

D-12 + B 26

Dr. 12A - Bk. 26

OFFICE OF COUNTY ENGINEER  
RAMSEY CO. MINN.

PLAN Survey

KENNARD ST.

From LARPENTEUR Co. FROST AVE'S.

Road Acc't. No. N-47

Date Filed. 12-28-38

File

1  
Kennard Street

New Canada Township Sec. 14

Bratager

Wilke

Moeschler.

6/38

Plan Survey

Angle.

Sta. Point Lt. Rt.

6+01.93 P.O.T.

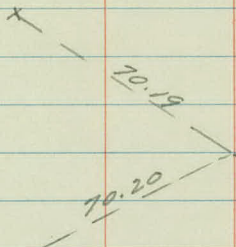
0+94.87 P.O.T.

0+00 P.O.T.

# Reference Points

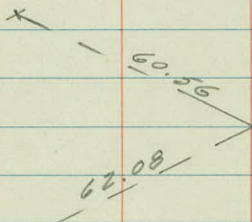
2/

Hub



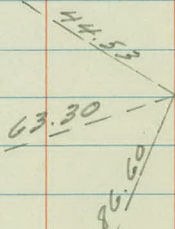
Hub.

Hub.



Hub.

Gen. R.I. Post.



Stone Monument.  
1/4 Cor.

Guy Pole.

Power Pole.



Angle.

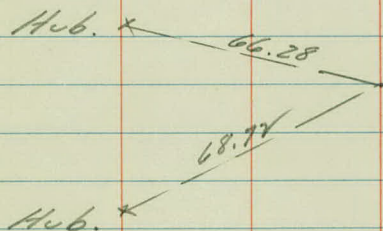
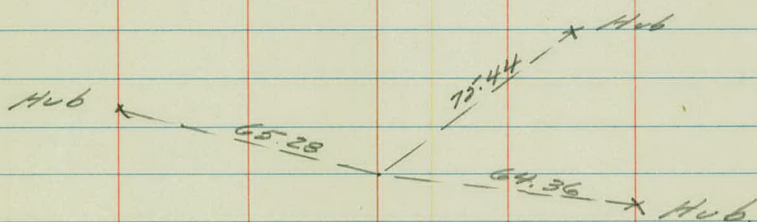
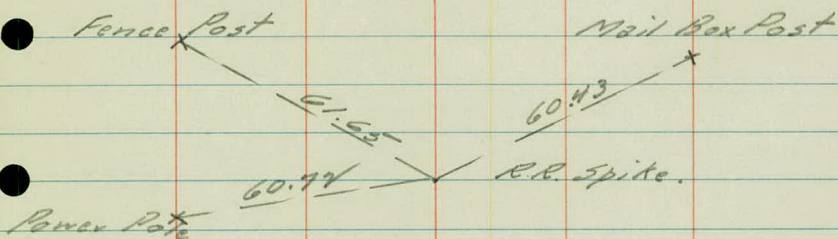
Sta. Point Lt. Rt.

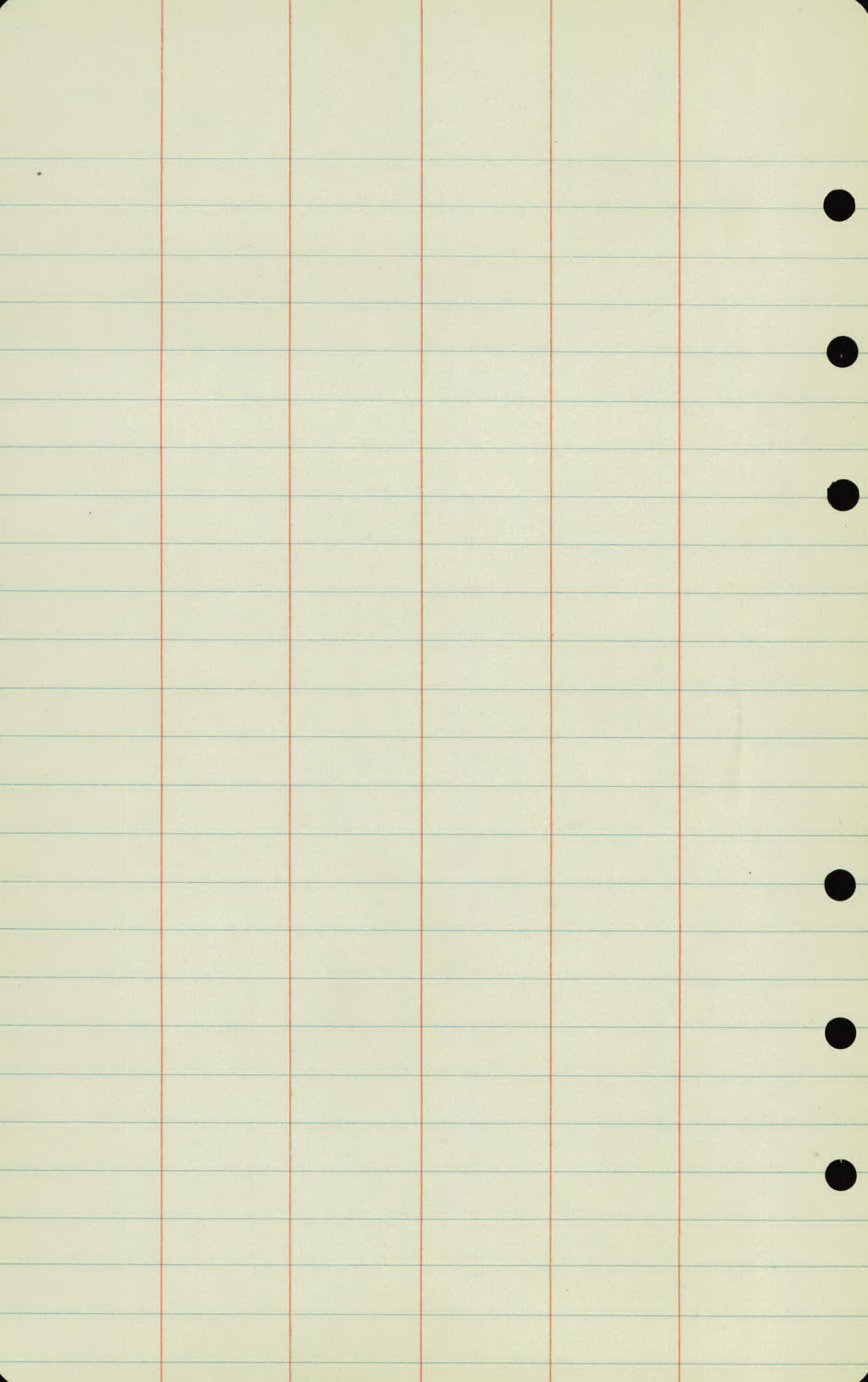
26+28.04 P.O.T.

23+00 P.O.T.

10+31.77 P.O.T.

# Reference Points





North ↑

Frost

Avenue

[2652.72]

Record.

2653.14

Measured

Stone Mon.

Stone Mon.

1326.57

1326.57

Sta. 26+28.04

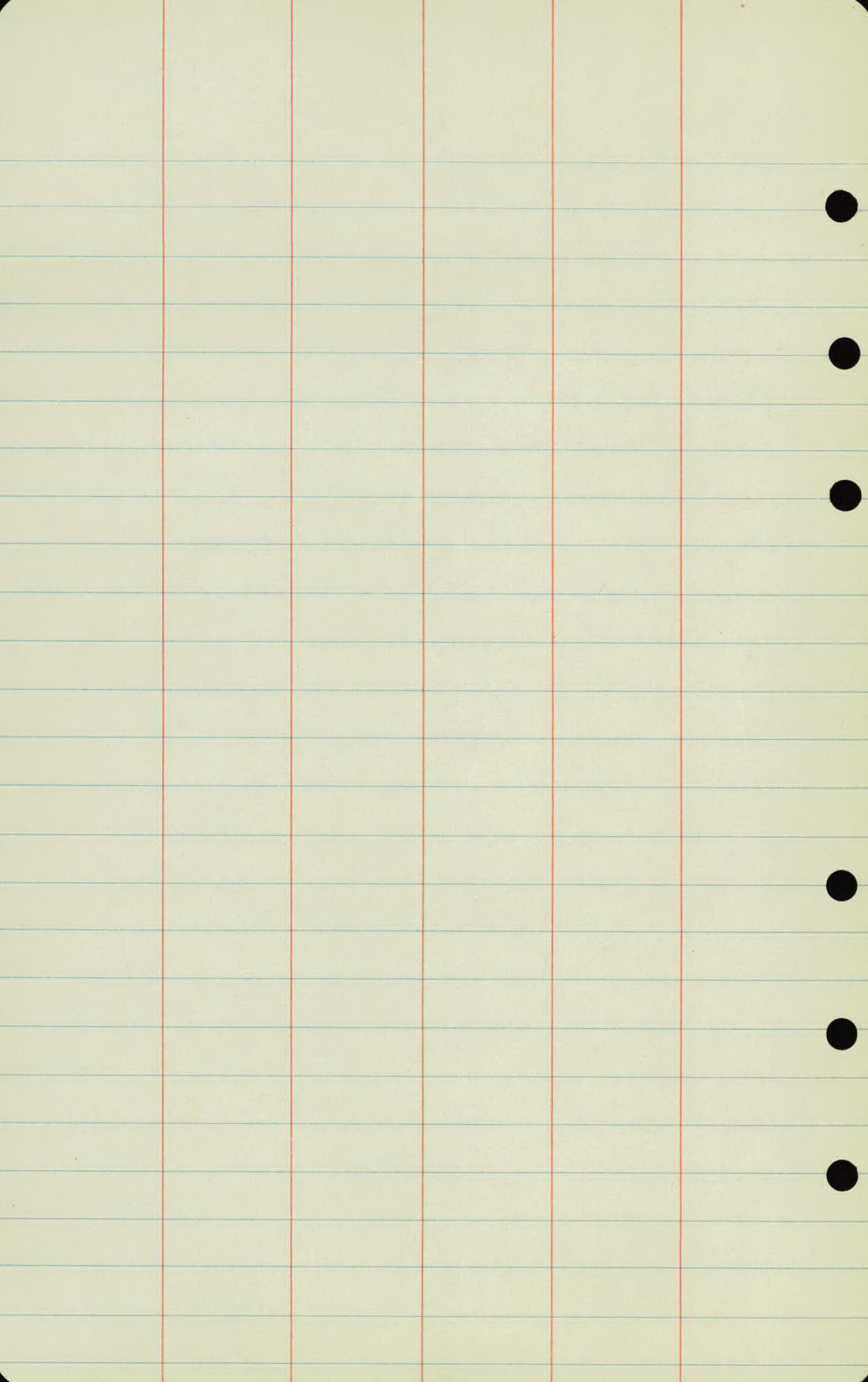
89035'

Kennard St.

Sta. 0+00

Stone Mon. 1/4 Cor.

Larpen Ave.





Topography.

12

10

8

6

4

2

0+00

Posture

1/2 Foss  
Plotted Property

3 B.W. Fencing →  
1" L Iron Posts.

0+50

0+11 Edge Black Top.

Carpenter. Are. 20' Black top.

23

21

19

18

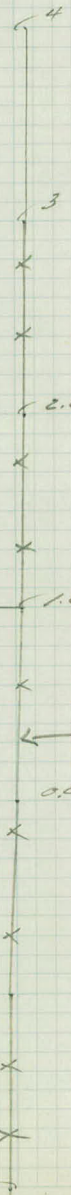
16

14

12

Posters

Posters



Plotted Property

Grass

38 W. Fencing  
1" Iron Posts

1/2



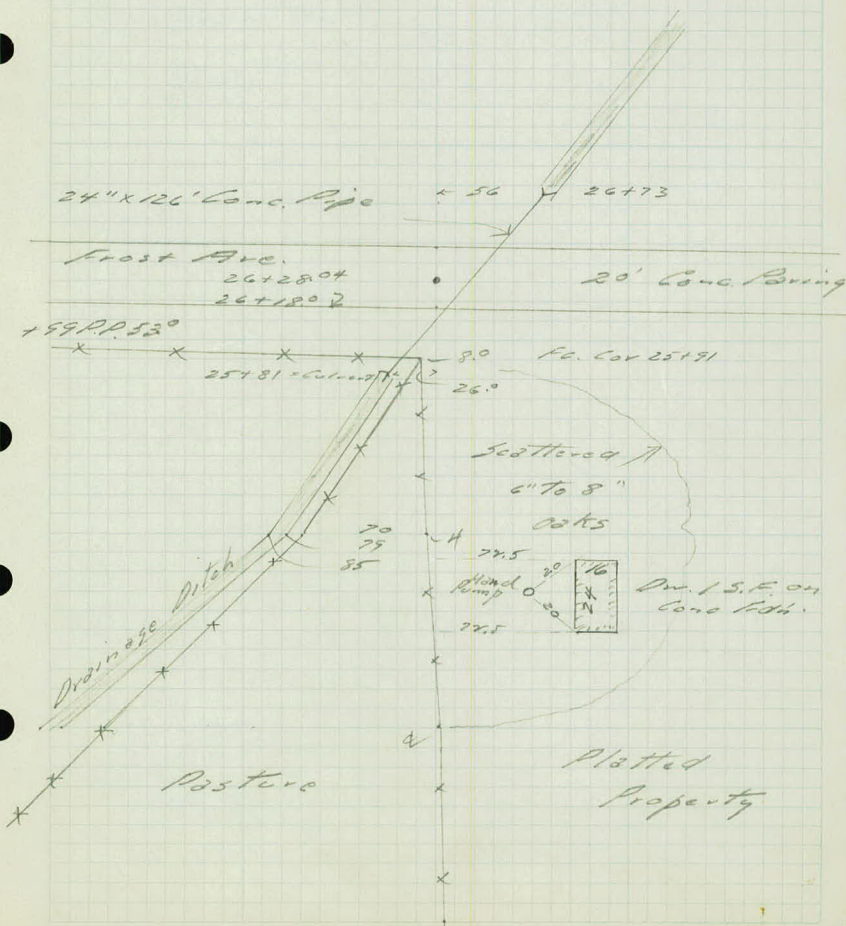


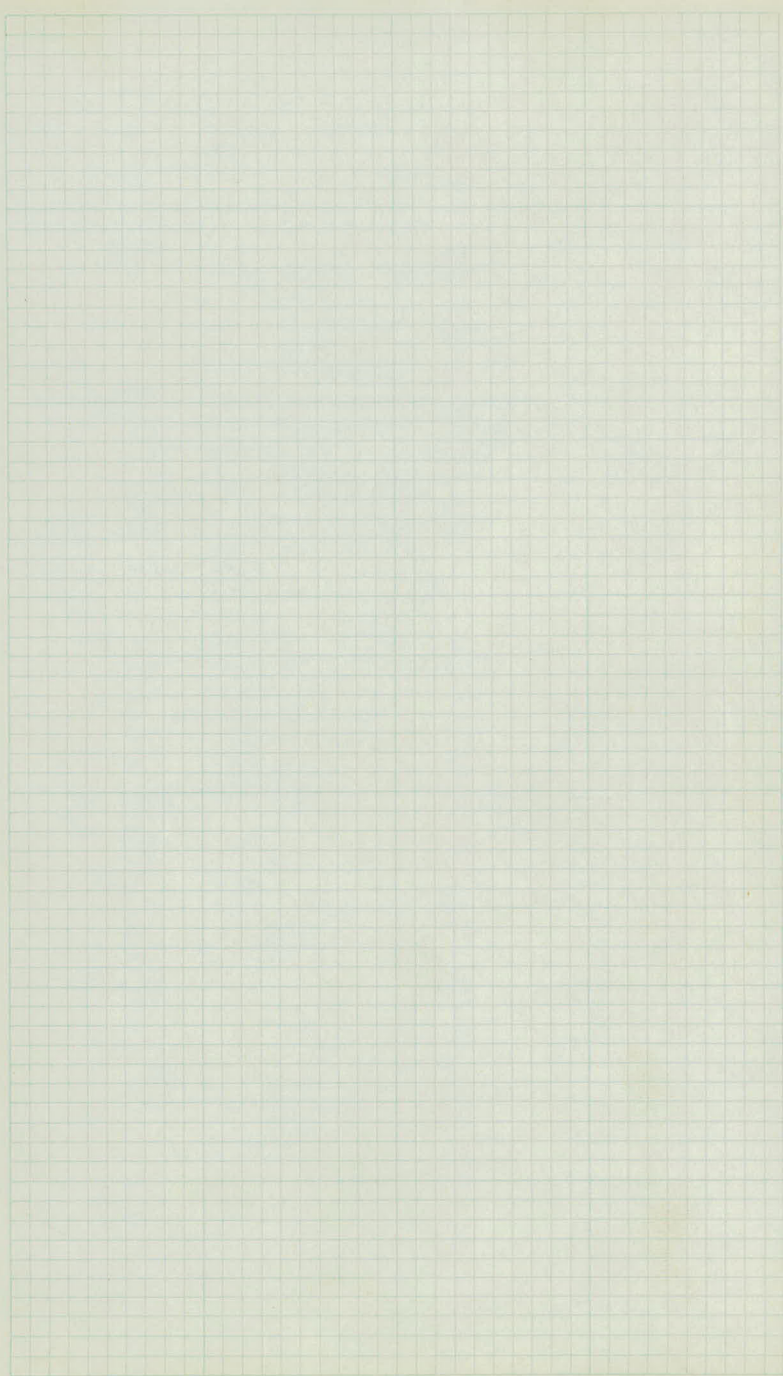
26

25

24

23





Preliminary Cross Sections.  
Kennard St.

| Sta. | +    | Σ        | -     | Elev.    |
|------|------|----------|-------|----------|
| B.M. | 0.93 | 955.01 ✓ |       | 954.08 ✓ |
| T.P. | 0.45 | 944.16 ✓ | 13.30 | 941.71 ✓ |
| B.M. | 7.80 | 944.16 ✓ | 7.80  | 934.36 ✓ |

0+00 933.6

0+15 33.8

0+20 30.8

0+23 30.8 ✓

T.P. 10.71 951.61 ✓ 1.26 940.90 ✓

0+45 42.5

1 47.6 ✓

T.P. 9.75 960.75 ✓ 0.61 951.00 ✓

+50 51.3

2 53.8

150 53.5

3 53.8

T.P. 11.21 967.51 ✓ 4.44 956.31 ✓



Lt.

E

Rt

Spike in P.P. N.W. Cor. Flandreau &  
Lorpen Tour Arès

Spike in P.P. Prosperity - Lorpen Tour & Kennard Sts

$$\frac{130}{100} \quad \frac{107}{50} \quad \frac{86}{50} \quad \frac{63}{50} \quad \frac{46}{100}$$

$$\frac{135}{100} \quad \frac{112}{50} \quad \frac{84}{50} \quad \frac{65}{50} \quad \frac{46}{100}$$

$$\frac{165}{100} \quad \frac{142}{50} \quad \frac{114}{50} \quad \frac{95}{50} \quad \frac{76}{100}$$

$$\frac{165}{100} \quad \frac{142}{50} \quad \frac{114}{50} \quad \frac{95}{50} \quad \frac{76}{100}$$

$$\frac{169}{100} \quad \frac{133}{50} \quad \frac{91}{50} \quad \frac{67}{40} \quad \frac{73}{50} \quad \frac{58}{100}$$

$$\frac{130}{100} \quad \frac{82}{65} \quad \frac{71}{50} \quad \frac{40}{50} \quad \frac{19}{50} \quad \frac{0.0}{90} \quad \frac{+05}{100}$$

$$\frac{210}{100} \quad \frac{180}{85} \quad \frac{137}{50} \quad \frac{112}{27} \quad \frac{99}{5} \quad \frac{95}{50} \quad \frac{71}{50} \quad \frac{55}{80} \quad \frac{49}{100}$$

$$\frac{169}{100} \quad \frac{170}{50} \quad \frac{104}{35} \quad \frac{75}{50} \quad \frac{70}{50} \quad \frac{46}{50} \quad \frac{33}{100}$$

$$\frac{127}{100} \quad \frac{112}{44} \quad \frac{73}{50} \quad \frac{36}{50} \quad \frac{17}{100}$$

$$\frac{78}{100} \quad \frac{73}{50} \quad \frac{78}{31} \quad \frac{70}{50} \quad \frac{53}{27} \quad \frac{30}{50} \quad \frac{00}{100}$$

| Sta. | +     | $\pi$    | -    | Elev.    |
|------|-------|----------|------|----------|
|      |       | 967.54   |      |          |
| 3+50 |       |          |      | 955.5    |
| 4    |       |          |      | 58.2     |
| T.P. | 11.84 | 977.17 ✓ | 2.24 | 965.78 ✓ |
| +50  |       |          |      | 64.6     |
| 5    |       |          |      | 70.6     |
| +50  |       |          |      | 71.6     |
| 6    |       |          |      | 72.4     |
| +50  |       |          |      | 73.2     |
| 7    |       |          |      | 72.4     |
| +50  |       |          |      | 72.6     |
| 8    |       |          |      | 72.4     |
| B.M. | 2.41  | 977.17 ✓ | 2.41 | 974.71 ✓ |
| +50  |       |          |      | 72.1     |
| T.P. | 6.08  | 978.97 ✓ | 4.73 | 972.89 ✓ |

Lt.

E

Rt.

$$\frac{107}{100}$$

$$\frac{114}{50}$$

$$\frac{123}{30}$$

$$\frac{170}{/}$$

$$\frac{58}{38}$$

$$\frac{47}{100}$$

$$\frac{76}{100}$$

$$\frac{71}{50}$$

$$\frac{89}{28}$$

$$\frac{93}{/}$$

$$\frac{83}{25}$$

$$\frac{58}{50}$$

$$\frac{25}{100}$$

$$\frac{133}{50}$$

$$\frac{115}{50}$$

$$\frac{123}{27}$$

$$\frac{125}{/}$$

$$\frac{122}{20}$$

$$\frac{95}{50}$$

$$\frac{65}{100}$$

$$\frac{93}{100}$$

$$\frac{75}{50}$$

$$\frac{65}{/}$$

$$\frac{51}{50}$$

$$\frac{37}{100}$$

$$\frac{58}{50}$$

$$\frac{55}{/}$$

$$\frac{45}{50}$$

$$\frac{47}{50}$$

$$\frac{47}{/}$$

$$\frac{52}{50}$$

$$\frac{38}{50}$$

$$\frac{43}{32}$$

$$\frac{39}{/}$$

$$\frac{43}{5}$$

$$\frac{49}{50}$$

$$\frac{40}{50}$$

$$\frac{47}{/}$$

$$\frac{53}{50}$$

$$\frac{51}{50}$$

$$\frac{45}{25}$$

$$\frac{45}{/}$$

$$\frac{41}{50}$$

$$\frac{71}{50}$$

$$\frac{66}{30}$$

$$\frac{47}{/}$$

$$\frac{27}{50}$$

Spike in Fence Post 300' Rt. Sta. 7+75

$$\frac{50}{50}$$

$$\frac{31}{31}$$

$$\frac{50}{/}$$

$$\frac{28}{50}$$

| Sts. | + | $\pi$ ✓ | - | Elc. |
|------|---|---------|---|------|
|      |   | 978.97  |   |      |

|        |  |  |  |       |
|--------|--|--|--|-------|
| 9 + 00 |  |  |  | 972.4 |
|--------|--|--|--|-------|

|     |  |  |  |      |
|-----|--|--|--|------|
| +50 |  |  |  | 71.3 |
|-----|--|--|--|------|

|         |  |  |  |      |
|---------|--|--|--|------|
| 10 + 00 |  |  |  | 20.8 |
|---------|--|--|--|------|

|     |  |  |  |      |
|-----|--|--|--|------|
| +50 |  |  |  | 68.9 |
|-----|--|--|--|------|

|    |  |  |  |      |
|----|--|--|--|------|
| 11 |  |  |  | 65.9 |
|----|--|--|--|------|

|      |      |          |       |          |
|------|------|----------|-------|----------|
| T.P. | 2.23 | 968.55 ✓ | 12.65 | 966.32 ✓ |
|------|------|----------|-------|----------|

|     |  |  |  |      |
|-----|--|--|--|------|
| +50 |  |  |  | 63.5 |
|-----|--|--|--|------|

|    |  |  |  |      |
|----|--|--|--|------|
| 12 |  |  |  | 60.6 |
|----|--|--|--|------|

|     |  |  |  |      |
|-----|--|--|--|------|
| +50 |  |  |  | 58.0 |
|-----|--|--|--|------|

|    |  |  |  |      |
|----|--|--|--|------|
| 13 |  |  |  | 55.9 |
|----|--|--|--|------|

|      |      |          |       |          |
|------|------|----------|-------|----------|
| T.P. | 3.39 | 958.63 ✓ | 13.31 | 955.24 ✓ |
|------|------|----------|-------|----------|

|     |  |  |  |      |
|-----|--|--|--|------|
| +50 |  |  |  | 54.5 |
|-----|--|--|--|------|

|    |  |  |  |      |
|----|--|--|--|------|
| 14 |  |  |  | 51.7 |
|----|--|--|--|------|

|     |  |  |  |      |
|-----|--|--|--|------|
| +50 |  |  |  | 46.8 |
|-----|--|--|--|------|

Lt.

E

Rt.

$$\frac{126}{50}$$

$$\frac{117}{33}$$

$$\frac{66}{/}$$

$$\frac{23}{50}$$

$$\frac{140}{50}$$

$$\frac{77}{/}$$

$$\frac{32}{50}$$

$$\frac{138}{50}$$

$$\frac{125}{33}$$

$$\frac{52}{3}$$

$$\frac{82}{/}$$

$$\frac{47}{80}$$

$$\frac{150}{50}$$

$$\frac{128}{27}$$

$$\frac{101}{/}$$

$$\frac{69}{50}$$

$$\frac{180}{50}$$

$$\frac{166}{33}$$

$$\frac{142}{8}$$

$$\frac{131}{/}$$

$$\frac{100}{80}$$

$$\frac{82}{50}$$

$$\frac{76}{34}$$

$$\frac{51}{/}$$

$$\frac{43}{9}$$

$$\frac{23}{50}$$

$$\frac{95}{50}$$

$$\frac{99}{32}$$

$$\frac{80}{/}$$

$$\frac{71}{18}$$

$$\frac{48}{50}$$

$$\frac{133}{50}$$

$$\frac{129}{33}$$

$$\frac{106}{/}$$

$$\frac{100}{16}$$

$$\frac{79}{50}$$

$$\frac{157}{50}$$

$$\frac{127}{/}$$

$$\frac{120}{12}$$

$$\frac{95}{50}$$

$$\frac{89}{60}$$

$$\frac{60}{19}$$

$$\frac{41}{/}$$

$$\frac{34}{8}$$

$$\frac{12}{50}$$

$$\frac{126}{50}$$

$$\frac{101}{24}$$

$$\frac{78}{5}$$

$$\frac{71}{4}$$

$$\frac{69}{/}$$

$$\frac{65}{14}$$

$$\frac{51}{50}$$

$$\frac{122}{50}$$

$$\frac{145}{16}$$

$$\frac{150}{6}$$

$$\frac{118}{/}$$

$$\frac{104}{17}$$

$$\frac{85}{50}$$



| Sta. | +    | $\pi$    | -     | Elev.    |
|------|------|----------|-------|----------|
|      |      | 958.63 ✓ |       |          |
| B.M. | 4.03 | 958.63 ✓ | 4.03  | 954.60 ✓ |
| T.P. | 2.35 | 948.03 ✓ | 17.95 | 945.68 ✓ |
| +100 |      |          |       | 43.7     |
| +50  |      |          |       | 42.9     |
| 16   |      |          |       | 42.5     |
| +50  |      |          |       | 41.2     |
| 17   |      |          |       | 36.4 ✓   |
| T.P. | 4.22 | 939.56 ✓ | 17.69 | 935.34 ✓ |
| +50  |      |          |       | 33.8     |
| 18   |      |          |       | 30.5     |
| +10  |      |          |       | 30.1     |
| +50  |      |          |       | 28.9     |
| 19   |      |          |       | 25.8 ✓   |
| T.P. | 4.25 | 930.55 ✓ | 13.26 | 926.30 ✓ |

Lt.

Z

Rt.

Spike in P.P. 300' Rt. Sta. 16 + 60

$$\begin{array}{r} 76 \\ 50 \end{array} \quad \begin{array}{r} 54 \\ 18 \end{array} \quad \begin{array}{r} 43 \\ \hline \end{array} \quad \begin{array}{r} 32 \\ 6 \end{array} \quad \begin{array}{r} 16 \\ 20 \end{array}$$

$$\begin{array}{r} 78 \\ 50 \end{array} \quad \begin{array}{r} 66 \\ 26 \end{array} \quad \begin{array}{r} 51 \\ \hline \end{array} \quad \begin{array}{r} 44 \\ 5 \end{array} \quad \begin{array}{r} 35 \\ 50 \end{array}$$

$$\begin{array}{r} 76 \\ 50 \end{array} \quad \begin{array}{r} 88 \\ 41 \end{array} \quad \begin{array}{r} 63 \\ 14 \end{array} \quad \begin{array}{r} 55 \\ \hline \end{array} \quad \begin{array}{r} 48 \\ 4 \end{array} \quad \begin{array}{r} 44 \\ 50 \end{array}$$

$$\begin{array}{r} 133 \\ 50 \end{array} \quad \begin{array}{r} 107 \\ 24 \end{array} \quad \begin{array}{r} 68 \\ \hline \end{array} \quad \begin{array}{r} 42 \\ 50 \end{array}$$

$$\begin{array}{r} 170 \\ 50 \end{array} \quad \begin{array}{r} 131 \\ 16 \end{array} \quad \begin{array}{r} 114 \\ 8 \end{array} \quad \begin{array}{r} 96 \\ \hline \end{array} \quad \begin{array}{r} 93 \\ 6 \end{array} \quad \begin{array}{r} 107 \\ 10 \end{array} \quad \begin{array}{r} 50 \\ 15 \end{array} \quad \begin{array}{r} 54 \\ 50 \end{array}$$

$$\begin{array}{r} 117 \\ 50 \end{array} \quad \begin{array}{r} 83 \\ 15 \end{array} \quad \begin{array}{r} 58 \\ \hline \end{array} \quad \begin{array}{r} 53 \\ 7 \end{array} \quad \begin{array}{r} 20 \\ 10 \end{array} \quad \begin{array}{r} 49 \\ 14 \end{array} \quad \begin{array}{r} 04 \\ 50 \end{array}$$

$$\begin{array}{r} 145 \\ 50 \end{array} \quad \begin{array}{r} 91 \\ \hline \end{array} \quad \begin{array}{r} 83 \\ 7 \end{array} \quad \begin{array}{r} 25 \\ 23 \end{array} \quad \begin{array}{r} 52 \\ 50 \end{array}$$

$$\begin{array}{r} 145 \\ 50 \end{array} \quad \begin{array}{r} 129 \\ 29 \end{array} \quad \begin{array}{r} 95 \\ \hline \end{array} \quad \begin{array}{r} 88 \\ 6 \end{array} \quad \begin{array}{r} 78 \\ 31 \end{array} \quad \begin{array}{r} 20 \\ 50 \end{array}$$

$$\begin{array}{r} 166 \\ 50 \end{array} \quad \begin{array}{r} 130 \\ 11 \end{array} \quad \begin{array}{r} 107 \\ \hline \end{array} \quad \begin{array}{r} 70 \\ 27 \end{array} \quad \begin{array}{r} 42 \\ 50 \end{array}$$

$$\begin{array}{r} 212 \\ 50 \end{array} \quad \begin{array}{r} 190 \\ 25 \end{array} \quad \begin{array}{r} 138 \\ \hline \end{array} \quad \begin{array}{r} 125 \\ 15 \end{array} \quad \begin{array}{r} 83 \\ 31 \end{array} \quad \begin{array}{r} 63 \\ 40 \end{array}$$

942.31

| Sta.  | +     | K        | -     | Elev.                     |
|-------|-------|----------|-------|---------------------------|
| 19+50 |       | 930.55 ✓ |       | 923.0<br><del>921.0</del> |
| 20    |       |          |       | 22.1                      |
| +50   |       |          |       | 20.2                      |
| B.M.  | 2.73  | 923.25 ✓ | 10.93 | 919.62 ✓                  |
| 21    |       |          |       | 16.1                      |
| +50   |       |          |       | 13.1                      |
| +80   |       |          |       | 13.6                      |
| 22    |       |          |       | 15.0                      |
| +25   |       |          |       | 18.1                      |
| T.P.  | 10.42 | 931.85 ✓ | 1.92  | 921.43 ✓                  |
| +50   |       |          |       | 20.8                      |
| 23    |       |          |       | 26.6                      |
| +25   |       |          |       | 24.6                      |
| T.P.  | 2.97  | 921.84 ✓ | 14.98 | 918.87 ✓                  |

Lt.

E

Rt.

$$\frac{130}{50} \quad \frac{116}{25} \quad \frac{76}{\cancel{50}} \quad \frac{63}{7} \quad \frac{15}{50}$$

$$\frac{118}{50} \quad \frac{85}{21} \quad \frac{85}{\cancel{50}} \quad \frac{77}{13} \quad \frac{25}{31} \quad \frac{48}{50}$$

$$\frac{154}{50} \quad \frac{142}{43} \quad \frac{117}{19} \quad \frac{104}{\cancel{50}} \quad \frac{50}{21} \quad \frac{71}{34} \quad \frac{61}{50}$$

Top of Boulder 200' Lt 512.20+20

$$\frac{110}{50} \quad \frac{110}{28} \quad \frac{106}{13} \quad \frac{73}{\cancel{50}} \quad \frac{62}{6} \quad \frac{104}{38} \quad \frac{08}{50}$$

$$\frac{112}{50} \quad \frac{110}{12} \quad \frac{103}{\cancel{50}} \quad \frac{87}{6} \quad \frac{27}{40} \quad \frac{16}{50}$$

$$\frac{140}{50} \quad \frac{110}{19} \quad \frac{98}{\cancel{50}} \quad \frac{83}{5} \quad \frac{29}{23} \quad \frac{57}{50}$$

$$\frac{120}{50} \quad \frac{119}{30} \quad \frac{102}{9} \quad \frac{84}{\cancel{50}} \quad \frac{70}{1} \quad \frac{32}{35} \quad \frac{40}{50}$$

$$\frac{118}{50} \quad \frac{101}{20} \quad \frac{53}{\cancel{50}} \quad \frac{46}{\cancel{50}} \quad \frac{40}{7} \quad \frac{00}{23} \quad \frac{05}{41} \quad \frac{24}{50}$$

$$\frac{138}{25} \quad \frac{158}{60} \quad \frac{122}{50} \quad \frac{155}{21} \quad \frac{111}{\cancel{50}} \quad \frac{97}{4} \quad \frac{83}{9} \quad \frac{55}{31} \quad \frac{07}{40} \quad \frac{28}{50} \quad \frac{126}{75}$$

$$\frac{97}{25} \quad \frac{94}{50} \quad \frac{83}{28} \quad \frac{53}{\cancel{50}} \quad \frac{43}{8} \quad \frac{15}{30} \quad \frac{07}{50} \quad \frac{15}{60} \quad \frac{40}{75}$$

$$\frac{152}{25} \quad \frac{133}{50} \quad \frac{108}{28} \quad \frac{73}{\cancel{50}} \quad \frac{71}{7} \quad \frac{25}{50} \quad \frac{18}{65} \quad \frac{12}{75}$$

Sta.      +      K      -      Elev.

921.84

+60

913.5

+75

08.8

T.P.      4.01      912.06      13.79      908.05

24

06.0

+80

04.4

+80±      Floor of Dr. Rt.

25

03.4

B.M.      3.68      913.84      1.90      910.16

+50

03.2

+90

05.6

26+08

07.5

+18

08.1

+28.04

08.2

Com. Culv. Under Frost (See Topog.)



Lt.

E

Rt.

$$\begin{array}{r} 15.6 \\ 75 \end{array} \quad \begin{array}{r} 14.1 \\ 50 \end{array} \quad \begin{array}{r} 11.6 \\ 18 \end{array} \quad \begin{array}{r} 8.3 \\ \hline \end{array} \quad \begin{array}{r} 6.4 \\ 12 \end{array} \quad \begin{array}{r} 2.4 \\ 50 \end{array} \quad \begin{array}{r} +0.2 \\ 75 \end{array}$$

$$\begin{array}{r} 18.4 \\ 75 \end{array} \quad \begin{array}{r} 12.6 \\ 50 \end{array} \quad \begin{array}{r} 15.6 \\ 23 \end{array} \quad \begin{array}{r} 13.0 \\ \hline \end{array} \quad \begin{array}{r} 11.6 \\ 12 \end{array} \quad \begin{array}{r} 6.7 \\ 50 \end{array} \quad \begin{array}{r} 3.5 \\ 75 \end{array}$$

$$\begin{array}{r} 10.6 \\ 75 \end{array} \quad \begin{array}{r} 9.9 \\ 50 \end{array} \quad \begin{array}{r} 7.8 \\ 28 \end{array} \quad \begin{array}{r} 6.1 \\ \hline \end{array} \quad \begin{array}{r} 2.1 \\ 50 \end{array} \quad \begin{array}{r} +0.5 \\ 75 \end{array}$$

$$\begin{array}{r} 10.8 \\ 50 \end{array} \quad \begin{array}{r} 10.3 \\ 33 \end{array} \quad \begin{array}{r} 7.7 \\ \hline \end{array} \quad \begin{array}{r} 5.4 \\ 29 \end{array} \quad \begin{array}{r} 4.1 \\ 47 \end{array} \quad \begin{array}{r} 3.7 \\ 50 \end{array}$$

+0.3

$$\begin{array}{r} 9.2 \\ 50 \end{array} \quad \begin{array}{r} 8.7 \\ \hline \end{array} \quad \begin{array}{r} 2.5 \\ 25 \end{array} \quad \begin{array}{r} 2.6 \\ 50 \end{array}$$

Spike in 6" Oak 90' Rt. 512 25+00

$$\begin{array}{r} 45 \\ 75 \end{array} \quad \begin{array}{r} 115 \\ 60 \end{array} \quad \begin{array}{r} 168 \\ 47 \end{array} \quad \begin{array}{r} 168 \\ 43 \end{array} \quad \begin{array}{r} 185 \\ 42 \end{array} \quad \begin{array}{r} 12.1 \\ 37 \end{array} \quad \begin{array}{r} 11.2 \\ 25 \end{array} \quad \begin{array}{r} 10.6 \\ \hline \end{array} \quad \begin{array}{r} 9.3 \\ 50 \end{array}$$

$$\begin{array}{r} 11.2 \\ 50 \end{array} \quad \begin{array}{r} 11.5 \\ 39 \end{array} \quad \begin{array}{r} 10.7 \\ 28 \end{array} \quad \begin{array}{r} 10.7 \\ 10 \end{array} \quad \begin{array}{r} 8.1 \\ 5 \end{array} \quad \begin{array}{r} 8.2 \\ \hline \end{array} \quad \begin{array}{r} 8.1 \\ 7 \end{array} \quad \begin{array}{r} 9.6 \\ 11 \end{array} \quad \begin{array}{r} 8.6 \\ 50 \end{array}$$

$$\begin{array}{r} 7.2 \\ 50 \end{array} \quad \begin{array}{r} 6.3 \\ \hline \end{array} \quad \begin{array}{r} 3.4 \\ 50 \end{array}$$

$$\begin{array}{r} 7.0 \\ 50 \end{array} \quad \begin{array}{r} 5.7 \\ \hline \end{array} \quad \begin{array}{r} 3.2 \\ 50 \end{array}$$

$$\begin{array}{r} 7.1 \\ 50 \end{array}$$

$$\begin{array}{r} 908.20 \\ 5.6 \\ \hline \end{array}$$

$$\begin{array}{r} 3.3 \\ 50 \end{array}$$

Inv.  
5. End.

$$\begin{array}{r} 17.6 \\ \hline \end{array}$$

Inv.  
15. End

$$\begin{array}{r} 12.6 \\ \hline \end{array}$$

| Sta. | +     | Σ      | -    | Elev.         |
|------|-------|--------|------|---------------|
|      |       | 913.84 |      |               |
| T.P. | 13.54 | 926.57 | 0.81 | 913.03        |
| T.P. | 13.35 | 939.80 | 0.11 | 926.45        |
| T.P. | 9.75  | 948.31 | 0.74 | 939.06        |
| B.M. |       |        | 5.97 | 942.34        |
|      |       |        |      | <u>942.35</u> |

Lt.

E

Rt.

Spike in E.P. No. 510 Frost Arc. 21 Flandreau  
See Flandreau Slope Stake Notes

Sta. + K - Elev.

Slope Stakes  
Kennard St  
Larperter to Frost Ave

13' .05' Lower than Profile  
16 - 1.25' Ditch

18' .25' Lower than Profile

28 Profile Grade Top of Berm

11



| Sta  | +     | $\pi$  | - | Flav  | Grade |
|------|-------|--------|---|-------|-------|
| B.M  | 13.69 | 948.05 |   | 93436 |       |
| 0+00 |       |        |   |       | 33.6  |

+45

34.7

|      |       |        |      |       |  |
|------|-------|--------|------|-------|--|
| T.P. | 11.08 | 957.94 | 1.19 | 94686 |  |
|------|-------|--------|------|-------|--|

1+00

38.7

+50

42.3

2

45.9

+50

49.5

3

53.1

|      |       |        |      |        |  |
|------|-------|--------|------|--------|--|
| T.P. | 13.28 | 966.42 | 4.80 | 953.14 |  |
|------|-------|--------|------|--------|--|

+50

56.7

4

60.3

|      |       |        |      |        |  |
|------|-------|--------|------|--------|--|
| T.P. | 10.85 | 976.10 | 1.17 | 965.25 |  |
|------|-------|--------|------|--------|--|

+50

63.6

5

66.5

+50

68.8

Grade Rod

Lt

St

Rt

Spt P.P. Larp. + Kennard St

$$\begin{array}{r} 87 \\ 13.4 \quad \underline{C47.4} \\ 38.4 \end{array}$$

$$\begin{array}{r} 5.5 \\ \underline{C7.9} \end{array}$$

$$\begin{array}{r} 3.4 \\ \underline{C10.0} \\ 480 \end{array}$$

Top of Stake

6' Lt 0+95

$$\begin{array}{r} 13.2 \\ 19.2 \quad \underline{C6.0} \\ 40.0 \end{array}$$

$$\begin{array}{r} 10.4 \\ \underline{C8.8} \end{array}$$

$$\begin{array}{r} 8.1 \\ \underline{C11.1} \\ 50.2 \end{array}$$

$$\begin{array}{r} 10.1 \\ 15.6 \quad \underline{C5.5} \\ 37.0 \end{array}$$

$$\begin{array}{r} 6.8 \\ \underline{C8.8} \end{array}$$

$$\begin{array}{r} 4.3 \\ \underline{C11.3} \\ 50.6 \end{array}$$

$$\begin{array}{r} 7.8 \\ 12.0 \quad \underline{C4.2} \\ 36.4 \end{array}$$

$$\begin{array}{r} 4.2 \\ \underline{C7.8} \end{array}$$

$$\begin{array}{r} 1.7 \\ \underline{C10.3} \\ 48.6 \end{array}$$

$$\begin{array}{r} 7.2 \\ 8.4 \quad \underline{C1.2} \\ 30.4 \end{array}$$

$$\begin{array}{r} 4.5 \\ \underline{C3.9} \end{array}$$

$$\begin{array}{r} 1.3 \\ \underline{C7.1} \\ 42.2 \end{array}$$

$$\begin{array}{r} 4.8 \\ 4.8 \quad \underline{C0.0} \\ 28.0 \end{array}$$

$$\begin{array}{r} 4.1 \\ \underline{C0.7} \end{array}$$

$$\begin{array}{r} 1.8 \\ \underline{C3.0} \\ 34.0 \end{array}$$

$$\begin{array}{r} 11.2 \\ 9.7 \quad \underline{F1.2} \\ 31.0 \end{array}$$

$$\begin{array}{r} 10.8 \\ \underline{F1.1} \end{array}$$

$$\begin{array}{r} 10.3 \\ \underline{B.T} \\ 13.0 \end{array}$$

$$\begin{array}{r} 9.6 \\ \underline{C0.1} \\ 28.2 \end{array}$$

$$\begin{array}{r} 7.6 \\ 6.1 \quad \underline{F1.3} \\ 31.0 \end{array}$$

$$\begin{array}{r} 8.3 \\ \underline{F2.2} \end{array}$$

$$\begin{array}{r} 6.5 \\ \underline{F0.4} \\ 28.8 \end{array}$$

$$\begin{array}{r} 11.0 \\ 12.5 \quad \underline{C1.3} \\ 31.0 \end{array}$$

$$\begin{array}{r} 11.6 \\ \underline{C0.9} \end{array}$$

$$\begin{array}{r} 10.3 \\ \underline{C3.2} \\ 32.4 \end{array}$$

$$\begin{array}{r} 6.2 \\ 9.6 \quad \underline{C3.4} \\ 34.8 \end{array}$$

$$\begin{array}{r} 5.5 \\ \underline{C4.1} \end{array}$$

$$\begin{array}{r} 4.6 \\ \underline{C5.0} \\ 38.0 \end{array}$$

$$\begin{array}{r} 4.7 \\ 7.3 \quad \underline{C2.5} \\ 33.2 \end{array}$$

$$\begin{array}{r} 4.5 \\ \underline{C7.8} \end{array}$$

$$\begin{array}{r} 3.5 \\ \underline{C3.8} \\ 35.6 \end{array}$$

| Sta | + | X | - | Elev | Grade |
|-----|---|---|---|------|-------|
|-----|---|---|---|------|-------|

976.10

6+00

70.6

+50

71.9

7

72.8

+50

73.3

B.M

1.42

976.10

1.42

974.71

974.38

8

73.8

T.P

6.40

979.38

3.12

972.98

+50

73.8

9

73.4

+50

72.4

10

70.9

T.P

3.92

973.52

978

969.60

+50

68.9

11

66.5

+50

64.0

Grade Red

Lt

R

Rt

$$\begin{array}{r} 3.8 \\ 5.5 \quad \underline{C1.7} \\ 31.4 \end{array}$$

$$\begin{array}{r} 3.7 \\ \underline{C1.8} \end{array}$$

$$\begin{array}{r} 4.2 \\ \underline{C1.3} \\ 30.6 \end{array}$$

$$\begin{array}{r} 3.4 \\ 4.2 \quad \underline{C0.8} \\ 29.6 \end{array}$$

$$\begin{array}{r} 3.1 \\ \underline{C1.1} \end{array}$$

$$\begin{array}{r} 3.9 \\ \underline{C0.3} \\ 29.6 \end{array}$$

$$\begin{array}{r} 2.3 \quad 13' \\ 3.3 \quad 2.8 \quad \underline{BT \quad 0.0} \\ 29.0 \end{array}$$

$$\begin{array}{r} 9.7 \quad 3.8 \\ \underline{F0.4 \quad BT \quad 0.0} \\ 13 \end{array}$$

$$\begin{array}{r} 4.3 \\ \underline{F1.0} \\ 30.0 \end{array}$$

$$\begin{array}{r} 2.8 \quad 13' \\ 2.8 \quad 3.3 \quad \underline{F1.2} \\ 30.4 \quad \underline{BT \quad 0.0} \\ 75' \end{array}$$

$$\begin{array}{r} 3.5 \\ \underline{F0.7} \end{array}$$

$$\begin{array}{r} 3.3 \\ \underline{BT \quad 0.0} \\ 13' \end{array}$$

$$\begin{array}{r} 3.3 \\ \underline{F0.3} \\ 29.0 \end{array}$$

Sph in For Post 300 ft 7+75'

$$\begin{array}{r} 2.3 \quad 13' \\ 2.3 \quad 2.8 \quad \underline{F3.5} \\ 35.0 \end{array}$$

$$\begin{array}{r} 3.5 \\ \underline{F1.2} \end{array}$$

$$\begin{array}{r} 2.3 \\ \underline{BT \quad 0.0} \\ 28.0 \end{array}$$

$$\begin{array}{r} 5.6 \quad 13' \\ 5.6 \quad 6.1 \quad \underline{F5.1} \\ 38.2 \end{array}$$

$$\begin{array}{r} 7.3 \\ \underline{F1.7} \end{array}$$

$$\begin{array}{r} 6.1 \\ \underline{BT \quad 0.0} \\ 13 \end{array}$$

$$\begin{array}{r} 4.7 \\ \underline{C0.9} \\ 29.8 \end{array}$$

$$\begin{array}{r} 6.0 \quad 13' \\ 6.0 \quad 6.5 \quad \underline{F6.3} \\ 40.6 \end{array}$$

$$\begin{array}{r} 7.1 \\ \underline{F1.1} \end{array}$$

$$\begin{array}{r} 4.1 \\ \underline{C1.8} \\ 31.8 \end{array}$$

$$\begin{array}{r} 7.0 \\ 7.0 \quad \underline{F6.4} \\ 40.8 \end{array}$$

$$\begin{array}{r} 8.2 \\ \underline{F1.2} \end{array}$$

$$\begin{array}{r} 5.3 \\ \underline{C1.7} \\ 31.4 \end{array}$$

$$\begin{array}{r} 8.5 \\ 8.5 \quad \underline{F4.8} \\ 37.6 \end{array}$$

$$\begin{array}{r} 8.7 \\ \underline{F0.2} \end{array}$$

$$\begin{array}{r} 6.2 \\ \underline{C2.3} \\ 32.6 \end{array}$$

$$\begin{array}{r} 4.6 \\ 4.6 \quad \underline{F3.4} \\ 34.8 \end{array}$$

$$\begin{array}{r} 0.0 \\ \underline{C0.0} \end{array}$$

$$\begin{array}{r} 2.3 \\ \underline{C2.3} \\ 32.6 \end{array}$$

$$\begin{array}{r} 7.0 \\ 7.0 \quad \underline{F4.6} \\ 37.2 \end{array}$$

$$\begin{array}{r} 7.8 \\ \underline{F0.8} \end{array}$$

$$\begin{array}{r} 5.2 \\ \underline{C1.8} \\ 31.6 \end{array}$$

$$\begin{array}{r} 7.5 \\ 7.5 \quad \underline{F5.1} \\ 38.2 \end{array}$$

$$\begin{array}{r} 10.1 \\ \underline{F2.6} \end{array}$$

$$\begin{array}{r} 8.2 \\ \underline{F0.7} \\ 29.4 \end{array}$$



| Sta   | +    | $\Sigma$ | -     | Elev   | Grade  |
|-------|------|----------|-------|--------|--------|
|       |      | 973.52   |       |        |        |
| 12+00 |      |          |       |        | 61.5   |
| T.P.  | 2.72 | 963.85   | 12.39 | 961.13 |        |
| +50   |      |          |       |        | 59.0   |
| 13    |      |          |       |        | 56.5   |
| +50   |      |          |       |        | 54.0   |
| T.P.  | 3.84 | 956.33   | 11.36 | 952.49 |        |
| 14    |      |          |       |        | 51.5   |
| B.M   | 1.74 | 956.33   | 1.74  | 954.60 | 954.59 |
| +50   |      |          |       |        | 49.0   |
| 15    |      |          |       |        | 46.5   |
| T.P.  | 2.58 | 946.40   | 12.51 | 943.82 |        |
| +50   |      |          |       |        | 44.0   |
| 16    |      |          |       |        | 41.5   |
| +50   |      |          |       |        | 39.0   |
| 17    |      |          |       |        | 36.5   |
| T.P.  | 3.49 | 937.82   | 12.07 | 934.33 |        |
| +50   |      |          |       |        | 34.0   |



Grade Rod

L+

Z

R+

$$\begin{array}{r}
 15.3 \\
 12.0 \quad \underline{F3.3} \\
 34.6
 \end{array}
 \qquad
 \begin{array}{r}
 13.0 \\
 \underline{F1.0}
 \end{array}
 \qquad
 \begin{array}{r}
 11.2 \\
 \underline{C0.8} \\
 29.6
 \end{array}$$

$$\begin{array}{r}
 2 \quad 13 \\
 4.8-58 \quad \underline{F3.6} \\
 35.2
 \end{array}
 \qquad
 \begin{array}{r}
 5.9 \\
 \underline{F1.1} \quad \text{BT } 0.0 \\
 13
 \end{array}
 \qquad
 \begin{array}{r}
 5.3 \\
 \underline{C0.8} \\
 28.8
 \end{array}$$

$$\begin{array}{r}
 2 \quad 13 \\
 7.4-7.9 \quad \underline{F3.0} \\
 34.0
 \end{array}
 \qquad
 \begin{array}{r}
 8.0 \\
 \underline{F0.6}
 \end{array}
 \qquad
 \begin{array}{r}
 6.4 \\
 \underline{C1.0} \\
 30.0
 \end{array}$$

$$\begin{array}{r}
 10.4 \quad 11.15 \quad 12.5 \quad 11.15 \quad 10.4 \\
 99 \quad 13 \quad 18 \quad \underline{F2.6} \quad \underline{BT} \quad \underline{BT} \quad 0.0 \\
 33.2 \quad 18 \quad 13.0 \quad \underline{C0.6}
 \end{array}
 \qquad
 \begin{array}{r}
 7.1 \\
 \underline{C2.5} \\
 33.0
 \end{array}$$

$$\begin{array}{r}
 8.6 \\
 4.8 \quad \underline{F3.8} \\
 35.6
 \end{array}
 \qquad
 \begin{array}{r}
 4.6 \\
 \underline{C0.2}
 \end{array}
 \qquad
 \begin{array}{r}
 3.2 \\
 \underline{C1.6} \\
 31.2
 \end{array}$$

SPK in PP 300' LT Sta 16+6.2

$$\begin{array}{r}
 14.3 \\
 7.3 \quad \underline{F7.0} \\
 42.0
 \end{array}
 \qquad
 \begin{array}{r}
 9.5 \\
 \underline{F2.2}
 \end{array}
 \qquad
 \begin{array}{r}
 7.3 \\
 \underline{BT} \\
 28.0
 \end{array}$$

$$\begin{array}{r}
 15.2 \\
 9.8 \quad \underline{F5.4} \\
 39.8
 \end{array}
 \qquad
 \begin{array}{r}
 12.6 \\
 \underline{F1.8}
 \end{array}
 \qquad
 \begin{array}{r}
 11.0 \\
 \underline{F1.2} \\
 30.4
 \end{array}$$

$$\begin{array}{r}
 5.5 \\
 2.4 \quad \underline{F3.1} \\
 34.2
 \end{array}
 \qquad
 \begin{array}{r}
 3.5 \\
 \underline{F1.1}
 \end{array}
 \qquad
 \begin{array}{r}
 2.4 \\
 \underline{BT} \\
 28
 \end{array}$$

$$\begin{array}{r}
 6.1 \\
 4.9 \quad \underline{F1.2} \\
 30.4
 \end{array}
 \qquad
 \begin{array}{r}
 5.15 \\
 \underline{BT} \\
 18
 \end{array}
 \qquad
 \begin{array}{r}
 3.8 \\
 \underline{C1.1}
 \end{array}
 \qquad
 \begin{array}{r}
 3.3 \\
 \underline{C1.2} \\
 31.2
 \end{array}$$

$$\begin{array}{r}
 10.0 \\
 7.4 \quad \underline{F2.6} \\
 33.2
 \end{array}
 \qquad
 \begin{array}{r}
 5.2 \\
 \underline{C2.2}
 \end{array}
 \qquad
 \begin{array}{r}
 2.8 \\
 \underline{C4.6} \\
 37.2
 \end{array}$$

$$\begin{array}{r}
 13.9 \\
 9.9 \quad \underline{F4.0} \\
 36.0
 \end{array}
 \qquad
 \begin{array}{r}
 8.2 \\
 \underline{C1.7}
 \end{array}
 \qquad
 \begin{array}{r}
 4.2 \\
 \underline{C5.0} \\
 38.0
 \end{array}$$

$$\begin{array}{r}
 9.1 \\
 3.8 \quad \underline{F5.3} \\
 38.6
 \end{array}
 \qquad
 \begin{array}{r}
 4.1 \\
 \underline{F0.3}
 \end{array}
 \qquad
 \begin{array}{r}
 0.7 \\
 \underline{C3.1} \\
 34.2
 \end{array}$$

| Sta | + | $\pi$  | - | Elev | Grade |
|-----|---|--------|---|------|-------|
|     |   | 937.82 |   |      |       |

|    |  |  |  |  |      |
|----|--|--|--|--|------|
| 18 |  |  |  |  | 31.6 |
|----|--|--|--|--|------|

|     |  |     |  |  |      |
|-----|--|-----|--|--|------|
| +10 |  | ant |  |  | 31.1 |
|-----|--|-----|--|--|------|

|     |  |  |  |  |      |
|-----|--|--|--|--|------|
| +50 |  |  |  |  | 29.3 |
|-----|--|--|--|--|------|

|      |      |        |       |        |  |
|------|------|--------|-------|--------|--|
| T.P. | 8.07 | 934.14 | 11.75 | 926.07 |  |
|------|------|--------|-------|--------|--|

|    |  |  |  |  |      |
|----|--|--|--|--|------|
| 17 |  |  |  |  | 27.1 |
|----|--|--|--|--|------|

|      |      |        |      |        |  |
|------|------|--------|------|--------|--|
| T.P. | 4.25 | 930.32 | 8.07 | 926.07 |  |
|------|------|--------|------|--------|--|

|     |  |  |  |  |      |
|-----|--|--|--|--|------|
| +50 |  |  |  |  | 25.2 |
|-----|--|--|--|--|------|

|     |      |        |       |        |        |
|-----|------|--------|-------|--------|--------|
| B.M | 6.66 | 926.28 | 10.72 | 919.60 | 919.62 |
|-----|------|--------|-------|--------|--------|

|    |  |  |  |  |      |
|----|--|--|--|--|------|
| 20 |  |  |  |  | 23.4 |
|----|--|--|--|--|------|

|     |  |  |  |  |      |
|-----|--|--|--|--|------|
| +50 |  |  |  |  | 21.7 |
|-----|--|--|--|--|------|

|    |  |  |  |  |      |
|----|--|--|--|--|------|
| 21 |  |  |  |  | 20.1 |
|----|--|--|--|--|------|

|     |  |  |  |  |      |
|-----|--|--|--|--|------|
| +50 |  |  |  |  | 18.5 |
|-----|--|--|--|--|------|

|     |  |  |  |  |      |
|-----|--|--|--|--|------|
| +80 |  |  |  |  | 17.5 |
|-----|--|--|--|--|------|

|    |  |  |  |  |      |
|----|--|--|--|--|------|
| 22 |  |  |  |  | 16.9 |
|----|--|--|--|--|------|

|     |  |  |  |  |      |
|-----|--|--|--|--|------|
| +25 |  |  |  |  | 16.1 |
|-----|--|--|--|--|------|

Grade Rod

Lt

R

Pt

$$\begin{array}{r} 11.7 \\ F5.2 \\ \hline 39.0 \end{array}$$

$$\begin{array}{r} 7.4 \\ F1.2 \\ \hline \end{array}$$

$$\begin{array}{r} 5.9 \\ C0.3 \\ \hline 28.6 \end{array}$$

6.7

None Reg

$$\begin{array}{r} 14.5 \\ F6.0 \\ \hline 42.0 \end{array}$$

$$\begin{array}{r} 8.9 \\ F0.4 \\ \hline \end{array}$$

$$\begin{array}{r} 4.1 \\ C4.4 \\ \hline 36.8 \end{array}$$

$$\begin{array}{r} 15.6 \\ F8.6 \\ \hline 45.2 \end{array}$$

$$\begin{array}{r} 8.5 \\ F1.5 \\ \hline \end{array}$$

$$\begin{array}{r} 2.0 \\ C5.8 \\ \hline 38.0 \end{array}$$

$$\begin{array}{r} 12.5 \\ F7.4 \\ \hline 42.6 \end{array}$$

$$\begin{array}{r} 4.4 \\ F2.3 \\ \hline \end{array}$$

$$\begin{array}{r} 3.8 \\ C1.3 \\ \hline 30.6 \end{array}$$

Top Boulder 200' Lt Sta 20420

$$\begin{array}{r} 13.0 \\ 5.5 \\ F2.6 \\ 33.2 \\ \hline 16.0 \end{array}$$

$$\begin{array}{r} 4.15 \\ 4.2 \\ F1.3 \\ \hline 13.0 \end{array}$$

$$\begin{array}{r} 3.4 \\ 3.3 \\ F0.6 \\ \hline 29.8 \end{array}$$

$$\begin{array}{r} 11.3 \\ F6.7 \\ \hline 41.4 \end{array}$$

$$\begin{array}{r} 6.1 \\ F1.5 \\ \hline \end{array}$$

$$\begin{array}{r} 48.5 \\ 13.7 \\ \hline 18.1 \end{array}$$

$$\begin{array}{r} 3.4 \\ C1.2 \\ \hline 30.4 \end{array}$$

$$\begin{array}{r} 14.6 \\ F8.4 \\ \hline 44.8 \end{array}$$

$$\begin{array}{r} 10.2 \\ F4.0 \\ \hline \end{array}$$

$$\begin{array}{r} 2.9 \\ C3.3 \\ \hline 34.2 \end{array}$$

$$\begin{array}{r} 15.4 \\ F2.4 \\ \hline 43.2 \end{array}$$

$$\begin{array}{r} 13.0 \\ F5.2 \\ \hline \end{array}$$

$$\begin{array}{r} 7.8 \\ 13.1 \\ \hline 28.9 \end{array}$$

$$\begin{array}{r} 12.2 \\ F3.4 \\ \hline \end{array}$$

$$\begin{array}{r} 10.1 \\ F1.3 \\ \hline 30.6 \end{array}$$

$$\begin{array}{r} 14.9 \\ F5.5 \\ \hline 39.0 \end{array}$$

$$\begin{array}{r} 11.3 \\ F1.9 \\ \hline \end{array}$$

$$\begin{array}{r} 5.9 \\ C3.3 \\ \hline 35.0 \end{array}$$

$$\begin{array}{r} 14.1 \\ F3.9 \\ \hline 35.8 \end{array}$$

$$\begin{array}{r} 8.2 \\ C2.0 \\ \hline \end{array}$$

$$\begin{array}{r} 3.7 \\ C6.5 \\ \hline 41.0 \end{array}$$

| Sta | + | $\pi$ | - | Elev | Grade |
|-----|---|-------|---|------|-------|
|-----|---|-------|---|------|-------|

726.28

22+50

15.3

T.P.

10.79

932.22

4.85

921.43

23

13.7

+25

12.9

T.P.

2.81

921.67

13.36

918.86

+60

11.8

T.P.

2.85

912.00

12.52

909.15

+75

11.3

24

10.7

+50

09.6

25

08.8

B.M.

3.35

913.51

1.85

910.15

710.16

+50

08.3

+90

08.0

26+08

07.9

3.35

910.16

+18

07.9

B.M.

910.16



Grade Rod

L+

E

R+

11.0

$$\begin{array}{r} 10.4 \\ C06 \\ \hline 29.2 \end{array}$$

$$\begin{array}{r} 5.6 \\ C5.4 \\ \hline \end{array}$$

$$\begin{array}{r} 1.8 \\ C9.2 \\ \hline 46.4 \end{array}$$

18.5

$$\begin{array}{r} 9.6 \\ C8.9 \\ \hline 45.8 \end{array}$$

$$\begin{array}{r} 5.7 \\ C12.8 \\ \hline \end{array}$$

$$\begin{array}{r} 2.3 \\ C16.2 \\ \hline 60.4 \end{array}$$

19.3

$$\begin{array}{r} 13.2 \\ C1 \\ \hline 40.2 \end{array}$$

$$\begin{array}{r} 7.6 \\ C11.7 \\ \hline \end{array}$$

$$\begin{array}{r} 0.7 \\ C18.6 \\ \hline 65.2 \end{array}$$

9.9

$$\begin{array}{r} 13.8 \\ F3.9 \\ \hline 35.8 \end{array}$$

$$\begin{array}{r} 8.2 \\ C1.7 \\ \hline \end{array}$$

$$\begin{array}{r} 1.8 \\ C8.1 \\ \hline 44.2 \end{array}$$

0.7

$$\begin{array}{r} 6.8 \\ F6.1 \\ \hline 40.2 \end{array}$$

$$\begin{array}{r} 3.3 \\ F2.6 \\ \hline \end{array}$$

$$\begin{array}{r} 1.1 \\ F0.4 \\ \hline 28.8 \end{array}$$

1.3

$$\begin{array}{r} 9.4 \\ F8.1 \\ \hline 44.2 \end{array}$$

$$\begin{array}{r} 6.0 \\ F4.7 \\ \hline \end{array}$$

$$\begin{array}{r} 3.7 \\ F2.4 \\ \hline 32.8 \end{array}$$

2.4

$$\begin{array}{r} 10.6 \\ F8.2 \\ \hline 44.4 \end{array}$$

$$\begin{array}{r} 7.7 \\ F5.3 \\ \hline \end{array}$$

$$\begin{array}{r} 5.9 \\ F2.5 \\ \hline 35.0 \end{array}$$

3.2

$$\begin{array}{r} 9.4 \\ F6.2 \\ \hline 40.4 \end{array}$$

$$\begin{array}{r} 8.7 \\ F5.3 \\ \hline \end{array}$$

$$\begin{array}{r} 6.9 \\ F3.7 \\ \hline 35.4 \end{array}$$

5.2

$$\begin{array}{r} 16.3 \\ F11.1 \\ \hline 50.2 \end{array}$$

$$\begin{array}{r} 10.5 \\ F5.3 \\ \hline \end{array}$$

$$\begin{array}{r} 9.5 \\ F4.3 \\ \hline 36.6 \end{array}$$

5.5

$$\begin{array}{r} 11.6 \\ F6.1 \\ \hline 40.2 \end{array}$$

$$\begin{array}{r} 7.8 \\ F2.3 \\ \hline \end{array}$$

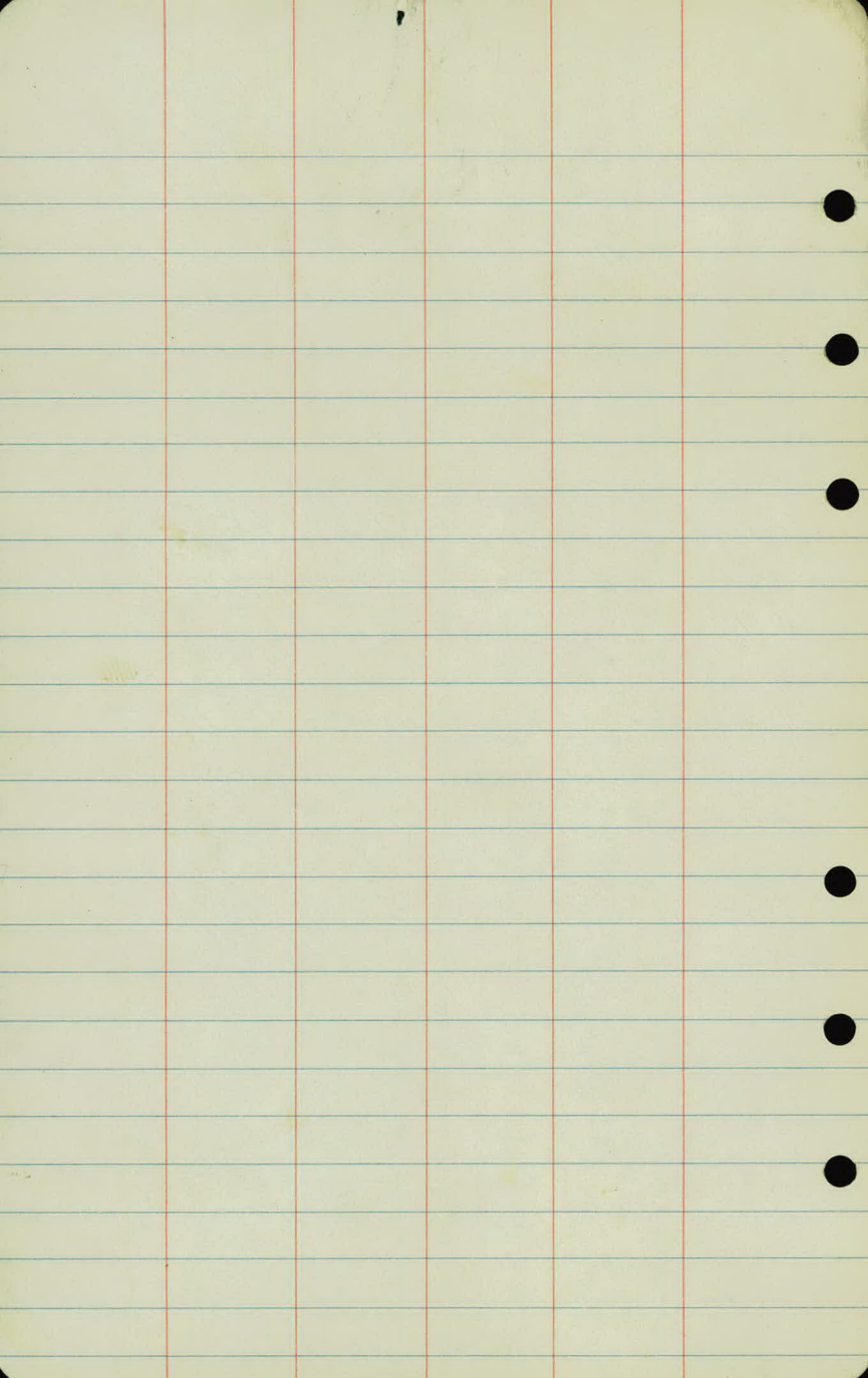
$$\begin{array}{r} 8.9 \\ F3.4 \\ \hline 34.8 \end{array}$$

5.6

$$\begin{array}{r} 5.9 \\ F0.3 \\ \hline \end{array}$$

Spk in 6" Oak 90' RT of Stg 25x00





Kennard St

Blue Tops.

| Sta  | + | x | - | Grade  |
|------|---|---|---|--------|
| B.M. |   |   |   | 934.36 |

|   |     |  |  |       |
|---|-----|--|--|-------|
| 0 | +00 |  |  | 933.6 |
|---|-----|--|--|-------|

|  |     |  |  |      |
|--|-----|--|--|------|
|  | +45 |  |  | 34.7 |
|--|-----|--|--|------|

|   |  |  |  |      |
|---|--|--|--|------|
| 1 |  |  |  | 38.7 |
|---|--|--|--|------|

|  |     |  |  |      |
|--|-----|--|--|------|
|  | +50 |  |  | 42.3 |
|--|-----|--|--|------|

|   |  |  |  |      |
|---|--|--|--|------|
| 2 |  |  |  | 45.9 |
|---|--|--|--|------|

|  |     |  |  |      |
|--|-----|--|--|------|
|  | +50 |  |  | 49.5 |
|--|-----|--|--|------|

|   |  |  |  |      |
|---|--|--|--|------|
| 3 |  |  |  | 53.1 |
|---|--|--|--|------|

|  |     |  |  |      |
|--|-----|--|--|------|
|  | +50 |  |  | 56.7 |
|--|-----|--|--|------|

|   |  |  |  |      |
|---|--|--|--|------|
| 4 |  |  |  | 60.3 |
|---|--|--|--|------|

|  |     |  |  |      |
|--|-----|--|--|------|
|  | +50 |  |  | 63.6 |
|--|-----|--|--|------|

|   |  |  |  |      |
|---|--|--|--|------|
| 5 |  |  |  | 66.5 |
|---|--|--|--|------|

Gr. Rod.

Lt

R

Lt

Spk. in R.R. Lagg & Kemord.

| Sta. | +   | $\pi$  | - | Grade    |
|------|-----|--------|---|----------|
| 5    | +50 |        |   | 68.8     |
| 6    |     |        |   | 70.6     |
|      | +50 |        |   | 71.9     |
| 7    |     |        |   | 72.8     |
|      | +50 |        |   | 73.3     |
| B.M. |     |        |   | (974.71) |
| 8    |     |        |   | 73.8     |
|      | +50 |        |   | 73.8     |
| T.P. | 376 | 976.90 |   | 973.14   |
| 9    |     |        |   | 73.4     |
|      | +50 |        |   | 72.4     |
| 10   |     |        |   | 70.9     |
|      | +50 |        |   | 68.9     |



Co. Rod

Lt

R

Rt

←  
Spt. in F.R. 300' Rt 71-75

Top Blue Top Rt 9100

3.5

18

$\frac{3.75}{18}$  ✓

4.5

18 ✓

$\frac{4.75}{18}$

6.0

18 ✓

$\frac{6.25}{18}$  ✓

8.0

18 ✓

$\frac{8.25}{18}$  ✓

| sta. | +    | $\Sigma$ | -     | Grade  |
|------|------|----------|-------|--------|
|      |      | 976.90   |       |        |
| 11   |      |          |       | 66.5   |
|      | +50  |          |       | 64.0   |
| T.P. | 0.39 | 963.39   | 13.85 | 963.05 |
| 12   |      |          |       | 61.5   |
|      | +50  |          |       | 59.0   |
| 13   |      |          |       | 56.5   |
|      | +50  |          |       | 54.0   |
| 14   |      |          |       | 51.5   |
| T.P. | 0.46 | 950.62   | 13.23 | 950.16 |
|      | +50  |          |       | 49.0   |
| 15   |      |          |       | 46.5   |
|      | +50  |          |       | 44.0   |
| 16   |      |          |       | 41.5   |

Gr. Rod.

Lt

L

Rt

10.4

18 ✓

 $\frac{1465}{18}$  ✓

12.90

18 ✓

 $\frac{13.15}{18}$  ✓

1.89

18

 $\frac{2.14}{18}$  ✓

4.39

18 ✓

 $\frac{9.64}{18}$  ✓

6.87

 $\frac{7.14}{18}$  ✓ $\frac{7.14}{18}$ 

9.39

 $\frac{9.60}{18}$  ✓ $\frac{9.64}{18}$  ✓

17.89

18 ✓

 $\frac{12.14}{18}$  ✓

1.62

18

 $\frac{18.7}{18}$ 

4.12

18 ✓

 $\frac{4.27}{18}$  ✓

6.62

18 ✓

 $\frac{6.87}{18}$  ✓

9.12

18 ✓

 $\frac{9.87}{18}$  ✓

| Sta  | +    | X      | -     | Grade  |          |
|------|------|--------|-------|--------|----------|
|      |      | 950.62 |       |        |          |
| 16   | +50  |        |       | 39.0   |          |
| T.P. | 1.46 | 938.62 | 13.46 | 927.16 | (927.16) |
| 17   |      |        |       | 36.5   |          |
|      | +50  |        |       | 34.0   |          |
| 18   |      |        |       | 31.6   |          |
|      | +50  |        |       | 29.3   |          |
| 19   |      |        |       | 27.1   |          |
| T.P. | 1.68 | 926.63 | 13.67 | 929.95 |          |
|      | +50  |        |       | 26.2   |          |
| 20   |      |        |       | 23.4   |          |
| B.M. |      | 926.67 | 7.01  |        | (919.62) |
|      | +50  |        |       | 21.7   |          |
| 21   |      |        |       | 20.1   |          |
|      | +50  |        |       | 18.5   |          |

Cor. Rod.

Lt

2

Rt.

11.62

18

$\frac{11.87}{18} \checkmark$

~~3rd. in P.P. 300' at 11.50~~

2.12

$\frac{2.37}{18}$

4.62

18  $\checkmark$

$\frac{4.87}{18} \checkmark$

2.02

18

$\frac{2.27}{18} \checkmark$

7.32

18  $\checkmark$

$\frac{9.57}{18} \checkmark$

11.52

18  $\checkmark$

$\frac{11.77}{18} \checkmark$

1.43

18

$\frac{1.68}{18}$

1.43

1.68

3.23

18  $\checkmark$

$\frac{3.48}{18} \checkmark$

Top Boulder. 200' Lt 5 to 20 + 20

1.97

18

$\frac{5.22}{18}$

6.57

18  $\checkmark$

$\frac{6.82}{18} \checkmark$

8.17

18  $\checkmark$

$\frac{8.92}{18} \checkmark$



| Sta | + | $\pi$  | - | Grade |
|-----|---|--------|---|-------|
|     |   | 926.67 |   |       |

|    |  |  |  |      |
|----|--|--|--|------|
| 22 |  |  |  | 16.9 |
|----|--|--|--|------|

|     |  |  |  |      |
|-----|--|--|--|------|
| +25 |  |  |  | 16.1 |
|-----|--|--|--|------|

|     |  |  |  |      |
|-----|--|--|--|------|
| +50 |  |  |  | 15.3 |
|-----|--|--|--|------|

|    |  |  |  |      |
|----|--|--|--|------|
| 23 |  |  |  | 13.7 |
|----|--|--|--|------|

|      |      |        |       |        |
|------|------|--------|-------|--------|
| I.P. | 1.98 | 919.89 | 13.77 | 912.90 |
|------|------|--------|-------|--------|

|     |  |  |  |      |
|-----|--|--|--|------|
| +25 |  |  |  | 12.9 |
|-----|--|--|--|------|

|     |  |  |  |      |
|-----|--|--|--|------|
| +60 |  |  |  | 11.8 |
|-----|--|--|--|------|

|    |  |  |  |      |
|----|--|--|--|------|
| 24 |  |  |  | 10.7 |
|----|--|--|--|------|

|     |  |  |  |      |
|-----|--|--|--|------|
| +50 |  |  |  | 09.6 |
|-----|--|--|--|------|

|    |  |  |  |      |
|----|--|--|--|------|
| 25 |  |  |  | 08.8 |
|----|--|--|--|------|

|     |  |  |  |      |
|-----|--|--|--|------|
| +50 |  |  |  | 08.3 |
|-----|--|--|--|------|

|     |  |  |  |      |
|-----|--|--|--|------|
| +90 |  |  |  | 08.0 |
|-----|--|--|--|------|

|      |  |  |      |  |
|------|--|--|------|--|
| B.M. |  |  | 4.72 |  |
|------|--|--|------|--|

910.16

08.2

Gp Rod.

11

12

13

9.77

$\frac{10.02}{18}$

10.57

✓

$\frac{\checkmark 10.82}{18}$

11.37

18 ✓

$\frac{11.62}{18}$  ✓

12.97 ✓

18

$\frac{13.22}{18}$

1.98

$\frac{198}{28}$

$\frac{225}{18}$

3.08

$\frac{3.33}{18}$

4.18

✓

5.28

✓

6.08

✓

6.58

✓

6.88

✓

Spk in G' Oak 90' at 15+00

6.68

