

Dr. 12A B25

Dr. 12A - Bk. 25

OFFICE OF COUNTY ENGINEER
RAMSEY CO. MINN.

.....PLAN.....Survey

.....KUEFFNER PLACE.....
From: Near Co. Rd A² & Arcade St.

Road Acc't. No.

Date Filed. 12-29-38

File.

N.C.TWP.

1

Kueffner Place

New Canada, 17-29-22
Forest Heights Addition
Reproduction of
original survey.

6/38

{ Bratager
Wilke
Mooschter.

No Plan. made
H.P.

Angle.

Sta.	Point	Lt.	Rt.
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4+10.6	P.I.		52°51'
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1+78.5	P.O.T.		
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0+00	P.O.T.		
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Tangents

R.R. Tie.

62.30

57.57

Set 2"x2" Hub.

10" Oak

68.92

R.R. Tie.

R.R. Tie.

74.36

Original 1/2" Iron Pipe.

500 Line

59.75

56.00

24" Oak

68.37

R.R. Tie.

For in

18" Oak

90.48

R.R. Tie.

56.03

44.80 - 24" Oak

Original 1/2" Iron Pipe.

500 Line

59.82

31.75

on

R.R. F.P.

Ties

Angle.

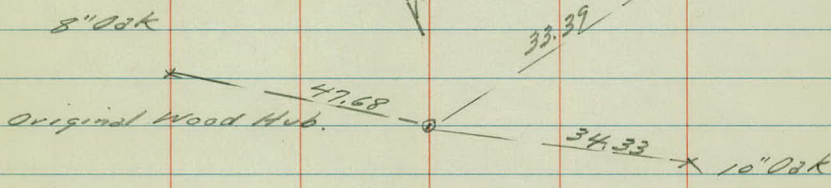
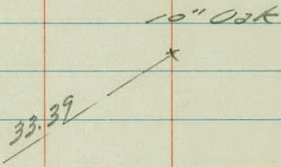
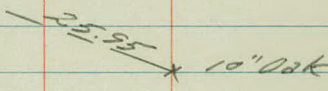
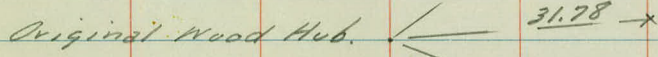
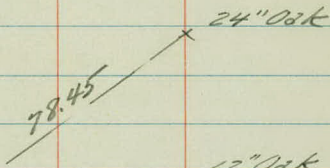
Sta.	Point	Lt.	Rt.
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9+14.2	P.I.	39°08'	
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7+68.23	P.I.	34°00'	
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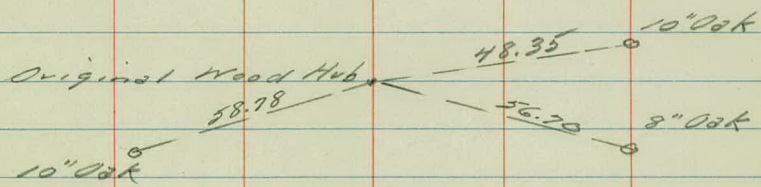
5+74.58	P.I.		10°18'
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Tangents.



Forward

To



Ties

Angle.

Sta. Point Lt. Rt.

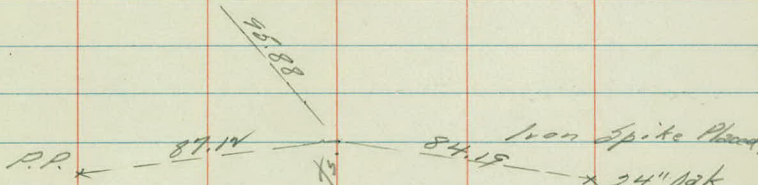
14+67.84 P.O.T.

12+14.1 P.O.T.

11+10.5 P.I.

16°39'

End Conc. Ed.
Rail Post. Topctr.

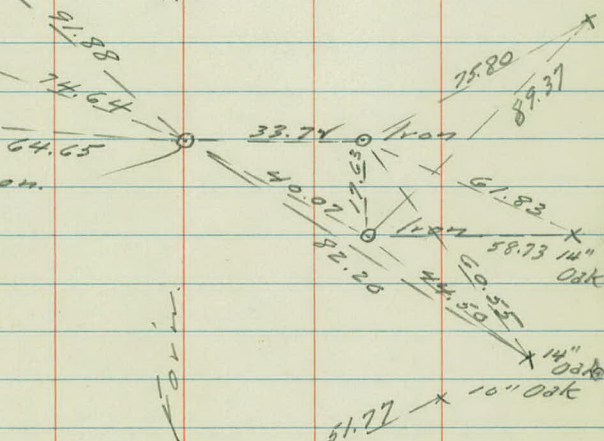


12" Oak.

Tangents.

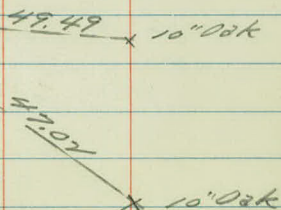
Garage.
Edn.
Corners

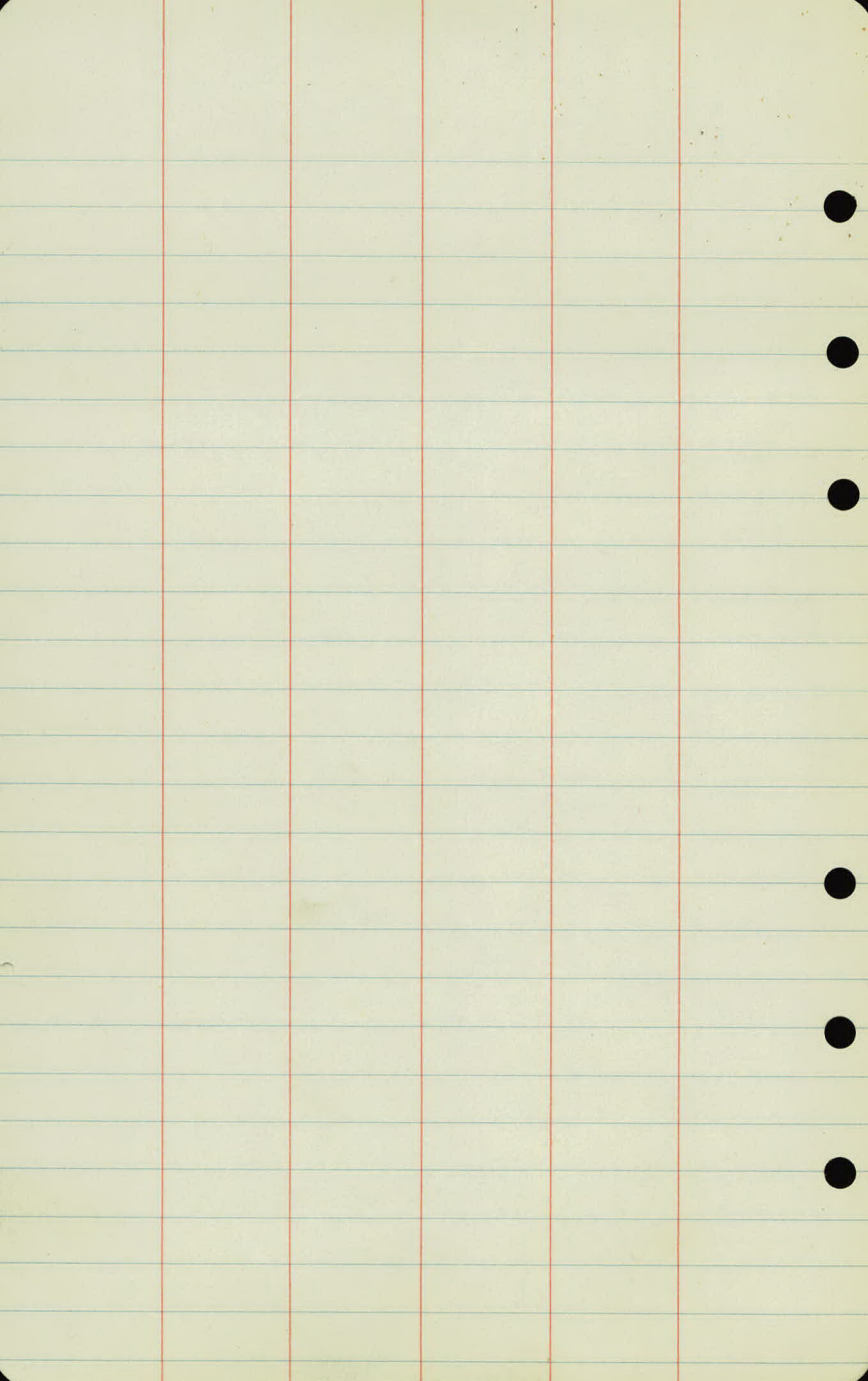
Original Iron.



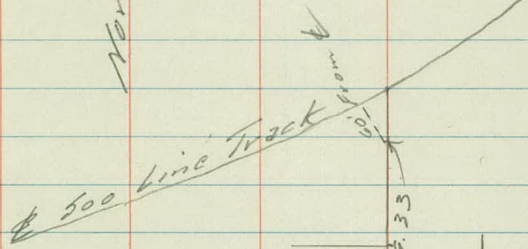
Iron.

Original Wood Hub.



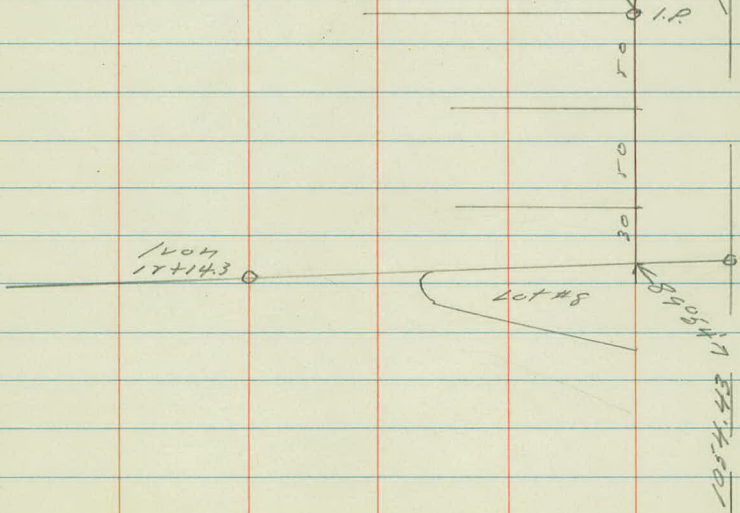


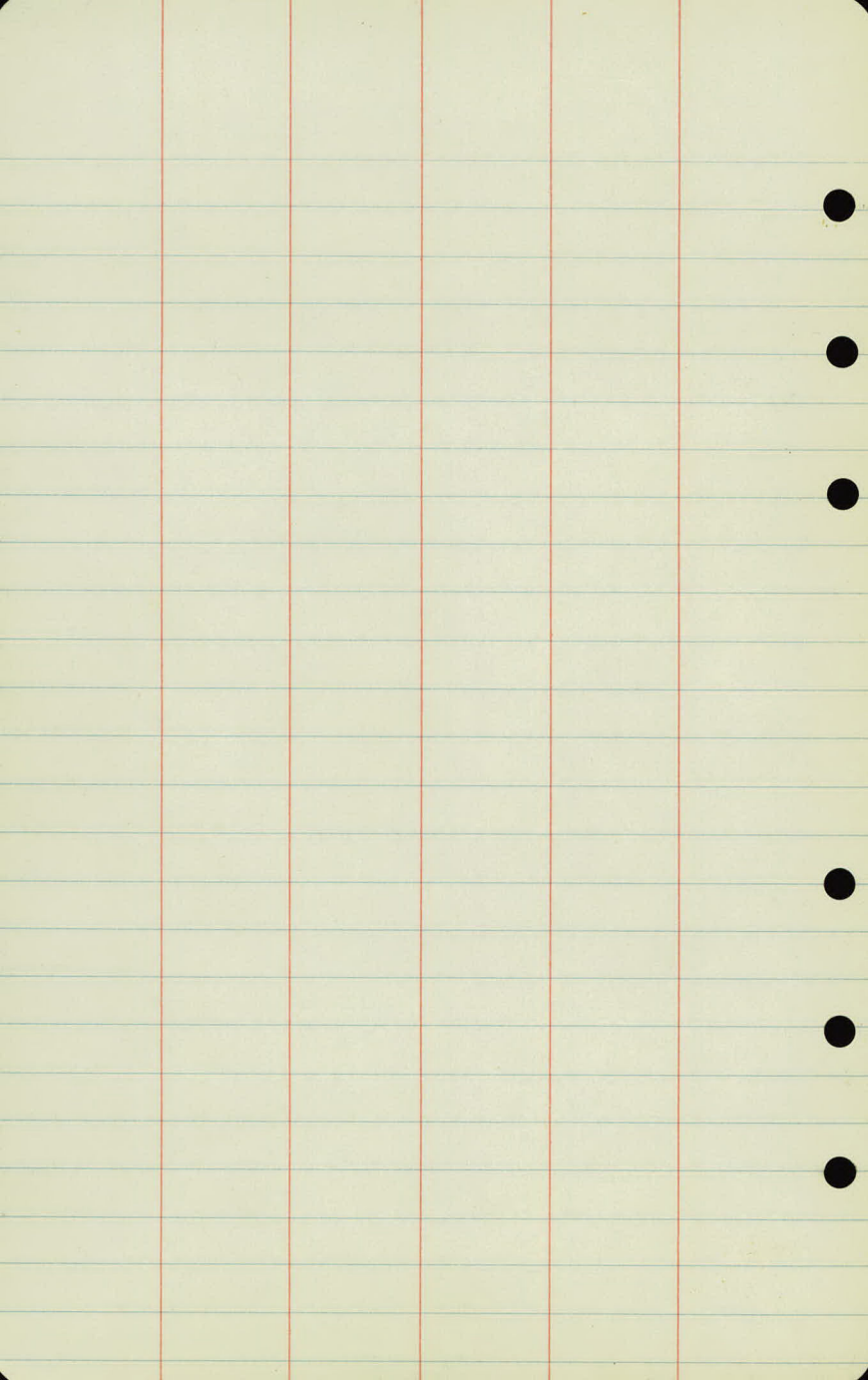
North →



Iron Pipe Presumably on $\frac{1}{4}$ 4

Acres 54





Topography.

11+75

5

4

3

2

1

0

4403-12' from Gate

500 Line Rg.

60 - 1.8

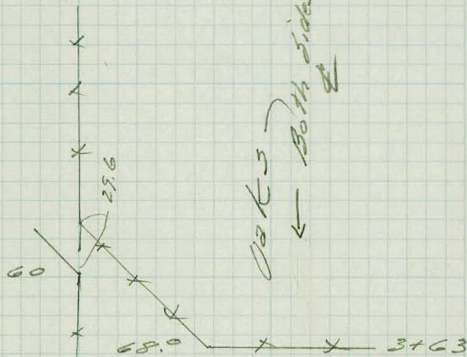
Blk Fence

1.0

60 - 1.5
2.5
10.5

Scattered

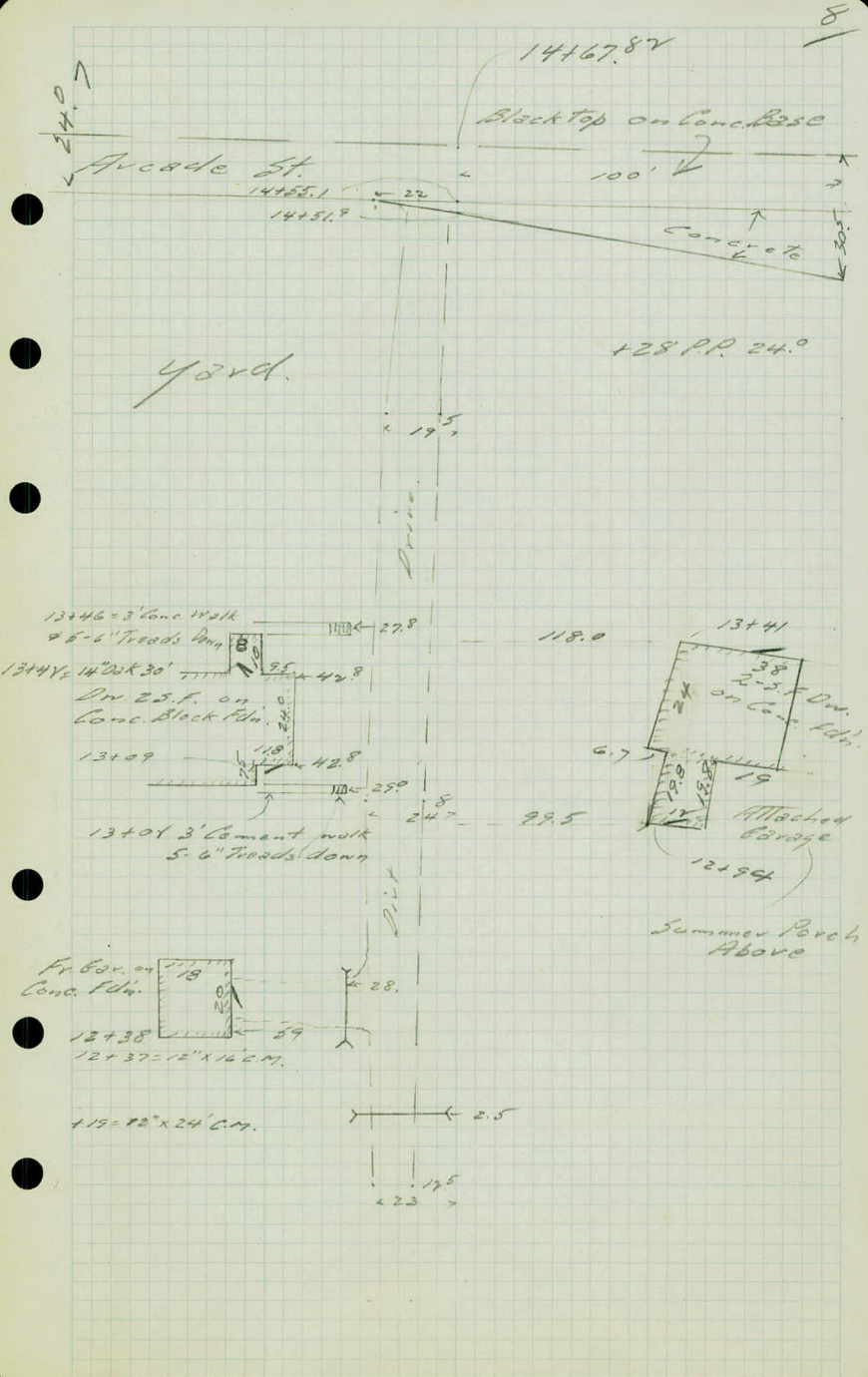
Gross and
Marsh
Land



14

13

12





Bench Levels

Sta	+	K	-	Elev.
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B.M.	3.14	916.45		912.33
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T.P.	0.37	904.17	12.65	903.80
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B.M.	4.65	896.94	11.90	892.27
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T.P.	0.58	885.06	12.44	884.48
------	------	--------	-------	--------

T.P.	3.17	881.86	6.37	878.69
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B.M.			8.47	873.39
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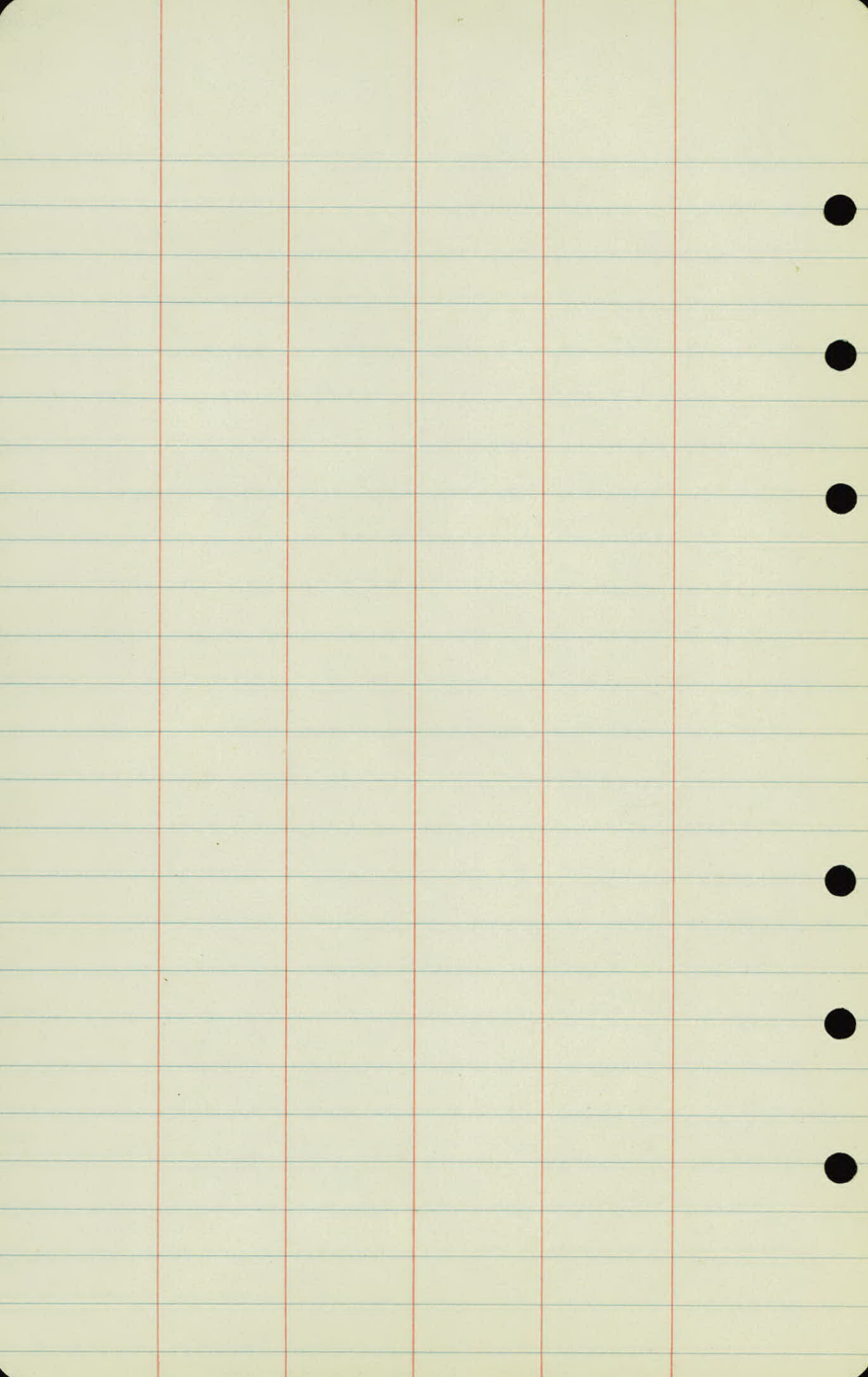
10

Description

Top of hydrant East side of
Arcade at Bellwood St. For
source of elev. see notes on
Bellwood & Kenwood Sts.

Top of lower tread of concrete steps
27' Lt. St. 13+45. East End.

Spike in 24" Oak 60' Rt. St. 0+70.



Cross Sections

Sta.	+	π	-	Elev.
B.M.	8.47	881.86		873.39
0+00				71.0.
0+50				78.0.
0+68				77.8.
1+00				73.4.
1+10				72.6.
1+50				71.3.
T.P.	0.27	873.66	8.47	873.39
1+78				68.2.
2+00				65.3.
+50				64.0.
T.P.	17.88	885.81	0.73	874.93.
3			16.1	69.7.
+50			C.O	79.8.

Lt.

L

Rt.

12

Spike in 24" Oak 60' Rt. Sta. 0+70

T.Tie

44	44	50	50	39	63	89	10.9	14.8	163	120
60	56	53	50	46	30	10		22	80	100

T.T.

43	44	50	50	07	39	9.1	15.1
60	56	53	50	41	30	50	100

T.T.

41	48	49	22	4.1	6.2	8.4	14.2
60	54	49	43	4.1	24	50	100

T.T.

41	44	48	74	8.5	10.0	12.1	15.3
60	54	50	33	21	50	100	

T.T.

40	43	49	61	8.5	9.3	10.6	12.9	16.8
60	53	50	46	24	22	50	100	

T.T.

3.9	41	48	49	8.5	10.6	14.0	17.6	18.8	22.1	25.8
60	54	50	46	16	23	50	58	71	100	

+43	+40	+26	+32	20	8.8	140	163	200
60	54	49	46	15	17	38	50	100

84	8.8	117	140	167	184	220
4	14	20	34	50	100	

97

Sta.	+	K	-	Elev.
		885.81		
3+84			0.6	85.2
T.P.	9.72	887.58	2.95	887.86
4			6.7	85.9
+10.6			7.7	84.9
+50			6.3	86.3
5			6.6	86.0
+74			4.9	87.7
B.M.	7.34	892.58	7.34	885.24
6			4.8	87.8
+50			7.2	85.4
7			11.5	81.1
+50			13.6	79.0
T.P.	0.82	881.10	12.30	880.28
7+68.3			3.6	77.5
8			6.5	74.6
+50			10.9	70.2
9			5.7	75.4
+14.2			4.8	76.3
T.P.	12.22	889.38	4.44	876.66
+30			9.9	79.5
9+50			8.8	80.6

Lt.

2

Lt.

13

Spike in 12" Oak 25' Lt. 5+74

$$\frac{26^3}{50}$$

$$\frac{20^8}{43}$$

$$\frac{12^1}{28}$$

$$\frac{7^8}{13}$$

$$\frac{8^8}{/}$$

$$\frac{12^3}{20}$$

$$\frac{15^9}{36}$$

$$\frac{19^1}{50}$$

Sta.	+	π	-	Elev.
		889.38		
10+00				880.7
+23				83.8
+50				90.4
T.P.	13.28	899.97 ✓	2.69	886.69
+75				96.5
11+00				899.8
T.P.	6.37	904.54 ✓	1.84	898.15
+22				901.8
+50				98.3
T.P.	6.34	897.90 ✓	12.94	891.58
B.M.	6.44	898.74 ✓	5.60	894.30 (894.27)
11+75				93.3
T.P.	4.35	896.65 ✓	6.44	894.30
12+00				88.2
Floor Garage Lt.				
+50				86.9
13+00				88.5
13+00 ±	Bottom Conc. Steps Lt.			
+45 ±	Bottom Conc. Steps Lt.			

Lt.

E

Rt.

14

$$\begin{array}{r} 20.0 \\ 50 \end{array} \quad \begin{array}{r} 13.0 \\ 33 \end{array} \quad \begin{array}{r} 9.3 \\ 16 \end{array} \quad \begin{array}{r} 8.7 \\ \hline \end{array} \quad \begin{array}{r} 10.5 \\ 19 \end{array} \quad \begin{array}{r} 14.3 \\ 44 \end{array} \quad \begin{array}{r} 16.5 \\ 50 \end{array}$$

$$\begin{array}{r} 15.8 \\ 50 \end{array} \quad \begin{array}{r} 10.9 \\ 37 \end{array} \quad \begin{array}{r} 6.6 \\ 18 \end{array} \quad \begin{array}{r} 5.6 \\ \hline \end{array} \quad \begin{array}{r} 7.6 \\ 24 \end{array} \quad \begin{array}{r} 11.5 \\ 44 \end{array} \quad \begin{array}{r} 13.5 \\ 50 \end{array}$$

$$\begin{array}{r} 8.0 \\ 50 \end{array} \quad \begin{array}{r} 5.7 \\ 44 \end{array} \quad \begin{array}{r} 12 \\ 17 \end{array} \quad \begin{array}{r} 11.0 \\ \hline \end{array} \quad \begin{array}{r} 0.6 \\ 15 \end{array} \quad \begin{array}{r} 5.5 \\ 35 \end{array} \quad \begin{array}{r} 9.2 \\ 50 \end{array}$$

$$\begin{array}{r} 13.8 \\ 50 \end{array} \quad \begin{array}{r} 9.4 \\ 34 \end{array} \quad \begin{array}{r} 5.6 \\ 16 \end{array} \quad \begin{array}{r} 3.5 \\ \hline \end{array} \quad \begin{array}{r} 5.3 \\ 23 \end{array} \quad \begin{array}{r} 7.5 \\ 41 \end{array} \quad \begin{array}{r} 12.0 \\ 50 \end{array}$$

$$\begin{array}{r} 11.7 \\ 50 \end{array} \quad \begin{array}{r} 7.7 \\ 34 \end{array} \quad \begin{array}{r} 1.9 \\ 14 \end{array} \quad \begin{array}{r} 0.2 \\ \hline \end{array} \quad \begin{array}{r} 13 \\ 22 \end{array} \quad \begin{array}{r} 6.3 \\ 43 \end{array} \quad \begin{array}{r} 8.2 \\ 50 \end{array}$$

$$\begin{array}{r} 11.6 \\ 50 \end{array} \quad \begin{array}{r} 6.9 \\ 33 \end{array} \quad \begin{array}{r} 3.5 \\ 15 \end{array} \quad \begin{array}{r} 2.7 \\ \hline \end{array} \quad \begin{array}{r} 4.5 \\ 16 \end{array} \quad \begin{array}{r} 5.3 \\ 37 \end{array} \quad \begin{array}{r} 13.8 \\ 50 \end{array}$$

$$\begin{array}{r} 9.5 \\ 50 \end{array} \quad \begin{array}{r} 3.6 \\ 30 \end{array} \quad \begin{array}{r} 5.9 \\ 23 \end{array} \quad \begin{array}{r} 6.2 \\ \hline \end{array} \quad \begin{array}{r} 4.4 \\ 1 \end{array} \quad \begin{array}{r} 8.6 \\ 18 \end{array} \quad \begin{array}{r} 14.2 \\ 37 \end{array} \quad \begin{array}{r} 19.2 \\ 50 \end{array}$$

Lower Conc. Step - See Bench Levels

$$\begin{array}{r} 4.5 \\ 50 \end{array} \quad \begin{array}{r} 3.5 \\ 44 \end{array} \quad \begin{array}{r} 2.3 \\ 29 \end{array} \quad \begin{array}{r} 5.5 \\ 13 \end{array} \quad \begin{array}{r} 5.4 \\ \hline \end{array} \quad \begin{array}{r} 9.6 \\ 15 \end{array} \quad \begin{array}{r} 13.3 \\ 30 \end{array} \quad \begin{array}{r} 18.0 \\ 50 \end{array}$$

$$\begin{array}{r} 4.0 \\ 50 \end{array} \quad \begin{array}{r} 4.0 \\ 38 \end{array} \quad \begin{array}{r} 5.4 \\ 25 \end{array} \quad \begin{array}{r} 5.5 \\ 12 \end{array} \quad \begin{array}{r} 8.5 \\ \hline \end{array} \quad \begin{array}{r} 11.8 \\ 16 \end{array} \quad \begin{array}{r} 17.8 \\ 50 \end{array}$$

$$\begin{array}{r} 1.8 \\ \hline \end{array} \quad \begin{array}{r} 2.7 \\ 50 \end{array} \quad \begin{array}{r} 3.7 \\ 40 \end{array} \quad \begin{array}{r} 5.5 \\ 30 \end{array} \quad \begin{array}{r} 5.6 \\ 8 \end{array} \quad \begin{array}{r} 9.8 \\ \hline \end{array} \quad \begin{array}{r} 10.9 \\ 5 \end{array} \quad \begin{array}{r} 13.2 \\ 20 \end{array} \quad \begin{array}{r} 17.6 \\ 50 \end{array}$$

$$\begin{array}{r} 1.1 \\ 50 \end{array} \quad \begin{array}{r} 1.7 \\ 34 \end{array} \quad \begin{array}{r} 5.1 \\ 28 \end{array} \quad \begin{array}{r} 5.6 \\ 6 \end{array} \quad \begin{array}{r} 8.2 \\ \hline \end{array} \quad \begin{array}{r} 10.3 \\ 13 \end{array} \quad \begin{array}{r} 11.2 \\ 31 \end{array} \quad \begin{array}{r} 14.3 \\ 50 \end{array}$$

$$\begin{array}{r} 4.7 \\ \hline \end{array} \quad 91.95$$

$$\begin{array}{r} 5.0 \\ \hline \end{array} \quad 91.45$$

Sta. + π - Elev.

896.65

13+50

90.5

14+00

91.1

+19

90.3

+30

89.2

+40

88.1

+67.82

88.9

T.P.

13.11

909.48

0.28

896.37

T.P.

7.02

916.46

0.04

909.44

B.M.

3.11

913.35

913.33

Lt.

E

Rt.

15

$$\frac{11}{50}$$

$$\frac{18}{33}$$

$$\frac{45}{27}$$

$$\frac{52}{5}$$

$$\frac{62}{5}$$

$$\frac{91}{27}$$

$$\frac{120}{50}$$

$$\frac{23}{50}$$

$$\frac{26}{30}$$

$$\frac{49}{26}$$

$$\frac{60}{1}$$

$$\frac{56}{5}$$

$$\frac{43}{5}$$

$$\frac{63}{30}$$

$$\frac{60}{50}$$

$$\frac{33}{50}$$

$$\frac{37}{37}$$

$$\frac{57}{26}$$

$$\frac{63}{11}$$

$$\frac{64}{5}$$

$$\frac{49}{5}$$

$$\frac{52}{22}$$

$$\frac{71}{37}$$

$$\frac{86}{50}$$

$$\frac{58}{50}$$

$$\frac{65}{25}$$

$$\frac{75}{5}$$

$$\frac{87}{27}$$

$$\frac{98}{50}$$

$$\frac{69}{50}$$

$$\frac{80}{25}$$

$$\frac{86}{5}$$

$$\frac{95}{25}$$

$$\frac{101}{50}$$

$$\frac{48}{100}$$

$$\frac{64}{50}$$

$$\frac{78}{5}$$

$$\frac{92}{50}$$

$$\frac{108}{100}$$

