

Book 41 Dr. 12A

OFFICE OF COUNTY ENGINEER
RAMSEY CO. MINN.

Plan _____ Survey _____
Grade stakes - 8700 to 8723

_____ MARYLAND ST. _____

From Plum St. To East Co. Line

Road Acc't. No. _____

Date Filed 3-16-44

File _____

1

St.
MARYLAND ~~Ave~~

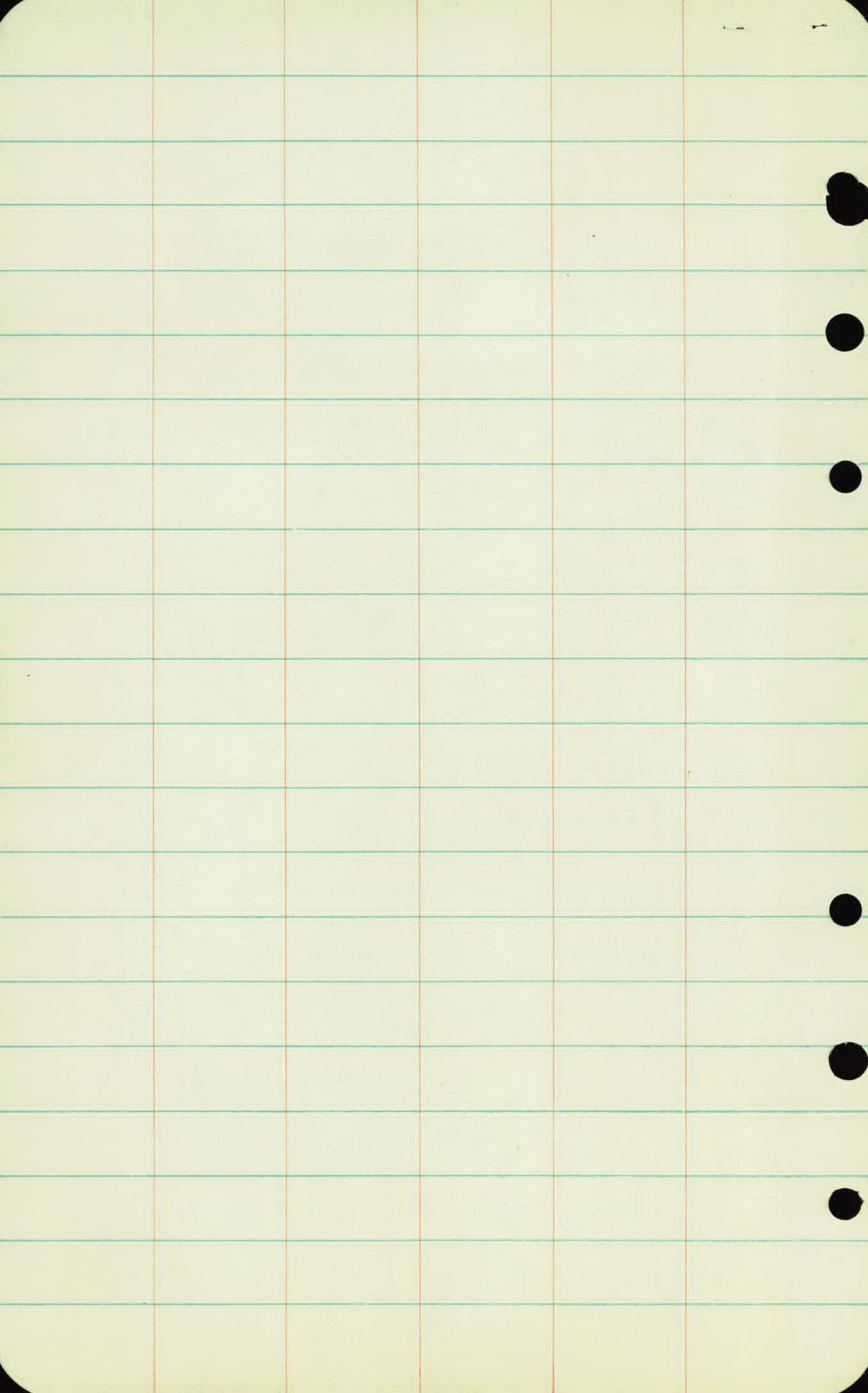
East Ave to Lakewood Dr.

Plan Survey

INDEX:

Align	2-3	30 pages
Topog	4-7	
Bench	8-9	
X-Sec.	10-30	

Rec'd. 2/25/57
K.A.



Dec 5, 1936

2

FA
RG
KP
WH

Alignment

Sta	Point	ΔLt	ΔRt
-----	-------	-------------	-------------

13+22.68	± Lakewood Dr		
----------	---------------	--	--

0+00	± East Ave		
------	------------	--	--

FK
RG
KR
WH

Dec. 6, 1956
Cloudy Snowing 15°

3

G.P. 0 34.13 25.06 0 G.P.
26.62 0 P.P.

Iron

P.P. 0

119.27

167.18

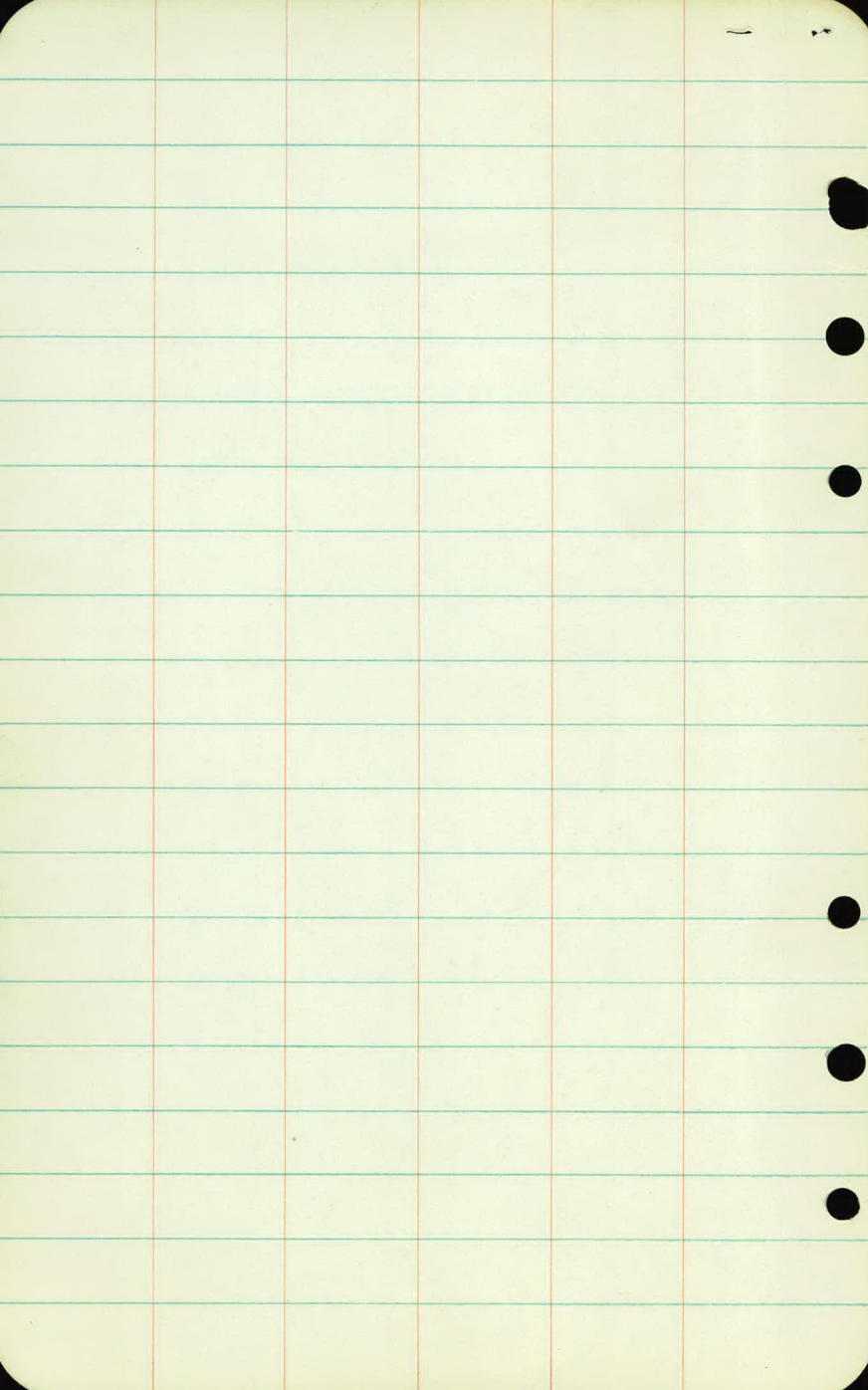
0 PP

30.03 0 Arc. Lt.

Mant

80.45
A2.82
8 Hyd

Cor.
Fo.



Dec 6, 1956

A

Topography

5

Road
14-12

+98 Garage shed
52 76.6

+86 PP
28

+42 Fe Cor
33

+78 STP
22

Road
2-14

+39 6"0
47

+37 12"0
40 (175+PS)
20-40'

+54 End SWP
6.5'

+27 6"0
41

+25 PP
29

3

SWP
164-16

Road
1-145

+12 6"0
45

2

SWP
100'-8"
12"CM
+92 12.7

Road
1'-13
12x32 CM
x Drain

+86 12"CM
18.8

PP
+64 29

+60 SWP
12-20

+20 10 STP
+15 12-20'

+18 20 STP
+90 23-30

1

Road
2-11

+85 STP
25

+90 Lin Ditch
33

+65 Lin Ditch
71

+34 ER
12

+50 Ditch
145

+44 PP
31

0

+03 E.R.
40

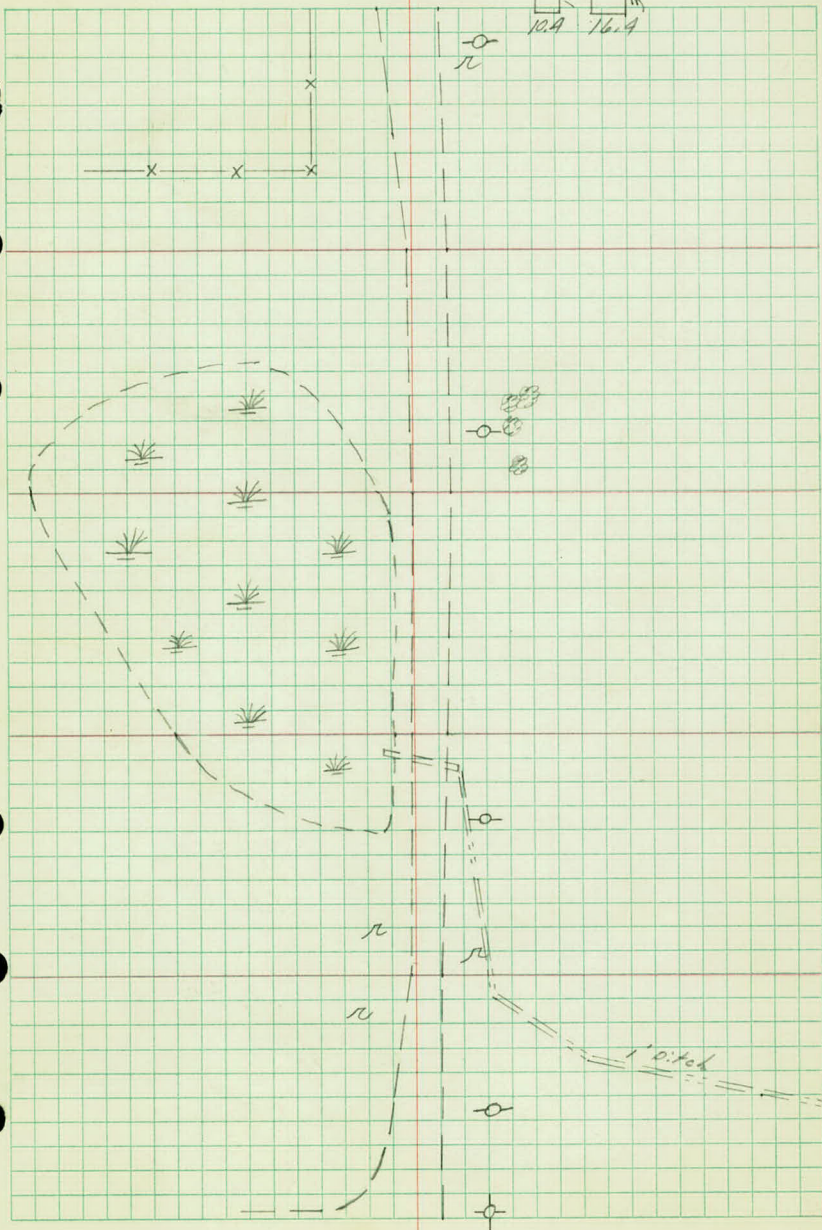
+03 Arch Lt.
30'

+00 Road
10

Dec 6, 1956

5

10.4 12.7 16.4 30.4



10 +00 $\frac{2 \text{ Ent}}{51}$ 10+00 $\frac{\text{N. Pt. of Island}}{42}$ Road $\frac{16-2}{16-2}$ 10+00 $\frac{\text{NW Corner of House}}{44}$
 +91 $\frac{\text{Island (W. Edge)}}{16}$ +75 PP +84 4"0.
 +72 $\frac{\text{Rtic}}{\text{Ent 11}}$ 23 33

20 Stumps
5'-60'

7 Road $\frac{13-4}{13-4}$ +01 $\frac{8"0.}{35}$
 +76 $\frac{10"BE}{37}$
 +66 $\frac{5"0}{39}$ +45 $\frac{8"0}{40}$

27 Stumps
14-31

8 ? Road $\frac{9-2.6}{9-2.6}$ +19 $\frac{PP}{25}$ +08 $\frac{6"BE}{43}$ +18 $\frac{10"0}{41}$
 +93 $\frac{\text{Row Seedling Pines}}{31.}$ 4"Elm +97 $\frac{8"Elm}{33}$?
 +68 $\frac{4"Elm}{33}$ +80 $\frac{\text{Ent 12 X 20 CM}}{18}$

19 Stumps
15-40

+138 $\frac{4"Elm}{33.8}$ +77 $\frac{6"0}{43}$ +80 $\frac{6"0}{47}$
 +33 $\frac{\text{S.W. Cor Ho}}{73}$ +08 $\frac{4"Elm}{33.5}$ +59 $\frac{14"0}{42}$
 7 +01 $\frac{\text{Fe Cor}}{33}$ Road $\frac{7-9.5}{7-9.5}$ +74 $\frac{4"0}{40}$

+98 $\frac{6"0}{36}$
 12 Stumps
20-40'

+139 $\frac{6"0}{39}$ +47 $\frac{5"0}{41}$ +55 $\frac{6"0}{43}$
 +41 $\frac{PP}{26}$ +41 Begin
 Stumps Rt

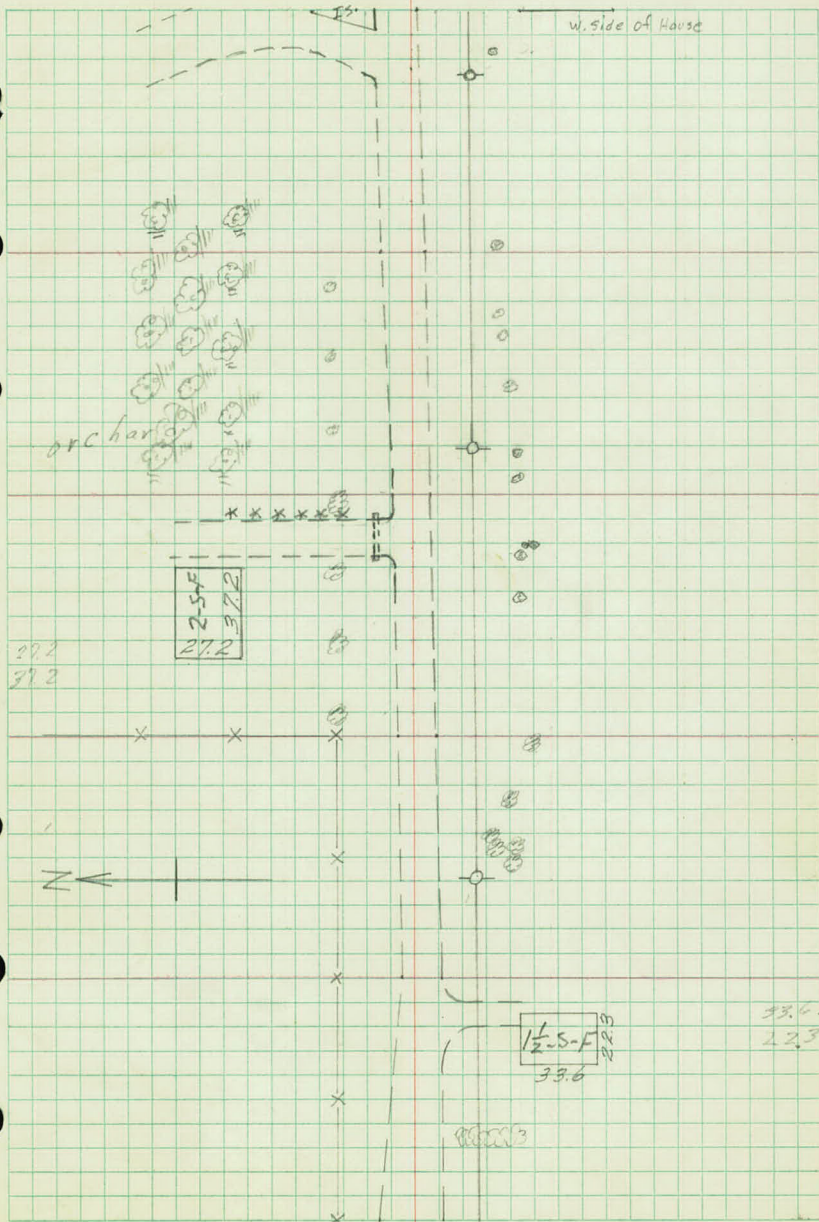
6 Fe 33 Road $\frac{6-11}{6-11}$ +93 $\frac{\text{Ent}}{\text{Rt}}$
 165 $\frac{\text{NW Cor Ho}}{44.5}$
 Lilac Hedge
 +35 17-45

5

JAN 17, 1956
 10°-15° Snow

RG
 KP
 WH

6



$$\begin{array}{r}
 120 \text{ Edge Rd} \\
 \underline{2} \\
 134 \text{ ER} \\
 \underline{61} \\
 22.8 \\
 \text{Iron}
 \end{array}
 \quad
 \begin{array}{r}
 142 \text{ guy pole} \\
 \underline{17}
 \end{array}$$

$$\begin{array}{r}
 +00 \text{ guy pole} \\
 \underline{28} \\
 3 \text{ stumps} \\
 28-33-28
 \end{array}
 \quad
 \begin{array}{r}
 114 \text{ ER} \\
 \underline{26} \\
 \text{Road} \\
 11-11
 \end{array}
 \quad
 \begin{array}{r}
 +01 \text{ PP} \\
 \underline{17}
 \end{array}$$

$$\begin{array}{r}
 +40-55 \\
 \underline{28-33-28}
 \end{array}
 \quad
 \begin{array}{r}
 130 \text{ in radius} \\
 \underline{2} \\
 +70
 \end{array}
 \quad
 \begin{array}{r}
 +92 \text{ guy pole} \\
 \underline{17}
 \end{array}$$

$$\begin{array}{r}
 173 \text{ ER} \\
 \underline{17}
 \end{array}
 \quad
 \begin{array}{r}
 +53 \text{ SW Cor. Foundation} \\
 \underline{64'} \\
 \text{Abandoned}
 \end{array}$$

$$\begin{array}{r}
 \text{Road} \\
 \underline{16-1} \\
 195 \text{ Ent Rd} \\
 \underline{2'} \\
 18A \text{ Ent} \\
 \underline{21} \text{ Shed} \\
 20 \times 19 \\
 +44 \text{ 26}
 \end{array}
 \quad
 \begin{array}{r}
 +95 \text{ 10" Elm} \\
 \underline{37} \\
 +95 \\
 +51 \text{ PP} \\
 \underline{18}
 \end{array}$$

$$\begin{array}{r}
 +08 \text{ 9" Apple} \\
 \underline{33}
 \end{array}$$

$$\begin{array}{r}
 \text{Road} \\
 \underline{14-2}
 \end{array}$$

$$\begin{array}{r}
 +90 \text{ 10" Apple} \\
 \underline{33} \\
 +49 \text{ 1 Cement wall} \\
 \underline{7-Garage}
 \end{array}$$

$$\begin{array}{r}
 +37 \text{ Garage} \\
 \underline{59'} \\
 +33 \text{ Brick wall} \\
 \underline{24}
 \end{array}$$

$$\begin{array}{r}
 +45 \text{ Range tie} \\
 \underline{\text{Ent Lt}}
 \end{array}$$

$$\begin{array}{r}
 +40 \text{ 1/2" x 16" cm} \\
 \underline{5w-7E}
 \end{array}$$

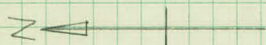
$$\begin{array}{r}
 +23 \text{ E. edge of Island} \\
 \underline{16 \text{ Road}} \\
 16-2
 \end{array}$$

$$\begin{array}{r}
 +16 \text{ 36" Elm} \\
 \underline{37} \\
 +18-30 \text{ Lilac hedge} \\
 \underline{3}
 \end{array}$$

JAN 17, 1956
10°-15° Snow

RG
KP
WH

7



guy pole

Surrounded
by
Brush

22.5

Sked

18

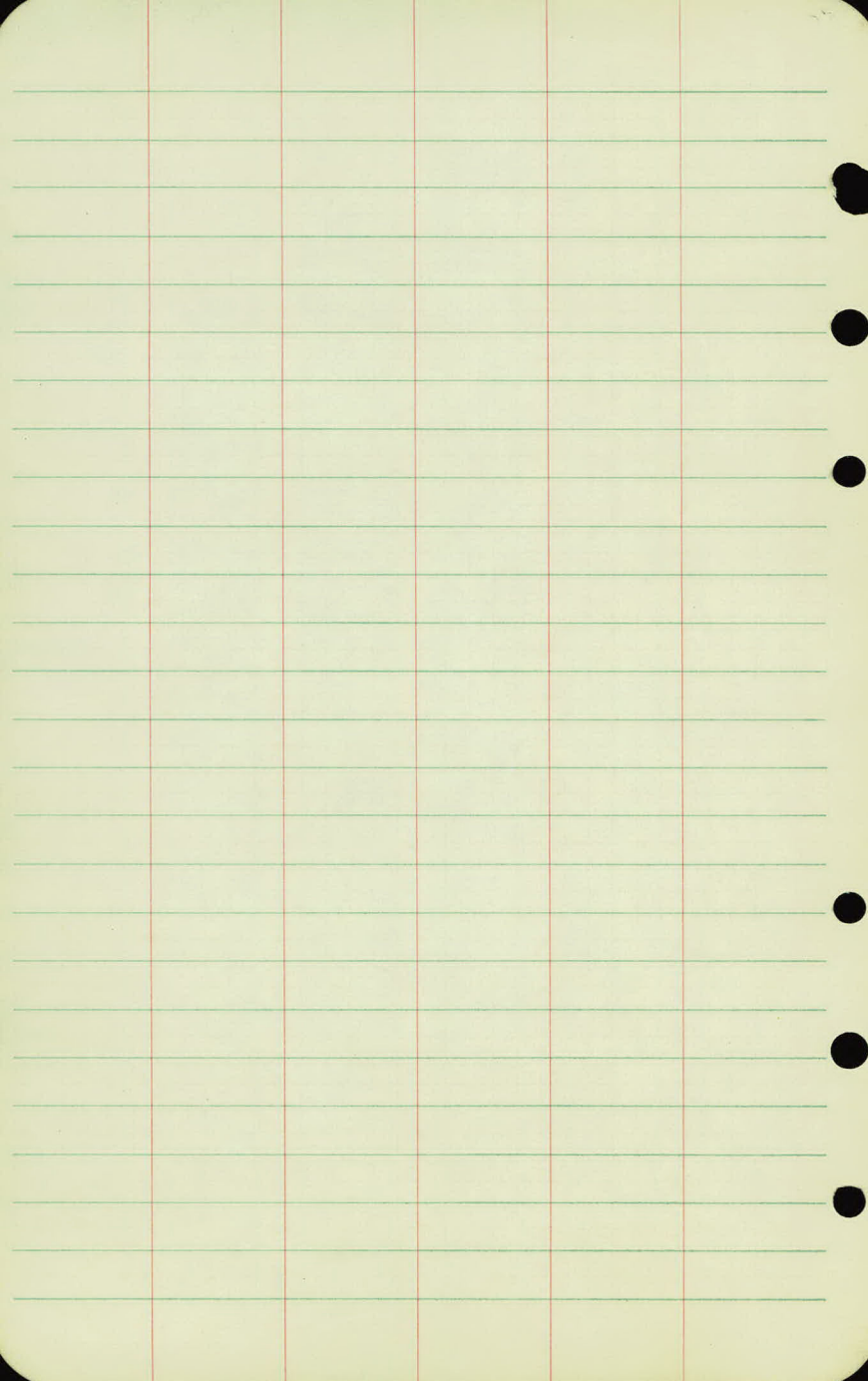
14

27.5

12-5-5

40.5

Island



FX
RG
WH
MH

Feb 15, 1957
Cloudy Windy 30°

8

Bench Levels

Sta	+	π	-	Elev
BM	0.279	975.529		(975.25)
TP	13.320	977.184	11.665	963.864
TP	12.007	987.528	1.663	975.521
BM			1.15	986.38 (986.38)
TP	0.940	976.848	11.62	975.908
BM			6.266	970.582 (970.58)
TP	0.541	966.429	10.960	965.888
BM	9.317	9.66.429	9.317	957.112 (957.11)
TP	13.445	979.334	0.54	965.889
BM			8.744	970.590 (970.58)
TP	11.47	987.38	3.429	975.910
BM			0.985	986.395 (986.38)
TP	3.065	978.605	11.84	975.54
TP	9.97	975.735	12.84	965.765
TP			11.885	963.850
BM			0.49	975.245 (975.25)

Feb 15, 1957

9

Top Hyd N.W. Cor East Ave + Maryland

E End Front Door Sill Ho #2325 Maryland

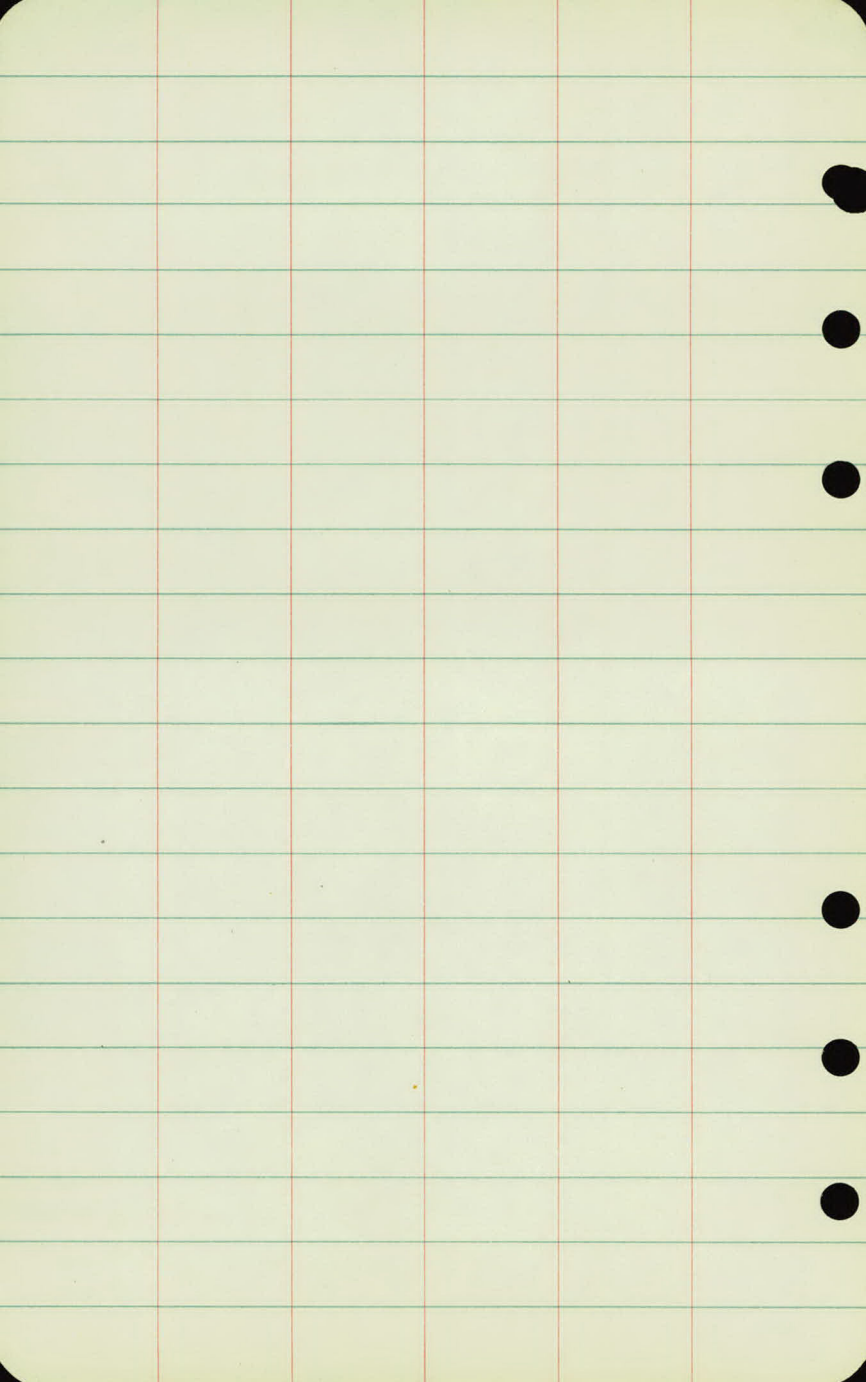
Nail in Dead Apple Branch 33' Rt Sta 11408

Spike in G.P. S.E. Cor Maryland + Lakewood Dr.

Nail in dead apple 33' Rt Sta 11408

E. End Front Door Sill Ho #2325 Maryland

Top Hyd N.W. Cor East Ave + Maryland



Maryland
E. Ave to Lakewood Dr.

additional x-sections

Rec 3/21/57

3:00 P.M.

L.C.

Sta + π - E/ev.

BM 11.96 987.21

975.25

3+59

✓

+ 83

4+00

+31

RG
XP
FS

March 21, 1957

RT

6

Top Hyd N.W. Cor Maryland & East Ave

✓ 72.6	16.0	77.9	80.6	80.1	81.3
14.6	11.2	9.3	6.6	7.1	5.9
23	36	42	52	59	80

80.5	81.2
6.7	6.0
100	95

✓ 10.9	80.0	81.7	82.6	83.2	83.1	80.3
16.3	7.2	5.5	4.6	4.0	4.1	6.9
22	30	36	49	66	81	100

✓ 73.7	82.5	83.4	83.5	84.1	83.6	80.3
13.5	4.7	3.8	3.7	3.1	3.6	6.9
25	36	40	53	67	82	100

✓ 78.6	79.6	83.9	84.0	83.6	82.6	80.8
8.6	7.6	3.3	3.2	3.6	4.6	6.4
31	36	46	50	58	68	82

76.8	78.6	80.3
10.4	8.6	6.9
100	94	89

Sta	+	π	-	Elev
-----	---	-------	---	------

		987.21		
--	--	--------	--	--

4+50				
------	--	--	--	--

4+69				
------	--	--	--	--

5+00				
------	--	--	--	--

March 26/1957

✓

BT

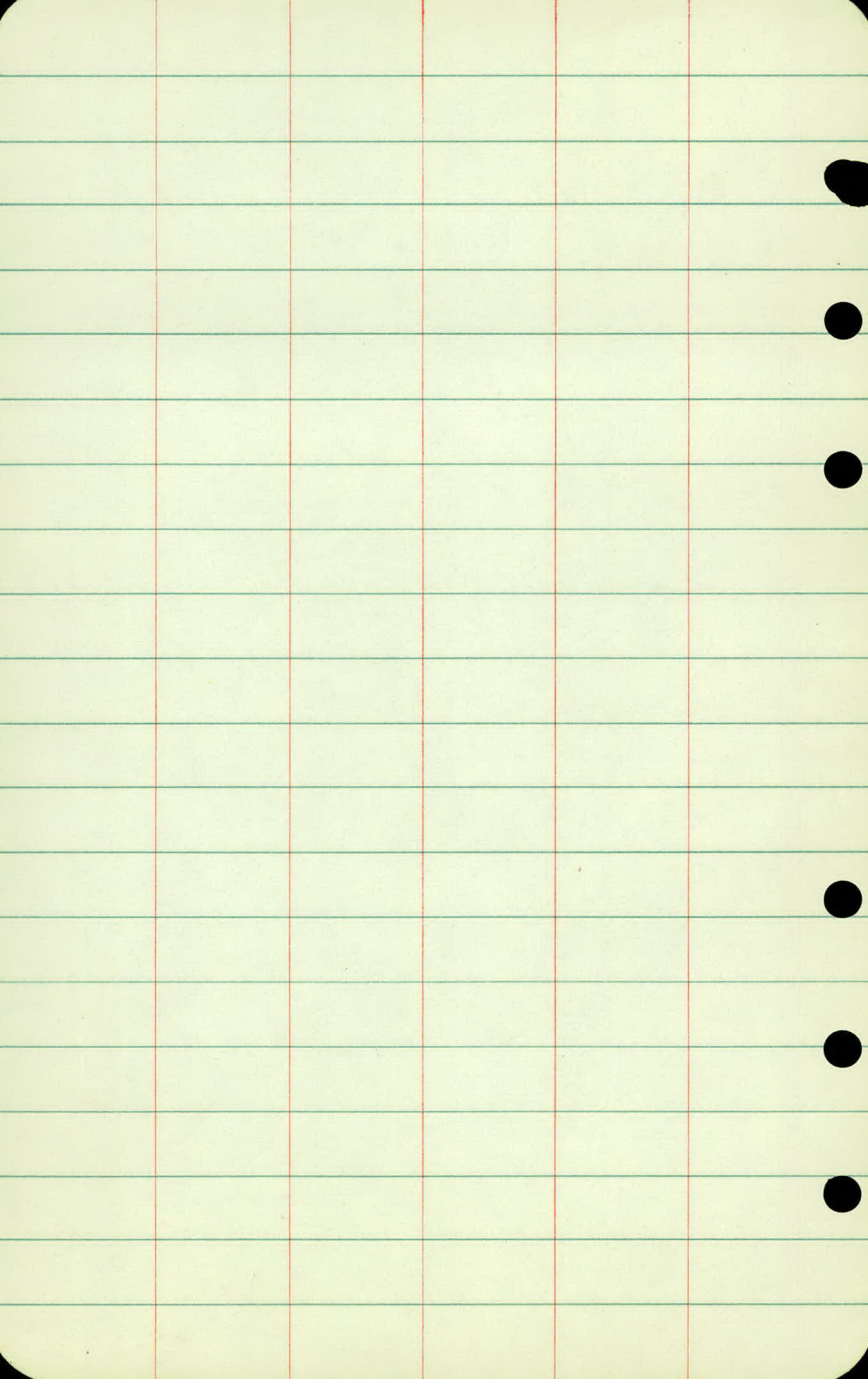
c

78.8	82.8	83.3	82.9	81.6	79.6	74.1
8.4	4.4	3.9	4.3	5.6	7.6	13.1
26	31	36	48	64	78	100

✓

81.9	82.4	82.0	80.8	79.8
5.3	4.8	5.2	6.4	7.4
25	33	48	63	73

75.1	79.4	80.9	80.4	80.6	80.7	78.6
12.1	7.8	6.3	6.8	6.6	6.5	8.6
5	21	29	34	43	49	52
						Garage



FK
RG
WH
MH

Feb 18, 1957
Cold Windy 11°

10

X-Sections

Sta	+	π	-	Elev.
-----	---	-------	---	-------

BM	0.12	975.37		
----	------	--------	--	--

				975.25
--	--	--	--	--------

0-50				
------	--	--	--	--

			4.0	971.4
--	--	--	-----	-------

0-100				
-------	--	--	--	--

			1.8	73.6
--	--	--	-----	------

0-150				
-------	--	--	--	--

			0.3	75.1
--	--	--	-----	------

0+00				
------	--	--	--	--

✓				
---	--	--	--	--

+23				
-----	--	--	--	--

+47				
-----	--	--	--	--

Feb 18, 1957

Lt

Rt

11

Top Hyd NW Cor Maryland & East Ave

72.1	71.6	70.7	70.2	70.0 ⁵ ₀₂	69.6	69.3	69.5	70.0
3.3	3.8	4.7	5.2	5.35	5.8	6.1	5.9	5.4
50	41	24	13		10	13	17	30

67.0	68.4	68.9
8.4	7.0	6.5
50	42	36

68.6	68.1	69.0	69.1	69.0	68.1	68.4	68.7	68.9	67.0	67.6
6.8	6.7	6.4	6.3	6.4	6.3	7.0	6.7	6.5	8.4	9.2
50	46	38	28	19		12	16	28	37	50

65.5	65.6	65.9	67.1	67.5	67.8	67.1	67.1	67.0	65.4	65.4
9.9	9.8	9.5	8.0	7.9	7.6	8.3	8.3	8.4	10.0	10.5
50	40	32	20	12		12	18	24	32	45

64.8
10.6
50

Sta + π - Elev

975.37

0 + 71

✓

1

✓

TP 5.29 971.05 9.61 965.76

+37

Feb 18, 1957

LT

RT 12

$\bar{b}A.7$	$\bar{b}5.1$	$\bar{b}6.1$	$\bar{b}6.1$	$\bar{b}6.8$	$\bar{b}6.2$	$\bar{b}6.2$	$\bar{b}6.1$	$\bar{b}A.2$	$\bar{b}3.2$
10.7	10.0	9.0	9.0	8.6	9.2	9.2	10.3	11.2	12.2
29	22	15	11		13	21	27	36	50

$\bar{b}A.4$	$\bar{b}A.0$	$\bar{b}A.0$
11.0	11.4	11.4
36	43	50

$\bar{b}A.4$	$\bar{b}5.2$	$\bar{b}5.1$	$\bar{b}5.6$	$\bar{b}5.9$	$\bar{b}5.2$	$\bar{b}5.2$	$\bar{b}3.8$
11.0	10.2	10.0	9.8	9.5	10.2	10.2	11.6
21	15	10	4		14	18	30

$\bar{b}3.8$	$\bar{b}3.2$	$\bar{b}3.2$
11.6	12.2	12.2
30	40	50

$\bar{b}3.7$	$\bar{b}3.6$
11.7	11.8
50	39

$\bar{b}3.3$	$\bar{b}3.5$	$\bar{b}4.4$	$\bar{b}4.9$	$\bar{b}4.9$	$\bar{b}4.7$	$\bar{b}4.5$	$\bar{b}3.4$	$\bar{b}3.0$
7.8	7.6	6.7	6.2	6.2	6.4	6.6	7.7	8.1
19	14	12	6		12	14	17	26

$\bar{b}3.1$	$\bar{b}3.1$	$\bar{b}3.0$
8.0	8.0	8.1
30	42	50

$\bar{b}4.6$	$\bar{b}4.2$	$\bar{b}3.9$	$\bar{b}3.4$
6.5	6.9	7.2	7.7
50	44	38	31

Sta	+	π	-	Elev.
-----	---	-------	---	-------

Sta	+	π	-	Elev.
-----	---	-------	---	-------

97105

Sta	+	π	-	Elev.
-----	---	-------	---	-------

1+69

Sta	+	π	-	Elev.
-----	---	-------	---	-------

✓

Sta	+	π	-	Elev.
-----	---	-------	---	-------

+86 Rt

Sta	+	π	-	Elev.
-----	---	-------	---	-------

+92 Lt

Sta	+	π	-	Elev.
-----	---	-------	---	-------

2+00

Sta	+	π	-	Elev.
-----	---	-------	---	-------

✓

Sta	+	π	-	Elev.
-----	---	-------	---	-------

+40

£ Feb 18, 1957

LT

RT 13

$\begin{smallmatrix} .8 \\ 62. \end{smallmatrix}$	$\begin{smallmatrix} .8 \\ 62. \end{smallmatrix}$	$\begin{smallmatrix} .9 \\ 63. \end{smallmatrix}$	$\begin{smallmatrix} .3 \\ 64. \end{smallmatrix}$	$\begin{smallmatrix} .4 \\ 64. \end{smallmatrix}$	$\begin{smallmatrix} .3 \\ 64. \end{smallmatrix}$	$\begin{smallmatrix} .0 \\ 64. \end{smallmatrix}$	$\begin{smallmatrix} .8 \\ 62. \end{smallmatrix}$	$\begin{smallmatrix} .0 \\ 63. \end{smallmatrix}$
8.3	8.3	7.2	6.8	6.7	6.8	7.1	8.3	8.1
21	12	8	4		11	15	20	25

$\begin{smallmatrix} .8 \\ 62. \end{smallmatrix}$	$\begin{smallmatrix} .8 \\ 62. \end{smallmatrix}$	$\begin{smallmatrix} .7 \\ 62. \end{smallmatrix}$
8.3	8.3	8.4
32	42	50

$\begin{smallmatrix} .2 \\ 65. \end{smallmatrix}$	$\begin{smallmatrix} .0 \\ 65. \end{smallmatrix}$	$\begin{smallmatrix} .8 \\ 65. \end{smallmatrix}$
5.9	6.1	5.3
50	43	32

$\begin{smallmatrix} .9 \\ 61. \end{smallmatrix}$
 9.06
 FL 12" CM
 12.7

$\begin{smallmatrix} .37 \\ 62. \end{smallmatrix}$
 8.68
 FL 12" CM
 18.8

$\begin{smallmatrix} .6 \\ 62. \end{smallmatrix}$	$\begin{smallmatrix} .7 \\ 62. \end{smallmatrix}$	$\begin{smallmatrix} .7 \\ 62. \end{smallmatrix}$	$\begin{smallmatrix} .9 \\ 63. \end{smallmatrix}$	$\begin{smallmatrix} .9 \\ 63. \end{smallmatrix}$	$\begin{smallmatrix} .0 \\ 64. \end{smallmatrix}$	$\begin{smallmatrix} .7 \\ 62. \end{smallmatrix}$	$\begin{smallmatrix} .9 \\ 62. \end{smallmatrix}$	$\begin{smallmatrix} .9 \\ 62. \end{smallmatrix}$
8.5	8.4	8.4	7.2	7.2	7.1	7.4	8.2	8.2
34	21	12	5		11	15	18	24

$\begin{smallmatrix} .6 \\ 62. \end{smallmatrix}$	$\begin{smallmatrix} .6 \\ 62. \end{smallmatrix}$
8.5	8.5
44	50

$\begin{smallmatrix} .6 \\ 65. \end{smallmatrix}$	$\begin{smallmatrix} .9 \\ 65. \end{smallmatrix}$	$\begin{smallmatrix} .2 \\ 66. \end{smallmatrix}$	$\begin{smallmatrix} .9 \\ 65. \end{smallmatrix}$
5.5	5.2	4.9	5.2
50	41	37	31

$\begin{smallmatrix} .6 \\ 62. \end{smallmatrix}$	$\begin{smallmatrix} .6 \\ 62. \end{smallmatrix}$	$\begin{smallmatrix} .6 \\ 62. \end{smallmatrix}$	$\begin{smallmatrix} .7 \\ 62. \end{smallmatrix}$	$\begin{smallmatrix} .7 \\ 63. \end{smallmatrix}$	$\begin{smallmatrix} .0 \\ 64. \end{smallmatrix}$	$\begin{smallmatrix} .2 \\ 64. \end{smallmatrix}$	$\begin{smallmatrix} .1 \\ 64. \end{smallmatrix}$	$\begin{smallmatrix} .9 \\ 63. \end{smallmatrix}$	$\begin{smallmatrix} .4 \\ 63. \end{smallmatrix}$
8.5	8.5	8.5	8.4	7.4	7.1	6.9	7.0	7.2	7.7
50	32	24	11	6		7	14	18	20

Sta + π - Elev

971.05

2+40

+67

✓

+80

✓

3

11

Feb 18, 1957

AT

14

$\checkmark$
 $\begin{matrix} 63.3 & 65.2 & 65.5 & 65.8 & 65.9 \\ 7.8 & 5.9 & 5.6 & 5.3 & 5.0 \\ 25 & 30 & 38 & 46 & 50 \end{matrix}$

$\begin{matrix} 62.7 & 62.3 & 62.7 & 64.0 & 64.5 & 64.8 & 64.6 & 64.3 & 63.9 \\ 8.4 & 8.8 & 8.4 & 7.1 & 6.6 & 6.3 & 6.5 & 6.8 & 7.2 \\ 22 & 15 & 9 & 3 & 7 & 15 & 20 & 23 \end{matrix}$

$\begin{matrix} 62.7 & 62.7 & 62.6 & 66.0 & 66.0 & 65.5 & 65.0 \\ 8.4 & 8.4 & 8.5 & 5.1 & 5.1 & 5.6 & 6.1 \\ 31 & 39 & 50 & 50 & 42 & 36 & 27 \end{matrix}$

$\begin{matrix} 62.8 & 62.8 & 62.8 & 63.0 & 64.4 & 64.9 & 65.0 & 64.9 & 64.5 & 64.1 \\ 8.3 & 8.3 & 8.3 & 8.1 & 6.7 & 6.2 & 6.1 & 6.2 & 6.6 & 7.0 \\ 31 & 22 & 14 & 9 & 5 & 7 & 14 & 18 & 21 \end{matrix}$

$\begin{matrix} 62.7 & 62.6 & 64.3 & 63.9 & 63.3 & 63.3 & 63.4 & 63.5 \\ 8.4 & 8.5 & 6.8 & 7.2 & 7.6 & 7.8 & 7.7 & 7.6 \\ 41 & 50 & 50 & 48 & 40 & 33 & 28 & 24 \end{matrix}$

$\begin{matrix} 63.1 & 63.4 & 64.2 & 64.8 & 65.4 & 65.5 & 65.2 & 65.0 & 64.2 \\ 8.0 & 7.7 & 6.9 & 6.3 & 5.7 & 5.6 & 5.9 & 6.1 & 6.9 \\ 18 & 13 & 10 & 5 & 7 & 16 & 22 & 24 \end{matrix}$

$\begin{matrix} 62.7 & 62.7 & 62.7 & 62.7 & 67.1 & 65.4 & 64.8 & 64.0 & 63.9 \\ 8.4 & 8.4 & 8.4 & 8.4 & 7.0 & 5.7 & 6.3 & 7.1 & 7.2 \\ 23 & 33 & 43 & 50 & 50 & 47 & 41 & 39 & 30 \end{matrix}$

Sta + π - Elev

971.05

3+21

✓

+59

✓

+83

2 Feb. 18, 1957

15

LT

RT

$\begin{matrix} i3.3 & i4.0 & i4.9 & i5.5 & i6.0 & i6.2 & i6.1 & i6.0 & i7.0 \\ 7.8 & 7.1 & 6.2 & 5.6 & 5.1 & 4.9 & 5.0 & 5.1 & 4.1 \\ 20 & 15 & 9 & 7 & & 7 & 14 & 17 & 21 \end{matrix}$

$\begin{matrix} i2.9 & i2.7 & i2.6 & i2.6 & i9.3 & i7.4 & i6.4 \\ 8.2 & 8.4 & 8.5 & 0.5 & 1.8 & 3.7 & 4.7 \\ 28 & 35 & 50 & 50 & 39 & 31 & 25 \end{matrix}$

$\begin{matrix} i5.1 & i6.0 & i6.7 & i7.4 & i8.0 & i8.2 & i8.2 & i8.1 & i9.3 \\ 6.0 & 5.1 & 4.4 & 3.7 & 3.1 & 2.9 & 2.9 & 3.0 & 1.8 \\ 19 & 14 & 10 & 6 & & 6 & 14 & 17 & 20 \end{matrix}$

$\begin{matrix} i4.5 & i4.0 & i3.5 \\ 6.6 & 7.1 & 7.6 \\ 28 & 39 & 50 \end{matrix}$

$\begin{matrix} i6.6 & i7.8 & i8.7 & i9.2 & i9.5 & i9.8 & i9.8 & i9.7 \\ 4.5 & 3.3 & 2.9 & 1.9 & 1.6 & 1.3 & 1.3 & 1.4 \\ 33 & 24 & 18 & 10 & & 7 & 13 & 16 \end{matrix}$

$\begin{matrix} i5.6 & i4.7 & i4.2 \\ 5.5 & 6.4 & 6.9 \\ 40 & 18 & 50 \end{matrix}$

Sta + π - Elev

977.05

4

✓

TP 9.15 978.32 1.88 969.17

+ 31

✓

+ 50

Feb. 18, 1957

16

LT

RT

✓

69.8	70.8	70.7	70.4	70.8	71.1	71.0
1.3	0.3	0.4	0.7	0.3	0.0	0.1
20	14	7	4		11	15

68.8	67.6	66.7	65.5
------	------	------	------

2.3	3.5	4.4	5.6
27	33	40	50

Nail in PPRT Sta 3+22±

69.6	70.4	72.0	72.4	72.3	72.8	72.7	74.2	75.3
8.7	7.9	6.3	5.9	5.8	5.5	5.6	4.1	3.0
28	22	17	6		7	14	18	23

67.7	66.5	66.0
10.6	11.8	12.3
34	41	50

77.3
1.0
27

✓

71.4	72.6	73.4	73.3	73.2	73.5	73.7	73.4	75.1	76.4	78.3
6.9	5.7	4.9	5.0	5.1	4.8	4.6	4.9	3.2	1.9	0.0
22	18	14	8	4		7	14	17	20	25

70.0	68.7	67.2	66.4
8.3	9.6	11.1	11.9
28	32	40	50

Sta	+	π	-	Elev
-----	---	-------	---	------

		978.32		
--	--	--------	--	--

4+69				
------	--	--	--	--

✓				
---	--	--	--	--

5				
---	--	--	--	--

✓				
---	--	--	--	--

TP	5.60	980.60	332	975.00
----	------	--------	-----	--------

+24				
-----	--	--	--	--

Feb 18, 1957

17

17

17

71.9	73.0	74.0	74.0	74.3	74.3	74.1	75.6	77.7
6.4	5.3	4.3	4.3	4.0	4.0	4.2	2.7	0.6
21	18	11	5		7	14	18	21

70.6	69.2	67.8	66.6
7.7	9.1	10.5	11.7
27	33	40	50

72.3	73.5	74.3	75.0	75.1	75.1	74.9	76.3	77.9
6.0	4.8	4.0	3.3	3.2	3.2	3.4	2.0	0.4
25	19	13	5		10	13	17	19

71.0	69.9	68.7	68.4
7.3	8.4	9.6	9.9
32	38	47	50

72.1	74.6	75.0	75.2	75.6	75.4	75.2	76.2	78.5
8.5	6.0	5.6	5.4	5.0	5.2	5.4	4.4	2.1
32	21	16	7		9	14	15	20

71.2	70.1	71.0	71.1	71.1	71.1
9.4	10.5	3.6	2.5	2.5	2.1
41	50	50	42	35	31

Sta	+	π	-	Elev
-----	---	-------	---	------

		980.60		
--	--	--------	--	--

5+50				
------	--	--	--	--

✓				
---	--	--	--	--

+80				
-----	--	--	--	--

✓				
---	--	--	--	--

6				
---	--	--	--	--

Feb 18, 1957

RT 18

11

74.4	75.9	75.9	75.5	75.9	75.8	75.8	76.6	78.0
6.2	4.7	4.7	5.1	4.7	4.8	4.8	3.0	2.6
32	24	16	9		9	13	16	27

73.2
7.4
40

71.9
8.7
50

71.2
3.4
50

71.4
3.2
41

75.8	76.9	76.0	75.7	76.0	76.1	76.6	76.9	77.3
4.8	3.7	4.6	4.9	4.6	4.5	4.0	3.7	3.3
32	21	16	8		9	14	22	31

74.8
5.8
40

73.4
7.2
56

77.4
3.2
44
House

74.8	75.5	75.9	75.5	75.9	75.9	75.9	77.3	77.3
5.8	5.1	4.7	5.1	4.7	4.7	4.7	3.3	3.3
33	25	17	9		8	13	17	24

73.8
6.8
~~22~~
42

72.9
7.7
50

76.7
3.9
50

77.1
3.5
43

77.5
3.1
34

Sta + π - Elev

980.60

6+22

✓

Feb 18, 1957

19

Lt

RT

71.9	72.7	75.0	75.3	75.8	75.3	75.4	74.6	74.0
8.7	7.9	5.6	5.3	4.8	5.3	5.2	6.0	6.6
33	17	14	9		12	14	17	21

71.7	71.1
8.9	9.5
42	50

V

71.9	72.5	72.8
8.7	8.1	7.8
50	38	28

Sta + π - Elev

980.60

6 + 40

✓

+ 56

✓

+ 77

✓

Feb 18, 1951

20

14

84

70.4	71.4	75.0	75.3	75.7	75.2	75.0	73.7	71.9
10.2	9.2	5.6	5.3	4.9	5.4	5.6	6.9	8.7
33	19	12	6		7	14	17	26

70.4	70.4
10.2	10.2
40	50

70.3	71.0
10.3	9.6
50	38

70.6	70.9	74.8	75.3	75.7	75.3	75.4	74.0	72.9
10.0	9.7	5.8	5.3	4.9	5.3	5.2	6.6	7.7
33	19	12	8		11	13	17	24

70.5	70.5
10.1	10.1
41	50

71.7	72.3	72.3
8.9	8.3	8.3
50	40	31

71.3	71.9	75.1	75.6	75.9	75.7	76.3	76.6	76.6
9.3	8.7	5.5	5.0	4.7	4.9	4.3	4.0	4.0
33	22	13	7		10	13	18	26

71.6	71.7
9.0	8.9
43	50

77.0	76.9
3.6	3.7
50	33

Sta + π - Elev

980.60

7

✓

TP 11.68 987.20 5.09 975.51 (975.52)

+ 11

✓

+ 42

✓

Feb 18, 1957

21

21

RT

73.9	74.1	75.7	76.0	76.4	76.4	78.5	79.8	80.5
6.7	6.5	4.9	4.6	4.2	4.2	2.1	0.8	0.1
29	20	14	8		11	15	24	33

74.5	75.2	76.1		80.6	80.9
6.1	5.4	4.5		0.0	10.3
33	43	50		50	42

74.8	74.7	76.0	76.2	76.7	76.8	79.5	80.3	81.1
12.4	12.5	11.2	11.0	10.5	10.4	7.7	6.9	6.1
23	20	14	10		11	17	25	27

77.2	78.3	79.5		81.1
10.0	8.9	7.7		6.1
34	42	50		50

76.8	76.5	77.0	77.4	77.7	77.8	80.6	81.3	82.1
10.4	10.7	10.2	9.8	9.5	9.4	6.6	5.9	5.1
24	19	14	8		10	18	26	34

78.6	80.2	81.0		81.7	81.8
8.6	7.0	6.2		5.5	5.4
35	45	50		50	41

Sta + π - Elev.

987.20

7+68

✓

BM 6.31 992.69 0.81 986.39 986.38

8+00

✓

7+83 Profile Ent Lt

FX
RB
MH
AB

Feb 18, 1957
Feb 20, 1957
Snow Cloudy Rt

22

14
78.0 77.4 78.4 78.4 78.8 78.8 80.3 81.7 82.3
9.2 9.8 8.8 8.8 8.4 8.4 6.7 5.5 4.9
26 21 13 9 10 17 25 34

79.2 80.1 80.8 82.0 82.3
8.0 7.1 6.4 5.2 4.9
35 45 50 50 43

Top E. End Front Door Sill H₀ 23 25 Maryland

79.1 79.7 80.2 80.7 80.6 82.4 84.3 84.2
13.6 13.0 12.5 12.0 12.1 10.3 8.4 8.5
21 13 8 9 15 30 40

78.5 78.5 78.9 83.8
14.2 14.2 13.8 8.9
28 41 50 50

81.8 80.7 79.5 78.9
10.9 12.0 13.2 13.8
65 50 35 20

82.7 83.4
10.0 9.3
80 H0

Sta + π - Elev

992.69

8433

✓

+ 50

✓

+ 72

Feb 20, 1957 23

1+

RT

80.1	81.0	81.9	82.4	82.8	82.8	82.6	86.2	86.6
12.6	11.7	10.8	10.3	9.9	9.9	10.1	6.5	6.1
35	23	17	11		7	10	16	28

→ 13.795
50

8.1 84.6
50 40

81.5	81.9	83.1	83.5	83.7	83.4	83.4	87.1	87.3
11.2	10.8	9.6	9.2	9.0	9.3	9.3	5.6	5.4
42	29	17	11		8	10	16	24

→ 12.5
50

85.0 85.8 86.7
7.7 6.9 6.0
50 45 34

83.3	83.5	84.1	84.5	84.7	84.4	84.3	88.8	88.3
9.4	9.2	8.6	8.2	8.0	8.3	8.4	2.9	4.4
37	27	18	13		6	9	15	25

82.7 82.5
10.0 10.2
48 50

84.6 85.9 87.1
8.1 6.8 5.6
50 43 35

Sta + π - Elev.

992.69

9+00

✓

+28

✓

+48

✓

2 Feb 20, 1957 24

Lt

Rt

84.2	84.3	84.4	84.8	85.1	85.0	85.0	90.4	90.5
8.5	8.4	8.3	7.9	7.6	7.7	7.7	2.3	2.2
33	23	18	13		5	8	15	23

84.0	84.1					84.8	86.6	88.9
8.7	8.6					2.9	6.1	3.8
44	50					50	43	33

84.0	83.9	83.7	83.9	84.3	84.3	90.6	90.5	88.8
8.7	8.8	9.0	8.8	8.4	8.4	2.1	2.2	3.9
39	28	21	13		5	16	23	32

84.0						85.7	86.8
8.7						7.0	5.9
50						50	42

83.5	82.8	82.3	82.6	83.1	83.0	89.6	89.9	88.3
9.2	9.9	10.2	10.1	9.6	9.7	9.1	2.8	4.4
35	23	17	13		4	13	23	35

83.2	83.1							85.3
9.5	9.6							7.4
45	50							50

Sta + π - Elev.

992.69

9+70

✓

- $\pm$ Ent

TP 0.25 987.12 5.82 986.87

+ 88

✓

10

FK 14
RG RC
KP + Lt

Feb 20, 1957
Feb 25, 1957
RH

25

81.7	81.5	81.1	81.2	81.1	81.1	81.7	82.0
11.0	11.2	11.6	11.5	11.6	11.6	11.0	10.7
34	27	19	12		4	11	15

81.6	81.0		82.6	84.2	85.6	86.8
11.1	11.7		10.1	8.5	7.1	5.9
43	50		50	42	32	21

92.1	91.1	88.7	83.5
06	1.6	4.0	9.2
Front 174	150	100	

Ho spike in PP 23' Rt sta 9+75

80.4	80.3	80.3	80.1	80.0	79.6	79.6	79.7	80.9	83.9
6.7	6.8	6.8	7.0	7.1	7.5	7.5	7.4	6.2	3.2
50	43	23	15	7	3	5	7	14	

In Ent

81.0		79.8	80.4	81.7	82.0
7.5		7.3	6.7	5.4	5.1
In Ent		50	48	35	23

80.4	79.9	79.3	79.2	78.8	78.6	78.8	78.4	77.8
6.7	7.2	7.8	7.9	8.2	8.5	8.3	8.7	9.3
29	19	17	7	3	5	9	12	

Sta + π - Elev

987.12

10

+30

+48

✓

TP 3.86 979.97 11.01 976.11

+52

Feb 25, 1957

26

14

RT

79.7
7.4
50
in Ent

80.1
70
40

76.5
10.6
23

76.1
11.0
36

76.1
11.0
44
40

75.9
9.2
25

77.3
9.8
24

77.0
10.1
18

77.2
9.9
8

76.9
10.2
~~10.18~~

76.7
10.4
2

76.4
10.7
5

76.7
10.4
8

78.5
8.6
37

79.9
7.2
50

75.5
11.6
50
Ho

75.5
11.6
41

75.4
11.7
31

75.6
11.5
18

77.6
9.5
22

76.5
10.6
19

76.1
11.0
16

76.3
10.8
8

75.9
11.2
~~11.16~~

75.5
11.6
3

75.3
11.8
10

74.4
12.7
21

73.5
13.6
32

78.1
9.0
36

79.4
7.7
50

79.3
7.8
Garage

72.6
14.5
50

72.9
14.2
41

77.0
3.0
21

76.1
3.9
18

75.9
4.1
15

76.0
4.0
7

75.8
4.2
~~4.18~~

75.4
4.6
4

74.4
5.6
8

74.5
5.5
11

73.1
6.9
19

77.6
2.4
31

78.6
1.4
43

79.4
0.6
50

68.5
11.5
50

69.9
10.1
43

71.7
8.3
31

Sta + π - Elev.

979.97

10+79

✓

11

✓

TP 2.20 973.81 8.36 971.61

✓ BM

3.22 970.59 (970.58)

+25

Feb 25, 1951

27

14

AT

77.0	75.7	74.7	74.7	74.5	74.2	72.3	70.9	70.0
30	4.3	5.3	5.3	5.5	5.8	7.7	9.1	10.0
22	20	16	7	4	9	21	31	

77.6	78.7	79.5	64.6	65.9	68.3
2.4	1.3	0.5	1.54	1.1	1.17
32	40	50	50	42	35

76.9	73.4	73.2	73.6	73.5	73.2	72.3	71.3	70.0
3.1	4.6	6.8	6.1	6.5	6.8	7.7	8.7	10.0
25	18	15	8	6	9	16	29	

76.6	77.1	77.2	77.2	63.9	64.6	65.8	68.9
3.4	2.9	2.8	2.8	1.61	1.54	1.42	1.11
29	34	46	50	50	45	40	34

73.3	71.7	71.5	71.7	71.6	71.5	71.6	72.0	70.6
0.5	2.1	2.3	2.1	2.2	2.3	2.2	1.8	3.2
22	19	15	6	3	5	6	18	

73.7	73.5	73.6	73.3	62.5	65.9	69.0
0.1	0.3	0.2	0.5	1.3	7.9	4.8
25	33	45	50	50	38	28

Sta + π - Elev

973.81

11450

✓

+ 71

✓

12

12

✓

TP 5.91 966.89 12.83 960.98

Feb

28

70.7	69.3	69.3	69.5	69.2	69.1	69.1	69.6	69.5
3.1	4.5	4.5	4.3	4.6	4.7	4.7	4.2	4.3
26	19	16	7	1	3	5	9	

70.0	69.8	69.3	62.5	67.7	68.4
3.8	4.0	4.5	11.3	6.1	5.4
39	47	50	25.5	25	18

Shed Floor Shed

68.8	67.4	67.5	67.5	67.4	67.3	67.3	65.7	64.9
5.0	6.4	6.3	6.3	6.4	6.5	6.5	8.1	8.9
23	20	16	9	3	6	13	21	

69.3	68.7	68.5	68.4	60.4	61.8	62.4	63.4
4.5	5.1	5.3	5.4	13.4	12.0	11.4	10.4
27	37	47	50	50	47	37	27

67.8	65.0	65.0	65.3	64.9	64.9	64.2	63.2	60.7
6.0	8.8	8.8	8.5	8.9	8.9	9.6	10.6	13.1
26	21	17	10	4	10	21	31	

67.7	68.3	68.1	56.3	57.7
6.1	5.5	5.7	17.5	16.1
31	47	50	50	41

Sta + π - Elev

966.89

12 + 31

✓

+37

✓

+70

Feb 25, 1957

B1 29

14

62.7	62.6	62.7	62.3	62.5	61.2	60.2	60.0
4.2	4.3	4.15 4.2	4.6	4.4	5.7	6.7	6.9
22	19	10		4	8	17	20

65.3	65.6	66.2	66.5	56.0	58.1	59.6
16	1.3	0.7	0.4	10.9	8.8	7.3
26	34	44	50	50	35	24

64.2	62.3	62.2	62.2	61.7	61.9	60.7	59.8	59.0
2.7	4.6	4.7	4.7	5.18 5.2	5.0	6.2	7.1	7.9
27	23	18	10	3	7	15	25	

64.4	64.8	64.9	56.1	57.6
2.5	2.1	2.0	10.8	9.3
34	46	50	50	38

63.4	60.6	60.2	60.0	59.1	58.8	57.8	57.3	56.3
3.5	6.3	6.7	6.9	7.8	8.1	9.1	9.6	10.6
28	22	18	10		5	12	21	31

64.1	64.7	55.3	55.9
2.8	2.2	11.6	11.0
38	50	50	44

Sta + π - Elev

966.89

13+00

✓

+22.68 $\pm$ Lohers Rd

✓

BM

9.79 957.10 (957.11)

Feb 25, 1957

30

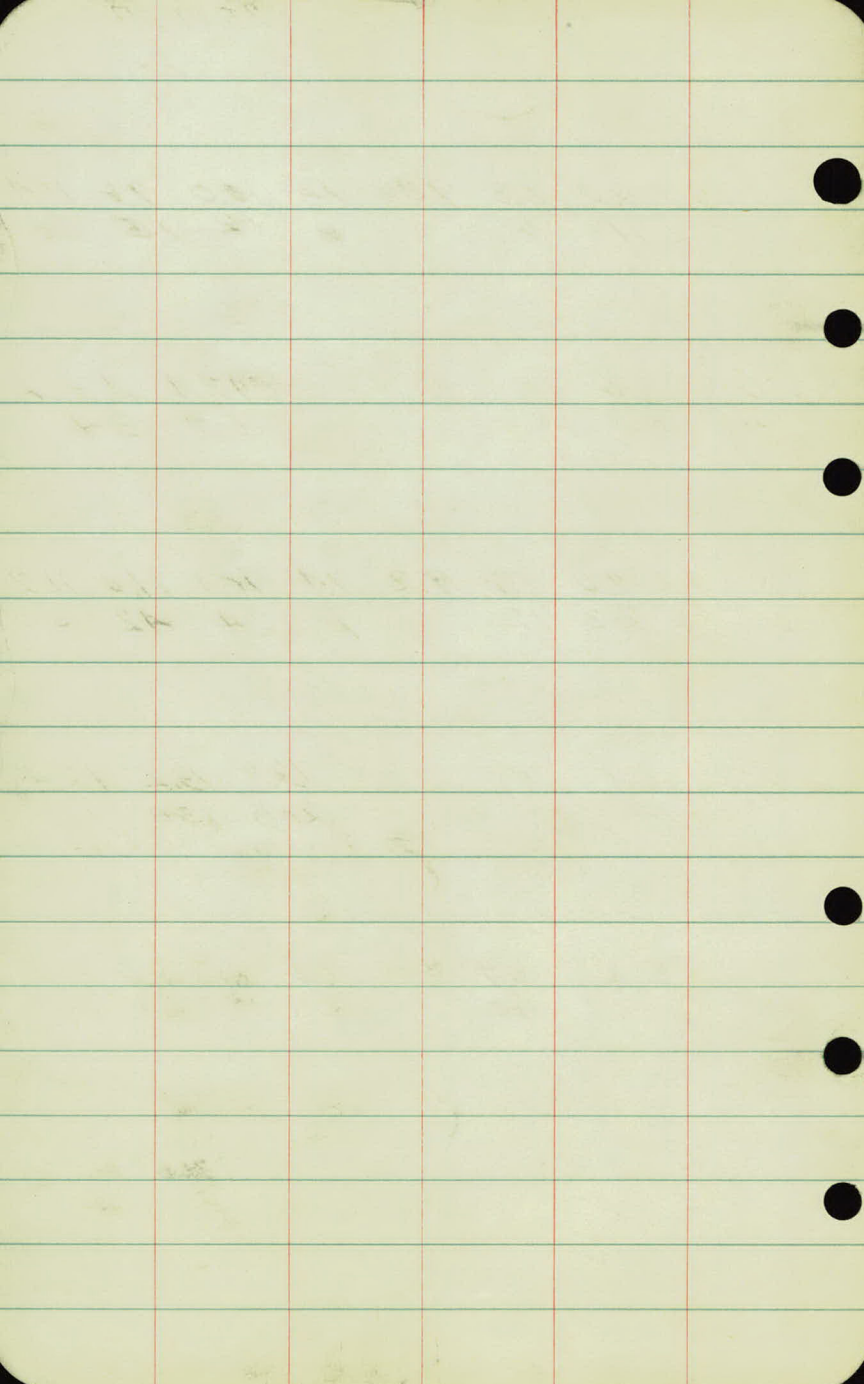
60.0	59.0	58.9	58.6	57.9	57.5	56.9	57.3	56.5
6.9	7.9	8.0	8.3	9.0	9.4	10.0	9.6	10.4
28	22	11	6		6	12	15	20

60.6	61.3					54.8	55.6	
6.3	5.6					12.1	11.3	
40	50					50	34	

59.1	58.7	58.3	58.3	57.7	57.5	56.8	55.9	55.7
7.8	8.2	8.6	8.6	9.2	9.4	10.1	11.0	11.2
50	36	23	12		7	24	42	50

53.1	53.7	54.5
13.8	13.2	12.4
200	150	100

Spike in G. Pole SE Cor. Maryland Ave & Lake Mead



Align
Maryland Str
From Plum. to Ea. Co Line (STH #100)

216-44

HAW

AM

L-G

Plan sheet drawn up
3/13/44 WJB

579 Pt ΔL ΔR

13+17.40 Mon

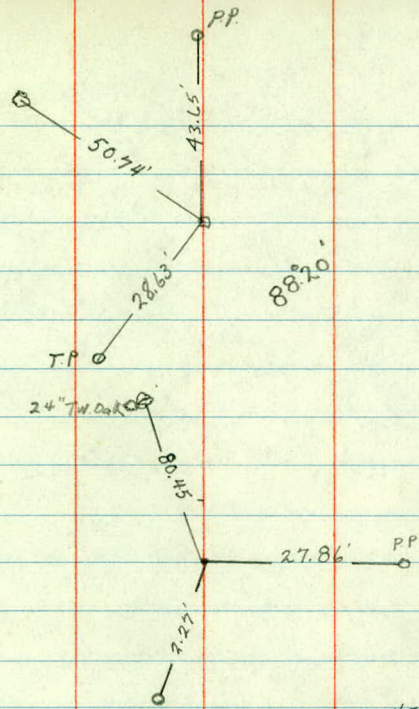
10+72.85 P.O.T

4+98.42 P.O.T

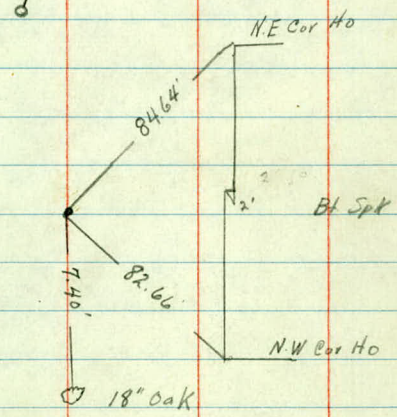
0+00 P.I

N.E. Cor Sec 25

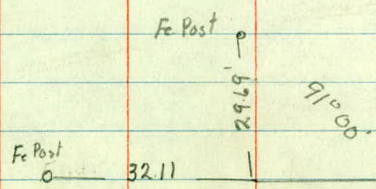
Nail
Mon On
Used Ties in
Sec Book to
E67



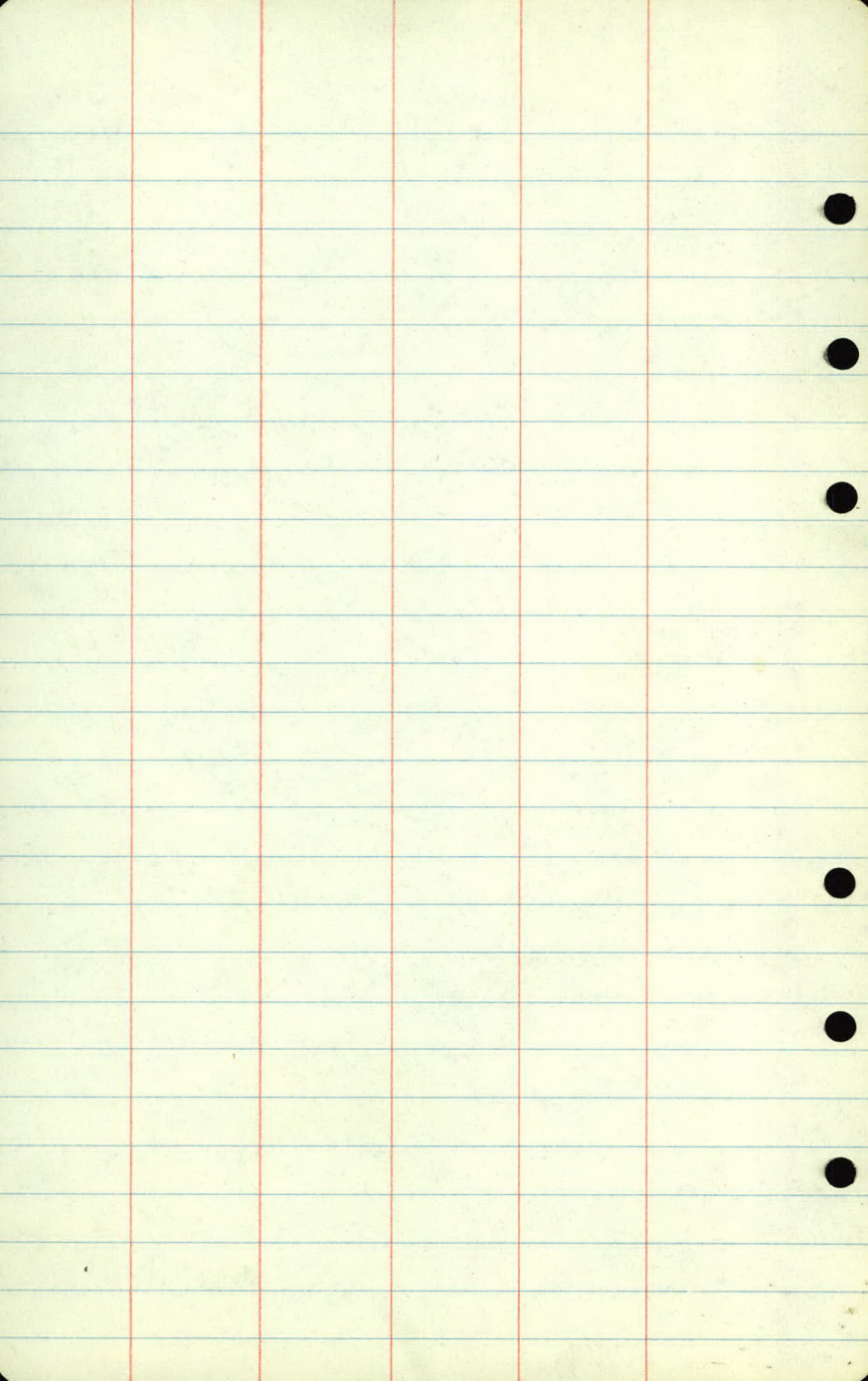
Boat Spk.



Bl Spk



91°00'



Topography
Maryland Str.

2-16-44

HAW
AM
L.G.

6

Rd Rd
6 x 20'

5

6-22'

4

+30 Bog Rd 6' + 19' + Bog Hedge 26'
2 Turnpike 15'

3

17' x Turnpike

2

15' x Turnpike

+47 6" Oak 8'
+45 6" Oak 20'

1

20' x Turnpike

0

Fe 0.0

Fe 0.0

Fe 1'

+83 Fe Cor 0.0'

Fe 0.0

+40 4" Oak 29'
 +34 6" Oak 14'
 +33 12" Oak 16'
 +24 2 10" Oak 25' + 30'
 +20 12" Oak 36'
 +19 4" Oak 26'
 +12 12" Tin Oak 11'
 +10 24" Oak 1'

Fe 0.0

+81 Fe Cor 0.1'

Cultivated

Meadow

Cultivated

+35 PP 24'

+33 End Hedge 26'

+90 30" Oak 2'



+85 End Cult 23'
 +81 NW Cor HD 81'
 +67 Bog 12" X 20" CM 20
 +18 18" Oak 3'
 +00 Stu 4'

+87 Stu 3'

+53 12" Oak 4'
 +52 Stu 4'
 +33 12" Oak 5'
 +33 x Fe 31'
 +21 15" Oak 4'

Platted

13

6'

Rd Rd
+ 98 18" x 40' x Drain

34'

12

6' x 22'

11

6' x 22'

10

6' x 21'

9

6' x 21'

8

6' - 22

7

5' x 19'

6

6' x 20'

+90 T.P. 11'
+85 End Fe 0.0'

+85 Beg Red 5' x 21'

+27 18" Oak 4'

+13 4" Oak 4'

Fe 1'

+52 TW 18" Oak 4'

Fe 2'

+71 G.P. 0.0'

+71 P.P. 28'

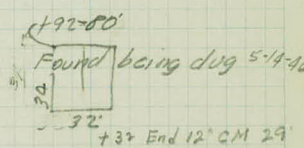
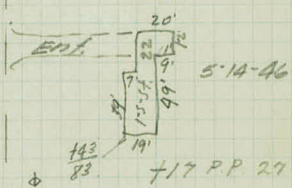
+39 10" Oak 5'

Fe 1'

+34 8" Oak 1'

Fe 0.0

Cultivated



Fe 0.0

+22 Ent +12 Beg 12" x 20" CM 22'
+10 End Hedge 32'



+85 NW Cor H.O. 85'

+36 Cor Hedge 32'

+34 P.P. 27'

+32 End 12' CM 24'

+12 2" A-4 32'

+12 Beg 12" x 20" CM 24'



+92 NW Cor H.O. 81'

+89 Bush 35'

+69 Bush 35'

+58 Bush 35'

+45 Bush 35'

+33 Bush 35'

+00 stu 4'

14

128 Edge Blacktop

13

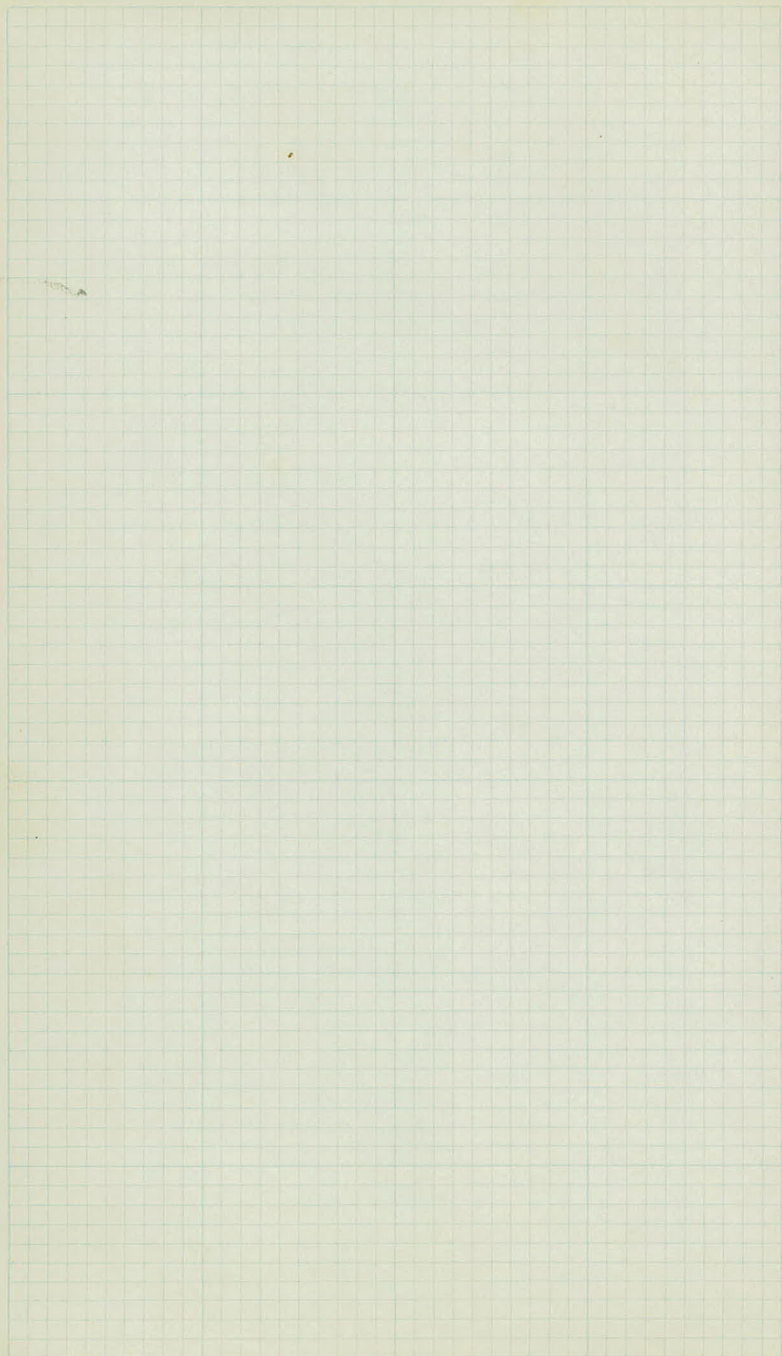
+08 Edge "

S.T.H # 100'

20' Blacktop

+08 End Rad 11'

+08 End Rad 39'



Bench Levels

X Sections from 9150 to E. Co. Line are n.g.
on rt. side. Hill being graded. 5-14-46
K. H.

Sta	+	Σ	-	Elev
B.M	2.30	1023.33		1021.03
	0.96	1012.66	11.63	1011.70
	6.00	1007.77	10.89	1001.77
	0.12	994.46	13.43	994.34
	0.28	986.07	8.67	985.79
T.P	12.87	986.31	12.63	973.44
B.M	7.57	986.31	7.57	978.74
	12.51	998.30	0.52	985.79
	10.63	1008.09	0.84	997.46
	12.34	1019.41	3.02	1006.07
	11.29	1028.05	0.65	1016.72
B.M			12.12	1015.93

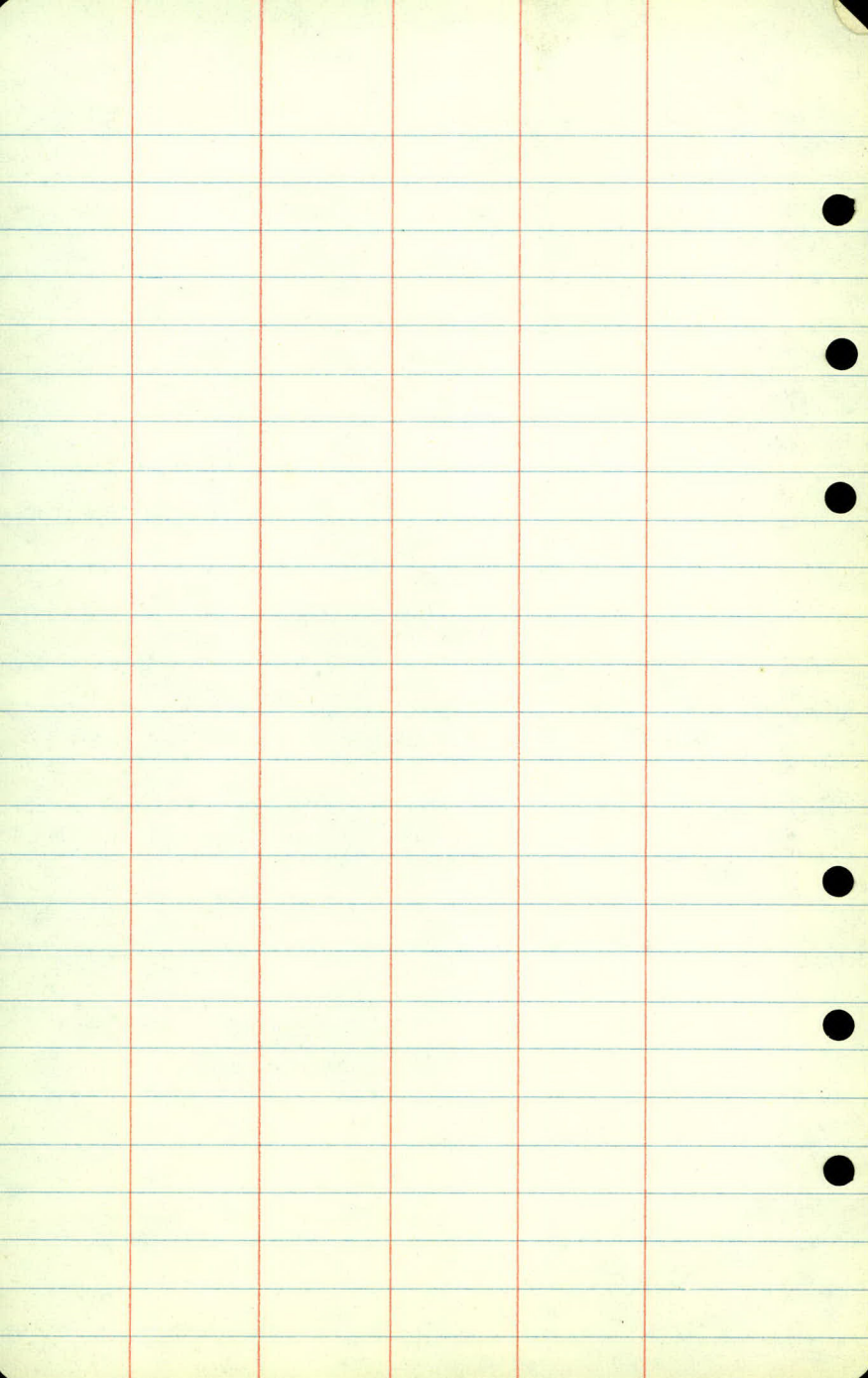
Description

Top & Red Sta 0+00

Top Spk 0+00 Maryland Str.

Spk in 18" Oak 1' L/ Sta 1+10

Spk in P.P. N.E. Cor. STH. #100 & Maryland Str



X Sections
Maryland str.

Sta	+	X	-	Elev
B.M	475	983.49		978.74
0+20				72.3
0+00				73.6
+50				75.7
1+00				77.1
+50				76.7
2+00				76.6
+50				79.1
T.P.	13.31	996.13	0.67	982.82
3				84.7
+50				88.0
T.P.	1339	1008.74	0.78	995.35
4				95.7
+50				02.3
+80				05.2

L+

Z

RT

Spk in Oak 1'41 Sta 1+10

$$\begin{array}{ccccccc} 12.1 & 11.8 & 11.9 & 12.3 & 11.3 & 11.8 & 11.8 & 12.5 \\ \hline 50 & 27 & 7 & 5.3 & 2 & 11.2 & 5 & 25 & 50 \end{array}$$

$$\begin{array}{ccccccc} 10.6 & 10.6 & 10.8 & 10.8 & 10.4 & 10.3 & 11.4 & 11.7 \\ \hline 50 & 25 & 4 & 2 & 9.9 & 10 & 27 & 31 & 50 \end{array}$$

$$\begin{array}{ccccccc} 9.3 & 8.3 & 8.0 & 8.4 & 7.8 & 8.8 \\ \hline 50 & 25 & 21 & 35 & 37 & 50 \end{array}$$

$$\begin{array}{cccc} 8.6 & 7.6 & 6.4 & 6.3 \\ \hline 50 & 25 & 25 & 50 \end{array}$$

$$\begin{array}{cccc} 9.4 & 8.1 & 6.0 & 4.4 \\ \hline 50 & 25 & 14 & 30 & 50 \end{array}$$

$$\begin{array}{cccc} 8.8 & 8.4 & 6.1 & 5.6 \\ \hline 50 & 26 & 12 & 30 & 50 \end{array}$$

$$\begin{array}{cccc} 6.4 & 5.7 & 3.5 & 2.9 \\ \hline 50 & 25 & 10 & 26 & 50 \end{array}$$

$$\begin{array}{ccccccc} 14.7 & 14.0 & 12.7 & 11.7 & 11.3 & 11.8 & 11.3 & 10.6 & 10.6 \\ \hline 50 & 25 & 8 & 4 & 11.4 & 3 & 5 & 16 & 39 & 50 \end{array}$$

$$\begin{array}{ccccccc} 10.0 & 9.6 & 8.5 & 7.6 & 7.6 & 7.0 & 7.0 & 7.7 & 6.9 & 6.2 & 6.1 \\ \hline 50 & 30 & 7 & 3 & 81 & 10 & 12 & 21 & 23 & 26 & 36 & 50 \end{array}$$

$$\begin{array}{ccccccc} 15.9 & 15.2 & 14.0 & 12.4 & 13.4 & 13.0 & 12.2 & 12.1 & 12.5 & 11.8 \\ \hline 50 & 30 & 9 & 3 & 13.0 & 2 & 6 & 8 & 20 & 22 & 24 \end{array}$$

$$\begin{array}{ccccccc} 8.3 & 8.0 & 7.4 & 6.1 & 6.1 & 6.2 & 6.1 & 6.6 & 6.1 & 6.6 \\ \hline 50 & 25 & 10 & 6 & 2 & 6.4 & 8 & 21 & 22 & 23 & 25 & 50 \end{array}$$

$$\begin{array}{ccccccc} 4.6 & 4.8 & 4.0 & 3.2 & 3.5 & 4.1 & 3.6 & 3.6 & 4.3 & 3.6 & 4.2 \\ \hline 50 & 30 & 14 & 10 & 35 & 3 & 5 & 16 & 22 & 23 & 25 & 50 \end{array}$$

 Elevat
Ho. 2.7

Sta + A - Elev

100874.

5 06.6.

T.P. 466 101236 1.04 100770

+50 08.2.

+88 08.6.

6 07.9.

+50 03.8.

7 04.5.

+50 06.4.

8 08.3.

+50 11.2.

T.P. 13.12 1024.96 0.52 1011.84.

9 15.5.

+17 16.9.

+50 18.7.

Lt.

R

Rt

$$\frac{25}{50} \quad \frac{23}{25} \quad \frac{1.4}{7} \quad \frac{1.4}{4} \quad 21 \quad \frac{28}{4} \quad \frac{25}{14} \quad \frac{28}{21} \quad \frac{31}{24} \quad \frac{26}{25} \quad \frac{38}{50}$$

$$\frac{29}{50} \quad \frac{31}{32} \quad \frac{28}{8} \quad \frac{3.4}{4} \quad 42 \quad \frac{45}{2} \quad \frac{48}{3} \quad \frac{45}{13} \quad \frac{5.2}{22} \quad \frac{55}{25} \quad \frac{7.5}{50} \quad \frac{100}{50}$$

$$\frac{3.4}{50} \quad \frac{33}{28} \quad \frac{28}{5} \quad 38 \quad \frac{41}{1} \quad \frac{5.8}{3} \quad \frac{5.6}{6} \quad \frac{5.6}{13} \quad \frac{6.4}{22} \quad \frac{7.3}{24} \quad \frac{6.9}{25} \quad \frac{8.9}{43}$$

$$\frac{4.9}{50} \quad \frac{45}{29} \quad \frac{3.9}{9} \quad \frac{3.4}{4} \quad 45 \quad \frac{55}{2} \quad \frac{66}{4} \quad \frac{6.3}{6} \quad \frac{6.4}{13} \quad \frac{7.0}{21} \quad \frac{8.0}{25} \quad \frac{9.2}{35} \quad \frac{10.6}{50}$$

$$\frac{9.0}{50} \quad \frac{8.2}{25} \quad \frac{7.9}{8} \quad 86 \quad \frac{8.9}{4} \quad \frac{8.6}{6} \quad \frac{8.7}{14} \quad \frac{9.1}{23} \quad \frac{10.5}{50} \quad \text{Floor at Ho}$$

$$\frac{9.4}{50} \quad \frac{8.6}{25} \quad \frac{7.7}{12} \quad 7.9 \quad \frac{8.1}{5} \quad \frac{7.9}{13} \quad \frac{8.2}{22} \quad \frac{9.0}{24} \quad \frac{8.5}{26} \quad \frac{8.9}{27} \quad \frac{6.3}{50}$$

$$\frac{7.1}{50} \quad \frac{6.4}{25} \quad \frac{5.7}{10} \quad 60 \quad \frac{6.7}{4} \quad \frac{6.5}{12} \quad \frac{6.6}{22} \quad \frac{7.5}{25-29} \quad \frac{7.3}{31} \quad \frac{7.5}{50} \quad \text{Floor at Ho}$$

$$\frac{5.8}{50} \quad \frac{4.5}{25} \quad \frac{3.4}{7} \quad 41 \quad \frac{4.1}{6} \quad \frac{4.0}{14} \quad \frac{4.3}{23} \quad \frac{5.1}{25-29} \quad \frac{4.8}{31} \quad \frac{4.5}{50} \quad 2.8$$

$$\frac{3.5}{50} \quad \frac{2.4}{25} \quad \frac{0.9}{7} \quad 1.2 \quad \frac{1.2}{2} \quad \frac{1.5}{4} \quad \frac{1.2}{5} \quad \frac{1.1}{13} \quad \frac{1.5}{23} \quad \frac{2.2}{25-27} \quad \frac{0.9}{28} \quad \frac{1.3}{50}$$

$$\frac{11.6}{50} \quad \frac{10.8}{25} \quad \frac{10.0}{10} \quad \frac{9.1}{2} \quad 95 \quad \frac{10.3}{2.3} \quad \frac{9.9}{6} \quad \frac{9.6}{14} \quad \frac{9.8}{21} \quad \frac{10.3}{24} \quad \frac{9.7}{25} \quad \frac{9.4}{39} \quad \frac{9.1}{50}$$

$$\frac{10.8}{50} \quad \frac{10.2}{29} \quad \frac{9.4}{14} \quad \frac{8.1}{2} \quad 8.1 \quad \frac{8.4}{2} \quad \frac{8.9}{2} \quad \frac{8.6}{6} \quad \frac{8.3}{13} \quad \frac{8.5}{22} \quad \frac{9.0}{25} \quad \frac{8.0}{26} \quad \frac{7.3}{50}$$

$$\frac{9.2}{50} \quad \frac{8.5}{30} \quad \frac{7.1}{11} \quad \frac{6.0}{5} \quad 6.3 \quad \frac{6.6}{3} \quad \frac{6.1}{13} \quad \frac{6.3}{23} \quad \frac{6.7}{25} \quad \frac{5.9}{26} \quad \frac{5.0}{50}$$

Sta	+	π	-	Elev
10400		1024.96		20.2
+35				23.0
T.P.	9.24	1030.22	3.98	1020.98
+73				26.1
11				24.1
+50				20.3
T.P.	2.31	1021.33	11.20	1019.02
12				15.4
+50				14.3
+85				15.0
+92				14.3
+97		18' x 40' CM		14.7
13				14.7
+05				14.8

Lt

R

R1

$$\frac{9.3}{50} \frac{8.1}{27} \frac{6.6}{15} \frac{5.2}{4} 48 \frac{3.7}{7} \frac{3.4}{13} \frac{3.5}{22} \frac{3.8}{24} \frac{2.2}{27} \frac{1.2}{50}$$

$$\frac{5.6}{50} \frac{4.8}{25} \frac{3.2}{9} \frac{1.6}{5} 20 \frac{1.7}{3} \frac{1.1}{6} \frac{0.6}{13} \frac{0.7}{23} \frac{10.7}{25} \frac{11.8}{50}$$

Top Stake Sta 10400

$$\frac{8.3}{50} \frac{7.7}{33} \frac{5.7}{10} \frac{4.3}{5} 41 \frac{4.5}{6} \frac{4.2}{13} \frac{4.4}{23} \frac{3.5}{25} \frac{2.8}{37} \frac{2.4}{50}$$

$$\frac{10.1}{50} \frac{8.4}{31} \frac{6.7}{9} 61 \frac{6.0}{3} \frac{5.5}{6} \frac{5.3}{13} \frac{5.6}{23} \frac{5.1}{25} \frac{4.7}{28} \frac{3.9}{50}$$

$$\frac{14.4}{50} \frac{13.2}{32} \frac{11.3}{15} \frac{9.9}{6} 99 \frac{10.0}{3} \frac{9.7}{6} \frac{9.3}{12} \frac{9.6}{20} \frac{10.2}{23} \frac{9.0}{23} \frac{8.6}{28} \frac{8.4}{50}$$

$$\frac{8.0}{50} \frac{7.3}{33} \frac{6.3}{13} \frac{5.7}{9} 59 \frac{6.0}{4} \frac{5.5}{6} \frac{5.6}{20} \frac{5.4}{29} \frac{6.0}{50}$$

$$\frac{8.1}{50} \frac{7.7}{33} \frac{6.6}{12} 70 \frac{7.1}{6} \frac{7.1}{14} \frac{7.4}{25} \frac{8.2}{50}$$

$$\frac{7.4}{50} \frac{7.1}{25} 63 \frac{7.0}{3} \frac{6.7}{6} \frac{7.0}{24} \frac{7.5}{31} \frac{8.4}{50}$$

$$\frac{7.4}{50} \frac{7.0}{25} 70 \frac{6.6}{14} \frac{7.1}{31} \frac{10.5}{31} \frac{10.3}{34} \frac{10.5}{50}$$

$$\frac{1010.53}{6} \text{Inv}$$

$$\frac{10.5}{50} \frac{10.0}{23} \frac{9.7}{5} \frac{9.2}{5} 66 \frac{6.6}{18} \frac{7.0}{33} \frac{9.7}{35} \frac{10.0}{50} \frac{10.5}{31} \text{Inv}$$

$$1010.83$$

$$\frac{10.5}{50} \frac{10.0}{23} \frac{9.7}{5} \frac{9.2}{5} 66 \frac{6.6}{18} \frac{7.0}{33} \frac{9.7}{35} \frac{10.0}{50}$$

$$\frac{6.8}{50} \frac{6.7}{25} 65 \frac{6.6}{25} \frac{6.8}{50}$$

Inv

Inv

Sta + Δ - Elev

1021.33

13+17.40

Δ 5TH #100 15.13

BM

5.38 1015.95 1015.93

Lt

£

Rt

$$\frac{6.3}{50}$$

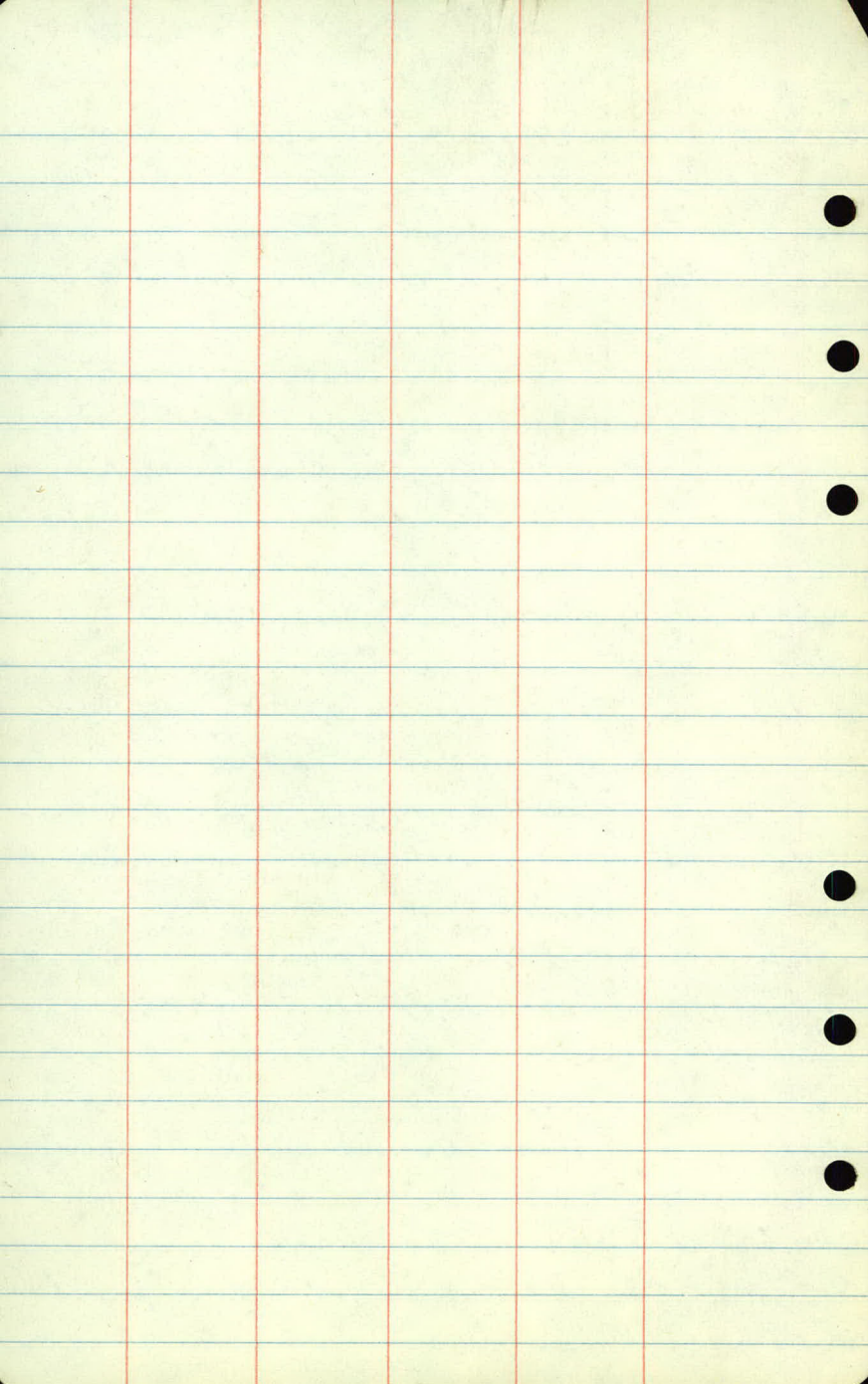
$$\frac{6.2}{25}$$

$$6.2$$

$$\frac{6.2}{25}$$

$$\frac{6.2}{50}$$

Sph in R.P. N.E Cor #100 + Maryland St



Maryland St.

Profile Levels

Sta. 4 to E. Co. Line

Profile is approx. 15' south of section
line and in approx. $\frac{1}{2}$ of travelled
roadway.

Sta.	+	π	-	Elev.
B.M.	8.34	987.08		(97874)
T.P.	12.66	999.27	047	986.61
T.P.	12.43	1011.47	023	999.04
4				97.6
+50				38.1
+80				83.3
5				1006.6
+50				
+75				
6				07.8
+35				
+70				
7				04.4
+50				

S-14-40
K.A.
A.M.
M.B.
C.F.

Lt

2

15' Bt

Spk in 18" Oct. 1' Lt sta. 1410

14.9 996.6

8.6 1002.9

6.5 05.0

49 5.4 06.1

3.8 07.7

4.2 07.3

37 5.6 05.9

7.3 04.2

7.5 04.0

71 7.1 04.4

71 7.1

5.5 06.0

Sta	+	π	-	Elev.
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		1011.47		
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8				68.2
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	+50			
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T.R	13.51	1024.13	0.85	1010.62
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9				15.4
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	+50			
--	-----	--	--	--

10				
----	--	--	--	--

	+30			
--	-----	--	--	--

	+73			
--	-----	--	--	--

11				
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	+50			
--	-----	--	--	--

12				
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T.R	3.23	1019.92	7.44	1016.69
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	+50			
--	-----	--	--	--

13				
----	--	--	--	--

	+17.4			
--	-------	--	--	--

B.M.			3.95	1015.97
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				1015.93
--	--	--	--	---------

Lt.

E

15' RA

33

3.2

08.3 .

0.3

11.2 .

0.7

9.0

15.1 .

5.3

18.8 .

21.6 .

2.5

20.3

3.8

Gar. f/100

0.9

23.2 .

0.2

23.9 .

0.9

23.2 .

4.3

19.8 .

7.4

16.7 .

4.6

15.3 .

4.9

15.0 .

4.7

15.2 .

Spk. in PP NE Cor Maryland and E. Co Line

Sta	+	π	-	Elev.
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+

↑

—

 $E/\text{eV.}$

Maryland St.

Grade stake at 8-8150-8175
set at 33' Rth.

Sta.	+	π	-	Grade	
B.M.	10.16	1026.09			101593

8	+50			11.3	
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	+75			12.8	
--	-----	--	--	------	--

9				14.3	
---	--	--	--	------	--

5-16-46
K.A.
A.M.
M.B.
C.F.

Gr. Rod

Spk. in RR at Maryland + E. Co Line

14.8

13.3

11.8

