

BK. 33 Dr. 12A.

OFFICE OF COUNTY ENGINEER
RAMSEY CO. MINN.

_____ Plan _____ Survey

Phalen Place & Sophia Str

From Sophia _____ To Edward
East Shore Drive To Good Str.

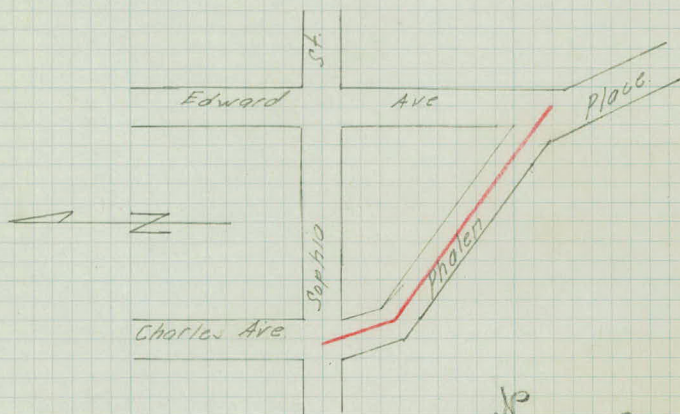
Road Acc't. No. _____

Date Filed _____

File _____

BK 33 Dr. 12A

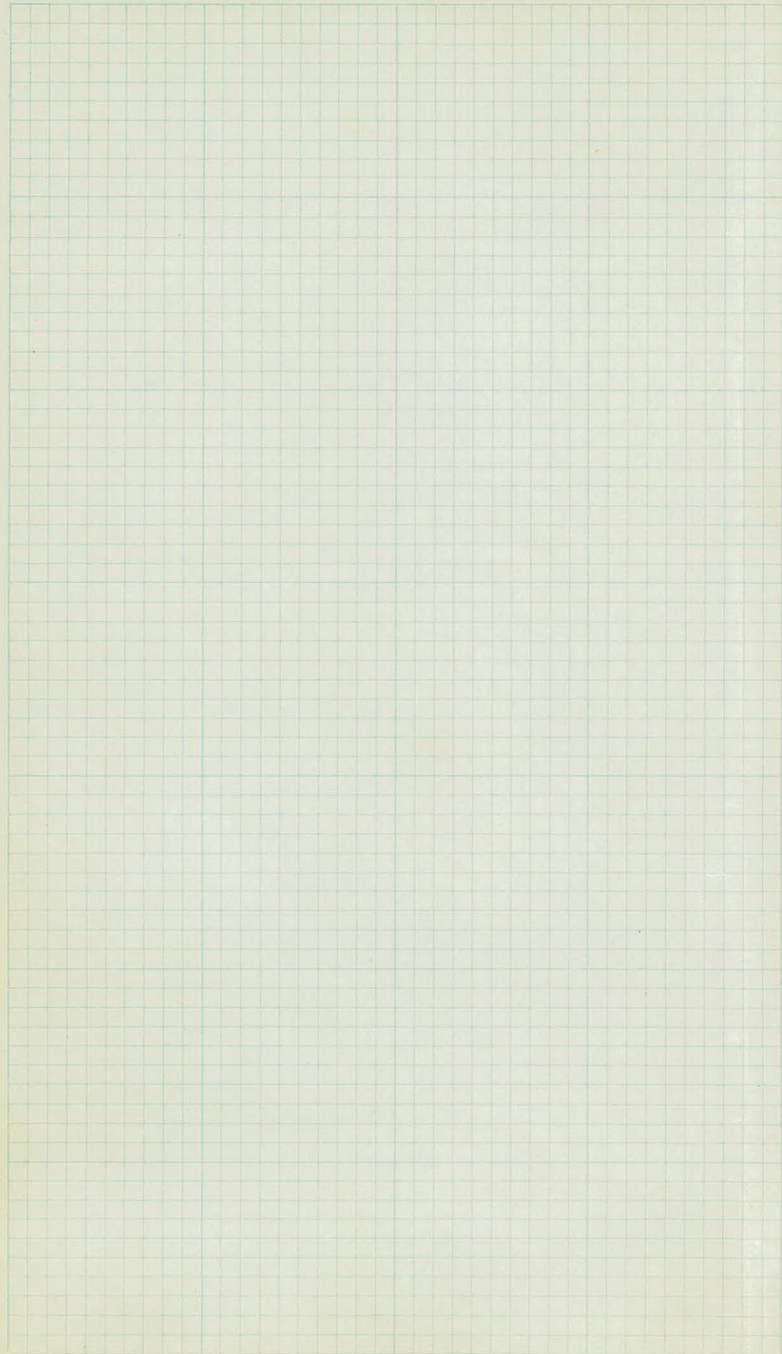
PLAN SURVEY
 PHALEN PLACE
 Sophia St to Edward Ave.



Drawn up
 Aug 26. 1940
 Howard W. B.

INDEX.

- Align - 1-2
- Topog. - 3-4
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- Bank Levels - 8-9



Alignment

40' R.O.W.

Sta.	Point	ΔLf	ΔRt
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4	+77.79 = E Edward Ave.		
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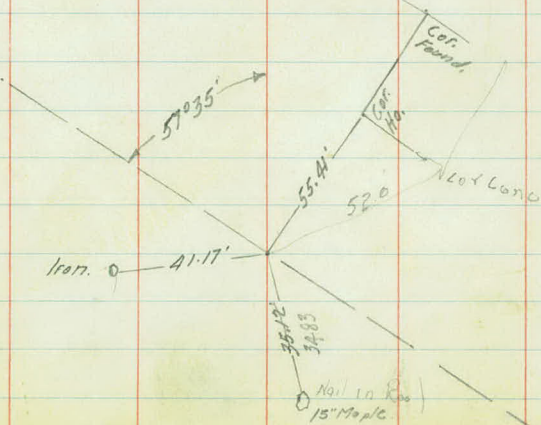
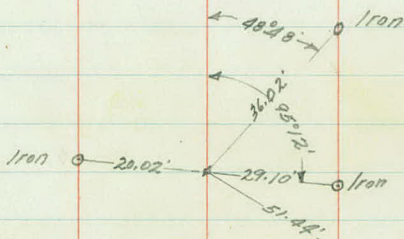
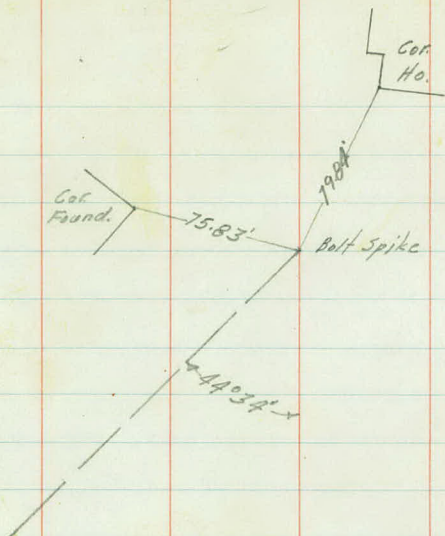
4	+15.20 Lot Iron 20' Lt.		
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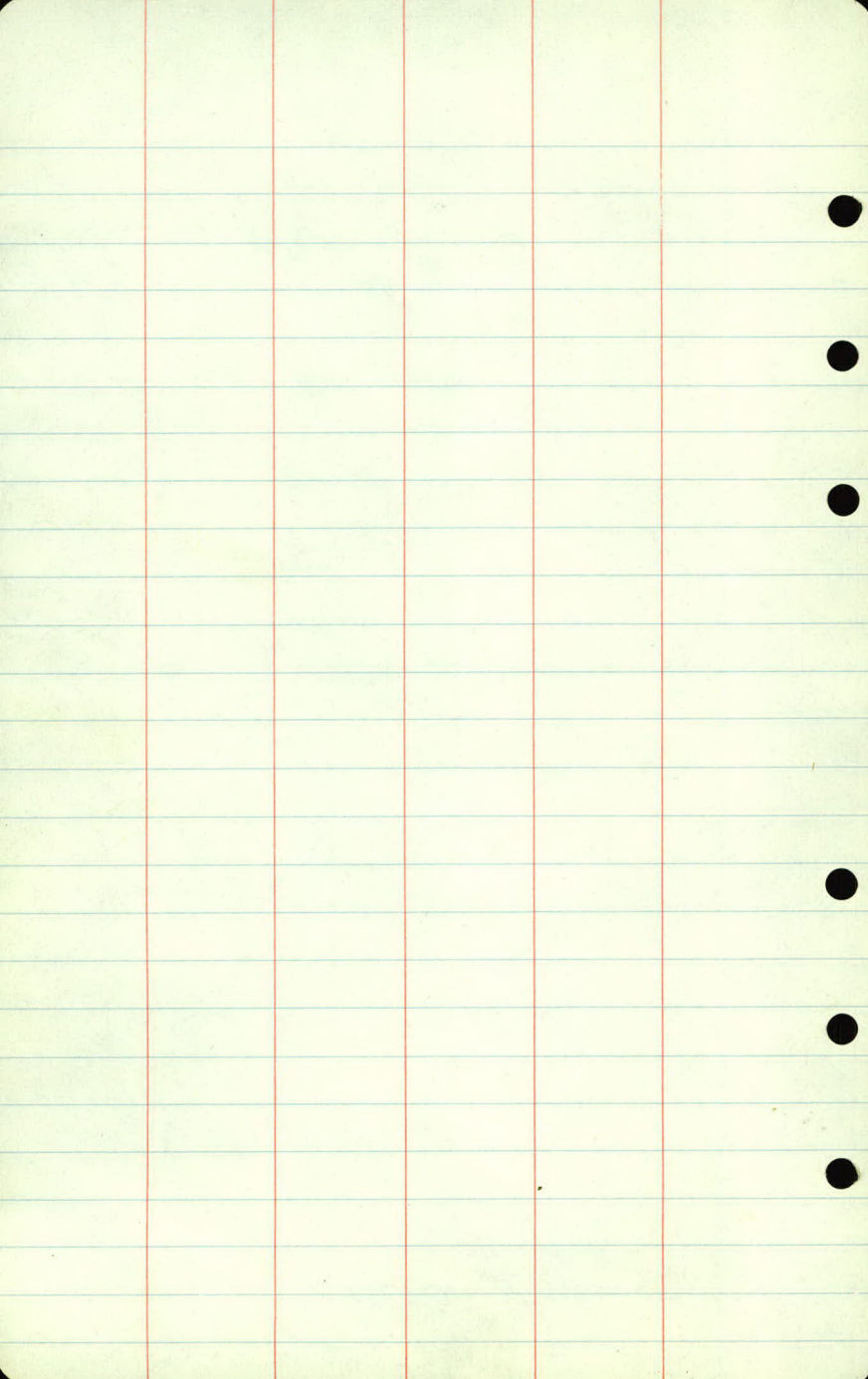
0	+95.38 P.I.	12°07'30"	
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0	+00 = E Sophia St.		
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8-15-40

2





Topography

00 24'

+83-End 15" C.M. - 17' 6" N. 7'
+18-End 12" Ent. C.M. - 23' 15" X 36 C.M.
+60-End 12" Ent. C.M. - 36'
+50-Ed - 38 - 15' +50 - 7'

+81-PP - 19'
12' - 74' +62-End 15" C.M. - 11'
+62-End Gutter 11' - 15'
7' Gutter - 10' - 14'

4 Edward Ave - 87' - 62' 10' 10' Gutter - 12' - 16'

+82-PA - 19' 4' wide
+72-Beg. Rubble Gutter - 14'
+65-11' 12'

+43-Cor. Ho. - 34'

+39-Cor. Garage - 51'
+43-6" B.E. - 30'
+30-Group 6-2" B.E. 8' 3-2" B.E. - 20'
+21-Group 6-2" B.E. - 8'

3 +19-Cor. Ho. - 44'

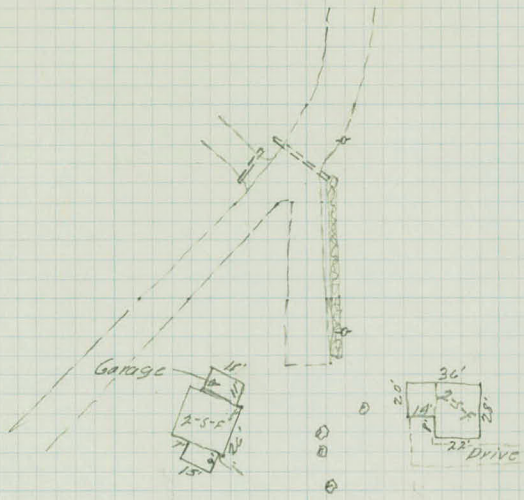
+01-5" B.E. - 12'

2

1

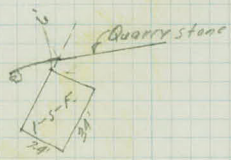
+12-5" Maple - 35' (+6 Cor. Ho. - 47')
+74-Beg. Wall - 26'
+74-Rango Tie to wall
+44-Cor. Ho. - 31'

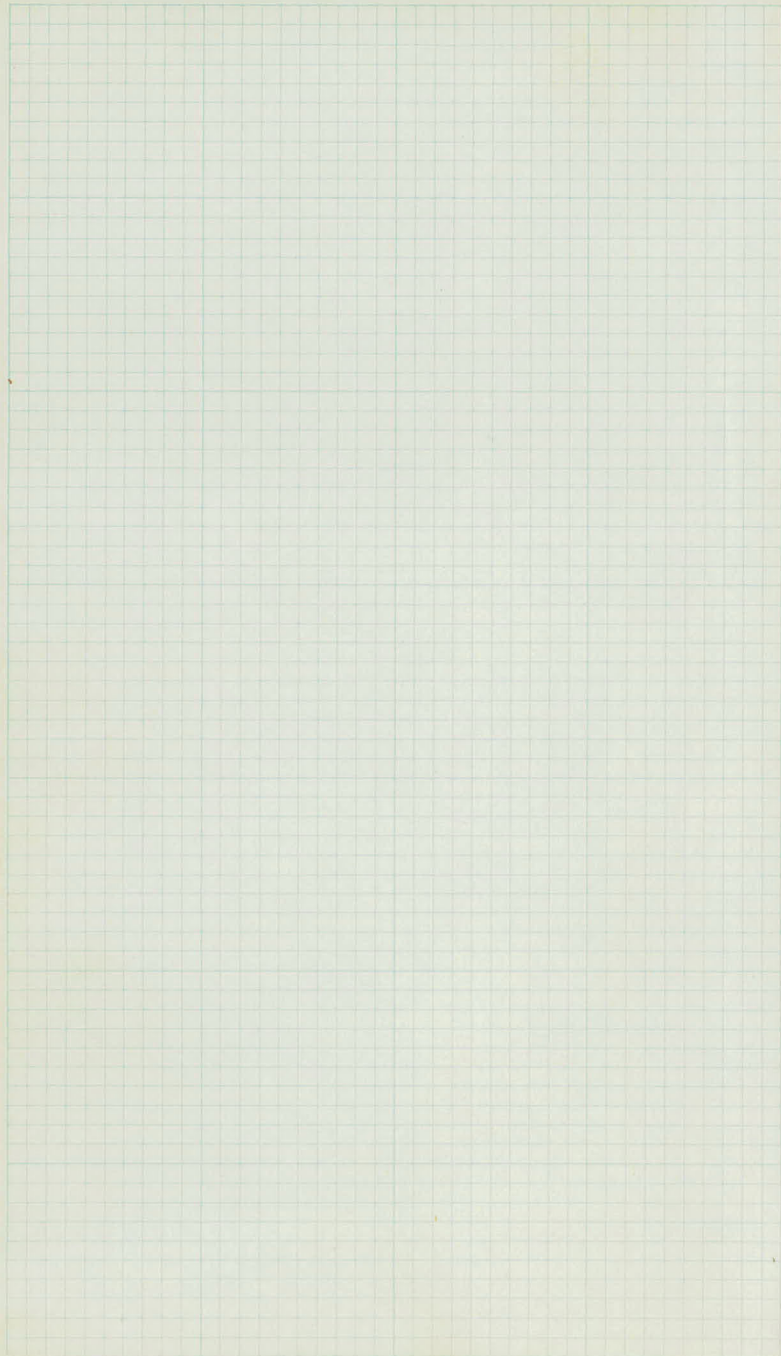
0+00



Uncult.

Uncult.





X Sections

Sta.	+	π	-	Elev.
B.M.	1023	877.75		(867.52)
0	+00			70.5
	+24			69.8
	+48			67.8
	+74			67.8
	+78			67.8
	+95.38	Rt Δ to Boul Tang.		67.2
	+95.38	Rt Δ to Fero Tang.		67.2
1	+15			66.7
	+19			66.7
	+41			65.8
	+67			65.9

K.H.

L.C.

M.B.

L.G.

Lt

C

Rt

Top R.R. Spike Int. East Shore Drive & Sophia St.

$$\frac{73}{8} \frac{78}{16} \frac{89}{28} \frac{93}{43} \frac{92}{50} \frac{83}{50}$$

$$\frac{49}{50} \frac{58}{32} \frac{72}{20} \frac{80}{18} \frac{88}{22} \frac{76}{42} \frac{83}{50} \frac{86}{50}$$

$$\frac{60}{50} \frac{76}{20} \frac{97}{9} \frac{100}{10} \frac{112}{19} \frac{107}{25} \frac{78}{31} \frac{75}{31}$$

$$\frac{61}{50} \frac{86}{22} \frac{100}{17} \frac{111}{26} \frac{104}{27} \frac{91}{48} \frac{79}{50} \frac{117}{50}$$

$$\frac{62}{50} \frac{86}{22} \frac{100}{17} \frac{111}{26} \frac{104}{26} \frac{117}{50}$$

$$\frac{69}{50} \frac{90}{37} \frac{94}{23} \frac{106}{23} \frac{115}{50} \frac{125}{50}$$

$$\frac{68}{50} \frac{90}{36} \frac{96}{21} \frac{106}{16} \frac{115}{29} \frac{117}{40} \frac{70}{50} \frac{85}{50}$$

$$\frac{74}{50} \frac{104}{21} \frac{111}{27} \frac{115}{36} \frac{74}{50} \frac{78}{50}$$

$$\frac{76}{50} \frac{105}{20} \frac{111}{8} \frac{111}{10} \frac{81}{29} \frac{75}{50} \frac{77}{50}$$

$$\frac{74}{50} \frac{84}{37} \frac{108}{21} \frac{120}{8} \frac{120}{11} \frac{84}{32} \frac{78}{50} \frac{78}{50}$$

$$\frac{74}{50} \frac{80}{41} \frac{99}{20} \frac{111}{12} \frac{119}{18} \frac{120}{14} \frac{87}{50} \frac{80}{50}$$

Sta	+	π	-	Elev
		877.75		
1	+72			66.0
2				67.0
	+50			68.7
	+87			73.4
3				74.4
T.P.	12.00	887.38	2.37	875.38
2	+87			73.4
3				74.4
	+27			77.7
Elev Garage Floor Rt. =			10.39	76.99
Elev Garage Floor Lt. =			0.80	86.58
	+59			81.80

Lt

k

Rt

$$\frac{74}{50} \frac{8.0}{43} \frac{101}{16} \frac{115}{8} \frac{118}{10} \frac{116}{32} \frac{129}{50} \frac{131}{50}$$

$$\frac{6.5}{50} \frac{8.8}{33} \frac{9.7}{17} \frac{108}{15} \frac{117}{38} \frac{128}{50} \frac{129}{50}$$

$$\frac{9.2}{50} \frac{6.6}{20} \frac{9.1}{17} \frac{10.3}{17} \frac{11.2}{37} \frac{11.5}{50}$$

$$\frac{4.4}{7} \frac{5.2}{25} \frac{6.8}{40} \frac{8.3}{50} \frac{8.9}{50}$$

$$\frac{3.4}{19} \frac{4.1}{19} \frac{6.2}{34} \frac{7.5}{50}$$

$$\frac{6.8}{50} \frac{7.1}{35} \frac{10.0}{25} \frac{13.3}{15} \quad 14.0$$

$$\frac{2.1}{50} \frac{3.3}{37} \frac{5.3}{30} \frac{10.3}{19} \frac{11.0}{17} \quad 13.0$$

$$\frac{1.9}{42} \frac{2.1}{30} \frac{3.2}{21} \frac{7.6}{13} \frac{9.5}{4} \frac{9.7}{6} \frac{9.9}{18} \frac{11.7}{28} \frac{12.6}{32} \frac{11.1}{50} \frac{11.1}{50}$$

$$\frac{1.8}{33} \frac{1.9}{28} \frac{3.7}{18} \frac{5.2}{14} \frac{5.6}{12} \frac{6.9}{15} \frac{9.5}{17} \frac{8.0}{18} \frac{10.0}{19} \frac{10.3}{50}$$

Sta	+	π	-	Elev
		887.38		
3	+77			82.4
	+79			82.5
4				84.4
T.P.	10.58	896.89	1.07	886.31
	+34			87.5
	+51			89.5
	+67			90.7
	+77.79			90.8
South Along Phalen Place. & St.				90.8
North Along Edward Ave. & St.				90.8
T.P.	8.40	904.98	0.31	896.58
B.M.			0.48	904.50
				(904.52)

Lt.

R.

Rt.

$$\frac{15}{50} \quad \frac{25}{25} \quad \frac{40}{17} \quad \frac{50}{50} \quad \frac{52}{12} \quad \frac{72}{15} \quad \frac{61}{17} \quad \frac{61}{18} \quad \frac{96}{20} \quad \frac{101}{50}$$

$$\frac{15}{50} \quad \frac{25}{25} \quad \frac{40}{17} \quad \frac{49}{50} \quad \frac{52}{12} \quad \frac{71}{15} \quad \frac{61}{17} \quad \frac{61}{18} \quad \frac{70}{19} \quad \frac{93}{50}$$

$$\frac{41.2}{50} \quad \frac{09}{41} \quad \frac{17}{29} \quad \frac{29}{20} \quad \frac{30}{50} \quad \frac{36}{11} \quad \frac{49}{14} \quad \frac{42}{16} \quad \frac{56}{20} \quad \frac{51}{40} \quad \frac{60}{50}$$

$$\frac{47}{50} \quad \frac{47}{40} \quad \frac{56}{28} \quad \frac{100}{17} \quad \frac{100}{11} \quad \frac{94}{7} \quad \frac{94}{50} \quad \frac{97}{9} \quad \frac{117}{14} \quad \frac{104}{16} \quad \frac{113}{21} \quad \frac{101}{50}$$

E.
Edward

$$\frac{6.3}{50} \quad \frac{65}{42} \quad \frac{54}{34} \quad \frac{52}{26} \quad \frac{59}{13}$$

$$\frac{74}{50} \quad \frac{77}{7} \quad \frac{105}{13} \quad \frac{100}{15} \quad \frac{94}{25} \quad \frac{85}{30} \quad \frac{86}{50}$$

$$\frac{6.2}{8} \quad \frac{6.6}{16} \quad \frac{93}{16} \quad \frac{83}{20} \quad \frac{6.3}{50}$$

$$\frac{61}{14} \quad \frac{6.5}{21} \quad \frac{86}{25} \quad \frac{75}{41} \quad \frac{61}{50}$$

$$\frac{61}{50} \quad \frac{63}{50} \quad \frac{64}{100} \quad \frac{67}{150}$$

$$\frac{21}{150} \quad \frac{26}{100} \quad \frac{49}{30} \quad \frac{61}{50}$$

Top. N.W. Cor. Steep Front Ent. to No. S.E. Cor. Sophia St. & Edward Ave.

Sta	+	-	Elev
B.M.	4.57	888.23	883.66
T.P.	0.07	874.69	874.62
T.P.	4.38	871.87	867.49
B.M.	7.99	875.51	867.52
T.P.	12.85	880.25	875.40
T.P.	13.63	901.66	888.03
T.P.	3.72	905.21	901.49
B.M.		0.69	904.52
T.P.	2.26	894.50	892.24
T.P.	0.87	888.14	887.27
B.M.		4.49	883.65

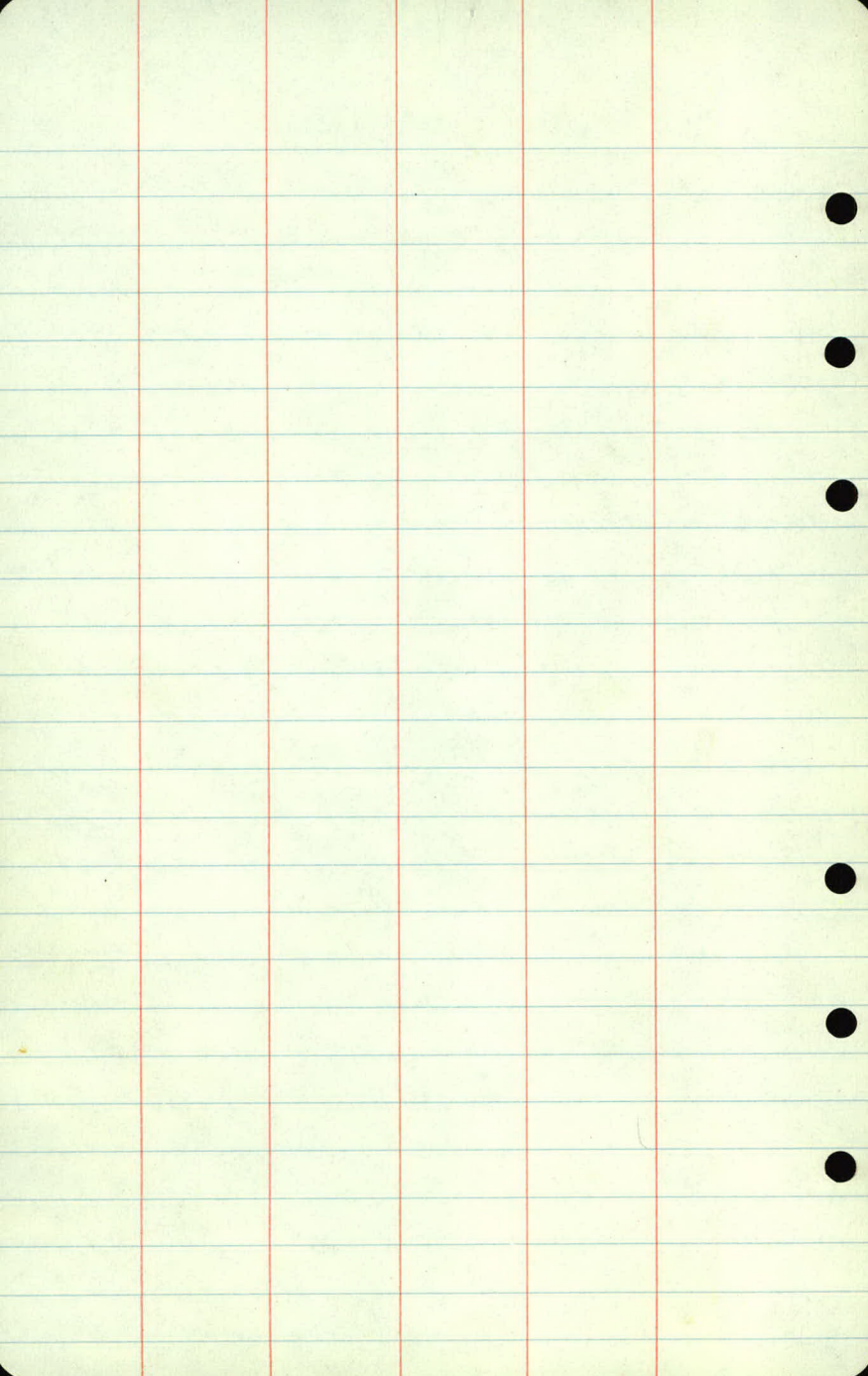
Description

Spk. in G.P. W side of Carpenter Ave. & East Shore Drive.

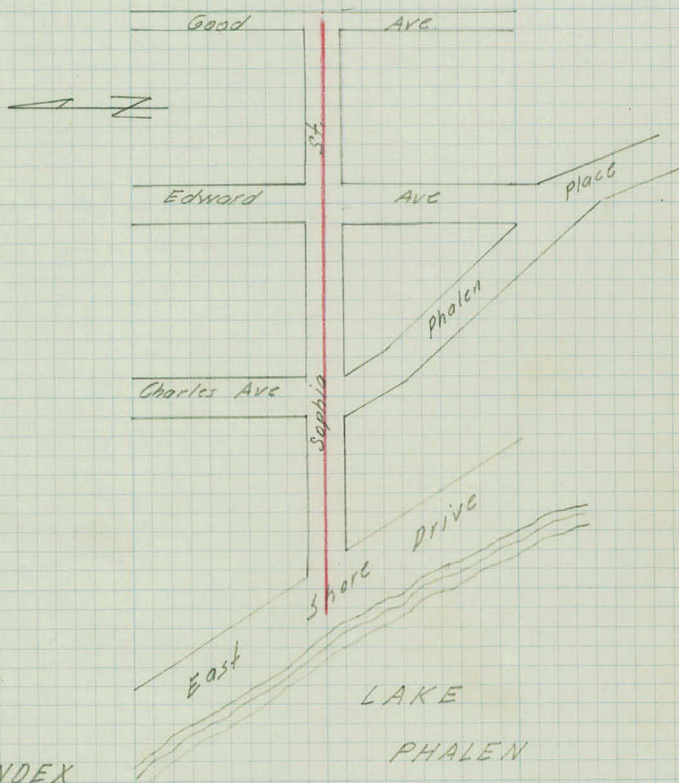
Top R.R. spike Int East Shore Drive & Sophie St.

Top N.W. Cor. Gang Stoop Front Ent to Hs. S.E. Cor. Sophie & Edward.

Spk. in G.P. W. side of Carpenter Ave. & East Shore Drive.



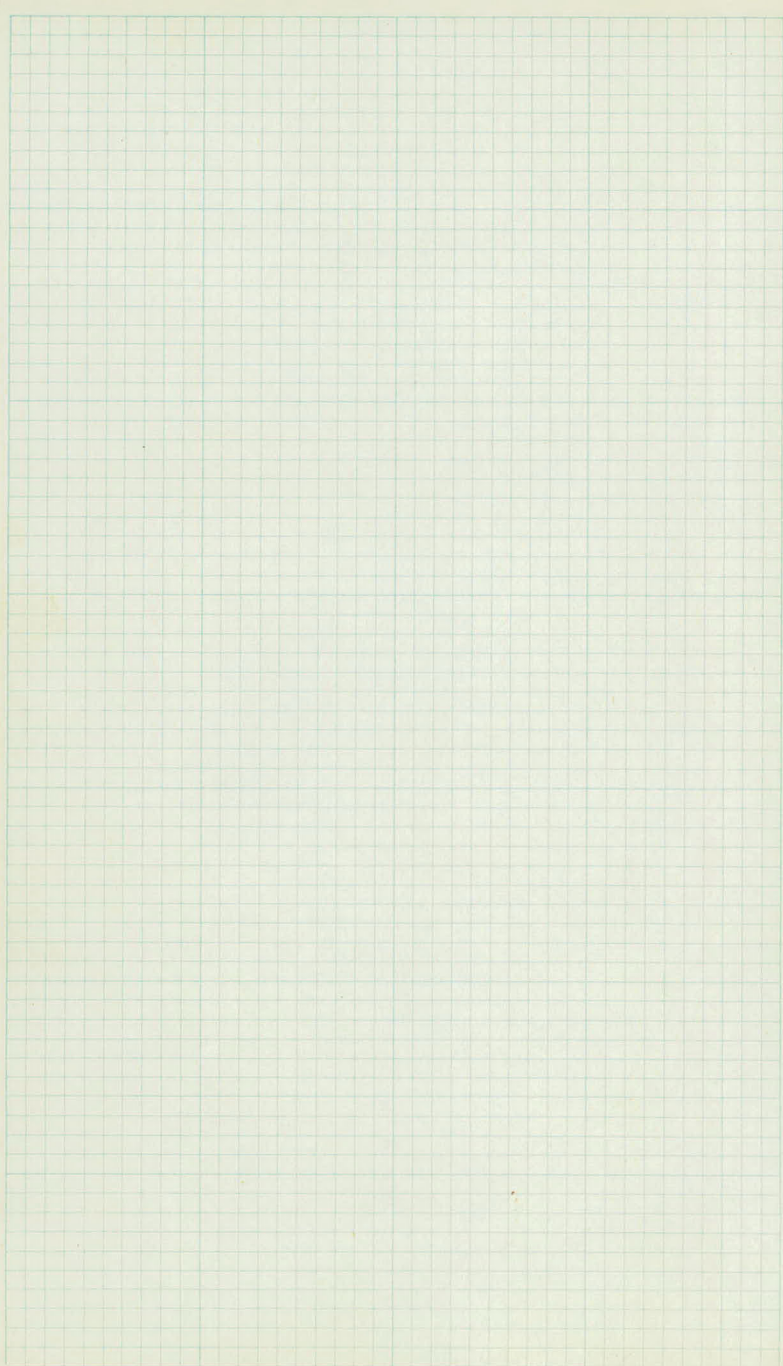
PLAN SURVEY
SOPHIA ST
East Shore Drive to Good Ave.



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- Align. - 1-2
Topog. - 3-5
X Sections - 6-11

Drawn up 1940
Aug 76
W. J. H. H.



Alignment

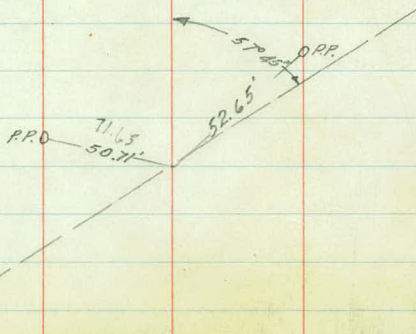
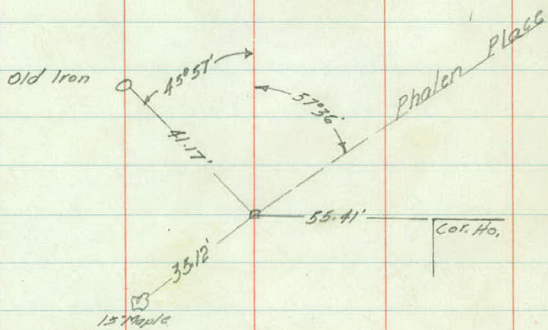
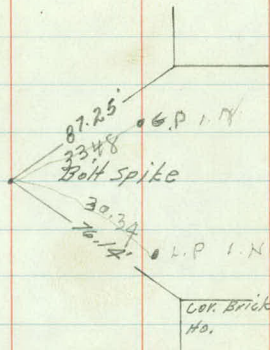
Sta	Point	ΔLt	ΔRt
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5	+58.50	P.O.T = 4 Edward Ave	
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2	+38.85	P.I.	$0^{\circ} 03' 30''$
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0	+00	4 East Shore Drive	
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8-15-40
K.H.
L.C.
L.G.



Sta.	Point	Δ Lt.	Δ Rt.
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8	+62.72	=	Good Ave.
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Topography

+97-Honey Suckle Bush - 37'

+89-Cor. Garden - 13'

+72-4' 12" X 20' C.M.

+44-4' 12" X 26' C.M.

+37-G.P. - 25'

+69-Rd. X 5' 6"

+49-Rd. X 5' 6"

+85-G.P. - 22'

+38-P.P. - 22'

+29-Cor. Retain Wall - 28'

5

8' 14'

+96-Beg. Quarry Stone Wall - 30'

+72-N.W. Cor. Ho. - 42'

+55-Wall - 34' +65-Wall - 41'

+97-Beg. Retain Wall - 22' Wall - 54'

+43-End 12" C.M. - 23'

+36-Wall - 49'

+26-Cor. Retain Wall - 38'

+23-Long. Tie

+07-End 12" C.M. - 25.3'

4

11' 10'

+92-P.P. - 44'

+92-P.P. - 22'

+59-12" P.E. - 33'

+21-15" B.E. - 15'

+84-15" Maple - 19'

3

+77-P.P. - 22'

+67-12" Maple - 19'

+58-12" Maple - 30'

+37-N.E. Cor. Ho. - 56'

+34-Long. Tie

+07-N.W. Cor. Play Ho. - 31'

2

+16-12" Maple - 29'

+99-5" Ash - 31'

+97-End Hedge - 32'

+76-4" Ash - 31'

+57-4" Ash - 31'

+73-N.E. Cor. Ho. - 49'

+46-P.P. - 23'

1

Hedge - 32'

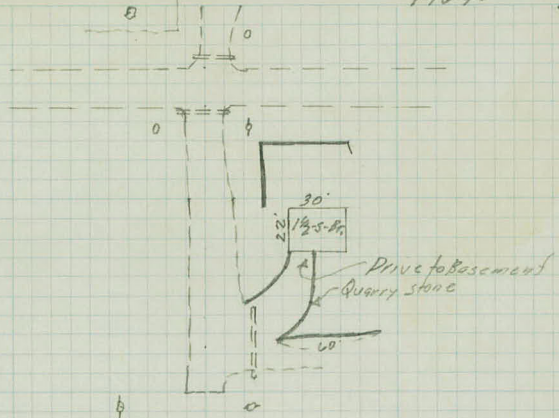
+88-Group 6-3" B.E. - 22'

+50-P.P. - 23'

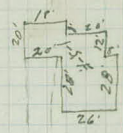
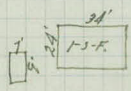
+38-Beg. Hedge - 32'

+19.9 - Edge Conc. Gut. Hor

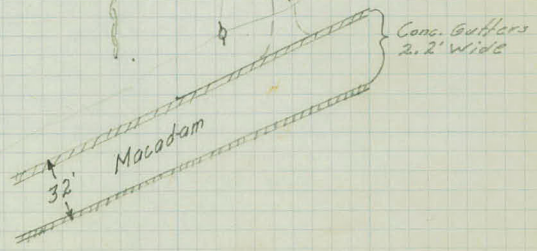
0+00



Uncult.



Drive



488-Shoulder 15 ft
 469-Shoulder 15 ft
 453-End Cult. 21' 16'

8

472-Cult 16' 19'
 469-NW Cor Cor - 75

452-NW Cor Ho - 67'

410-P.P. - 20'

7

480-End Cult - 9'

440-Cult - 11'

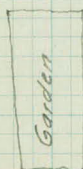
452-R - 2.5' Conc. Walk - 29.5'

407-SW Cor Pump - 50'

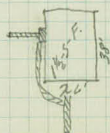
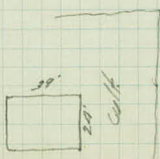
425-0 19' 418-NW Cor Ho - 48

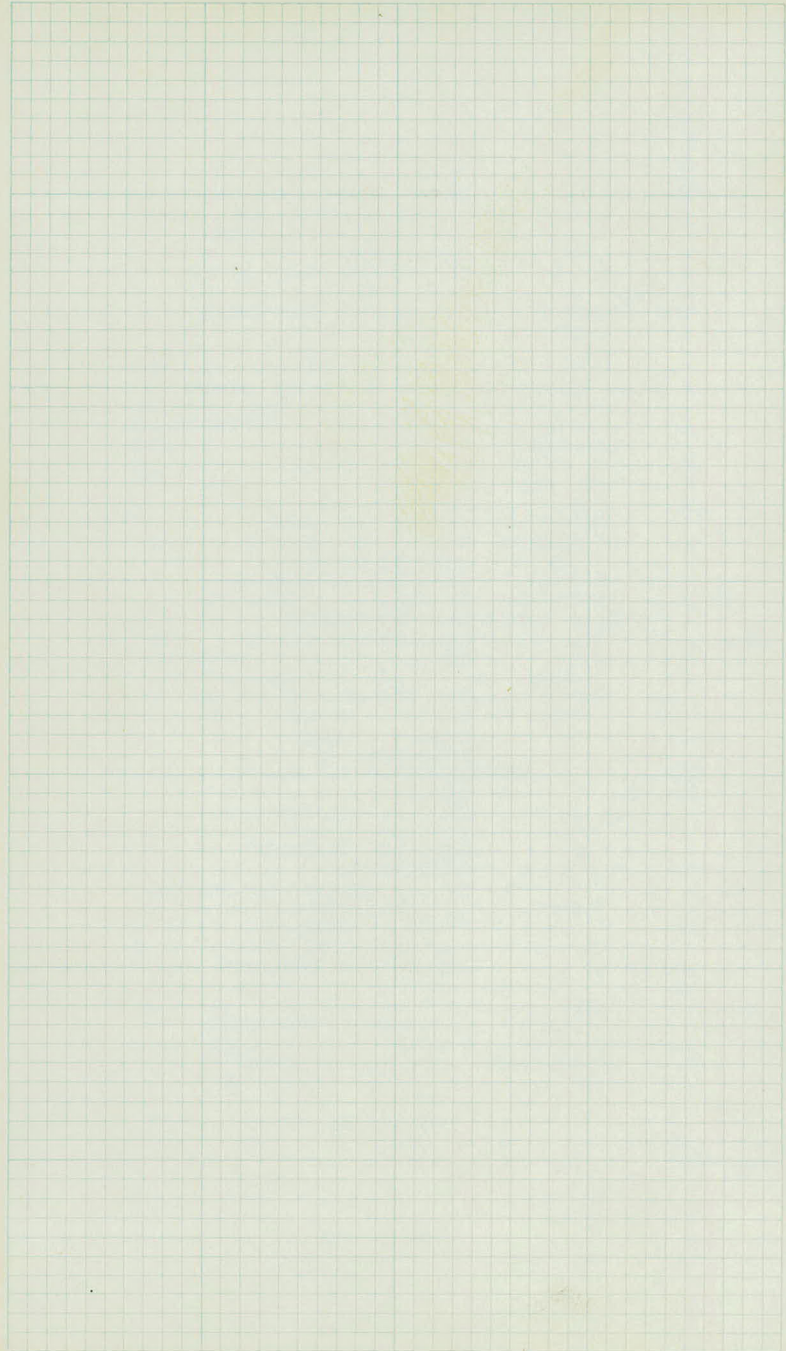
6

1' 19'



b





xsections

Sta	+	-	Elev.
B.M.	4.49	888.15	<u>883.66</u>
T.P.	0.01	878.87	878.86
T.P.	4.49	872.01	867.52
B.M.	7.99	875.53	867.54
T.P.	12.85	888.38	875.53 ⁴⁷
T.P.	13.63	901.79	888.16
T.P.	3.72	905.84	901.62
B.M.		0.69	904.65
T.P.	2.26	894.63	892.37
T.P.	0.87	888.27	887.40
B.M.		4.49	883.78
B.M.	8.21	875.73	<u>867.52</u>

Do Not Use These
Bench Levels

0	+00		66.98
	+18.9		67.30
	+30		67.9
T.P.	10.01	880.59	870.58
1			69.7
	+28		69.8

Lt

C

Rt

Spt in G.P. W. side of So. Shore Drive & Larpentour Ave.

Top R.R. Spike Int. East Shore Drive & Sophia St.

Front Ent.

Top N.W. Cor. Upper Steps of Ho. S.E. Cor. Sophia St. & Edward Ave.

Spt in G.P. W. side of S. Shore Blvd. & Larpentour Ave.

Top R.R. Spike Int. East Shore Drive & Sophia St.

8.75

<u>8.07</u>	<u>8.43</u>	<u>8.83</u>
50		50

<u>38</u>	<u>42</u>	<u>41</u>	<u>67</u>	<u>78</u>	<u>83</u>	<u>84</u>	<u>87</u>
50	30	26	10		8	30	50

<u>57</u>	<u>66</u>	<u>106</u>	<u>109</u>	<u>105</u>	<u>126</u>	<u>119</u>	<u>122</u>
50	27	19		15	28	31	50

<u>31</u>	<u>53</u>	<u>56</u>	<u>69</u>	<u>103</u>	<u>108</u>	<u>115</u>	<u>122</u>	<u>115</u>	<u>119</u>
50	37	24	18	12		13	27	27	50

Sta.	+	Σ	-	Elev.
		880.58 880.59		
1	+47			69.9.
	+73			70.1.
2				68.9.
	+38.85			70.5.
T.P.	9.53	880.26 880.27	9.85	870.73 870.74
	+63			71.6.
	+84			72.1.
3				73.7.
	+30			76.3.
T.P.	12.06	891.09 891.10	1.23	879.03 879.04
	+60			80.9.
	+77			83.8.
4				86.3.

Lt

K

Rt

$$\frac{1.2}{50} \quad \frac{35}{44} \quad \frac{50}{56} \quad \frac{54}{30} \quad \frac{44}{28} \quad \frac{53}{17} \quad \frac{100}{13} \quad \frac{107}{18} \quad \frac{115}{27} \quad \frac{118}{31} \quad \frac{113}{50}$$

$$\frac{31}{50} \quad \frac{42}{39} \quad \frac{54}{28} \quad \frac{61}{26} \quad \frac{66}{17} \quad \frac{100}{11} \quad \frac{105}{17} \quad \frac{112}{28} \quad \frac{117}{31} \quad \frac{110}{50} \quad \frac{118}{50}$$

$$\frac{40}{50} \quad \frac{40}{43} \quad \frac{56}{41} \quad \frac{62}{29} \quad \frac{81}{25} \quad \frac{94}{13} \quad \frac{111}{7} \quad \frac{117}{15} \quad \frac{125}{26} \quad \frac{118}{29} \quad \frac{111}{42} \quad \frac{119}{50} \quad \frac{118}{50}$$

$$\frac{46}{50} \quad \frac{69}{32} \quad \frac{81}{20} \quad \frac{95}{15} \quad \frac{101}{7} \quad \frac{106}{10} \quad \frac{111}{36} \quad \frac{116}{40} \quad \frac{105}{50} \quad \frac{106}{50}$$

$$\frac{54}{50} \quad \frac{68}{38} \quad \frac{81}{19} \quad \frac{87}{4} \quad \frac{90}{8} \quad \frac{94}{25} \quad \frac{110}{36} \quad \frac{125}{50} \quad \frac{127}{50}$$

$$\frac{25}{50} \quad \frac{57}{34} \quad \frac{70}{16} \quad \frac{85}{4} \quad \frac{82}{5} \quad \frac{83}{13} \quad \frac{93}{30} \quad \frac{98}{50} \quad \frac{114}{50}$$

$$\frac{10}{50} \quad \frac{20}{45} \quad \frac{48}{30} \quad \frac{67}{7} \quad \frac{70}{2} \quad \frac{66}{3} \quad \frac{67}{15} \quad \frac{86}{29} \quad \frac{95}{43} \quad \frac{109}{50} \quad \frac{112}{50}$$

$$\frac{127}{50} \quad \frac{105}{36} \quad \frac{09}{25} \quad \frac{22}{9} \quad \frac{40}{4} \quad \frac{39}{13} \quad \frac{56}{21} \quad \frac{62}{38} \quad \frac{82}{50} \quad \frac{93}{50}$$

$$\frac{48}{50} \quad \frac{64}{29} \quad \frac{85}{12} \quad \frac{102}{5} \quad \frac{101}{18} \quad \frac{126}{50} \quad \frac{180}{50}$$

$$\frac{12}{50} \quad \frac{34}{31} \quad \frac{58}{16} \quad \frac{73}{6} \quad \frac{81}{17} \quad \frac{99}{34} \quad \frac{128}{50} \quad \frac{153}{50}$$

$$\frac{121}{50} \quad \frac{103}{36} \quad \frac{27}{20} \quad \frac{40}{12} \quad \frac{48}{15} \quad \frac{65}{40} \quad \frac{105}{50} \quad \frac{124}{50}$$

Sta.	+	π	-	Elev
		891.09 891.10		
4	+07	Flow Line Culv Rt.		
		897.93.		886.58
T.P.	10.95	897.94	4.11	886.99
	+16			871.
	+26			89.5.
	+26			
	+43	Flow Line Culv. Rt.		
	+47			90.6.
	+72			93.6
		908.83.		896.46.
T.P.	12.37	908.84	1.47	896.47
5				97.4.
	+28			00.1.
	+28			
	+41			01.0.

Lt.

E.

Rt.

6.93 84.15

29 34 52 76 85 101 108 114 121 134 138
50 41 30 22 12 8 13 27 37 50

Top Wall
84 102 108 111 91 99 113
14 27 38 38 50 69

Bottom Wall 14.0 141
50 69

10.48 87.45

Top Wall Top Wall
01 05 33 46 75 79 75 73 78 82 92 65 92 100 96 66
50 33 25 15 6 4 3 11 19 22 22 24 36 53 53

74.03 Top Wall Base 100.03 Top Wall
118 113 102 12 43 47 54 46 43 44 47 53 40 39 88 89 37 94.03
50 31 18 13 11 7 6 4 7 17 19 22 43 43 52 52

Top Wall 96.93
73 75 81 92 118 122 113 114 115 120 127 117 119 128 129
50 40 18 14 12 9 7 9 15 17 20 31 31 50

900.03 Top Wall 99.73
57 63 80 87 84 87 90 95 88 91
50 20 15 12 10 14 16 19 31 50

Bottom Wall 128 131
31 50

51 55 59 76 73 78 83 90 86 91 95
50 34 17 15 13 13 15 17 36 50

Sta	+	π	-	Elev
		908.83. 908.84		
5	+44			01.1.
	+585 = R. Edward Ave.			01.5.
	+72			02.4.
	+76			02.8.
6				04.3.
	+40			03.4.
B.M.			4.32	904.51. 904.52 (904.52)
	+52 Sidewalk Rt.			
	+82			01.2✓
7				00.1
T.P.	0.76	900.65 900.66	8.94	899.89. 899.90
	+25			97.1.
	+40			96.3.

Lt

R

Rt

00.56
FLGWN

$$\begin{array}{r} 71 \ 75 \ 82.8 \ 70 \\ 50 \ 29 \ 14 \ 14 \end{array}$$

FLGWN 99.63

$$\begin{array}{r} 77 \ 79 \ 92 \ 95 \ 102 \\ 11 \ 12 \ 27 \ 50 \end{array}$$

$$\begin{array}{r} 46 \ 60 \ 73 \\ 100 \ 30 \end{array}$$

$$\begin{array}{r} 92 \ 105 \\ 50 \ 100 \end{array}$$

FLGWN 60.93

FLGWN 00.38

$$\begin{array}{r} 66 \ 79 \ 79 \ 66 \ 64 \ 71 \ 84.5 \ 86 \ 94 \\ 50 \ 21 \ 7 \ 7 \ 13 \ 13 \ 27 \ 50 \end{array}$$

$$\begin{array}{r} 40 \ 43 \ 48 \\ 50 \ 29 \ 8 \end{array}$$

$$\begin{array}{r} 6.0 \\ 6 \end{array}$$

$$\begin{array}{r} 6.0 \ 6.6 \ 75 \ 80 \\ 17 \ 32 \ 50 \end{array}$$

$$\begin{array}{r} 39 \ 40 \ 40 \ 45 \ 52 \ 56 \ 59 \\ 50 \ 30 \ 19 \ 18 \ 42 \ 50 \end{array}$$

$$\begin{array}{r} 49 \ 53 \ 51 \ 49 \ 54 \ 56 \ 57 \ 54 \\ 50 \ 30 \ 18 \ 7 \ 15 \ 31 \ 48 \end{array}$$

Front

Topstern

Top N.W. Cor. Conc. Sloop Ent. to Ho. S.E. Cor. Edward Ave. & Sophist.

$$\begin{array}{r} 572 \ 553 \ 493 \ 486 \\ 29.5 \ 43 \ 43 \ 48 \end{array}$$

$$\begin{array}{r} 10.0 \ 79 \ 76 \ 76 \ 72 \ 71 \ 63 \\ 50 \ 24 \ 11 \ 13 \ 30 \ 30 \end{array}$$

$$\begin{array}{r} 123 \ 108 \ 88 \ 87 \ 90 \ 80 \ 74 \\ 50 \ 25 \ 6 \ 19 \ 37 \ 50 \end{array}$$

Nail in R.R.

$$\begin{array}{r} 110 \ 82 \ 57 \ 36 \ 30 \ 31 \ 21 \ 12 \\ 50 \ 50 \ 5 \ 4 \ 18 \ 41 \ 50 \end{array}$$

$$\begin{array}{r} 13.3 \ 118 \ 93 \ 70 \ 42 \ 44 \ 36 \ 3.0 \ 2.2 \ 2.6 \\ 50 \ 35 \ 13 \ 9 \ 3 \ 5 \ 14 \ 35 \ 50 \end{array}$$

Sta	+	π' 900.65 900.66	-	Elev
7	+51			73.4
	+62			88.7
T.P.	3.25	891.44 891.45	12.46	88.19. 888.20 847.
8				
	+47			83.0
	+62.72			82.9
	+70			85.3
	+78			86.1
T.P.	11.65	902.51 902.52	0.58	890.86 890.87
T.P.	6.38	907.32 907.33	1.57	900.84 900.95
B.M.			2.81	904.51 894.52
				904.52 894.52

8-17-40
K.A.
L.G.
L.G.

11

41

4

Rt.

00.95

$\frac{139}{50}$ $\frac{122}{24}$ $\frac{106}{7}$ $\frac{73}{8}$ $\frac{46}{18}$ $\frac{42}{34}$ $\frac{23}{50}$ $\frac{26}{50}$ $\frac{10.3}{\text{Elev 1st floor Ho.}}$

$\frac{15.0}{50}$ $\frac{140}{25}$ $\frac{127}{70}$ $\frac{128}{5}$ $\frac{12.0}{16}$ $\frac{108}{35}$ $\frac{87}{45}$ $\frac{75}{50}$ $\frac{55}{50}$

Top N. End End Calc.

$\frac{81}{50}$ $\frac{84}{41}$ $\frac{77}{38}$ $\frac{75}{22}$ $\frac{67}{19}$ $\frac{61}{36}$ $\frac{57}{50}$ $\frac{44}{50}$

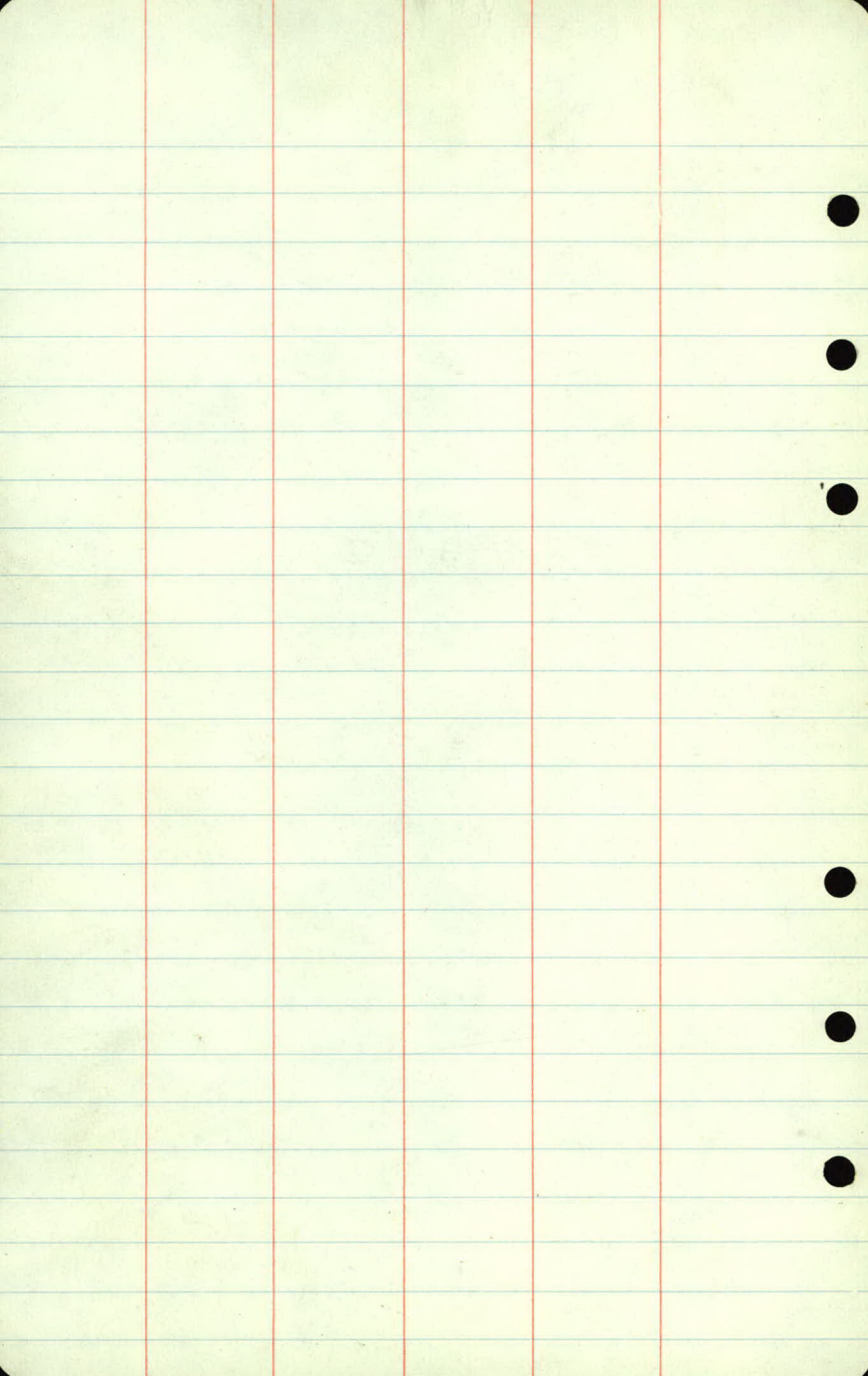
$\frac{87}{50}$ $\frac{88}{36}$ $\frac{92}{26}$ $\frac{96}{24}$ $\frac{84}{50}$ $\frac{80}{50}$ $\frac{70}{50}$

$\frac{90}{50}$ $\frac{89}{23}$ $\frac{85}{23}$ $\frac{83}{23}$ $\frac{76}{50}$

$\frac{68}{50}$ $\frac{64}{22}$ $\frac{61}{23}$ $\frac{53}{23}$ $\frac{45}{50}$

$\frac{71}{100}$ $\frac{63}{50}$ $\frac{58}{50}$ $\frac{40}{50}$ $\frac{21}{100}$

Top N.W. Cor. Stoop Ent. to Front of Ho. S.E. Cor. Sophie & Edward Ave.



Align.

Sophia Str.

From Edward To Good Str.

Drawn up
9/26/41
WJB
Z.L.G.

Sta.	Pt.	Alt	Art.
------	-----	-----	------

8+77 ⁸¹	East ROW	Good Str.	
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8+47 ⁸¹	West ROW.		
--------------------	-----------	--	--

7+18.50	P.O.T.	± ALLEY	
---------	--------	---------	--

51	P.O.T.		
----	--------	--	--

5+58 ⁵⁰	P.O.T	± Edward	
--------------------	-------	----------	--

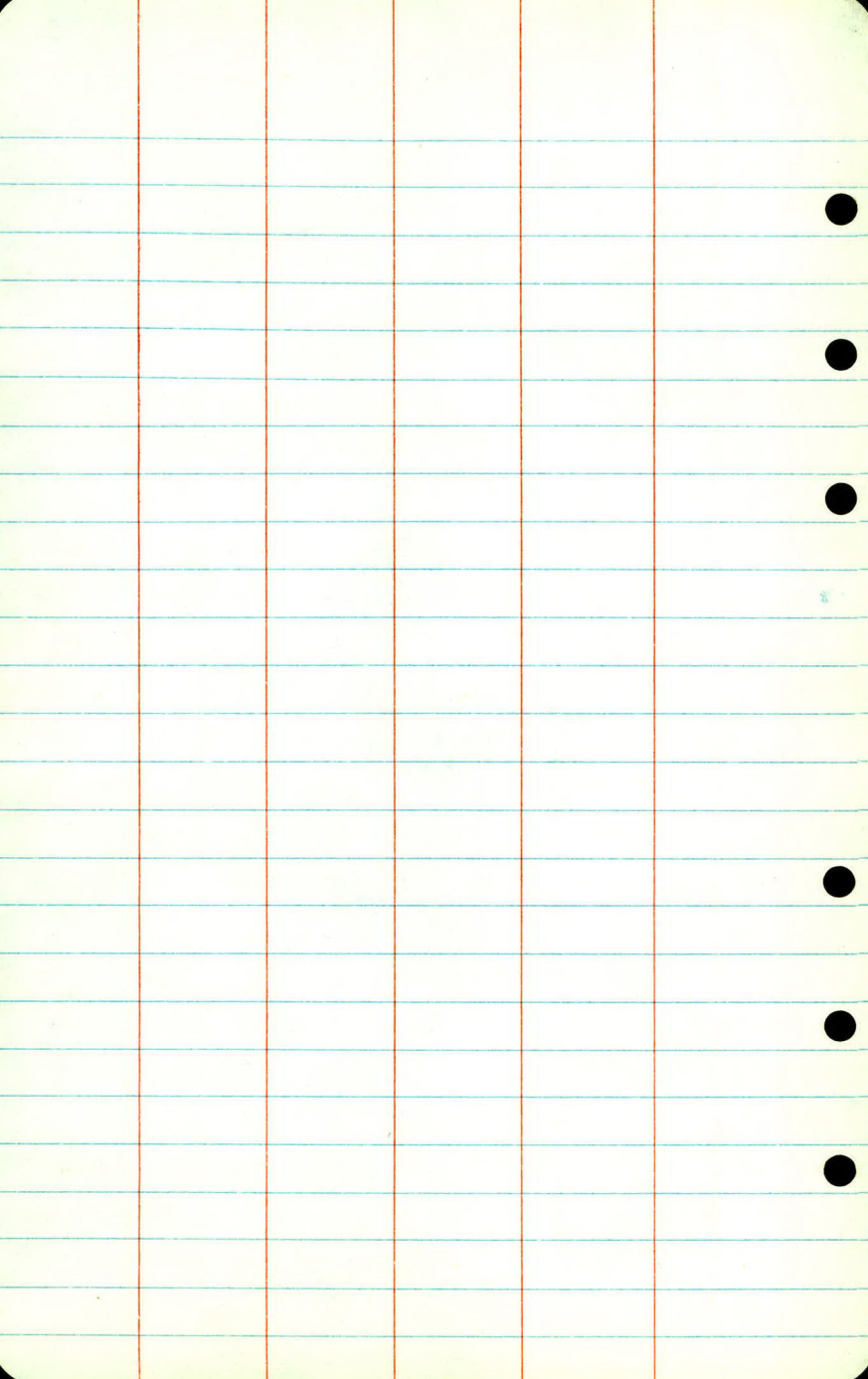
Iron • 36' Nail 36' Iron

68.24' Cor Foun

Spk 71.50 Cor. Foun.

87.25' Cor Foun

Boat Spk. 76.14' Cor. Brick Ho



Topography

9

Rd

Rd.

+86 Shoulder

+71 Shoulder

8

+80 End Rd

+50

4

14'

7

4'

11

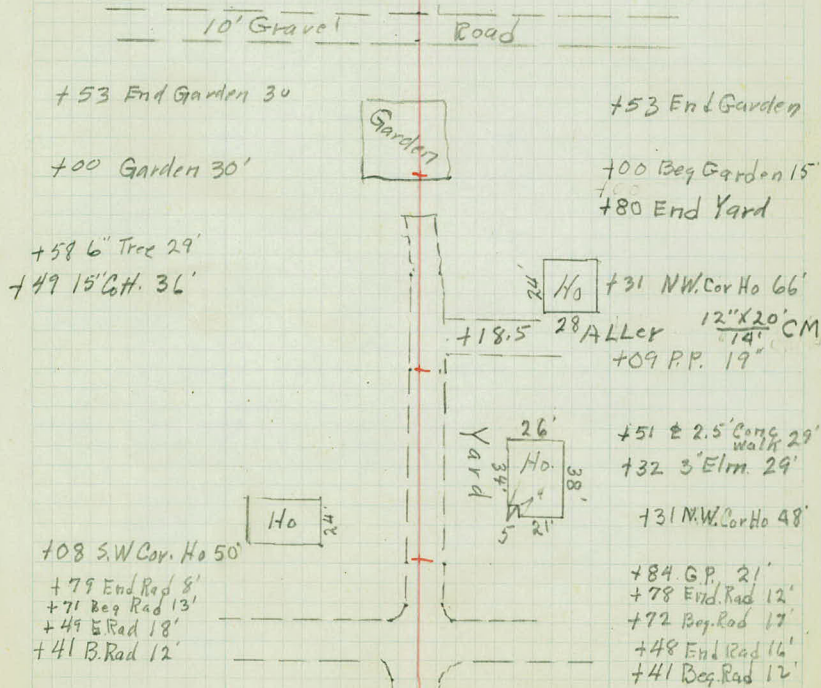
13' Roadway

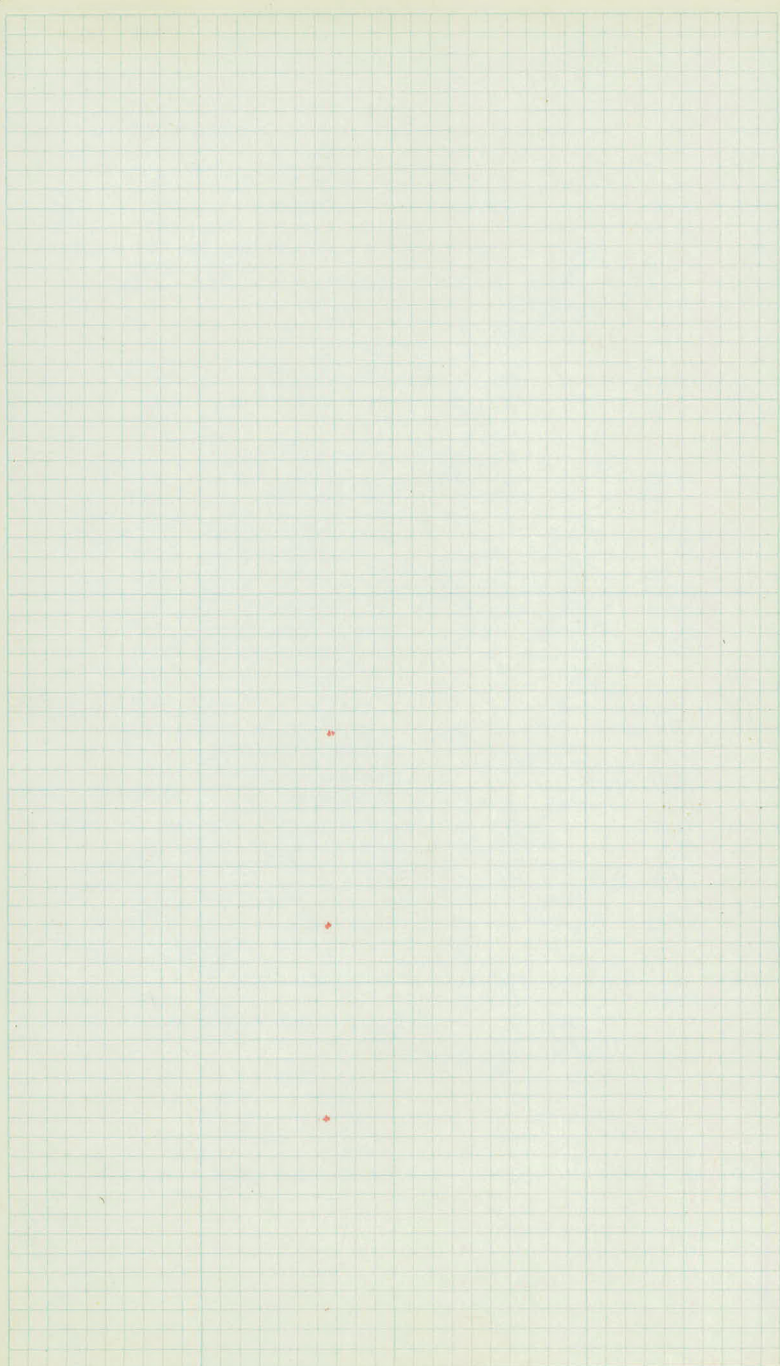
6

6'

12'

5





Cross Sections

Sta	+	Δ	-	Elev
B.M.	1.63	906.15.		904.52

5+58.5	$\neq$	Edward st.		901.6
--------	--------	------------	--	-------

+72				01.9
-----	--	--	--	------

+87				01.9
-----	--	--	--	------

6				01.7
---	--	--	--	------

+50				01.0
-----	--	--	--	------

+72				00.7
-----	--	--	--	------

+89				00.2
-----	--	--	--	------

7				899.7
---	--	--	--	-------

+10				99.0
-----	--	--	--	------

+12				98.9
-----	--	--	--	------

+28				97.6
-----	--	--	--	------

+50				
-----	--	--	--	--

Lt.

E

Rt

6

N.W. Cor Top Conc Step Ho. S.E. Cor Sophia + Edward

$$\frac{3.3}{50} \quad \frac{4.0}{25} \quad 4.6 \quad \frac{5.5}{25} \quad \frac{6.4}{50}$$

$$\frac{3.8}{50} \quad \frac{4.4}{18} \quad 4.3 \quad \frac{4.7}{12} \quad \frac{5.4}{20} \quad \frac{6.5}{50}$$

$$\frac{1.4}{50} \quad \frac{3.2}{13} \quad \frac{4.7}{7} \quad 4.3 \quad \frac{4.6}{14} \quad \frac{3.1}{18} \quad \frac{3.7}{50}$$

$$\frac{0.7}{\text{Elev of Gro. at Ho}} \quad \frac{1.0}{50} \quad \frac{1.8}{28} \quad \frac{2.9}{12} \quad \frac{4.8}{7} \quad 4.5 \quad \frac{4.7}{14} \quad \frac{3.0}{18} \quad \frac{2.7}{31} \quad \frac{3.1}{50}$$

$$\frac{2.8}{50} \quad \frac{2.9}{26} \quad \frac{4.0}{22} \quad \frac{4.0}{9} \quad \frac{5.5}{6} \quad 5.2 \quad \frac{5.4}{13} \quad \frac{3.6}{20} \quad \frac{2.9}{46} \leftarrow \text{Elev of Gro. at Ho}$$

$$\frac{5.3}{50} \quad \frac{4.4}{29} \quad \frac{4.8}{10} \quad \frac{6.3}{6} \quad \frac{5.8}{3} \quad 5.5 \quad \frac{5.7}{13} \quad \frac{4.2}{18} \quad \frac{3.2}{50}$$

$$\frac{6.5}{50} \quad \frac{6.2}{24} \quad \frac{6.0}{8} \quad \frac{6.7}{6} \quad \frac{6.2}{5} \quad 6.0 \quad \frac{6.2}{11} \quad \frac{6.6}{14} \quad \frac{5.5}{15} \quad \frac{4.3}{31} \quad \frac{3.9}{50}$$

$$\frac{10.4}{50} \quad \frac{9.5}{45} \quad \frac{8.0}{18} \quad \frac{6.7}{9} \quad \frac{6.9}{5} \quad \frac{6.7}{4} \quad 6.5 \quad \frac{6.7}{10} \quad \frac{7.5}{12-15} \quad \frac{6.3}{16} \quad \frac{4.4}{50}$$

$$\frac{12.8}{50} \quad \frac{11.0}{29} \quad \frac{8.7}{10} \quad \frac{7.3}{5} \quad 7.2 \quad \frac{7.3}{11} \quad \frac{8.4}{13-15} \quad \frac{6.8}{16} \quad \frac{5.3}{50}$$

$$\frac{12.8}{50} \quad \frac{11.0}{29} \quad \frac{8.7}{10} \quad \frac{7.3}{5} \quad 7.3 \quad \frac{7.5}{11} \quad \frac{8.4}{13-15} \quad \frac{8.3}{17} \quad \frac{7.9}{50}$$

$$\frac{16.9}{50} \quad \frac{12.5}{11} \quad \frac{8.9}{4} \quad 8.6 \quad \frac{8.9}{13} \quad \frac{9.8}{14-15} \quad \frac{8.6}{18} \quad \frac{7.4}{50}$$

Sta	+	Δ	-	Elev
		906.15		
7+50				95.2
T.P.	1.49	896.57	11.07	895.08.
7+50				95.2
B.M.	7.57	896.57	7.57	889.00
+65				92.5
+85				87.0
8				85.2
+48	West Prop Line			83.1
+64				83.2
+70	Top West Shoulder			85.6
+78	£ Good Str			86.0
+88	Top East Shoulder			85.6
T.P.	10.74	905.79	1.52	895.05
B.M.			1.28	904.51 904.52

Z

$$\frac{11.6}{4} \quad 110 \quad \frac{10.6}{15} \quad \frac{11.1}{16} \quad \frac{10.3}{19} \quad \frac{9.0}{30} \quad \frac{7.9}{50} \quad \frac{6.9}{\text{Elev. of}} \\ \text{Gro. Ho}$$

$$\frac{10.1}{50} \quad \frac{8.9}{33} \quad \frac{6.9}{14} \quad (1.4)$$

Spt in 15" CoH 33 Lt Sta 7149

$$\frac{11.1}{50} \quad \frac{10.5}{31} \quad \frac{8.8}{12} \quad \frac{4.3}{3} \quad 41 \quad \frac{3.7}{14} \quad \frac{5.2}{21} \quad \frac{3.3}{44} \quad \frac{2.1}{50}$$

$$\frac{12.4}{50} \quad \frac{11.8}{29} \quad \frac{10.5}{5} \quad 9.6 \quad \frac{9.2}{14} \quad \frac{9.5}{25} \quad \frac{6.6}{50}$$

$$\frac{13.3}{50} \quad \frac{12.6}{26} \quad 11.4 \quad \frac{11.2}{21} \quad \frac{9.3}{50}$$

$$\frac{13.8}{50} \quad \frac{13.6}{18} \quad 13.5 \quad \frac{13.3}{29} \quad \frac{12.2}{50}$$

$$\frac{13.8}{50} \quad \frac{13.8}{24} \quad 13.4 \quad \frac{13.1}{25} \quad \frac{12.3}{50}$$

$$\frac{12.0}{50} \quad \frac{11.5}{21} \quad 11.0 \quad \frac{10.4}{22} \quad \frac{9.7}{50}$$

$$\frac{11.3}{50} \quad \frac{11.0}{24} \quad 10.6 \quad \frac{9.8}{22} \quad \frac{9.1}{50}$$

$$\frac{11.7}{50} \quad \frac{11.4}{22} \quad 11.0 \quad \frac{10.6}{16} \quad \frac{9.9}{50}$$

Top N.W Cor Conc Step S.E. Cor Ho, Sophia & Edward

