

OFFICE OF COUNTY ENGINEER
RAMSEY CO. MINN.

Plan Survey

Eli Road

From Centerville Rd. To De Soto St.

Slope stakes

Road Acc't. No.

Date Filed 8-4-47

File

Nadeau Rd. Alignment 9-29-48

Save

File with Eli Rd.

NADEAU RD. - Alignment

9-29-48 K.A.



Approx. $\frac{1}{4}$ - $\frac{1}{2}$ Line 2



Cop.
54000
House.

Cor.
Brick
Found.

Centerville Ed.

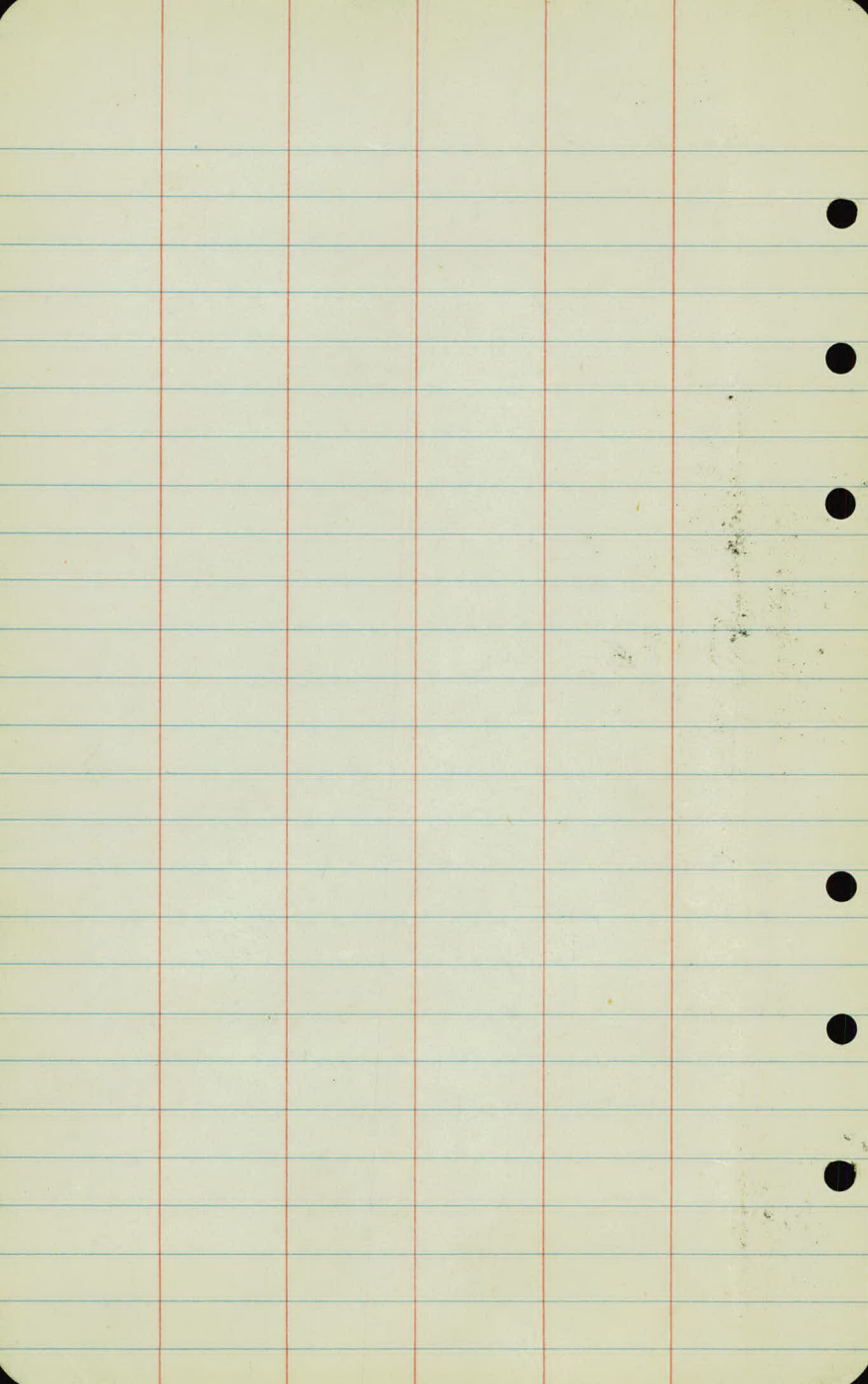
cen.

Sec. 6

1321.31

1321.31'

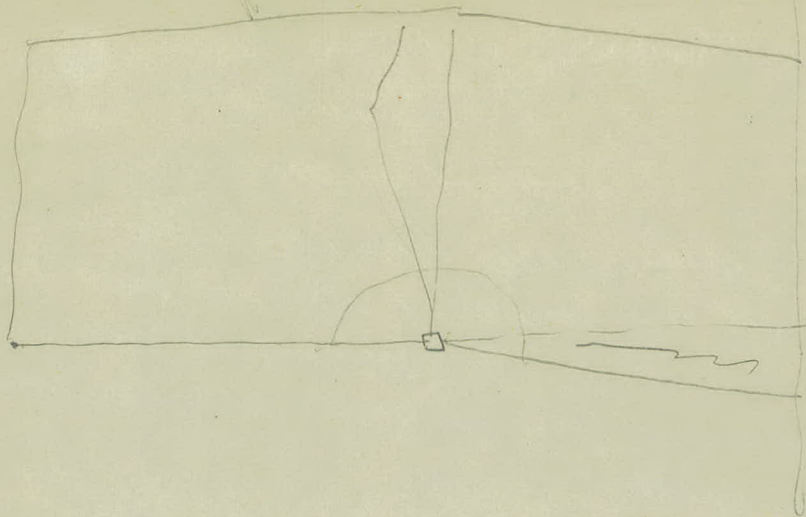
1001



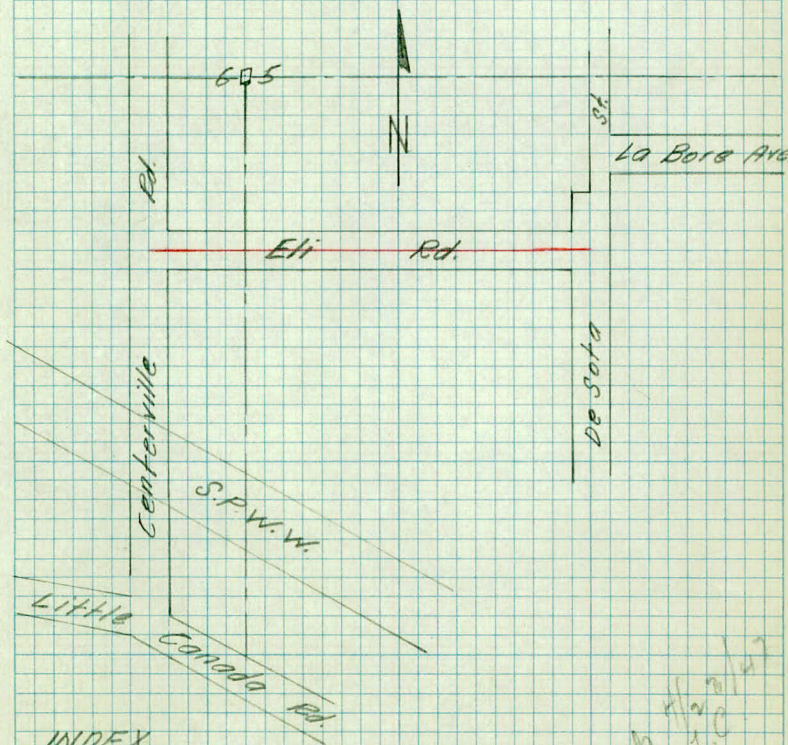
Walter:

By shifting this line 0.54'
N at sta. 3+30 and 16+39.06 then
producing this line W to Centerville
road the angle at sta. 3+30 will be
eliminated. This line would still give
36 acres between Eli Rd. & sec. line
to north.

K. A.



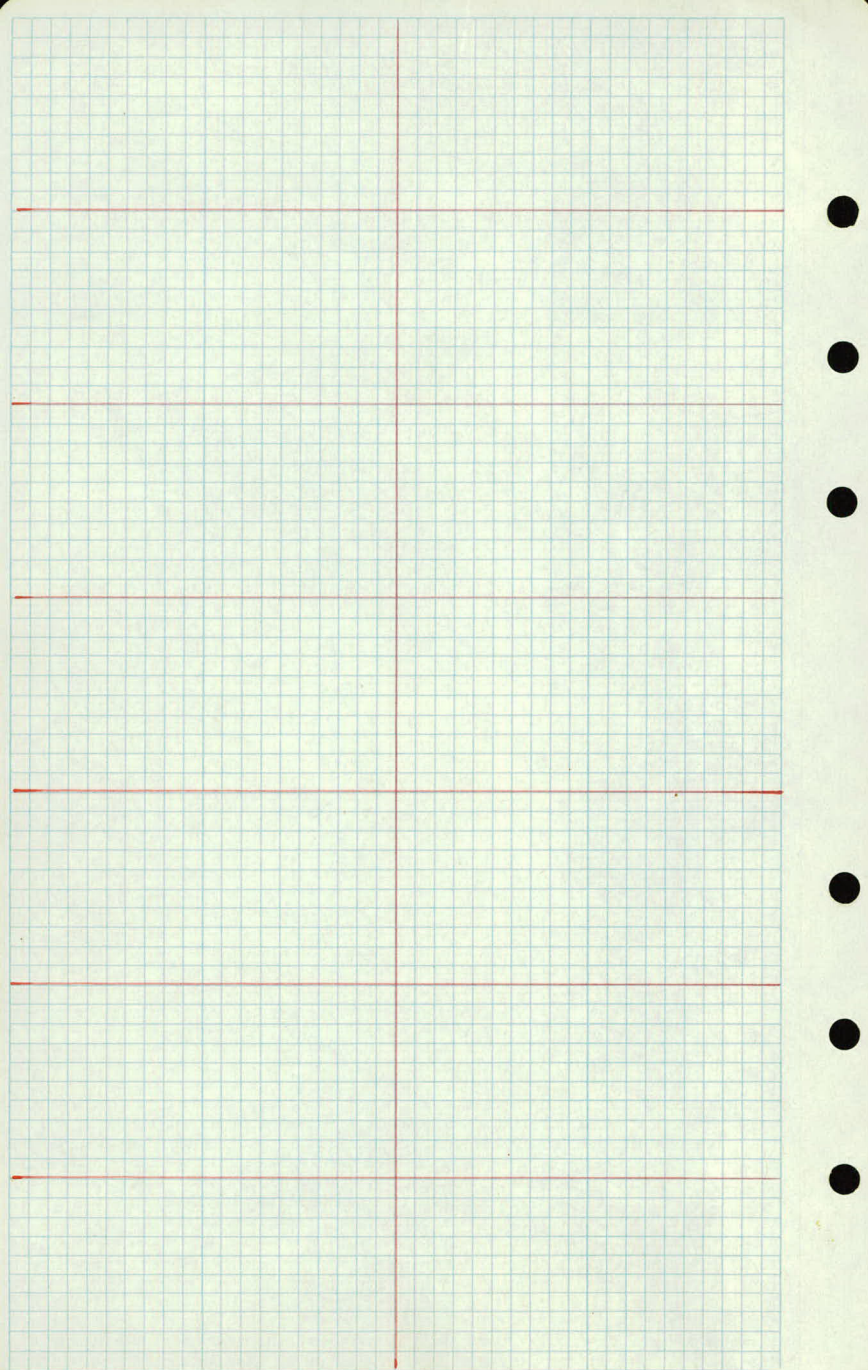
PLAN SURVEY
ELI ROAD
Centerville Rd to De Soto St.



INDEX

- Align - 1-2
- Topog. - 3-6
- Bench - 7-8
- Levels
- X Sections - 9-15

Approved H. 2. 2/47
J. 2. 2/47



1

Alignment

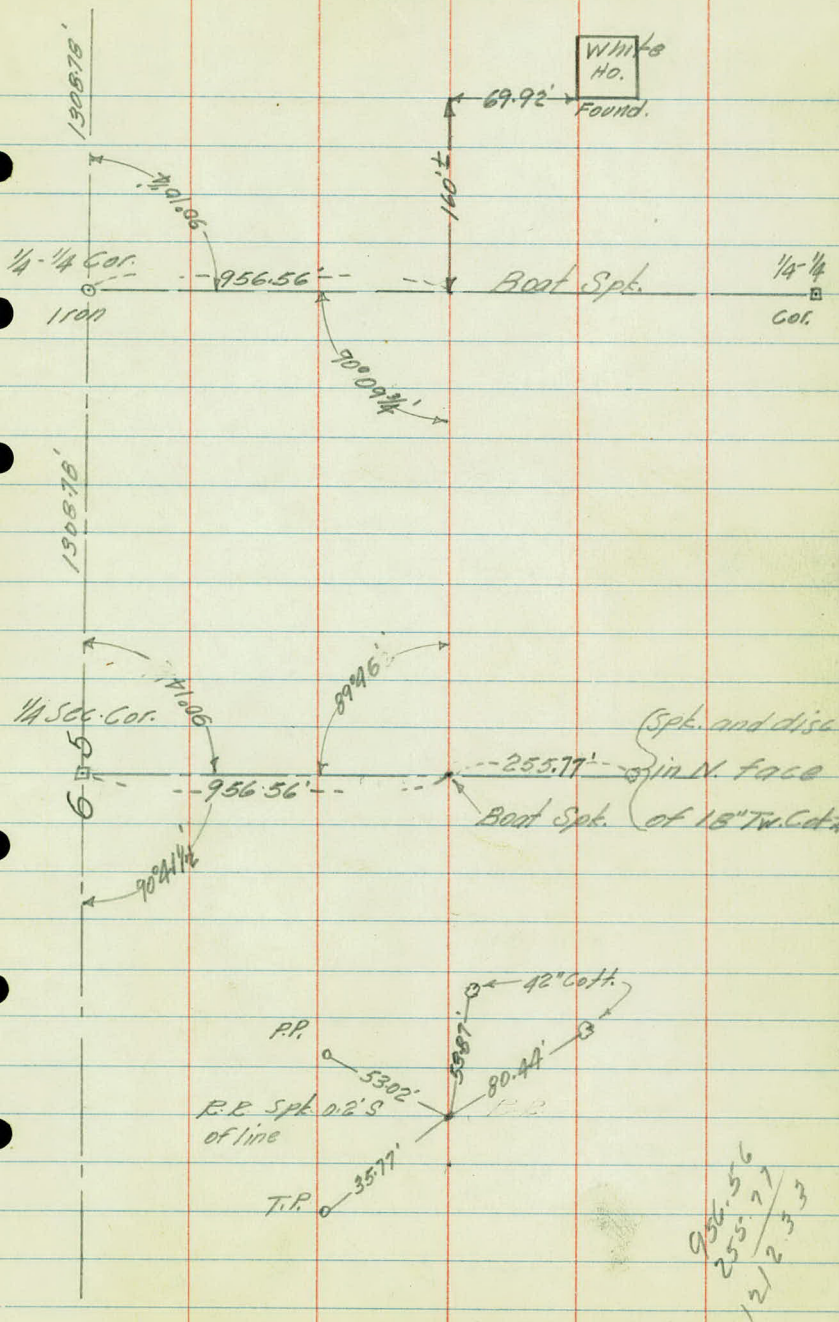
Sta.	Point	ΔL	ΔB
------	-------	------------	------------

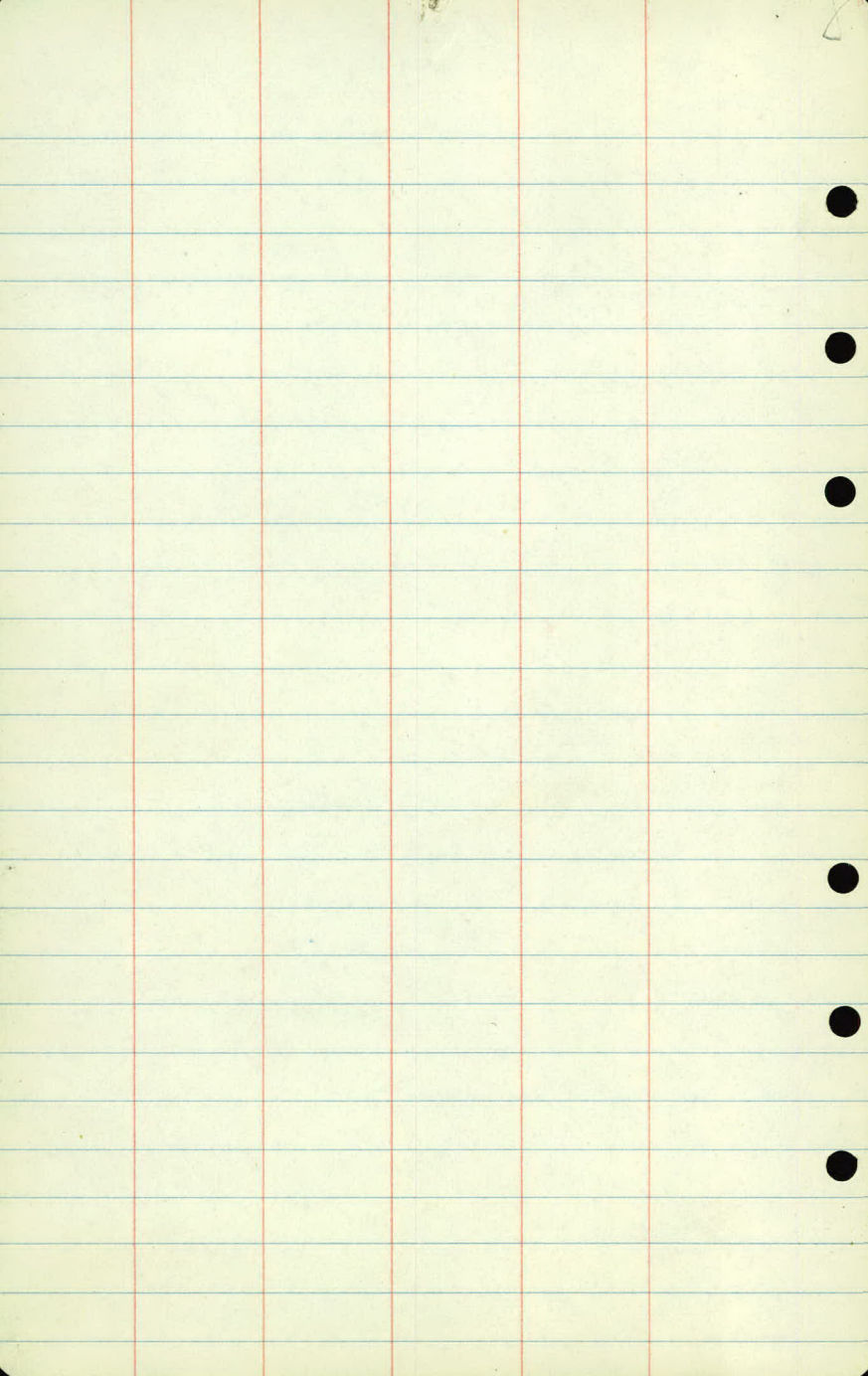
16 + 39.82	P.O.T.	-	E De Soto St.
------------	--------	---	---------------

3 + 50.00	P.I.	0° 55 1/2'	
-----------	------	------------	--

0 + 16.35	=	E Travelled Road	
-----------	---	------------------	--

0 + 100	=	E Centerville Rd.	
---------	---	-------------------	--





Topography

+95-18"0-11"

+69-54p-17'

+44-20"0-6'

+19-54p-18'

+12-18"0-36'

6

+89-54p-22'

+64-30"0-6'

+35-20"0-6'

+28-24"0-1'

+84-End Fe-7'

5

4

Fe-4'

3

Fe-3'

2

1

+82-Beg Fe-2'

+08-3"BE-1'

+92-12"0-20'

+79-8"BE-8'

+72-42"Colt-8'

0

+09-Edge of Bl. Top

2-26-41

K.A.
A.M.
M.B.
P.K.

4



A

x

x

x

x

x

x

x

x

x

x

x

x

x

x

x

x

x

Uncult.

Uncult.

Sketch in error
at 0+16.5

18

13

Fc-15'

12

Fc-14'

11

Fc-13'

10

+49-Bcg.Fc-12'

+0510"0.-13'

+13-18"0.-8'

+04-30"0.-3'

9

+98-5"ironwood-13'

+54-12"0.-13'

+45-16"Tw.0.-6'

+55-20"0.-11'

+46-8"0.-1'

+42-10"0.-4'

+28-10"0.-11'

+26-5"p-2' +22-5"p-6'

+23-6"0.-18' +13-5"p-8'

8

+98-5"p-12'

+18-5"p-30'

+99-16"Trip.0.-3'

+56-4"0.-14'

7

+19-5"p-22'

+12-30"0.-1'

Uncult.

Uncult.

Wooded



16

End FC-18'

15

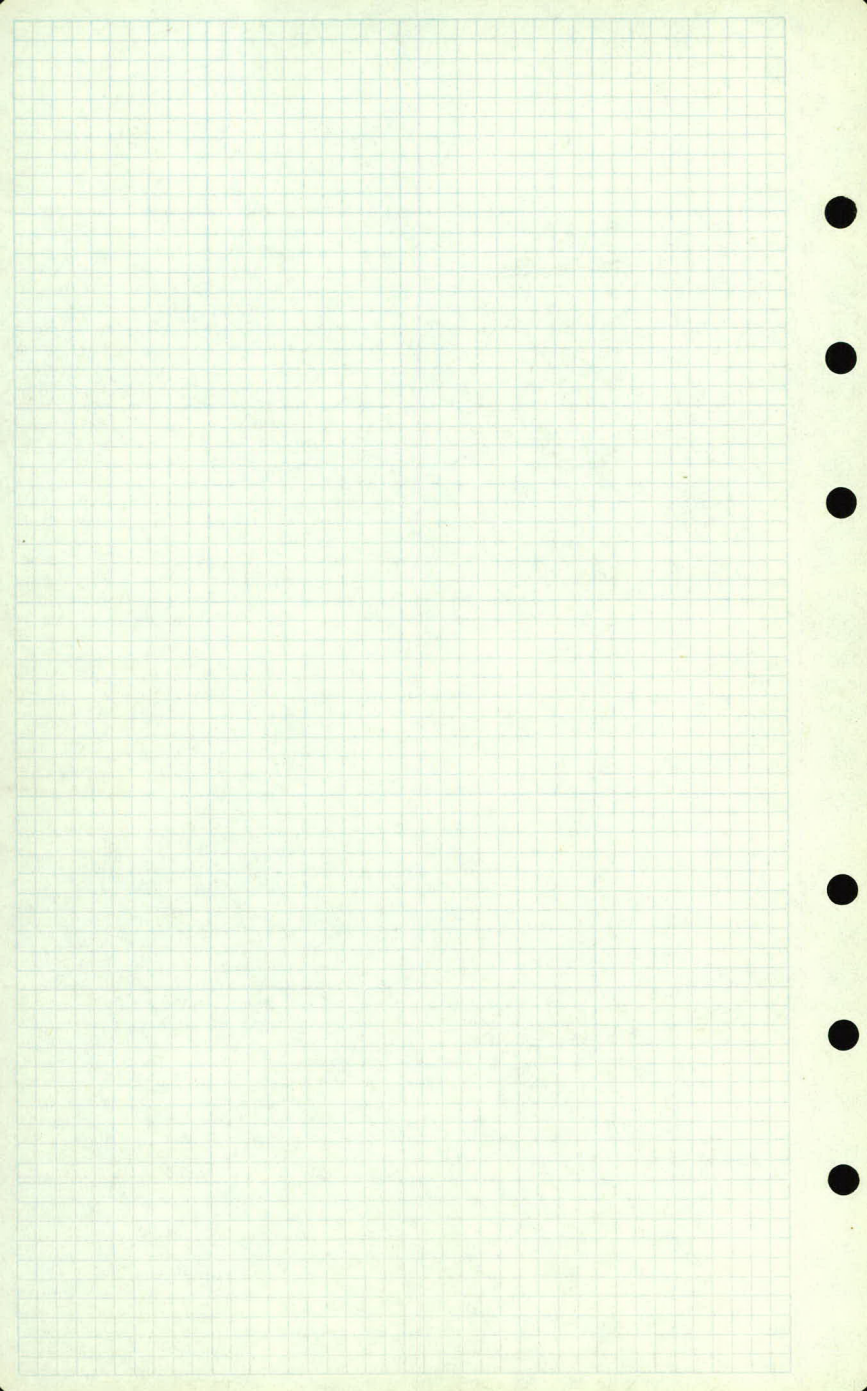
FC-18'

14

FC-15

Uncult.

Uncult.



Bench Level

Sta.	+	X	-	Elev.
B.M.	1.52	910.92		(909.40)
T.P.	9.20	907.06	13.06	897.86
B.M.	4.54	911.34	0.26	906.80
T.P.	11.11	922.46	+0.01	911.35
B.M.			6.01	916.45
T.P.	1.87	922.27	2.06	920.40
T.P.	3.88	920.82	5.33	916.94
T.P.	2.20	914.97	8.05	912.77
B.M.			17.52	897.45
B.M.	4.23	920.68		916.45
T.P.	0.14	911.08	9.74	910.94
B.M.	0.17	906.97	4.28	906.80
T.P.	9.42	911.48	4.91	902.06
B.M.			2.11	909.37 (909.40)

L

E

R

Top Mont. Center Sec. 5

A

Spt. in P.P. at La Bore Ave. + Vanderbilt St.
 P.R. Spt. in 15" Leaning B.E. 115' Pt. 16 + 39 (at De Soto St.)

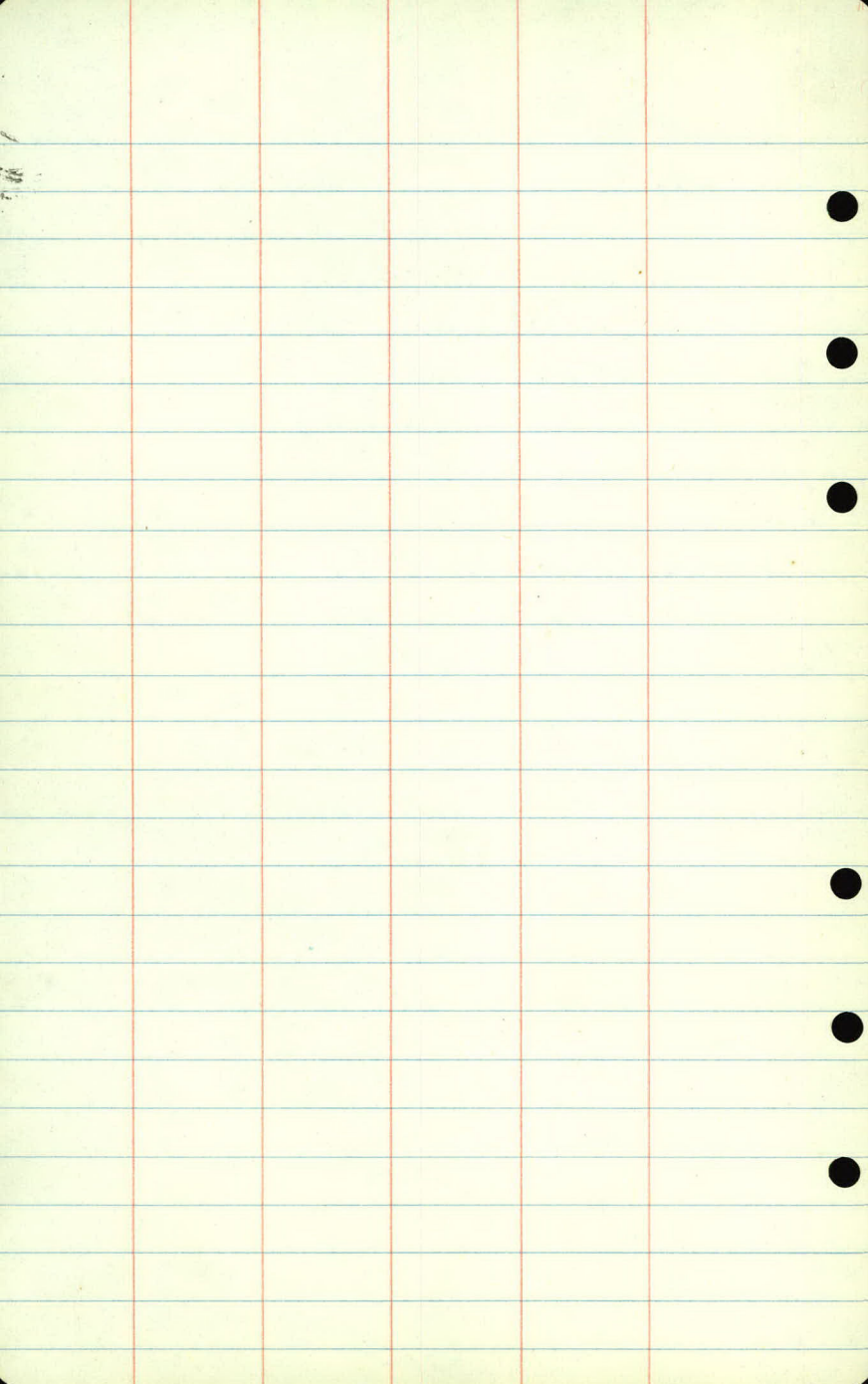
Spt. & sta. 1+00

P.R. Spt. in 42" Cott. S.W. Cor. Eli Rd. + Centerville Rd.

P.R. Spt. in 15" Leaning B.E. 150' S. of Eli Rd. + De Soto St.

Spt. in P.P. Vanderbilt + La Bore Ave.

Top Mont. at Cen. Sec. 5



X Sections

Sta	+	π	-	Elev.
B.M.	17.52	914.97		(897.45)

0 + 16.5 @ Carterville Rd				00.5
---------------------------	--	--	--	------

+29				00.2
-----	--	--	--	------

+34				98.4
-----	--	--	--	------

+42				97.6
-----	--	--	--	------

+63				01.8
-----	--	--	--	------

+82				11.8
-----	--	--	--	------

+93				12.3
-----	--	--	--	------

T.P	8.01	920.72	2.26	912.71
-----	------	--------	------	--------

1				12.2
---	--	--	--	------

2-26-41
K.A.
A.M.
M.B.
R.L.
L

P.P. Spk. in 42" Coll. S.E. Cor. Centerville & Elli.
Eds.

106 125 145 162 182 ✓
100 50 50 100

128 148 164 ✓
50 50

151 152 166 177 174 ✓
50 24 32 50

142 145 158 160 174 186 187 ✓
50 27 21 7 29 50

7.6 7.7 127 13.2 180 203 ✓
50 38 23 25 50

33 3.6 6.5 3.5 3.2 58 14.9 ✓
50 41 23 10 25 50

34 45 40 27 24 23 31 ✓
50 37 28 17 29 50

9.3 97 9.2 85 8.1 88 ✓
50 40 22 27 50

Sta	+	Σ	-	Elev
-----	---	----------	---	------

920.72

1 +50

13.4

2

14.5

+50

15.0

3

15.3

+50

15.6

4

16.3

+50

16.2

5

16.3

L

E

E

8.1 8.1 7.3 7.2 7.9 ✓
50 28 25 50

6.5 6.4 6.2 6.6 6.9 ✓
50 25 28 50

5.5 5.6 5.7 6.3 6.7 ✓
50 24 29 50

5.4 5.3 5.4 5.9 6.4 ✓
50 24 26 50

4.8 5.0 5.1 5.6 5.8 ✓
50 24 24 50

4.7 4.8 4.7 4.4 4.7 5.0 5.2 ✓
50 27 6 9 25 50

4.6 4.8 4.8 4.5 4.5 4.8 4.9 ✓
50 27 5 9 27 50

4.4 4.5 4.4 4.6 4.9 ✓
50 26 24 50

Sta	+	π	-	Elev.
-----	---	-------	---	-------

920.72

5 +50

16.7

6

16.8

+50

16.7

7

16.9

T.P

4.46

922.66

2.62

918.20

+50

17.3

8

17.3

9

17.1

10

17.7

L

2

R

41 43 40 4.2 4.4 ✓
50 19 24 50

4.0 3.7 4.0 3.9 4.1 4.3 ✓
50 24 9 24 50

4.2 4.2 4.0 3.7 3.8 ✓
50 27 24 50

3.6 3.7 3.8 3.7 4.1 4.2 ✓
50 30 12 18 50

5.3 5.5 5.4 5.1 5.9 6.0 ✓
50 24 13 21 50

5.3 5.4 5.4 5.3 5.8 6.0 ✓
50 25 15 22 50

5.0 5.3 5.6 5.5 5.8 6.3 ✓
50 33 14 28 50

4.6 5.0 5.0 4.9 4.7 6.0 6.4 ✓
50 26 9 13 29 50

Sta	+	π	-	Elev
		922.66		
11				17.5
12				17.6
13				17.8
T.P.	2.29	923.11	1.84	920.82
14				18.2
15				18.6
16				18.6
16 + 17				18.7
+39.96				19.7
B.M.			6.66	916.45 (916.45)

L E E

46	48	5.2	5.4	4.2	5.4	5.6	✓
50	30		8	15	25	50	

4.6	4.8		5.1	4.0	5.4	5.5	✓
50	29			13	25	50	

4.4	4.8	4.9	4.6	3.6	3.1	5.8	✓
50	25		9	16	26	50	

5.1	5.5	5.8	4.9	4.3	3.5	5.4	6.1	✓
50	23	7.2		10	16	29	50	

4.6	5.0	4.5	4.4	3.8	5.3	6.1	✓
50	24		10	17	27	50	

4.1	4.4		4.5	4.8	4.5	6.0	6.3	✓
50	26			13	17	29	50	

3.3	3.7	4.4		4.3	5.3	5.8	✓
50	27			16	27	50	

2.7	2.5	3.4	4.4	4.3	4.6	✓
50	28		20	35	50	

R.R. Spt. 10 15' Leaning B.E. 150' S. of Eli Rd + De Soto St.

Sta	Δ	π	-	Elev.
-----	----------	-------	---	-------

[illegible][illegible]

[illegible][illegible][illegible][illegible][illegible][illegible]

[illegible][illegible][illegible][illegible][illegible][illegible]

L

E

E

De Soto St

X sections

Sta	+	π	-	Elev
B.M.	666	923.11		916.45

0	= S. of Eli' Rd		12.4
---	-----------------	--	------

+50		15.7
-----	--	------

1		17.7
---	--	------

+50		18.5
-----	--	------

2	= S. of Eli' Rd	19.7
---	-----------------	------

+50		20.9
-----	--	------

3		19.5
---	--	------

Profile levels from here on

4		14.7
---	--	------

L E R

P.F. Spt. in learning 15' B.E. 150' S. of Eli Rd + DeSoto St.
Slopes South

10.1	9.9	10.7	11.8	11.3	✓
50	28		30	50	

7.9	7.5	7.4	9.1	9.5	✓
50	30		10	50	

6.4	5.4	6.9	7.7	✓
50		7	50	

6.5	5.9	4.6	5.8	6.5	6.3	✓
50	27		9	30	50	

3.4	4.5	5.6	✓
	11	50	

4.2	3.5	2.2	4.1	5.3	✓
50	28		10	50	

5.7	5.3	3.6	5.3	6.3	6.9	✓
50	27		8	27	50	

9.3		8.4		10.3
50				50

Sta	+	π	-	Elev
		923.11		

5				13.5
---	--	--	--	------

6				11.0
---	--	--	--	------

7	+50			08.1
---	-----	--	--	------

+50 - Approx @ La Bore Ave. 06.3

L

L

R

11.0
50

9.6

12.0
50

12.6
50

12.1

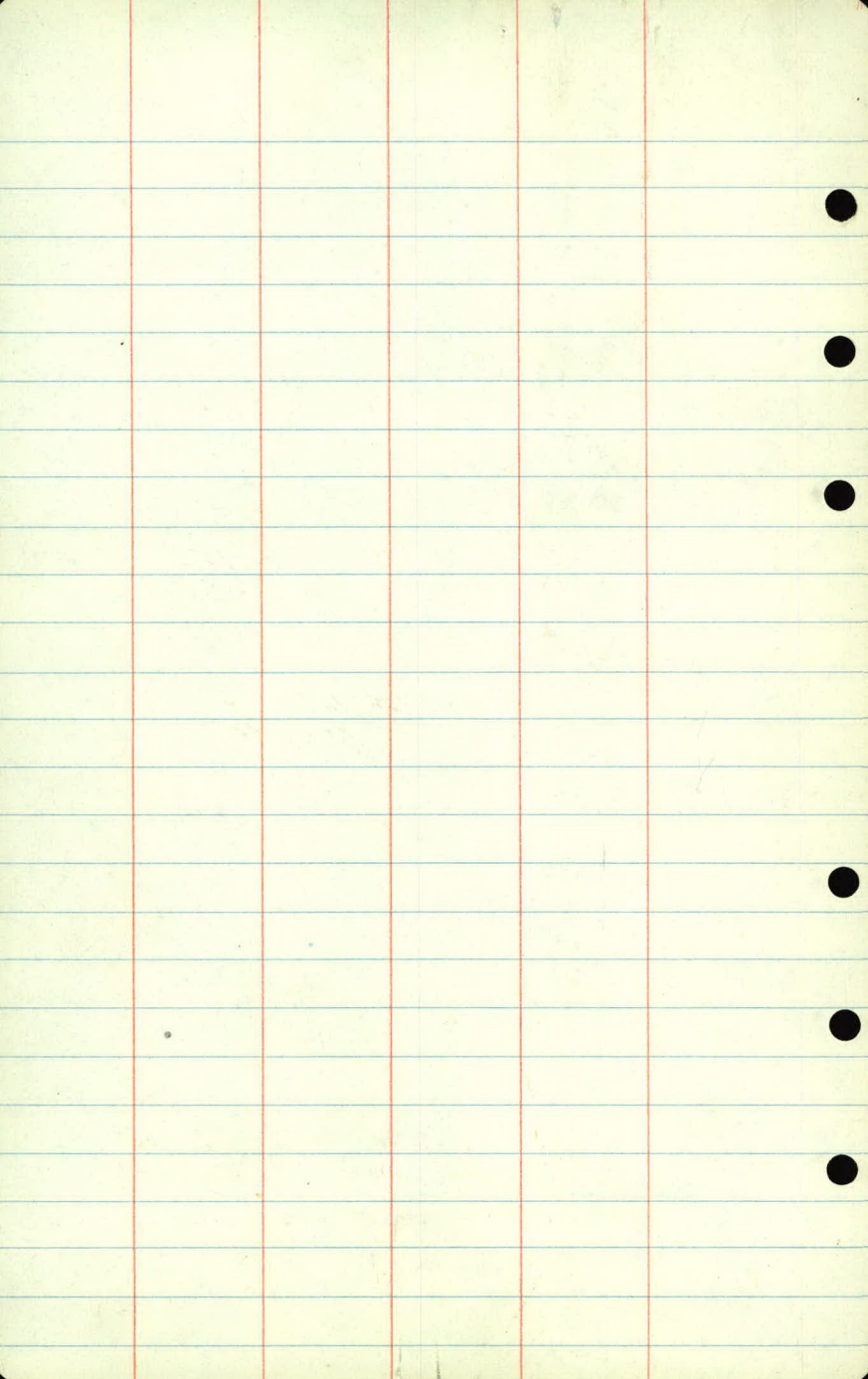
14.0
50

15.5
50

15.0

16.2
50

16.8 16.7 16.8
50 100



Lt

Rt

Rt

Slope Sta Res

El. Rd.

Sta	+	Σ	-	Elev	G. Rod
B.M	11.94	909.39		897.45	
0+34				00.3	9.1
0+42				00.3	9.1
+63					
+63				00.6	8.8
T.P					
T.P	10.01	919.40	0.00	909.39	
+82				01.9	17.5
+93				01.5	17.9
1				01.7	17.7
+50				04.6	14.8
2				08.2	11.2

0.5

2' 1 slope
15' TOP

Dip Rd

Lt

R

Rt

S.E. Cor Centerville + El. Rd

$$\begin{array}{r} 96 \\ 103 \\ \text{FO} 7 \\ \hline 164 \end{array}$$

$$\begin{array}{r} 005 \\ 86 \end{array}$$

$$\begin{array}{r} 9.2 \\ 0.6 \\ \hline 16.7 \end{array}$$

$$\begin{array}{r} 96 \\ 10.1 \\ \text{FO} 5 \\ \hline 160 \end{array}$$

$$\begin{array}{r} 012 \\ 7.9 \end{array}$$

$$\begin{array}{r} 8.2 \\ 0.14 \\ \hline 17.8 \end{array}$$

$$\begin{array}{r} 93 \\ 40 \\ \text{C} 53 \\ \hline 256 \end{array}$$

$$\begin{array}{r} 032 \\ 15.6 \end{array}$$

$$\begin{array}{r} 40 \\ 0.53 \\ \hline 25.6 \end{array}$$

$$\begin{array}{r} 18.0 \\ 11.2 \\ 0.68 \\ \hline 286 \end{array}$$

$$\begin{array}{r} 039 \\ 136 \end{array}$$

$$\begin{array}{r} 9.6 \\ 0.4 \\ \hline 31.8 \end{array}$$

$$\begin{array}{r} 18.4 \\ 9.2 \\ 0.92 \\ \hline 330 \end{array}$$

$$\begin{array}{r} 052 \\ 12.7 \end{array}$$

$$\begin{array}{r} 7.2 \\ 0.107 \\ \hline 330 \end{array}$$

$$\begin{array}{r} 18.2 \\ 8.4 \\ 0.98 \\ \hline 330 \end{array}$$

$$\begin{array}{r} 068 \\ 11.6 \end{array}$$

$$\begin{array}{r} 7.0 \\ 0.112 \\ \hline 330 \end{array}$$

$$\begin{array}{r} 15.3 \\ 7.0 \\ 0.83 \\ \hline 31.6 \end{array}$$

$$\begin{array}{r} 080 \\ 6.8 \end{array}$$

$$\begin{array}{r} 6.1 \\ 0.92 \\ \hline 330 \end{array}$$

$$\begin{array}{r} 11.7 \\ 5.2 \\ 0.65 \\ \hline 330 \end{array}$$

$$\begin{array}{r} 064 \\ 4.8 \end{array}$$

$$\begin{array}{r} 5.4 \\ 6.5 \\ \hline 330 \end{array}$$

Sta	+	7	-	Elev	G. Rod
		919.40			
2+50				11.3	8.1
3				13.6	5.8
4				15.0	4.4
4				15.5	3.9
					4.4
4+50				15.6	3.8
					4.3
5				15.7	3.7
				15.7	
4+50				15.8	4.1
6				15.8	4.1
T.P.	438	921.53	2.25	917.15	

Ditch Rod

Lt

R

Rt

86

$$\begin{array}{r} 43 \\ C 43 \\ \hline 222 \end{array}$$

C35

46

$$\begin{array}{r} 5.0 \\ C 3.6 \\ \hline 22.2 \end{array}$$

63

$$\begin{array}{r} 41 \\ C 22 \\ \hline 144 \end{array}$$

C17

41

$$\begin{array}{r} 45 \\ C 1.8 \\ \hline 18.6 \end{array}$$

49

$$\begin{array}{r} 39 \\ C 1.0 \\ \hline 17.0 \end{array}$$

C06

3.8

$$\begin{array}{r} 42 \\ C 0.7 \\ \hline 16.4 \end{array}$$

44

$$\begin{array}{r} 36 \\ C 0.8 \\ \hline 16.8 \end{array}$$

C07

32

$$\begin{array}{r} 3.5 \\ C 0.9 \\ \hline 16.8 \end{array}$$

43

$$\begin{array}{r} 35 \\ C 0.8 \\ \hline 16.6 \end{array}$$

C06

3.2

$$\begin{array}{r} 34 \\ C 0.9 \\ \hline 16.8 \end{array}$$

42

$$\begin{array}{r} 32 \\ C 1.0 \\ \hline 17.0 \end{array}$$

C05

32

$$\begin{array}{r} 3.3 \\ C 0.9 \\ \hline 16.8 \end{array}$$

41

$$\begin{array}{r} 31 \\ C 1.0 \\ \hline 17.0 \end{array}$$

C08

C28

$$\begin{array}{r} 27 \\ C 1.4 \\ \hline 17.8 \end{array}$$

41

$$\begin{array}{r} 28 \\ C 1.3 \\ \hline 17.6 \end{array}$$

C10

25

$$\begin{array}{r} 28 \\ C 1.3 \\ \hline 17.6 \end{array}$$

Sta	+	Σ	-	Elev	G. Rod
		921.53			

6+50				15.9	5.6
------	--	--	--	------	-----

7				16.0	5.5
---	--	--	--	------	-----

+50				16.1	5.4
-----	--	--	--	------	-----

8				16.1	5.4
---	--	--	--	------	-----

+50				16.2	5.3
-----	--	--	--	------	-----

9				16.3	5.2
T.P	3.15	922.57	241	918.92	

+50				16.3	6.3
-----	--	--	--	------	-----

10				16.4	6.2
----	--	--	--	------	-----

Ditch Red

Lt

2

Rt

6.1

49
C1.2
174

C0.7
49

50
C1.1
172

6.0

4.6
C1.4
17.8

C0.8
47

5.0
C1.0
17.0

5.9

4.6
C1.3
17.6

C1.1
4.3

4.7
C1.2
174

5.9

4.6
C1.3
17.6

C0.5
49

4.6
C1.3
17.6

5.8

4.8
C1.0
17.0

C0.6
4.9

5.0
C0.8
16.6

5.7

4.9
C0.8
16.6

C0.8
4.4

5.0
C0.7
164

SpK in 18" Oak 60' Lt Sta 9+00

6.8

5.3
C1.5
18.0

C0.7
5.1

5.9
C0.9
16.9

6.7

5.1
C1.6
18.2

C1.7
5.0

5.3
C1.4
17.9

Sta	+	π	-	Elev
		922.57		
10+50				16.5 6.1

11				16.6 6.0
----	--	--	--	----------

+50				16.6 6.0
-----	--	--	--	----------

12				16.7 5.9
----	--	--	--	----------

+50				16.8 5.8
-----	--	--	--	----------

13				16.9 5.7
----	--	--	--	----------

B.M	6.54	922.99	6.12	916.45
-----	------	--------	------	--------

+50				16.9 6.1
-----	--	--	--	----------

14				17.0 6.0
----	--	--	--	----------

Lt

R

Rt

6.6

$$\begin{array}{r} 5.2 \\ C1.4 \\ \hline 17.8 \end{array}$$

C0.8

5.3

$$\begin{array}{r} 4.9 \\ C1.7 \\ \hline 19.4 \end{array}$$

6.5

$$\begin{array}{r} 5.0 \\ C1.5 \\ \hline 18.0 \end{array}$$

C0.5

5.4

$$\begin{array}{r} 4.9 \\ 1.6 \\ \hline 18.2 \end{array}$$

6.5

$$\begin{array}{r} 5.0 \\ C1.5 \\ \hline 18.0 \end{array}$$

C1.0

5.0

$$\begin{array}{r} 4.6 \\ C1.9 \\ \hline 18.8 \end{array}$$

6.4

$$\begin{array}{r} 5.0 \\ C1.4 \\ \hline 17.8 \end{array}$$

C0.9

5.0

$$\begin{array}{r} 4.8 \\ C1.6 \\ \hline 18.2 \end{array}$$

6.3

$$\begin{array}{r} 5.1 \\ C1.2 \\ \hline 17.4 \end{array}$$

C0.8

5.1

$$\begin{array}{r} 4.1 \\ C2.2 \\ \hline 19.4 \end{array}$$

6.2

$$\begin{array}{r} 4.7 \\ C1.5 \\ \hline 18.0 \end{array}$$

C0.7

5.0

$$\begin{array}{r} 4.1 \\ C1.1 \\ \hline 19.2 \end{array}$$

15" B.E

15.0' Rt El. Rd

6.6

$$\begin{array}{r} 5.1 \\ C1.6 \\ \hline 18.0 \end{array}$$

C1.2

4.9

$$\begin{array}{r} 4.3 \\ C2.3 \\ \hline 19.2 \end{array}$$

6.5

$$\begin{array}{r} 5.3 \\ C1.2 \\ \hline 17.4 \end{array}$$

C1.2

4.8

$$\begin{array}{r} 4.2 \\ C2.3 \\ \hline 19.2 \end{array}$$

Sta	+	Δ	-	Elev	G.R
-----	---	----------	---	------	-----

		922.99			
--	--	--------	--	--	--

14+60					
-------	--	--	--	--	--

				17.1	5.9
--	--	--	--	------	-----

1					
---	--	--	--	--	--

15					
----	--	--	--	--	--

				17.2	5.8
--	--	--	--	------	-----

+50					
-----	--	--	--	--	--

				17.2	5.8
--	--	--	--	------	-----

16					
----	--	--	--	--	--

				17.3	5.7
--	--	--	--	------	-----

+17					
-----	--	--	--	--	--

				17.4	5.6
--	--	--	--	------	-----

+39.96					
--------	--	--	--	--	--

				17.4	5.6
--	--	--	--	------	-----

B.M					
-----	--	--	--	--	--

		6.54		916.45	
--	--	------	--	--------	--

L +

X

R +

64

$$\begin{array}{r} 5.2 \\ 01.2 \\ \hline 177 \end{array}$$

$$\begin{array}{r} C1.3 \\ 46 \end{array}$$

$$\begin{array}{r} 4.3 \\ 02.1 \\ \hline 19.2 \end{array}$$

63

$$\begin{array}{r} 5.0 \\ C1.3 \\ \hline 176 \end{array}$$

$$\begin{array}{r} C1.2 \\ 46 \end{array}$$

$$\begin{array}{r} 4.2 \\ C2.1 \\ \hline 19.2 \end{array}$$

63

$$\begin{array}{r} 4.9 \\ C1.4 \\ \hline 17.8 \end{array}$$

$$\begin{array}{r} C1.1 \\ 4.7 \end{array}$$

$$\begin{array}{r} 4.3 \\ C2.3 \\ \hline 19.0 \end{array}$$

6.2

$$\begin{array}{r} 4.4 \\ C1.8 \\ \hline 18.6 \end{array}$$

$$\begin{array}{r} C1.3 \\ 4.4 \end{array}$$

$$\begin{array}{r} 4.8 \\ C1.4 \\ \hline 17.8 \end{array}$$

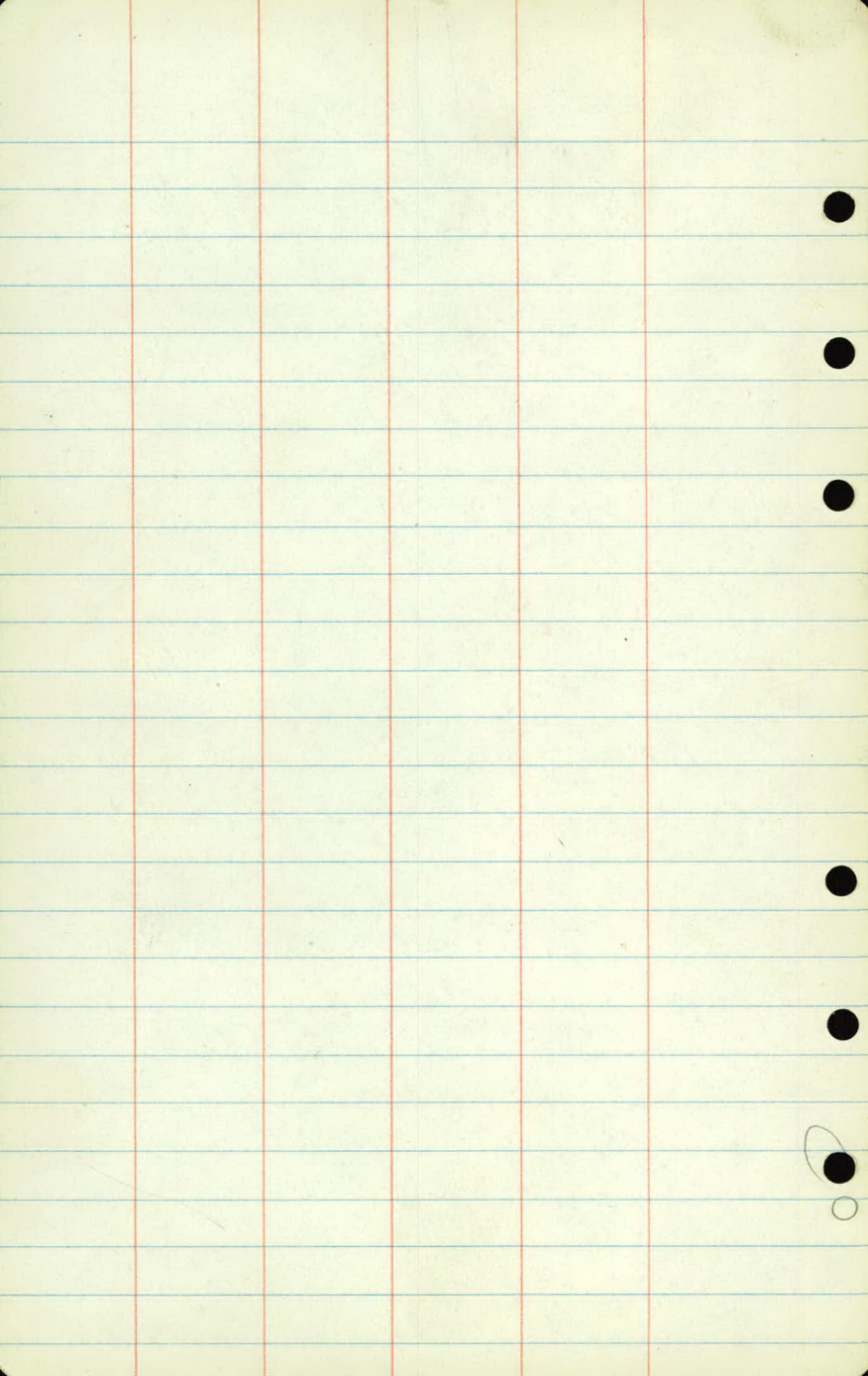
6.1

6.1

$$\begin{array}{r} C2.3 \\ 3.3 \end{array}$$

$$\begin{array}{r} 4.3 \\ C1.8 \\ \hline 18.6 \end{array}$$

R.R. Spk in 15" Learning B.F. 150' So
of Eli Rd & Desota Stv



August 4, 1961 ,

Eli Road

Profile

4 pages

drawn up on drawing #6605

8-28-61 R.C.

Sta	+	π	-	Elev.
BM	11.30	911.56 111.50		900.26 100.00

0+00			11.4	00.20 99.90
------	--	--	------	---------------------------

+16			11.1	00.5 100.2
-----	--	--	------	--------------------------

+26			11.1	00.5 100.2
-----	--	--	------	--------------------------

+50			9.5	02.1 101.8
-----	--	--	-----	--------------------------

+75			6.9	04.7 104.4
-----	--	--	-----	--------------------------

1			4.5	07.1 106.8
---	--	--	-----	--------------------------

+50			0.4	11.2 110.9
-----	--	--	-----	--------------------------

T.P.	10.64	920.86 120.60	1.34	910.22 109.96
------	-------	-----------------------------	------	-----------------------------

+69				
-----	--	--	--	--

2			7.1	13.8 113.5
---	--	--	-----	--------------------------

FX
WM
BZ

August 4, 1961 2

Top N. End Culvert NE Cor
Centerville Rd & Eli Road

± Centerville Rd

Gutter Line

13.50
7.36
Apron at
Garage
58' Lt

42.66
800 912.66
~~12.4~~
8.20
± Apron
Canc Lt
30' Lt

Sta	+	π	-	Elev.
		920.86 120.60		
2+50			6.0	14.9 14.6
3			5.1	15.8 15.5
+50			4.8	16.1 15.8
4			4.8	16.1 15.8
+50			4.8	16.1 15.8
5			4.6	16.3 16.0
+50			4.2	16.7 16.4
6			4.2	16.7 16.4
+50			4.3	16.6 16.3
7			4.2	16.7 16.4

Aug 3, 1961

3

Sta	+	Δ	-	Elev
		920.86 120.60		

7+50			4.1	16.8 16.5
------	--	--	-----	-------------------------

8			4.0	16.9 16.6
---	--	--	-----	-------------------------

+50			4.0	16.9 16.6
-----	--	--	-----	-------------------------

9			4.1	16.8 16.5
---	--	--	-----	-------------------------

+50			3.9	17.0 16.7
-----	--	--	-----	-------------------------

10			3.5	17.4 17.1 800 26 917.36
----	--	--	-----	---

+50			3.4	17.5 17.2
-----	--	--	-----	-------------------------

11			3.5	17.4 17.1
----	--	--	-----	-------------------------

+50			3.3	17.6 17.3
-----	--	--	-----	-------------------------

12			3.1	17.8 17.5 108 14 29 28
----	--	--	-----	--

Aug. 4, 1961

4

Sta	+	x	-	Elev.
-----	---	---	---	-------

		920.86		
		120.60		

12+50				
-------	--	--	--	--

			2.9	
--	--	--	-----	--

				18.0
--	--	--	--	------

				17.7
--	--	--	--	-----------------

13				
----	--	--	--	--

			2.9	
--	--	--	-----	--

				18.0
--	--	--	--	------

				17.7
--	--	--	--	-----------------

August 24, 1961 5

9	41
34.2	48
1	.7

2 -

Bench Levels

Sta	+	π	-	Elev.
BM	6.28	922.73		(916.45)
	0.84	922.30	1.27	921.46
		$\frac{18.92}{3.38}$		
BM			3.38	918.82 (918.92)
10			4.98	917.32
BM	2.00	921.98	2.32	919.98
TP	3.15	919.68	5.45	916.53
			7.04	912.44
TP	1.35	909.69	11.34	908.34
BM			9.43	900.26

1+60 S.W. Cor Garage 58'11"

FR
WM
BZ
DF

August 24, 1961

5

Spike in leaning 15" BE 150' S of Eli Rd at Desoto

Spike in 18" Oak 60' Lt Sta 9+00

SW. Cor Lower Step Ho[#] 421 Eli Rd

Nail in Transformer PP Sta 4+50±

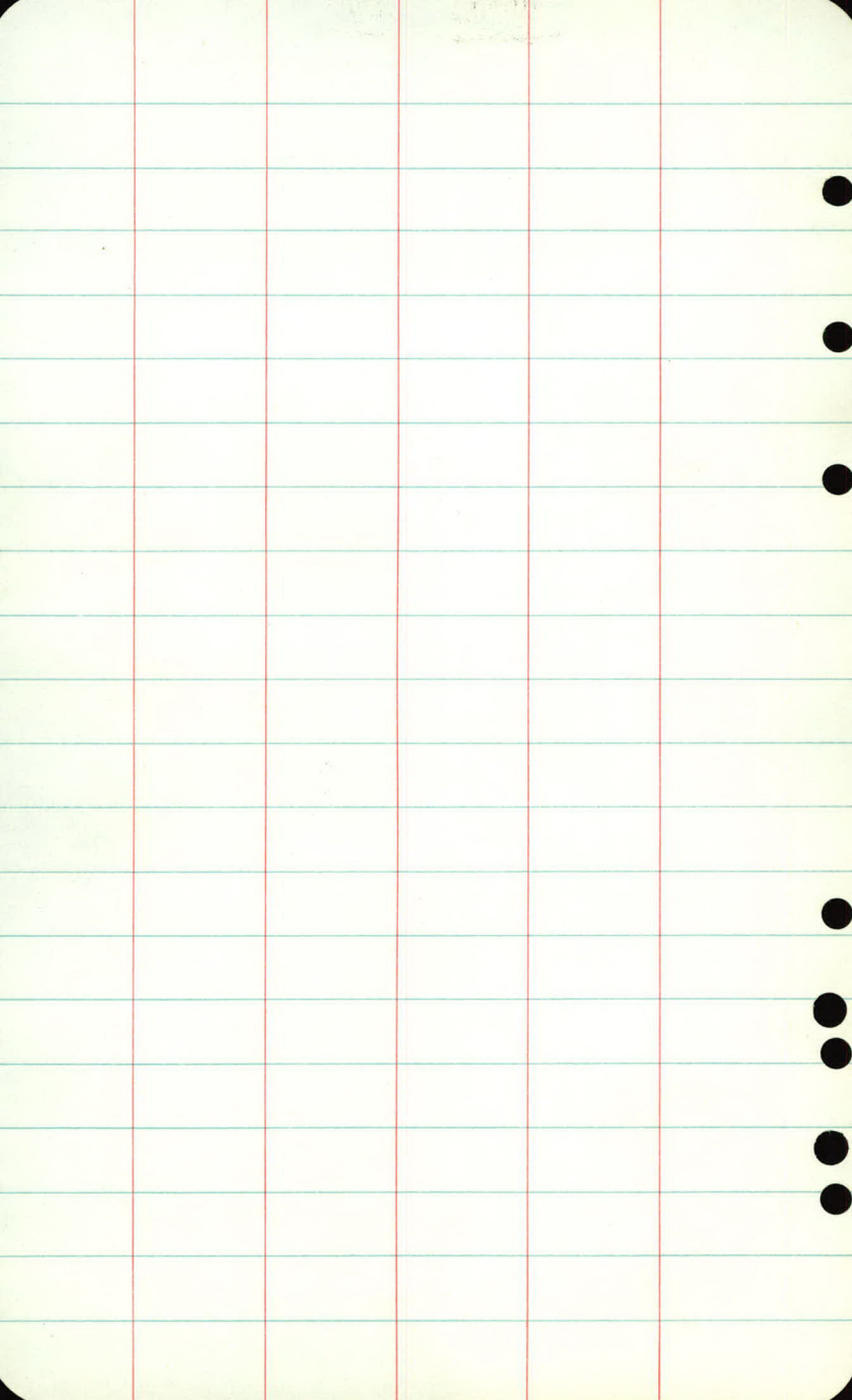
conc. Ent slab Lt Sta 1+69

Top N. End Culvert NE. Cor Centerville & Eli

3.41
2.32
1.09

E 40 W

N 22 S



1
Eli Road

Staking

DGR

Sta	PG	PCR	-	Elev
BM	13.74	914.00		900.26

0+55	00.55	13.45	14.0 17.3 <u>6.5</u>	2.8
------	-------	-------	----------------------------	-----

1	4.25	9.25	9.75 3.45 <u>7.3</u>	8.6 17.2
	06.86			

+50	8.87	6.13	6.63	
TP	6.40	920.17	0.23	913.77
+75	10.58			

2	12.00	8.17	8.67	
---	-------	------	------	--

+25	13.26			
-----	-------	--	--	--

+50	14.3	5.9	6.4	
-----	------	-----	-----	--

+75	15.3 ✓			
-----	--------	--	--	--

3	15.50 ✓	4.67	5.2	
---	---------	------	-----	--

+50	15.63	4.54		
-----	-------	------	--	--

4	15.75	4.42		
---	-------	------	--	--

+50		4.29		
-----	--	------	--	--

PK.
WM
MMe.

Sept 26, 1961
Clear Cool 58° 2

Top N. End Culvert NE Cor Centerville.

$\left\{ \begin{array}{l} 7.5 \\ D 6.5 \\ 28' \end{array} \right\}$

$\left\{ \begin{array}{l} 11.2 \\ D 28 \\ 20.6 \end{array} \right\}$

$\left\{ \begin{array}{l} 2.45 \\ D 7.3 \\ 29.6 \end{array} \right\}$

$\left\{ \begin{array}{l} 1.3 \\ D 5.3 \\ 25.6 \end{array} \right\}$

$\left\{ \begin{array}{l} 0.4 \\ D 6.2 \\ 27.4 \end{array} \right\}$

$\left\{ \begin{array}{l} 1.45 \\ D 8.3 \\ 31.2 \end{array} \right\}$

$\left\{ \begin{array}{l} 6.0 \\ D 2.7 \\ 20.4 \end{array} \right\}$

$\left\{ \begin{array}{l} 5.8' \\ D 20 \\ 20.8 \end{array} \right\}$

$\left\{ \begin{array}{l} 5.3 \\ D 1.1 \\ 12.2 \end{array} \right\}_{5.50}$

$\begin{array}{l} 5.2 \\ D 1.2 \\ 12.4 \end{array}$

$\begin{array}{l} 4.2 \quad 4.67 \\ \text{ET. 0.2 Gv} \end{array}$

$\begin{array}{l} 5.2 \quad 4.67 \\ \text{BT} \quad \text{2 Gv} \\ \text{2 Grade} \end{array}$

✓

✓

✓

✓

✓

✓

Sta	PG	PCR	-	Elev.
		920.17		
5	16.00	4.17		
+50		4.04		
6	16.25	3.92		
BM	5.53	922.06	3.64	916.53
		^{16.25} _{5.53}		(916.53)
+50	16.37	5.69		
7	16.50	5.56		
+50	16.63	5.43		
8	16.75	5.31		
+50		5.18		
9	17.00	5.06		

20' Lt

Sept. 20, 1961

3

20' Rt

✓

✓

✓

✓

✓

✓

Nail in PP Lt Sta 4+50⁺ Transformer Pole

✓

✓

4.56

C1.0

✓

4.43 C1.0

✓

✓

✓

4.18

C1.0

✓

✓

✓

Sta	PG	PGR	-	Elev.
		922.06		
9+50	17.13	4.93		
	4.23	922.36	3.93	918.13
10	17.25	5.11		
+50		4.98		
11	17.50	4.86		
+50		4.73		
12	17.75	4.61		
+50				
13	18.00			
+50				

20' L1

£

20' R1

✓

✓

✓

✓

✓

✓

✓

✓

✓

Sta	PG	PCR	DGR	
	13.21	913.47		900.26
0+55	00.55	12.92	13.42	
			13.9	
1	4.75	9.72	10.22	
+50	8.87	4.60	5.1	0.5
2	12.0	1.47	1.97	
		⁵	^{2.5}	
TP	7.15	920.19	0.43	913.04
		(919.85)		
+50	14.1	5.75	6.25	
		7.35	8.35	
			4.34	915.85
3	15.0	4.85	5.35	
		⁵		
+50	15.25	4.60	5.10	
4	15.50	4.35	4.85	
+50	15.75	4.10	4.60	
5	16.0	3.85	4.35	
		919.85	3.32	916.82 916.53

12.2 10.2
C2.0

12.9

12.9 13.5

12 Gr

8.7
C1.0

9.8
Gr

46
Gr

46
Gr

0.72
C1.0

Gr

5.25
C1.0

5.25
C1.0

✓

✓

C1.0

C1.0

C1.0

C1.0

Gr

