

DR 12-A - BK 22

OFFICE OF COUNTY ENGINEER
RAMSEY CO. MINN.

PLAN Survey

LAKE ST

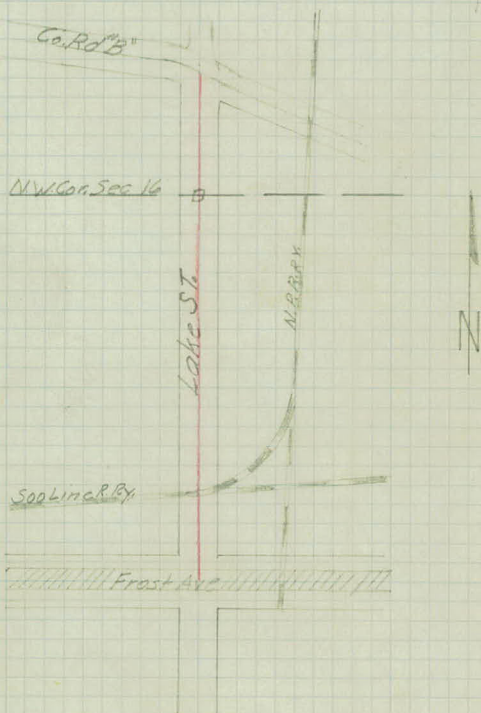
From FROST AVE To Co Rd "B"

Road Acc't. No. N-8

Date Filed June 38

D/2A-1322
File

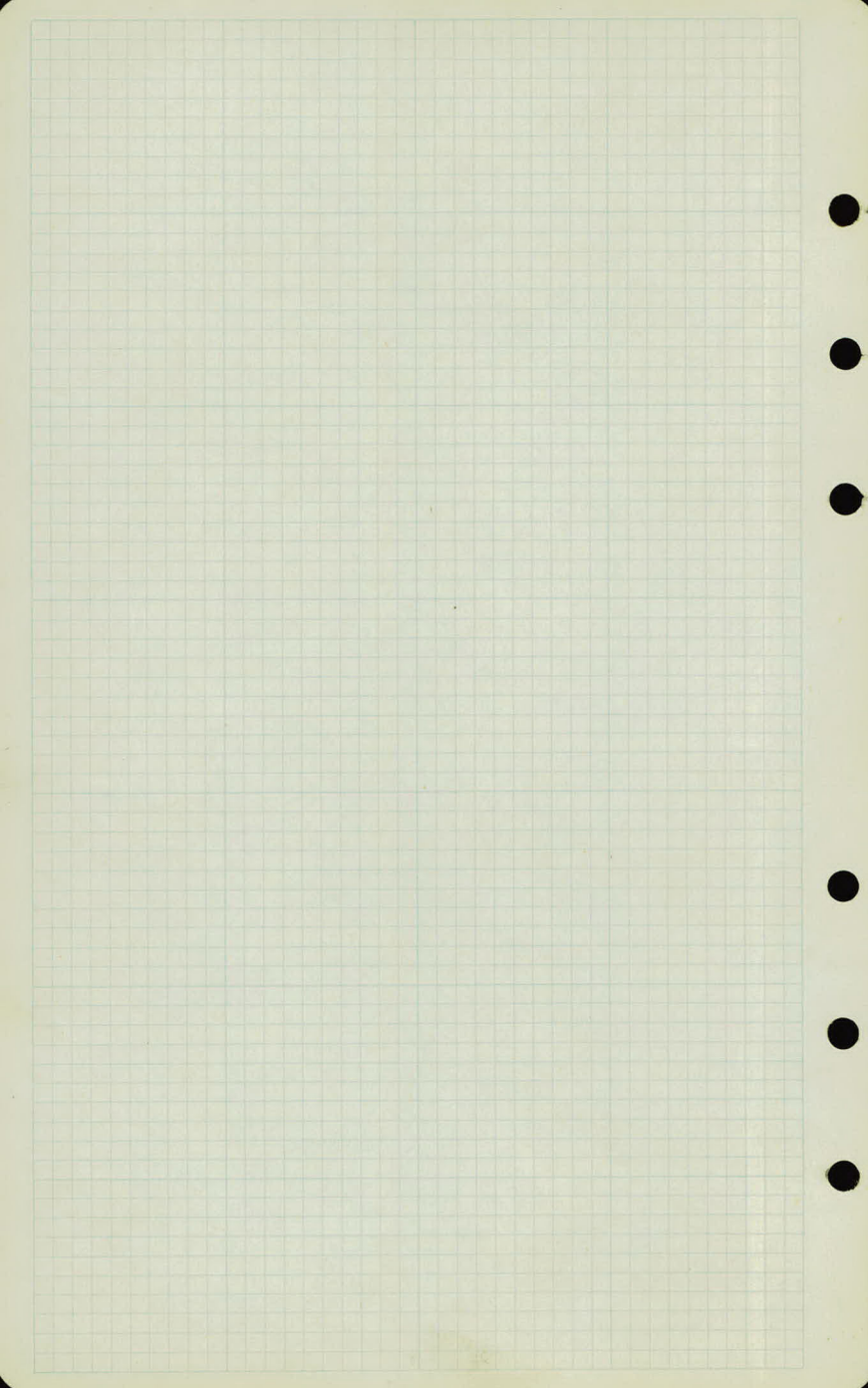
PLAN SURVEY
LAKE ST.
from
Frost Ave to Co. Rd "B"



INDEX

Align P. 1-3
Topog - 4-9
X-sections - 10-20
Levels - P. 20

H. Anker
4/1/38



Alignment

Sta	Point	ΔL	ΔR
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43 + 00	P.O.T.		
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33 + 5472	P.O.T.	= F. Soosling & N.P.R.R. Corner	
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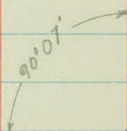
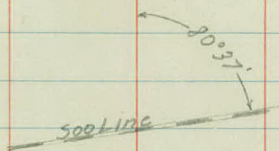
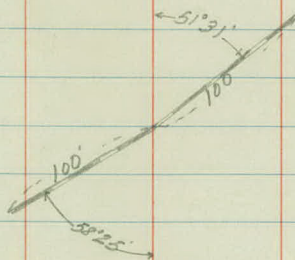
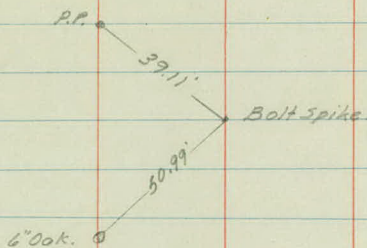
32 + 58	P.O.T.	= F. Soosling & P.Ry.	
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26 + 3912	= F. Frost Ave.		
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Lt

Rt

Rt



Brass Plug in Pav.

Sta	Point	ΔL	ΔR
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59 + 11.07 = Approx 2 Co Rd "B"

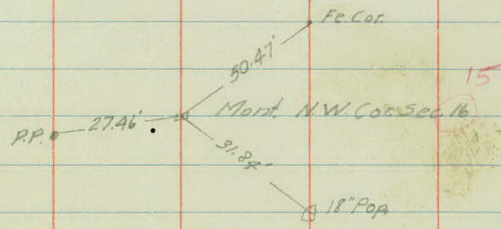
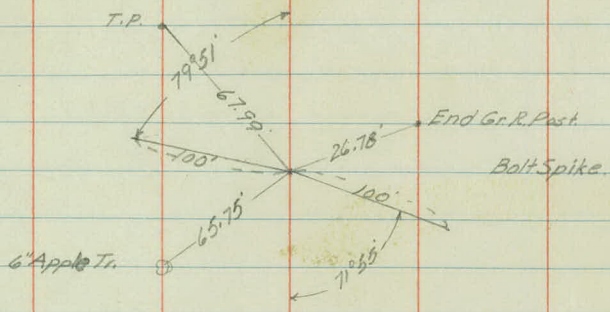
52 + 18.68 P.I.

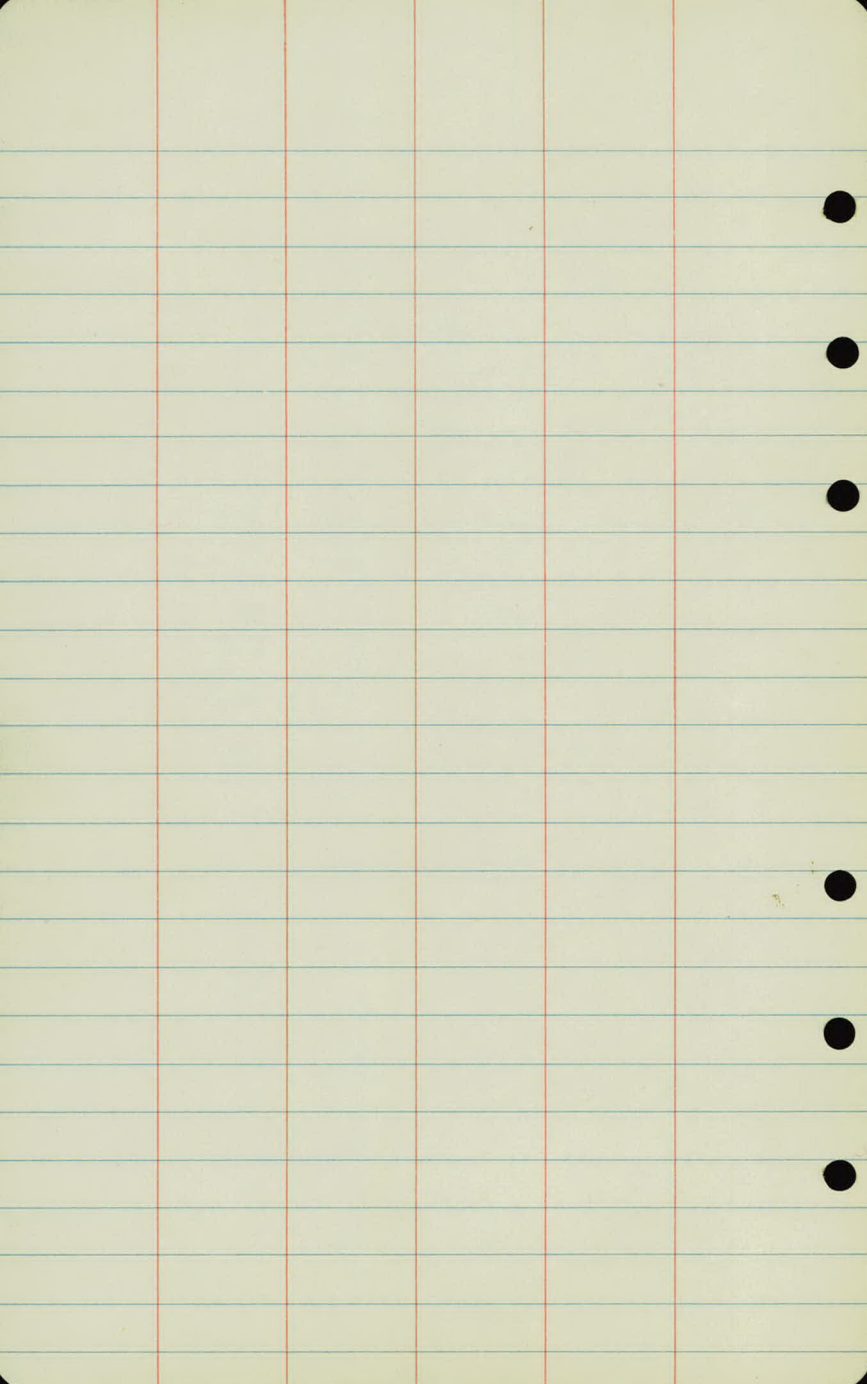
$0^{\circ} 21\frac{1}{2}''$

Lt.

E

Rt.





X Sections

Sta	+	π	-	Elev
B.M.	5.51	901.55		896.04

26 + 39.12

+99.12

896.0

+59

96.2

+65

96.1

27

95.7

+23

95.8

+27

95.8

+54

96.0

+83

96.3

+87

96.0

28

96.4

+50

96.9

Lt

E

Rt

Top Brass Plug Frost Ave + Lake St.

$$\begin{array}{r} 5.97 \\ 50 \end{array} \quad \begin{array}{r} 5.6 \\ 50 \end{array} \quad \begin{array}{r} 5.6 \\ 50 \end{array}$$

$$\begin{array}{r} 5.7 \\ 50 \end{array} \quad \begin{array}{r} 5.7 \\ 30 \end{array} \quad \begin{array}{r} 6.0 \\ 19 \end{array} \quad \begin{array}{r} 5.4 \\ 50 \end{array} \quad \begin{array}{r} 5.5 \\ 26 \end{array} \quad \begin{array}{r} 5.3 \\ 50 \end{array}$$

$$\begin{array}{r} 8.0 \\ 50 \end{array} \quad \begin{array}{r} 7.6 \\ 36 \end{array} \quad \begin{array}{r} 7.6 \\ 21 \end{array} \quad \begin{array}{r} 6.0 \\ 16 \end{array} \quad \begin{array}{r} 5.5 \\ 50 \end{array} \quad \begin{array}{r} 5.6 \\ 29 \end{array} \quad \begin{array}{r} 5.7 \\ 50 \end{array}$$

$$\begin{array}{r} 7.5 \\ 50 \end{array} \quad \begin{array}{r} 7.3 \\ 33 \end{array} \quad \begin{array}{r} 7.1 \\ 29 \end{array} \quad \begin{array}{r} 8.4 \\ 23 \end{array} \quad \begin{array}{r} 6.1 \\ 13 \end{array} \quad \begin{array}{r} 5.9 \\ 50 \end{array} \quad \begin{array}{r} 6.0 \\ 10 \end{array} \quad \begin{array}{r} 5.7 \\ 31 \end{array} \quad \begin{array}{r} 4.8 \\ 50 \end{array}$$

$$\begin{array}{r} 7.1 \\ 50 \end{array} \quad \begin{array}{r} 6.9 \\ 33 \end{array} \quad \begin{array}{r} 6.4 \\ 29 \end{array} \quad \begin{array}{r} 7.9 \\ 21 \end{array} \quad \begin{array}{r} 6.1 \\ 12 \end{array} \quad \begin{array}{r} 5.8 \\ 50 \end{array} \quad \begin{array}{r} 6.4 \\ 11 \end{array} \quad \begin{array}{r} 5.3 \\ 33 \end{array} \quad \begin{array}{r} 5.1 \\ 50 \end{array}$$

$$\begin{array}{r} 7.0 \\ 50 \end{array} \quad \begin{array}{r} 6.9 \\ 33 \end{array} \quad \begin{array}{r} 6.2 \\ 29 \end{array} \quad \begin{array}{r} 7.8 \\ 22 \end{array} \quad \begin{array}{r} 6.1 \\ 13 \end{array} \quad \begin{array}{r} 5.8 \\ 50 \end{array} \quad \begin{array}{r} 6.8 \\ 16 \end{array} \quad \begin{array}{r} 7.8 \\ 19 \end{array} \quad \begin{array}{r} 6.9 \\ 33 \end{array} \quad \begin{array}{r} 7.0 \\ 50 \end{array}$$

$$\begin{array}{r} 6.6 \\ 50 \end{array} \quad \begin{array}{r} 6.6 \\ 33 \end{array} \quad \begin{array}{r} 6.3 \\ 28 \end{array} \quad \begin{array}{r} 7.4 \\ 23 \end{array} \quad \begin{array}{r} 6.7 \\ 18 \end{array} \quad \begin{array}{r} 5.9 \\ 13 \end{array} \quad \begin{array}{r} 5.6 \\ 50 \end{array} \quad \begin{array}{r} 6.1 \\ 15 \end{array} \quad \begin{array}{r} 5.6 \\ 33 \end{array}$$

$$\begin{array}{r} 6.1 \\ 50 \end{array} \quad \begin{array}{r} 6.0 \\ 33 \end{array} \quad \begin{array}{r} 5.9 \\ 27 \end{array} \quad \begin{array}{r} 7.0 \\ 22 \end{array} \quad \begin{array}{r} 7.0 \\ 17 \end{array} \quad \begin{array}{r} 5.6 \\ 10 \end{array} \quad \begin{array}{r} 5.3 \\ 33 \end{array} \quad \begin{array}{r} 5.6 \\ 10 \end{array} \quad \begin{array}{r} 5.2 \\ 33 \end{array} \quad \begin{array}{r} 5.2 \\ 50 \end{array}$$

$$\begin{array}{r} 6.1 \\ 50 \end{array} \quad \begin{array}{r} 5.9 \\ 33 \end{array} \quad \begin{array}{r} 5.4 \\ 27 \end{array} \quad \begin{array}{r} 7.1 \\ 23 \end{array} \quad \begin{array}{r} 6.9 \\ 17 \end{array} \quad \begin{array}{r} 5.6 \\ 13 \end{array} \quad \begin{array}{r} 5.6 \\ 10 \end{array} \quad \begin{array}{r} 5.7 \\ 17 \end{array} \quad \begin{array}{r} 7.2 \\ 24 \end{array} \quad \begin{array}{r} 5.6 \\ 33 \end{array} \quad \begin{array}{r} 4.7 \\ 50 \end{array}$$

$$\begin{array}{r} 5.7 \\ 50 \end{array} \quad \begin{array}{r} 5.5 \\ 33 \end{array} \quad \begin{array}{r} 5.1 \\ 27 \end{array} \quad \begin{array}{r} 6.7 \\ 23 \end{array} \quad \begin{array}{r} 6.7 \\ 17 \end{array} \quad \begin{array}{r} 5.4 \\ 13 \end{array} \quad \begin{array}{r} 5.2 \\ 50 \end{array} \quad \begin{array}{r} 5.6 \\ 10 \end{array} \quad \begin{array}{r} 6.9 \\ 15 \end{array} \quad \begin{array}{r} 6.9 \\ 18 \end{array} \quad \begin{array}{r} 4.1 \\ 27 \end{array} \quad \begin{array}{r} 4.2 \\ 33 \end{array} \quad \begin{array}{r} 4.1 \\ 50 \end{array}$$

$$\begin{array}{r} 4.5 \\ 50 \end{array} \quad \begin{array}{r} 4.0 \\ 33 \end{array} \quad \begin{array}{r} 3.5 \\ 29 \end{array} \quad \begin{array}{r} 6.6 \\ 22 \end{array} \quad \begin{array}{r} 6.3 \\ 17 \end{array} \quad \begin{array}{r} 5.1 \\ 14 \end{array} \quad \begin{array}{r} 4.7 \\ 50 \end{array} \quad \begin{array}{r} 5.1 \\ 9 \end{array} \quad \begin{array}{r} 7.0 \\ 14 \end{array} \quad \begin{array}{r} 7.1 \\ 18 \end{array} \quad \begin{array}{r} 2.4 \\ 27 \end{array} \quad \begin{array}{r} 2.7 \\ 33 \end{array} \quad \begin{array}{r} 3.2 \\ 50 \end{array}$$

Sta	+	π	-	Elev
		901.55		
29				896.7
+ 50				96.4
30				96.3
+ 50				96.3
T.P.	6.25	902.49 [✓]	5.31	896.24 [✓]
31				96.3 . x
+ 50				96.6
32				97.1
+ 12				97.2
+ 23				97.3
+ 34				97.5
+ 43				97.7

Lt

E

Rt

$\frac{4.4}{50}$	$\frac{3.7}{33}$	$\frac{3.3}{29}$	$\frac{6.1}{23}$	$\frac{5.9}{16}$	$\frac{5.2}{14}$	$\frac{4.9}{10}$	$\frac{5.3}{10}$	$\frac{6.7}{15}$	$\frac{6.7}{18}$	$\frac{4.5}{25}$	$\frac{4.5}{33}$	$\frac{3.8}{50}$
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$\frac{5.0}{50}$	$\frac{4.5}{33}$	$\frac{4.5}{29}$	$\frac{5.9}{23}$	$\frac{5.8}{19}$	$\frac{5.3}{15}$	$\frac{5.2}{7}$	$\frac{5.5}{7}$	$\frac{5.5}{18}$	$\frac{5.1}{19}$	$\frac{4.3}{33}$	$\frac{4.3}{50}$
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$\frac{5.1}{50}$	$\frac{4.8}{33}$	$\frac{4.7}{29}$	$\frac{6.1}{24}$	$\frac{6.1}{21}$	$\frac{5.5}{16}$	$\frac{5.3}{8}$	$\frac{5.7}{8}$	$\frac{6.2}{11}$	$\frac{6.0}{13}$	$\frac{4.9}{33}$	$\frac{5.2}{50}$
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$\frac{6.3}{50}$	$\frac{6.2}{33}$	$\frac{5.9}{30}$	$\frac{7.0}{24}$	$\frac{6.9}{22}$	$\frac{5.7}{17}$	$\frac{5.2}{6}$	$\frac{5.3}{7}$	$\frac{5.7}{7}$	$\frac{6.5}{10}$	$\frac{6.3}{13}$	$\frac{6.4}{33}$	$\frac{6.7}{50}$
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$\frac{7.5}{50}$	$\frac{7.1}{33}$	$\frac{6.6}{29}$	$\frac{7.4}{24}$	$\frac{7.6}{21}$	$\frac{6.5}{16}$	$\frac{6.2}{7}$	$\frac{6.4}{7}$	$\frac{7.3}{10}$	$\frac{6.8}{14}$	$\frac{7.2}{33}$	$\frac{7.3}{50}$
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$\frac{5.7}{50}$	$\frac{5.7}{33}$	$\frac{5.7}{28}$	$\frac{6.8}{23}$	$\frac{7.0}{20}$	$\frac{6.1}{17}$	$\frac{5.9}{7}$	$\frac{6.3}{7}$	$\frac{8.6}{13}$	$\frac{6.9}{22}$	$\frac{5.9}{33}$	$\frac{6.4}{50}$
------------------	------------------	------------------	------------------	------------------	------------------	-----------------	-----------------	------------------	------------------	------------------	------------------

$\frac{5.1}{50}$	$\frac{5.4}{33}$	$\frac{6.6}{24}$	$\frac{6.5}{21}$	$\frac{5.7}{17}$	$\frac{5.4}{6}$	$\frac{5.6}{6}$	$\frac{7.7}{12}$	$\frac{7.7}{14}$	$\frac{6.0}{25}$	$\frac{6.2}{33}$	$\frac{6.2}{50}$
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$\frac{11.2}{50}$	$\frac{8.7}{33}$	$\frac{7.0}{27}$	$\frac{5.5}{17}$	$\frac{5.9}{6}$	$\frac{5.5}{6}$	$\frac{6.8}{11}$	$\frac{7.2}{19}$	$\frac{7.0}{33}$	$\frac{7.2}{50}$
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$\frac{10.8}{50}$	$\frac{8.5}{33}$	$\frac{8.3}{25}$	$\frac{5.9}{16}$	$\frac{5.1}{5}$	$\frac{5.2}{6}$	$\frac{5.2}{6}$	$\frac{8.8}{15}$	$\frac{11.4}{35}$	$\frac{12.1}{50}$
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$\frac{10.4}{50}$	$\frac{9.1}{33}$	$\frac{8.7}{24}$	$\frac{5.1}{16}$	$\frac{5.0}{5}$	$\frac{5.0}{5}$	$\frac{4.9}{5.0}$	$\frac{9.1}{14}$	$\frac{11.2}{33}$	$\frac{12.1}{50}$
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$\frac{5.6}{50}$	$\frac{5.5}{33}$	$\frac{5.6}{13}$	$\frac{4.8}{6}$	$\frac{4.9}{6}$	$\frac{8.1}{14}$	$\frac{9.5}{30}$	$\frac{11.5}{50}$
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Sta	+	Δ	-	Elev.
		902.49		
32	+52			897.9
	+55.4	Top Rail		
	+60.5	Top Rail		
	+62			98.0
	+69			97.9
	+78			97.8
	+94			97.5
33	+05			97.4
T.P.	6.13	902.04 ✓	6.58	895.91 ✓
	+16			97.5
	+30			97.6
	+45			97.4

Lt

R

Rt

$$\frac{5.2}{50} \quad \frac{5.3}{33} \quad \frac{4.7}{13} \quad \frac{4.6}{4} \quad \frac{4.6}{11} \quad \frac{5.2}{33} \quad \frac{5.1}{33} \quad \frac{5.3}{50}$$

$$\underline{450} \quad 897.99$$

$$\underline{445} \quad 898.04$$

$$\frac{8.5}{50} \quad \frac{7.0}{33} \quad \frac{4.5}{14} \quad \frac{4.5}{8} \quad \frac{4.5}{5} \quad \frac{4.9}{7} \quad \frac{5.0}{33} \quad \frac{5.0}{50}$$

$$\frac{12.2}{50} \quad \frac{9.6}{33} \quad \frac{8.1}{23} \quad \frac{9.5}{14} \quad \frac{4.6}{6} \quad \frac{4.6}{33} \quad \frac{5.0}{33} \quad \frac{4.9}{50}$$

$$\frac{14.0}{50} \quad \frac{13.2}{36} \quad \frac{12.4}{31} \quad \frac{4.8}{14} \quad \frac{4.7}{14} \quad \frac{4.9}{5} \quad \frac{8.8}{13} \quad \frac{8.5}{23} \quad \frac{8.4}{33} \quad \frac{6.0}{50}$$

$$\frac{14.0}{50} \quad \frac{13.2}{33} \quad \frac{11.3}{25} \quad \frac{4.9}{13} \quad \frac{5.0}{6} \quad \frac{5.3}{6} \quad \frac{11.6}{18} \quad \frac{12.5}{33} \quad \frac{13.3}{50}$$

$$\frac{7.5}{50} \quad \frac{11.7}{35} \quad \frac{11.7}{30} \quad \frac{5.0}{14} \quad \frac{5.0}{7} \quad \frac{5.1}{6} \quad \frac{5.3}{6} \quad \frac{10.2}{14} \quad \frac{13.7}{33} \quad \frac{14.1}{50}$$

$$\frac{5.4}{50} \quad \frac{5.1}{43} \quad \frac{1.9}{33} \quad \frac{9.3}{24} \quad \frac{4.7}{14} \quad \frac{4.5}{6} \quad \frac{4.6}{11} \quad \frac{5.7}{33} \quad \frac{6.4}{33} \quad \frac{7.6}{50}$$

$$\frac{5.4}{50} \quad \frac{5.1}{33} \quad \frac{5.2}{19} \quad \frac{4.5}{14} \quad \frac{4.4}{5} \quad \frac{4.5}{5} \quad \frac{5.5}{11} \quad \frac{6.0}{33} \quad \frac{6.4}{30}$$

$$\frac{5.8}{50} \quad \frac{5.4}{33} \quad \frac{5.3}{26} \quad \frac{4.6}{14} \quad \frac{4.6}{5} \quad \frac{4.7}{10} \quad \frac{5.6}{33} \quad \frac{6.1}{33} \quad \frac{6.2}{50}$$

Sta	+	π	-	Elev.
		902.04		
33	+51	Top Rail		
	+57	Top Rail		
	+61			897.4
	+79			97.0
	+91			96.9
34				96.8
T.P.	6.09	✓ 902.00	6.13	895.91
	+48			96.6
	+57			96.6
35				96.5
	+40			96.9
B.M.	2.90	✓ 892.00	2.90	899.10
36				96.7

Lt.

L

Rt.

442 897.62

454 897.50

$\frac{95}{50} \frac{93}{30} \frac{56}{21} \frac{45}{16} \frac{46}{50} \frac{50}{30} \frac{53}{25} \frac{54}{33} \frac{58}{50}$

$\frac{101}{50} \frac{100}{33} \frac{94}{26} \frac{60}{15} \frac{50}{5} \frac{50}{9} \frac{57}{19} \frac{55}{33} \frac{52}{30} \frac{53}{50}$

$\frac{100}{50} \frac{99}{33} \frac{91}{25} \frac{51}{15} \frac{48}{5} \frac{51}{3} \frac{53}{11} \frac{94}{17} \frac{93}{28} \frac{57}{50} \frac{53}{50}$

$\frac{103}{50} \frac{100}{33} \frac{96}{26} \frac{53}{16} \frac{50}{7} \frac{52}{5} \frac{55}{3} \frac{100}{8} \frac{99}{25} \frac{63}{37} \frac{54}{50}$

$\frac{7.6}{50} \frac{8.0}{33} \frac{8.0}{23} \frac{5.5}{17} \frac{5.2}{9} \frac{5.4}{5} \frac{5.6}{2} \frac{9.4}{11} \frac{9.8}{23} \frac{9.5}{50}$

$\frac{6.3}{50} \frac{6.1}{35} \frac{7.8}{28} \frac{7.8}{23} \frac{5.5}{17} \frac{6.2}{7} \frac{6.4}{5} \frac{5.6}{2} \frac{9.3}{10} \frac{9.8}{33} \frac{9.1}{50}$

$\frac{4.2}{50} \frac{5.1}{33} \frac{6.0}{25} \frac{6.5}{23} \frac{5.4}{20} \frac{5.1}{9} \frac{5.5}{5} \frac{5.5}{1} \frac{8.0}{11} \frac{8.4}{27} \frac{7.7}{36} \frac{7.3}{50}$

$\frac{3.8}{50} \frac{4.3}{33} \frac{6.0}{24} \frac{4.8}{21} \frac{4.7}{10} \frac{5.1}{5} \frac{5.1}{1} \frac{6.8}{9} \frac{7.4}{19} \frac{6.2}{33} \frac{5.6}{50}$

Top N.E. Cor. Comp. Parts

$\frac{4.4}{50} \frac{4.6}{38} \frac{5.1}{33} \frac{6.0}{25} \frac{5.3}{20} \frac{5.0}{11} \frac{5.3}{5} \frac{5.4}{1} \frac{6.9}{8} \frac{7.2}{22} \frac{5.8}{33} \frac{4.6}{50}$

Sta	+	Δ	-	Elev
		902.00		
36+50				896.6
37				96.8
+ 50				96.8
38				96.6
+ 50				96.6
T.P	8.32	905.12 ✓	5.20	896.80 ✓
39				96.7
+50				96.8
40				97.2
+50				98.1
41				99.2
+50				900.7

Lt

E

Rt

$\frac{4.6}{5.0}$	$\frac{4.3}{38}$	$\frac{5.4}{27}$	$\frac{6.3}{25}$	$\frac{6.2}{22}$	$\frac{5.3}{19}$	$\frac{5.1}{8}$	$\frac{5.4}{2}$	$\frac{5.5}{8}$	$\frac{6.9}{14}$	$\frac{6.2}{33}$	$\frac{5.7}{33}$	$\frac{6.0}{5.0}$
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$\frac{6.1}{50}$	$\frac{6.1}{33}$	$\frac{6.2}{28}$	$\frac{6.7}{27}$	$\frac{6.3}{23}$	$\frac{5.3}{19}$	$\frac{4.9}{9}$	$\frac{5.2}{2}$	$\frac{5.3}{5}$	$\frac{6.3}{11}$	$\frac{6.5}{22}$	$\frac{6.1}{33}$	$\frac{4.7}{33}$	$\frac{2.8}{50}$
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$\frac{5.4}{50}$	$\frac{5.7}{30}$	$\frac{6.3}{27}$	$\frac{6.4}{22}$	$\frac{5.4}{18}$	$\frac{5.0}{9}$	$\frac{5.2}{2}$	$\frac{5.3}{7}$	$\frac{6.6}{19}$	$\frac{6.7}{33}$	$\frac{5.0}{33}$	$\frac{3.7}{50}$
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$\frac{5.7}{50}$	$\frac{5.5}{37}$	$\frac{6.3}{28}$	$\frac{6.8}{26}$	$\frac{6.7}{23}$	$\frac{5.4}{19}$	$\frac{5.1}{9}$	$\frac{5.4}{2}$	$\frac{5.5}{5}$	$\frac{6.8}{5}$	$\frac{6.9}{20}$	$\frac{5.7}{33}$	$\frac{4.8}{50}$
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$\frac{6.8}{50}$	$\frac{6.6}{33}$	$\frac{6.6}{26}$	$\frac{7.0}{24}$	$\frac{6.8}{22}$	$\frac{5.7}{19}$	$\frac{6.2}{9}$	$\frac{5.4}{2}$	$\frac{5.5}{6}$	$\frac{7.1}{22}$	$\frac{7.3}{24}$	$\frac{6.7}{33}$	$\frac{6.2}{50}$
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$\frac{7.9}{50}$	$\frac{9.7}{39}$	$\frac{10.6}{28}$	$\frac{10.1}{22}$	$\frac{8.7}{18}$	$\frac{8.3}{8}$	$\frac{8.4}{3}$	$\frac{8.5}{6}$	$\frac{10.1}{20}$	$\frac{10.6}{33}$	$\frac{8.9}{50}$
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$\frac{10.2}{50}$	$\frac{10.2}{33}$	$\frac{10.0}{23}$	$\frac{8.3}{18}$	$\frac{8.0}{8}$	$\frac{8.3}{2}$	$\frac{8.4}{8}$	$\frac{10.7}{17}$	$\frac{11.3}{33}$	$\frac{10.5}{50}$
-------------------	-------------------	-------------------	------------------	-----------------	-----------------	-----------------	-------------------	-------------------	-------------------

$\frac{7.8}{30}$	$\frac{7.8}{33}$	$\frac{7.8}{23}$	$\frac{7.8}{18}$	$\frac{7.6}{8}$	$\frac{7.9}{3}$	$\frac{8.1}{9}$	$\frac{11.5}{33}$	$\frac{12.8}{50}$
------------------	------------------	------------------	------------------	-----------------	-----------------	-----------------	-------------------	-------------------

$\frac{9.0}{50}$	$\frac{9.0}{33}$	$\frac{9.0}{22}$	$\frac{12}{18}$	$\frac{6.7}{8}$	$\frac{7.0}{2}$	$\frac{7.1}{11}$	$\frac{10.9}{33}$	$\frac{12.0}{50}$
------------------	------------------	------------------	-----------------	-----------------	-----------------	------------------	-------------------	-------------------

$\frac{6.1}{50}$	$\frac{6.6}{33}$	$\frac{7.1}{25}$	$\frac{5.8}{18}$	$\frac{5.6}{8}$	$\frac{5.9}{3}$	$\frac{6.0}{7}$	$\frac{7.2}{13}$	$\frac{7.7}{33}$	$\frac{8.3}{50}$
------------------	------------------	------------------	------------------	-----------------	-----------------	-----------------	------------------	------------------	------------------

$\frac{9.1}{30}$	$\frac{3.7}{33}$	$\frac{4.4}{28}$	$\frac{4.3}{21}$	$\frac{4.2}{8}$	$\frac{4.4}{3}$	$\frac{4.5}{8}$	$\frac{5.5}{12}$	$\frac{4.8}{25}$	$\frac{3.3}{50}$
------------------	------------------	------------------	------------------	-----------------	-----------------	-----------------	------------------	------------------	------------------

Sta	+	π	-	Elev
		905.12		
42				902.1 ✓
I.P.	733	909.75 ✓	2.70	902.42 .
+50				03.1 .
43				04.1 .
+50				04.9 .
44				04.7 .
+50				04.4 .
45				03.6 .
+50				02.6 .
46				01.3 .
I.P.	0.78	900.96 ✓	2.57	900.15 ✓
+50				899.6 .
47				98.3 .

Lt.

E

Rt.

$$\frac{0.7}{50} \quad \frac{0.7}{33} \quad \frac{1.1}{28} \quad \frac{3.1}{29} \quad \frac{3.1}{27} \quad \frac{2.8}{18} \quad \frac{2.7}{9} \quad \frac{3.0}{3} \quad \frac{3.1}{5} \quad \frac{3.7}{9} \quad \frac{3.8}{9} \quad \frac{2.1}{12} \quad \frac{0.3}{26} \quad \frac{1.2}{50}$$

$$\frac{4.0}{50} \quad \frac{4.1}{39} \quad \frac{4.2}{30} \quad \frac{6.8}{24} \quad \frac{6.9}{19} \quad \frac{6.6}{18} \quad \frac{6.4}{8} \quad \frac{6.7}{3} \quad \frac{6.8}{9} \quad \frac{7.1}{4} \quad \frac{7.2}{9} \quad \frac{5.6}{12} \quad \frac{3.8}{29} \quad \frac{3.7}{50}$$

$$\frac{8.5}{50} \quad \frac{3.4}{32} \quad \frac{6.0}{22} \quad \frac{6.1}{20} \quad \frac{5.8}{19} \quad \frac{5.4}{8} \quad \frac{5.7}{3} \quad \frac{5.8}{5} \quad \frac{6.1}{9} \quad \frac{6.2}{9} \quad \frac{4.8}{13} \quad \frac{3.7}{26} \quad \frac{3.4}{33} \quad \frac{2.2}{50}$$

$$\frac{2.8}{50} \quad \frac{2.9}{33} \quad \frac{5.8}{27} \quad \frac{6.0}{21} \quad \frac{5.5}{19} \quad \frac{4.9}{8} \quad \frac{4.9}{7} \quad \frac{4.9}{9} \quad \frac{5.1}{9} \quad \frac{4.3}{12} \quad \frac{3.6}{20} \quad \frac{3.3}{33} \quad \frac{2.5}{50}$$

$$\frac{1.8}{50} \quad \frac{1.8}{33} \quad \frac{6.0}{25} \quad \frac{6.0}{20} \quad \frac{5.3}{18} \quad \frac{4.9}{9} \quad \frac{5.1}{7} \quad \frac{5.4}{7} \quad \frac{3.0}{20} \quad \frac{2.7}{33} \quad \frac{2.5}{50}$$

$$\frac{2.2}{50} \quad \frac{1.6}{33} \quad \frac{6.0}{25} \quad \frac{6.2}{21} \quad \frac{5.5}{18} \quad \frac{5.1}{9} \quad \frac{5.4}{7} \quad \frac{5.6}{7} \quad \frac{2.9}{22} \quad \frac{2.9}{33} \quad \frac{3.5}{50}$$

$$\frac{4.0}{50} \quad \frac{3.0}{33} \quad \frac{7.1}{24} \quad \frac{7.1}{20} \quad \frac{6.6}{18} \quad \frac{6.1}{7} \quad \frac{6.2}{8} \quad \frac{6.4}{16} \quad \frac{5.7}{16} \quad \frac{3.5}{36} \quad \frac{3.6}{50}$$

$$\frac{6.8}{50} \quad \frac{5.0}{35} \quad \frac{7.1}{27} \quad \frac{7.1}{28} \quad \frac{7.5}{18} \quad \frac{7.1}{9} \quad \frac{7.2}{6} \quad \frac{7.4}{6} \quad \frac{6.7}{17} \quad \frac{4.7}{33} \quad \frac{4.5}{50}$$

$$\frac{9.8}{50} \quad \frac{7.5}{33} \quad \frac{7.8}{22} \quad \frac{8.4}{16} \quad \frac{8.3}{6} \quad \frac{8.5}{8} \quad \frac{9.0}{12} \quad \frac{9.3}{14} \quad \frac{8.8}{40} \quad \frac{6.7}{50} \quad \frac{6.5}{50}$$

$$\frac{4.8}{50} \quad \frac{4.9}{33} \quad \frac{3.9}{20} \quad \frac{1.3}{16} \quad \frac{1.2}{7} \quad \frac{1.4}{4} \quad \frac{1.8}{4} \quad \frac{3.3}{8} \quad \frac{4.6}{14} \quad \frac{3.9}{24} \quad \frac{4.0}{33} \quad \frac{4.3}{50}$$

$$\frac{6.3}{50} \quad \frac{5.9}{33} \quad \frac{6.0}{27} \quad \frac{6.2}{22} \quad \frac{2.6}{13} \quad \frac{2.5}{5} \quad \frac{2.7}{5} \quad \frac{3.0}{5} \quad \frac{7.0}{13} \quad \frac{7.4}{33} \quad \frac{7.9}{50}$$

Sta	+	Δ	-	Elev
		900.9 ⁶ ₃		
47+50				897.4
48				96.5
+ 50				96.0
49				96.2
+ 50				97.0
T.P.	10.76	909.19 ✓	2.53	898.43 ✓
50				98.4
+ 33				99.4
+ 60				900.1
51				00.4
+ 50				00.5
52				00.5

Lt

R

Rt

$$\begin{array}{r} 6.8 \\ 50 \end{array} \quad \begin{array}{r} 6.3 \\ 26 \end{array} \quad \begin{array}{r} 7.0 \\ 22 \end{array} \quad \begin{array}{r} 6.4 \\ 19 \end{array} \quad \begin{array}{r} 3.8 \\ 12 \end{array} \quad \begin{array}{r} 3.6 \\ 5 \end{array} \quad \begin{array}{r} 3.7 \\ 5 \end{array} \quad \begin{array}{r} 7.8 \\ 12 \end{array} \quad \begin{array}{r} 7.7 \\ 27 \end{array} \quad \begin{array}{r} 8.1 \\ 33 \end{array} \quad \begin{array}{r} 9.0 \\ 50 \end{array}$$

$$\begin{array}{r} 8.2 \\ 50 \end{array} \quad \begin{array}{r} 7.7 \\ 33 \end{array} \quad \begin{array}{r} 7.5 \\ 25 \end{array} \quad \begin{array}{r} 8.4 \\ 23 \end{array} \quad \begin{array}{r} 8.4 \\ 19 \end{array} \quad \begin{array}{r} 4.8 \\ 12 \end{array} \quad \begin{array}{r} 4.5 \\ 6 \end{array} \quad \begin{array}{r} 4.8 \\ 6 \end{array} \quad \begin{array}{r} 8.7 \\ 11 \end{array} \quad \begin{array}{r} 8.9 \\ 33 \end{array} \quad \begin{array}{r} 9.0 \\ 50 \end{array}$$

$$\begin{array}{r} 10.5 \\ 50 \end{array} \quad \begin{array}{r} 10.1 \\ 33 \end{array} \quad \begin{array}{r} 9.2 \\ 23 \end{array} \quad \begin{array}{r} 8.4 \\ 18 \end{array} \quad \begin{array}{r} 5.1 \\ 12 \end{array} \quad \begin{array}{r} 5.0 \\ 5 \end{array} \quad \begin{array}{r} 5.2 \\ 6 \end{array} \quad \begin{array}{r} 9.2 \\ 13 \end{array} \quad \begin{array}{r} 9.1 \\ 18 \end{array} \quad \begin{array}{r} 8.9 \\ 19 \end{array} \quad \begin{array}{r} 9.5 \\ 33 \end{array} \quad \begin{array}{r} 10.4 \\ 50 \end{array}$$

$$\begin{array}{r} 11.0 \\ 50 \end{array} \quad \begin{array}{r} 11.2 \\ 33 \end{array} \quad \begin{array}{r} 10.6 \\ 21 \end{array} \quad \begin{array}{r} 5.0 \\ 12 \end{array} \quad \begin{array}{r} 4.8 \\ 8 \end{array} \quad \begin{array}{r} 5.1 \\ 8 \end{array} \quad \begin{array}{r} 10.6 \\ 16 \end{array} \quad \begin{array}{r} 11.8 \\ 25 \end{array} \quad \begin{array}{r} 12.7 \\ 50 \end{array}$$

$$\begin{array}{r} 8.7 \\ 50 \end{array} \quad \begin{array}{r} 8.7 \\ 30 \end{array} \quad \begin{array}{r} 7.9 \\ 20 \end{array} \quad \begin{array}{r} 4.3 \\ 13 \end{array} \quad \begin{array}{r} 4.0 \\ 5 \end{array} \quad \begin{array}{r} 4.5 \\ 10 \end{array} \quad \begin{array}{r} 8.0 \\ 16 \end{array} \quad \begin{array}{r} 8.3 \\ 25 \end{array} \quad \begin{array}{r} 8.2 \\ 35 \end{array} \quad \begin{array}{r} 8.8 \\ 50 \end{array}$$

$$\begin{array}{r} 9.4 \\ 50 \end{array} \quad \begin{array}{r} 8.5 \\ 31 \end{array} \quad \begin{array}{r} 12.0 \\ 24 \end{array} \quad \begin{array}{r} 11.8 \\ 19 \end{array} \quad \begin{array}{r} 10.7 \\ 16 \end{array} \quad \begin{array}{r} 10.8 \\ 5 \end{array} \quad \begin{array}{r} 11.3 \\ 8 \end{array} \quad \begin{array}{r} 12.0 \\ 11 \end{array} \quad \begin{array}{r} 12.5 \\ 20 \end{array} \quad \begin{array}{r} 6.9 \\ 29 \end{array} \quad \begin{array}{r} 9.2 \\ 38 \end{array} \quad \begin{array}{r} 10.2 \\ 50 \end{array}$$

$$\begin{array}{r} 5.3 \\ 50 \end{array} \quad \begin{array}{r} 4.3 \\ 33 \end{array} \quad \begin{array}{r} 10.9 \\ 24 \end{array} \quad \begin{array}{r} 10.9 \\ 17 \end{array} \quad \begin{array}{r} 10.0 \\ 14 \end{array} \quad \begin{array}{r} 9.8 \\ 5 \end{array} \quad \begin{array}{r} 10.5 \\ 11 \end{array} \quad \begin{array}{r} 11.2 \\ 13 \end{array} \quad \begin{array}{r} 11.5 \\ 22 \end{array} \quad \begin{array}{r} 6.4 \\ 33 \end{array} \quad \begin{array}{r} 7.9 \\ 50 \end{array}$$

$$\begin{array}{r} 4.0 \\ 50 \end{array} \quad \begin{array}{r} 2.6 \\ 33 \end{array} \quad \begin{array}{r} 10.3 \\ 24 \end{array} \quad \begin{array}{r} 10.3 \\ 17 \end{array} \quad \begin{array}{r} 9.6 \\ 13 \end{array} \quad \begin{array}{r} 9.1 \\ 5 \end{array} \quad \begin{array}{r} 9.7 \\ 11 \end{array} \quad \begin{array}{r} 10.8 \\ 14 \end{array} \quad \begin{array}{r} 10.4 \\ 21 \end{array} \quad \begin{array}{r} 5.2 \\ 31 \end{array} \quad \begin{array}{r} 7.1 \\ 50 \end{array}$$

$$\begin{array}{r} 5.5 \\ 50 \end{array} \quad \begin{array}{r} 4.0 \\ 33 \end{array} \quad \begin{array}{r} 10.2 \\ 25 \end{array} \quad \begin{array}{r} 9.9 \\ 17 \end{array} \quad \begin{array}{r} 9.3 \\ 14 \end{array} \quad \begin{array}{r} 8.8 \\ 5 \end{array} \quad \begin{array}{r} 9.3 \\ 11 \end{array} \quad \begin{array}{r} 10.7 \\ 15 \end{array} \quad \begin{array}{r} 10.4 \\ 19 \end{array} \quad \begin{array}{r} 3.7 \\ 29 \end{array} \quad \begin{array}{r} 4.0 \\ 33 \end{array} \quad \begin{array}{r} 5.2 \\ 50 \end{array}$$

$$\begin{array}{r} 9.7 \\ 50 \end{array} \quad \begin{array}{r} 7.8 \\ 33 \end{array} \quad \begin{array}{r} 7.5 \\ 27 \end{array} \quad \begin{array}{r} 10.3 \\ 21 \end{array} \quad \begin{array}{r} 9.9 \\ 16 \end{array} \quad \begin{array}{r} 9.2 \\ 12 \end{array} \quad \begin{array}{r} 8.7 \\ 5 \end{array} \quad \begin{array}{r} 9.1 \\ 12 \end{array} \quad \begin{array}{r} 9.7 \\ 13 \end{array} \quad \begin{array}{r} 9.6 \\ 19 \end{array} \quad \begin{array}{r} 4.7 \\ 27 \end{array} \quad \begin{array}{r} 4.2 \\ 33 \end{array} \quad \begin{array}{r} 4.6 \\ 50 \end{array}$$

$$\begin{array}{r} 13.5 \\ 50 \end{array} \quad \begin{array}{r} 13.2 \\ 39 \end{array} \quad \begin{array}{r} 12.2 \\ 28 \end{array} \quad \begin{array}{r} 11.7 \\ 16 \end{array} \quad \begin{array}{r} 9.1 \\ 9 \end{array} \quad \begin{array}{r} 8.9 \\ 5 \end{array} \quad \begin{array}{r} 9.0 \\ 13 \end{array} \quad \begin{array}{r} 9.8 \\ 15 \end{array} \quad \begin{array}{r} 10.0 \\ 23 \end{array} \quad \begin{array}{r} 5.4 \\ 34 \end{array} \quad \begin{array}{r} 5.4 \\ 50 \end{array}$$

Sta	+	↑	-	Elev
		909.19		
52 +35				900.6
+42				00.6
+75				00.7
+81				00.6
BM	8.89	902.12 ✓	8.90	900.29 ✓
53				00.7
+50				01.3
54				02.1
+50				03.1
55				03.9
+50				05.0
56				06.0
T.P	8.11	914.22 ✓	2.31	906.61 ✓

Lt

E

Rt

<u>13.7</u>	<u>13.8</u>	<u>13.3</u>	<u>12.1</u>	<u>9.1</u>	<u>8.6</u>	<u>8.9</u>	<u>9.0</u>	<u>6.7</u>	<u>6.3</u>
50	33	20	15	8		13	31	36	50

<u>13.7</u>	<u>13.7</u>	<u>13.4</u>	<u>9.5</u>	<u>9.0</u>	<u>8.6</u>		<u>8.7</u>	<u>8.9</u>	<u>8.1</u>
50	33	18	10	7			14	33	50

<u>12.3</u>	<u>12.6</u>	<u>10.7</u>	<u>10.1</u>	<u>10.2</u>	<u>9.0</u>	<u>8.5</u>	<u>8.7</u>	<u>11.3</u>	<u>11.3</u>	<u>10.8</u>	<u>10.5</u>
50	39	31	27	10	7		15	20	27	31	50

<u>9.7</u>	<u>9.8</u>	<u>10.1</u>	<u>10.5</u>	<u>10.2</u>	<u>9.1</u>	<u>8.6</u>	<u>8.8</u>	<u>11.6</u>	<u>11.5</u>	<u>11.0</u>	<u>10.7</u>
50	33	23	18	10	7		15	20	27	31	50

Top Mont

<u>74</u>	<u>94</u>	<u>93</u>	<u>104</u>	<u>102</u>	<u>57</u>	<u>84</u>	<u>84</u>	<u>87</u>	<u>112</u>	<u>117</u>	<u>113</u>	<u>111</u>	<u>112</u>
50	33	27	17	10	6	4	15	20	24	27	33	50	

<u>76</u>	<u>80</u>	<u>85</u>	<u>100</u>	<u>99</u>	<u>80</u>	<u>78</u>	<u>78</u>	<u>84</u>	<u>118</u>	<u>125</u>	<u>134</u>
50	33	25	17	11	6	6	17	23	33	50	

<u>49</u>	<u>55</u>	<u>58</u>	<u>78</u>	<u>79</u>	<u>72</u>	<u>70</u>	<u>70</u>	<u>74</u>	<u>98</u>	<u>104</u>	<u>118</u>	<u>128</u>
50	33	21	16	10	6	7	17	23	31	36	50	

<u>34</u>	<u>39</u>	<u>47</u>	<u>70</u>	<u>71</u>	<u>62</u>	<u>60</u>	<u>60</u>	<u>65</u>	<u>70</u>	<u>79</u>	<u>95</u>	<u>104</u>
50	33	16	18	8	6	6	19	20	33	36	50	

<u>18</u>	<u>30</u>	<u>33</u>	<u>65</u>	<u>65</u>	<u>55</u>	<u>52</u>	<u>51</u>	<u>55</u>	<u>67</u>	<u>69</u>	<u>87</u>	<u>96</u>
50	33	22	16	8	6	7	19	22	33	36	50	

<u>14</u>	<u>23</u>	<u>22</u>	<u>56</u>	<u>55</u>	<u>44</u>	<u>41</u>	<u>40</u>	<u>45</u>	<u>58</u>	<u>53</u>	<u>58</u>	<u>69</u>	<u>77</u>
50	33	22	15	9	6	7	18	24	26	33	36	50	

<u>102</u>	<u>01</u>	<u>08</u>	<u>35</u>	<u>38</u>	<u>34</u>	<u>31</u>	<u>29</u>	<u>32</u>	<u>44</u>	<u>57</u>	<u>60</u>
50	33	17	12	8	6	6	17	23	41	50	

Sta + π - Elev.

914.72

56 +50

907.2

57

08.4

+50

09.4

58

10.2

+60

10.0

+72

09.4

+79

09.1

+92

09.0

59

09.0

+110.7

09.4

B.M.

4.95

910.27 ✓

Lt.

E

Rt.

40	40	41	70	76	75	77	76	93	98
50	53	22	14	6	15	18	25	50	

71
1st Floor Elev

905.62

23	27	26	63	65	63	62	64	84	96	105
50	33	23	12	2	7	18	24	35	50	

10	07	07	60	56	53	51	53	63	70	89	87
50	33	22	19	6	7	15	19	28	31	36	

04	45	59	47	45	43	47	79	90	103
24	21	12	6	6	76	20	33	50	

See Page 20

18	49	52	48	47	47	54	81	110
29	22	9	6	6	21	39	50	

04	04	36	50	53	53	52	58	54	116	133
50	32	30	19	6	8	17	24	36	50	

05	06	48	56	61	56	59	60	65	109	102	94
50	35	25	15	6	6	15	22	29	40	50	

62	66	71	62	57	59	74	86	= E.B. Top.
50	35	19	8	11	27	50		

60	64	62	57	57	72	= E.B. Top.
50	37	22	11	31		

E.C. Rd 8" = $\frac{3.3}{50}$ $\frac{4.3}{25}$ $\frac{5.3}{50}$

Top W. End C. M. Gully N. W. Cor. B. & L. G. C. St.

Sta	+	π	-	Elev.
B.M.	10.86	921.13		910.27

58				10.2
----	--	--	--	------

+60				10.0
-----	--	--	--	------

Bench Levels

B.M.	3.52	901.56 ✓		896.04 ✓
T.P.	6.19	902.38 ✓	5.32	896.24 ✓
T.P.	6.20	902.11 ✓	6.47	895.91 ✓
B.M.	3.00	902.11 ✓	3.00	899.11 ✓
T.P.	11.17	902.78 ✓	3.50	896.61 ✓
T.P.	2.56	905.44 ✓	1.90	902.88 ✓
B.M.	12.86	913.22 ✓	5.08	900.36 ✓
B.M.			2.90	910.32 ✓

Lt.

C

Rt.

Top G.M. GULV.

$$\frac{38}{75} \quad \frac{34}{50} \quad \frac{31}{27} \quad (10.9)$$

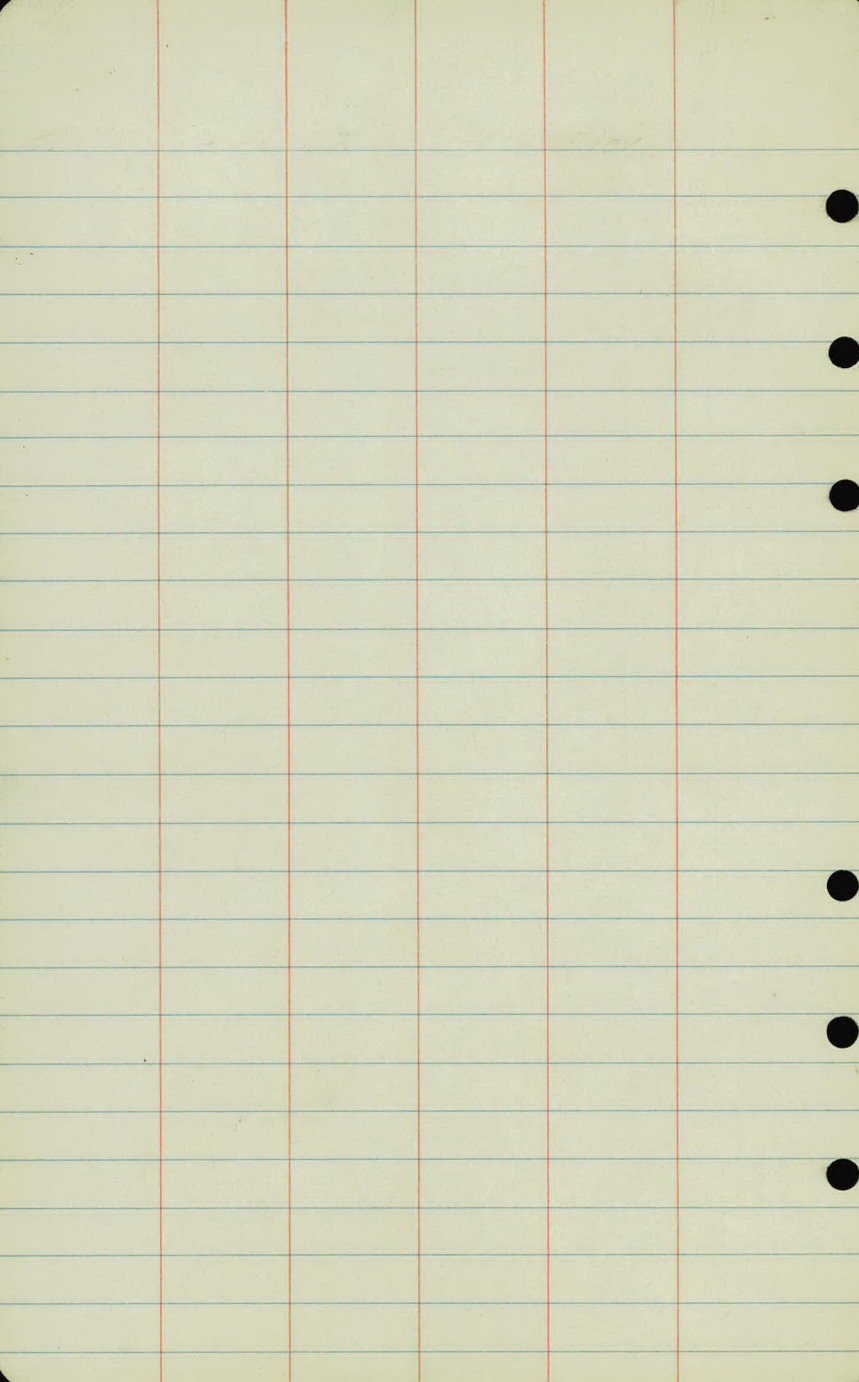
$$\frac{39}{75} \quad \frac{44}{50} \quad \frac{50}{35} \quad (11.1)$$

Top Brass Plug in Port Front Air + Lake St.

Top N.E. Car Conc. Porch

Top Mant.

Top W. End G.M. GULV. N.W. Cor. Lake 6 "B"



Topog

31

16'

5'

30

15

5'

29

14'

6'

28

12'

10'

27

15' 148" C.M.
12'

10'

+39.12 = 2.20 P.O.V.

26

178 P.P. - 28'

105 P.P. - 28'

129 P.P. - 29'

102 W. End 15" C.M. - 23'

Cult

Cult

125 12" Ash 36'
116 10" Ash 36'
106 15" Bender 36'
188 24" Magn 35'
185 N. End 15" C.M. - 19'

153 S. W. Cor 60x - 37'
153 S. End 15" C.M. - 19'
128 E. End 15" C.M. - 17'
120 N. End End
108 S. W. Cor 15x10 - 53'
198 60x Pump - 54'



38

18'

2'

37

19'

1

+44.5E Cor. Ho 89'

36

19'

00

35

19'

1

34

15'

1'

33

13'

4'

32

15'

5'

+14 P.P. 27'
Fc. 31'

Fc. 12'

Cult.

+26-6 Box Elder - 33'

+84-Group - 6-4" Trs. 27'
+71-Box Fc 31'

2-5-F

23'

Yard

+38-P.P. 27'

+33-18" Elm - 39'

+19-20" Elm - 40'

+90-20" Elm - 40'

+75-18" Elm - 40'

+62-End 15" K200.M. 35'

Meadow

+156-Fc. Cor 13'

+30-18" Maple 39'

+20-5 Box Elder 38'

+02-18" Box Elder 38'

+01-P.P. 27'

2-5-F

22'

Yard

+62-Lilac Bush - 43'

+40-Group - 6-5" Box Elders 22'

+22-8" 4" Box Elders - 22'

Cult.

+70-P.P. 27'

+88-G.R. - 26'

500 Line & M.P. Comm.

See Align. Notes for Δ & sta.

500 Line

+99-End Fc. 34'

+33-P.P. 27'

+02-Fc. Cor 34'

+13-Fc. Cor - 34'

+01-T.P. 32'

+72-Box Fc 33'

+54-End Fc 35'

+33-G.R. 29'

+12-Fc. Cor 34'

45

16'

3'

44

17'

3'

43

18'

2'

42

18'

1'

41

17'

2'

40

17'

1'

158-12" x 30' G.M.

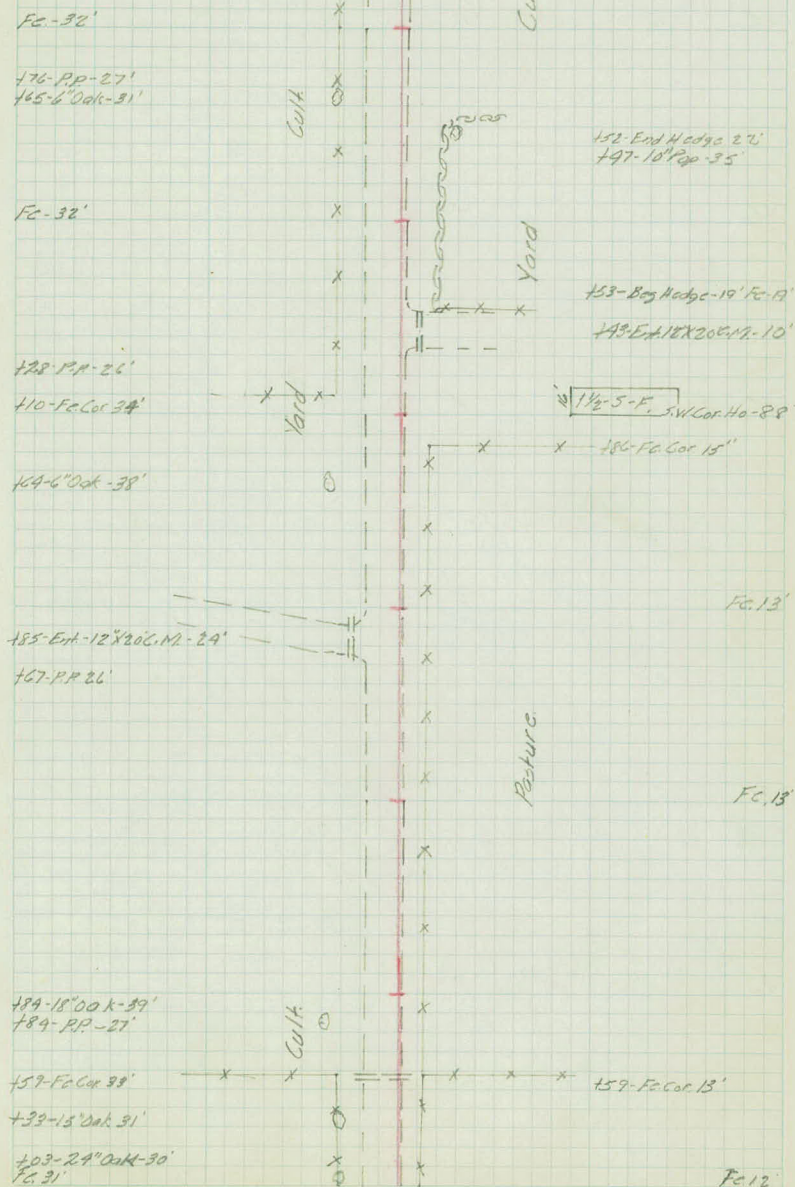
22' L1.

8' L1

39

18'

1'



56

9'

12

51

14'

10'

50

14'

9'

49

11

7'

48

18'

5'

47

13'

4'

46

46 - Great Lakes Pipe Line X's R

K

4'

+78-Fe Cor 15'
+66-P.P.-26

+59-Fe Cor-32'
+58-18" Oak-25'
+96-Ent.
+30-48" Oak-20'

+66-Stamp-20'
Fe-20'
+97-Stamp-25'
+80-6" Oak-31'
+67-12" Oak-31'
+61-6" Oak-31'
+50-8" Oak-33'

+12-6" Elder-40'

+12-6" Elder-39'
170-5.5" Cor. Ho-80'

+23-5" Oak-33'

+96-6" Maple-37

Fe-32'

+96-6" Oak-29'

+73-P.P.-26'

Fe-30'

+70-Ent.

+96-P.P.-26'
26' 26" 26"

Fe-22'

+85-10" Triple Oak-20'

+60-15" Oak-21'

+94-10" Oak-24'

Fe-25'

+82-P.P.-26'

+73-15" Triple Oak-26'

Fe-29

+20-P.P.-26'

Fe-35'

+62-Fe-37

59 ^{411.07}

15" x 40' C.M.

58

5'

17'

57

6'

16'

56

5'

15'

55

5'

15'

54

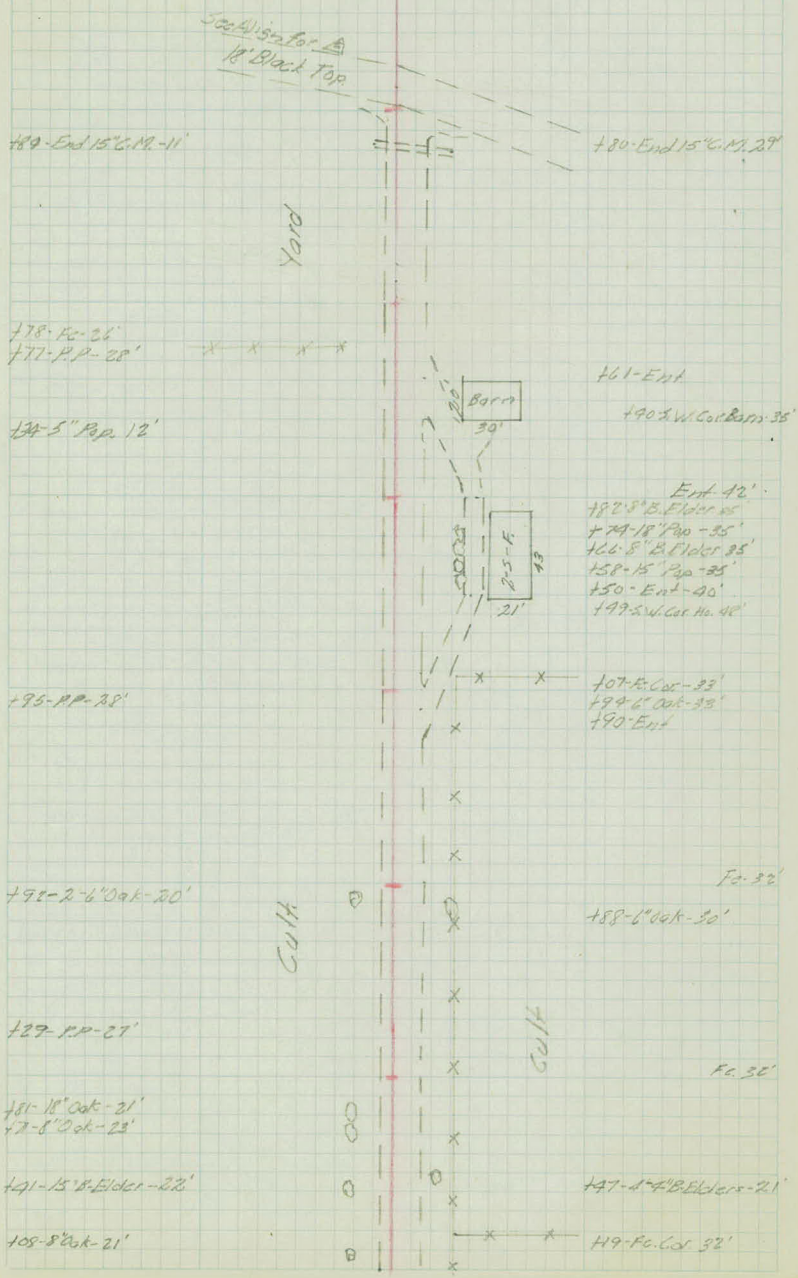
6'

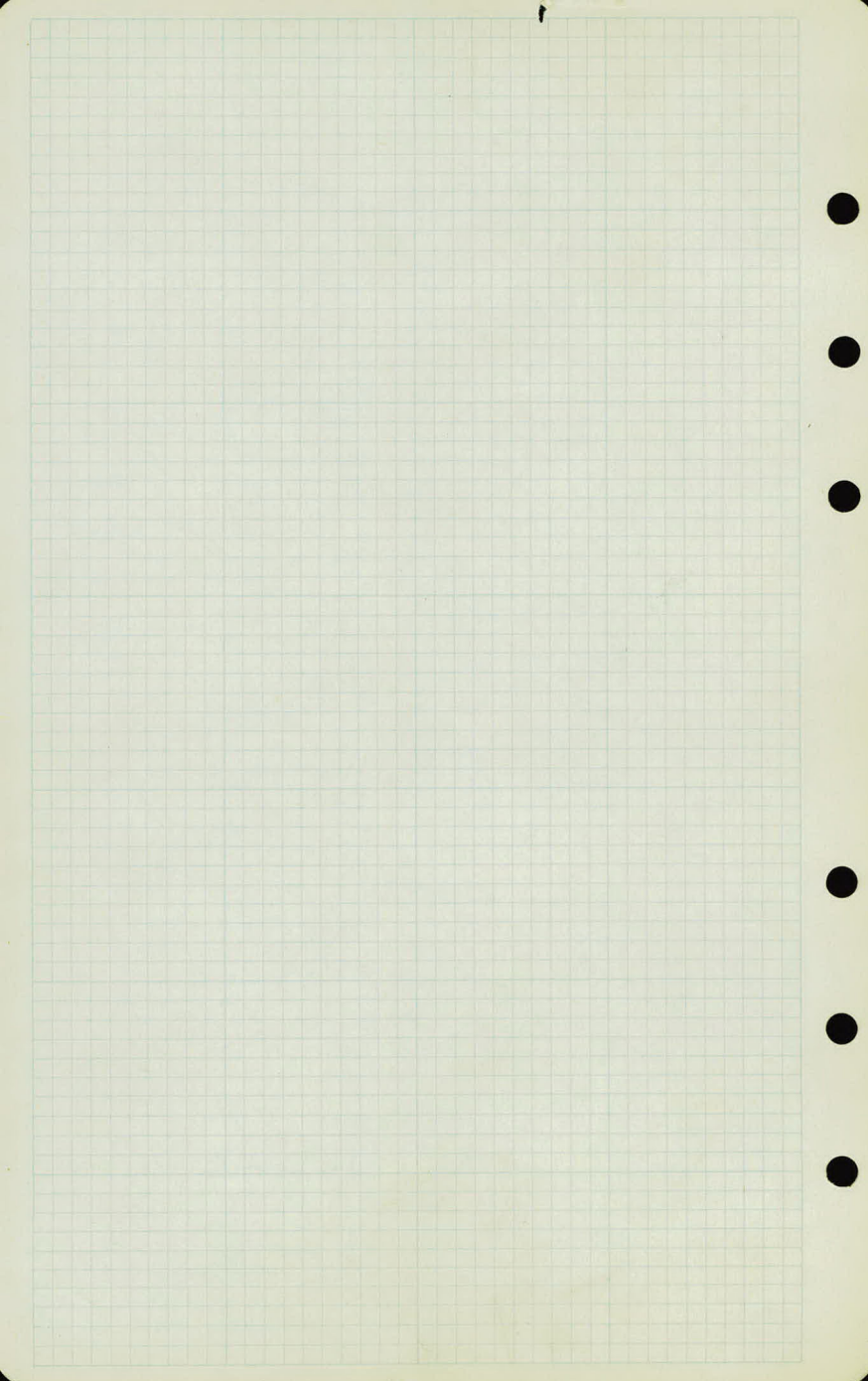
15'

53

6'

15'





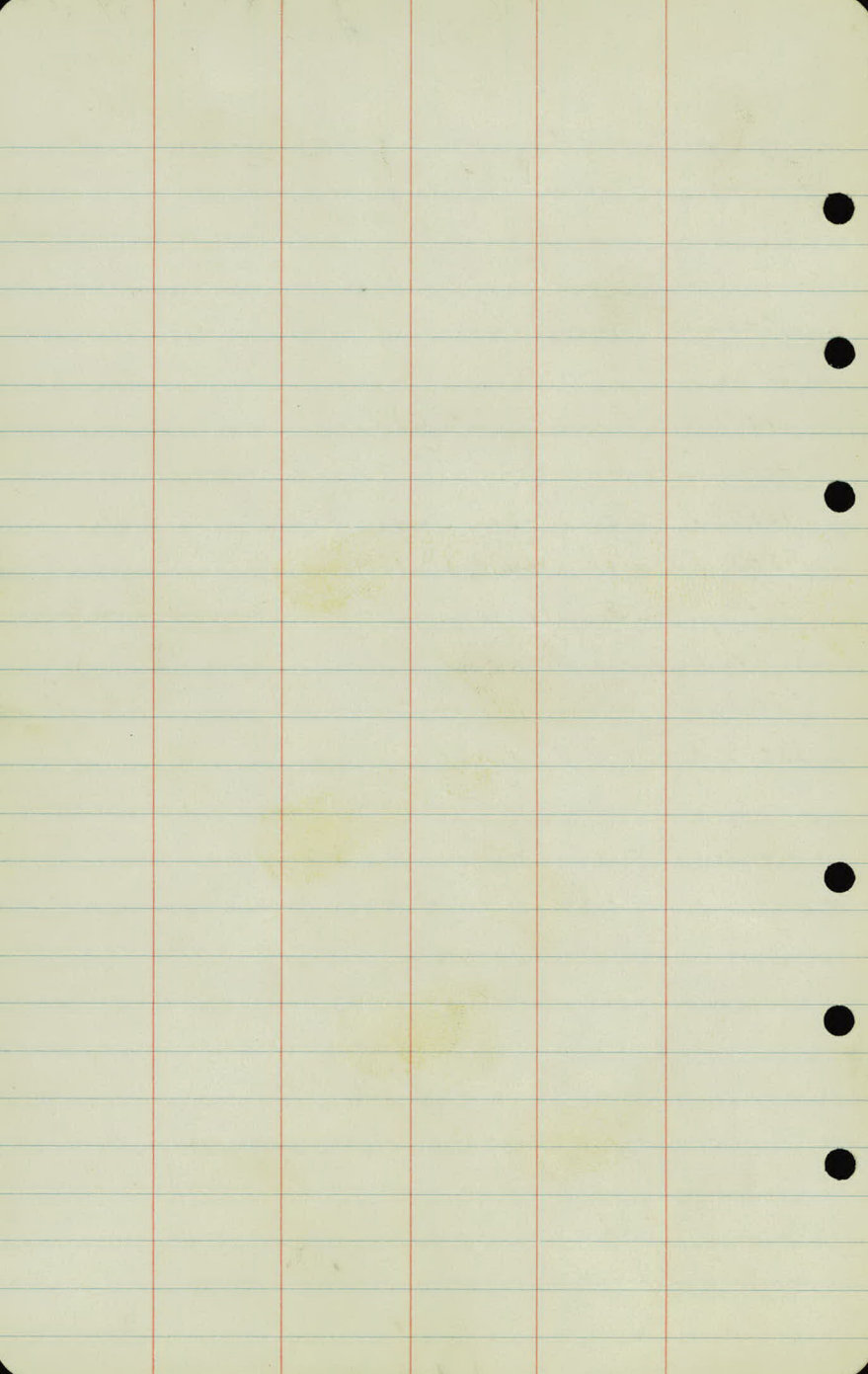
Lake St. Plans in Hand

4-25-38

M.W.C.

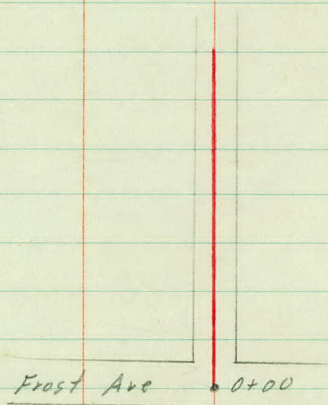
A.L.B.

27+15 £	O.K. Leave
27+69 R	Rem + Rep.
30+00 R	Pl. 15" X 20' C.M.
30+00 L	Pl. 15" X 20' C.M.
35+62 L	Rem. & Rep.
37+00 R	Pl. 15" X 20' C.M.
39+58 £	Rem & Pl. 24" Conc.
41+85 L	Rem. + Rep.
43+43 R	Rem. - No Culv. Reg. Haul to 49+70 Rt.
49+70 R	Rep. From 43+43 Rt.
52+46 R	No Culv. Reg.
55+90 R	" " "
57+61 R	" " "
58+83 £	Rem & Pl. 18" Conc.



1

~~Frost Ave.~~
ENGLISH ST.
X-Sections
at Frost Ave
~~at English~~



X-Sections 1-3

Topog. 4-6

6 pages

Sta	+	π	-	Elev
BM	5.33	901.32		895.99

9.24.46
notes

0+00

+28

+50

1

+50

+48

+58 $\pm$ Ent 15" x 20' CM

+68

2

+40

+50 $\pm$ Ent 15" x 20' CM

+60

3 Feb 1953

FK
AM
LC
MB

2

Lt

Q

Top Steel Plate intersection Frost Ave & English

q5.0	q5.29	q5.49	q5.65	q5.99
6.3	6.03	5.83	5.67	5.33
200	150	100	50	

q2.1	q3.6	q5.3	q5.5	q5.6	q5.5	q6.2
9.2	7.7	6.0	5.8	5.7	5.8	5.1
250	200	150	100	50	15	

q5.8	q5.6	q6.0
5.5	5.7	5.3
50	20	

q5.8	q5.7	q5.4	q6.0
5.5	5.6	5.9	5.3
50	27	20	

q5.4	q5.7	q4.5	q4.9	q6.3
5.9	5.6	6.8	6.4	5.0
50	27	24	20	

q4.67
6.65
FL
22

q5.9	q6.4	q6.1	q6.4
5.4	4.9	5.2	4.9
50	27	15	

6.67
FL
22

q7.8	q7.2	q5.0	q5.1	q6.5	q6.9
3.5	4.1	6.3	6.2	4.8	4.4
50	31	24	20	13	

q8.27

3.05
FL
22

q8.26

3.06
FL
22

q7.1	q6.7	q6.6	q6.9
4.2	4.6	4.7	4.4
50	23	13	

Sta + π - Elev

901.32

3

+50

4

+50

5

+50

+75

6

+16.35 Top S. Rail

3.0

BM

5.33

L+

P

96.8	96.2	95.4	95.2	96.6	96.9
4.5	5.1	5.9	6.1	4.7	4.4
50	29	24	20	14	

96.4	96.6	95.6	95.5	96.7	97.0
4.9	4.7	5.7	5.8	4.6	4.3
50	28	23	19	13	

95.7	95.6	94.9	95.4	96.8	97.0
5.6	5.7	6.4	5.9	4.5	4.3
50	28	23	19	13	

95.0	95.3	95.2	95.6	96.9	97.2
6.3	6.0	6.1	5.5	4.4	4.1
50	35	24	20	13	

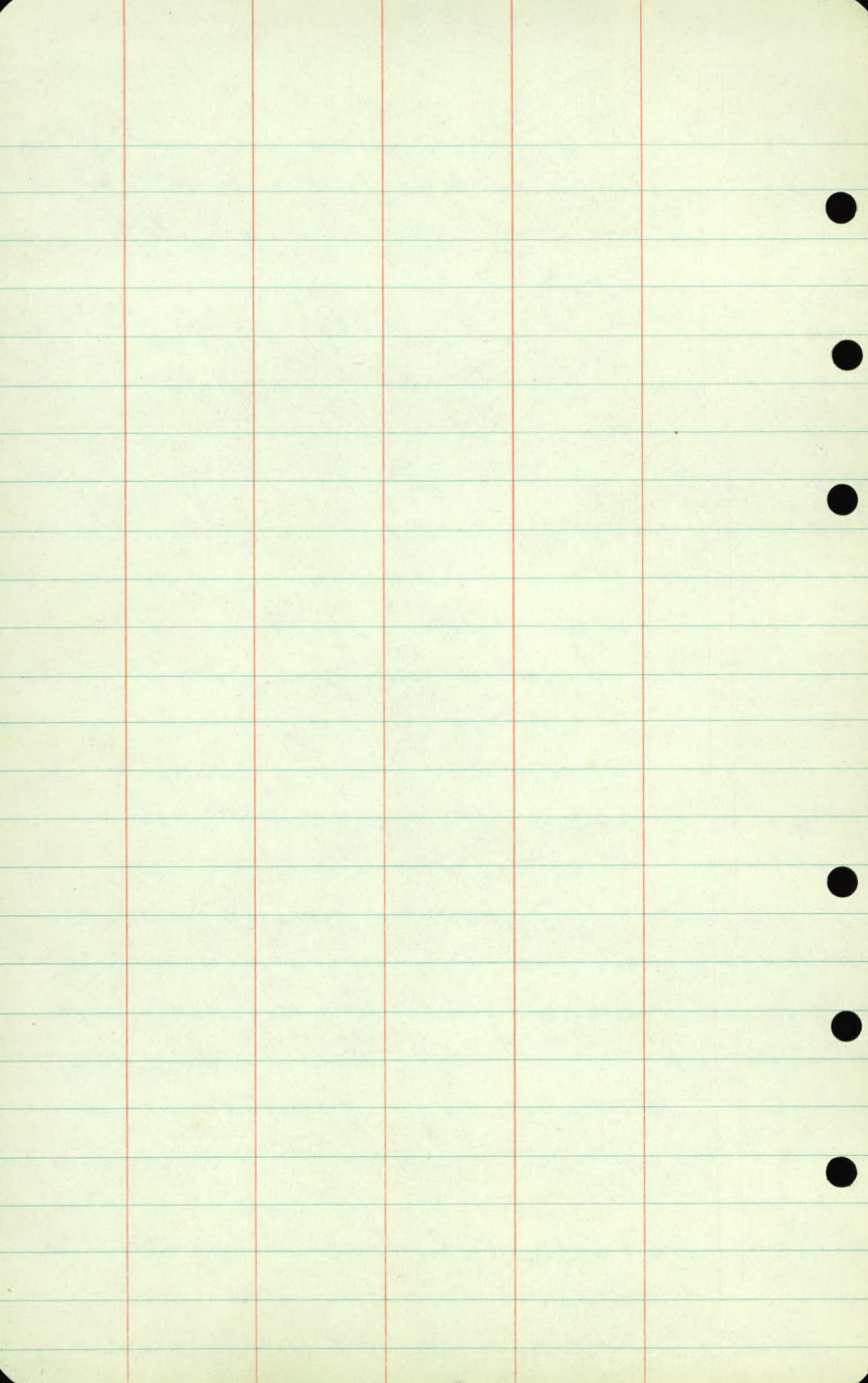
96.0	96.2	96.8	97.2	97.5
5.3	5.1	4.5	4.1	3.8
50	29	15	10	

97.6	97.1	96.1	97.4	97.6
3.7	4.2	5.2	3.9	3.7
50	28	20	13	

90.9	92.0	95.3	97.4	97.7
10.4	9.3	6.0	3.9	3.6
50	40	29	16	

93.9	95.1	96.1	97.7	97.9
7.4	6.2	5.2	3.6	3.4
50	35	23	14	

Top Steel Plate int, Frost Ave & English



Topography

+ 21 NE Cor 62' 32' Front to shop

+ 83 SE Cor. Ho. 41 23 X 30

152 Ent 15" X 20' CM 22'

+ 96 SE Cor. Ho. 57 30 X 30

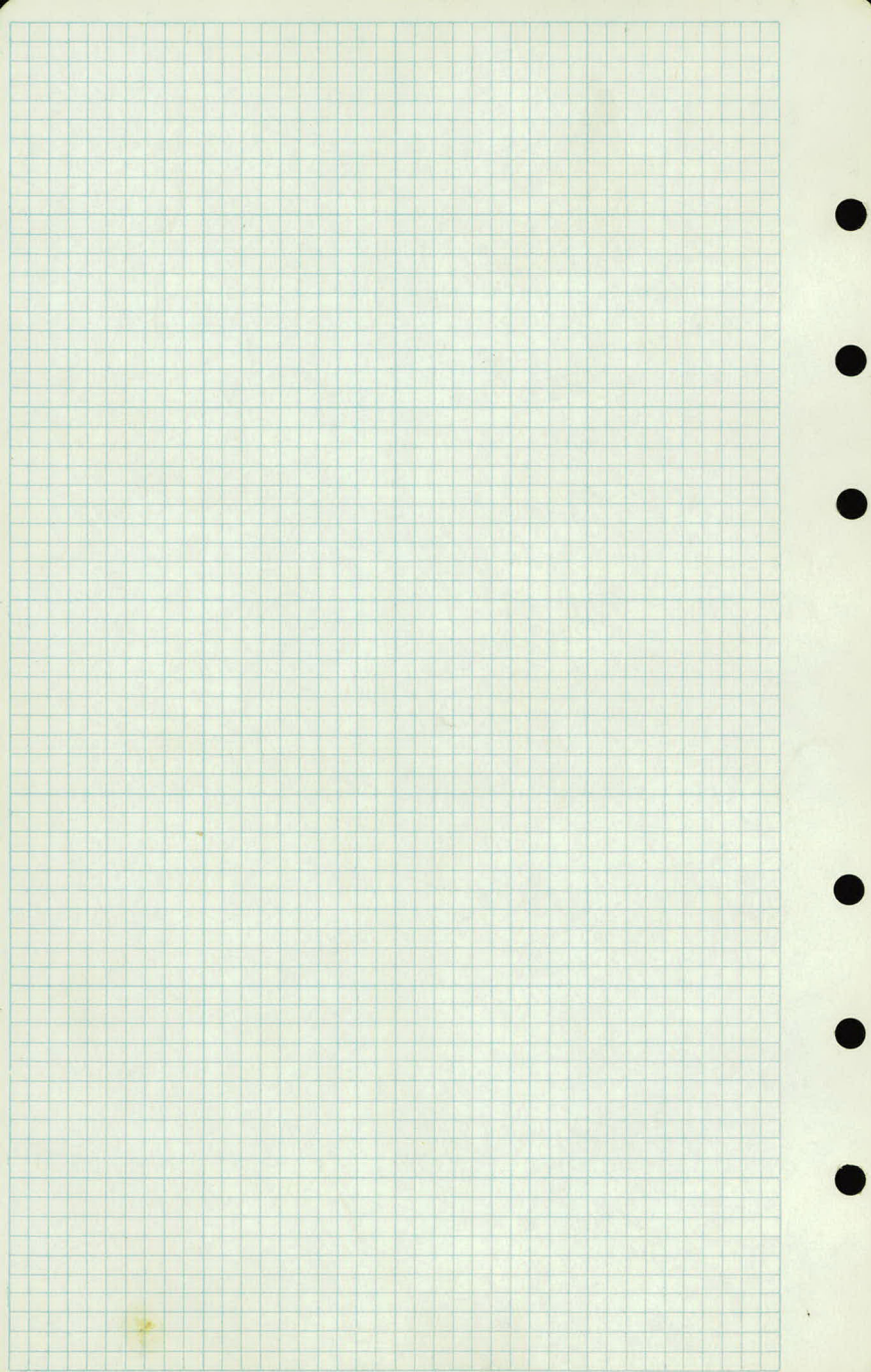
+ 60 Ent 15" X 20' CM 22'

+ 68 SE Cor. Restaurant 85'



6 +16.35 So Rail of Tracks

~~XXXXXXXXXXXXXXXXXXXX~~



9

10

90°42'

50.47 + Fa. Cor.
90°11'

27.46
R.P.
89°39'
16

31.84 @ 18" Top
90°26 1/2
15

St.

NA

15" O.
B 46.08

12" O.
B 59.83

2639.75 R.
2638.71 Meas
2639.56 K.A. Planning

English

90°07'

90°31'

Frost

2637.52

13/9.78

FX
RG
KP
JT

March 22 1957

Fair 39°

1

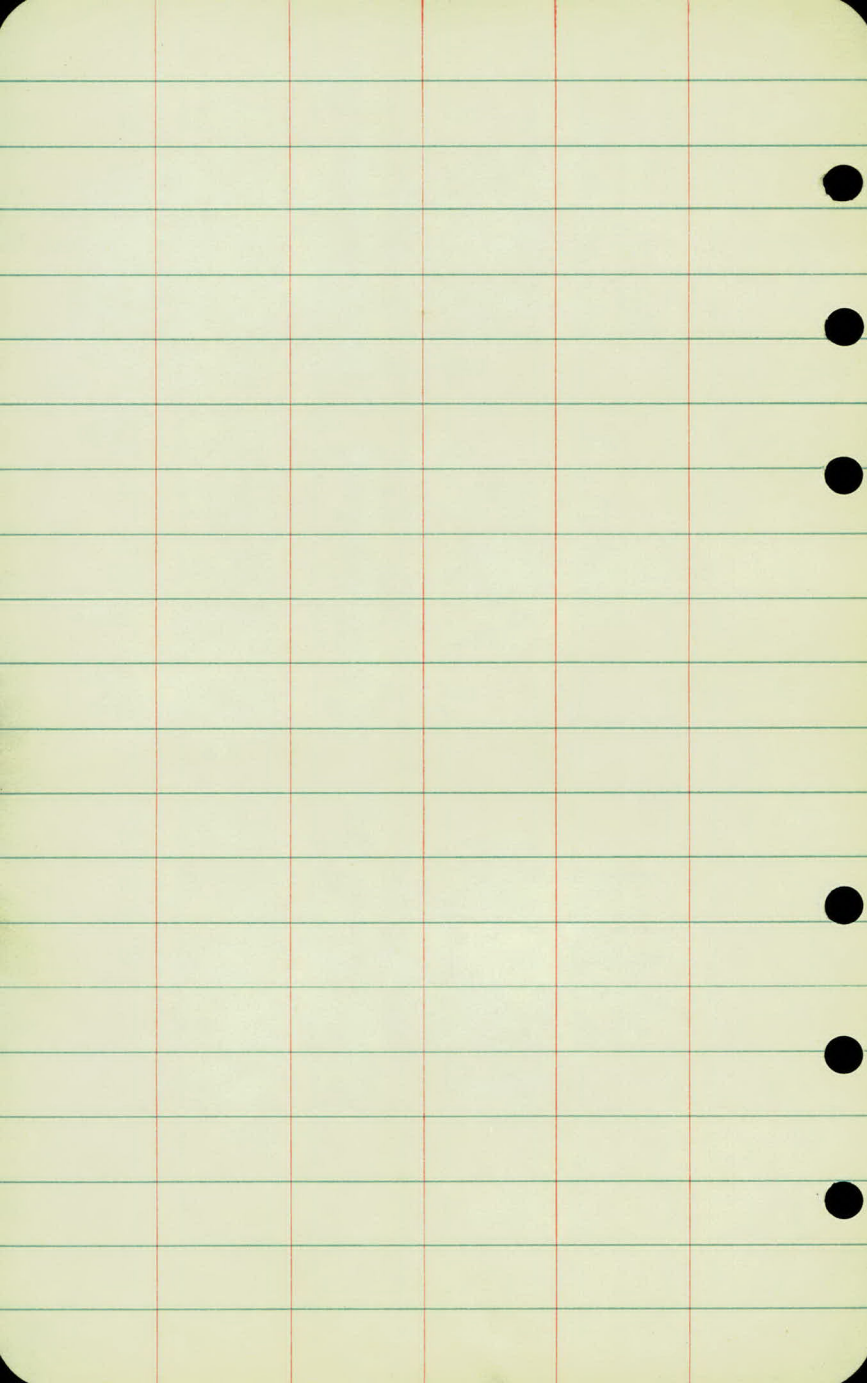
English

Coe Rd "B" to S.T.H. #36

Plan Survey

21 pages

Rec. 6/3/57



March 27, 1957

2

Alignment

Sta Point ΔL ΔR

A+00 P.O.T.

0+00 = P.I. of Co. Rd. "B"

2

85.51

4+00.5
NW Cor
Ho, Fo.

Cor Fo.

PP 0
89.82
89.96
66.75
A.54
1
1

spike
spike

PP 0

66.1'

Sta	Point	ΔIt	ΔRt
-----	-------	-------------	-------------

6+71.84			
---------	--	--	--

6+71.74			
---------	--	--	--

6+52.34	P.O.T.	$\frac{1}{4}$	$\frac{1}{4}$ Line
---------	--------	---------------	--------------------

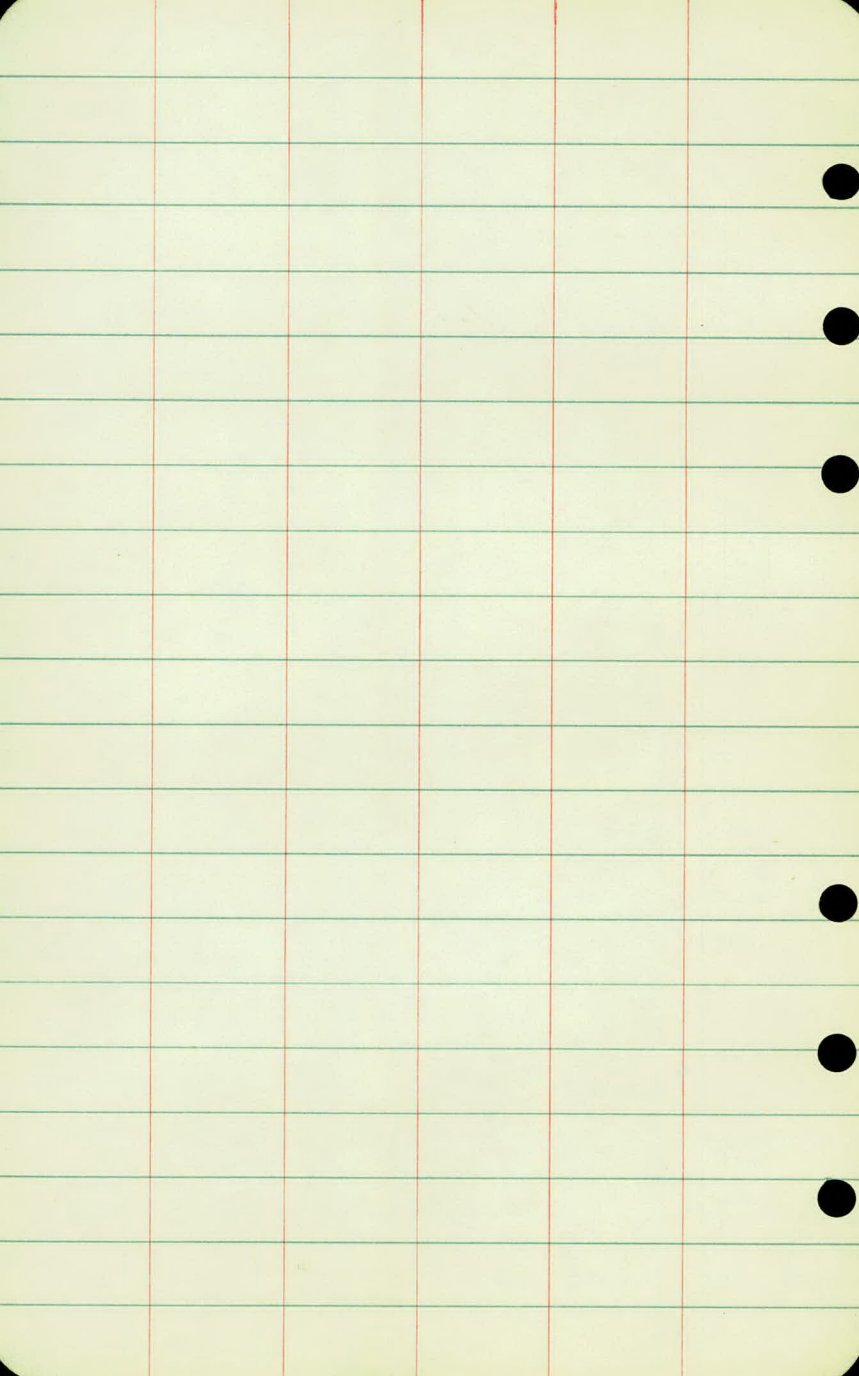
R/W Iran
(State)

70.48

74.52

R/W Spike
(State)

0.13' W. of Line Bolt



FR
RG
KP
JT

March 28, 1957
Fair 30°

5

TOPOGRAPHY

4

21

$$\begin{array}{r} \text{B.T.} \\ 5-12 \end{array}$$

Rt

$$154 \frac{PP}{31.5}$$

$$+16 \frac{6'' \text{Ce}}{24}$$

$$+127 \frac{4'' \text{Ce}}{32}$$

3

$$\frac{BT}{7-9.5}$$

$$+46 \frac{PP}{31}$$

$$+44 \frac{\text{End } 6' \text{ Brush Row}}{14}$$

$$124 \frac{\text{Box Brush } 6'}{22}$$

2

$$\frac{B.T.}{8.5-6}$$

$$+67 \frac{4'' \text{BE}}{20'}$$

$$+37 \frac{PP}{30.5}$$

$$+31 \frac{STP}{3T}$$

1

$$\frac{B.T.}{10 \ 4}$$

$$+13 \frac{STP}{24}$$

$$+61 \frac{STP}{22}$$

$$+88 \frac{STP}{22}$$

$$+88 \frac{N.E. \text{ Co Ho}}{63}$$

$$+85 \frac{18'' \times 34' \text{ CM}}{17-17}$$

$$+58 \frac{STP}{21}$$

$$+53 \frac{STP}{24}$$

$$+26 \frac{PP}{29}$$

$$+27 \frac{STP}{29}$$

0+00

$$+06 \frac{E.R.}{10}$$

$$+00 \frac{E.R. \text{ BT}}{10.8 \ 2'}$$

$$+03 \frac{E.R.}{8}$$

$$-15 \frac{B.R.}{34}$$

$$-02 \frac{WE 12' \times 30' \text{ CM}}{15'}$$

$$-12 \frac{E. \text{ End } 12' \times 30' \text{ CM}}{13.5}$$

$$-31 \frac{ER}{49}$$

$$-21 \frac{C.R. \text{ BT}}{4}$$

$$-31 \frac{BR}{40}$$

$$-51 \frac{15'' \times 52' \text{ CM}}{22.4}$$

$$-52 \frac{ER}{45}$$

$$-61 \frac{PP}{29}$$

$$-60 \frac{15'' \times 52' \text{ CM}}{29}$$

$$-72 \frac{B.R.}{12}$$

$$-82 \frac{BR}{9.5}$$

$$\frac{B.T.}{11 \cdot 10}$$

March 28, 1957

6

30' 302'

2-5-F

φ

XX

φ

5000

φ

φ

n

n

NR45
P 384

38
24

Foundation

= = =

H
r

φ

n

Co. Rd.

B

£

8

BT
11 11

7

BT
11 10

+99 PP
34

+60 Edge St
ST RT 12" X 28' CM
+52 31

+50 Ent
LT +34 12" X 36 CM
-27
+29 W.E. 12 X 36 CM
9' +31 P.O.R.
21.5

+90 STP
47 +71 4" E.E.
50
+A3 ER
47

6

BT
8.11

BR
11A 12

+83 PP
33

5

+100 20' Ent
LT

BT
6-14

+50 4" N.A.
47

+86 2-3" Plu.
38+51

+34 Ent
RT

+11 10' Fine
27

+11 4' Fine
33

+57 PP
32.5

+106 4' Fine
30

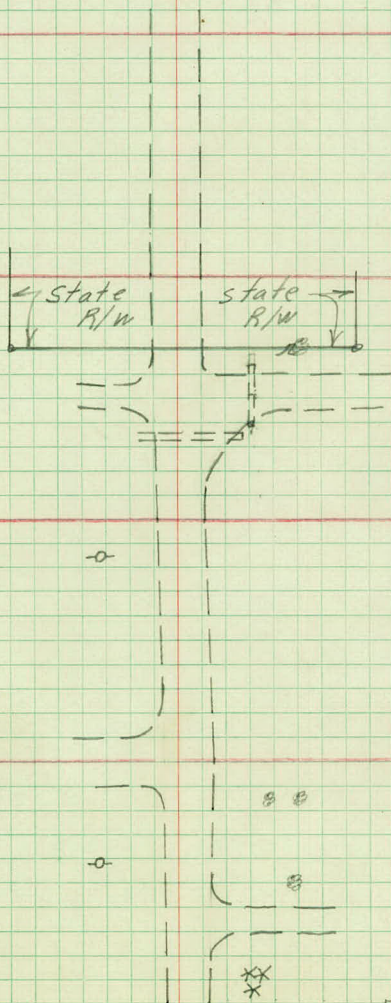
BT
5 12

NW Cor Ho
100.5 85.6

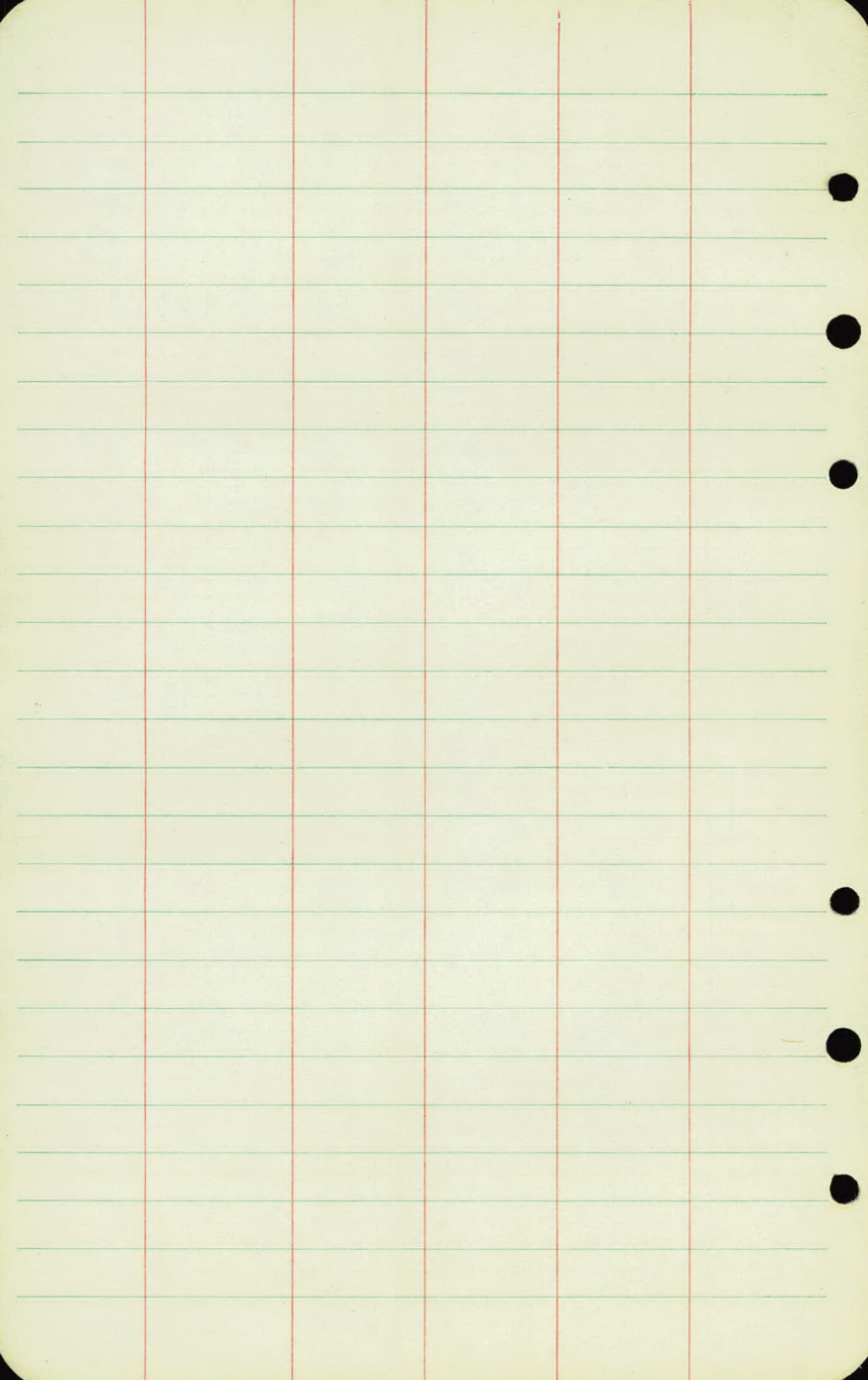
4

March 28/1957

2



N 30.2 S
E 30. W



FK
RG
KP
JT

LN
P
X
N

March 28, 1957

7

BENCH LEVELS

Sta	+	π	-	Elev.
BM	7.27	907.63		(900.36)
TP	7.25	914.57	0.31	907.32
BM			9.26	905.31
TP	12.07	923.77	2.87	911.70
BM			3.87	919.90
BM	13.72	923.77	13.72	910.05
TP	3.67	914.59	12.85	910.92
BM			9.29	905.30
TP	0.70	908.03	7.26	907.33
BM			7.67	900.36 (900.36)

March 28, 1951
Windy

8

Top Mont S.E. Cor Sec. 9-29-22

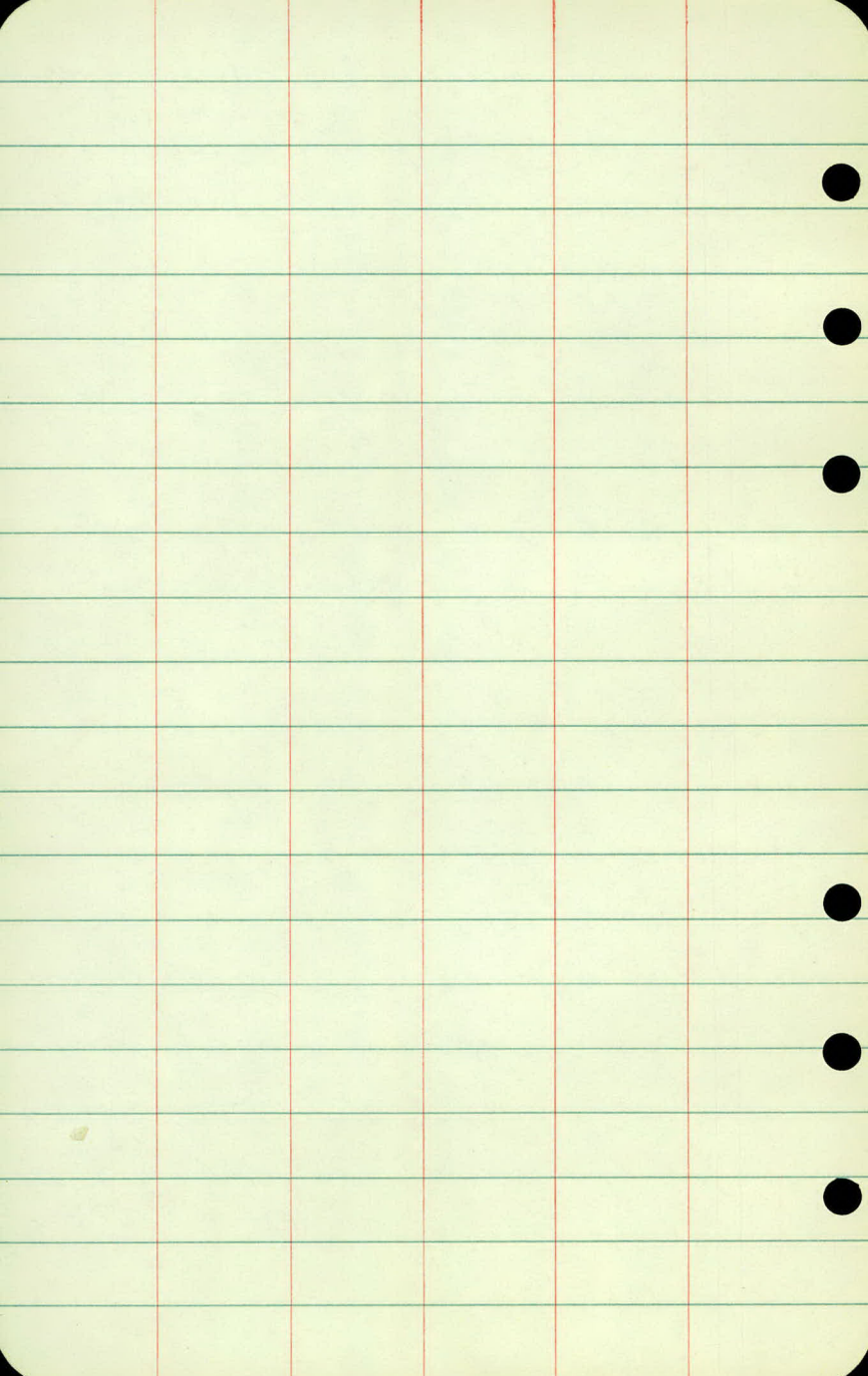
Top E. End 18"x34' CM 17' Rt Sta 0+85

NW Cor Conc Garage Apron Rt Sta 4+40

Top R/W Guard post 74' Rt Sta 6+72

Top E. End 18"x34' CM 17' Rt Sta 0+85

Top Mont S.E. Cor Sec 9-29-22



X-Sections

Sta + π - Elev.

BM 8.80 914.10

905.30

0+00

-23

-31 $\neq$ C.R.B

-42

-60

-100

2 March 28, 1959

14

RT 10

Top E. End 18" x 34 CM 17' RT Sta 0+85

09.9

4.2

09.6

4.5

09.3

4.8

09.1

5.0

09.3

4.8

10.0

4.1

Sta + π - Elev

914.10

- 150

- 200

- 250

VTP

6.77 907.33

907.33

BM

8.90 914.20

905.30

0-31

Profile Co Rd 'B'

0-10

FX
RG
KP
JT

Lt

March 28, 1957

March 29, 1957

RT 11

10.0

4.1

09.4

4.7

08.5

5.6

Top E. End 18" x 34' CM 12' RT Sta 0+85

14.2

11.5

09.3

06.3

03.9

P

0.0

2.7

4.4

7.9

10.3

99

50

50

100

11.7

10.3

10.4

10.1

09.9

09.6

08.7

08.3

04.8

2.5

3.9

3.8

4.1

4.3

4.6

5.5

5.9

9.4

50

41

22

9

6

14

20

27

P

00.3

01.8

13.9

12.4

50

35

Sta + π - Elev.

9/14.20

0+00

✓

+15

✓

+28

✓

March 29, 1957

11.6 Lt. 11.0 10.1 09.7 10.2 09.4 09.0 08.4 Rt. 12 04.8

26 32 4.1 4.5 4.0 4.8 5.2 5.8 9.4
50 33 17 15 8 14 21 27

P.

900.0 01.5
14.2 12.7
50 33

11.8 07.0 07.6 08.5 09.2 09.6 09.2 08.8 05.9 03.2

24 6.2 4.6 5.7 5.0 4.6 5.0 5.4 8.3 11.0
33 25 19 17 9 6 18 23 28

P.

899.9 00.1 00.9
14.2 14.1 13.3
50 37 32

911.9
2.3
50

07.6 07.0 08.4 08.6 09.1 09.0 09.0 05.4 01.8

6.6 7.2 5.8 5.6 5.1 5.2 5.2 8.8 12.4
30 17 15 10 9 11 17 23

P.

00.3 00.1 00.4
13.9 14.1 13.8
51 42 32

10.0 11.5 11.7

4.2 2.7 2.5
38 44 50

Sta + π - Elev

914.20

0 + 60

✓

+ 85 this x-Drain is directly in line with New
Garage in basement

1

✓

+ 50

March 29, 1957

07.7 06.7 07.3 08.1 08.3 08.4 08.3 04.8 01.3

6.5 7.5 6.9 6.1 5.9 5.8 5.9 9.4 12.9
23 16 14 10 7 10 16 22

09.2 11.2 11.1

00.2 00.3

5.0 3.0 3.1
35 47 50

14.0 13.9
50 32

10.5

05.49

03.72

3.7
about what
Garage Floor
will be

8.71
FL 18" x 34" CM
17'

10.48
FL 18" x 34" CM
17

07.5 06.7 08.0 08.0 08.0 08.1 08.0 05.3 01.7

6.7 7.5 6.2 6.2 6.2 6.1 6.2 8.9 12.5
23 16 12 8 4 10 15 21

08.5 09.4 11.3 11.9

00.4 00.5 00.6

5.7 4.8 2.9 2.3
25 32 39 50

13.8 13.7 13.6
50 42 31

09.8 08.4 08.0 08.3 08.4 08.4 08.2 07.9 06.1 02.5 01.6

4.4 5.8 6.2 5.9 5.8 5.8 6.0 6.3 8.1 11.7 12.6
26 21 17 13 8 5 10 15 21 27

10.4 11.3

01.4 01.2

3.8 2.9
38 50

12.8 13.0
50 39

Sta + π - Elev.

914.20

2

✓

TP 9.83 920.62 3.41 910.79

+ 28

✓

+ 70

2 March 29, 1957

09.9

09.1

09.2

09.4

09.7

09.5

09.5

09.2

06.6

4.3
21

5.1
17

5.0
14

4.8
8

4.5

4.7
6

4.7
10

5.0
12

7.6
18

11.1

11.9

13.3

04.1

03.6

03.6

04.3

3.1
27

2.3
38

0.9
50

10.1
50

10.4
43

10.6
30

9.9
23

12.4

10.0

10.3

10.4

10.9

10.5

10.3

09.6

07.1

8.2
26

10.6
17

10.3
13

10.2
8

9.7

10.1
8

10.3
11

11.0
13

13.5
17

12.9

14.0

05.9

05.2

05.5

7.7
38

6.6
50

14.7
50

15.4
38

15.1
26

16.2

16.3

14.0

12.4

12.1

13.1

12.6

13.2

12.5

11.7

11.6

4.4
24

4.3
23

4.6
18

8.2
13

8.1
8

7.5

8.0
11

7.4
14

8.1
25

8.9
35

9.0
44

15.4

15.2

15.6

15.3

16.5

11.4

5.2
26

5.4
28

5.0
35

5.3
39

4.1
50

9.2
50

sta + π - Elev.

920.62

3+00

✓

TP 10.51 929.35 1.78 918.84

+25

✓

+39

March 29, 1951

Lt

Rt 15

17.8

15.2

14.5

14.4

15.1

14.4

14.9

15.4

15.9

2.8 5.4 6.1 6.2 5.5 6.2 5.7 5.2 4.7
19 15 11 8 11 14 23 31

20.5

18.5

19.3

20.1

14.7

15.3

P.

→ 0.1 2.1 1.3 0.5 5.9 5.3
24 29 41 50 50 35

21.0

18.5

16.4

16.2

16.8

16.1

16.6

17.6

18.2

8.4 10.9 13.0 13.2 12.6 13.3 12.8 11.8 11.2
21 16 10 7 11 14 21 37

23.3

22.3

22.3

22.6

23.7

P.

19.4

→ 6.1 2.1 2.1 6.8 5.7 11.0
26 29 37 42 50 50

25.0

21.1

17.4

16.9

17.5

17.0

17.5

18.1

18.4

4.4 8.3 12.0 12.5 11.9 12.4 11.9 11.3 11.0
25 20 13 7 13 14 25 39

25.3

25.9

26.2

P.

18.7

→ 4.1 3.5 3.2 10.7
29 40 50 50

Sta	+	π	-	Elev.
-----	---	-------	---	-------

		929.35		
--	--	--------	--	--

3+45				
------	--	--	--	--

✓				
---	--	--	--	--

+71				
-----	--	--	--	--

✓				
---	--	--	--	--

4				
---	--	--	--	--

March 29, 1957

18.5	17.4	17.3	17.9	17.3	17.9	19.1	19.8
10.9	12.0	12.1	11.5	12.1	11.5	10.3	9.6
15	11	7		12	13	22	38

22.2	26.2	26.6	26.7			20.0
2.2	3.2	2.8	2.7			9.4
20	25	33	50			50

24.2	20.7	19.1	18.5	18.6	18.9	19.1	18.6	19.9	20.5
5.2	8.7	10.3	10.9	10.8	10.5	10.3	10.8	9.5	8.9
22	16	12	8	4		2	12	20	29

26.8	27.5	27.7	27.2	28.3		21.7	20.7
2.6	1.9	1.7	2.2	1.1		2.7	8.7
25	28	36	38	50		40	50

25.4	22.3	19.2	19.3	19.7	19.9	19.5	21.1	21.3	21.2
4.0	2.1	10.2	10.1	9.7	9.5	9.9	8.3	8.1	8.2
25	21	12	8		3	13	22	33	50

28.4	28.5	28.8	28.9
1.0	0.9	0.6	0.5
29	38	47	50

Sta + π - Elev

929.35

4+26

✓

+50

✓

+74

✓

BM 1.47 921.37 9.43 919.92 (919.90)

March 29, 1957

14

Rt

17

23.3

21.1

20.2

19.6

19.9

20.1

19.8

19.8

20.0

6.1

8.3

9.2

9.8

9.5

9.3

9.6

9.6

9.4

21

15

10

8

5

14

23

25

27.7

28.0

27.8

27.9

P.

20.1

20.2

1.7
28

1.4
31

1.6
40

1.5
50

9.3
50

9.2
39

25.0

23.2

21.8

19.6

19.4

19.6

19.6

19.4

19.6

19.7

4.0

6.2

7.6

9.8

10.0

9.8

9.8

10.0

9.8

9.7

26

22

17

10

5

6

15

21

35

25.7

25.8

26.1

26.6

P.

19.6

3.7
28

3.6
35

3.3
45

2.8
50

9.8
50

21.6

20.8

19.9

18.5

18.8

18.8

18.7

18.4

18.1

18.2

7.8

8.6

9.5

10.9

10.6

10.6

10.7

11.0

11.3

11.2

23

17

15

11

5

4

13

16

19

22.7

23.5

23.9

P.

17.7

18.1

6.7
26

5.9
39

5.5
50

11.7
50

11.3
37

NW Cor Conc Garage Apron Rt Sta 4+40

Sta + π - Elev.

921.37

A+88 Good for Ent Lt. Beyond 30'

✓

5 Good for Ent Lt to 30'

✓

+50

2 March 29/1957

RT 18

17.8	17.9	17.8	18.2	18.3	18.2	17.9	17.4	17.8
3.6	3.5	3.6	3.2	3.1	3.2	3.5	4.0	3.6
25	16	12	6		5	13	17	19

18.9	19.9	21.4			17.1	17.3	17.4
2.5	1.5	0.0			4.3	4.1	4.0
33	50	70			50	44	32

19.4	18.1	17.4	17.7	17.9	17.9	17.6	16.6	17.0
2.0	3.3	4.0	3.7	3.5	3.5	3.8	4.8	4.4
41	24	12	8		5	13	18	26

20.0						16.5	16.7	16.9
1.4						4.9	4.7	4.5
50						50	44	33

18.9	17.6	16.1	16.3	16.2	16.1	15.9	15.5	14.8
25	3.8	5.3	5.1	5.2	5.3	5.5	5.9	6.6
34	20	11	7		11	17	21	23

19.4	18.7					14.3	14.9	15.1
2.0	2.7					7.1	6.5	6.3
44	50					50	34	25

Sta + π - E/ev

921.37

6

✓

+29 W. End x-Drain Burnied

+30

✓

+34

Sta + π - Elev

921.37

6+38

+40

+50 $\neq$ Start Left

+62

+66

+67

March 29, 1957

LT

RT 20

10.9/10.85

10.52

FL SE 12"X48"CM

31

16.4

15.7

15.3

14.8

14.9

14.7

14.1

12.9

11.9

11.4

11.2

5.0 5.7 6.1 6.6 6.5 6.7 7.3 8.5 9.5 10.0 10.0
50 37 27 18 10 11 20 30 40 50

19.4

16.7

16.4

15.7

14.7

14.3

13.6

12.3

11.2

10.6

2.0 4.7 5.0 5.7 6.7 7.1 7.8 9.1 10.2 11.8
100 50 44 29 10 12 32 50 100

16.1

14.9

14.0

13.8

13.8

13.0

12.5

11.8

11.6

10.7

5.3 6.5 7.4 7.6 7.6 8.4 8.9 9.6 9.8 10.0
50 32 17 9 11 18 28 37 50

909.34

12.03

FL 12"CM

31

15.5

14.9

14.3

13.8

13.5

13.5

12.7

11.7

10.4

10.1

09.2

5.9 6.5 7.1 7.6 7.9 7.9 8.7 9.7 11.0 11.3 12.0
50 40 28 17 10 11 22 28 38 50

Sta	+	π	-	Elev
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		921.37		
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7

✓

BM	1.77	911.82	11.32	910.05	910.05
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+50

8

✓

+50

2.2

9

9.7

+50

12.2

BM

1.77

910.05

910.05

Lt

4

Rt

21

11.5

10.7

11.2

11.7

12.0

11.7

11.1

09.1

9.9

10.7

10.2

9.7

9.4

9.7

10.3

12.3

24

20

17

7

10

15

25

14.2

14.8

15.3

06.7

07.8

7.2

6.6

6.1

14.7

13.6

34

41

50

50

35

Top R/W Guard post 74' Rt Sta 6+72

04.3

2.1

05.2

05.2

06.3

06.9

07.2

06.8

06.0

04.9

05.3

6.6

6.6

5.5

4.9

4.6

5.0

5.8

6.9

6.5

20

18

13

10

10

15

20

24

06.3

09.0

11.5

13.3

14.3

04.8

05.4

06.0

5.5

2.8

0.3

+1.5

+2.5

70

6.4

5.8

24

30

36

41

50

50

45

34

04.6

99.6 02.1

Top R/W Guard Post 74' Rt Sta 6+72

Sta	+	x	-	Elev
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4

7

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Elev