

BK 29 - Dr. 12 A

OFFICE OF COUNTY ENGINEER
RAMSEY CO. MINN.

----- PLAN ----- Survey

----- FLOWER ST. -----

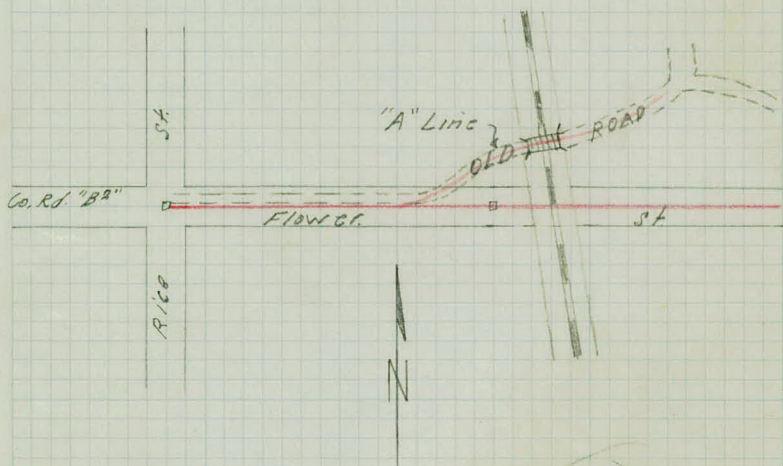
From RICE ST. To Line R.R.

Road Acc't. No. -----

Date Filed 4/40 ----- File -----

BK 29 Dr. 12 A

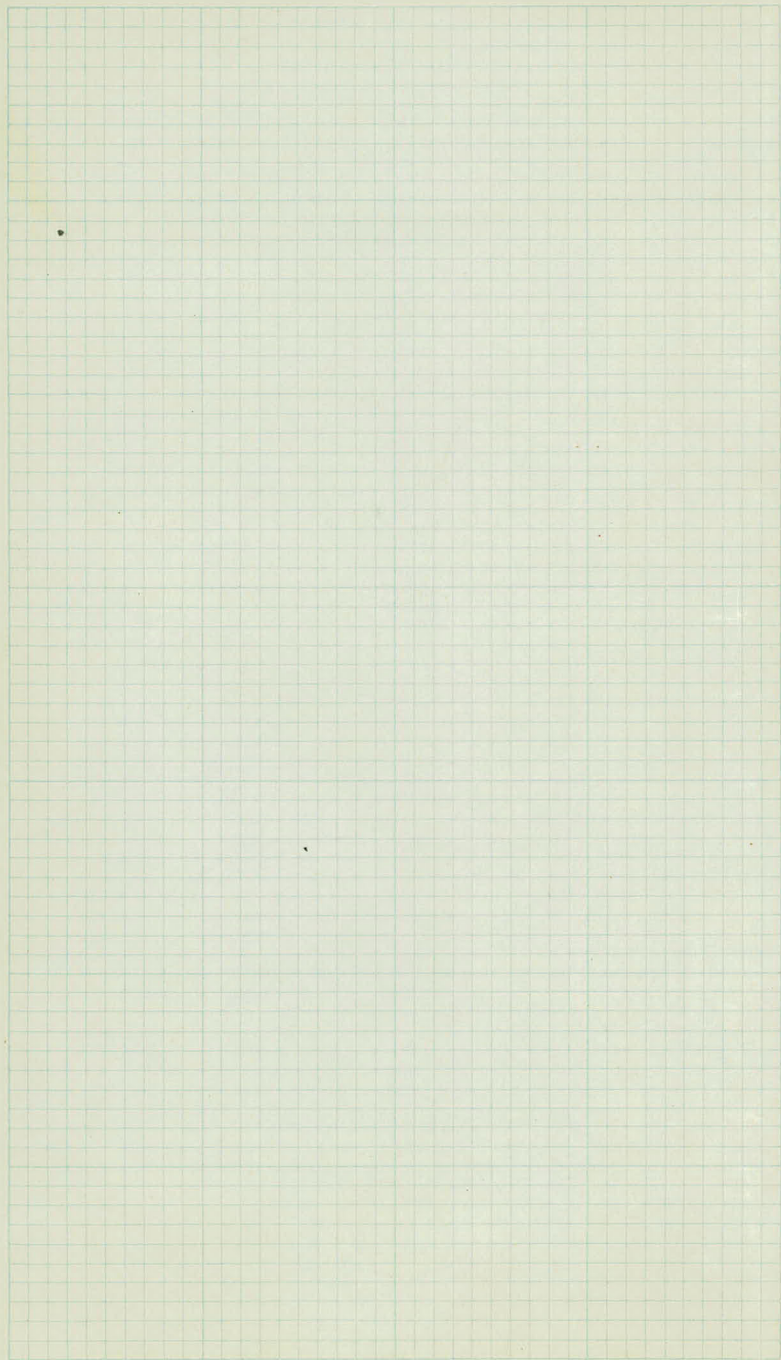
PLAN SURVEY
FLOWER ST.
RICE ST. EAST



INDEX.

Align	- 1-3
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"A" Line	
Align.	- 28-30
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Drawn up
H/5/40
WGB



Alignment

Sta	Point	ΔLt	ΔRt
-----	-------	-------------	-------------

25	+26.09	P.O.T.	
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24	+06.37	P.I.	0°04'
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22	+0163	P.O.T.	
----	-------	--------	--

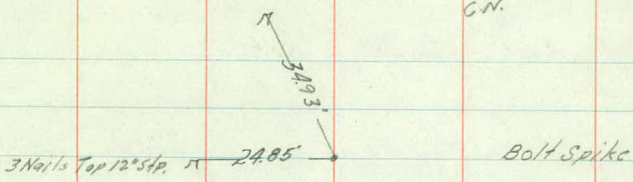
0	+00	= E. Rice St	
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313140

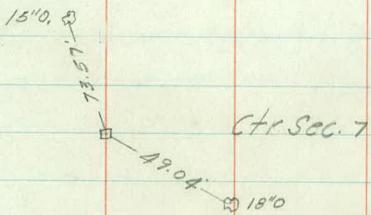
2

K.A.
L.C.
M.B.
C.N.

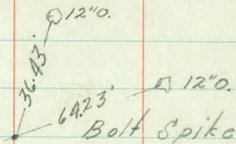
12" stump



13"0.

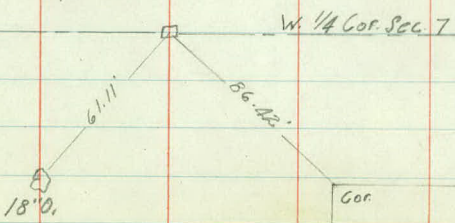


12"0.



90°40½'

89°37'



Sta.	Point	ΔLt	ΔRt
------	-------	-------------	-------------

54 +58.44	= ϕ McMenamy St		
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50 +38.64	P.I.	$0^{\circ}50'$	
-----------	------	----------------	--

26 +66.32	P.O.T. = ϕ R.R. Track		
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18" Cherry Tr. (1)

89°35'

79.67'

E. 1/4 Cor. Sec. 7

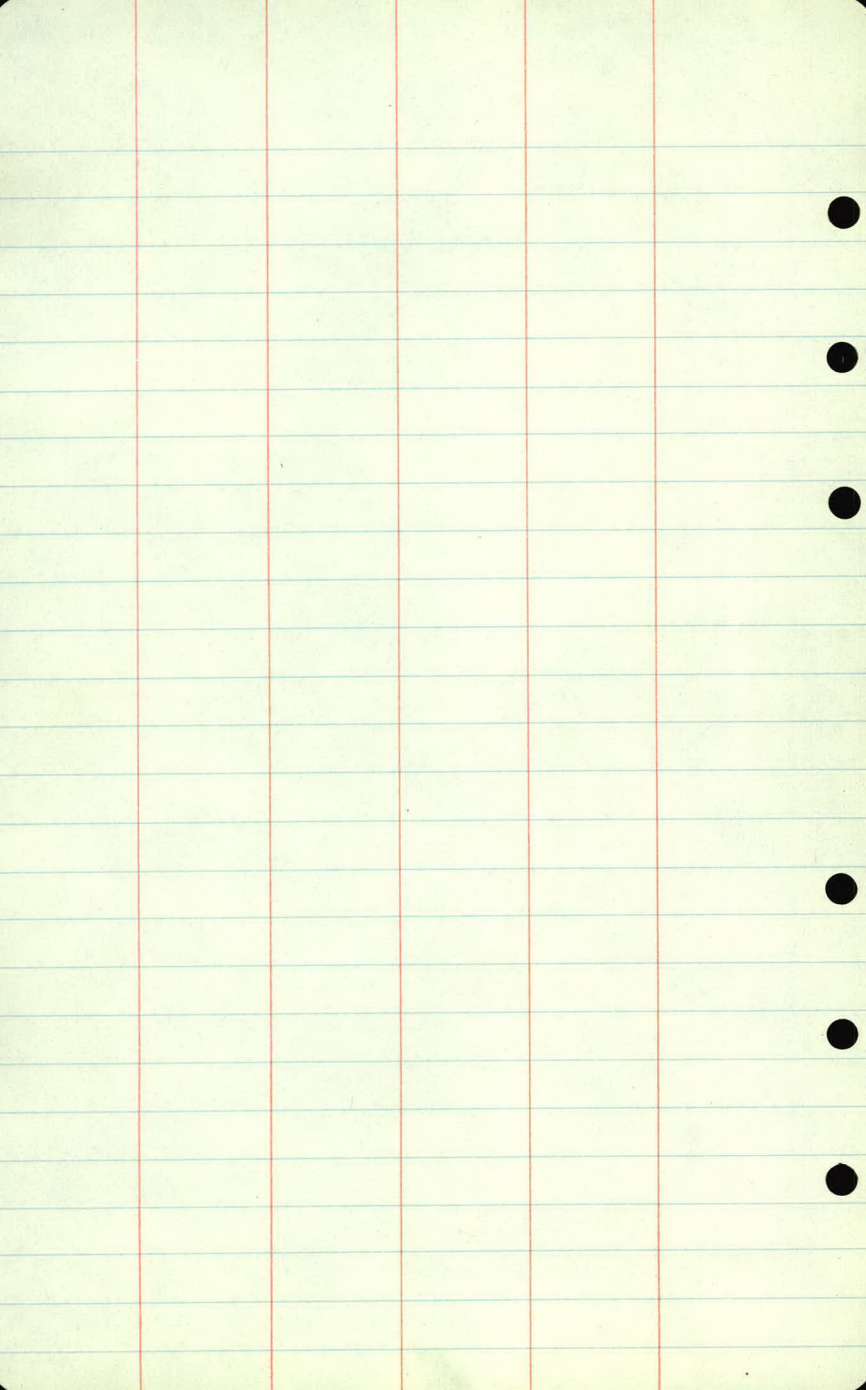
End of Curve

107°07'

2° Curve

178°05'

262.27'



Topography

+81-End Fc-31'

+50-PP-28'

5 Fc-30' 23'-7'

+85-End Fc-2'

+33-Beg. Fc-30'

4 +89-S.W. Cor Garage-55'
PP-28' 22'-7'

+99-42" Cotten-1'

+93-End Fc-32'

+76-36" Cotten-1'

+54-S.W. Cor Ho-56'

+35-Beg Fc-32'

+11-36" Cotten-1'

3 23'-7'

+97-Beg. Fc-31'

+85-End Fc-30'

+31-PP-28'

2 Fc-30' 22'-8'

1 Fc-28' 22'-8'

+70-PP-4TP-27'

+23-Fc Cor-28' +30-20'-8'

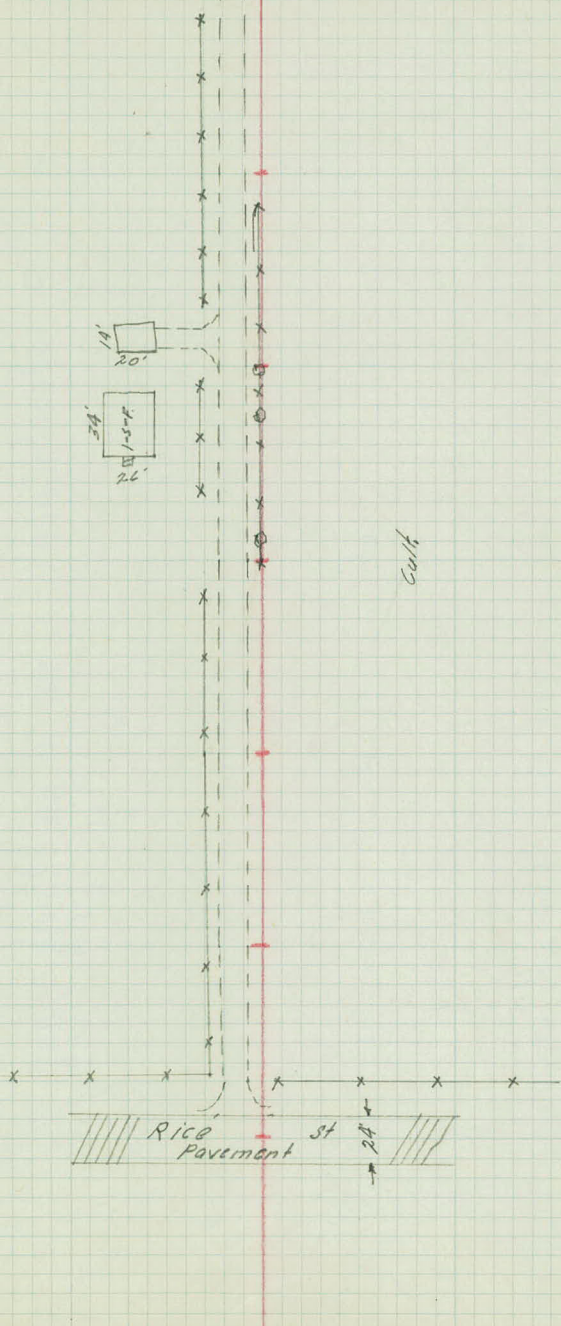
+24-TP-30'

+30-F. Line-6'

0+00

3-8-40

5



12 +04-E. Cor-37' 23'-8'

+62-PP-29'

11 22'-7'

+27-PP-29'

10 22'-8'

9 22'-8'

+71-PP-29'

+27-Entf-

8 22'-8'

+88-3" Elm -38'

+77-S.W. Cor. Ho-68'

+64-6" B. Elder-38'

+43-2" Plum-42'

7 +10-PP-28' 22'-8'

6 21'-8'

x x x x

Posture.

x

x

x

Cult.

Fe. along line down

Cult.

22' 2.5 ft 30'

0 0 0

+81-Kong Tie to Found -
+77-Cor Conc Found - 36'
+61-Cor Conc Found - 31'
+55-6" B. Elder - 35'

+90-Grass - 6-4" B. Elder - 0.0'
+71-12" W. Oak - 2'

+38-E Edge Ent -
Ent.

19 +03-Fc Cor - 33' 23'-10' FC-4'
+4-8" B. Elders - 38'

+90-12" B. Elder - 37'

+60-S W Cor Patch - 49'

+97-15" W. O. - 6'

+32-Fc Cor - 31'

+21-Cor Orchard - 42'

18 +08-End PP - 30' 23'-7'

+89-12" S/P - 33'

+71-12" Stump - 31'

+39-Cor Orchard - 45'

17 Fc - 32' Fc - 1' 22'-8'

+99-PP - 30'

+06-Fc Cor - 33'

16 Fc - 3' 22'-10'

15 Fc - 3' 23'-10'

+95-PP - 30'

+85-Fc Cor - 32'

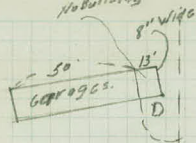
+77-Ent. 41'

+20-Fc Cor - 1'

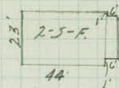
14 Fc - 34' 23'-10'

+90-PP - 30'

13 Bag Fc - 2' 23'-8'



X X X X X



X X X X X

X X X X X

X X X X X

X X X X X

X X X X X

X X X X X

Hog Yard

X X X X X

Pasture

X X X X X

Pasture

+95-End 12" C.M. - 11'

+53-End 12" Core C.M. - 7'

+27-T.P. - 4' R.R.

+15-R X 5

+13-18" O. - 15'

+11-Stop - 26'

+06-Stop - 4'

Runs along track

+04-6" O. - 9'

FC - 4'

+91-15" W. O. - 31'

+94-Stop - 4'

+86-Stop - 4'

26

+67-Stop - 12' +73-Stop - 7'

+66-Stop - 14'

+61-Stop - 18' - 26'

+59-Stop - 13'

+55-Stop - 11'

+49-Stop - 14'

+31-Stop - 29'

+28-Stop - 32'

+24-Stop - 25'

25

+15-Stop - 30'

+91-12" O. - 25' +83-6" O. - 25'

+79-Tr. Stop - 33'

+80-15" O. - 11'

+67-15" O. - 6'

FC - 3'

+96-15" W. O. - 3'

24

FC - 0.0

23

FC - 69' FC - 1' 63' - 46'

+03-18" O. - 5'

+94-Stop - 35'

+88-Stop - 1'

+82-12" W. O. - 35'

+59-Stop - 10'

+38-15" W. O. - 7'

+37-Stop - 14'

+18-Stop - 15'

+09-Stop - 3'

+08-6" W. O. - 7'

+25-FC - 32' 26' - 14'

+19-Stop - 5'

22

FC - 29' FC - 1' 23' - 10'

+50-22' - 8'

21

FC - 27'

21' - 9'

FC - 0.0

+93-Stop - 11'

+89-Stop - 15'

+66-Stop - 22'

+68-End

+29-FC Cor. - 27'

+17-8" B. Gl. St. - 27'

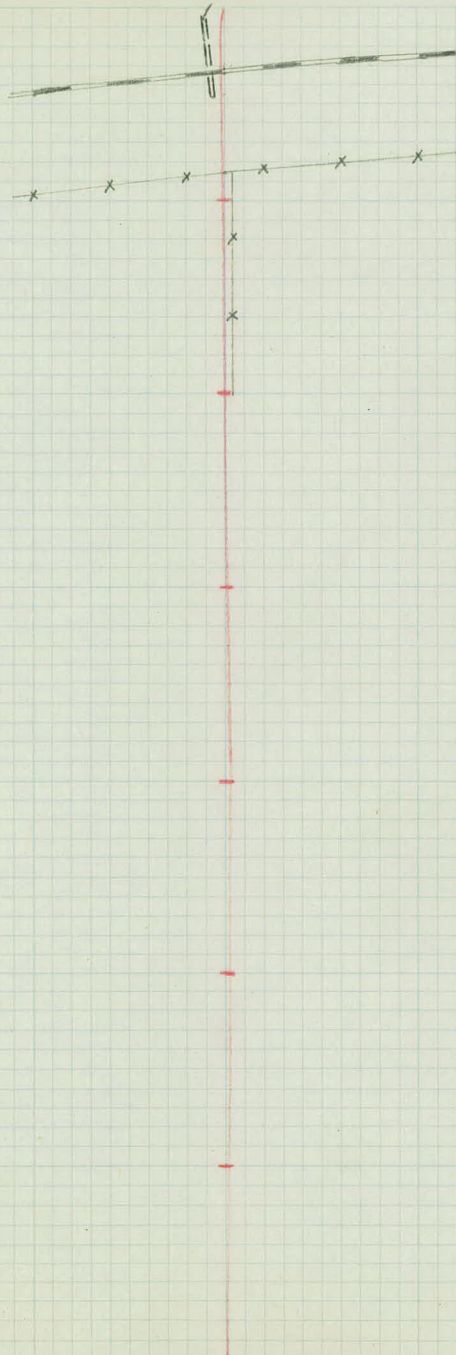
+37-18" O. - 0.0

20

22' - 8'

+02-18" W. O. - 20'

FC - 1'



+24-S.W. Cor. Bormp - 73'

+22-Fc Cor - 15'

+38-Fc Cor - 6'

+24-Fc Cor - 7'

33

+65-Fc Cor 14'

+68-Fc Cor - 6'

32

Fc - 7'

+39-54p - 30'

+37-10" O - 23'

+29-15" O - 10'

+23-54p - 27'

+15-54p - 31'

+13-15" O - 17'

+09-54p - 30'

31

34p - 17'

Fc - 7'

+92-54p - 11'

+70-18" O - 15'

+62-15" O - 36'

+58-10" O - 43'

+57-12" O - 28'

+68-Fc Cor -

30

Fc - 7'

29

Fc - 7'

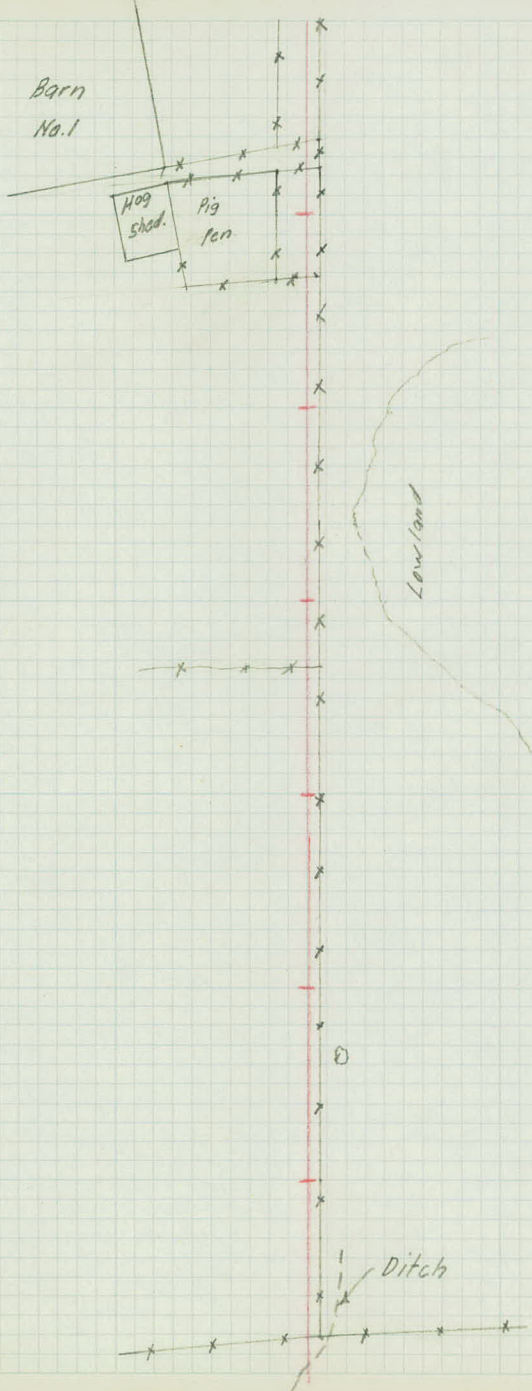
+65-12" Tw. Elm - 16'

28

Fc - 7'

27

+19-Fc Cor - 7'



36

+93-FC. Cor. - 16'

FC-A'

+67-S. E. Cor. Barn - 128'

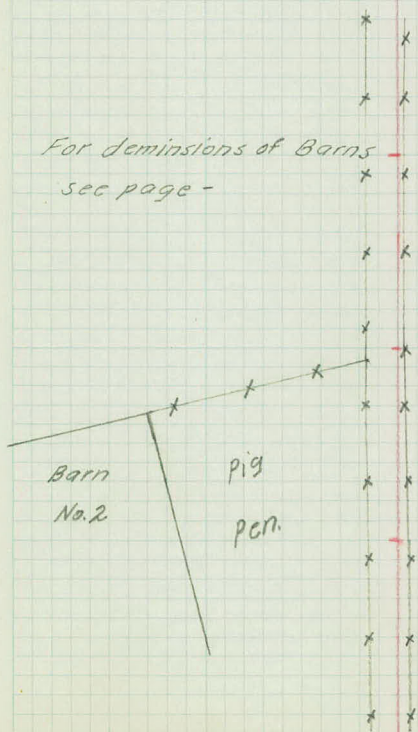
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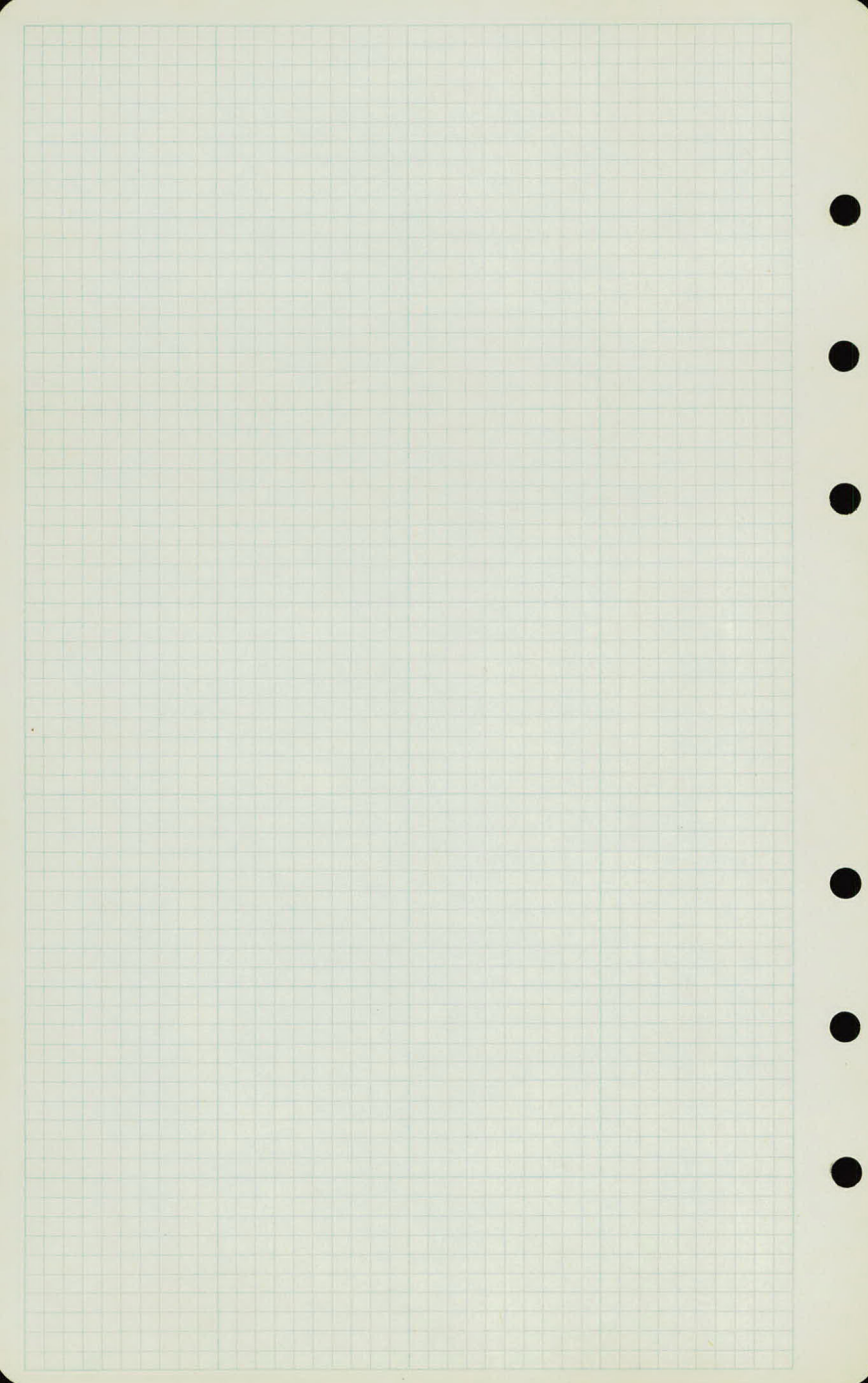
FC-15'

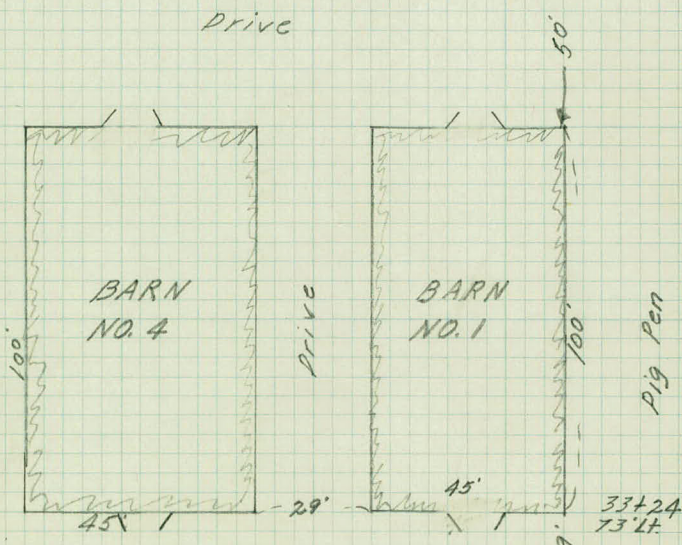
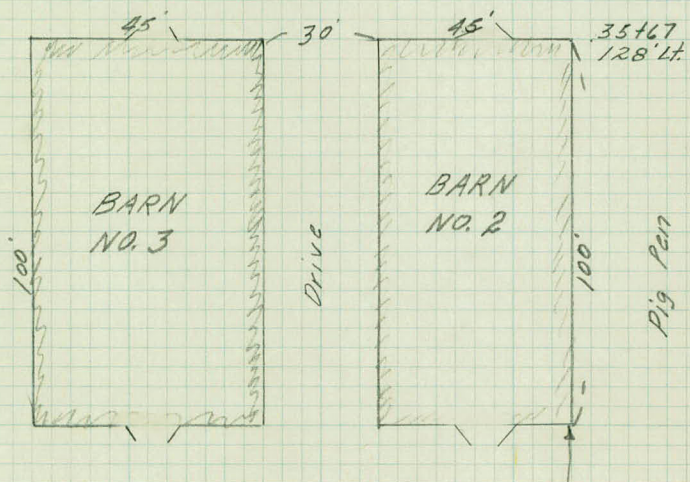
FC-6'

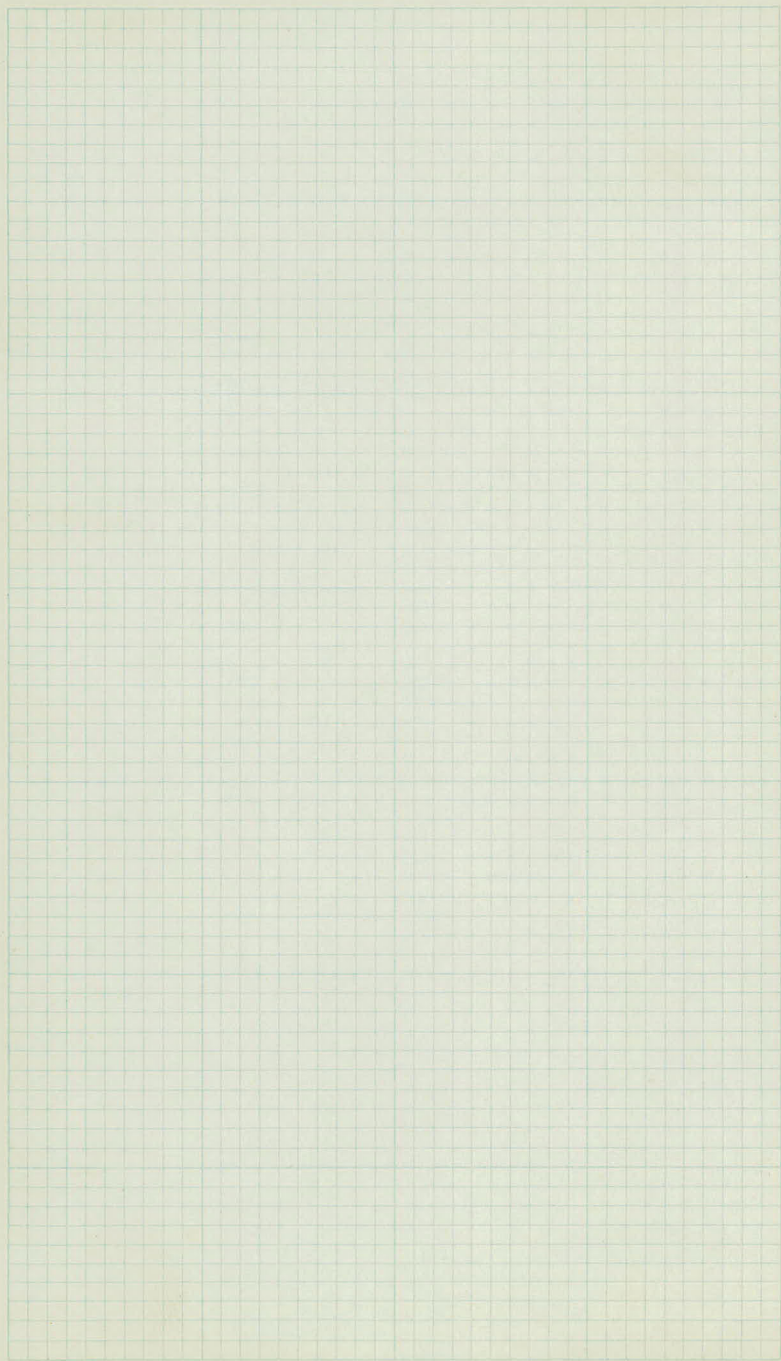
34

For deminsions of Barns
see page -









Alignment
"A" Line

Sta	Point	ΔL	ΔR
-----	-------	------------	------------

+42.13	P.T.		$7^{\circ}52.5' \Delta 15^{\circ}45'$
25			$5^{\circ}20.8' D-12^{\circ} R$
+77.04	P.I.		$T-66.16'$
+50			$2^{\circ}20.8' L-131.25'$
24 +10.88	P.C.		$0^{\circ}00' R-478.34'$

+99.13	P.T.	$13^{\circ}57.9'$	
+75		$12^{\circ}16.6'$	
+50		$10^{\circ}31.6'$	$\Delta 27^{\circ}56'$
+25		$8^{\circ}46.6'$	$D-14^{\circ}-L$
+01.63	P.I. = P.O.T. Main Line		$T-102.02'$
22		$7^{\circ}01.6'$	$L-199.52'$
+75		$5^{\circ}16.6'$	$R-410.28'$
+50		$3^{\circ}31.6'$	
21 +25		$1^{\circ}46.6'$	
20 +99.61	P.C. =	$0^{\circ}00'$	
20 +99.61	P.O.T. Main Line		

Bolt Spike



Bolt Spike

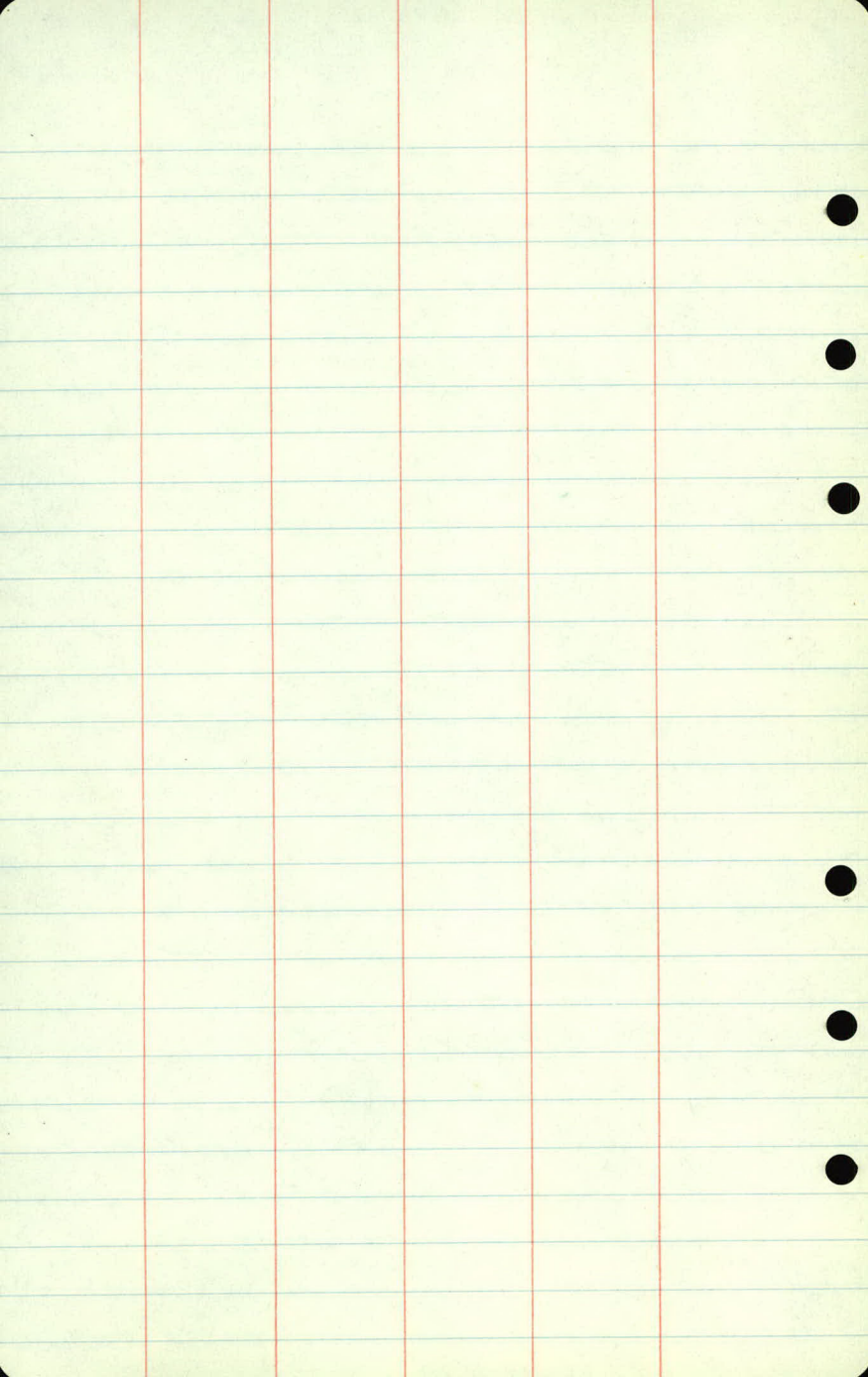
Sta.	Point	ΔLt	ΔRt
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26	+88.11	P.L.	
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26	+06.52	P.L.	6° 01'
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• Nail in E End of Bridge

• Nail in W End of Bridge



Topography

+88.11 - End Bridge

		17' between Railings.	
26	+05-Fc Cor. - 10.5'	+06.52 - End Bridge	
	Fc -	6'	6'
	Fc - 11' +60.	6'	6'
	Fc - 11' +30	6'	6'
25	Fc - 15'	6'	7'
	+50-Fc - 14'	7'	6'
24	Fc - 14'	8'	5'
23	Fc - 16'	9'	6'
	+75-Fc - 15'	8'	1'
	+61-18" O. - 20'		Fc - 40'
	+50-Fc - 13'	8'	1'
			Fc - 30'
	+25-Fc - 12'	8'	5'
			Fc - 18'
22	Fc - 18'	12'	2'
			Fc - 11'
	+50-Fc - 25'	19'-5"	
			Fc - 3'
21	Fc - 27'	21'-9"	
		Fc - 00	

x x x

x

x

x

x

x

x

x

x

x

x

x

x

x

x

x

Pasture

19

x

x

x

x

x

x

x

x

x

x

x

x

x

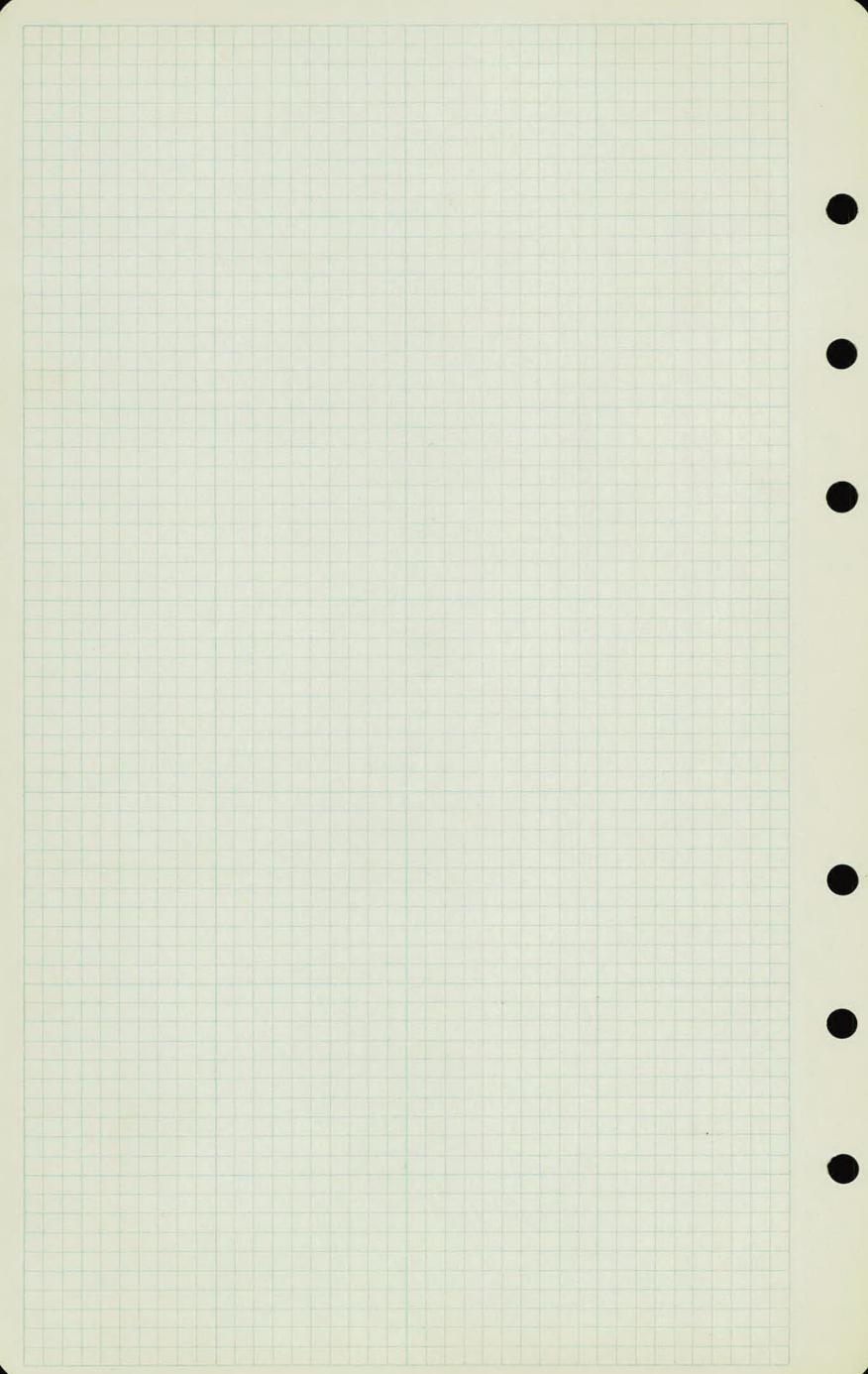
x

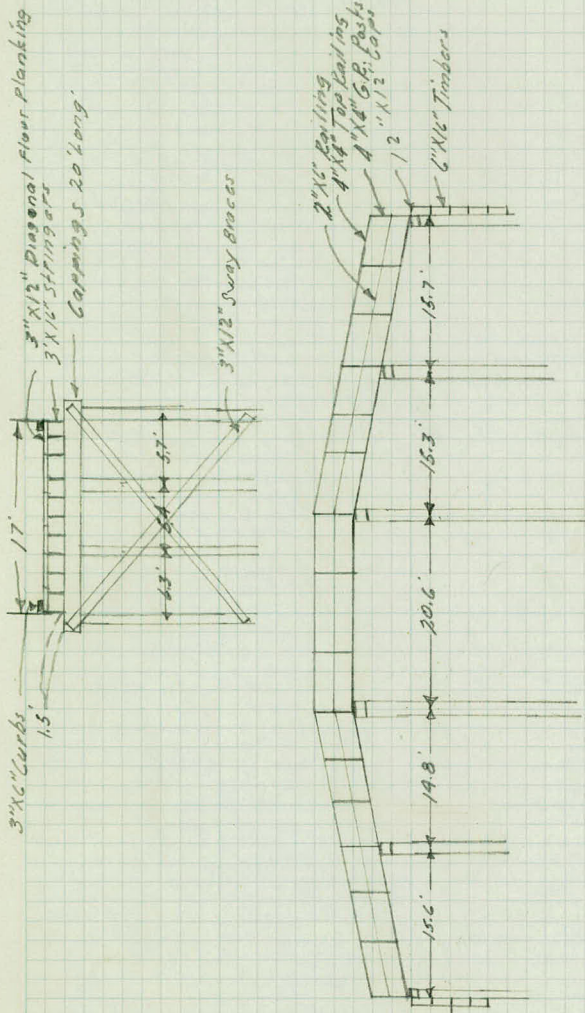
x

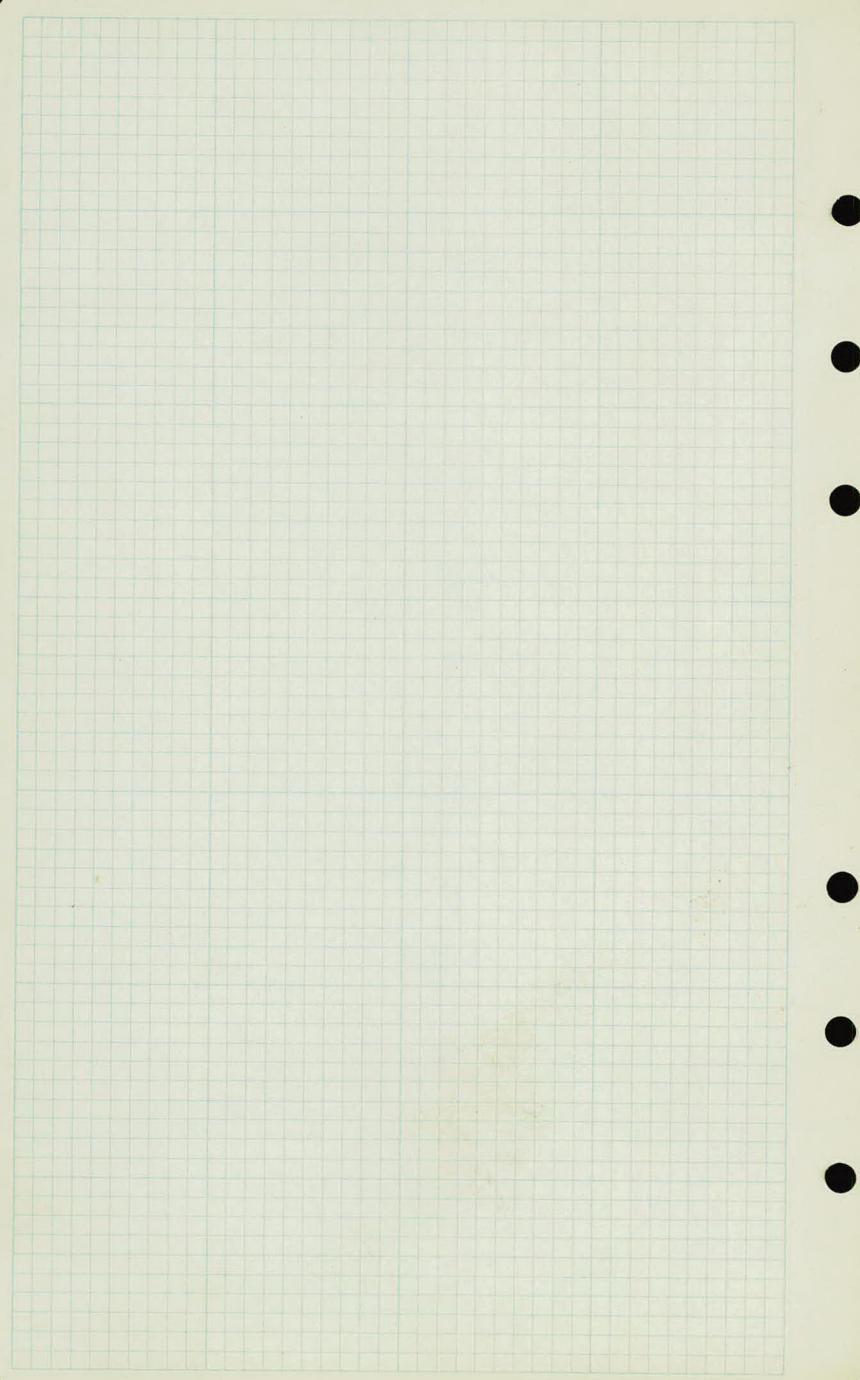
x

x

x







Bench Levels

Sta	t	π	-	Elev
B.M.	9.86	973.37		963.51
B.M.			3.05	970.32
B.M.	6.22	969.73		963.51
T.P.	1.93	959.36	12.30	957.43
T.P.	0.43	950.93	8.86	950.50
B.M.			0.60	950.33
T.P.	1.83	941.44	11.32	939.61
B.M.	0.22	934.60	7.06	934.38
T.P.	0.80	922.62	12.78	921.82
T.P.	0.87	910.44	13.05	909.57
T.P.	4.97	902.40	13.01	897.47
T.P.	2.72	899.17	5.95	896.45
B.M.	7.14	896.84	9.47	889.70
T.P.	4.03	888.25	12.62	884.22
T.P.	8.53	888.82	7.96	880.29
B.M.			9.83	878.99
T.P.	7.01	885.11	10.72	872.10
B.M.			6.42	878.69

Description

Spike in P.P. 28' Lt sta 4+00

Top Mont. Rice St & Flower St. sta 0+00

Spike in P.P. 28' Lt sta. 4+00

Top S.E. Cor. Cong. Found. 36' Lt 19+77

Top R. Stake sta 23+00

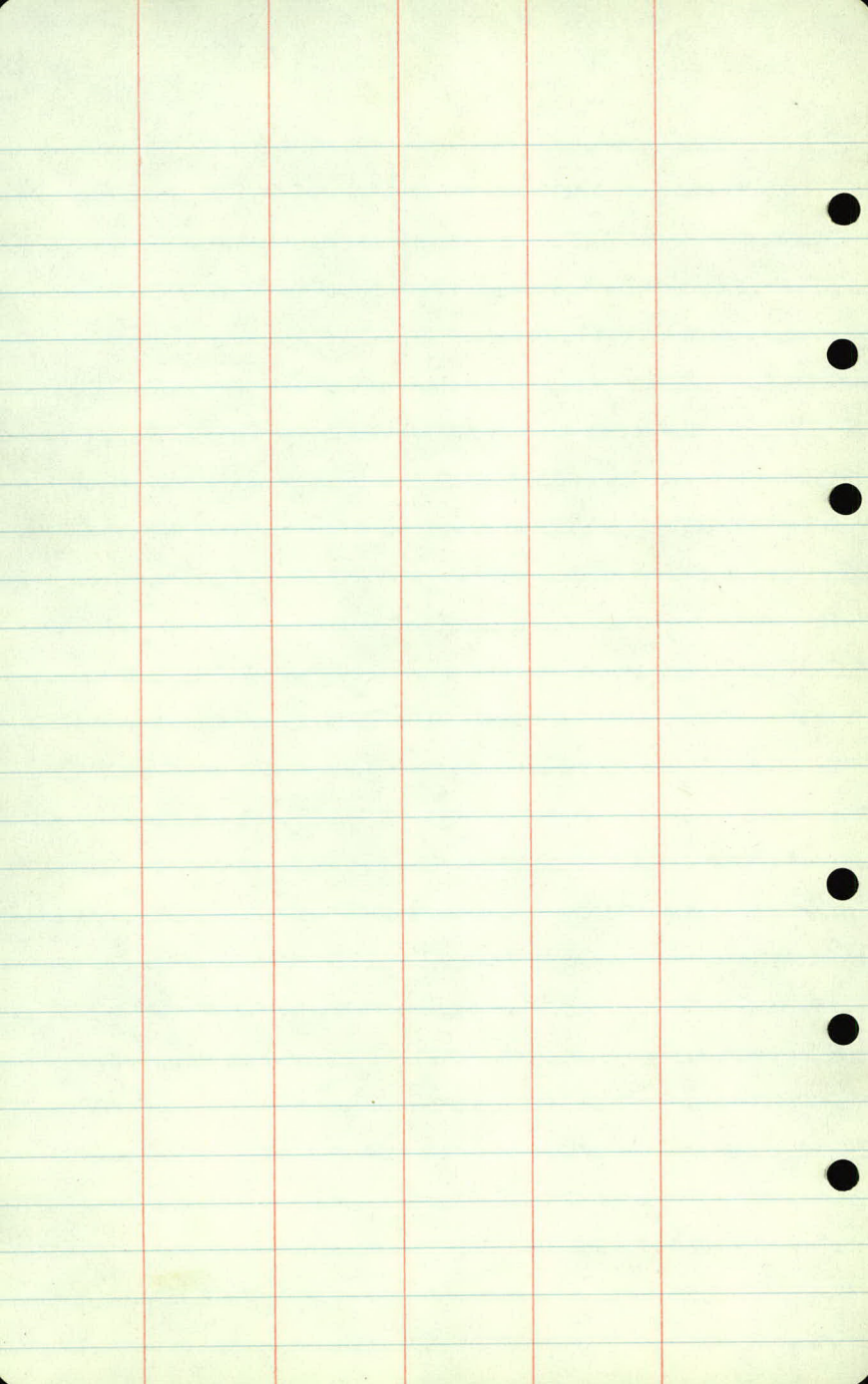
Spike in S.E. Cor. Curbing S.E. Cor. Bridge

Spk. in 15" O. 35' Rt. sta 38+64

Top Mont. sta 50+38.64

Top Found by W. Side of Door on Pump Ho.

These levels run
in strong wind
and should be
checked.



xsections

Sta.	+	π	-	Elev
B.M.	5.11	915.43		(970.32)

0	+00			70.32
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	+12			70.25
--	-----	--	--	-------

	+26			69.3
--	-----	--	--	------

	+31			69.3
--	-----	--	--	------

	+60			72.2
--	-----	--	--	------

1				72.0
---	--	--	--	------

	+50			70.5
--	-----	--	--	------

2				68.2
---	--	--	--	------

	+36			67.0
--	-----	--	--	------

	+70			65.8
--	-----	--	--	------

3				65.1
---	--	--	--	------

LT

R

RT

Top Mont. Rice St & Flower St

69.78 5.11 70.18
5.65 5.11 4.65

69.64 5.18 70.61
5.79 5.18 4.82

75 59 55 61 55 54 54
50 38 15 18 37 50

39 47 58 57 61 55 33 39 48
50 27 25 14 2 4 18 50

37 35 38 66 66 67 36 32 40 56 65
50 41 27 24 15 6 2 6 30 50

50 41 47 70 71 37 34 38 49 61 68
50 37 28 25 7 2 4 21 40 50

65 60 62 76 74 76 49 55 70 79
50 38 29 26 16 6 5 26 50

82 76 83 82 85 70 72 77 87 89
50 36 26 16 6 40 8 29 50

76 84 88 83 90 83 85 84 90 97 98
50 39 29 25 16 6 4 8 25 50

101 100 96 99 96 101 106 105
50 28 16 7 7 28 50

110 119 114 105 101 104 103 108 113 110
50 34 30 26 16 8 6 28 50

Sta	+	π	-	Elev.
		975.43		
3	+50			64.1
T.P.	6.95	970.46	11.92	963.51
4				63.4
	+32			62.9
	+38			62.7
5				62.7
	+50			63.6
6				64.9
	+50			66.2
7				66.2
	+50			67.2
8				67.5

Lt

L

Rt

$$\frac{120}{50} \quad \frac{126}{29} \quad \frac{114}{26} \quad \frac{109}{17} \quad \frac{111}{8} \quad \frac{113}{15} \quad \frac{119}{35} \quad \frac{119}{50}$$

$$\frac{76}{50} \quad \frac{75}{35} \quad \frac{84}{29} \quad \frac{70}{24} \quad \frac{67}{9} \quad \frac{71}{12} \quad \frac{78}{30} \quad \frac{74}{50}$$

$$\frac{78}{50} \quad \frac{91}{30} \quad \frac{80}{28} \quad \frac{74}{25} \quad \frac{69}{16} \quad \frac{69}{4} \quad \frac{76}{11} \quad \frac{80}{30} \quad \frac{75}{50}$$

$$\frac{108}{50} \quad \frac{98}{34} \quad \frac{88}{29} \quad \frac{74}{26} \quad \frac{69}{16} \quad \frac{74}{4} \quad \frac{78}{12} \quad \frac{80}{29} \quad \frac{81}{50}$$

$$\frac{110}{50} \quad \frac{111}{32} \quad \frac{74}{25} \quad \frac{72}{15} \quad \frac{72}{6} \quad \frac{76}{3} \quad \frac{78}{15} \quad \frac{80}{32} \quad \frac{75}{50}$$

$$\frac{112}{50} \quad \frac{107}{33} \quad \frac{78}{27} \quad \frac{74}{23} \quad \frac{73}{15} \quad \frac{74}{4} \quad \frac{69}{7} \quad \frac{73}{19} \quad \frac{73}{50}$$

$$\frac{97}{50} \quad \frac{90}{37} \quad \frac{78}{27} \quad \frac{73}{22} \quad \frac{72}{6} \quad \frac{60}{7} \quad \frac{56}{9} \quad \frac{61}{22} \quad \frac{54}{50}$$

$$\frac{74}{50} \quad \frac{72}{37} \quad \frac{70}{31} \quad \frac{68}{16} \quad \frac{68}{6} \quad \frac{46}{2} \quad \frac{43}{17} \quad \frac{48}{34} \quad \frac{46}{50}$$

$$\frac{54}{50} \quad \frac{57}{36} \quad \frac{59}{29} \quad \frac{62}{26} \quad \frac{62}{16} \quad \frac{63}{6} \quad \frac{39}{2} \quad \frac{43}{14} \quad \frac{43}{33} \quad \frac{44}{50}$$

$$\frac{39}{50} \quad \frac{42}{30} \quad \frac{60}{26} \quad \frac{59}{15} \quad \frac{58}{6} \quad \frac{34}{7} \quad \frac{33}{9} \quad \frac{40}{35} \quad \frac{44}{50}$$

$$\frac{25}{50} \quad \frac{30}{33} \quad \frac{40}{29} \quad \frac{60}{25} \quad \frac{56}{16} \quad \frac{56}{6} \quad \frac{30}{7} \quad \frac{32}{6} \quad \frac{38}{28} \quad \frac{49}{50}$$

Sta	+	π	-	Elev.
		970.46		
8	+25 for ent. grade only.			
	+50			67.7
9				67.4
	+50			66.2
T.P.	6.19	967.63	9.02	961.44
10				64.6
	+23			63.2
	+60			59.0
11				56.6
	+50			54.2
12				54.0
	+50			55.8
T.P.	6.43	964.45	9.61	958.02

LH

4

RH

$$\frac{35}{60} \frac{43}{50} \frac{47}{34} \frac{54}{22} \frac{55}{15}$$

$$\frac{24}{50} \frac{21}{32} \frac{59}{24} \frac{60}{6} \frac{28}{1} \frac{28}{7} \frac{38}{22} \frac{46}{50} \frac{68}{50}$$

$$\frac{28}{50} \frac{25}{31} \frac{63}{24} \frac{62}{15} \frac{63}{6} \frac{31}{7} \frac{41}{32} \frac{62}{50} \frac{80}{50}$$

$$\frac{36}{50} \frac{30}{32} \frac{72}{25} \frac{71}{17} \frac{72}{6} \frac{42}{2} \frac{43}{7} \frac{53}{32} \frac{76}{50} \frac{91}{50}$$

$$\frac{29}{50} \frac{33}{29} \frac{57}{26} \frac{53}{15} \frac{56}{5} \frac{30}{2} \frac{30}{16} \frac{48}{32} \frac{56}{50} \frac{70}{50}$$

$$\frac{46}{50} \frac{64}{30} \frac{62}{28} \frac{60}{5} \frac{44}{3} \frac{44}{13} \frac{59}{23} \frac{60}{50} \frac{78}{50}$$

$$\frac{58}{50} \frac{72}{31} \frac{69}{17} \frac{71}{9} \frac{74}{4} \frac{86}{2} \frac{92}{13} \frac{98}{23} \frac{98}{50} \frac{106}{50}$$

$$\frac{77}{50} \frac{84}{31} \frac{80}{17} \frac{86}{6} \frac{110}{3} \frac{122}{16} \frac{125}{35} \frac{146}{50} \frac{153}{50}$$

$$\frac{98}{50} \frac{104}{32} \frac{100}{30} \frac{94}{17} \frac{98}{8} \frac{110}{4} \frac{134}{3} \frac{156}{24} \frac{180}{50} \frac{198}{50}$$

$$\frac{109}{60} \frac{112}{37} \frac{110}{31} \frac{106}{29} \frac{102}{26} \frac{101}{16} \frac{104}{8} \frac{116}{6} \frac{136}{2} \frac{150}{23} \frac{168}{50} \frac{192}{50}$$

$$\frac{94}{50} \frac{103}{31} \frac{105}{29} \frac{101}{16} \frac{104}{6} \frac{118}{3} \frac{132}{17} \frac{151}{37} \frac{165}{50} \frac{172}{50}$$

Sta.	+	π	-	Elev.
		964.45		

13				56.7
----	--	--	--	------

	+50			58.2
--	-----	--	--	------

14				60.0
----	--	--	--	------

	+27			61.7
--	-----	--	--	------

	+50			61.7
--	-----	--	--	------

15				58.3
----	--	--	--	------

T.P.	566	959.12	10.99	953.46
	+50			544

16				50.4
----	--	--	--	------

T.P.	2.59	951.77	9.94	949.18
	+32			476

	+70			43.6
--	-----	--	--	------

17				42.6
----	--	--	--	------

Lt.

C

Rt.

$$\frac{57}{50} \quad \frac{60}{35} \quad \frac{62}{30} \quad \frac{73}{29} \quad \frac{68}{16} \quad \frac{66}{4} \quad \frac{78}{2} \quad \frac{86}{14} \quad \frac{96}{24} \quad \frac{106}{24} \quad \frac{113}{50}$$

$$\frac{50}{50} \quad \frac{55}{32} \quad \frac{71}{28} \quad \frac{65}{17} \quad \frac{68}{6} \quad \frac{62}{4} \quad \frac{63}{9} \quad \frac{68}{31} \quad \frac{72}{50}$$

$$\frac{52}{50} \quad \frac{54}{30} \quad \frac{78}{26} \quad \frac{76}{17} \quad \frac{77}{8} \quad \frac{43}{4} \quad \frac{45}{4} \quad \frac{42}{19} \quad \frac{43}{32} \quad \frac{44}{32} \quad \frac{43}{50}$$

$$\frac{59}{50} \quad \frac{62}{31} \quad \frac{83}{27} \quad \frac{81}{17} \quad \frac{82}{9} \quad \frac{28}{8} \quad \frac{26}{19} \quad \frac{29}{33} \quad \frac{43}{50} \quad \frac{59}{50}$$

$$\frac{65}{50} \quad \frac{69}{31} \quad \frac{85}{28} \quad \frac{83}{18} \quad \frac{83}{9} \quad \frac{28}{12} \quad \frac{28}{20} \quad \frac{35}{37} \quad \frac{44}{50} \quad \frac{85}{50}$$

$$\frac{74}{50} \quad \frac{69}{31} \quad \frac{95}{27} \quad \frac{96}{18} \quad \frac{97}{8} \quad \frac{62}{8} \quad \frac{71}{18} \quad \frac{83}{29} \quad \frac{97}{29} \quad \frac{142}{50}$$

$$\frac{24}{50} \quad \frac{31}{32} \quad \frac{62}{27} \quad \frac{58}{23} \quad \frac{55}{18} \quad \frac{61}{6} \quad \frac{38}{4} \quad \frac{47}{6} \quad \frac{56}{19} \quad \frac{73}{35} \quad \frac{103}{50} \quad \frac{133}{50}$$

$$\frac{59}{50} \quad \frac{63}{32} \quad \frac{88}{29} \quad \frac{82}{23} \quad \frac{80}{17} \quad \frac{83}{7} \quad \frac{75}{5} \quad \frac{87}{8} \quad \frac{103}{24} \quad \frac{123}{24} \quad \frac{170}{50}$$

$$\frac{34}{50} \quad \frac{30}{34} \quad \frac{26}{29} \quad \frac{27}{26} \quad \frac{26}{17} \quad \frac{28}{7} \quad \frac{31}{3} \quad \frac{42}{9} \quad \frac{52}{19} \quad \frac{61}{37} \quad \frac{80}{50} \quad \frac{94}{50}$$

$$\frac{101}{50} \quad \frac{87}{35} \quad \frac{41}{27} \quad \frac{41}{16} \quad \frac{45}{7} \quad \frac{82}{10} \quad \frac{106}{22} \quad \frac{124}{38} \quad \frac{143}{50} \quad \frac{157}{50}$$

$$\frac{107}{50} \quad \frac{97}{35} \quad \frac{47}{25} \quad \frac{46}{17} \quad \frac{50}{7} \quad \frac{92}{6} \quad \frac{116}{21} \quad \frac{128}{35} \quad \frac{147}{35} \quad \frac{176}{50}$$

Sta	+	π	-	Elev
		951.27		

17	+50			44.8
----	-----	--	--	------

18				45.4
----	--	--	--	------

	+26			48.6
--	-----	--	--	------

T.P.	7.83	958.21	1.39	950.39
------	------	--------	------	--------

	+55			51.2
--	-----	--	--	------

	+80			52.1
--	-----	--	--	------

19				53.7
----	--	--	--	------

	+30			52.5
--	-----	--	--	------

	+50			52.6
--	-----	--	--	------

B.M.	1.01	951.34	7.84	950.37	(950.33)
------	------	--------	------	--------	----------

20	+76			47.1
----	-----	--	--	------

20				43.9
----	--	--	--	------

	+50			39.6
--	-----	--	--	------

Lt

A

Rt

Deep Hole Rt

$$\frac{10.5}{50} \quad \frac{10.3}{38} \quad \frac{5.8}{29} \quad \frac{5.3}{27} \quad \frac{5.0}{15} \quad \frac{5.2}{6} \quad \frac{7.0}{2} \quad \frac{7.0}{9} \quad \frac{8.0}{23} \quad \frac{9.9}{42} \quad \frac{13.5}{42} \quad \frac{15.8}{50}$$

$$\frac{10.1}{50} \quad \frac{11.1}{42} \quad \frac{9.2}{32} \quad \frac{4.8}{27} \quad \frac{4.3}{16} \quad \frac{4.6}{5} \quad \frac{6.3}{2} \quad \frac{6.4}{10} \quad \frac{6.8}{26} \quad \frac{8.8}{26} \quad \frac{13.8}{50}$$

$$\frac{10.4}{50} \quad \frac{6.9}{32} \quad \frac{3.3}{28} \quad \frac{2.6}{17} \quad \frac{3.0}{7} \quad \frac{3.2}{12} \quad \frac{4.7}{12} \quad \frac{7.2}{27} \quad \frac{11.4}{50}$$

$$\frac{8.6}{50} \quad \frac{8.1}{42} \quad \frac{7.7}{30} \quad \frac{9.0}{27} \quad \frac{8.4}{16} \quad \frac{8.7}{4} \quad \frac{7.0}{2} \quad \frac{5.3}{12} \quad \frac{6.0}{29} \quad \frac{7.6}{29} \quad \frac{10.8}{50}$$

$$\frac{7.7}{47} \quad \frac{7.8}{29} \quad \frac{8.4}{27} \quad \frac{7.9}{16} \quad \frac{8.2}{7} \quad \frac{8.1}{3} \quad \frac{6.1}{4} \quad \frac{2.4}{4} \quad \frac{2.5}{10} \quad \frac{2.6}{24} \quad \frac{4.0}{43} \quad \frac{4.9}{50}$$

$$\frac{7.4}{50} \quad \frac{7.7}{32} \quad \frac{7.7}{28} \quad \frac{8.0}{27} \quad \frac{7.7}{17} \quad \frac{8.0}{9} \quad \frac{7.7}{4} \quad \frac{4.5}{3} \quad \frac{2.2}{17} \quad \frac{1.9}{27} \quad \frac{2.4}{43} \quad \frac{4.7}{50}$$

$$\frac{8.2}{50} \quad \frac{7.9}{37} \quad \frac{8.2}{31} \quad \frac{8.6}{26} \quad \frac{8.0}{18} \quad \frac{8.3}{10} \quad \frac{8.2}{5} \quad \frac{5.7}{2} \quad \frac{1.9}{13} \quad \frac{2.8}{34} \quad \frac{5.4}{34} \quad \frac{6.0}{50}$$

$$\frac{7.9}{50} \quad \frac{8.0}{33} \quad \frac{9.1}{31} \quad \frac{9.1}{26} \quad \frac{8.9}{16} \quad \frac{9.2}{11} \quad \frac{9.4}{5} \quad \frac{5.6}{2} \quad \frac{5.2}{13} \quad \frac{6.5}{27} \quad \frac{7.4}{27} \quad \frac{9.3}{50}$$

Top S.E. Cor. Camp. Found. 36' Lt. 19177

$$\frac{1.3}{50} \quad \frac{2.6}{36} \quad \frac{3.8}{29} \quad \frac{3.1}{26} \quad \frac{3.5}{16} \quad \frac{3.6}{10} \quad \frac{3.1}{5} \quad \frac{4.2}{7} \quad \frac{4.9}{23} \quad \frac{5.9}{23} \quad \frac{8.3}{50}$$

$$\frac{7.4}{50} \quad \frac{6.2}{34} \quad \frac{4.7}{26} \quad \frac{4.5}{16} \quad \frac{4.6}{10} \quad \frac{4.8}{6} \quad \frac{7.4}{3} \quad \frac{8.2}{12} \quad \frac{8.3}{12} \quad \frac{8.8}{27} \quad \frac{9.2}{50}$$

$$\frac{7.2}{50} \quad \frac{6.7}{28} \quad \frac{5.5}{23} \quad \frac{5.3}{74} \quad \frac{5.9}{6} \quad \frac{11.7}{9} \quad \frac{8.5}{18} \quad \frac{8.7}{18} \quad \frac{9.3}{31} \quad \frac{12.3}{50}$$

Sta.	+	Δ	-	Elev.
		951.34		
20	+84			45.4
21				45.7.
	+46			48.7.
	+71			49.3.
22				46.1.
	+32			43.1.
	+71			41.3.
T.P.			11.72	939.62.

LH

R

RH

$\frac{20}{50}$	$\frac{20}{34}$	$\frac{46}{30}$	$\frac{52}{26}$	$\frac{50}{14}$	$\frac{52}{8}$	$\frac{59}{6}$	$\frac{74}{18}$	$\frac{91}{35}$	$\frac{114}{50}$	$\frac{129}{50}$
-----------------	-----------------	-----------------	-----------------	-----------------	----------------	----------------	-----------------	-----------------	------------------	------------------

$\frac{14}{50}$	$\frac{19}{33}$	$\frac{52}{27}$	$\frac{48}{14}$	$\frac{56}{5}$	$\frac{56}{16}$	$\frac{82}{36}$	$\frac{112}{50}$
-----------------	-----------------	-----------------	-----------------	----------------	-----------------	-----------------	------------------

$\frac{60}{50}$	$\frac{59}{40}$	$\frac{49}{30}$	$\frac{53}{26}$	$\frac{49}{15}$	$\frac{53}{6}$	$\frac{24}{2}$	$\frac{26}{14}$	$\frac{41}{29}$	$\frac{69}{50}$	$\frac{108}{50}$
-----------------	-----------------	-----------------	-----------------	-----------------	----------------	----------------	-----------------	-----------------	-----------------	------------------

$\frac{87}{50}$	$\frac{79}{42}$	$\frac{56}{29}$	$\frac{62}{27}$	$\frac{54}{15}$	$\frac{57}{5}$	$\frac{19}{2}$	$\frac{20}{15}$	$\frac{32}{34}$	$\frac{51}{50}$	$\frac{71}{50}$
-----------------	-----------------	-----------------	-----------------	-----------------	----------------	----------------	-----------------	-----------------	-----------------	-----------------

$\frac{94}{50}$	$\frac{68}{30}$	$\frac{73}{25}$	$\frac{70}{16}$	$\frac{74}{5}$	$\frac{52}{2}$	$\frac{52}{17}$	$\frac{45}{36}$	$\frac{49}{50}$	$\frac{59}{50}$
-----------------	-----------------	-----------------	-----------------	----------------	----------------	-----------------	-----------------	-----------------	-----------------

$\frac{107}{50}$	$\frac{113}{39}$	$\frac{103}{30}$	$\frac{92}{23}$	$\frac{96}{11}$	$\frac{94}{3}$	$\frac{82}{1}$	$\frac{82}{15}$	$\frac{69}{34}$	$\frac{67}{50}$	$\frac{76}{50}$
------------------	------------------	------------------	-----------------	-----------------	----------------	----------------	-----------------	-----------------	-----------------	-----------------

$\frac{128}{50}$	$\frac{123}{39}$	$\frac{122}{29}$	$\frac{120}{19}$	$\frac{115}{4}$	$\frac{102}{2}$	$\frac{100}{14}$	$\frac{92}{35}$	$\frac{82}{50}$	$\frac{82}{50}$
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Top R stake sta 23

Sta	+	π	-	Elev
T.P	1.23	940.84		939.61

23				38.7
----	--	--	--	------

+26				32.3
-----	--	--	--	------

+57				24.1
-----	--	--	--	------

T.P	1.92	931.19	11.57	929.27
-----	------	--------	-------	--------

+81				21.4
-----	--	--	--	------

24				20.7
----	--	--	--	------

+32				19.9
-----	--	--	--	------

+52				20.2
-----	--	--	--	------

+62				20.9
-----	--	--	--	------

+87				23.2
-----	--	--	--	------

25				24.2
----	--	--	--	------

+26				24.7
-----	--	--	--	------

3-11-40
K.H.
L.G.
M.B.
G.N.

21

Lt

K

Rt

Top of stake 23400 Elev from Bench Levels.

$\frac{31}{50}$ $\frac{35}{41}$ $\frac{48}{36}$ $\frac{48}{23}$ $\frac{31}{9}$ $\frac{28}{5}$ $\frac{17}{20}$ $\frac{21}{20}$ $\frac{21}{38}$ $\frac{27}{50}$

$\frac{65}{50}$ $\frac{74}{26}$ $\frac{79}{11}$ $\frac{85}{12}$ $\frac{85}{22}$ $\frac{80}{50}$ $\frac{71}{50}$

$\frac{111}{50}$ $\frac{164}{25}$ $\frac{170}{10}$ $\frac{167}{12}$ $\frac{156}{30}$ $\frac{126}{42}$ $\frac{108}{50}$ $\frac{103}{50}$

$\frac{46}{50}$ $\frac{65}{45}$ $\frac{92}{28}$ $\frac{100}{13}$ $\frac{98}{10}$ $\frac{82}{23}$ $\frac{56}{34}$ $\frac{36}{42}$ $\frac{24}{50}$ $\frac{22}{50}$

$\frac{60}{50}$ $\frac{72}{43}$ $\frac{87}{33}$ $\frac{104}{18}$ $\frac{109}{8}$ $\frac{105}{8}$ $\frac{97}{18}$ $\frac{77}{28}$ $\frac{56}{39}$ $\frac{40}{50}$ $\frac{31}{50}$

$\frac{74}{50}$ $\frac{72}{42}$ $\frac{73}{28}$ $\frac{110}{5}$ $\frac{113}{5}$ $\frac{115}{15}$ $\frac{100}{27}$ $\frac{76}{44}$ $\frac{46}{50}$ $\frac{42}{50}$

$\frac{79}{50}$ $\frac{72}{41}$ $\frac{71}{31}$ $\frac{104}{8}$ $\frac{110}{7}$ $\frac{106}{17}$ $\frac{88}{29}$ $\frac{65}{43}$ $\frac{42}{50}$ $\frac{37}{50}$

$\frac{81}{50}$ $\frac{72}{39}$ $\frac{82}{23}$ $\frac{105}{8}$ $\frac{103}{8}$ $\frac{90}{11}$ $\frac{59}{24}$ $\frac{38}{37}$ $\frac{28}{50}$

$\frac{108}{50}$ $\frac{90}{30}$ $\frac{95}{16}$ $\frac{80}{16}$ $\frac{46}{34}$ $\frac{14}{34}$ $\frac{16}{50}$

$\frac{129}{50}$ $\frac{106}{31}$ $\frac{98}{20}$

$\frac{70}{8}$ $\frac{53}{25}$ $\frac{20}{34}$ $\frac{13}{50}$ $\frac{23}{50}$

$\frac{147}{50}$ $\frac{104}{29}$ $\frac{93}{21}$ $\frac{65}{19}$ $\frac{41}{28}$ $\frac{38}{36}$ $\frac{42}{50}$ $\frac{54}{50}$

Sta	+	π	-	Elev
		931.19		
25 + 58				22.5
+76				20.3
26				16.0
I.P.	116	918.88	13.47	917.72
26				16.0
+24				09.9
+38 -				09.5
+42				11.6
+48				11.8
+55 Ditch Along Track				08.4
+63.7 Top Ctr. W. Rail				11.09
+68.9 Top Ctr. E. Rail				11.35

Lt

R

Rt

$$\frac{165}{30} \quad \frac{118}{21} \quad \frac{92}{6} \quad \frac{87}{20} \quad \frac{72}{20} \quad \frac{64}{32} \quad \frac{53}{50}$$

$$\frac{185}{50} \quad \frac{185}{43} \quad \frac{145}{24} \quad \frac{127}{11} \quad \frac{109}{7} \quad \frac{97}{29} \quad \frac{69}{38} \quad \frac{61}{50} \quad \frac{58}{50}$$

$$\frac{152}{72} \quad \frac{136}{39} \quad \frac{87}{50} \quad \frac{90}{50}$$

$$\frac{56}{50} \quad \frac{67}{35} \quad \frac{63}{28} \quad \frac{52}{17}$$

(29)

$$\frac{55}{50} \quad \frac{72}{37} \quad \frac{85}{22} \quad \frac{91}{6} \quad \frac{90}{11} \quad \frac{82}{21} \quad \frac{73}{21} \quad \frac{47}{36} \quad \frac{29}{50}$$

$$\frac{54}{50} \quad \frac{78}{32} \quad \frac{93}{15}$$

$$\frac{94}{7} \quad \frac{97}{21} \quad \frac{103}{26} \quad \frac{111}{26} \quad \frac{109}{50}$$

$$\frac{36}{50} \quad \frac{59}{32} \quad \frac{71}{13} \quad \frac{92}{8} \quad \frac{90}{6} \quad \frac{73}{6}$$

$$\frac{87}{50}$$

$$\frac{41}{50} \quad \frac{59}{32} \quad \frac{72}{12}$$

$$\frac{94}{7} \quad \frac{94}{4} \quad \frac{71}{4}$$

$$\frac{89}{50}$$

$$\frac{96}{50}$$

$$\frac{103}{18}$$

$$\frac{11.85}{18 \text{ cm} \times 7} \quad \frac{105}{7}$$

$$\frac{107}{50}$$

$$\frac{738}{50}$$

$$\frac{779}{50}$$

$$\frac{817}{50}$$

$$\frac{716}{50}$$

$$\frac{753}{50}$$

$$\frac{794}{17}$$

Sta	+	π	-	Elev
		918.88		
26	+77			09.3
	+87			09.3
	+95		13.30	
27				08.3
T.P.	2.46	911.19	10.15	908.73
	+25			06.0
	+52			04.9
	+80			00.9
28				97.9
T.P.	1.24	899.94	12.49	898.70
	+50			91.2
29				87.5
	+50			85.3

Lt

K

Rt

$$\frac{98}{50} \quad \frac{101}{27} \quad \frac{96}{34} \quad \frac{96}{50}$$

$$\frac{75}{50} \quad \frac{84}{31} \quad \frac{103}{8} \quad \frac{96}{50} \quad \frac{94}{50}$$

F.L. 12" G.M. GULV. 11' Lt

05.58

$$\frac{74}{50} \quad \frac{89}{30} \quad \frac{111}{19} \quad \frac{104}{13} \quad \frac{125}{10} \quad \frac{125}{7} \quad \frac{106}{17} \quad \frac{106}{29} \quad \frac{161}{50} \quad \frac{173}{50}$$

$$\frac{07}{50} \quad \frac{42}{26} \quad \frac{53}{14} \quad \frac{52}{9} \quad \frac{53}{10} \quad \frac{56}{12} \quad \frac{51}{25} \quad \frac{52}{36} \quad \frac{39}{50} \quad \frac{95}{50}$$

$$\frac{40}{50} \quad \frac{44}{14} \quad \frac{48}{31} \quad \frac{51}{17} \quad \frac{63}{14} \quad \frac{70}{18} \quad \frac{87}{21} \quad \frac{69}{50} \quad \frac{68}{50}$$

$$\frac{59}{50} \quad \frac{62}{36} \quad \frac{68}{27} \quad \frac{83}{13} \quad \frac{103}{11} \quad \frac{115}{17} \quad \frac{116}{21} \quad \frac{131}{24} \quad \frac{118}{50} \quad \frac{112}{50}$$

$$\frac{87}{50} \quad \frac{93}{29} \quad \frac{108}{17} \quad \frac{133}{10} \quad \frac{142}{26} \quad \frac{144}{50} \quad \frac{146}{50}$$

$$\frac{80}{50} \quad \frac{89}{31} \quad \frac{91}{15} \quad \frac{87}{25} \quad \frac{88}{50} \quad \frac{88}{50}$$

$$\frac{143}{50} \quad \frac{146}{31} \quad \frac{124}{15} \quad \frac{116}{32} \quad \frac{111}{42} \quad \frac{99}{50} \quad \frac{88}{50}$$

$$\frac{166}{50} \quad \frac{185}{31} \quad \frac{156}{8} \quad \frac{146}{9} \quad \frac{130}{22} \quad \frac{105}{50} \quad \frac{34}{50}$$

Sta	+	π	-	Elev
		899.94		
30				86.6
T.P.	0.67	887.57	13.04	886.90
+35				84.0
+67				82.4
31				82.3
+50				81.3
+85				81.6
32				83.4
+48				83.8
T.P.	10.03	896.41	11.9	886.38
+61				86.4
33				88.7
+35				89.4

Lt.

A

Rt.

$$\frac{16.6}{50} \quad \frac{15.3}{20} \quad \frac{13.3}{25} \quad \frac{9.8}{25} \quad \frac{6.3}{50}$$

$$\frac{44}{50} \quad \frac{46}{23} \quad \frac{36}{25} \quad \frac{2.3}{25} \quad \frac{1.0}{50}$$

$$\frac{21}{30} \quad \frac{26}{29} \quad \frac{28}{23} \quad \frac{36}{14} \quad \frac{45}{8} \quad \frac{5.2}{17} \quad \frac{6.0}{50} \quad \frac{5.8}{50}$$

Drains - 5.11.01

$$\frac{0.0}{50} \quad \frac{36}{18} \quad \frac{53}{35} \quad \frac{7.0}{35} \quad \frac{8.3}{50}$$

$$\frac{2.8}{50} \quad \frac{50}{25} \quad \frac{6.3}{25} \quad \frac{8.0}{25} \quad \frac{9.3}{50}$$

$$\frac{37}{50} \quad \frac{54}{25} \quad \frac{6.0}{25} \quad \frac{7.8}{25} \quad \frac{9.4}{50}$$

$$\frac{2.8}{50} \quad \frac{41}{29} \quad \frac{35}{23} \quad \frac{42}{7} \quad \frac{51}{8} \quad \frac{64}{28} \quad \frac{7.8}{28} \quad \frac{90}{50}$$

$$\frac{+2.1}{50} \quad \frac{+0.7}{35} \quad \frac{2.2}{27} \quad \frac{2.9}{19} \quad \frac{3.8}{7} \quad \frac{36}{27} \quad \frac{6.0}{27} \quad \frac{7.9}{50}$$

$$\frac{6.3}{50} \quad \frac{74}{31} \quad \frac{8.0}{20} \quad \frac{90}{10} \quad \frac{100}{7} \quad \frac{110}{25} \quad \frac{13.8}{25} \quad \frac{156}{50}$$

$$\frac{37}{50} \quad \frac{41}{41} \quad \frac{5.5}{20} \quad \frac{6.2}{13} \quad \frac{7.7}{7} \quad \frac{8.3}{25} \quad \frac{11.9}{25} \quad \frac{15.0}{50}$$

$$\frac{40}{50} \quad \frac{57}{25} \quad \frac{7.0}{6} \quad \frac{7.2}{9} \quad \frac{9.0}{31} \quad \frac{131}{31} \quad \frac{148}{50}$$

Sta	+	π	-	Elev
		896.41.		
			0.20	
38	+75			84.7.
34				83.3.
Elev. of Buildings - Floor. = Approx - 896.40				
	+40			83.4.
	+70			83.4.
35				86.0.
	+21		8.2	88.2.
	+50		7.3	89.1.
	+86		6.7	89.7.
36			7.8	88.6.

Lt.

Q

Rt.

Elev. S.W. Cor. Barn #1

96.21

$$\frac{5.0}{50} \quad \frac{7.3}{28} \quad \frac{8.9}{10} \quad \frac{11.7}{7} \quad \frac{12.7}{30} \quad \frac{14.6}{50} \quad \frac{15.3}{50}$$

$$\frac{6.3}{50} \quad \frac{9.6}{25} \quad \frac{10.7}{10} \quad \frac{13.1}{6} \quad \frac{13.6}{8} \quad \frac{14.3}{32} \quad \frac{15.6}{50} \quad \frac{16.2}{50}$$

$$\frac{8.4}{50} \quad \frac{10.1}{36} \quad \frac{11.3}{14} \quad \frac{13.0}{7} \quad \frac{13.3}{9} \quad \frac{14.2}{30} \quad \frac{16.2}{50} \quad \frac{15.8}{50}$$

$$\frac{9.3}{50} \quad \frac{10.2}{43} \quad \frac{11.3}{14} \quad \frac{13.0}{6} \quad \frac{12.9}{10} \quad \frac{13.7}{36} \quad \frac{14.2}{50} \quad \frac{14.3}{50}$$

$$\frac{9.5}{50} \quad \frac{10.6}{31} \quad \frac{10.7}{18} \quad \frac{10.4}{7} \quad \frac{9.7}{27} \quad \frac{10.0}{50} \quad \frac{10.1}{50}$$

Sta	+	π	-	Elev
		896.41		
36	+15		9.1	87.3
T.P.	11.14	895.30	12.25	884.16
	+50		13.4	81.9
	+65		15.7	79.6
	+75		14.6	80.7
37			13.7	81.6
	+20		13.8	81.5
	+55		17.5	77.8
	+78		18.0	77.3
38			17.7	77.6
	+28		16.5	78.8
B.M.			5.60	889.70
	+74		9.2	86.1

(889.70)

Lt

R

Rt

Spk. in 15" 0.35 Rk 38464

Sta.	+	π	-	Elev
		895.30'		
39			5.1	90.2.
+22			1.9	93.4.
+50			1.3	94.0.
+81			4.1	91.2.
40			4.2	91.1.
+50			5.7	89.6.
41			10.3	85.0.
+50			16.2	79.1.
42			19.8	75.5.
+50			21.8	73.5.
B.M.	6.52	896.22.		
T.P.	0.47	883.36.	13.33	882.89.
43			11.5	71.9.

889.70

Lt

R

Rt.

Bog, Swamp.

Spt. in 15" O. 35' Rt. 38 + 64

Sta	+	π	-	Elev
-----	---	-------	---	------

883.36

43	+50		11.6	71.8
----	-----	--	------	------

44			11.7	71.7
----	--	--	------	------

	+50		11.7	71.7
--	-----	--	------	------

45			11.8	71.6
----	--	--	------	------

T.P.	13.58	886.79.	10.15	873.21.
------	-------	---------	-------	---------

	+50		15.3	71.5
--	-----	--	------	------

46			15.2	71.6
----	--	--	------	------

	+50		15.2	71.6
--	-----	--	------	------

47			15.1	71.7
----	--	--	------	------

	+50		13.6	73.2
--	-----	--	------	------

48			12.6	74.2
----	--	--	------	------

	+27		10.1	76.7
--	-----	--	------	------

Sta	+	T	-	Elev.
		886.79		
48	+38		8.0	78.8
	+62		6.4	80.4
	+80		5.6	81.2
49			4.9	81.9
	+14		5.4	81.4
	+27		6.5	80.3
	+50		10.5	76.3
	+80		12.8	74.0
50			12.5	74.3
	+14		11.5	75.3
	+38		8.5	78.3
B.M.	7.87	886.86	7.87	878.92
				(878.99)

Top Mont.

Sta.	+	T	-	Elev.
		886.86		
50	+50		7.2	77.7
	+75		3.7	83.2
51			1.6	85.3
	+38		3.4	83.5
T.P.	6.26	885.09	8.03	878.83
	+76		5.3	79.8
52			7.6	77.5
	+35		10.1	75.0
	+70		10.4	74.7
53			11.2	73.9
	+50		10.8	74.3
54			9.3	75.8

Sta	+	π	-	Elev
-----	---	-------	---	------

		885.09		
--	--	--------	--	--

54 +18				
--------	--	--	--	--

			6.9	
--	--	--	-----	--

				78.2
--	--	--	--	------

+42				
-----	--	--	--	--

			3.0	
--	--	--	-----	--

				82.1
--	--	--	--	------

+58.44				
--------	--	--	--	--

			2.0	
--	--	--	-----	--

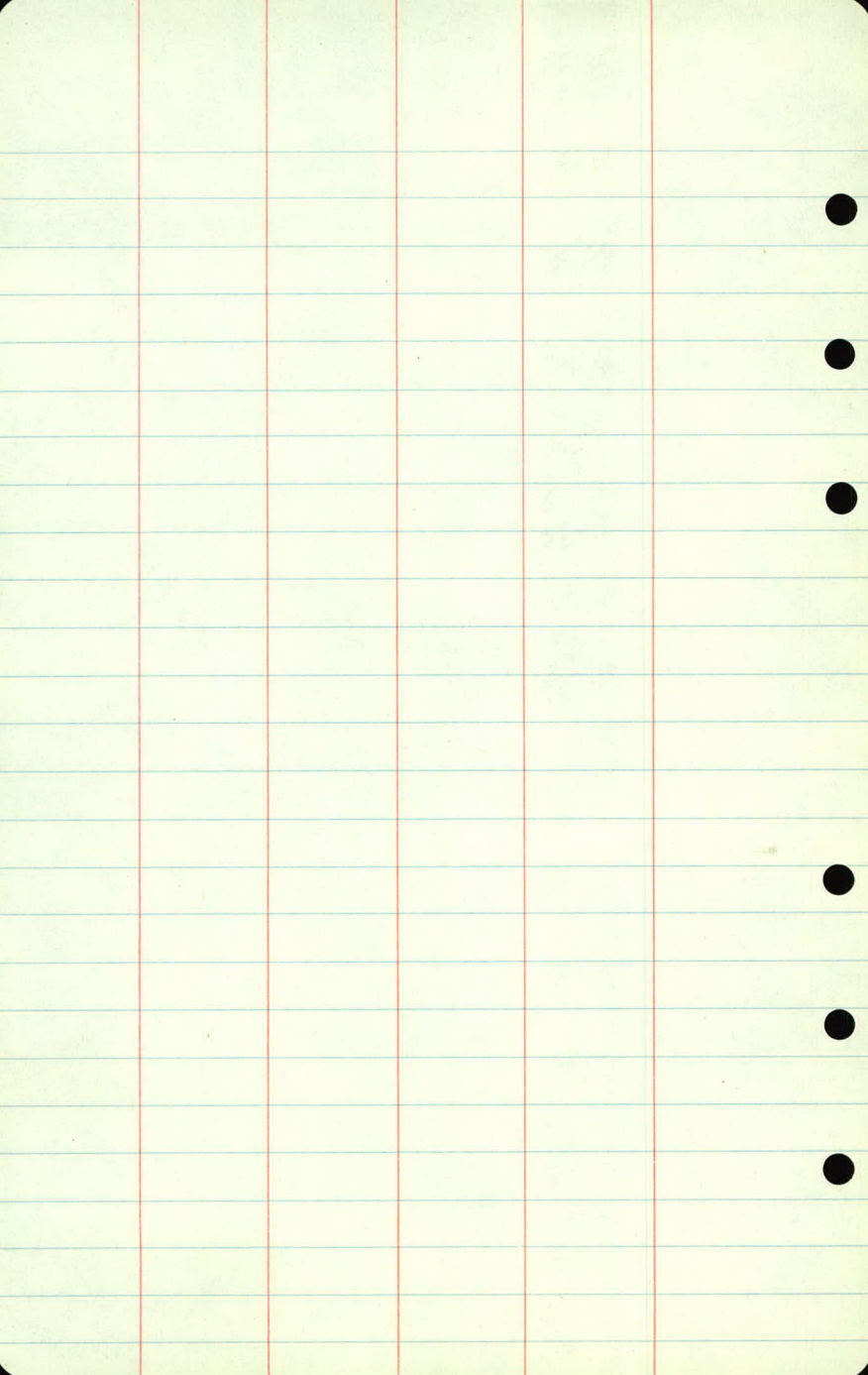
				83.1
--	--	--	--	------

			6.40	
--	--	--	------	--

				878.69
--	--	--	--	--------

				(878.69)
--	--	--	--	----------

219^c Mcnemy St.
Floor Pump Ho.



"A" Line
& Levels.

Sta.	+	π	-	Elev.
B.M.	1.00	951.33. 950.33		950.33

21			5.6	45.7.
----	--	--	-----	-------

+41			2.9	48.4.
-----	--	--	-----	-------

+65			5.1	46.2.
-----	--	--	-----	-------

22			7.1	44.2.
----	--	--	-----	-------

+25			8.5	42.8.
-----	--	--	-----	-------

+50			10.5	40.8.
-----	--	--	------	-------

23			13.4	37.9.
----	--	--	------	-------

+50		940.31	14.6	36.7.
T.P.	2.23	939.31.	13.25	938.08. 937.08.

24			4.2	36.1.
----	--	--	-----	-------

+50			5.5	34.8.
-----	--	--	-----	-------

25			7.0	33.3.
----	--	--	-----	-------

Top S.F. Cor. Conc. Found. 36' Lt. 19477

Sta	+	π	-	Elev.
		940.31 939.31		
25	+50		7.2	33.1
26			6.2	34.1
	+06.52		6.3	34.0
	+2.3		5.2	35.1
	+36.9		4.5	35.8
	+57.4		4.3	36.0
	+72.6		5.4	34.9
	+88.11		6.2	34.1
B.M.	0.50	934.89 934.88	5.91	934.40 933.40
27			2.3	32.6
	+50		8.2	26.7
28			13.4	21.5

(934.38)

W. End of Bridge

E. End Bridge

Sph. in S.E. Cor. Carb. S.E. Cor. Bridge

Sta	+	Σ	-	Elev
		934.88		
28	+50		16.1	18.8
T.P.	0.42	924.82	10.48	924.40

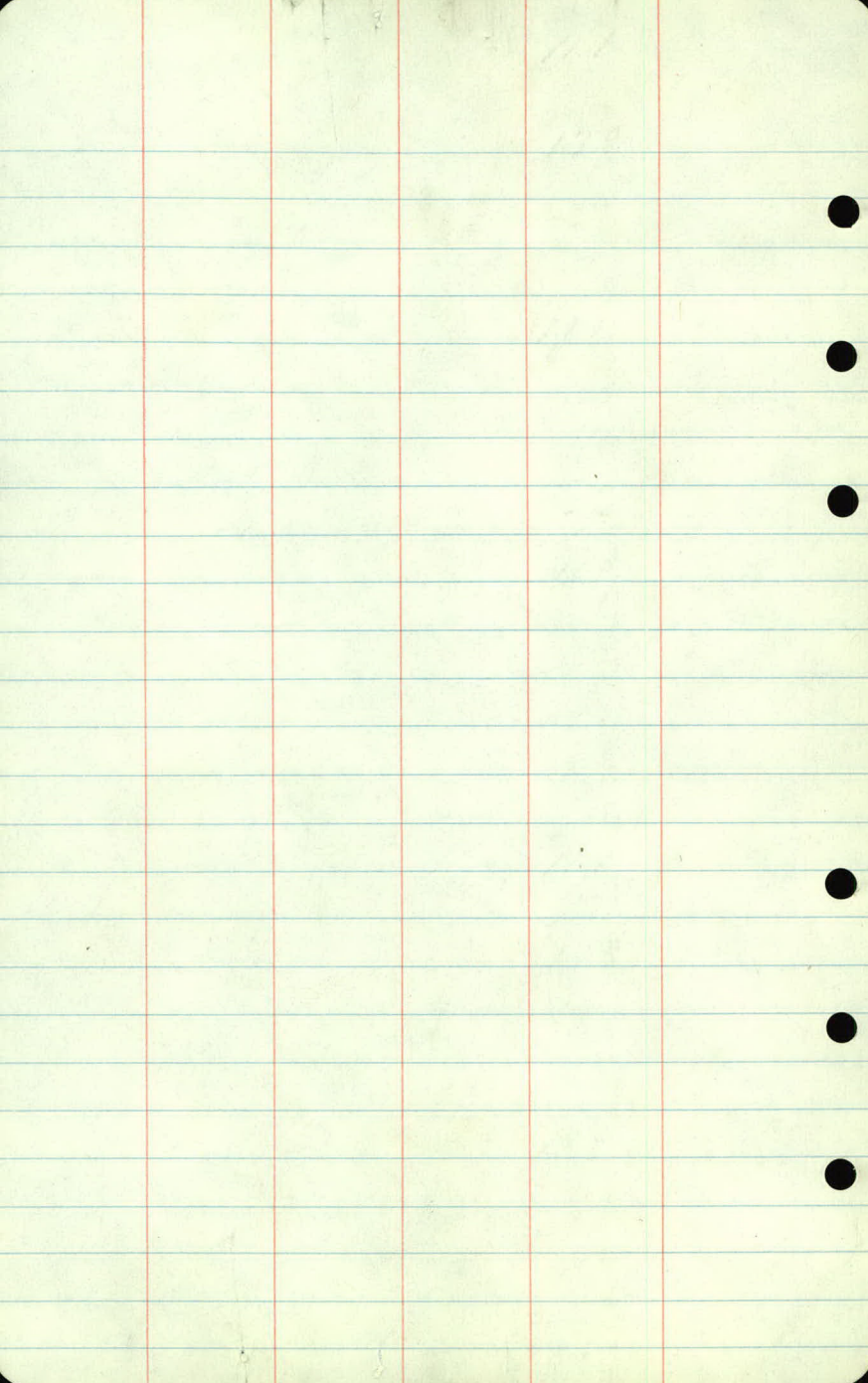
Levels under Bridge

26	+40		13.8	11.0
	+45		12.38	12.44
	+50		12.22	12.60
	+56		13.7	11.1
	+64		7.0	17.8

Int. with cut that runs N. to Ho.

Top W. Rail

Top E. Rail



Slope Stakes

Flower St.

Sta.	+	π	-	Grade	
B.M.	5.24	975.58			(970.34)
0	+00			63.51	
	+31			69.6	
	+60			68.1	
1				68.5	
	+50			67.7	
2				66.9	
	+36			66.3	
	+70			65.8	
3				65.3	
	+50			64.5	
B.M.	6.18	969.69	12.07	963.51	
4	+03			63.7	

$$\begin{array}{r} 963.51 \\ 12.07 \\ \hline 975.58 \\ 5.24 \\ \hline 970.34 \end{array}$$

6-19-40

Gr. Rod.

Lt

£

Rt

Top Mont. Rice & Flower St

26

6.0

$$29.6' / \frac{41}{11.3}$$

$$\frac{6.2}{-0.2}$$

$$\frac{48}{11.2} / 29.4'$$

6.5

$$32.4' / \frac{38}{12.7}$$

$$\frac{3.4}{13.1}$$

$$\frac{57}{10.8} / 28.6'$$

7.1

$$32.0' / \frac{46}{12.5}$$

$$\frac{37}{12.4}$$

$$\frac{58}{11.3} / 29.6'$$

7.9

$$30.2' / \frac{6.3}{11.6}$$

$$\frac{52}{12.7}$$

$$\frac{72}{10.7} / 28.4'$$

8.7

$$28.0' / \frac{82}{10.5}$$

$$\frac{72}{11.5}$$

$$\frac{88}{12.19} / 26.8'$$

9.3

$$26.8' / \frac{94}{12.19}$$

$$\frac{84}{10.9}$$

$$\frac{97}{12.16} / 26'$$

9.8

$$26.4' / \frac{101}{12.17}$$

$$\frac{97}{10.1}$$

$$\frac{107}{12.11} / 25.2'$$

10.3

$$25.8' / \frac{108}{12.14}$$

$$\frac{106}{-0.3}$$

$$\frac{113}{12.10} / 25.0'$$

11.1

$$25.8' / \frac{117}{12.14}$$

$$\frac{116}{-0.6}$$

$$\frac{121}{12.10} / 25.0'$$

Spl. in RR Lt.

6.0

$$26.0' / \frac{65}{12.15}$$

$$\frac{64}{-0.4}$$

$$\frac{71}{12.09} / 24.8'$$

Sta	+	π	-	Grade
		969.69		
4	+32			63.3
	+38			63.2
	+70			63.0
5	Pipe 18" X 34' Long.			62.7
	+50			62.7
6				62.9
	+50			63.3
7				63.7
	+50			64.1
8				64.3
I.P.	2.24	970.06	1.87	967.82
	+50			64.2

Gr. Rod

Lt

R

Rt

6.4

$$26.2' / \frac{6.8}{R16}$$

$$\frac{6.8}{-0.9}$$

$$\frac{7.4}{R210/250'}$$

6.5

$$8.9 / \frac{8.9}{+0.0}$$

$$1.9 / \frac{8.9}{-2.4}$$

$$\frac{6.9}{-0.9}$$

$$\frac{7.2}{R213/256'}$$

6.7

$$28.2' / \frac{8.7}{R20.0}$$

$$\frac{6.7}{-0.9}$$

$$\frac{7.2}{R215/26.0'}$$

7.0

$$\frac{9.8}{R2.644} / \frac{+0.0}{12.476} / \frac{2.6}{2.6}$$

$$2.6 / \frac{9.8}{+0.2}$$

$$2.6 / \frac{9.8}{+0.2}$$

$$\frac{7.1}{R219/26.8'}$$

$$\frac{9.0}{R2.644} / \frac{+3.0}{10.0 \text{ offset}}$$

7.0

$$29.6' / \frac{9.0}{R20.0}$$

$$\frac{6.1}{+0.9}$$

$$\frac{6.1}{+0.9/28.8'}$$

6.8

$$26.4' / \frac{7.1}{R1.7}$$

$$\frac{4.6}{+2.2}$$

$$\frac{5.0}{+1.8/30.6'}$$

6.4

$$27.6' / \frac{6.1}{+0.3}$$

$$\frac{3.5}{+2.9}$$

$$\frac{3.9}{+2.5/32.0'}$$

6.0

$$28.8' / \frac{5.1}{+0.9}$$

$$\frac{3.0}{+3.0}$$

$$\frac{3.6}{+2.4/31.8'}$$

5.6

$$31.6' / \frac{3.3}{+2.3}$$

$$\frac{2.6}{+3.0}$$

$$\frac{3.6}{+2.0/31.0'}$$

5.4

$$33.0' / \frac{2.3}{+2.1}$$

$$\frac{2.2}{+3.2}$$

$$\frac{4.2}{+4.2/29.4'}$$

5.9

$$33.0' / \frac{1.8}{+4.1}$$

$$\frac{2.3}{+3.6}$$

$$\frac{4.9}{+1.0/29.0'}$$

Sta.	+	π	-	Grade		
		970.06				
9				63.7		
+50				62.9		
10				61.9		
+23				61.4	special ditch Lt.	
+60				60.7	Gr Rod	Grade.
T.P.	5.35	962.23	13.18	956.88		
11				59.9	57.9	
+50				59.0	5.7	50.5
12	Place 18" X 48' Corn.	$\frac{+2.0}{90ft sch.}$		58.3	7.0	51.3
+33	Place 18" X 48' Corn.	$\frac{+2.0}{20.5.}$				55.2
+50				57.7	6.9	55.3
13				57.3	6.8	55.4
+50				57.0	6.7	55.5

Flower St

Grade Change

Sta 7+00

Sta	+	X	-	Elev
BM	4.46	967.97		963.51
7+00				63.7

150				64.2
-----	--	--	--	------

8				64.5
---	--	--	--	------

+50				64.5
-----	--	--	--	------

9				64.1	64.0
---	--	--	--	------	------

+50				63.4	63.2
-----	--	--	--	------	------

10				62.5	62.2
----	--	--	--	------	------

T.O	0.45	962.92	5.507	962.47	
-----	------	--------	-------	--------	--

+23				62.1	61.7
-----	--	--	--	------	------

+60				61.4	61.0
-----	--	--	--	------	------

11				60.7	60.3
----	--	--	--	------	------

+50				59.9	59.5
-----	--	--	--	------	------

12				59.3	58.9
----	--	--	--	------	------

Grade Rod.

Lt

±

Rt

4.3

3.8

B.T

B.T

3.5

B.T

B.T

3.5

B.T

B.T

3.9

B.T

B.T

4.6

B.T

B.T

5.5

B.T

Sta

0.7

B.T

B.T

1.9

B.T

B.T

2.2

B.T

B.T

3.4

B.T

B.T

4.0

Sta	+	+	-	Elev	
			96292		
12+50				58.8	58.2
13				58.1	57.7
+50				57.7	57.4
14				57.2	56.8
+27				56.9	56.5
+50				56.5	56.1
15				56.5	55.1
+50				54.2	54.1
T.P.	1.12	955.24	8.80	954.12	
16				53.2	53.0
+32				52.3	52.2
+70				51.4	51.4
17				50.9	

Lt.

A

Rt

4.7

B.T

B.T

5.2

B.T

B.T

5.5

B.T

B.T

6.1

B.T

B.T

6.4

B.T

B.T

6.8

B.T

B.T

7.8

B.T

B.T

8.8

B.T

B.T

BT

2.24

B.T

B.T

3.04

B.T

B.T

3.84

B.T

B.T

4.34

B.T

B.T

Sta	+	π	-	Elev	
		955.24			
17+50				50.1	50.0
18				49.4	49.2
+26				49.1	48.8
+55				48.6	48.3
+80				48.4	48.0
19				48.1	47.7
+30				47.7	47.2
+50				47.4	46.9
+76				47.1	46.5
20				46.8	46.2
+50				46.1	45.4
	0.98	946.36	9.86	945.38	
+84				45.5	44.8

LT

R

RT

5.24 ✓

BT

B.T.

6.04 ✓

BT

BT

6.44 ✓

BT

BT

6.94 ✓

BT

B.T.

7.24 ✓

1 BT

BT

7.54 ✓

1 BT

B.T.

8.04 ✓

BT

BT.

~~8.74~~ 8.34 ✓

13.7

BT

8.74 ✓

BT

BT

9.04 ✓

13.7

13.7

9.84 ✓

BT ✓

13.7 ✓

19.62

Sta	+	π	-	Elev	
		946.36			
21				45.1	44.5
+46				43.2	42.9
+71				42.1	41.9
22				40.3	40.3
+32				38.2	38.1
+71				35.1	34.9
	0.13	935.04	11.45	934.91	
23				32.8	32.6
+24				30.7	30.4
+57				28.3	28.0
+81				26.4	26.1
24				24.9	24.7

RT

~~R~~

RT

1.8L

✓

3.4L

✓

4.4L

✓

6.0L

✓

8.2L

✓

11.4L

✓

2.44

✓

4.64

7.04

Sta	+	π	-	Elev
-----	---	-------	---	------

24+32				22.4	22.2
-------	--	--	--	------	------

+52				20.8	20.7
-----	--	--	--	------	------

+92					
-----	--	--	--	--	--

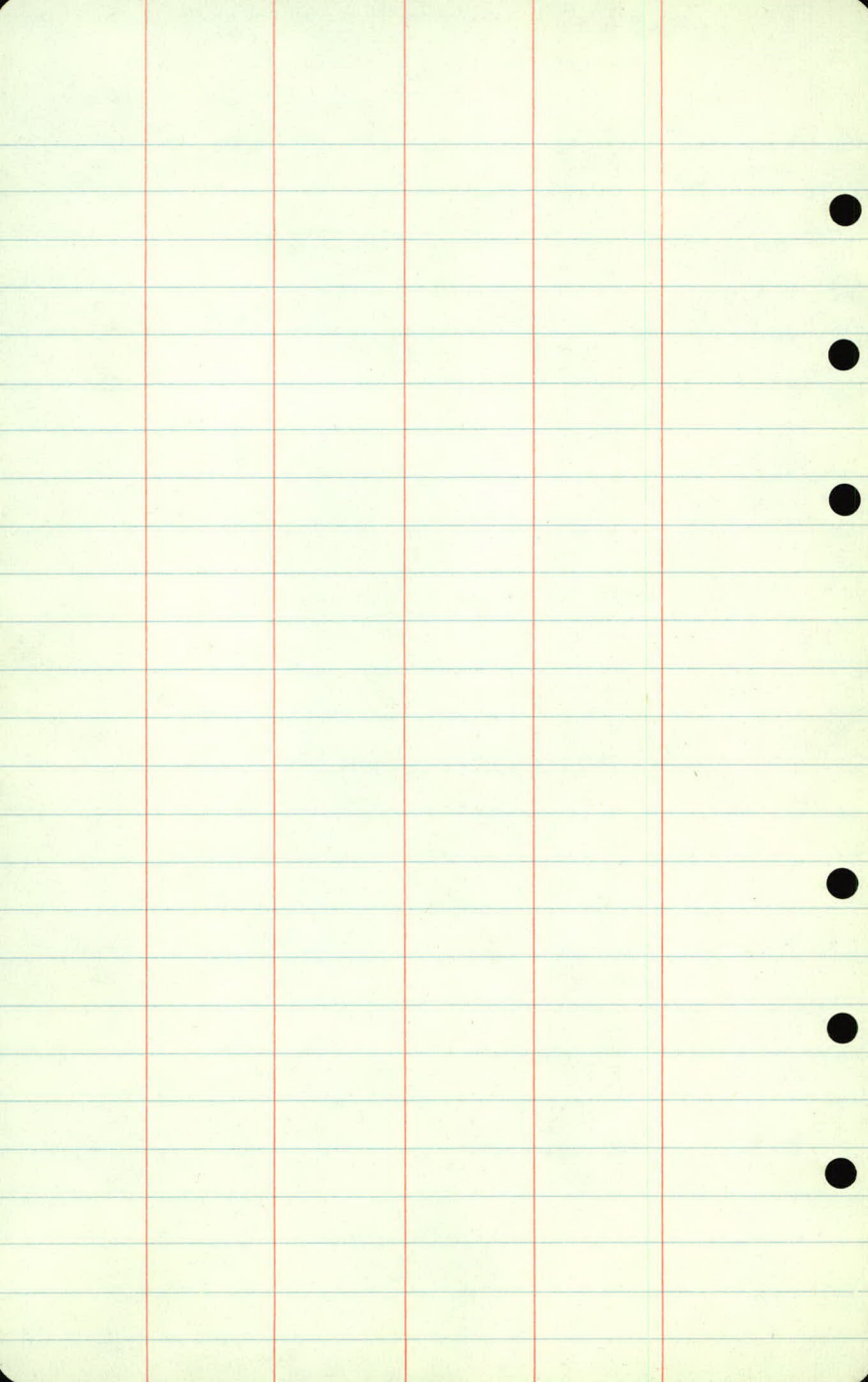
+87					
-----	--	--	--	--	--

25-				17.3	17.3
-----	--	--	--	------	------

LT

✱

RT



Gr. Rod	Lt.	A	Rt.
6.4	$33.0' / \frac{2.1}{+4.3}$	$\frac{27}{+3.7}$	$\frac{54}{+0.280'}$
7.2	$33.0' / \frac{2.6}{+4.6}$	$\frac{35}{+3.7}$	$\frac{6.7}{+0.5/280'}$
8.2	$33.0' / \frac{5.2}{+3.0}$	$\frac{55}{+2.7}$	$\frac{29}{+0.3/276'}$
8.7	$28.0' / \frac{8.2}{+0.5}$	$\frac{48}{+0.9}$	$\frac{8.8}{+0.19/26.8'}$
9.4	$26.4' / \frac{9.1}{+2.17}$	$\frac{14}{-2.0}$	$\frac{12.2}{-2.8/20.6'}$
2.3	$26.0' / \frac{2.8}{+1.5}$	$\frac{5.9}{-3.6}$	$\frac{8.9}{-4.6/28.2'}$
3.2	$25.0' / \frac{1.1}{+1.0}$	$\frac{8.4}{-5.2}$	$\frac{13.3}{-10.1/330'}$
3.9	$25.0' / \frac{5.1}{+2.10}$	$\frac{8.4}{-4.5}$	$\frac{12.3}{-5.4/31.8'}$
4.5	$27.8' / \frac{4.9}{+2.0}$	$\frac{6.4}{-1.9}$	$\frac{10.2}{-5.7/26.4'}$
4.9	$26.6' / \frac{4.9}{+1.9}$	$\frac{5.5}{-0.6}$	$\frac{7.6}{-2.7/20.4'}$
5.2	$25.4' / \frac{5.0}{+1.7}$	$\frac{4.9}{+0.3}$	$\frac{4.9}{+0.3/21.6'}$

+13 = $\frac{1.0}{6.00/230'}$

Sta.	+	π	-	Grade		
		962.23				
14				56.6	6.6	55.6
T.P.	6.89	963.26	5.86	956.37		
+27				56.3	8.4	54.9
+50				56.0	9.0	54.3
15				55.1	10.2	53.1
+50				54.1		
T.P.	0.31	953.89	9.68	953.58		
16				53.0		
+32				52.2		
+70				51.4		
T.P.	8.30	951.65	10.54	949.35		
17	Pl. 18" X 80' G.M.E.I.	54.7 46.2	E140.7 - Lt. 33.8	50.9		
+50				50.0		
18				49.2		

Gr Rod

Lt.

E

Rt.

5.6

21.0

$$\frac{292'}{21.1} \frac{55}{21.1}$$

$$\frac{21}{135}$$

$$\frac{21}{135} \frac{33.0}{33.0}$$

7.0

21.8

$$\frac{244'}{21.3} \frac{71}{21.3}$$

$$\frac{16}{134}$$

$$\frac{31}{139} \frac{33.0}{33.0}$$

7.3

22.4

$$\frac{256'}{21.6} \frac{74}{21.6}$$

$$\frac{17}{156}$$

$$\frac{48}{125} \frac{32.0}{32.0}$$

8.2

$$\frac{318'}{22.4} \frac{58}{22.4}$$

$$\frac{5.0}{13.2}$$

$$\frac{85}{127} \frac{26.4}{26.4}$$

$$+33.2 \frac{8.8}{100} \frac{23.0}{23.0}$$

9.2

$$\frac{250'}{22.0} \frac{10.2}{22.0}$$

$$\frac{8.9}{10.3}$$

$$\frac{12.1}{120.0} \frac{20.8}{20.8}$$

0.9

$$\frac{22.7'}{22.0} \frac{2.9}{22.0}$$

$$\frac{35}{-26}$$

$$\frac{82}{-73} \frac{29.6}{29.6}$$

1.7

$$\frac{214'}{22.2} \frac{4.9}{22.2}$$

$$\frac{6.7}{-50}$$

$$\frac{10.2}{-85} \frac{32.0}{32.0}$$

2.5

$$\frac{22.8'}{22.9} \frac{6.4}{22.9}$$

$$\frac{10.2}{-7.7}$$

$$\frac{18.1}{-15.6} \frac{46.2}{46.2}$$

Top of stake start 17.00

0.8

$$\frac{22.6'}{22.8} \frac{4.6}{22.8}$$

$$\frac{9.2}{-8.3}$$

$$\frac{17.2}{-16.4} \frac{47.8}{47.8}$$

1.7

$$\frac{22.0'}{22.5} \frac{5.2}{22.5}$$

$$\frac{6.9}{-52}$$

$$\frac{14.7}{-100} \frac{35.0}{35.0}$$

2.5

$$\frac{21.2'}{22.0} \frac{2.5}{22.0}$$

$$\frac{6.3}{-38}$$

$$\frac{9.0}{-70} \frac{29.0}{29.0}$$

Sta	+	π	-	Grade	
		951.65			
18	+26			48.8	
T.P.		9.03	958.58	2.10	949.55
	+55			48.3	
	+80			48.0	
19				47.7	
	+30			47.2	
	+50			46.9	
	+76			46.5	
B.M.		0.47	950.80	8.26	950.32 (950.33)
20				46.2	
	+50			45.4	
	+84			44.7	
21				44.3	
T.P.		4.39	950.84	4.35	946.45

Gr. Rod	Lt	R	Rt
			134 $\frac{5.0}{2.04}$ / 18.0
2.9	26.4' $\frac{8.2}{2.17}$	$\frac{33}{-0.4}$	$\frac{6.2}{-33}$ / 21.6
10.3	31.2' $\frac{8.2}{2.1}$	$\frac{74}{+29}$	$\frac{8.2}{+21}$ / 31.2
10.6	32.2' $\frac{8.0}{2.6}$	$\frac{63}{+43}$	$\frac{46}{+6.0}$ / 39.0
10.9	32.3' $\frac{7.7}{2.2}$	$\frac{49}{+6.0}$	$\frac{42}{+6.7}$ / 40.4
11.4	33.0' $\frac{8.4}{2.0}$	$\frac{41}{+6.7}$	$\frac{55}{+9.9}$ / 36.8
11.7	33.0' $\frac{8.5}{2.2}$	$\frac{61}{+5.6}$	$\frac{85}{+32}$ / 33.4
12.1	29.2' $\frac{11.0}{2.1}$	$\frac{11.5}{+0.6}$	$\frac{134}{+20.7}$ / 24.4
Top S.E. Cor. Camp. Found 36.1 ft. 19477			
4.6	27.2' $\frac{1.5}{2.1}$	$\frac{6.4}{-1.8}$	$\frac{81}{-35}$ / 22.0
5.4	26.2' $\frac{5.8}{2.6}$	$\frac{0.7}{-2.3}$	$\frac{8.3}{-29}$ / 2.5
6.1	33.0' $\frac{1.5}{2.6}$	$\frac{5.3}{+9.8}$	$\frac{8.2}{-2.42}$ / 26
6.5	33.0' $\frac{1.3}{2.2}$	$\frac{5.1}{+1.4}$	$\frac{85}{+20.0}$ / 19.4

& stake at P.C.

Sta.	+	π	-	Grade
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		950.84		
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21	+46			42.5
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	+71			41.4
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22				39.7
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	+32			37.6
--	-----	--	--	------

	+71			34.6
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Gr. Rod

Lb

K

Pt.

8.3

$$\frac{32.0/45}{125}$$

$$\frac{21}{16.2}$$

$$\frac{54}{11.9/30.8}$$

9.4

$$\frac{32.0/54}{14.0}$$

$$\frac{14}{18.0}$$

$$\frac{5.0}{14.4/35.8}$$

11.1

$$\frac{32.0/6.5}{14.6}$$

$$\frac{49}{16.2}$$

$$\frac{47}{16.4/39.8}$$

13.2

$$\frac{32.0/27}{14.5}$$

$$\frac{77}{15.5}$$

$$\frac{6.5}{16.7/40.4}$$

16.2

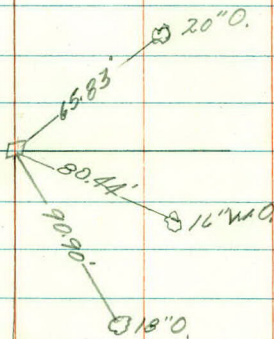
$$\frac{32.0/11.5}{14.7}$$

$$\frac{94}{16.8}$$

$$\frac{73}{18.9/44.8}$$

Ties to Mark

N



Sta	+	π	-	Grade
B.M.	1.01	951.34		950.33
T.P.	0.27	942.05	9.56	941.78

23				32.4
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+26				30.3
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T.P.	2.82	931.64	13.23	928.82
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+57				28.0
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+81				26.1
-----	--	--	--	------

24				24.7
----	--	--	--	------

+32				22.2
-----	--	--	--	------

+52				20.7
-----	--	--	--	------

+62				19.9
-----	--	--	--	------

+87				18.1
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25				17.3
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6-18-40

Gr Rod Lt & Ft.

Top S.E. Cor Conc. Foundation 36' Lt. sta 19+17

Top stake 22+71

$$9.7 \quad \begin{array}{r} 32.4' / 70 \\ +27 \end{array} \quad \begin{array}{r} 64 \\ +6.3 \end{array} \quad \begin{array}{r} 33 \\ +64 / 39.8' \end{array}$$

$$10.8 \quad \begin{array}{r} 30.4' / 71 \\ +17 \end{array} \quad \begin{array}{r} 99 \\ +9.9 \end{array} \quad \begin{array}{r} 90 \\ +19 / 30.6' \end{array}$$

$$3.6 \quad \begin{array}{r} 21.0' / 6.9 \\ -3.3 \end{array} \quad \begin{array}{r} 72 \\ -36 \end{array} \quad \begin{array}{r} 35 \\ +21 / 27.2' \end{array}$$

$$5.5 \quad \begin{array}{r} 23.4' / 9.7 \\ -4.2 \end{array} \quad \begin{array}{r} 10.4 \\ -4.9 \end{array} \quad \begin{array}{r} 55 \\ +20 / 27.0' \end{array}$$

$$6.9 \quad \begin{array}{r} 22.0' / 10.4 \\ -3.5 \end{array} \quad \begin{array}{r} 11.0 \\ -4.1 \end{array} \quad \begin{array}{r} 56 \\ +13 / 29.6' \end{array}$$

$$9.4 \quad \begin{array}{r} 30.8' / 7.5 \\ +1.9 \end{array} \quad \begin{array}{r} 11.8 \\ -2.4 \end{array} \quad \begin{array}{r} 6.9 \\ +25 / 32.0' \end{array}$$

$$10.9 \quad \begin{array}{r} 33.0' / 7.4 \\ +3.5 \end{array} \quad \begin{array}{r} 11.4 \\ -0.5 \end{array} \quad \begin{array}{r} 5.1 \\ +58 / 38.6' \end{array}$$

$$11.7 \quad \begin{array}{r} 33.0' / 7.7 \\ +4.0 \end{array} \quad \begin{array}{r} 10.9 \\ +0.8 \end{array} \quad \begin{array}{r} 36 \\ +81 / 43.2' \end{array}$$

$$13.5 \quad \begin{array}{r} 33.0' / 9.7 \\ +3.8 \end{array} \quad \begin{array}{r} 8.4 \\ +5.7 \end{array} \quad \begin{array}{r} 2.0 \\ +11.5 / 50.0' \end{array}$$

$$14.3 \quad \begin{array}{r} 33.0' / 11.3 \\ +2.0 \end{array} \quad \begin{array}{r} 7.5 \\ +6.8 \end{array} \quad \begin{array}{r} 2.8 \\ +11.5 / 50.0' \end{array}$$

Sta	+	π	-	Grade
		931.64		
25	+26			15.8
T.P.	5.94	926.19	11.39	920.25
	+58			141
	+76			133
26				12.4
T.P.	1.23	914.41	13.01	913.18
	+24			11.6
	+38			11.3
	+42			11.2
		+30		
	+47	= End New 18" Conc. Lt. Elev 907.00		11.0
	+55			10.9
		+30		
	+62	= End New 18" Conc. Lt. = Elev 902.00		10.8
T.P.	4.12	914.10	4.43	909.98
		Culv 252' Lt. (+30)		
	+77	End Culv Lt. = Elev 906.70		10.8
		Ditch 1 To Grade Lt.		

$$11.1 = 3.3$$

$$\begin{array}{r} 5.30 \\ 2.1 \\ \hline 7.9 \end{array} \quad \begin{array}{r} 6-18-40 \\ 3.27 \\ \hline 1.03 \end{array}$$

Gr. Rod

Lt

R

Rt

$$15.8 \quad \begin{array}{r} 33.0' / 11.4 \\ \hline 14.4 \end{array} \quad \begin{array}{r} 70 \\ \hline 188 \end{array} \quad \begin{array}{r} 5.8 \\ \hline 110.0 / 47.0' \end{array}$$

$$12.1 \quad \begin{array}{r} 31.8' / 9.7 \\ \hline 12.4 \end{array} \quad \begin{array}{r} 40 \\ \hline 181 \end{array} \quad \begin{array}{r} 0.5 \\ \hline 111.6 / 50.2' \end{array}$$

$$12.9 \quad \begin{array}{r} 29.6' / 11.6 \\ \hline 11.3 \end{array} \quad \begin{array}{r} 60 \\ \hline 169 \end{array} \quad \begin{array}{r} 0.8 \\ \hline 112.1 / 51.2' \end{array}$$

$$13.8 \quad \begin{array}{r} 27.2' / 13.7 \\ \hline 10.1 \end{array} \quad \begin{array}{r} 10.5 \\ \hline 133 \end{array} \quad \begin{array}{r} 4.2 \\ \hline 19.6 / 46.2' \end{array}$$

$$2.8 \quad \begin{array}{l} \text{Ditch} \\ 2.0 \\ \text{Deep} \end{array} \quad \begin{array}{r} 25.0' / 3.8 \\ \hline 12.10 \end{array} \quad \begin{array}{r} 46 \\ \hline -1.8 \end{array} \quad \begin{array}{r} 0.4 \\ \hline 12.4 / 31.8' \end{array}$$

$$3.1 \quad \begin{array}{l} \text{Ditch} \\ 3.1' \\ \text{Deep} \end{array} \quad \begin{array}{r} 34.6' / 1.7 \\ \hline 12.47 \end{array}$$

$$3.2 \quad \begin{array}{l} \text{Ditch} \\ 3.4' \\ \text{Deep} \end{array} \quad \begin{array}{r} 6.6 \\ \hline 12.00 / 25.8' \end{array} \quad \begin{array}{l} \text{Ditch} \\ 3.4' \\ \text{Deep} \end{array}$$

$$3.4 \quad \begin{array}{l} \text{Ditch} \\ 4.0' \\ \text{Deep} \end{array} \quad \text{Culv 25 Lt,}$$

$$3.5 \quad \begin{array}{r} 3.6 \\ \hline 12.35 / 33.2' \end{array} \quad \begin{array}{l} \text{Ditch} \\ 3.6' \\ \text{Deep} \end{array}$$

$$3.6 \quad \text{Culv. 24.6 Lt,} \quad \begin{array}{l} \text{Ditch} \\ 3.8' \\ \text{Deep} \end{array}$$

$$3.3 \quad \begin{array}{l} \text{Ditch} \\ 4.1' \\ \text{Deep} \end{array} \quad \begin{array}{r} 33.8' / 9.1 \\ \hline 12.33 \end{array} \quad \begin{array}{r} 18.4 / 4.9 \\ \hline -1.6 \end{array} \quad \begin{array}{r} 47 \\ \hline 14 \end{array}$$

Sta.	+	π	-	Grade.
		914.10		
		CULV 26.4' RT +20		
26	+92	End Culv. $PI = E/10 \times 906.0$		10.7
27				10.6
	+25			09.9
	+52			08.6
	+80			06.7
T.P.	2.58	904.23	12.45	901.65
28				05.0
	+50			900.2
T.P.	2.58	899.18	12.63	891.60
29				895.9
	+50			92.3
30				89.5
	+35			88.0
	+49	Place 18" x 48' C.M.		87.5

6-17-40

Gr. Rod

L^t

K

R^t

3.4

$$\frac{52}{-18} \frac{49}{-15} / 100'$$

 Dike
4.7'
Deep

3.5

 Dike
4.0'
Deep

$$\frac{44}{-14} \frac{38}{R.3.7}$$

$$\frac{58}{-23}$$

$$\frac{11.3}{-75} / 30.6'$$

4.2

 Dike
3.5'
Deep

$$27.2' / \frac{7.1}{R.0.6}$$

$$\frac{8.2}{-40}$$

$$\frac{7.8}{-3.6} / 22.2'$$

5.5

 Dike
2.5'
Deep

$$24.4' / \frac{7.8}{R.0.2}$$

$$\frac{9.3}{-3.8}$$

$$\frac{9.9}{-4.4} / 23.8'$$

7.4

$$21.2' / \frac{10.5}{-3.1}$$

$$\frac{18.2}{-5.8}$$

$$\frac{19.8}{-7.4} / 29.8'$$

-0.8

$$23.2' / \frac{3.3}{-9.1}$$

$$\frac{6.4}{-7.2}$$

$$\frac{8.4}{-9.2} / 33.0'$$

4.0

$$33.0' / \frac{13.1}{-9.1}$$

$$\frac{13.1}{-9.1}$$

$$\frac{13.1}{-9.1} / 33.0'$$

-1.7

$$33.0' / \frac{8.7}{-10.4}$$

$$\frac{6.6}{-9.3}$$

$$\frac{5.5}{-7.2} / 29.4'$$

1.9

$$32.8' / \frac{10.8}{-8.9}$$

$$\frac{9.1}{-7.2}$$

$$\frac{4.9}{-3.0} / 21.0'$$

$$+55 \frac{4.3}{R.0.0} / 2.0$$

4.7

$$25.0' / \frac{9.7}{-5.0}$$

$$\frac{7.6}{-2.9}$$

$$\frac{2.4}{-2.3} / 31.6'$$

$$+30 \frac{1.8}{R.0.0} / 2.0$$

6.2

$$24.8' / \frac{11.1}{-4.9}$$

$$\frac{10.3}{-4.1}$$

$$\frac{9.8}{-2.8} / 20.6'$$

$$\text{Culv Elev } \frac{82.3}{24'}$$

$$\text{Culv Elev } \frac{82.0}{24'}$$

Sta	+	π	-	Grade
		894.18		

30	+67			86.9
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I.P.	4.24	887.24	11.18	883.00
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31				86.2
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	+50			85.7
--	-----	--	--	------

	+85			85.6
--	-----	--	--	------

32				85.6
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	+48			85.4
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B.M.			0.92	886.32
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I.P.	12.30	899.05	0.49	886.75
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I.P.	13.79	910.51	2.33	896.72
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I.P.	11.53	921.34	0.70	909.81
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I.P.	13.45	934.71	0.08	921.26
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B.M.			0.34	924.37
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934.38

Gr. Rod

Lt

R

Rt

7.3

$$20.6' / \frac{10.1}{-2.8}$$

$$\frac{11}{-4.4}$$

$$\frac{12.3}{-5.0} / 25.0'$$

1.0

$$19.6' / \frac{3.3}{-2.3}$$

$$\frac{4.9}{-3.9}$$

$$\frac{6.4}{-5.4} / 25.6'$$

1.5

$$21.6' / \frac{4.8}{-3.3}$$

$$\frac{5.9}{-4.4}$$

$$\frac{7.8}{-6.3} / 27.6'$$

1.6

$$22.0' / \frac{5.1}{-3.5}$$

$$\frac{5.8}{-4.2}$$

$$\frac{7.9}{-6.3} / 27.6'$$

1.6

$$18.4' / \frac{3.3}{-1.9}$$

$$\frac{3.8}{-1.2}$$

$$\frac{7.5}{-5.9} / 26.8'$$

1.8

$$17.0' / \frac{2.8}{-1.0}$$

$$\frac{3.4}{-1.6}$$

$$\frac{5.0}{-3.2} / 21.4'$$

Spt. in 15° O. 40' Lt. 30' 165'

Spt. in S.E. Curb S.E. Cor. E.R. Bridge

