

BK 32 Dr. 12A

OFFICE OF COUNTY ENGINEER
RAMSEY CO. MINN.

..... Plan Survey

..... Labore Ave.

From Noel To Edgerton

Road Acc't. No. N-60

Date Filed..... File.....

BK 32 Dr 12A

PLAN SURVEY

LABORE AVE

Completed. 8-14-40

INDEX :

Alignment 1-2

Topography 3-5

Cross Sections 6-11

PARTY:

R. Reese

A. Moeschter

L. Goldberg

C. Fewer.

Plan Partial Completed

Dropped

9-10-40

sto.

12+75.94 £ Edgerton

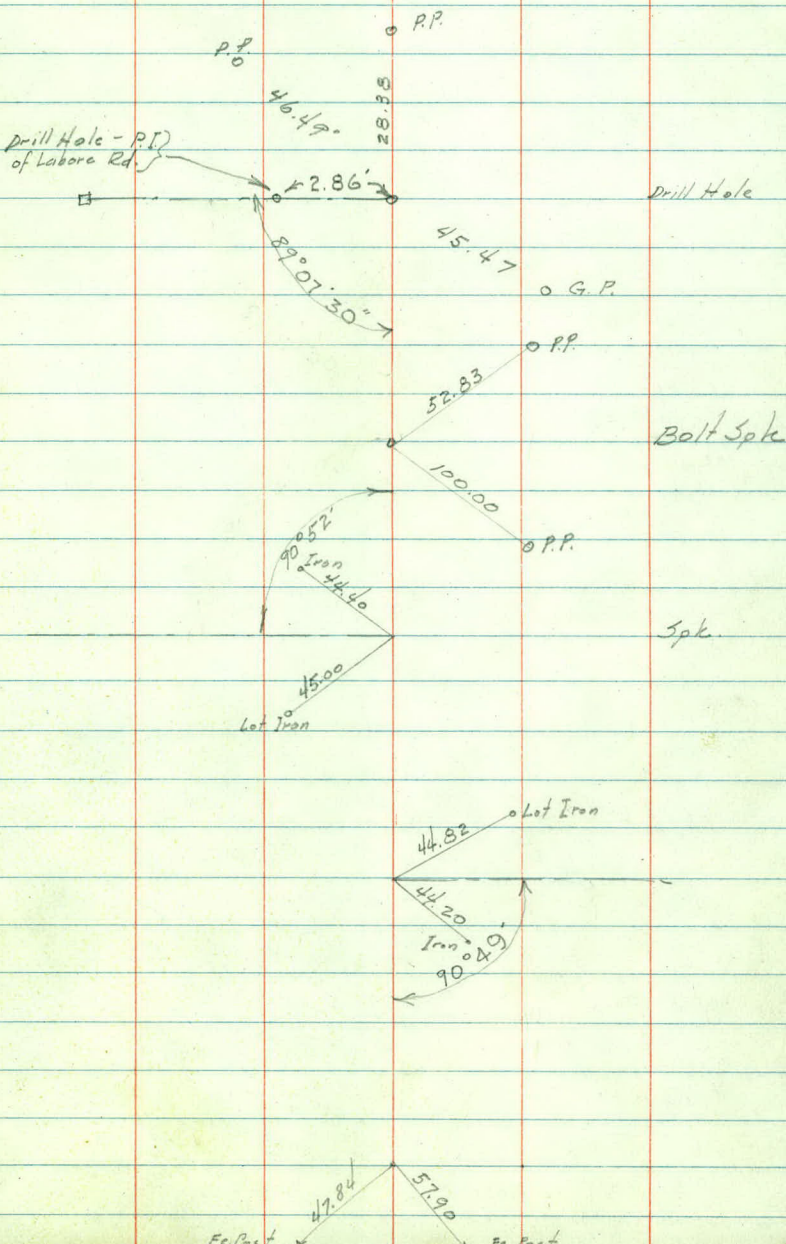
7+50 P.O.T.

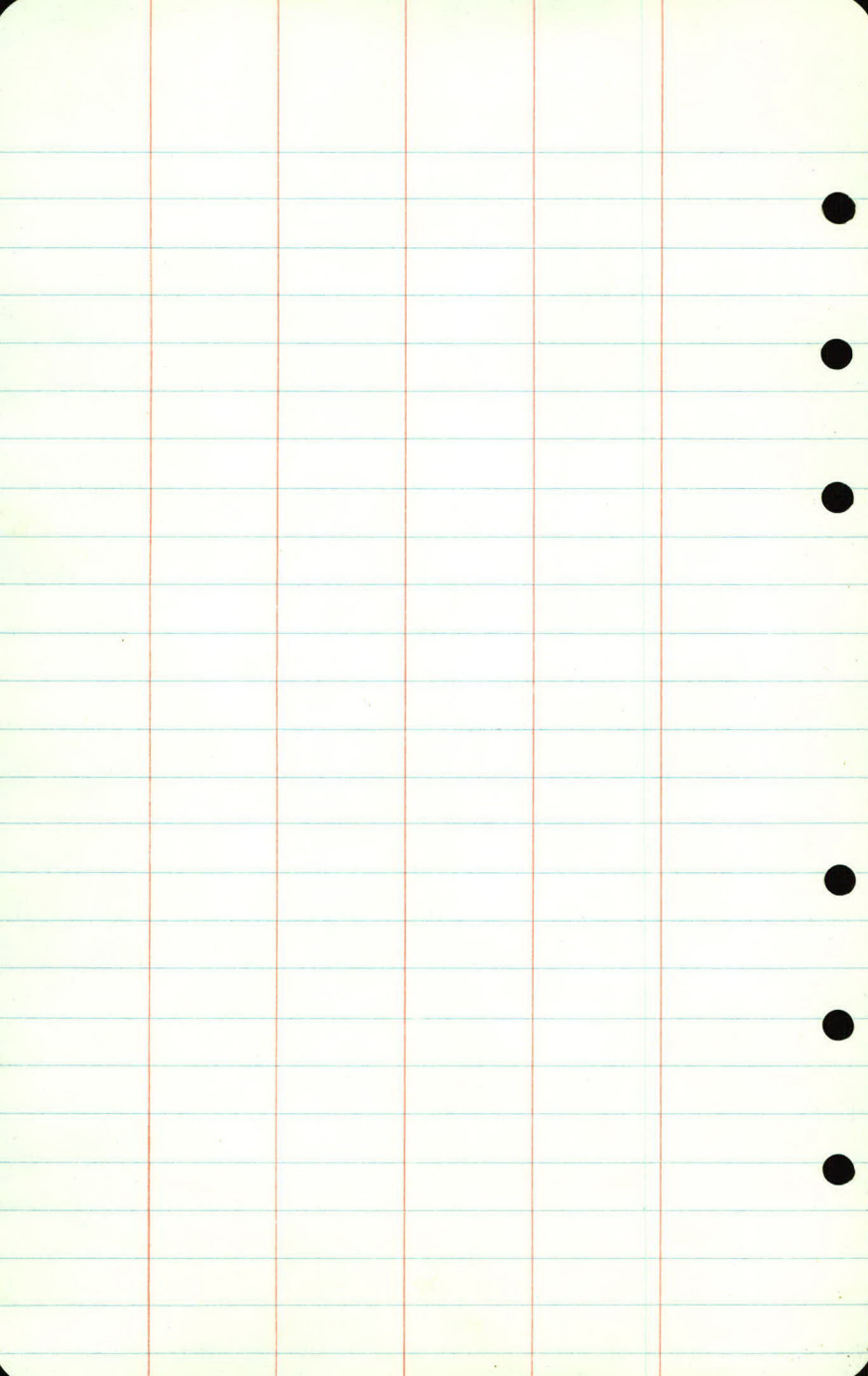
5+76.13 £ Vander Bie

2+29.99 £ Noel

6+00

0+00





Topography

LABORE AVE.

6
5
4
3
2
1
0

1
10
10
11

9
9
8

+20 Shldr xs £

0-33 Fc xs £

+86 Bag Rad 39
 +170 End Rad 30
 +60 Bag Rad 10
 +42 1" Sap 38

VANDER BIE

+92 1" Sap 38
 +76 1" Sap 38
 +62 1" Sap 38

+98 1" Sap 38

108 P.P. 25
 +93 Ent

+58 1" Sap 38

+49 Ent

+23 Ent
 +16 1" Sap 38

+74 1" Sap 38

+61 P.P. 24

+33 1" Sap 38

+92 1" Sap 38

+77 End Rad. -12

+77 Bag. Cul. 40
 +51 1" Sap 38
 +50 Shldr. 09

+40 Bag. Rad. 50

NOEL

+09 1" Sap 38
 +08 G.P. 25

+09 P.P. 25
 Ent 6'
 Ditch - 22

+67 1" Sap 38

Yard.

+62 2" Stand Pipe 39

+27 1" Sap 38

+44 Ent 6'

+25 Ent -22

+47 1" Sap 38

Cultivated

+04 1" Sapling 38

x x x x x x x

13

22

 $+54 - 15^{\circ} \times 40^{\circ} \text{ C.M.}$
 $+66 \text{ P.O.C. } \times 3 \frac{1}{2}$

18

12

//

//

11

12

//

19

 $+02 - 18^{\circ} \times 40^{\circ} \text{ C.M.}$

21

10

8

//

9

10

//

8

//

//

7

//

//

6

//

EDGERTON ST.

+66 End Rod 35
+44 Bag. Rod 13

+66 End Rod 36
+53 G.P. 39
+42 Fe. Cor 33
+33 Bag. Rod 11
+07 P.P. 25
Fe 38

Fe 54
+83 P.P. 25

+40 P.P. 25

+97 P.P. 25

+62 Ent

+33 1" Sap 38

+93 1" Sap 38

+51 1" Sap 38

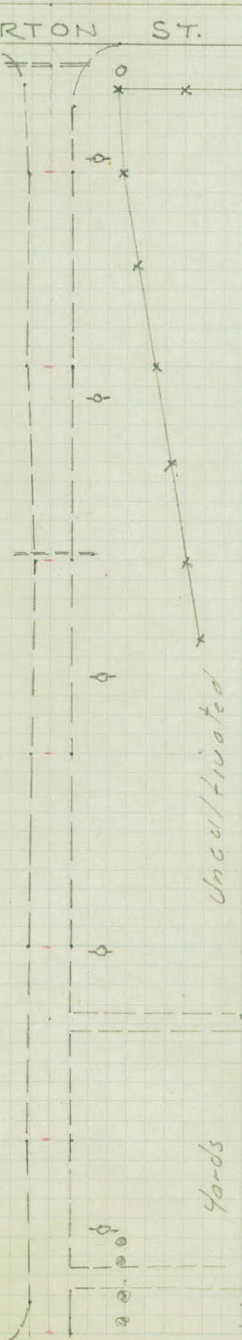
+14 End. Road 10
+09 1" Sap 38

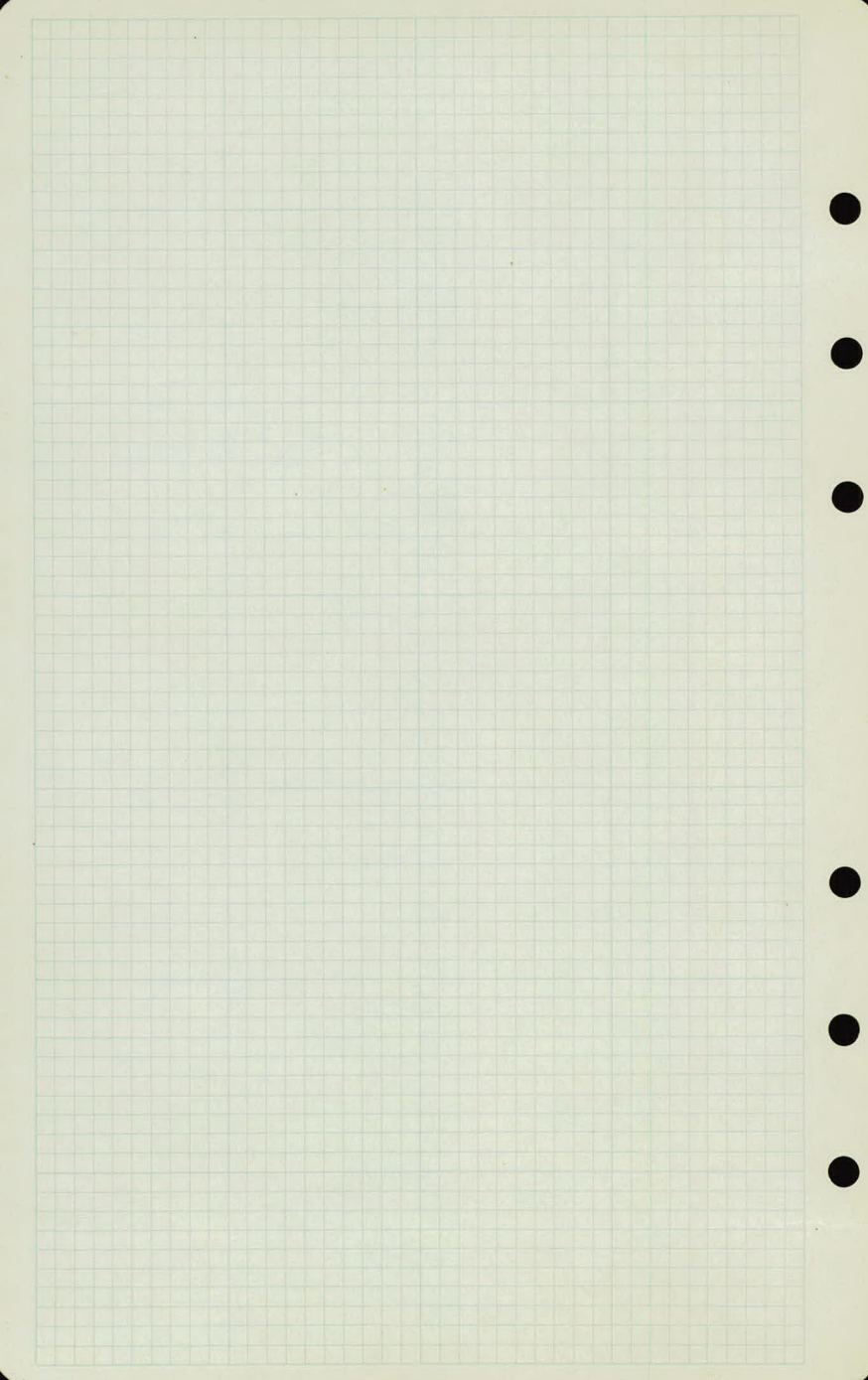
+54 P.P. 25
+49 1" Sap 38
+38 1" Sap 38
+27 Ent
+20 1" Sap 38
+06 1" Sap 38

Hay Field

Uncultivated

Yards





6
1
Cross Sections

LABORE AVE.

Sta.	+	π	-	Elev.
B.M.	6.65	903.61		896.96
T.P.	11.17	909.70	3.08	898.53
T.P.	3.51	912.35	0.86	908.84
B.M.	3.63	911.44	4.54	907.81
0+00			6.1	05.3

+50		6.0	05.4
-----	--	-----	------

1		5.8	05.6
---	--	-----	------

+50		5.7	05.7
-----	--	-----	------

2		5.6	05.8
---	--	-----	------

+15		5.4	06.0
-----	--	-----	------

+18		5.4	06.0
-----	--	-----	------

+20		5.3	06.1
-----	--	-----	------

+30 $\pm$ 1/200		5.3	06.1
-----------------	--	-----	------

+40		5.3	06.1
-----	--	-----	------

+42		5.3	06.1
-----	--	-----	------

41.

E

RT.

Spike G.P. 50' Lt. Sta. 1+25 (Labore Rd.)

Top Bolt Spike Sta. 7+50

Top Spike G.P. 25' Lt. 2+09

$\frac{6.5}{50}$	$\frac{6.5}{37}$		$\frac{5.6}{32}$	$\frac{5.3}{50}$
------------------	------------------	--	------------------	------------------

$\frac{6.4}{50}$	$\frac{6.1}{26}$	$\frac{6.0}{30}$	$\frac{5.7}{30}$	$\frac{5.3}{50}$
------------------	------------------	------------------	------------------	------------------

$\frac{6.1}{50}$	$\frac{6.1}{30}$	$\frac{5.8}{22}$	$\frac{5.4}{22}$	$\frac{5.2}{50}$
------------------	------------------	------------------	------------------	------------------

$\frac{5.7}{50}$	$\frac{5.7}{25}$	$\frac{5.5}{19}$	$\frac{5.7}{23}$	$\frac{5.3}{24}$	$\frac{5.0}{33}$	$\frac{3.5}{50}$
------------------	------------------	------------------	------------------	------------------	------------------	------------------

$\frac{5.7}{50}$	$\frac{5.5}{31}$	$\frac{5.2}{21}$	$\frac{5.8}{22}$	$\frac{5.3}{23}$	$\frac{5.0}{33}$	$\frac{4.7}{50}$
------------------	------------------	------------------	------------------	------------------	------------------	------------------

$\frac{5.6}{50}$	$\frac{5.4}{30}$	$\frac{5.4}{21}$	$\frac{5.5}{23}$	$\frac{5.2}{21}$	$\frac{4.7}{50}$
------------------	------------------	------------------	------------------	------------------	------------------

$\frac{5.6}{50}$	$\frac{5.4}{30}$	$\frac{5.4}{21}$	$\frac{5.6}{23}$	$\frac{5.7}{22}$	$\frac{5.3}{50}$
------------------	------------------	------------------	------------------	------------------	------------------

$\frac{5.5}{50}$	$\frac{5.4}{28}$	$\frac{5.3}{23}$	$\frac{5.2}{22}$	$\frac{4.8}{50}$
------------------	------------------	------------------	------------------	------------------

$\frac{5.5}{50}$	$\frac{5.4}{29}$	$\frac{5.6}{12}$	$\frac{5.3}{25}$	$\frac{4.4}{50}$	$\frac{3.9}{75}$	$\frac{3.4}{100}$
------------------	------------------	------------------	------------------	------------------	------------------	-------------------

$\frac{5.5}{50}$	$\frac{5.5}{32}$	$\frac{5.6}{11}$	$\frac{6.0}{10.9}$	$\frac{5.4}{8}$	$\frac{5.1}{14}$	$\frac{4.7}{46}$	$\frac{4.7}{50}$
------------------	------------------	------------------	--------------------	-----------------	------------------	------------------	------------------

$\frac{5.5}{50}$	$\frac{5.5}{34}$	$\frac{5.6}{11}$	$\frac{6.0}{10.9}$	$\frac{5.4}{8}$	$\frac{5.2}{27}$	$\frac{5.5}{35}$	$\frac{5.2}{46}$	$\frac{5.2}{50}$
------------------	------------------	------------------	--------------------	-----------------	------------------	------------------	------------------	------------------

Sta.	+	∇ 911.44	-	Elev.
2 + 46			5.3	06.1
+54			5.3	06.1
3			5.0	06.4
+50			4.6	06.8
4			4.4	07.0
+50			4.0	07.4
5			4.0	07.4
T.P.	3.24	91230	2.38	909.06
+50			5.1	07.2
+62			5.3	07.0
+64			5.3	07.0
+66			5.3	07.0
+76	E Vander Bie		5.3	07.0

L1

E

R1

$$\begin{array}{cccccccccccc} \underline{5.4} & \underline{5.5} & \underline{5.6} & \underline{6.2} & \underline{5.5} & & \underline{5.3} & \underline{5.8} & \underline{5.0} & \underline{4.7} & \underline{4.6} \\ 50 & 32 & 18 & 9.8 & 5 & 5.3 & 24 & 30 & 32 & 46 & 50 \end{array}$$

$$\begin{array}{cccccccccccc} \underline{5.4} & \underline{5.4} & \underline{5.5} & \underline{6.2} & \underline{5.5} & & \underline{5.3} & \underline{5.9} & \underline{5.3} & \underline{4.6} \\ 50 & 33 & 10 & 9.8 & 5 & 5.3 & 15 & 22 & 23 & 50 \end{array}$$

$$\begin{array}{cccccccccccc} \underline{5.5} & \underline{5.3} & \underline{5.2} & \underline{5.9} & \underline{5.2} & & \underline{5.0} & \underline{5.8} & \underline{4.7} & \underline{4.3} & \underline{4.2} \\ 50 & 33 & 12 & 11-10 & 8 & 5.0 & 10 & 13-14 & 15 & 33 & 50 \end{array}$$

$$\begin{array}{cccccccccccc} \underline{5.5} & \underline{5.3} & \underline{5.1} & \underline{5.9} & \underline{5.1} & & \underline{4.8} & \underline{5.6} & \underline{4.7} & \underline{4.2} & \underline{4.0} \\ 50 & 33 & 12 & 11-10 & 8 & 4.6 & 10 & 12-14 & 15 & 34 & 50 \end{array}$$

$$\begin{array}{cccccccccccc} \underline{5.2} & \underline{4.9} & \underline{4.9} & \underline{5.6} & \underline{4.8} & & \underline{4.6} & \underline{5.2} & \underline{4.3} & \underline{3.8} & \underline{3.8} \\ 50 & 33 & 12 & 11 & 9 & 4.4 & 9 & 13-14 & 15 & 32 & 50 \end{array}$$

$$\begin{array}{cccccccccccc} \underline{4.8} & \underline{4.5} & \underline{4.3} & \underline{5.1} & \underline{4.3} & & \underline{4.3} & \underline{5.0} & \underline{4.2} & \underline{3.9} & \underline{3.6} \\ 50 & 35 & 13 & 12-11 & 8 & 4.0 & 9 & 13-14 & 15 & 28 & 50 \end{array}$$

$$\begin{array}{cccccccccccc} \underline{4.9} & \underline{4.8} & \underline{4.4} & \underline{5.2} & \underline{4.4} & & \underline{4.2} & \underline{4.8} & \underline{4.0} & \underline{3.6} & \underline{3.0} \\ 50 & 35 & 15 & 13-12 & 9 & 4.0 & 9 & 12-13 & 14 & 30 & 50 \end{array}$$

$$\begin{array}{cccccccccccc} \underline{5.9} & \underline{5.7} & \underline{5.4} & \underline{6.1} & \underline{5.3} & & \underline{5.2} & \underline{5.8} & \underline{5.0} & \underline{4.3} & \underline{3.8} \\ 50 & 33 & 16 & 14-13 & 10 & 5.1 & 10 & 11-12 & 13 & 32 & 50 \end{array}$$

$$\begin{array}{cccccccccccc} \underline{6.3} & \underline{6.1} & \underline{5.9} & \underline{6.2} & \underline{5.6} & & \underline{5.6} & \underline{5.8} & \underline{5.3} & \underline{4.8} & \underline{4.4} \\ 50 & 35 & 17 & 16-14 & 12 & 5.3 & 9 & 11-12 & 13 & 30 & 50 \end{array}$$

$$\begin{array}{cccccccccccc} \underline{7.9} & \underline{6.5} & \underline{5.6} & & & & \underline{5.4} & \underline{5.8} & \underline{5.3} & \underline{4.8} & \underline{4.4} \\ 50 & 18 & 11 & & & 5.3 & 9 & 11-12 & 13 & 33 & 50 \end{array}$$

$$\begin{array}{cccccccccccc} \underline{6.4} & & \underline{6.0} & & & & \underline{5.3} & \underline{5.6} & \underline{5.2} & \underline{4.7} & \underline{4.3} \\ 50 & & 22 & & & 5.3 & 9 & 11-12 & 13 & 30 & 50 \end{array}$$

$$\begin{array}{cccccccccccc} \underline{6.5} & \underline{6.4} & \underline{6.3} & \underline{6.2} & \underline{6.1} & \underline{5.7} & & \underline{5.2} & \underline{5.4} & \underline{5.1} & \underline{4.7} & \underline{4.3} \\ 200 & 150 & 100 & 75 & 50 & 25 & 5.3 & 9 & 11-12 & 13 & 30 & 50 \end{array}$$

Sta.	+	π	-	Elev.
		91230		
5 + 87			5.4	<u>06.9</u>
+ 89			5.3	07.0
+ 91			5.3	07.0
6			5.4	06.9
+ 50			5.2	07.1
7			3.9	08.4
+ 35			3.3	09.0
+ 50			3.4	08.9
8			5.7	06.6
T.P.	2.99	907.50	7.79	904.51
+ 50			4.8	02.7
9			8.7	98.8
+ 50			11.4	96.1
	5.75	903.90	9.35	898.15

Lt.

F

Rt.

6.4	6.3	5.6		5.2	5.4	5.1	4.9	4.0
50	35	14	5.4	10	11-12	13	31	50

7.1	7.0	6.4	5.6		5.2	5.4	4.8	4.0
50	31	25	13	5.3	10	11-12	31	50

6.5	6.3	6.8	6.3	5.6		5.1	5.0	4.7	3.9
50	31	30	24	11	5.3	10	12	21	50

6.3	6.3	5.8	6.6	6.1	5.6		5.0	4.5	4.6	3.9
50	33	19	18	15	8	5.4	9	11	31	50

6.5	6.3	6.0	5.3		5.7	5.2	4.5	3.6
50	35	13	9	5.2	13	16	32	50

5.9	5.4	4.7	5.0	4.3		4.3	4.6	4.1	3.6	3.2
50	36	17	12	8	3.9	10	15	16	34	50

5.3	4.6	3.9	4.3	3.5		3.7	4.0	3.4	3.1	3.1
50	38	17	16	8	3.3	11	13	16	34	50

4.9	4.5	4.1	4.4	3.7		3.8	4.1	3.5	3.7
50	42	17	16	9	3.4	9	15	16	50

7.9	7.3	6.4	7.1	6.2		6.0	6.4	5.4	5.1	4.9
50	32	18	17	12	5.7	11	15	16	35	50

7.4	5.6	6.4	5.2		4.9	5.0	3.5	2.3	0.7
50	18	17	9	4.8	12	16	17	34	50

11.1	10.6	10.1	10.5	9.2		8.5	8.7	7.8	6.3	4.5
50	36	18	17	11	8.7	12	16	17	35	50

13.6	13.4	12.8	1.8		11.4	12.0	10.5	9.2
50	28	14	12	11.4	11	16	36	50

Sta.	+	⌒	-	Elev
		903 90.		
9+85			8.4	95.5
10+02	Sec. thru 18" C.M.		8.1	95.8
+20			7.4	96.5
+67			5.5	98.4
11			4.6	99.3
+50			4.7	99.2
+75			5.1	98.8
12			5.3	98.6
+43			5.4	98.5
+54	Sec. thru 15" C.M.		5.7	98.2
+66			6.1	97.8
+66	Edge Pavement		6.23	97.67

Lt. E Rt.

$\frac{10.8}{50} \frac{11.0}{33} \frac{10.7}{16} \frac{8.5}{12} \frac{8.4}{8.4} \frac{8.8}{11} \frac{10.5}{21} \frac{10.0}{50}$

FL 92.48
 $\frac{11.0}{50} \frac{11.2}{36} \frac{11.4}{19} \frac{11.4}{19} \frac{8.4}{128.1} \frac{8.5}{13} \frac{11.95}{21} \frac{11.1}{20} \frac{11.1}{34} \frac{11.0}{50}$
FL 91.95

$\frac{9.9}{50} \frac{10.3}{38} \frac{10.4}{18} \frac{7.5}{12} \frac{7.4}{7.4} \frac{7.9}{12} \frac{11.1}{20} \frac{12.0}{32} \frac{12.6}{50}$

$\frac{7.4}{50} \frac{7.0}{34} \frac{6.5}{15} \frac{5.8}{14} \frac{5.5}{5.5} \frac{5.9}{13} \frac{6.8}{16} \frac{8.0}{37} \frac{8.5}{50}$

$\frac{6.0}{50} \frac{4.4}{23} \frac{5.8}{20} \frac{5.0}{16} \frac{5.0}{12} \frac{4.6}{4.6} \frac{4.9}{11} \frac{5.9}{16} \frac{5.6}{20} \frac{5.3}{47} \frac{2.3}{49} \frac{2.3}{50}$

$\frac{6.5}{50} \frac{6.2}{38} \frac{5.5}{21} \frac{6.0}{19} \frac{5.1}{12} \frac{4.7}{4.7} \frac{4.9}{11} \frac{5.5}{14} \frac{4.5}{31} \frac{4.3}{41} \frac{+0.4}{43} \frac{+1.7}{50}$

$\frac{7.1}{50} \frac{6.7}{31} \frac{6.0}{13} \frac{5.3}{11} \frac{5.1}{5.1} \frac{5.4}{12} \frac{5.9}{14} \frac{5.3}{28} \frac{5.1}{36} \frac{1.1}{38} \frac{+1.9}{50}$

$\frac{6.5}{50} \frac{6.7}{31} \frac{6.3}{14} \frac{5.6}{11} \frac{5.3}{5.3} \frac{5.5}{11} \frac{6.1}{14} \frac{5.3}{34} \frac{3.2}{35} \frac{1.5}{50}$

$\frac{4.2}{50} \frac{4.8}{34} \frac{5.4}{15} \frac{5.4}{5.4} \frac{5.8}{13} \frac{6.4}{15} \frac{5.7}{27} \frac{3.1}{30} \frac{1.9}{50}$

FL 90.42
 $\frac{6.6}{50} \frac{7.0}{37} \frac{7.48}{28} \frac{7.5}{28} \frac{5.3}{20} \frac{6.0}{5.7} \frac{6.6}{9} \frac{6.6}{10} \frac{8.70}{19} \frac{8.4}{19} \frac{9.1}{37} \frac{9.5}{50}$
FL 95.20

$\frac{4.7}{50} \frac{5.3}{28} \frac{5.7}{10} \frac{6.1}{6.1} \frac{6.9}{23} \frac{7.4}{7.1} \frac{7.6}{50}$

$\frac{4.72}{50} \frac{5.34}{28} \frac{6.23}{6.23} \frac{7.01}{28} \frac{7.63}{50}$

Sta. + X - Elev

903.90

12 + 75.94 ± Edgerton

6.20

97.70

B.M.

6.94

896.96

896.96

$$\frac{468}{50}$$

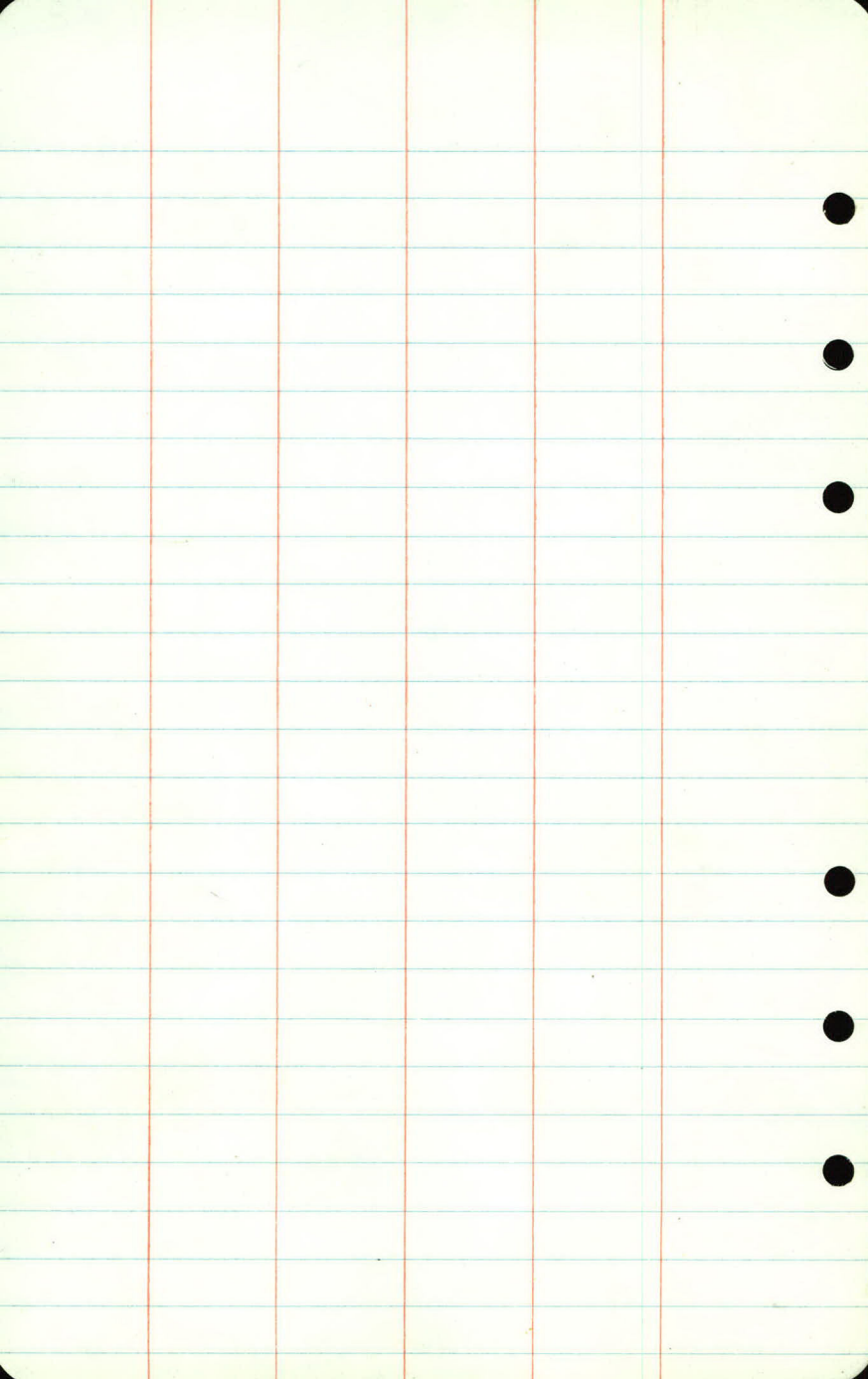
$$\frac{5.21}{32}$$

$$6.20$$

$$\frac{6.84}{22}$$

$$\frac{7.60}{50}$$

Spike G.P. 50' Lt. 1+25 (Libore Rd) = G.P. 39' Rt. 12+53 (Libore Av.)



LABORE AVE

Additional Levels

Profile Rt. and Lt. on

sta	i	π	-	Elev.
B.M.	2.77	910.58		907.81
0-30			4.5	906.1
T.P.	11.49	921.89	0.18	910.40

Cross Sections going south on

B.M.	8.94	916.75		907.81
0+00			10.6	

+18			10.5	
-----	--	--	------	--

+50			9.8	
-----	--	--	-----	--

1			8.8	
---	--	--	-----	--

+50			7.9	
-----	--	--	-----	--

2			6.8	
---	--	--	-----	--

+50			5.6	
-----	--	--	-----	--

3			5.1	
---	--	--	-----	--

+50			4.8	
-----	--	--	-----	--

4			4.5	
---	--	--	-----	--

Desota St.

Spk. in G.P. 25' Lt. sta 2109

$\frac{6.8}{400}$ $\frac{6.6}{350}$ $\frac{6.3}{300}$ $\frac{6.1}{250}$ $\frac{5.8}{200}$ $\frac{6.6}{150}$ $\frac{6.1}{100}$ $\frac{5.0}{50}$ $\frac{3.2}{45}$ $\frac{2.2}{50}$ $\frac{1.2}{150}$ $\frac{0.3}{200}$

$\frac{9.7}{250}$ $\frac{8.9}{300}$ $\frac{8.3}{350}$ $\frac{7.9}{400}$

Noel st. - sta. 2+2999 Labore = 0 100

$\frac{10.6}{50}$ $\frac{10.6}{33}$ $\frac{10.6}{19}$ $\frac{10.8}{106}$ $\frac{11.0}{14}$ $\frac{11.0}{35}$ $\frac{11.0}{50}$

$\frac{10.3}{50}$ $\frac{10.6}{29}$ $\frac{11.2}{26-23}$ $\frac{10.8}{22}$ $\frac{10.3}{9}$ $\frac{10.6}{10.5}$ $\frac{11.1}{9}$ $\frac{10.6}{10-12}$ $\frac{10.8}{13}$ $\frac{10.8}{32}$ $\frac{10.8}{50}$

$\frac{9.8}{50}$ $\frac{9.9}{34}$ $\frac{10.0}{16}$ $\frac{10.5}{14-12}$ $\frac{10.2}{10}$ $\frac{9.9}{9.8}$ $\frac{10.5}{8}$ $\frac{10.1}{11-13}$ $\frac{10.0}{16}$ $\frac{9.6}{35}$ $\frac{9.6}{50}$

$\frac{9.0}{50}$ $\frac{9.2}{31}$ $\frac{9.1}{16}$ $\frac{9.8}{14-12}$ $\frac{9.2}{9}$ $\frac{9.2}{8.8}$ $\frac{9.8}{10}$ $\frac{9.3}{11-13}$ $\frac{9.2}{15}$ $\frac{8.9}{35}$ $\frac{8.9}{50}$

$\frac{8.5}{50}$ $\frac{8.4}{32}$ $\frac{8.2}{15}$ $\frac{8.8}{13-11}$ $\frac{8.3}{10}$ $\frac{8.3}{7.9}$ $\frac{9.1}{9}$ $\frac{8.4}{11-13}$ $\frac{8.7}{16}$ $\frac{7.9}{31}$ $\frac{7.6}{34}$ $\frac{7.6}{50}$

$\frac{7.3}{50}$ $\frac{7.1}{33}$ $\frac{7.1}{15}$ $\frac{7.9}{12-10}$ $\frac{7.2}{9}$ $\frac{7.5}{6.8}$ $\frac{8.1}{9}$ $\frac{7.6}{12-14}$ $\frac{7.6}{16}$ $\frac{7.1}{31}$ $\frac{7.2}{34}$ $\frac{7.2}{50}$

Cross Sections going North on

B.M.	4.46	912.27 ✓	907.81
0+00		5.3	07.0
+15		5.6	06.7
+50		6.0	06.3
1		6.3	06.0
+50		6.2	06.1
2		6.4	05.9
+50		6.3	06.0
3		6.2	06.1
+50		6.2	06.1
4		6.4	05.9
+50		6.4	05.9
5		6.3	06.0

Vanderbilt St. Sta, 5+76.13 Labore = 0+00

$\frac{5.0}{50}$ $\frac{5.1}{23}$ 5.3 $\frac{5.5}{26}$ $\frac{5.6}{50}$

$\frac{5.3}{50}$ $\frac{5.1}{33}$ $\frac{5.9}{20}$ $\frac{6.1}{16}$ $\frac{5.7}{9}$ 5.6 $\frac{5.7}{12}$ $\frac{6.4}{24}$ $\frac{6.1}{30}$ $\frac{6.2}{50}$

$\frac{5.8}{50}$ $\frac{5.8}{29}$ $\frac{6.3}{15}$ $\frac{7.0}{13}$ $\frac{6.2}{11}$ 6.0 $\frac{6.4}{11}$ $\frac{6.9}{13-14}$ $\frac{6.4}{15}$ $\frac{6.4}{32}$ $\frac{7.0}{50}$

$\frac{6.2}{50}$ $\frac{6.0}{32}$ $\frac{6.5}{15}$ $\frac{7.1}{14}$ $\frac{6.8}{12}$ $\frac{6.4}{8}$ 6.3 $\frac{6.5}{11}$ $\frac{7.3}{13-14}$ $\frac{6.7}{15}$ $\frac{6.7}{32}$ $\frac{7.0}{50}$

$\frac{6.5}{50}$ $\frac{6.2}{33}$ $\frac{6.8}{14}$ $\frac{7.4}{12}$ $\frac{6.9}{11}$ $\frac{6.5}{8}$ 6.2 $\frac{6.6}{11}$ $\frac{7.4}{13-15}$ $\frac{6.7}{16}$ $\frac{6.6}{32}$ $\frac{7.0}{50}$

$\frac{7.0}{50}$ $\frac{6.6}{31}$ $\frac{6.9}{15}$ $\frac{7.5}{14}$ $\frac{6.9}{12}$ 6.4 $\frac{6.6}{11}$ $\frac{7.5}{14-16}$ $\frac{7.0}{17}$ $\frac{6.9}{38}$ $\frac{7.3}{50}$

$\frac{6.9}{50}$ $\frac{6.3}{34}$ $\frac{6.9}{16}$ $\frac{7.3}{14}$ $\frac{6.9}{12}$ 6.3 $\frac{6.6}{11}$ $\frac{7.6}{13-15}$ $\frac{6.8}{17}$ $\frac{6.6}{32}$ $\frac{6.7}{50}$

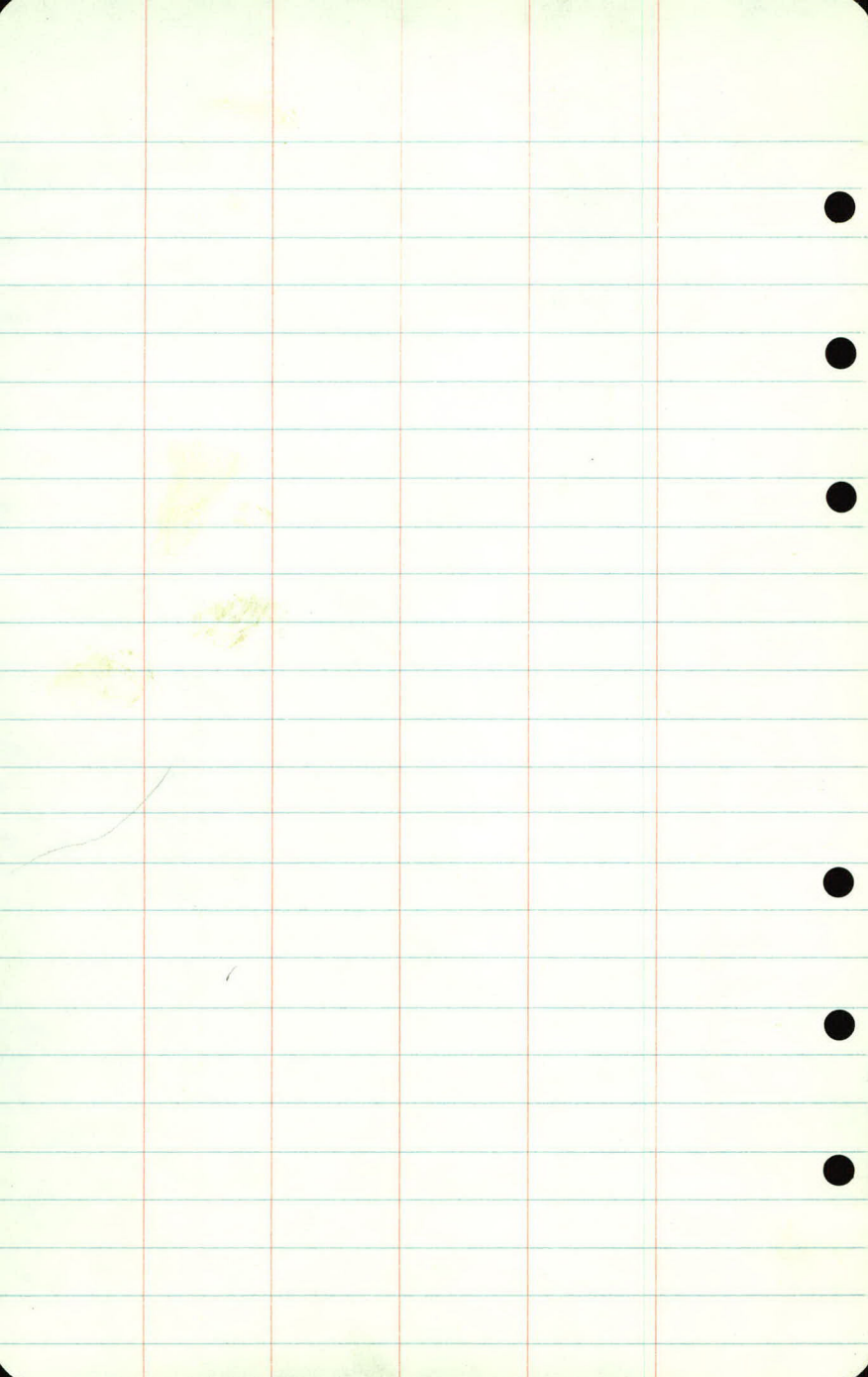
$\frac{6.9}{50}$ $\frac{6.5}{34}$ $\frac{6.7}{16}$ $\frac{7.3}{14}$ $\frac{6.8}{13}$ $\frac{6.4}{8}$ 6.2 $\frac{6.4}{10}$ $\frac{7.4}{12-14}$ $\frac{6.6}{16}$ $\frac{6.4}{32}$ $\frac{6.7}{50}$

$\frac{6.8}{50}$ $\frac{6.8}{32}$ $\frac{6.8}{16}$ $\frac{7.5}{14}$ $\frac{6.7}{13}$ 6.2 $\frac{6.5}{10}$ $\frac{7.1}{12-14}$ $\frac{6.4}{15}$ $\frac{6.1}{35}$ $\frac{6.3}{50}$

$\frac{7.1}{50}$ $\frac{6.8}{30}$ $\frac{6.9}{17}$ $\frac{7.5}{15}$ $\frac{7.1}{13}$ $\frac{6.6}{8}$ 6.4 $\frac{6.6}{10}$ $\frac{7.4}{11-13}$ $\frac{6.4}{15}$ $\frac{6.1}{29}$ $\frac{6.3}{50}$

$\frac{7.1}{50}$ $\frac{6.7}{31}$ $\frac{7.1}{17}$ $\frac{7.7}{16}$ $\frac{7.1}{13}$ 6.4 $\frac{6.6}{9}$ $\frac{7.4}{12-13}$ $\frac{6.8}{14}$ $\frac{6.4}{33}$ $\frac{6.2}{50}$

$\frac{7.9}{50}$ $\frac{6.6}{30}$ $\frac{7.1}{17}$ $\frac{7.5}{16}$ $\frac{6.8}{14}$ 6.3 $\frac{6.6}{8}$ $\frac{7.5}{11-13}$ $\frac{6.7}{14}$ $\frac{6.4}{30}$ $\frac{6.4}{50}$



Labore Ave

Slope Stakes

ReStaked New Section

9/26/41

Naw

AM

CIV-

LL

Sta	+	Δ	-	Elev
B.M.	2.71	91052		907.81

0 + 00				05.3
--------	--	--	--	------

+ 50				05.3
------	--	--	--	------

1				05.2
---	--	--	--	------

+ 50				05.2
------	--	--	--	------

2				05.1
---	--	--	--	------

+ 50				05.1
------	--	--	--	------

3				05.0
---	--	--	--	------

+ 50				05.0
------	--	--	--	------

4				04.9
---	--	--	--	------

+ 50				04.9
------	--	--	--	------

5				04.8
---	--	--	--	------

Lt

Z

Rt

Spk in CP 25' Rt. Sta 2109

$$\begin{array}{rcl}
 5.2 & 67 & \begin{array}{r} 5.5 \\ C0.1 \\ \hline 21.4 \end{array} \\
 & & \begin{array}{r} 5.4 \\ F0.2 \end{array} \\
 & & \begin{array}{r} 48 \\ C0.4 \\ \hline 228 \end{array}
 \end{array}$$

$$\begin{array}{rcl}
 5.2 & 67 & \begin{array}{r} 5.1 \\ C0.1 \\ \hline 22.2 \end{array} \\
 & & \begin{array}{r} 5.9 \\ F0.7 \end{array} \\
 & & \begin{array}{r} 50 \\ C0.2 \\ \hline 224 \end{array}
 \end{array}$$

$$\begin{array}{rcl}
 5.3 & 68 & \begin{array}{r} 5.0 \\ C0.3 \\ \hline 22.6 \end{array} \\
 & & \begin{array}{r} 5.6 \\ F0.3 \end{array} \\
 & & \begin{array}{r} 44 \\ C0.9 \\ \hline 238 \end{array}
 \end{array}$$

$$\begin{array}{rcl}
 5.3 & 68 & \begin{array}{r} 4.7 \\ C0.6 \\ \hline 23.2 \end{array} \\
 & & \begin{array}{r} 5.5 \\ F0.2 \end{array} \\
 & & \begin{array}{r} 43 \\ C1.2 \\ \hline 240 \end{array}
 \end{array}$$

$$\begin{array}{rcl}
 5.4 & 69 & \begin{array}{r} 4.6 \\ C0.8 \\ \hline 23.6 \end{array} \\
 & & \begin{array}{r} 5.6 \\ F0.2 \end{array} \\
 & & \begin{array}{r} 43 \\ C1.0 \\ \hline 242 \end{array}
 \end{array}$$

$$\begin{array}{rcl}
 5.4 & 69 & \begin{array}{r} 4.6 \\ C0.8 \\ \hline 23.6 \end{array} \\
 & & \begin{array}{r} 5.7 \\ F0.3 \end{array} \\
 & & \begin{array}{r} 46 \\ C0.8 \\ \hline 236 \end{array}
 \end{array}$$

$$\begin{array}{rcl}
 5.5 & 70 & \begin{array}{r} 4.3 \\ C1.2 \\ \hline 24.4 \end{array} \\
 & & \begin{array}{r} 5.5 \\ C0.0 \end{array} \\
 & & \begin{array}{r} 34 \\ C2.1 \\ \hline 26.2 \end{array}
 \end{array}$$

$$\begin{array}{rcl}
 5.5 & 70 & \begin{array}{r} 4.3 \\ C1.2 \\ \hline 24.4 \end{array} \\
 & & \begin{array}{r} 5.1 \\ C0.4 \end{array} \\
 & & \begin{array}{r} 35 \\ C2.0 \\ \hline 26.0 \end{array}
 \end{array}$$

$$\begin{array}{rcl}
 5.6 & 71 & \begin{array}{r} 4.0 \\ C1.6 \\ \hline 25.2 \end{array} \\
 & & \begin{array}{r} 5.2 \\ C0.4 \end{array} \\
 & & \begin{array}{r} 30 \\ C2.6 \\ \hline 27.2 \end{array}
 \end{array}$$

$$\begin{array}{rcl}
 5.6 & 71 & \begin{array}{r} 3.4 \\ C2.2 \\ \hline 26.4 \end{array} \\
 & & \begin{array}{r} 4.6 \\ C1.0 \end{array} \\
 & & \begin{array}{r} 29 \\ C2.7 \\ \hline 27.4 \end{array}
 \end{array}$$

$$\begin{array}{rcl}
 5.7 & 72 & \begin{array}{r} 3.7 \\ C2.0 \\ \hline 26.0 \end{array} \\
 & & \begin{array}{r} 4.3 \\ C1.4 \end{array} \\
 & & \begin{array}{r} 27 \\ C3.0 \\ \hline 28.0 \end{array}
 \end{array}$$

Sta	+	π	-	Elev
		910.52		
5+50				04.8
T.P.	4.87	911.92	3.47	907.05
6				04.7
+50				04.7
7				04.5
+35				04.3
+50				04.1
8				03.5
+50				02.7
9				01.8
T.P.	2.93	903.92	10.93	00.99
+50				00.9
T.P.			10.93	
+85				00.4
1				
10+02				00.1

LT

Z

RT

$$5.7 \quad 7.2 \quad \begin{array}{r} 4.0 \\ C1.7 \\ \hline 25.4 \end{array} \quad \begin{array}{r} 4.7 \\ C1.0 \end{array} \quad \begin{array}{r} 3.0 \\ C2.7 \\ \hline 27.4 \end{array}$$

$$7.2 \quad 8.7 \quad \begin{array}{r} 5.5 \\ C1.7 \\ \hline 25.4 \end{array} \quad \begin{array}{r} 6.1 \\ C1.1 \end{array} \quad \begin{array}{r} 4.4 \\ C2.8 \\ \hline 27.6 \end{array}$$

$$7.2 \quad 8.7 \quad \begin{array}{r} 5.6 \\ C1.6 \\ \hline 25.2 \end{array} \quad \begin{array}{r} 6.0 \\ 0.2 \end{array} \quad \begin{array}{r} 4.1 \\ C3.1 \\ \hline 28.2 \end{array}$$

$$7.4 \quad 8.9 \quad \begin{array}{r} 4.6 \\ C2.8 \\ \hline 27.6 \end{array} \quad \begin{array}{r} 5.6 \\ C1.8 \end{array} \quad \begin{array}{r} 3.3 \\ C4.1 \\ \hline 30.2 \end{array}$$

$$7.6 \quad \begin{array}{r} 3.9 \\ C3.7 \\ \hline 29.4 \end{array} \quad \begin{array}{r} 4.6 \\ C3.0 \end{array} \quad \begin{array}{r} 2.7 \\ C4.9 \\ \hline 31.8 \end{array}$$

$$7.8 \quad \begin{array}{r} 3.9 \\ C3.9 \\ \hline 29.8 \end{array} \quad \begin{array}{r} 4.5 \\ C3.3 \end{array} \quad \begin{array}{r} 3.2 \\ C4.6 \\ \hline 31.2 \end{array}$$

$$8.4 \quad \begin{array}{r} 6.6 \\ C1.8 \\ \hline 25.6 \end{array} \quad \begin{array}{r} 5.4 \\ C3.0 \end{array} \quad \begin{array}{r} 4.8 \\ C3.5 \\ \hline 29.2 \end{array}$$

$$9.2 \quad 10.7 \quad \begin{array}{r} 10.5 \\ R0.2 \\ \hline 19.4 \end{array} \quad \begin{array}{r} 9.2 \\ C0.0 \end{array} \quad \begin{array}{r} 7.2 \\ C2.0 \\ \hline 26.0 \end{array}$$

$$10.1 \quad 11.6 \quad \begin{array}{r} 14.8 \\ F4.7 \\ \hline 22.4 \end{array} \quad \begin{array}{r} 10.8 \\ F0.7 \end{array} \quad \begin{array}{r} 12.1 \\ F2.0 \\ \hline 17.0 \end{array}$$

$$3.0 \quad \begin{array}{r} 9.7 \\ F6.7 \\ \hline 26.4 \end{array} \quad \begin{array}{r} 3.4 \\ F0.4 \end{array} \quad \begin{array}{r} 8.0 \\ F5.0 \\ \hline 23.0 \end{array}$$

$$3.5 \quad \begin{array}{r} 11.1 \\ F7.6 \\ \hline 28.2 \end{array} \quad \begin{array}{r} 4.0 \\ F0.5 \end{array} \quad \begin{array}{r} 10.3 \\ F6.8 \\ \hline 26.6 \end{array}$$

$$3.8 \quad \begin{array}{r} 11.1 \\ F7.3 \\ \hline 27.6 \end{array} \quad \begin{array}{r} 4.3 \\ F0.5 \end{array} \quad \begin{array}{r} 11.5 \\ F7.7 \\ \hline 28.4 \end{array}$$

Sta	+	T	-	Elev
-----	---	---	---	------

		903.92		
--	--	--------	--	--

10420				
-------	--	--	--	--

				99.9
--	--	--	--	------

+67				
-----	--	--	--	--

				99.3
--	--	--	--	------

11				
----	--	--	--	--

				99.0
--	--	--	--	------

+50				
-----	--	--	--	--

				98.6
--	--	--	--	------

+75				
-----	--	--	--	--

				98.3
--	--	--	--	------

12				
----	--	--	--	--

				98.1
--	--	--	--	------

+43				
-----	--	--	--	--

				97.7
--	--	--	--	------

		6.96		896.96 ✓
--	--	------	--	----------

Lt

Σ

Rt

4.0

$$\begin{array}{r} 103 \\ F63 \\ \hline 25.6 \end{array}$$

$$\begin{array}{r} 4.6 \\ F0.6 \end{array}$$

$$\begin{array}{r} 11.6 \\ F7.4 \\ \hline 29.2 \end{array}$$

4.6

$$\begin{array}{r} 66 \\ F2.0 \\ \hline 17.0 \end{array}$$

$$\begin{array}{r} 5.2 \\ F0.6 \end{array}$$

$$\begin{array}{r} 6.8 \\ F2.2 \\ \hline 17.4 \end{array}$$

4.9 6.4

$$\begin{array}{r} 4.4 \\ C0.5 \\ \hline 23.0 \end{array}$$

$$\begin{array}{r} 4.6 \\ C0.3 \end{array}$$

$$\begin{array}{r} 5.7 \\ C0.7 \\ \hline 20.4 \end{array}$$

5.3 6.8

$$\begin{array}{r} 5.8 \\ D1.8 \\ \hline 21.0 \end{array}$$

$$\begin{array}{r} 4.7 \\ C0.6 \end{array}$$

5.6 7.1

$$\begin{array}{r} 6.4 \\ D0.2 \\ \hline 20.4 \end{array}$$

$$\begin{array}{r} 5.1 \\ C0.5 \end{array}$$

$$\begin{array}{r} 5.7 \\ D1.4 \\ \hline 21.8 \end{array}$$

5.8 7.3

$$\begin{array}{r} 6.4 \\ D0.9 \\ \hline 20.8 \end{array}$$

$$\begin{array}{r} 5.2 \\ C0.6 \end{array}$$

$$\begin{array}{r} 5.9 \\ D1.4 \\ \hline 21.8 \end{array}$$

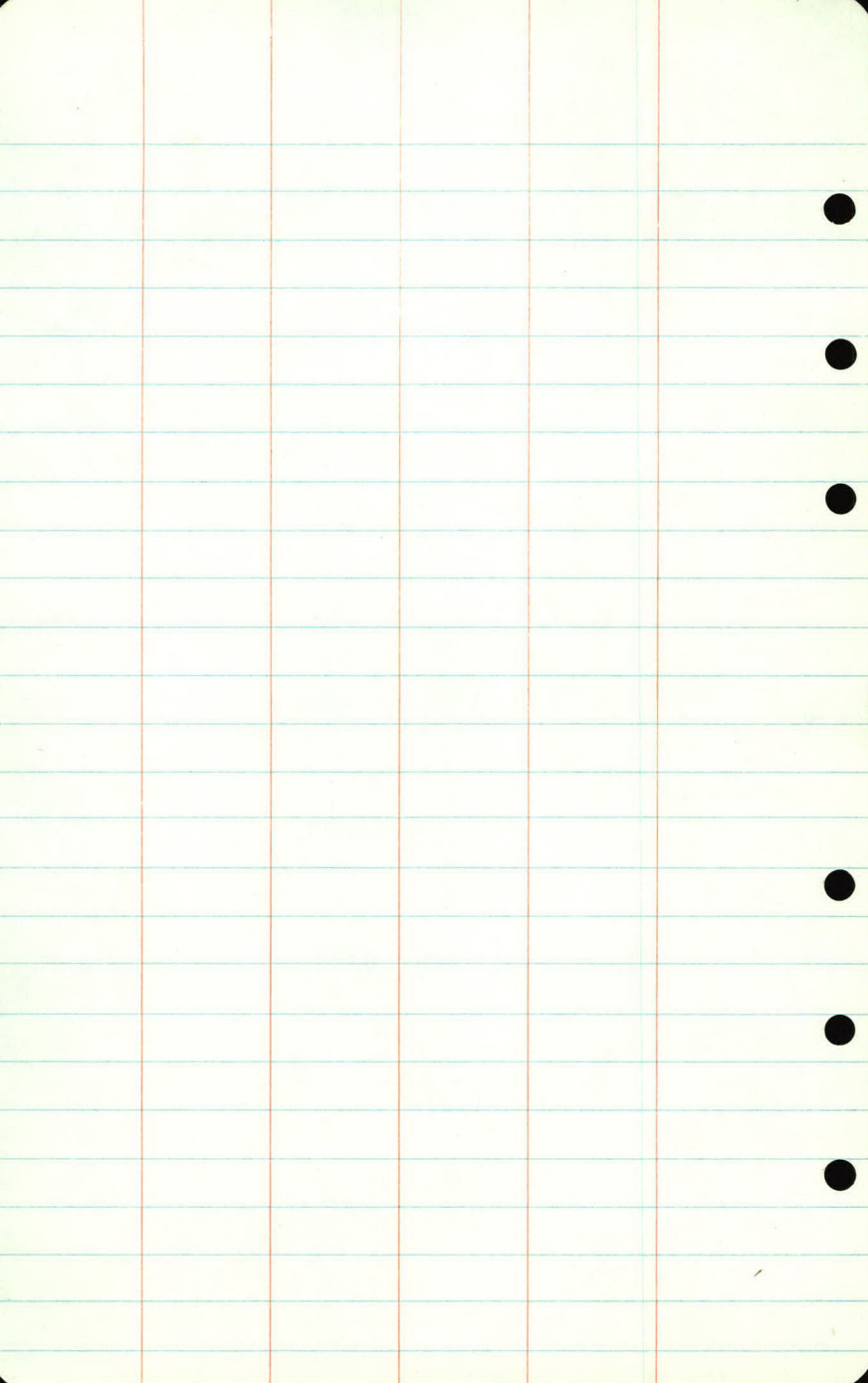
6.2 7.7

$$\begin{array}{r} 5.0 \\ C1.2 \\ \hline 24.4 \end{array}$$

$$\begin{array}{r} 5.5 \\ C0.7 \end{array}$$

$$\begin{array}{r} 6.0 \\ C0.2 \\ \hline 22.4 \end{array}$$

Spk G.P. 39' Rt Sta 12+53



Slope stakes

Vander Bie St.

Sta	+	π	-	Elev	Gr Rod.
B.M	4.19	912.00		907.81	

0+15				048	7.2-8.0
------	--	--	--	-----	---------

+50				05.0	7.0 7.8
-----	--	--	--	------	---------

1+00				05.3	6.7 7.5
------	--	--	--	------	---------

+50				05.6	6.4 7.2
-----	--	--	--	------	---------

2				05.9	6.1 6.9
---	--	--	--	------	---------

LT

~~X~~

RT

$$\begin{array}{r} 5.9 \\ DC1.9 \\ \hline 16.8 \end{array}$$

$$\begin{array}{r} 5.6 \\ C1.4 \end{array}$$

$$\begin{array}{r} 6.1 \\ DC1.7 \\ \hline 16.4 \end{array}$$

$$\begin{array}{r} 6.2 \\ DC1.3 \\ \hline 15.6 \end{array}$$

$$\begin{array}{r} 5.9 \\ C0.8 \end{array}$$

$$\begin{array}{r} 6.3 \\ DC1.2 \\ \hline 15.4 \end{array}$$

$$\begin{array}{r} 7.0 \\ DC0.2 \\ \hline 13.4 \end{array}$$

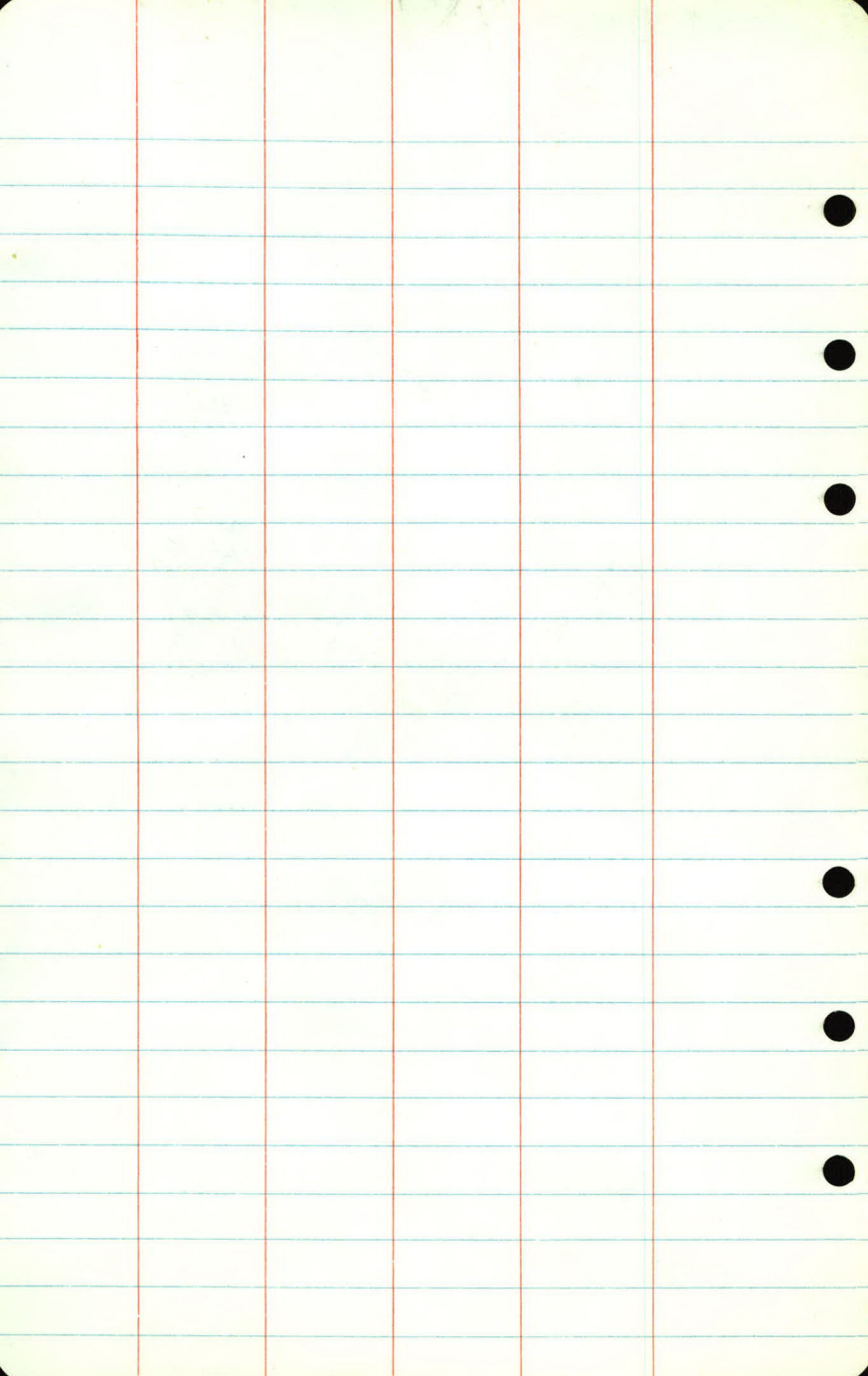
$$\begin{array}{r} 5.9 \\ C0.5 \end{array}$$

$$\begin{array}{r} 6.9 \\ DC0.3 \\ \hline 13.6 \end{array}$$

$$\begin{array}{r} 7.2 \\ F0.3 \\ \hline 13.6 \end{array}$$

$$\begin{array}{r} 6.1 \\ C0.0 \end{array}$$

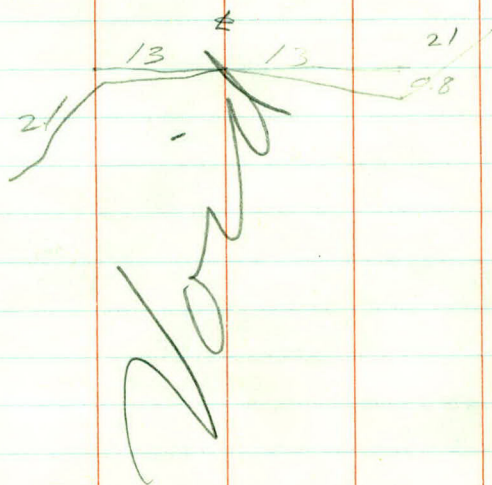
$$\begin{array}{r} 6.8 \\ DC0.1 \\ \hline 13.2 \end{array}$$



7-13-41

Slope Stakes

Labore Ave



Sta	+	Δ	-	Elev	Gr. Rod.
BM	3.63	911.44		907.81	
0+00				05.3	6.1 - 6.9
+50				05.3	6.1 - 6.9
1				05.2	6.2 - 7.0
+50				05.2	6.2 - 7.0
2				05.1	6.3 - 7.1
+15				05.1	6.3 - 7.1
+18				05.1	6.3 - 7.1
+28				05.1	
+30				05.1	6.3 - 7.1
+40				05.1	6.3 - 7.1

LT

£

RT

Spk. G.P. 25' RT Sta, 2+07

6.3
DC 0.7/4.4

6.1
C 0.0

5.9
DC 1.1/5.2

6.2
DC 0.7/4.4

6.1
C 0.0

5.9
DC 1.0/5.0

6.0
DC 1.0/5.0

5.8
C 0.4

5.5
DC 1.2/6.0

5.6
DC 1.4/6.8

5.7
C 0.5

5.4
DC 1.6/6.2

5.6
DC 1.5/6.0

5.5
C 0.8

5.5
DC 1.6/6.2

5.4
DC 1.7/6.4

5.7
C 0.6

5.3
DC 1.8/6.2

No Stakes

No Stakes

5.4
DC 1.7/6.4

5.3
C 1.0

No Stakes

No Stakes

Sta	+	π	-	Elev	Gh. Rod
		911.44			
2+42				05.1	
+46				05.1	
+54				05.0	6.4 - 7.2
3				05.0	6.4 - 7.2
T.P.	5.45	911.94	4.95	906.49	
+50				05.0	6.9 7.7
4				04.9	7.8 7.8
+50				04.9	7.0 7.8
5				04.8	7.1 7.9
+50				04.8	7.1 7.9
+62				04.7	7.2 8.0
+64				04.7	7.2 8.0
+89				04.7	

Lt

X

Rt

No Stake

No Stake

$$\begin{array}{r} 5.5 \\ DC 1.7 \\ \hline 16.4 \end{array}$$

$$\begin{array}{r} 5.3 \\ C 1.1 \\ \hline \end{array}$$

$$\begin{array}{r} 5.6 \\ DC 1.6 \\ \hline 16.2 \end{array}$$

$$\begin{array}{r} 5.1 \\ DC 2.1 \\ \hline 17.2 \end{array}$$

$$\begin{array}{r} 4.9 \\ C 1.5 \\ \hline \end{array}$$

$$\begin{array}{r} 4.6 \\ DC 2.6 \\ \hline 19.2 \end{array}$$

$$\begin{array}{r} 5.7 \\ DC 2.0 \\ \hline 17.0 \end{array}$$

$$\begin{array}{r} 5.3 \\ C 1.5 \\ \hline \end{array}$$

$$\begin{array}{r} 5.1 \\ DC 2.6 \\ \hline 18.2 \end{array}$$

$$\begin{array}{r} 5.4 \\ DC 2.4 \\ \hline 17.8 \end{array}$$

$$\begin{array}{r} 5.0 \\ C 2.0 \\ \hline \end{array}$$

$$\begin{array}{r} 4.7 \\ DC 3.1 \\ \hline 19.2 \end{array}$$

$$\begin{array}{r} 4.9 \\ DC 2.9 \\ \hline 18.8 \end{array}$$

$$\begin{array}{r} 4.5 \\ C 2.5 \\ \hline \end{array}$$

$$\begin{array}{r} 5.2 \\ DC 2.6 \\ \hline 18.2 \end{array}$$

$$\begin{array}{r} 5.0 \\ DC 2.9 \\ \hline 18.8 \end{array}$$

$$\begin{array}{r} 4.5 \\ C 2.6 \\ \hline \end{array}$$

$$\begin{array}{r} 4.5 \\ DC 3.4 \\ \hline 19.8 \end{array}$$

$$\begin{array}{r} 5.2 \\ DC 2.7 \\ \hline 18.4 \end{array}$$

$$\begin{array}{r} 4.7 \\ C 2.4 \\ \hline \end{array}$$

$$\begin{array}{r} 4.5 \\ DC 3.4 \\ \hline 19.8 \end{array}$$

$$\begin{array}{r} 5.9 \\ DC 2.1 \\ \hline 17.2 \end{array}$$

$$\begin{array}{r} 4.8 \\ C 2.4 \\ \hline \end{array}$$

$$\begin{array}{r} 4.8 \\ DC 3.2 \\ \hline 19.4 \end{array}$$

No Stake

No Stake

Sta	+	∇	-	Elev	Gr. Rod
		911.94			
5+91				04.7	7.2 8.0
6				04.7	7.2 8.0
+50				04.7	7.2 8.0
7				04.5	7.4 8.2
+35				04.3	7.6 8.4
+50				04.1	7.8 8.6
8				03.5	8.4 9.2
+50				02.7	9.2 10.0
T. P.	1.99	904.22	9.71	902.23	
9				01.8	2.4 3.2
+50				00.9	3.3 4.1
+85				00.4	3.8 4.6
10+02				00.1	4.1 4.9

Lt

X

Rt

No stake

$$\begin{array}{r} 4.9 \\ C2.3 \\ \hline \end{array}$$

$$\begin{array}{r} 4.7 \\ DC3.3 \\ \hline 19.6 \end{array}$$

$$\begin{array}{r} L.1 \\ DC1.9 \\ \hline 12.8 \end{array}$$

$$\begin{array}{r} 5.0 \\ C2.2 \\ \hline \end{array}$$

$$\begin{array}{r} 5.0 \\ DC3.0 \\ \hline 19.0 \end{array}$$

$$\begin{array}{r} 5.5 \\ DC2.5 \\ \hline 18.0 \end{array}$$

$$\begin{array}{r} 4.8 \\ C2.4 \\ \hline \end{array}$$

$$\begin{array}{r} 4.4 \\ DC3.6 \\ \hline 20.2 \end{array}$$

$$\begin{array}{r} 4.5 \\ DC3.2 \\ \hline 20.4 \end{array}$$

$$\begin{array}{r} 3.5 \\ C3.9 \\ \hline \end{array}$$

$$\begin{array}{r} 3.1 \\ DC4.6 \\ \hline 22.2 \end{array}$$

$$\begin{array}{r} 3.7 \\ DC4.7 \\ \hline 22.4 \end{array}$$

$$\begin{array}{r} 3.0 \\ C4.6 \\ \hline \end{array}$$

$$\begin{array}{r} 2.8 \\ DC5.6 \\ \hline 24.2 \end{array}$$

$$\begin{array}{r} 3.7 \\ DC4.9 \\ \hline 22.8 \end{array}$$

$$\begin{array}{r} 3.1 \\ C4.7 \\ \hline \end{array}$$

$$\begin{array}{r} 3.2 \\ DC5.4 \\ \hline 23.9 \end{array}$$

$$\begin{array}{r} L.1 \\ DC3.1 \\ \hline 19.2 \end{array}$$

$$\begin{array}{r} 5.4 \\ C3.0 \\ \hline \end{array}$$

$$\begin{array}{r} 5.1 \\ DC4.1 \\ \hline 21.2 \end{array}$$

$$\begin{array}{r} 10.4 \\ FO.4 \\ \hline 13.8 \end{array}$$

$$\begin{array}{r} 9.2 \\ C0.0 \\ \hline \end{array}$$

$$\begin{array}{r} 7.8 \\ DC2.2 \\ \hline 17.4 \end{array}$$

$$\begin{array}{r} 7.0 \\ F3.8 \\ \hline 20.6 \end{array}$$

$$\begin{array}{r} 5.6 \\ F3.2 \\ \hline \end{array}$$

$$\begin{array}{r} 4.8 \\ F1.6 \\ \hline 16.2 \end{array}$$

$$\begin{array}{r} 10.1 \\ F6.0 \\ \hline 25.0 \end{array}$$

$$\begin{array}{r} 8.2 \\ FA.9 \\ \hline \end{array}$$

$$\begin{array}{r} 8.4 \\ FA.3 \\ \hline 21.6 \end{array}$$

$$\begin{array}{r} 11.4 \\ F6.8 \\ \hline 26.6 \end{array}$$

$$\begin{array}{r} 8.7 \\ FA.9 \\ \hline \end{array}$$

$$\begin{array}{r} 10.9 \\ F6.3 \\ \hline 25.6 \end{array}$$

$$\begin{array}{r} 11.6 \\ F6.7 \\ \hline 26.4 \end{array}$$

$$\begin{array}{r} 8.4 \\ FA.3 \\ \hline \end{array}$$

$$\begin{array}{r} 11.9 \\ F7.0 \\ \hline 27.0 \end{array}$$

Sta	+	π	-	Elev	Gr. Rod
		90422			
10+20				99.9	43 51
+67				99.3	49 - 57
11				99.0	52 - 60
+50				98.6	5.6 64
+75				98.3	5.9 6.7
12				98.1	6.1 6.9
+43				97.7	6.5 7.3
+54				97.6	
+60				97.6	
+66				97.5	
+75.94					
B.M.			7.28	896.94	896.92

L1

R

R1

$$\begin{array}{r} 10.7 \\ F5.6 \\ \hline 24.2 \end{array}$$

$$\begin{array}{r} 6.8 \\ F1.1 \\ \hline 15.2 \end{array}$$

$$\begin{array}{r} 5.2 \\ DC0.4 \\ \hline 13.8 \end{array}$$

$$\begin{array}{r} 6.0 \\ DC0.4 \\ \hline 13.8 \end{array}$$

$$\begin{array}{r} 6.2 \\ DC0.5 \\ \hline 14.0 \end{array}$$

$$\begin{array}{r} 6.5 \\ DC0.4 \\ \hline 13.8 \end{array}$$

$$\begin{array}{r} 5.5 \\ DC1.8 \\ \hline 16.6 \end{array}$$

$$\begin{array}{r} 7.7 \\ F3.4 \\ \hline \end{array}$$

$$\begin{array}{r} 5.9 \\ F1.0 \\ \hline \end{array}$$

$$\begin{array}{r} 4.9 \\ C0.3 \\ \hline \end{array}$$

$$\begin{array}{r} 5.0 \\ C0.6 \\ \hline \end{array}$$

$$\begin{array}{r} 5.4 \\ C0.5 \\ \hline \end{array}$$

$$\begin{array}{r} 5.5 \\ C0.6 \\ \hline \end{array}$$

$$\begin{array}{r} 5.8 \\ C0.7 \\ \hline \end{array}$$

$$\begin{array}{r} 11.8 \\ F6.7 \\ \hline 26.4 \end{array}$$

$$\begin{array}{r} 7.1 \\ F1.4 \\ \hline 15.8 \end{array}$$

$$\begin{array}{r} 5.8 \\ DC0.2 \\ \hline 13.4 \end{array}$$

$$\begin{array}{r} 5.8 \\ DC0.6 \\ \hline 14.2 \end{array}$$

$$\begin{array}{r} 6.2 \\ DC0.5 \\ \hline 14.0 \end{array}$$

$$\begin{array}{r} 6.4 \\ DC0.5 \\ \hline 14.0 \end{array}$$

$$\begin{array}{r} 6.5 \\ DC0.8 \\ \hline 14.6 \end{array}$$

Sph G. P. 39 Rt Sta 12453

