

B-23-D-12A
Dr. 12A-B.23

OFFICE OF COUNTY ENGINEER
RAMSEY CO. MINN.

PLAN Survey

ARCADE ST. EXT.

From Labore Rd. To N.E. Cor. Sec. 5

Road Acc't. No. N-48

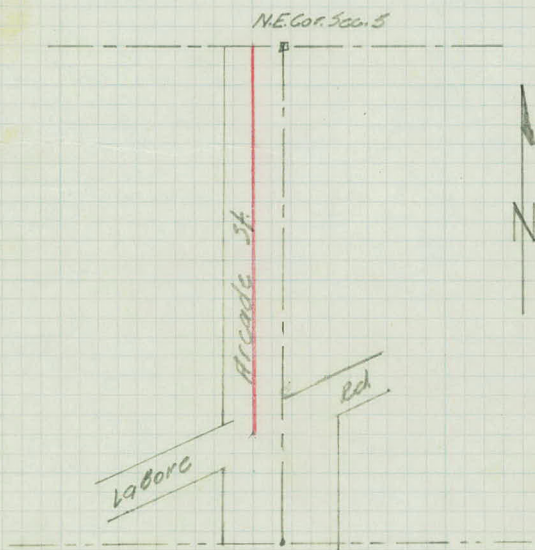
Date Filed 12-23-38 File

N.C.TWP.

PLAN SURVEY

ARCADE ST.

L & Bore Rd to N. Line of Sec. 5



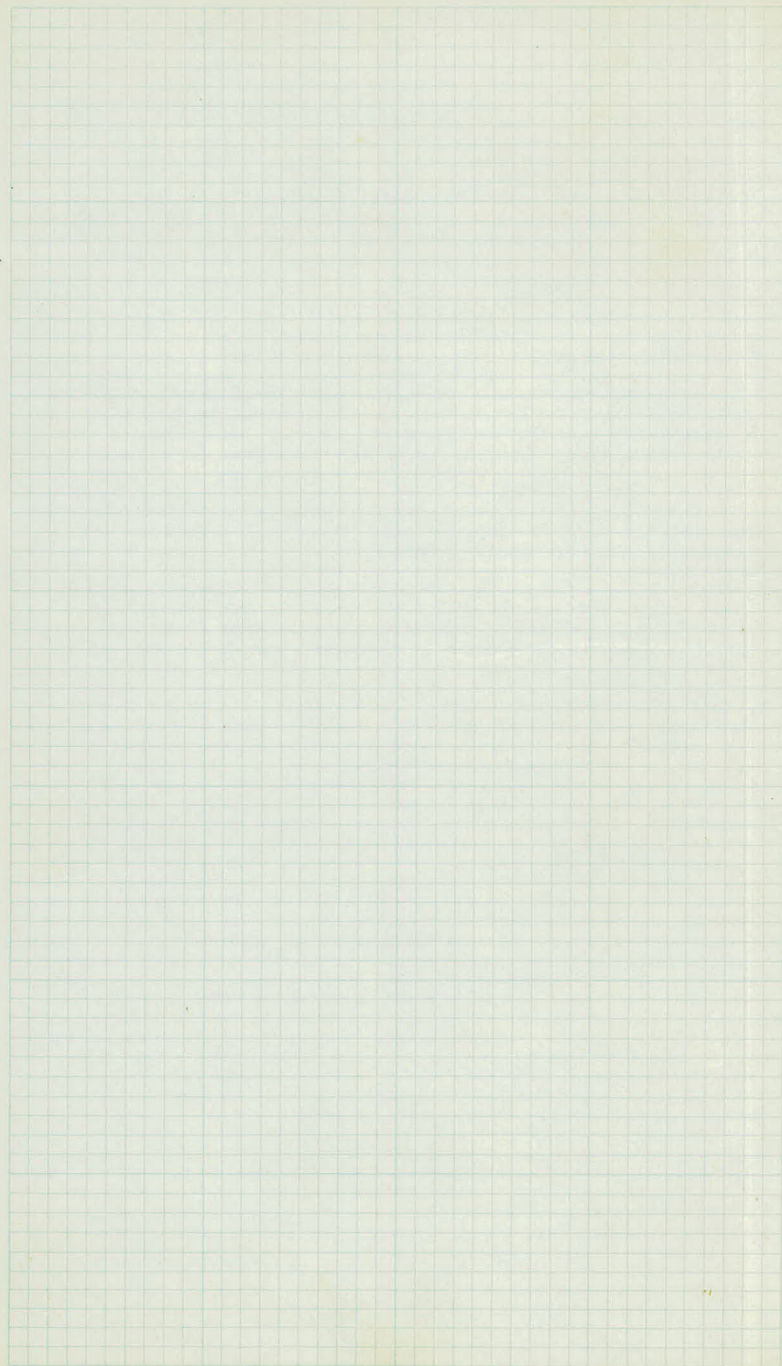
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X-sections - 8-12

10-17-38



1

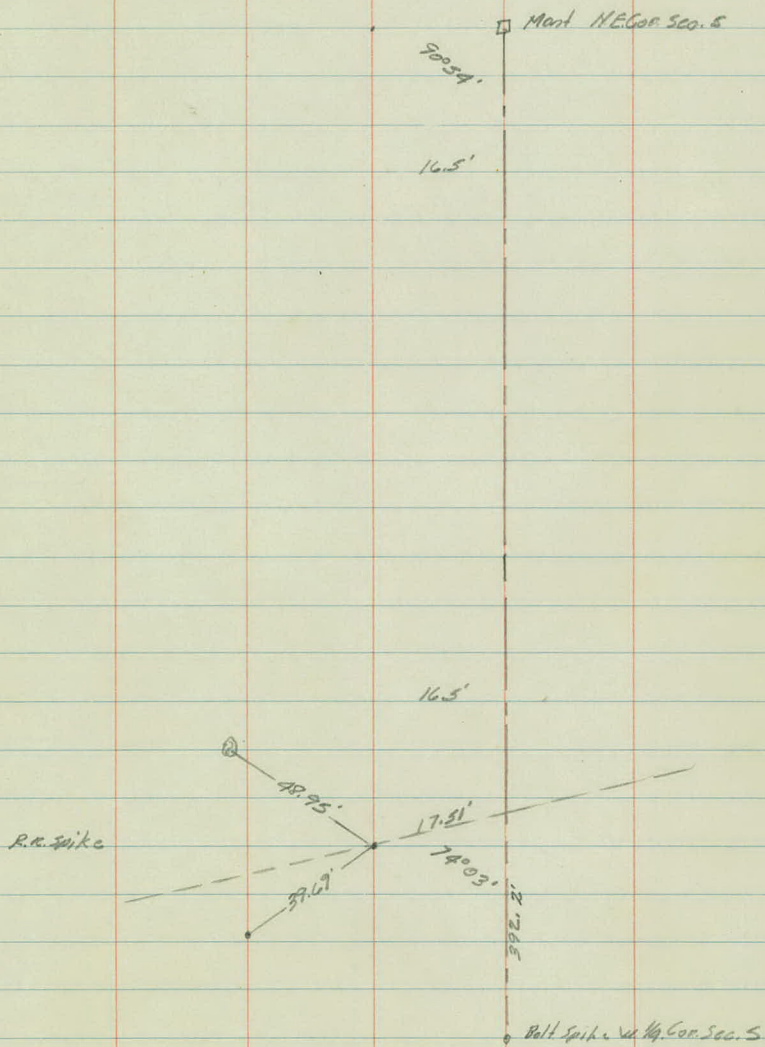
Alignment

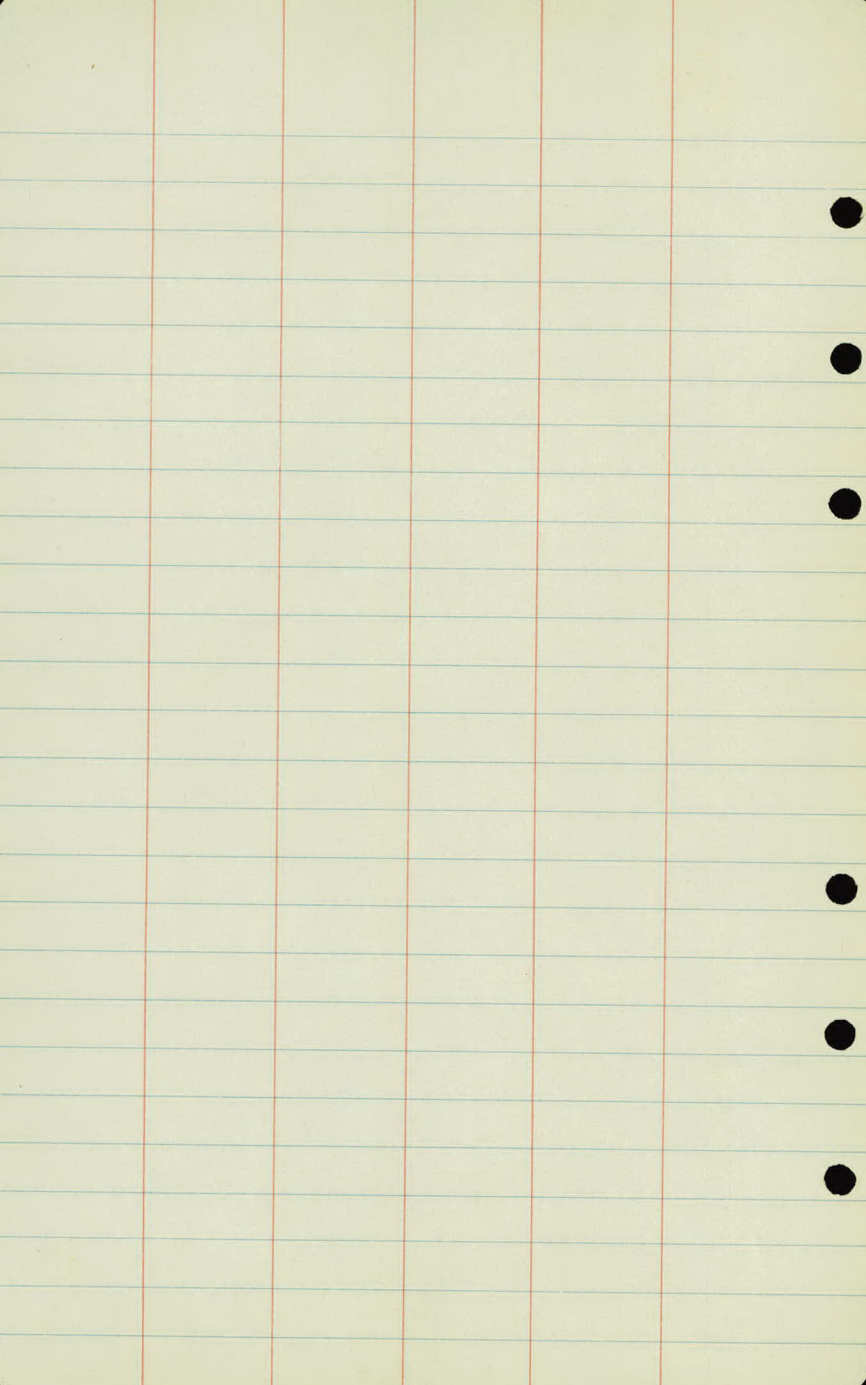
2A 159.6

0400 = 4.19 Bore Rd.

K.F.
L.B.H.
L.C.
M.J.G.

2





Topography

5

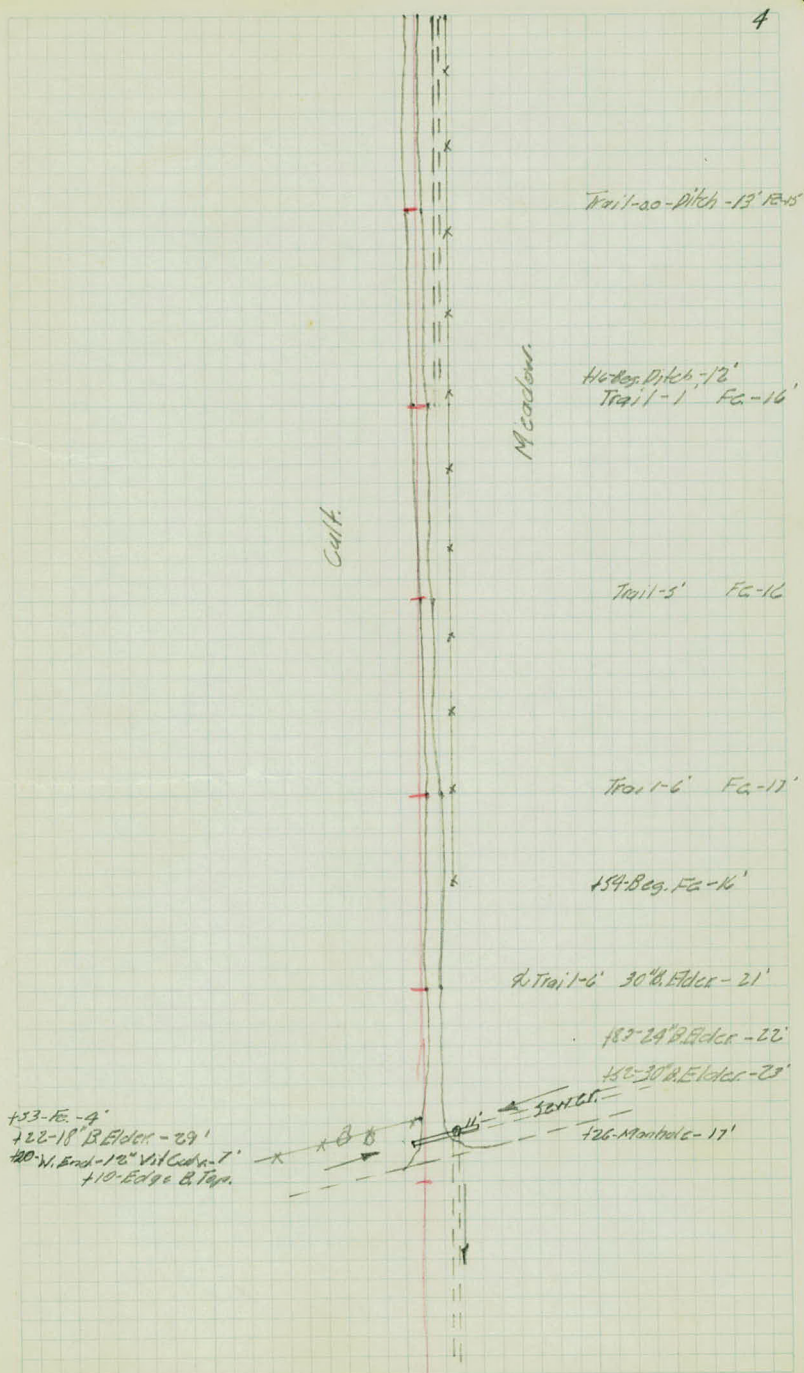
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3

2

1

0+00



12

11

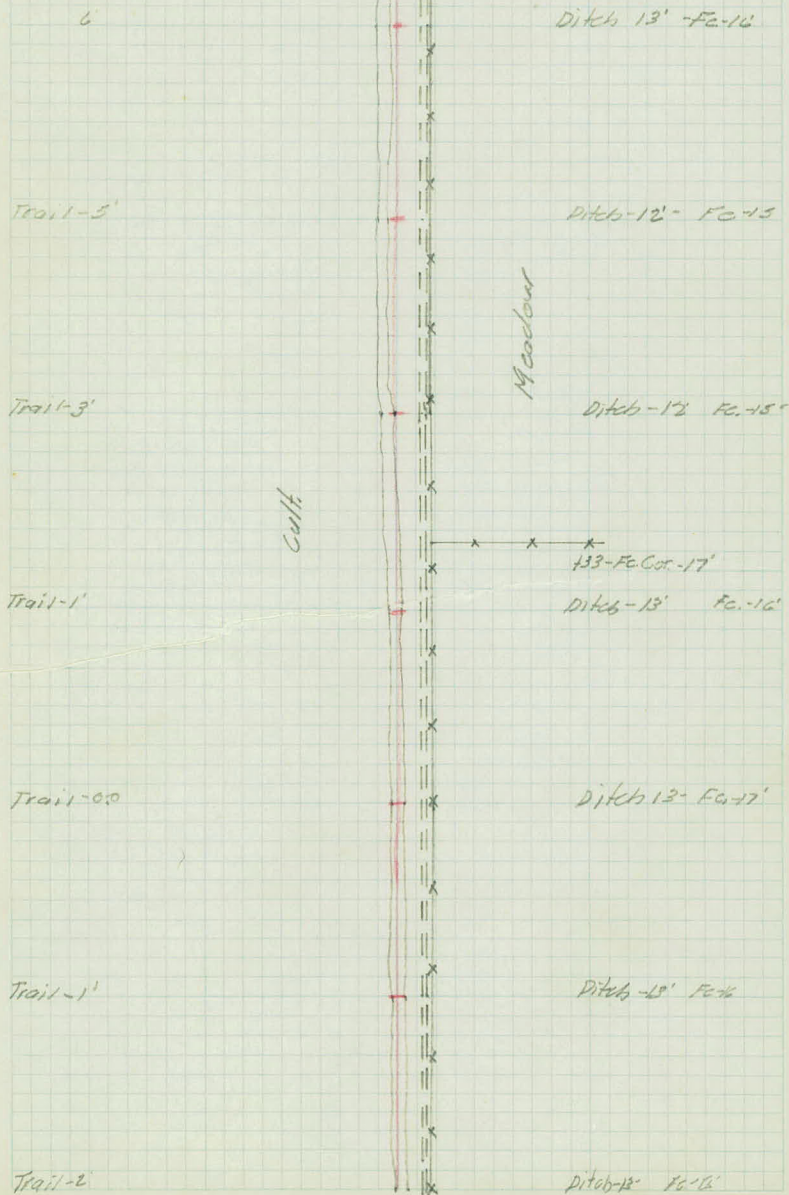
10

9

8

7

6



19

18

17

16

15

14

13

High Line X to Trail 5'

FC-19'

Trails - Shading & Brown

Trail 11'

107-FC Cor-19'

128-FC RS &

Trail 11' FC-19'

Meadow.

Trail 10' - FC-19'

Trail 11' FC-19'

Trail 1' FC-19'

 Δ in Pitch 15'
 178-FC Cor-18'

154-Ditch X to

 103-End &
 110-115'


Trail 6'

Ditch-13-FC-16'

25

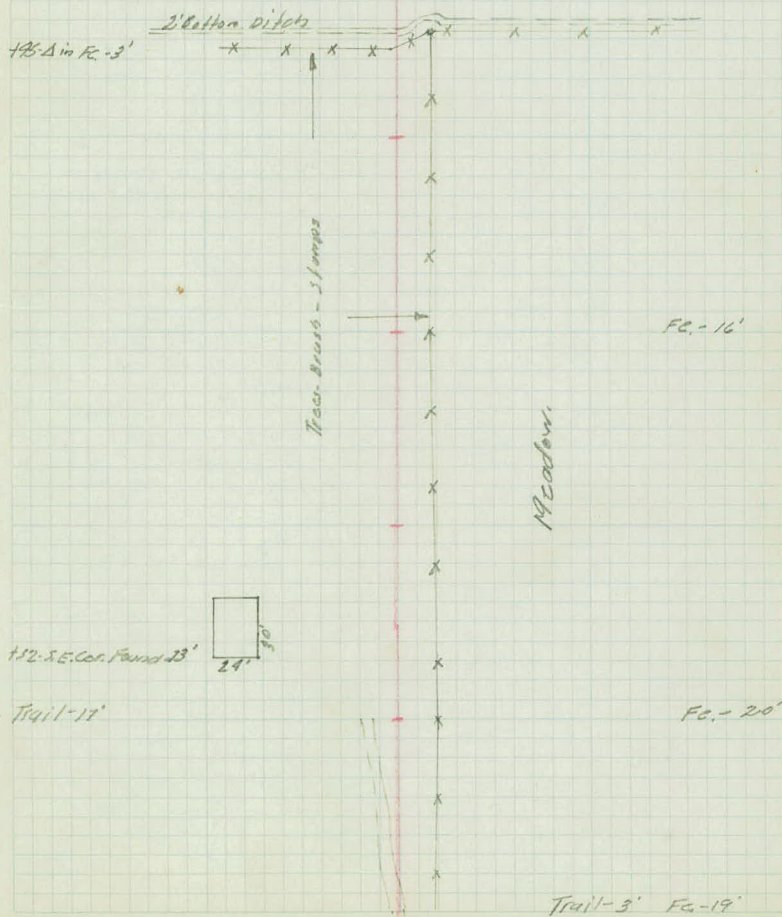
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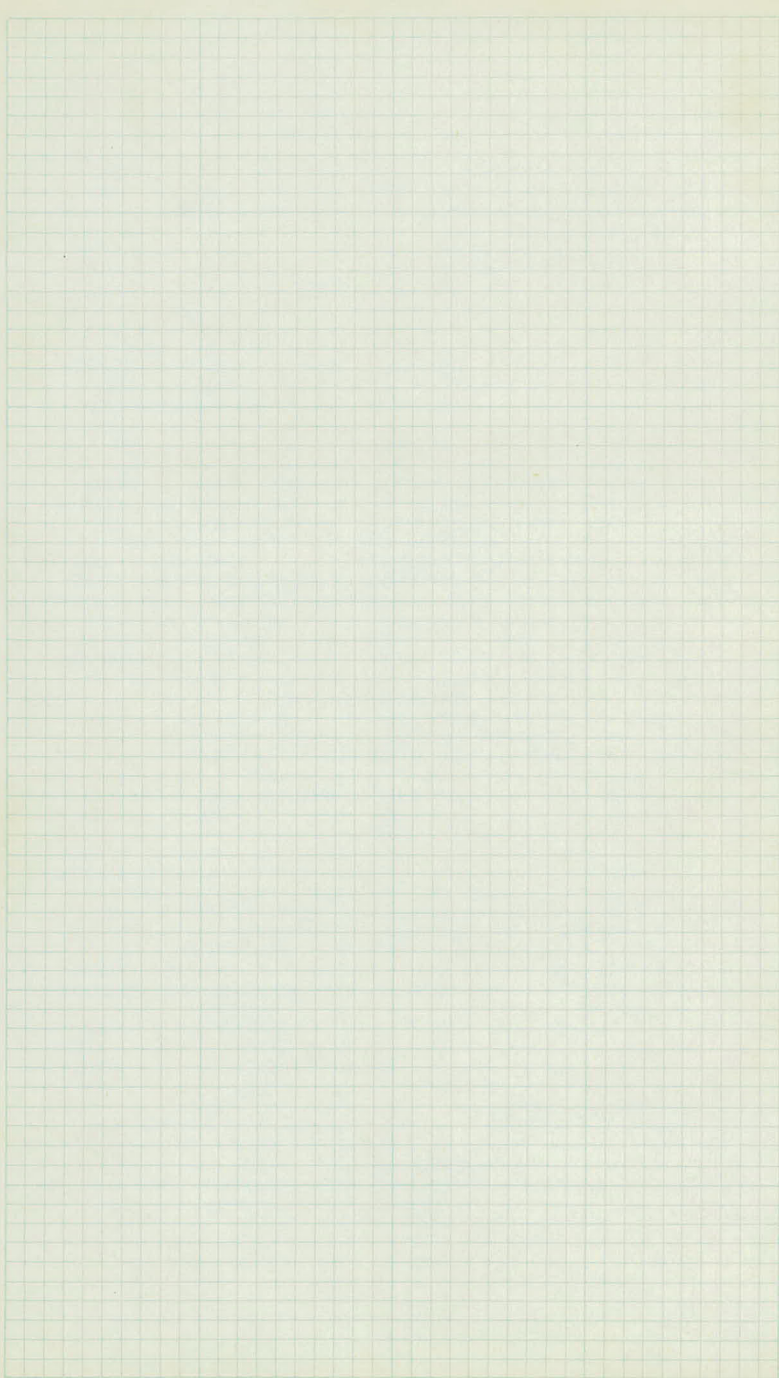
23

22

21

20





X sections

Sta	+	π	-	Elck	
B.M.	11.78	908.77			896.99
T.P.	13.52	922.26	0.03	908.74	
T.P.	1.97	919.23	5.00	917.26	
T.P.	10.43	924.10	5.56	913.67	
T.P.	2.42	919.52	7.00	912.10	
B.M.	9.49	922.67	6.34	913.18	
0	+00			12.7	
	+11			12.5	
	+20			12.5	
	+26				
	+27			12.7	
	+33			15.0	
	+48			13.7	
1	+00			16.4	
	+28			17.7	
T.P.	3.80	922.71	3.26	918.91	

Lt

K

Rt.

Spk. in G.P. Edgerton Harbor.

Top W. Edge Frame Manhole.

10.0

11.9	11.8	10.3	10.2	10.0
<u>20</u>	<u>18</u>	<u>9</u>	<u>10.2</u>	<u>20</u>

Fl. Calc.

11.6	12.0	10.4	10.2	10.0
<u>16.5</u>	<u>7</u>	<u>6</u>	<u>10.2</u>	<u>20</u>

04.87

17.8

F.L. Manhole.

12.1 10.57

F.L. to F. End Culm

56	100	98	100
<u>18</u>	<u>16</u>	<u>22</u>	

51	52	77	92	99
<u>16.5</u>	<u>5</u>		<u>3</u>	<u>16.5</u>

48	47	90	95	95	47
<u>16.5</u>	<u>5</u>	<u>4</u>	<u>12</u>	<u>18</u>	

51	52
<u>16.5</u>	<u>4</u>

63	74	71	53
<u>3</u>	<u>13</u>	<u>16.5</u>	

49
<u>16.5</u>

50

50
<u>16.5</u>

Sta.	+	π	-	E/cv
		922.71		
2				18.1
3				18.4
4				18.0
5				17.7
6				17.6
7				17.5
8				17.8
T.P.	4.72	921.27	5.56	917.15
9				17.2
10				16.9
11				16.5
12				16.6

Lt

K

Rt

$$\frac{4.9}{16.5}$$

$$\frac{4.6}{16.5}$$

$$\frac{4.6}{16.5}$$

$$\frac{4.6}{16.5}$$

$$\frac{4.3}{16.5}$$

$$\frac{4.4}{16.5}$$

$$\frac{4.8}{16.5}$$

$$\frac{4.7}{16.5}$$

$$\frac{4.3}{16.5}$$

$$\frac{5.0}{16.5}$$

$$\frac{5.0}{10} \frac{5.7}{11} \frac{6.3}{12} \frac{6.3}{13} \frac{5.0}{15} \frac{5.0}{16.5}$$

$$\frac{5.0}{16.5}$$

$$\frac{5.1}{11} \frac{5.2}{12} \frac{6.3}{13} \frac{6.3}{15} \frac{5.3}{16.5}$$

$$\frac{5.2}{16.5}$$

$$\frac{5.2}{10} \frac{5.3}{11} \frac{6.4}{12} \frac{6.4}{13} \frac{4.9}{15} \frac{4.9}{16.5}$$

$$\frac{4.9}{16.5}$$

$$\frac{4.9}{19} \frac{5.5}{11} \frac{6.4}{12} \frac{6.4}{13} \frac{5.3}{15} \frac{5.3}{16.5}$$

$$\frac{4.6}{16.5}$$

$$\frac{4.7}{11} \frac{5.2}{12} \frac{5.8}{13} \frac{5.8}{14} \frac{4.6}{15} \frac{4.6}{16.5}$$

$$\frac{4.8}{16.5}$$

$$\frac{5.0}{11} \frac{5.3}{12} \frac{6.2}{13} \frac{6.2}{14} \frac{5.1}{15} \frac{5.1}{16.5}$$

$$\frac{5.0}{16.5}$$

$$\frac{5.4}{10} \frac{5.6}{11} \frac{6.5}{12} \frac{6.5}{13} \frac{5.3}{15} \frac{5.3}{16.5}$$

$$\frac{5.1}{16.5}$$

$$\frac{5.3}{7} \frac{5.3}{13} \frac{6.4}{14} \frac{6.4}{15} \frac{5.3}{16.5}$$

Sta	+	π	-	Elev
		921.87		
13				16.6
14	+78			17.0
	+83	to 3' Bottom Ditch		16.4
	+88			16.8
14				17.2
T.R.	4.69	922.89	3.67	918.20
15				17.5
16				17.5
17				17.6
18				18.0
19				18.1
20				17.9

L4

L6

L1

$$\frac{49}{145}$$

$$\frac{53}{11} \quad \frac{56}{15} \quad \frac{64}{18} \quad \frac{69}{18} \quad \frac{57}{145}$$

$$\frac{48}{145}$$

$$\frac{49}{11} \quad \frac{52}{14} \quad \frac{65}{17} \quad \frac{65}{18} \quad \frac{56}{18}$$

$$\frac{72}{300} \quad \frac{63}{250} \quad \frac{66}{200} \quad \frac{66}{100} \quad \frac{68}{50} \quad \frac{69}{145} \quad \frac{53}{6} \quad \frac{64}{6} \quad \frac{67}{19}$$

$$\frac{50}{145}$$

$$\frac{51}{145}$$

$$\frac{46}{165}$$

$$\frac{46}{145}$$

$$\frac{47}{145}$$

$$\frac{50}{145}$$

$$\frac{50}{145}$$

$$\frac{54}{145}$$

$$\frac{55}{145}$$

$$\frac{55}{145}$$

$$\frac{54}{145}$$

$$\frac{50}{145}$$

$$\frac{54}{145}$$

$$\frac{53}{145}$$

$$\frac{50}{145}$$

$$\frac{49}{145}$$

$$\frac{49}{145}$$

$$\frac{52}{145}$$

$$\frac{47}{145}$$

$$\frac{48}{145}$$

$$\frac{46}{145}$$

$$\frac{50}{165}$$

$$\frac{50}{165}$$

$$\frac{46}{165}$$

Sta.	+	x	-	Elev.
		722.89		
21				18.1
T.P.	4.05	923.41	3.53	919.36
22				18.6
23				17.9
24				18.1
150				18.5
+546	Ditch Lt.			18.6
B.M.		4.92	918.48	918.42

Lt.

Z

Rt.

$$\frac{49}{165}$$

$$\frac{48}{165}$$

$$\frac{47}{165}$$

$$\frac{51}{165}$$

$$\frac{48}{165}$$

$$\frac{47}{165}$$

$$\frac{56}{165}$$

$$\frac{55}{165}$$

$$\frac{53}{165}$$

$$\frac{54}{165}$$

$$\frac{53}{165}$$

$$\frac{55}{165}$$

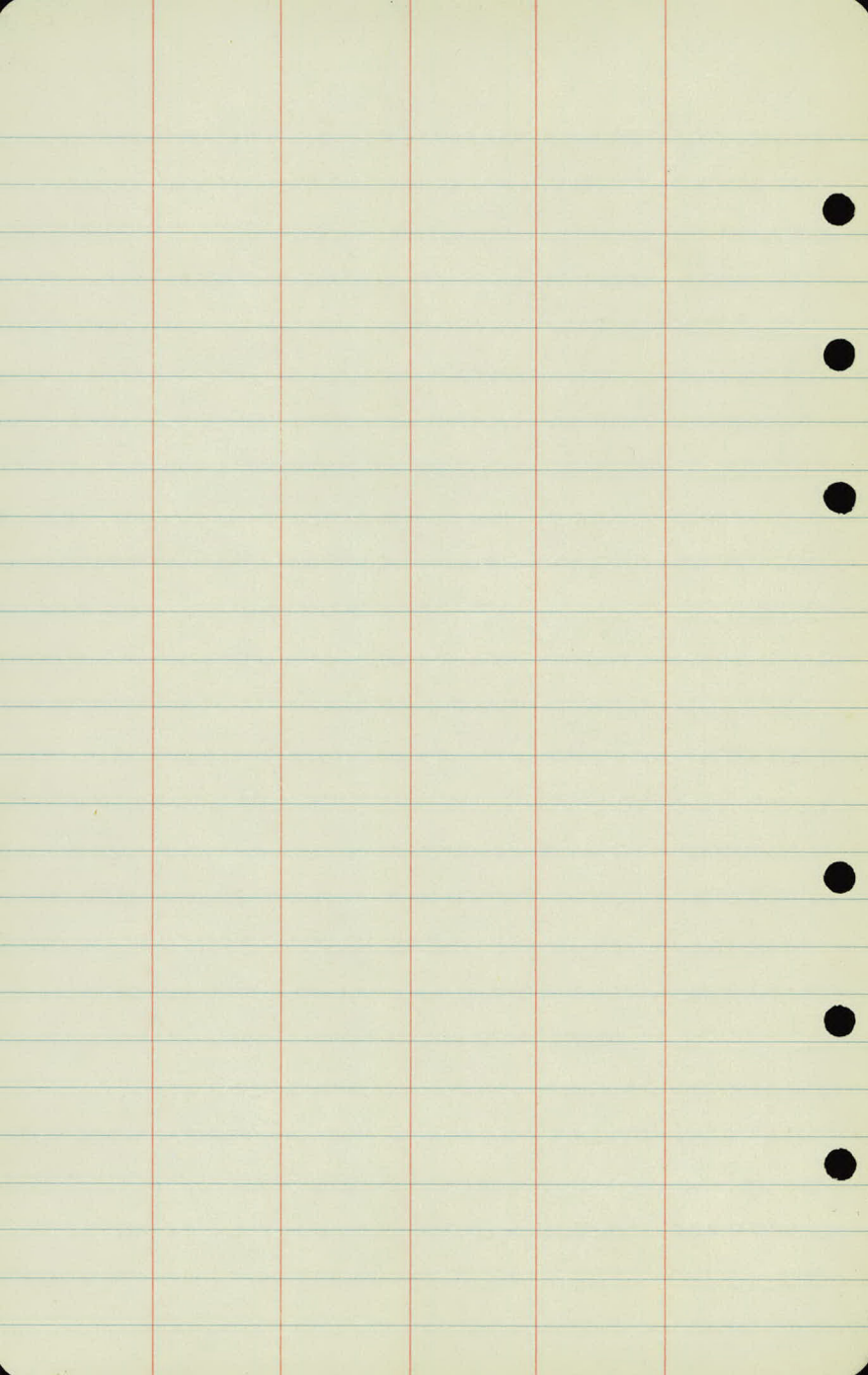
$$\frac{49}{165}$$

$$\frac{49}{165}$$

$$\frac{52}{165}$$

$$\leftarrow \frac{85}{200} \quad \frac{75}{150} \quad \frac{75}{100} \quad \frac{75}{50} \quad \frac{67}{6} \quad \frac{98}{17} \quad \frac{43}{36} \quad \frac{76}{50} \quad \frac{70}{50} \quad \frac{68}{100}$$

Top. Mont. Col. Rd. "D" & Arcade St.



1
Slope stakes

Gravel st.

LaBore to Co. Rd "D"

6 Pages

Sta.	+	x	-	Grade	
B.M.	9.55	922.73			913.18 916.82
0	+00				
	+27			12.6	
	+33			12.9	
	+48			13.8	
1				16.0	
	+28			16.6	
	+50			16.75	
2				16.8	
	+50			16.80	
3				16.9	
T.P.	2.44	922.58	2.59	919.14	
	+50			16.90	

Cor. Rod. Lt. 3. 10 ft

Top W Edge Frame Manhole 17' 10" at 26

Set in stump S. E. Cor. Fire Dept. H. O. Base St.

10.1

$$9.8 \quad \begin{array}{r} 16.5 / 5.2 \\ \hline 19.6 \end{array} \quad \begin{array}{r} 77 \\ \hline 121 \end{array} \quad \begin{array}{r} 96 \\ \hline 192 / 16.5 \end{array}$$

$$8.9 \quad \begin{array}{r} 16.5 / 49 \\ \hline 190 \end{array} \quad \begin{array}{r} 80 \\ \hline 109 \end{array} \quad \begin{array}{r} 53 \\ \hline 196 / 16.5 \end{array}$$

$$6.7 \quad \begin{array}{r} 16.5 / 5.2 \\ \hline 115 \end{array} \quad \begin{array}{r} 64 \\ \hline 103 \end{array} \quad \begin{array}{r} 51 \\ \hline 116 / 16.5 \end{array}$$

$$6.1 \quad \begin{array}{r} 16.5 / 5.0 \\ \hline 111 \end{array} \quad \begin{array}{r} 51 \\ \hline 110 \end{array} \quad \begin{array}{r} 50 \\ \hline 111 / 16.5 \end{array}$$

$$6.0 \quad \begin{array}{r} 16.5 / 49 \\ \hline 111 \end{array} \quad \begin{array}{r} 49 \\ \hline 111 \end{array} \quad \begin{array}{r} 49 \\ \hline 111 / 16.5 \end{array}$$

$$5.9 \quad \begin{array}{r} 16.5 / 49 \\ \hline 110 \end{array} \quad \begin{array}{r} 47 \\ \hline 112 \end{array} \quad \begin{array}{r} 49 \\ \hline 110 / 16.5 \end{array}$$

$$5.9 \quad \begin{array}{r} 16.5 / 49 \\ \hline 110 \end{array} \quad \begin{array}{r} 45 \\ \hline 114 \end{array} \quad \begin{array}{r} 46 \\ \hline 113 / 16.5 \end{array}$$

$$5.8 \quad \begin{array}{r} 16.5 / 47 \\ \hline 111 \end{array} \quad \begin{array}{r} 44 \\ \hline 114 \end{array} \quad \begin{array}{r} 43 \\ \hline 115 / 16.5 \end{array}$$

$$5.7 \quad \begin{array}{r} 16.5 / 45 \\ \hline 112 \end{array} \quad \begin{array}{r} 42 \\ \hline 115 \end{array} \quad \begin{array}{r} 43 \\ \hline 114 / 16.5 \end{array}$$

Sta	+	X	-	Grade
		922.58		

4	100			17.0
---	-----	--	--	------

	150			17.0
--	-----	--	--	------

5				17.1
---	--	--	--	------

	150			17.1
--	-----	--	--	------

6				17.2
---	--	--	--	------

	150			17.2
--	-----	--	--	------

7				17.3
---	--	--	--	------

	150			17.3
--	-----	--	--	------

8				17.4
---	--	--	--	------

T.P.	3.60	921.86	1.32	918.26
------	------	--------	------	--------

	150			17.4
--	-----	--	--	------

9				17.5
---	--	--	--	------

Ger. Wood

Lt

F

Rt

$$5.6 \quad 16.5 / \frac{47}{10.9} \quad \frac{46}{11.0} \quad \frac{44}{11.2} / 16.5'$$

$$5.6 \quad 16.5 / \frac{44}{11.2} \quad \frac{45}{11.1} \quad \frac{48}{10.8} / 16.5$$

$$5.5 \quad 16.5 / \frac{49}{10.6} \quad \frac{50}{10.5} \quad \frac{47}{10.8} / 16.5$$

$$5.5 \quad 16.5 / \frac{49}{10.6} \quad \frac{54}{10.1} \quad \frac{48}{10.7} / 16.5$$

$$5.4 \quad 16.5 / \frac{50}{10.4} \quad \frac{49}{10.5} \quad \frac{50}{10.9} / 16.5$$

$$5.4 \quad 16.5 / \frac{50}{10.4} \quad \frac{51}{10.3} \quad \frac{49}{10.5} / 16.5$$

$$5.3 \quad 16.5 / \frac{50}{10.3} \quad \frac{51}{10.2} \quad \frac{49}{10.4} / 16.5$$

$$5.3 \quad 16.5 / \frac{49}{10.4} \quad \frac{50}{10.3} \quad \frac{53}{10.0} / 16.5$$

$$5.2 \quad 16.5 / \frac{48}{10.4} \quad \frac{50}{10.2} \quad \frac{52}{10.0} / 16.5$$

$$4.8 \quad 16.5 / \frac{43}{10.2} \quad \frac{44}{10.1} \quad \frac{45}{10.0} / 17.5$$

$$4.7 \quad 16.5 / \frac{46}{10.13} \quad \frac{47}{10.3} \quad \frac{48}{10.11} / 16.5$$

Sta	+	π	-	Grade
		921.86		
9	450			17.5
10				17.6
T.P.	3.90	921.69	3.57	918.29
	450			17.6
11				17.7
	450			17.7
12				17.8
T.P.	5.12	922.32	4.49	917.20
	450			17.8
13				17.9
	450			17.9
	450	9.61/4.		18.0
14				18.0

Gr. Rod

Lt

L

Rt

$$4.4 \quad 16.5 / \begin{array}{r} 47 \\ R.12 \end{array} \quad \begin{array}{r} 51 \\ -97 \end{array} \quad \begin{array}{r} 50 \\ R.09 / 16.5 \end{array}$$

$$4.3 \quad 16.5 / \begin{array}{r} 48 \\ R.10 \end{array} \quad \begin{array}{r} 50 \\ -97 \end{array} \quad \begin{array}{r} 51 \\ R.07 / 16.5 \end{array}$$

Nail in Cor. Fe Rod

$$4.1 \quad 16.5 / \begin{array}{r} 48 \\ R.08 \end{array} \quad \begin{array}{r} 53 \\ -12 \end{array} \quad \begin{array}{r} 51 \\ R.05 / 16.5 \end{array}$$

$$4.0 \quad 16.5 / \begin{array}{r} 49 \\ R.06 \end{array} \quad \begin{array}{r} 58 \\ -18 \end{array} \quad \begin{array}{r} 51 \\ R.04 / 16.5 \end{array}$$

$$4.0 \quad 16.5 / \begin{array}{r} 48 \\ R.07 \end{array} \quad \begin{array}{r} 54 \\ -14 \end{array} \quad \begin{array}{r} 51 \\ R.04 / 16.5 \end{array}$$

$$3.9 \quad 16.5 / \begin{array}{r} 50 \\ R.04 \end{array} \quad \begin{array}{r} 55 \\ -16 \end{array} \quad \begin{array}{r} 53 \\ R.01 / 16.5 \end{array}$$

Top S.S. Rod

$$4.5 \quad 16.5 / \begin{array}{r} 54 \\ R.06 \end{array} \quad \begin{array}{r} 57 \\ -14 \end{array} \quad \begin{array}{r} 57 \\ R.03 / 16.5 \end{array}$$

$$4.4 \quad 16.5 / \begin{array}{r} 54 \\ R.08 \end{array} \quad \begin{array}{r} 58 \\ -14 \end{array} \quad \begin{array}{r} 67 \\ -23 / 14.9 \end{array}$$

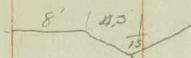
$$4.4 \quad 16.5 / \begin{array}{r} 52 \\ R.07 \end{array} \quad \begin{array}{r} 55 \\ -11 \end{array} \quad \begin{array}{r} 66 \\ -22 / 14.6 \end{array}$$

Fl. Curv. set at 17.2

4.3

$$4.3 \quad 16.5 / \begin{array}{r} 52 \\ R.06 \end{array} \quad \begin{array}{r} 52 \\ -97 \end{array} \quad \begin{array}{r} 50 \\ R.04 / 16.5 \end{array}$$

Sta	+	x	-	Grade
		722.32		
14	+50			180
15				18.1
	+50			181
16				182
	+50			182
17				183
	+50			183
18				18.4
T.P.	2.98	722.05	2.25	722.07
	+50			18.4
19				18.5
	+50			18.5



Ger. 1000

Lt

Rt

Rt

$$4.3 \quad 16.5 \overline{) \frac{51}{R.07}}$$

$$\frac{50}{-07}$$

$$\frac{50}{R.07/16.5}$$

$$4.2 \quad 16.5 \overline{) \frac{49}{R.08}}$$

$$\frac{49}{-08}$$

$$\frac{49}{R.10/16.5}$$

$$4.2 \quad 16.5 \overline{) \frac{49}{R.08}}$$

$$\frac{50}{-08}$$

$$\frac{49}{R.08/16.5}$$

$$4.1 \quad 16.5 \overline{) \frac{48}{R.08}}$$

$$\frac{49}{-08}$$

$$\frac{46}{R.10/16.5}$$

$$4.1 \quad 16.5 \overline{) \frac{50}{R.06}}$$

$$\frac{48}{-07}$$

$$\frac{46}{R.10/16.5}$$

$$4.0 \quad 16.5 \overline{) \frac{48}{R.07}}$$

$$\frac{48}{-08}$$

$$\frac{44}{R.11/16.5}$$

$$4.0 \quad 16.5 \overline{) \frac{48}{R.07}}$$

$$\frac{48}{-08}$$

$$\frac{45}{R.10/16.5}$$

$$3.9 \quad 16.5 \overline{) \frac{44}{R.10}}$$

$$\frac{44}{-05}$$

$$\frac{46}{R.03/16.5}$$

$$4.7 \quad 16.5 \overline{) \frac{97}{R.00}}$$

$$\frac{46}{-01}$$

$$\frac{47}{R.00/16.5}$$

$$4.6 \quad 16.5 \overline{) \frac{50}{R.11}}$$

$$\frac{50}{-04}$$

$$\frac{48}{R.13/16.5}$$

$$4.6 \quad 16.5 \overline{) \frac{50}{R.11}}$$

$$\frac{50}{-04}$$

$$\frac{47}{R.14/16.5}$$

Sta.	+	Σ	-	Grade
		923.05		
20				18.6
	+50			18.6
21				18.7
	+50			18.7
22				18.8
T.P.	8.67	922.97	2.74	919.31
	+50			18.8
23				18.9
	+50			18.9
24				19.0
	+50			19.1
T.P.	9.50	923.04	2.49	919.54
B.M.			4.59	918.45
				918.42

918.42

10/29/38

6

Gr. Road

L1

L2

L3

$$4.5 \quad 16.5 / \frac{52}{R.08} \quad \frac{54}{-0.9} \quad \frac{4.9}{R.11 / 16.5'}$$

$$4.5 \quad 16.5 / \frac{51}{R.09} \quad \frac{52}{-0.7} \quad \frac{5.1}{R.09 / 16.5}$$

$$4.4 \quad 16.5 / \frac{51}{R.08} \quad \frac{50}{-0.6} \quad \frac{4.9}{R.10 / 16.5}$$

$$4.4 \quad 16.5 / \frac{47}{R.12} \quad \frac{46}{-0.2} \quad \frac{4.6}{R.12 / 16.5}$$

$$4.3 \quad 16.5 / \frac{45}{R.12} \quad \frac{44}{-0.1} \quad \frac{4.4}{R.12 / 16.5}$$

$$4.2 \quad 16.5 / \frac{48}{R.09} \quad \frac{47}{-0.5} \quad \frac{4.5}{R.12 / 16.5}$$

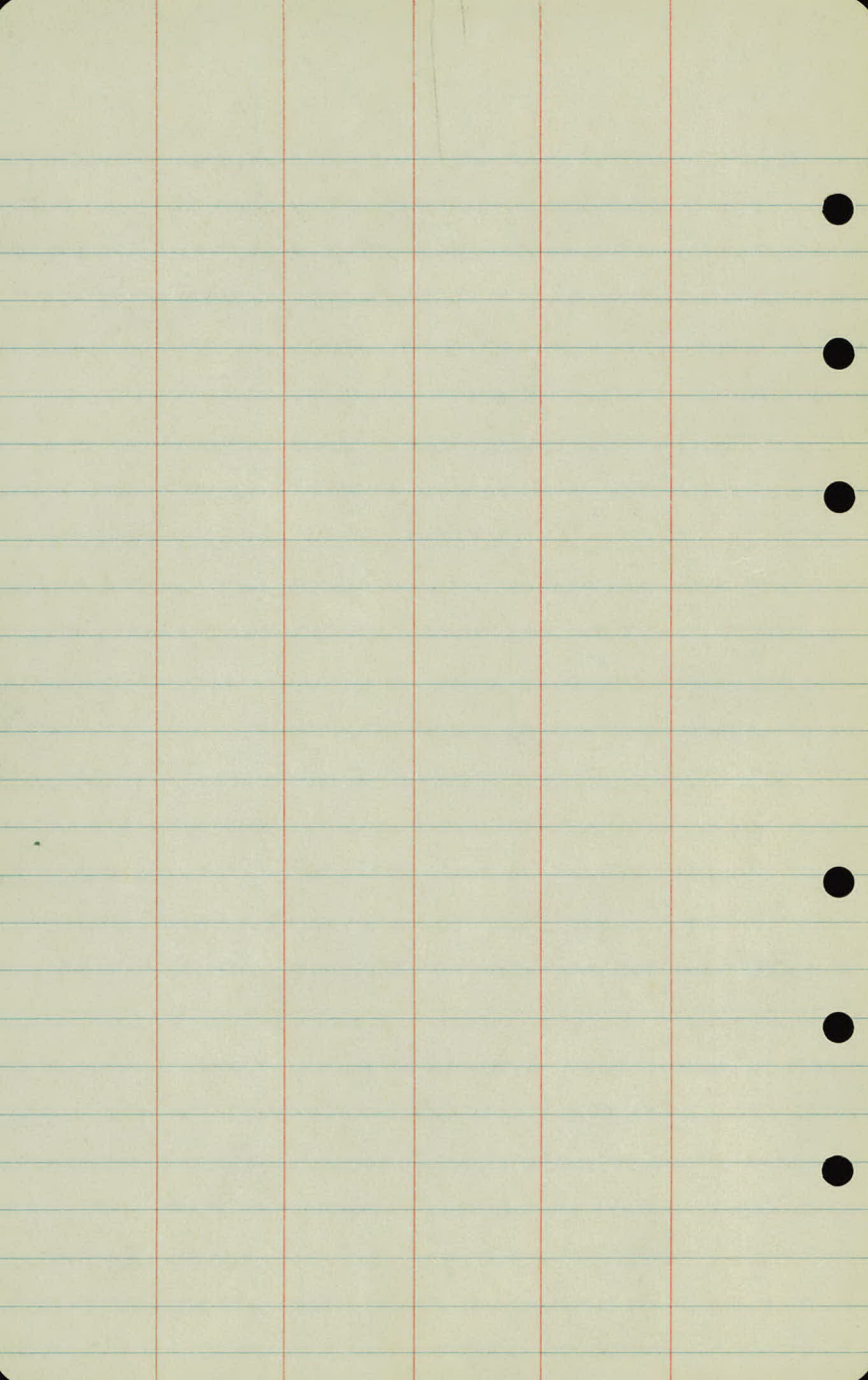
$$4.1 \quad 16.5 / \frac{5.1}{R.05} \quad \frac{50}{-0.9} \quad \frac{4.9}{R.07 / 16.5}$$

$$4.1 \quad 16.5 / \frac{5.0}{R.06} \quad \frac{5.0}{-0.9} \quad \frac{5.0}{R.06 / 16.5}$$

$$4.0 \quad 16.5 / \frac{4.9}{R.06} \quad \frac{4.9}{-0.9} \quad \frac{5.1}{R.09 / 16.5}$$

$$3.9 \quad 16.5 / \frac{4.7}{R.02} \quad \frac{4.6}{R.05 / 16.5'}$$

Top Mont



Arcade St.

Miss. St. To 624' South

B.M.	2.58	915.33	912.75	Rod
19+76			11.7	3.6

20		5.0	11.7	3.6
----	--	-----	------	-----

+50			11.6	3.7
-----	--	--	------	-----

21		5.1	11.6	3.7
----	--	-----	------	-----

+50			11.5	3.8
-----	--	--	------	-----

22		5.0	11.5	3.8
----	--	-----	------	-----

+50			11.4	3.9
-----	--	--	------	-----

23		5.2	11.4	3.9
----	--	-----	------	-----

+50			11.3	4.0
-----	--	--	------	-----

24		4.7	11.3	4.0
----	--	-----	------	-----

+50			11.2	4.1
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$$\begin{array}{r} 4.0 \cancel{6} \\ 22.2 \overline{) 5.0} \end{array}$$

$$\begin{array}{r} 4.7 \\ -1.1 \end{array}$$

$$\begin{array}{r} 4.0 \cancel{8} \\ 22.8 \overline{) 4.7} \end{array}$$

$$\begin{array}{r} 4.0 \cancel{6} \\ 22.2 \overline{) 5.0} \end{array}$$

$$\begin{array}{r} 4.6 \\ -1.0 \end{array}$$

$$\begin{array}{r} 4.1 \cancel{8} \\ 23.0 \overline{) 4.6} \end{array}$$

$$\begin{array}{r} 4.0 \cancel{5} \\ 22.0 \overline{) 5.2} \end{array}$$

$$\begin{array}{r} 4.9 \\ -1.2 \end{array}$$

$$\begin{array}{r} 4.1 \cancel{0} \\ 23.0 \overline{) 4.7} \end{array}$$

$$\begin{array}{r} 4.0 \cancel{6} \\ 22.2 \overline{) 5.1} \end{array}$$

$$\begin{array}{r} 5.0 \\ -1.3 \end{array}$$

$$\begin{array}{r} 4.0 \cancel{8} \\ 22.6 \overline{) 4.9} \end{array}$$

$$\begin{array}{r} 4.0 \cancel{8} \\ 22.6 \overline{) 5.0} \end{array}$$

$$\begin{array}{r} 4.9 \\ -1.1 \end{array}$$

$$\begin{array}{r} 4.1 \cancel{1} \\ 23.2 \overline{) 4.7} \end{array}$$

$$\begin{array}{r} 4.1 \cancel{1} \\ 23.2 \overline{) 4.7} \end{array}$$

$$\begin{array}{r} 4.7 \\ -0.9 \end{array}$$

$$\begin{array}{r} 4.1 \cancel{0} \\ 23.0 \overline{) 4.8} \end{array}$$

$$\begin{array}{r} 4.1 \cancel{3} \\ 23.6 \overline{) 4.6} \end{array}$$

$$\begin{array}{r} 4.4 \\ -0.3 \end{array}$$

$$\begin{array}{r} 4.1 \cancel{5} \\ 24.0 \overline{) 4.4} \end{array}$$

$$\begin{array}{r} 4.0 \cancel{9} \\ 22.8 \overline{) 5.0} \end{array}$$

$$\begin{array}{r} 4.8 \\ -0.9 \end{array}$$

$$\begin{array}{r} 4.1 \cancel{5} \\ 23.6 \overline{) 4.6} \end{array}$$

$$\begin{array}{r} 4.1 \cancel{4} \\ 23.8 \overline{) 4.6} \end{array}$$

$$\begin{array}{r} 4.8 \\ 7 \end{array}$$

$$\begin{array}{r} 4.4 \\ -0.4 \end{array}$$

$$\begin{array}{r} 4.1 \cancel{3} \\ 23.6 \overline{) 4.7} \end{array}$$

$$\begin{array}{r} 4.1 \cancel{3} \\ 23.6 \overline{) 4.7} \end{array}$$

$$\begin{array}{r} 4.7 \\ 8 \end{array}$$

$$\begin{array}{r} 4.2 \\ -0.2 \end{array}$$

$$\begin{array}{r} 4.1 \cancel{6} \\ 24.2 \overline{) 4.4} \end{array}$$

$$\begin{array}{r} 4.1 \cancel{6} \\ 24.2 \overline{) 4.5} \end{array}$$

$$\begin{array}{r} 4.7 \\ 8 \end{array}$$

$$\begin{array}{r} 4.2 \\ -0.1 \end{array}$$

$$\begin{array}{r} 4.1 \cancel{6} \\ 24.2 \overline{) 4.5} \end{array}$$

915.33

25

5.4

11.2

4.1

+50

11.1

4.2

26

11.1

4.2

$$\frac{26.07}{5.4} \\ \hline 22.4$$

$$\frac{5.0}{-0.9}$$

$$\frac{26.11}{5.0} \\ \hline 23.2$$

$$\frac{26.12}{5.0} \\ \hline 23.4$$

$$\frac{4.1}{+0.1}$$

$$\frac{26.18}{4.4} \\ \hline 24.6$$

$$\frac{26.14}{4.8} \\ \hline 23.8$$

$$\frac{3.2}{+0.5}$$

$$\frac{26.18}{4.3} \\ \hline 24.8$$

