

+72 Δ in Fe 3'

+33 Fe Cor 17'

0 0+07 Edge Blacktop 7'

+73 Stn 13'

+50 Fe 26'

+42 Stn 10'

+21 Stn 16'

+00 Fe 36'

+95 Stn 36'

+74 15" Oak 14'

+50 Fe 45'

+38 24" Oak 47'

+00 Fe 48'

+85 Stn 16'

+74 18" Tre 47'

Fe 45'

+34 Stn 5'

+16 24" Oak 30 Fe 53

+41 15" Oak 18'

+41 Stn 35'

+00 Stn 37' Fe 53'

Fe 56

+98 Fe Cor 0.0

F

+33 Fe Cor 59

Picture

Picture

Pathhole

Hay Meadow

9

8

+09 Fe Xk

Fe Cor 9'
Fo. 6'

+65 A Fe 5'

+28 Stn 5' Fe 6'

7 Fe 1' Stn 11

+41 Stn 5'

+25 Stn 4'

6

+95 Tw. 12" 60'
Oak

+62 Stn 1'

+50 Fe 9'

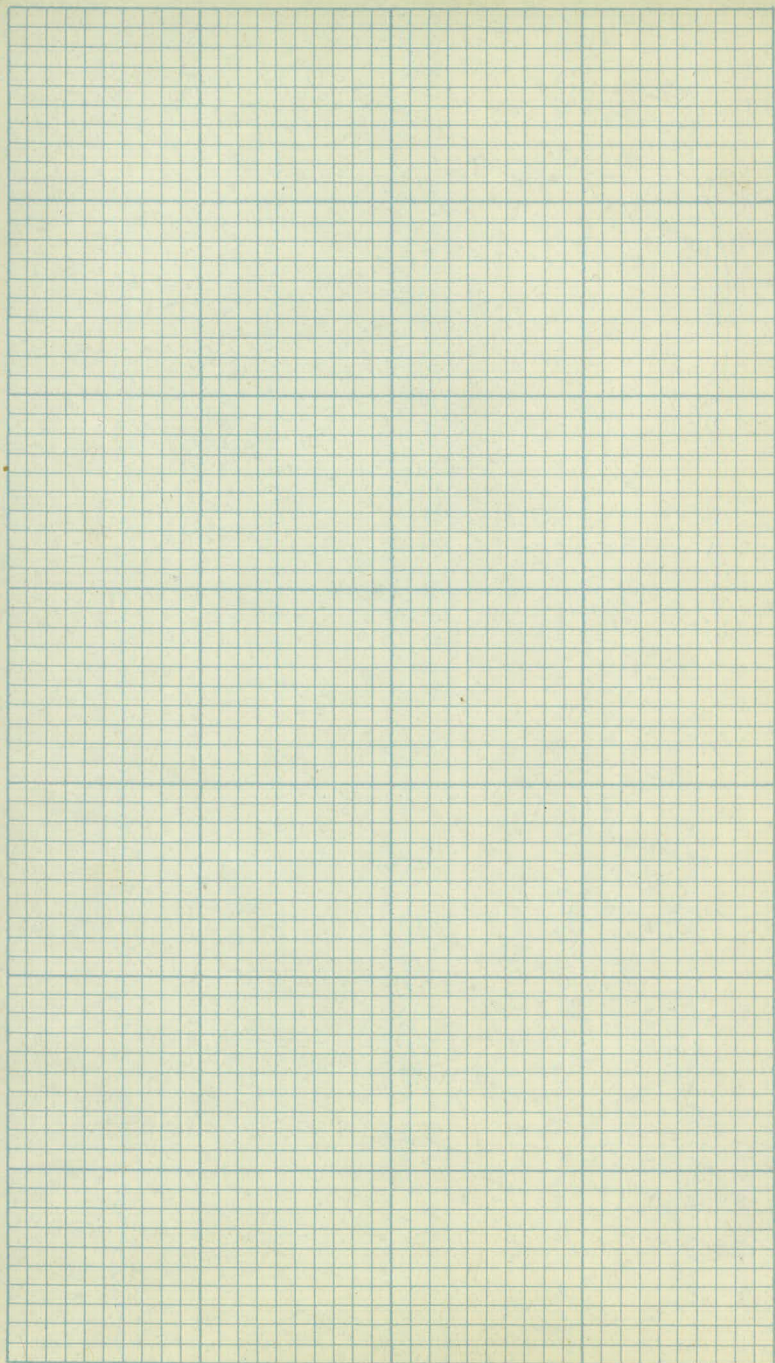
+16 Tw 4'

Fe 17.5'

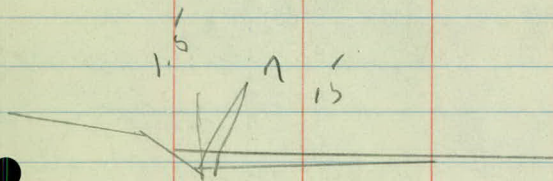
+87 15" Oak 14'

Cultivated

Pasture



Slope Stakes
Payne Ave



Sta	t	π	-	E/c.v	Gr. Rod
B.M.	3.88	913.76		909.88	

0+24				07.0	6.8
------	--	--	--	------	-----

0+32				07.0	6.8
------	--	--	--	------	-----

0+65				07.2	4.6
------	--	--	--	------	-----

1+00				07.3	6.5
------	--	--	--	------	-----

+50				08.0	5.9
-----	--	--	--	------	-----

2				09.5	4.3
---	--	--	--	------	-----

1					
+50				11.5	2.3
T.P	11.05	924.46	0.35	913.41	

3				13.5	11.0
---	--	--	--	------	------

Perm
Girade Rod

LT

L

RT

Spk in 18 Oak. SW Gr BY Payne.

07.3 6.5

$\begin{array}{r} 5.9 \\ 00.9 \end{array}$

$\begin{array}{r} 4.3 \\ 02.4 \\ \hline 3 \end{array}$

07.3, 6.5

$\begin{array}{r} 7.0 \\ 00.5 \\ \hline 31.0 \end{array}$

$\begin{array}{r} 5.9 \\ 00.9 \end{array}$

$\begin{array}{r} 4.3 \\ 02.4 \\ \hline 34.0 \end{array}$

13

$\begin{array}{r} 8.1 \\ 00.3 \\ \hline 34.6 \end{array}$

$\begin{array}{r} 7.9 \\ 00.3 \end{array}$

$\begin{array}{r} 5.8 \\ 00.5 \\ \hline 31.0 \end{array}$

6.2

$\begin{array}{r} 8.2 \\ 00.0 \\ \hline 34.0 \end{array}$

$\begin{array}{r} 7.8 \\ 00.3 \end{array}$

$\begin{array}{r} 1.3 \\ 00.1 \\ \hline 30.2 \end{array}$

083 55

$\begin{array}{r} 5.6 \\ 00.1 \\ \hline 30.2 \end{array}$

$\begin{array}{r} 5.3 \\ 00.5 \end{array}$

$\begin{array}{r} 3.4 \\ 02.1 \\ \hline 34.2 \end{array}$

098 4.0

$\begin{array}{r} 3.6 \\ 00.4 \\ \hline 30.8 \end{array}$

$\begin{array}{r} 3.4 \\ 00.9 \end{array}$

$\begin{array}{r} 1.3 \\ 02.1 \\ \hline 35.4 \end{array}$

20

$\begin{array}{r} 0.0 \\ 02.0 \\ \hline 34.0 \end{array}$

$\begin{array}{r} 0.4 \\ 01.7 \end{array}$

$\begin{array}{r} 1.8 \\ 00.2 \\ \hline 30.4 \end{array}$

10.7

$\begin{array}{r} 10.2 \\ 00.5 \\ \hline 31.0 \end{array}$

$\begin{array}{r} 9.8 \\ 01.2 \end{array}$

$\begin{array}{r} 9.4 \\ 01.1 \\ \hline 32.0 \end{array}$

Sta	+	Δ	-	Elev	$\pm$ Br Rod
		924.46			
3 + 30				14.7	9.8
3 + 60				15.9	8.6
4				17.5	7.0
+ 28				18.5	6.0
+ 68				19.5	5.0
5				19.9	4.1
+ 50				20.2	4.3
6				20.7	3.8

Born Or

L+

L

R+

9.5

$$\begin{array}{r} 8.5 \\ C1.0 \\ \hline 32.0 \end{array}$$

$$\begin{array}{r} 10.5 \\ C2.3 \\ \hline \end{array}$$

$$\begin{array}{r} 8.5 \\ C1.0 \\ \hline 32.0 \end{array}$$

8.3

$$\begin{array}{r} 7.0 \\ C1.3 \\ \hline 32.0 \end{array}$$

$$\begin{array}{r} 11.0 \\ C1.6 \\ \hline \end{array}$$

$$\begin{array}{r} 10.6 \\ F2.3 \\ \hline 34.1 \end{array}$$

6.7

$$\begin{array}{r} 3.5 \\ C2.2 \\ \hline 36.4 \end{array}$$

$$\begin{array}{r} 5.0 \\ C2.0 \\ \hline \end{array}$$

$$\begin{array}{r} 10.6 \\ C3.9 \\ \hline 37.8 \end{array}$$

5.7

$$\begin{array}{r} 2.9 \\ C2.8 \\ \hline 35.6 \end{array}$$

$$\begin{array}{r} 4.5 \\ C1.5 \\ \hline \end{array}$$

$$\begin{array}{r} 8.2 \\ F2.5 \\ \hline 35.0 \end{array}$$

4.7

$$\begin{array}{r} 3.8 \\ C0.9 \\ \hline 31.8 \end{array}$$

$$\begin{array}{r} 3.9 \\ C1.1 \\ \hline \end{array}$$

$$\begin{array}{r} 4.0 \\ C0.7 \\ \hline 31.4 \end{array}$$

4.3

$$\begin{array}{r} 3.7 \\ C1.5 \\ \hline 33.2 \end{array}$$

$$\begin{array}{r} 2.0 \\ C2.6 \\ \hline \end{array}$$

$$\begin{array}{r} 3.0 \\ C1.3 \\ \hline 32.6 \end{array}$$

4.0

$$\begin{array}{r} 3.4 \\ C0.6 \\ \hline 31.2 \end{array}$$

$$\begin{array}{r} 2.2 \\ C2.1 \\ \hline \end{array}$$

$$\begin{array}{r} 2.4 \\ C1.5 \\ \hline 33.2 \end{array}$$

3.5

$$\begin{array}{r} 5.2 \\ F1.7 \\ \hline 33.4 \end{array}$$

$$\begin{array}{r} 3.3 \\ C0.5 \\ \hline \end{array}$$

$$\begin{array}{r} 2.8 \\ C0.7 \\ \hline 31.4 \end{array}$$

Sta	+	Δ	-	Elev	$\frac{L}{\text{Gr Rod}}$
		924.46			

6+50				21.5	3.0
------	--	--	--	------	-----

T.P.	7.00	931.36	0.10	924.36	
------	------	--------	------	--------	--

7				22.4	9.0
---	--	--	--	------	-----

+50				23.3	8.1
-----	--	--	--	------	-----

8				24.2	7.2
---	--	--	--	------	-----

+13				24.4	7.0
-----	--	--	--	------	-----

+33				24.7	6.7
-----	--	--	--	------	-----

+58				25.2	6.2
-----	--	--	--	------	-----

9				25.3	6.1
---	--	--	--	------	-----

Bern
Orville

Lt

R

Rt

2.7

$$\begin{array}{r} 37 \\ F1.0 \\ \hline 320 \end{array}$$

$$\begin{array}{r} 1.6 \\ C1.4 \end{array}$$

$$\begin{array}{r} 1.5 \\ C1.2 \\ \hline 320 \end{array}$$

8.7

$$\begin{array}{r} 90 \\ F0.3 \\ \hline 306 \end{array}$$

$$\begin{array}{r} 7.3 \\ F1.7 \end{array}$$

$$\begin{array}{r} 7.8 \\ C0.9 \\ \hline 318 \end{array}$$

7.8

$$\begin{array}{r} 88 \\ F1.0 \\ \hline 320 \end{array}$$

$$\begin{array}{r} 66 \\ C1.2 \end{array}$$

$$\begin{array}{r} 6.8 \\ C1.0 \\ \hline 320 \end{array}$$

6.9

$$\begin{array}{r} 67 \\ C0.2 \\ \hline 304 \end{array}$$

$$\begin{array}{r} 70 \\ C0.2 \end{array}$$

$$\begin{array}{r} 73 \\ F0.4 \\ \hline 308 \end{array}$$

6.7

$$\begin{array}{r} 470 \\ C2.0 \\ \hline 340 \end{array}$$

$$\begin{array}{r} 49 \\ C2.1 \end{array}$$

$$\begin{array}{r} 57 \\ C1.0 \\ \hline 320 \end{array}$$

6.4

$$\begin{array}{r} 45 \\ C1.9 \\ \hline 33.8 \end{array}$$

$$\begin{array}{r} 46 \\ C2.1 \end{array}$$

$$\begin{array}{r} 55 \\ C0.9 \\ \hline 31.8 \end{array}$$

6.9

$$\begin{array}{r} 42 \\ C1.7 \\ \hline 334 \end{array}$$

$$\begin{array}{r} 34 \\ C2.8 \end{array}$$

$$\begin{array}{r} 41 \\ C1.8 \\ \hline 33.6 \end{array}$$

5.8

$$\begin{array}{r} 47 \\ C1.1 \\ \hline 322 \end{array}$$

$$\begin{array}{r} 43 \\ C1.8 \end{array}$$

$$\begin{array}{r} 47 \\ C1.1 \\ \hline 322 \end{array}$$

Sta + A - Elev K.D. Rod

93136

9750

24.3 7.1

+80

23.3 8.1

18

22.7 8.7

+52

20.9 10.3

B.M

7.93 923.43 ✓

Berm
Gr. Red

L+

X

R+

6.9

$$\begin{array}{r} 3.9 \\ C3.0 \\ \hline 36.0 \end{array}$$

$$\begin{array}{r} 4.6 \\ C2.5 \\ \hline \end{array}$$

$$\begin{array}{r} 5.7 \\ C1.2 \\ \hline 32.4 \end{array}$$

7.9

$$\begin{array}{r} 4.9 \\ C3.0 \\ \hline 36.0 \end{array}$$

$$\begin{array}{r} 5.6 \\ C2.5 \\ \hline \end{array}$$

$$\begin{array}{r} 6.0 \\ C1.9 \\ \hline 33.8 \end{array}$$

8.4

$$\begin{array}{r} 7.1 \\ C1.3 \\ \hline 32.6 \end{array}$$

$$\begin{array}{r} 8.0 \\ C0.7 \\ \hline \end{array}$$

$$\begin{array}{r} 6.4 \\ C2.0 \\ \hline 34.0 \end{array}$$

10.2

$$\begin{array}{r} 10.7 \\ F0.5 \\ \hline 31.0 \end{array}$$

$$\begin{array}{r} 10.0 \\ C0.2 \\ \hline \end{array}$$

$$\begin{array}{r} 7.7 \\ C2.5 \\ \hline 35.0 \end{array}$$

Top Iron 31 R1 Stc 10x52

