

DR 12A - Bk 21

OFFICE OF COUNTY ENGINEER
RAMSEY CO. MINN.

PLAN Survey
DEMONT AVE.
CLARK AVE.....

From RICE ST. To CORTLAND

Road Acc't. No.

Date Filed.....

File.....

2637.8

PROJ. # 62-132-177

CLARK AV.

ORIGINAL CROSS SECTIONS
FROM RICE ST. TO H. POINT
1/2 MILE EMST.

Rice to Cortland

Bk 21
Dr 12A

204

205

STA.	+	H.I.	-	ELEV.
B.M.	1.53	956.81		955.28 ✓
0+00				955.28
+12		EDGE OF PAVE.		955.12
+17				955.2
+32				954.5
				952.2
1+00				951.2
+50				951.7
2+00				952.0
+50				951.7
3+00				950.8
T.P.	6.26	955.91	7.16	949.65
+50				950.0
4+00				949.6
+50				948.9

7.79

7.16

$$\begin{array}{r} -0.57 \quad -0.33 \\ \underline{2.10} \quad \underline{1.86} \\ 100 \quad 50 \end{array} \quad \begin{array}{r} +.27 \quad +.33 \\ \underline{1.26} \quad \underline{0.86} \\ 50 \quad 100 \end{array}$$

$$\begin{array}{r} -.21 \quad -.12 \\ \underline{1.90} \quad \underline{1.81} \\ 33 \quad 15 \end{array} \quad \begin{array}{r} +.09 \quad +1.18 \\ \underline{1.60} \quad \underline{0.51} \\ 15 \quad 33 \end{array}$$

$$\begin{array}{r} -.02 \quad -.01 \\ \underline{1.8} \quad \underline{1.7} \\ 33 \quad 15 \end{array} \quad \begin{array}{r} -.01 \quad .00 \\ \underline{1.7} \quad \underline{1.6} \\ 15 \quad 33 \end{array}$$

$$\begin{array}{r} -4.4 \quad -3.8 \quad -0.3 \\ \underline{6.7} \quad \underline{6.1} \quad \underline{2.6} \\ 33 \quad 15 \quad 8 \end{array} \quad \begin{array}{r} -0.3 \quad -4.3 \quad -4.4 \\ \underline{2.6} \quad \underline{6.6} \quad \underline{6.7} \\ 11 \quad 21 \quad 33 \end{array}$$

$$\begin{array}{r} -2.8 \quad -2.8 \quad -1.0 \quad -1.6 \\ \underline{7.4} \quad \underline{7.4} \quad \underline{5.6} \quad \underline{5.2} \\ 33 \quad 15 \quad 11 \quad 9 \end{array} \quad \begin{array}{r} -0.7 \quad -3.0 \quad -3.4 \\ \underline{5.5} \quad \underline{7.6} \quad \underline{8.0} \\ 8 \quad 12 \quad 33 \end{array}$$

$$\begin{array}{r} -2.3 \quad -2.2 \quad -1.0 \quad -0.3 \\ \underline{7.4} \quad \underline{7.3} \quad \underline{6.1} \quad \underline{5.4} \\ 33 \quad 15 \quad 12 \quad 7 \end{array} \quad \begin{array}{r} -0.8 \quad -1.9 \quad -1.7 \quad -1.0 \\ \underline{5.9} \quad \underline{7.0} \quad \underline{6.8} \quad \underline{6.1} \\ 11 \quad 19 \quad 20 \quad 33 \end{array}$$

$$\begin{array}{r} -0.6 \quad -0.6 \quad -1.1 \quad -1.9 \quad -0.2 \\ \underline{5.4} \quad \underline{5.4} \quad \underline{5.9} \quad \underline{5.7} \quad \underline{5.0} \\ 33 \quad 21 \quad 16 \quad 11 \quad 5 \end{array} \quad \begin{array}{r} -0.2 \quad -.9 \quad +1.7 \quad +1.5 \\ \underline{5.0} \quad \underline{5.7} \quad \underline{8.1} \quad \underline{5.3} \\ 5 \quad 15 \quad 19 \quad 33 \end{array}$$

$$\begin{array}{r} +0.4 \quad +3.8 \quad -0.5 \quad -0.9 \quad -0.2 \\ \underline{4.7} \quad \underline{1.3} \quad \underline{5.2} \quad \underline{6.0} \quad \underline{5.3} \\ 33 \quad 20 \quad 15 \quad 12 \quad 6 \end{array} \quad \begin{array}{r} -0.2 \quad -0.5 \quad -1.0 \quad -0.9 \quad +0.9 \quad -0.5 \\ \underline{5.3} \quad \underline{5.6} \quad \underline{6.1} \quad \underline{6.0} \quad \underline{4.2} \quad \underline{5.6} \\ 4 \quad 7 \quad 11 \quad 15 \quad 18 \quad 33 \end{array}$$

$$\begin{array}{r} +.43 \quad +.35 \quad +.04 \quad .00 \\ \underline{1.7} \quad \underline{2.5} \quad \underline{6.6} \quad \underline{6.0} \\ 33 \quad 21 \quad 14 \quad 5 \end{array} \quad \begin{array}{r} -.03 \quad -.10 \quad -.02 \quad -.03 \quad -.20 \\ \underline{6.3} \quad \underline{7.0} \quad \underline{6.2} \quad \underline{6.3} \quad \underline{8.0} \\ 7 \quad 15 \quad 18 \quad 22 \quad 33 \end{array}$$

$$\begin{array}{r} +.25 \quad +.12 \quad +.07 \quad +.07 \quad +.02 \\ \underline{5.4} \quad \underline{4.7} \quad \underline{6.6} \quad \underline{6.6} \quad \underline{6.1} \\ 33 \quad 20 \quad 16 \quad 13 \quad 6 \end{array} \quad \begin{array}{r} -.03 \quad -.11 \quad -.16 \quad -.19 \quad .30 \\ \underline{6.2} \quad \underline{7.0} \quad \underline{7.5} \quad \underline{7.8} \quad \underline{8.9} \\ 5 \quad 10 \quad 12 \quad 19 \quad 33 \end{array}$$

$$\begin{array}{r} +.28 \quad +.11 \quad +.06 \quad +.05 \quad +.01 \\ \underline{5.5} \quad \underline{5.2} \quad \underline{6.9} \quad \underline{6.8} \quad \underline{6.4} \\ 33 \quad 20 \quad 17 \quad 10 \quad 6 \end{array} \quad \begin{array}{r} -.03 \quad -.17 \quad -.17 \quad -.20 \quad -.23 \\ \underline{6.6} \quad \underline{8.0} \quad \underline{8.0} \quad \underline{8.5} \quad \underline{8.6} \\ 6 \quad 12 \quad 15 \quad 17 \quad 33 \end{array}$$

$$\begin{array}{r} +.10 \quad +.51 \quad +.04 \quad +.07 \quad .00 \\ \underline{1.0} \quad \underline{1.9} \quad \underline{7.4} \quad \underline{7.7} \quad \underline{7.0} \\ 33 \quad 23 \quad 14 \quad 13 \quad 6 \end{array} \quad \begin{array}{r} -.04 \quad -.10 \quad -.12 \quad +.11 \quad -.16 \\ \underline{7.4} \quad \underline{8.0} \quad \underline{8.2} \quad \underline{5.7} \quad \underline{8.6} \\ 5 \quad 8 \quad 13 \quad 16 \quad 33 \end{array}$$

STN.	+	H.I.	-	ELEV
		955.91		
5+00				947.4.
	1.33	945.58	11.66	944.25.
+50				943.7.
6+00				939.8.
+50				936.8.
B.M.	0.68	939.77	6.46	939.12 939.09
7+00				935.2.
+50				934.5.
8+00				933.4.
+50				932.6.
9+00				932.3.
+50				931.5.
10+00				930.3.
T.P.	4.17	934.48	9.44	929.51
+50				929.7.
11+00				929.7
	618		27.58	

	^{+1.6} <u>2.4</u> 33	^{+5.9} <u>2.6</u> 25	^{+0.3} <u>2.8</u> 18	^{+0.1} <u>2.4</u> 10	8.5	^{+0.3} <u>2.8</u> 4	^{+0.9} <u>2.4</u> 9	^{+1.0} <u>2.5</u> 11	^{+1.4} <u>2.1</u> 15	^{+1.1} <u>2.4</u> 18	^{+2.4} <u>10.9</u> 33		
^{+1.2} <u>0.7</u> 33	^{+0.9} <u>1.0</u> 24	^{+0.8} <u>2.7</u> 19	^{+0.5} <u>2.4</u> 14	^{+0.0} <u>1.9</u> 10	^{+0.1} <u>1.8</u> 4	1.9	^{+0.6} <u>2.5</u> 7	^{+1.3} <u>3.2</u> 11	^{+1.6} <u>3.5</u> 16	^{+0.5} <u>2.4</u> 19	^{+0.9} <u>2.8</u> 24	^{+2.0} <u>3.9</u> 33	
	^{+1.5} <u>2.3</u> 33	^{+1.9} <u>2.7</u> 24	^{+1.2} <u>2.0</u> 16	^{+0.3} <u>2.1</u> 8	5.8	^{+0.2} <u>2.0</u> 6	^{+1.3} <u>2.1</u> 14	^{+1.6} <u>2.4</u> 21	^{+1.6} <u>2.4</u> 33				
	^{+2.5} <u>11.3</u> 33	^{+2.3} <u>11.1</u> 14	^{+0.7} <u>2.5</u> 11	^{+0.2} <u>2.0</u> 7	8.8	^{+0.1} <u>2.9</u> 8	^{+0.0} <u>2.8</u> 13	^{+0.8} <u>2.6</u> 17	^{+1.1} <u>10.0</u> 24	^{+0.2} <u>2.0</u> 27	^{+0.8} <u>2.0</u> 33		
^{+2.9} <u>2.5</u> 33	^{+3.1} <u>2.7</u> 21	^{+3.2} <u>2.8</u> 14	^{+0.9} <u>5.5</u> 9	^{+0.3} <u>4.9</u> 5	4.2	^{+0.1} <u>4.5</u> 2	^{+0.3} <u>4.8</u> 7	^{+0.9} <u>5.5</u> 14	^{+1.6} <u>6.2</u> 15	^{+1.5} <u>6.1</u> 23	^{+0.4} <u>5.0</u> 24	^{+0.1} <u>4.7</u> 29	^{+2.7} <u>3.9</u> 33
	^{+3.0} <u>2.3</u> 33	^{+3.0} <u>2.3</u> 24	^{+2.8} <u>2.1</u> 13	^{+0.6} <u>5.9</u> 8	5.3	^{+0.6} <u>5.8</u> 9	^{+1.5} <u>6.8</u> 14	^{+1.4} <u>6.7</u> 22	^{+0.3} <u>5.6</u> 30	^{+0.2} <u>5.5</u> 33			
	^{+2.8} <u>2.2</u> 33	^{+2.7} <u>2.1</u> 20	^{+2.4} <u>2.0</u> 14	^{+0.6} <u>2.0</u> 9	6.4	^{+0.3} <u>6.7</u> 9	^{+1.8} <u>2.2</u> 12	^{+1.5} <u>2.9</u> 18	^{+1.1} <u>2.5</u> 23	^{+0.9} <u>2.5</u> 26	^{+0.3} <u>6.7</u> 28	^{+0.1} <u>6.5</u> 33	
	^{+1.9} <u>2.1</u> 33	^{+2.2} <u>2.4</u> 20	^{+2.1} <u>2.3</u> 14	^{+0.5} <u>2.7</u> 11	7.2	^{+0.5} <u>2.7</u> 11	^{+1.9} <u>2.1</u> 14	^{+1.9} <u>2.1</u> 24	^{+1.8} <u>2.0</u> 27	^{+1.3} <u>2.5</u> 30	^{+1.2} <u>2.4</u> 33		
^{+1.1} <u>6.4</u> 33	^{+0.3} <u>2.8</u> 20	^{+1.6} <u>2.1</u> 17	^{+1.6} <u>2.1</u> 14	^{+0.5} <u>2.0</u> 13	7.5	^{+0.0} <u>2.5</u> 4	^{+0.6} <u>2.1</u> 14	^{+1.6} <u>2.1</u> 16	^{+1.7} <u>2.2</u> 20	^{+0.1} <u>2.6</u> 24	^{+0.1} <u>2.6</u> 33		
^{+1.9} <u>6.5</u> 33	^{+0.7} <u>2.6</u> 20	^{+1.3} <u>2.6</u> 17	^{+1.3} <u>2.6</u> 15	^{+0.2} <u>2.5</u> 13	8.3	^{+0.2} <u>2.5</u> 9	^{+0.6} <u>2.9</u> 15	^{+1.6} <u>2.9</u> 17	^{+1.6} <u>2.9</u> 20	^{+0.1} <u>2.4</u> 22	^{+0.0} <u>2.3</u> 33		
^{+2.3} <u>2.2</u> 33	^{+1.1} <u>2.4</u> 20	^{+0.7} <u>10.2</u> 18	^{+0.7} <u>10.2</u> 15	^{+0.2} <u>2.7</u> 14	9.5	^{+0.8} <u>10.3</u> 17	^{+2.4} <u>11.9</u> 21	^{+2.6} <u>12.1</u> 24	^{+2.0} <u>11.5</u> 26	^{+2.0} <u>11.5</u> 33			
	^{+2.7} <u>2.1</u> 33	^{+1.7} <u>2.1</u> 20	^{+0.2} <u>4.6</u> 18	^{+0.4} <u>4.4</u> 11	4.8	^{+0.6} <u>5.4</u> 15	^{+0.2} <u>5.0</u> 18	^{+0.4} <u>5.2</u> 19	^{+1.9} <u>6.7</u> 21	^{+2.0} <u>6.8</u> 23	^{+1.4} <u>6.2</u> 25	^{+1.4} <u>6.2</u> 33	
^{+3.8} <u>1.0</u> 33	^{+3.2} <u>1.6</u> 19	^{+0.2} <u>5.0</u> 15	^{+0.2} <u>4.6</u> 10	^{+0.4} <u>4.4</u> 5	4.8	^{+0.5} <u>5.3</u> 3	^{+0.4} <u>4.4</u> 10	^{+0.6} <u>4.2</u> 12	^{+0.2} <u>4.6</u> 20	^{+0.1} <u>4.9</u> 28	^{+0.3} <u>4.5</u> 33		

STN. + H. I. - ELEV.

934.48

750

928.7.

12700

927.1.

750

923.9.

T.P.

0.28

921.83

12.93

921.55

13700

920.5.

750

918.0.

14700

916.0.

750

914.0.

15700

914.9.

750

915.1.

16700

915.4.

T.P.

6.24

921.37

6.68

915.14

915.11

750

913.6.

17700

913.2.

780

913.1.

$$\begin{array}{r} +1.4 \\ 2.4 \\ 33 \end{array} \quad \begin{array}{r} +1.5 \\ 3.5 \\ 20 \end{array} \quad \begin{array}{r} +0.3 \\ 6.1 \\ 15 \end{array} \quad \begin{array}{r} +0.3 \\ 5.5 \\ 9 \end{array} \quad \begin{array}{r} +0.3 \\ 5.5 \\ 6 \end{array} \quad 5.8 \quad \begin{array}{r} +0.2 \\ 6.0 \\ 5 \end{array} \quad \begin{array}{r} +1.3 \\ 4.5 \\ 6 \end{array} \quad \begin{array}{r} +2.1 \\ 3.7 \\ 10 \end{array} \quad \begin{array}{r} +1.8 \\ 4.0 \\ 23 \end{array} \quad \begin{array}{r} +1.4 \\ 4.4 \\ 25 \end{array} \quad \begin{array}{r} +1.5 \\ 4.3 \\ 33 \end{array}$$

$$\begin{array}{r} +4.6 \\ 2.8 \\ 33 \end{array} \quad \begin{array}{r} +2.6 \\ 4.8 \\ 21 \end{array} \quad \begin{array}{r} +0.6 \\ 8.0 \\ 16 \end{array} \quad \begin{array}{r} 0.0 \\ 7.4 \\ 10 \end{array} \quad \begin{array}{r} +0.2 \\ 7.2 \\ 4 \end{array} \quad 7.4 \quad \begin{array}{r} +0.4 \\ 7.8 \\ 4 \end{array} \quad \begin{array}{r} +0.1 \\ 7.5 \\ 6 \end{array} \quad \begin{array}{r} +0.3 \\ 7.7 \\ 14 \end{array} \quad \begin{array}{r} +0.8 \\ 8.2 \\ 24 \end{array} \quad \begin{array}{r} +1.2 \\ 8.2 \\ 33 \end{array}$$

$$\begin{array}{r} +2.0 \\ 8.6 \\ 33 \end{array} \quad \begin{array}{r} +0.9 \\ 9.7 \\ 21 \end{array} \quad \begin{array}{r} +0.4 \\ 11.0 \\ 19 \end{array} \quad \begin{array}{r} +0.5 \\ 11.1 \\ 15 \end{array} \quad \begin{array}{r} +0.1 \\ 10.7 \\ 11 \end{array} \quad \begin{array}{r} +0.2 \\ 10.4 \\ 3 \end{array} \quad 10.6 \quad \begin{array}{r} +0.3 \\ 10.9 \\ 8 \end{array} \quad \begin{array}{r} +0.9 \\ 11.5 \\ 9 \end{array} \quad \begin{array}{r} +0.7 \\ 11.3 \\ 14 \end{array} \quad \begin{array}{r} +1.4 \\ 12.0 \\ 16 \end{array} \quad \begin{array}{r} +1.8 \\ 12.4 \\ 33 \end{array}$$

$$\begin{array}{r} +1.1 \\ 0.2 \\ 33 \end{array} \quad \begin{array}{r} +0.3 \\ 1.0 \\ 19 \end{array} \quad \begin{array}{r} +0.2 \\ 1.5 \\ 18 \end{array} \quad \begin{array}{r} +0.1 \\ 1.4 \\ 15 \end{array} \quad \begin{array}{r} +0.2 \\ 1.1 \\ 12 \end{array} \quad \begin{array}{r} +0.3 \\ 1.0 \\ 6 \end{array} \quad 1.3 \quad \begin{array}{r} +0.5 \\ 1.8 \\ 9 \end{array} \quad \begin{array}{r} +0.9 \\ 2.2 \\ 11 \end{array} \quad \begin{array}{r} +1.0 \\ 2.3 \\ 12 \end{array} \quad \begin{array}{r} +1.1 \\ 2.4 \\ 13 \end{array} \quad \begin{array}{r} +1.5 \\ 2.8 \\ 24 \end{array} \quad \begin{array}{r} +1.3 \\ 2.6 \\ 33 \end{array}$$

$$\begin{array}{r} +1.5 \\ 2.3 \\ 33 \end{array} \quad \begin{array}{r} +0.8 \\ 3.0 \\ 30 \end{array} \quad \begin{array}{r} +0.6 \\ 3.2 \\ 20 \end{array} \quad \begin{array}{r} +0.1 \\ 3.7 \\ 18 \end{array} \quad \begin{array}{r} +0.1 \\ 3.7 \\ 9 \end{array} \quad 3.8 \quad \begin{array}{r} +0.7 \\ 4.5 \\ 8 \end{array} \quad \begin{array}{r} +0.9 \\ 4.7 \\ 14 \end{array} \quad \begin{array}{r} +0.8 \\ 4.6 \\ 24 \end{array} \quad \begin{array}{r} +0.6 \\ 4.4 \\ 33 \end{array}$$

$$\begin{array}{r} +0.7 \\ 5.1 \\ 33 \end{array} \quad \begin{array}{r} +0.2 \\ 6.0 \\ 22 \end{array} \quad \begin{array}{r} +0.8 \\ 6.6 \\ 18 \end{array} \quad \begin{array}{r} +0.9 \\ 6.7 \\ 16 \end{array} \quad \begin{array}{r} +0.1 \\ 5.7 \\ 14 \end{array} \quad \begin{array}{r} +0.2 \\ 5.6 \\ 3 \end{array} \quad 5.8 \quad \begin{array}{r} +0.1 \\ 5.9 \\ 4 \end{array} \quad \begin{array}{r} +0.7 \\ 6.5 \\ 6 \end{array} \quad \begin{array}{r} +1.6 \\ 7.4 \\ 10 \end{array} \quad \begin{array}{r} +1.8 \\ 7.6 \\ 12 \end{array} \quad \begin{array}{r} +1.7 \\ 7.5 \\ 33 \end{array}$$

$$\begin{array}{r} +0.2 \\ 7.6 \\ 33 \end{array} \quad \begin{array}{r} +0.1 \\ 7.7 \\ 19 \end{array} \quad \begin{array}{r} +0.3 \\ 8.1 \\ 18 \end{array} \quad \begin{array}{r} +0.3 \\ 8.1 \\ 16 \end{array} \quad \begin{array}{r} +0.8 \\ 7.0 \\ 12 \end{array} \quad \begin{array}{r} +1.0 \\ 6.8 \\ 6 \end{array} \quad 7.8 \quad \begin{array}{r} +2.4 \\ 10.2 \\ 18 \end{array} \quad \begin{array}{r} +0.4 \\ 7.4 \\ 19 \end{array} \quad \begin{array}{r} 0.0 \\ 7.8 \\ 28 \end{array} \quad \begin{array}{r} +0.2 \\ 7.6 \\ 33 \end{array}$$

$$\begin{array}{r} +0.2 \\ 7.7 \\ 33 \end{array} \quad \begin{array}{r} +1.1 \\ 8.0 \\ 20 \end{array} \quad \begin{array}{r} +1.2 \\ 8.1 \\ 16 \end{array} \quad \begin{array}{r} +0.1 \\ 7.0 \\ 15 \end{array} \quad \begin{array}{r} +0.1 \\ 6.8 \\ 9 \end{array} \quad 6.9 \quad \begin{array}{r} +1.3 \\ 7.2 \\ 9 \end{array} \quad \begin{array}{r} +0.8 \\ 7.7 \\ 10 \end{array} \quad \begin{array}{r} +1.0 \\ 7.9 \\ 15 \end{array} \quad \begin{array}{r} +1.1 \\ 8.0 \\ 17 \end{array} \quad \begin{array}{r} +0.7 \\ 7.6 \\ 27 \end{array} \quad \begin{array}{r} +1.1 \\ 8.0 \\ 33 \end{array}$$

$$\begin{array}{r} +0.4 \\ 7.1 \\ 33 \end{array} \quad \begin{array}{r} +0.8 \\ 7.5 \\ 21 \end{array} \quad \begin{array}{r} +0.9 \\ 7.6 \\ 16 \end{array} \quad \begin{array}{r} +0.3 \\ 7.0 \\ 12 \end{array} \quad \begin{array}{r} +0.8 \\ 7.5 \\ 3 \end{array} \quad 6.7 \quad \begin{array}{r} +0.1 \\ 6.8 \\ 6 \end{array} \quad \begin{array}{r} +1.0 \\ 7.7 \\ 8 \end{array} \quad \begin{array}{r} +1.2 \\ 7.9 \\ 14 \end{array} \quad \begin{array}{r} +1.0 \\ 7.7 \\ 33 \end{array}$$

$$\begin{array}{r} +1.0 \\ 5.4 \\ 33 \end{array} \quad \begin{array}{r} +0.5 \\ 5.9 \\ 19 \end{array} \quad \begin{array}{r} +0.5 \\ 6.9 \\ 18 \end{array} \quad \begin{array}{r} +0.4 \\ 6.8 \\ 16 \end{array} \quad \begin{array}{r} +0.1 \\ 6.3 \\ 13 \end{array} \quad \begin{array}{r} +0.2 \\ 6.6 \\ 6 \end{array} \quad 6.4 \quad \begin{array}{r} 0.0 \\ 6.4 \\ 5 \end{array} \quad \begin{array}{r} +0.8 \\ 7.2 \\ 8 \end{array} \quad \begin{array}{r} +1.6 \\ 8.0 \\ 17 \end{array} \quad \begin{array}{r} +1.5 \\ 7.9 \\ 27 \end{array} \quad \begin{array}{r} +0.9 \\ 7.3 \\ 33 \end{array}$$

$$\begin{array}{r} +0.4 \\ 7.4 \\ 33 \end{array} \quad \begin{array}{r} +0.4 \\ 8.2 \\ 22 \end{array} \quad \begin{array}{r} +0.7 \\ 8.5 \\ 16 \end{array} \quad \begin{array}{r} +0.7 \\ 8.5 \\ 12 \end{array} \quad \begin{array}{r} +0.1 \\ 7.7 \\ 10 \end{array} \quad 7.8 \quad \begin{array}{r} +0.2 \\ 7.6 \\ 10 \end{array} \quad \begin{array}{r} +0.1 \\ 7.7 \\ 20 \end{array} \quad \begin{array}{r} +0.3 \\ 7.5 \\ 33 \end{array}$$

$$\begin{array}{r} +1.3 \\ 9.5 \\ 33 \end{array} \quad \begin{array}{r} +1.3 \\ 9.5 \\ 26 \end{array} \quad \begin{array}{r} +1.2 \\ 9.4 \\ 22 \end{array} \quad \begin{array}{r} +0.7 \\ 8.9 \\ 16 \end{array} \quad \begin{array}{r} 0.0 \\ 8.2 \\ 12 \end{array} \quad 8.2 \quad \begin{array}{r} 0.0 \\ 8.2 \\ 10 \end{array} \quad \begin{array}{r} +0.1 \\ 8.1 \\ 20 \end{array} \quad \begin{array}{r} +0.4 \\ 7.8 \\ 33 \end{array}$$

$$\begin{array}{r} +1.5 \\ 9.6 \\ 33 \end{array} \quad \begin{array}{r} +1.3 \\ 9.6 \\ 22 \end{array} \quad \begin{array}{r} +1.2 \\ 9.5 \\ 16 \end{array} \quad \begin{array}{r} +0.5 \\ 8.8 \\ 13 \end{array} \quad \begin{array}{r} +0.2 \\ 8.5 \\ 7 \end{array} \quad 8.3 \quad \begin{array}{r} +0.1 \\ 8.4 \\ 10 \end{array} \quad \begin{array}{r} +0.1 \\ 8.2 \\ 20 \end{array} \quad \begin{array}{r} +0.5 \\ 7.8 \\ 33 \end{array}$$

STA.	+	H.I.	-	ELEV.
		921.37		
18+00				915.4.
+50				916.4.
19+00				912.8.
+50				909.7.
T.P.	4.68	915.60	10.45	910.92.
20+00				908.2.
+50				907.6.
21+00				908.2.
+50				908.8.
22+00				912.3.
T.P.	10.45	922.19	3.86	911.74.
+62				918.8.
23+00				918.6.
+24				916.3.
B.M.	12.49	924.17	10.40	911.79.
+40				919.7.
				911.78

-1.6	-1.2	-1.1	-0.6		+0.4	+0.7	+0.8
<u>7.6</u>	<u>7.2</u>	<u>7.1</u>	<u>6.6</u>		<u>5.5</u>	<u>5.3</u>	<u>5.2</u>
33	22	16	10	60	14	20	33

-1.8	-1.0	-0.9	-0.6		+0.7	+1.8	+2.0	+2.7
<u>6.8</u>	<u>6.0</u>	<u>5.9</u>	<u>5.6</u>		<u>4.3</u>	<u>5.2</u>	<u>5.0</u>	<u>2.5</u>
33	23	12	7	5.0	6	18	27	33

-3.6	-2.7	-0.8	-0.6		+0.1	+1.0	+1.6	+2.3
<u>12.2</u>	<u>11.3</u>	<u>9.4</u>	<u>9.2</u>		<u>8.5</u>	<u>7.6</u>	<u>7.0</u>	<u>6.5</u>
33	19	7	6	8.6	7	15	27	33

-1.2	-1.1	-0.5			+0.1	+0.6	+0.8
<u>12.9</u>	<u>12.8</u>	<u>12.2</u>			<u>11.6</u>	<u>11.1</u>	<u>10.9</u>
33	11	6	11.7		11	18	33

-0.4	-0.3	-0.2	-0.6		+0.2	+0.8	+1.0
<u>7.8</u>	<u>7.7</u>	<u>7.6</u>	<u>8.0</u>		<u>7.2</u>	<u>6.6</u>	<u>6.4</u>
33	21	15	11	7.4	10	24	33

0.0	+0.4	+0.2			+0.7	+1.2	+1.3
<u>8.0</u>	<u>7.6</u>	<u>7.8</u>			<u>7.3</u>	<u>6.8</u>	<u>6.7</u>
33	15	8	8.0		13	24	33

-0.4	-0.1				+0.3	+0.4	+0.5
<u>7.8</u>	<u>7.5</u>				<u>7.1</u>	<u>7.0</u>	<u>6.9</u>
33	12	7.4			5	18	33

0.0	-0.2	0.0			0.0	+0.1	+0.5
<u>6.8</u>	<u>7.0</u>	<u>6.8</u>			<u>6.8</u>	<u>6.7</u>	<u>6.5</u>
33	17	5	6.8		10	20	33

+0.4	+0.4	+0.7	0.0		-0.4	-0.7	-0.7	-1.0	-3.1
<u>2.9</u>	<u>2.9</u>	<u>2.6</u>	<u>3.3</u>		<u>3.7</u>	<u>4.0</u>	<u>4.0</u>	<u>4.3</u>	<u>6.4</u>
33	20	16	6	3.3	10	20	33	50	115

+2.0	+1.2	+0.9	+0.4		+1.1	+1.6	+2.4	+3.1
<u>1.4</u>	<u>2.2</u>	<u>2.5</u>	<u>3.0</u>		<u>4.5</u>	<u>5.0</u>	<u>5.8</u>	<u>6.5</u>
33	27	16	10	3.4	16	21	30	33

+1.2	+0.2	+0.4			-1.0	-1.5	-1.7	-2.8
<u>2.4</u>	<u>3.4</u>	<u>3.2</u>			<u>4.6</u>	<u>5.1</u>	<u>5.3</u>	<u>6.4</u>
33	20	10	3.6		11	13	23	33

+2.7	+1.9	+0.9	+0.4	+0.1		+1.4	+0.7	-1.0	-1.5	-1.8
<u>5.2</u>	<u>4.0</u>	<u>5.0</u>	<u>5.5</u>	<u>5.8</u>		<u>4.5</u>	<u>5.2</u>	<u>6.9</u>	<u>7.4</u>	<u>7.7</u>
33	26	20	11	5	5.9	5	13	19	29	33

+0.1	0.0	-0.1			+0.3	+0.2	-0.5	-0.4
<u>4.5</u>	<u>4.6</u>	<u>4.7</u>			<u>4.3</u>	<u>4.4</u>	<u>5.1</u>	<u>5.0</u>
33	16	5	4.6		5	11	18	33

STN. + H.I. - ELEV.

914.27

+44⁷ TOP OF WEST RAIL

920.7.

+49⁷ TOP OF EAST RAIL

920.5.

B.M. 10.85 922.63 12.49

911.78

+55

919.6.

+67

917.2.

+80

913.9.

24

910.0.

+13

909.4.

B.M.

10.85 911.78

+1.26	+0.85	+0.57	+0.24	-0.25	-0.39	-0.49	-0.72
<u>2.34</u>	<u>2.75</u>	<u>3.03</u>	<u>3.32</u>	<u>3.85</u>	<u>3.99</u>	<u>4.09</u>	<u>4.32</u>
200	150	100	50	3.60	50	100	150
200	150	100	50	3.60	50	100	150
+1.40	+1.07	+0.70	+0.34	-0.71	-0.55	-0.58	0.78
<u>2.36</u>	<u>2.69</u>	<u>3.06</u>	<u>3.42</u>	<u>4.05</u>	<u>4.21</u>	<u>4.34</u>	<u>4.54</u>
200	150	100	50	3.76	50	100	150
200	150	100	50	3.76	50	100	150

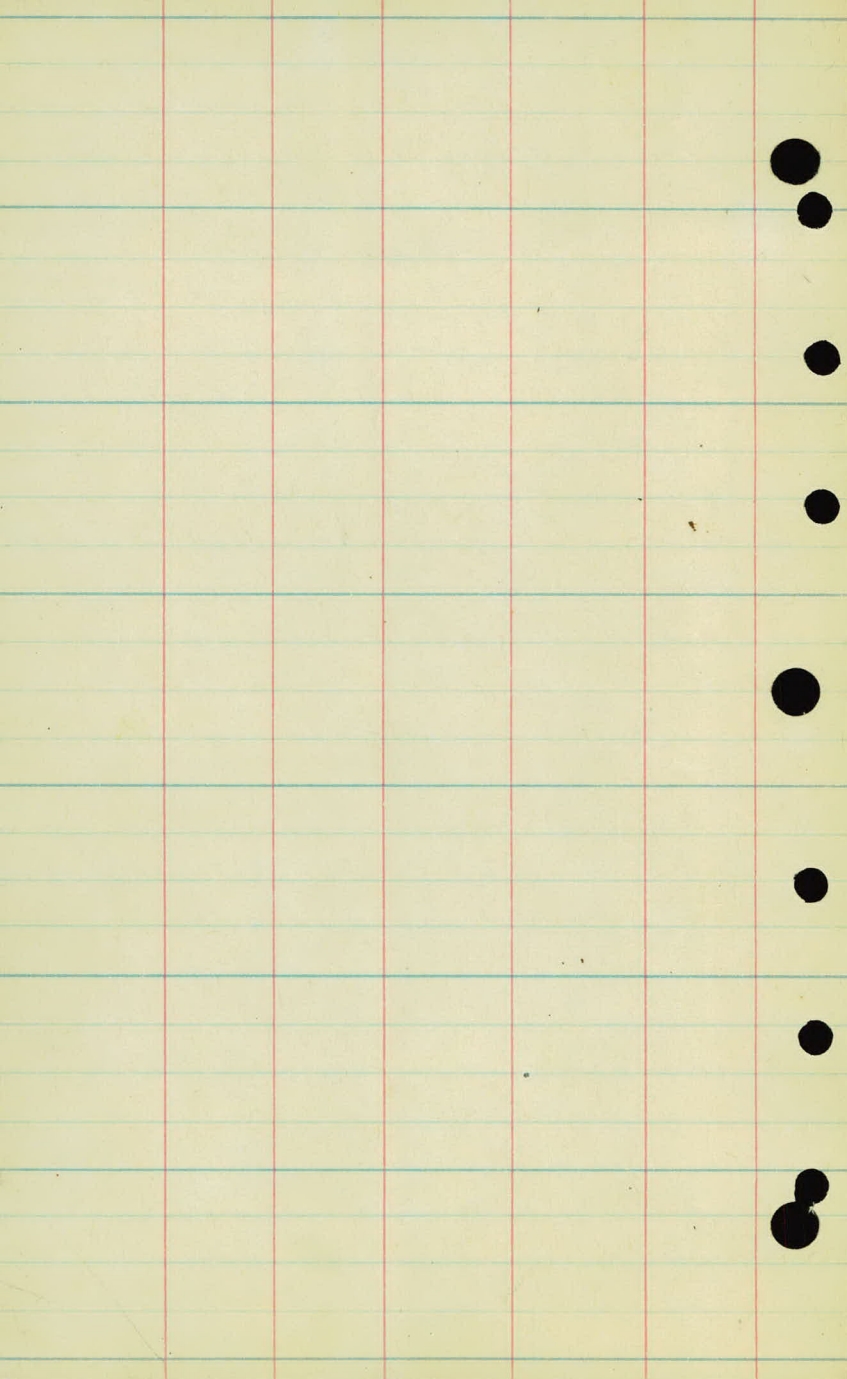
-0.1	-0.2	+0.1	-0.4	-0.6
<u>3.1</u>	<u>3.2</u>	<u>3.9</u>	<u>3.4</u>	<u>3.5</u>
33	5	3.0	11	16
33	5	3.0	11	16

+2.4	+1.5	+0.1	-0.5	0.0	+0.2	+1.1
<u>3.0</u>	<u>3.9</u>	<u>5.3</u>	<u>5.9</u>	<u>5.4</u>	<u>5.2</u>	<u>4.3</u>
33	19	3	7	15	18	33
33	19	3	7	15	18	33

+0.1	-1.0	-1.4	-0.1	-0.3	-1.9	-2.0
<u>8.6</u>	<u>9.7</u>	<u>10.1</u>	<u>8.8</u>	<u>9.0</u>	<u>10.6</u>	<u>10.7</u>
33	19	5	2	15	23	32
33	19	5	2	15	23	32

+0.7	+0.5	0.0	+0.1	-0.7	-1.1
<u>11.9</u>	<u>12.1</u>	<u>12.6</u>	<u>12.5</u>	<u>13.3</u>	<u>13.7</u>
33	22	10	10	13	33
33	22	10	10	13	33

+0.1	-0.2	-0.4	0.0	-0.5	-1.2	-1.3
<u>13.1</u>	<u>13.4</u>	<u>13.6</u>	<u>13.2</u>	<u>13.7</u>	<u>14.4</u>	<u>14.5</u>
33	22	11	8	8	14	33
33	22	11	8	8	14	33



PROJ. # 62-132-177.

CLARK AV.

CHECK LEVELS FROM RICE
ST. TO A POINT $\frac{1}{2}$ MILE
EAST.

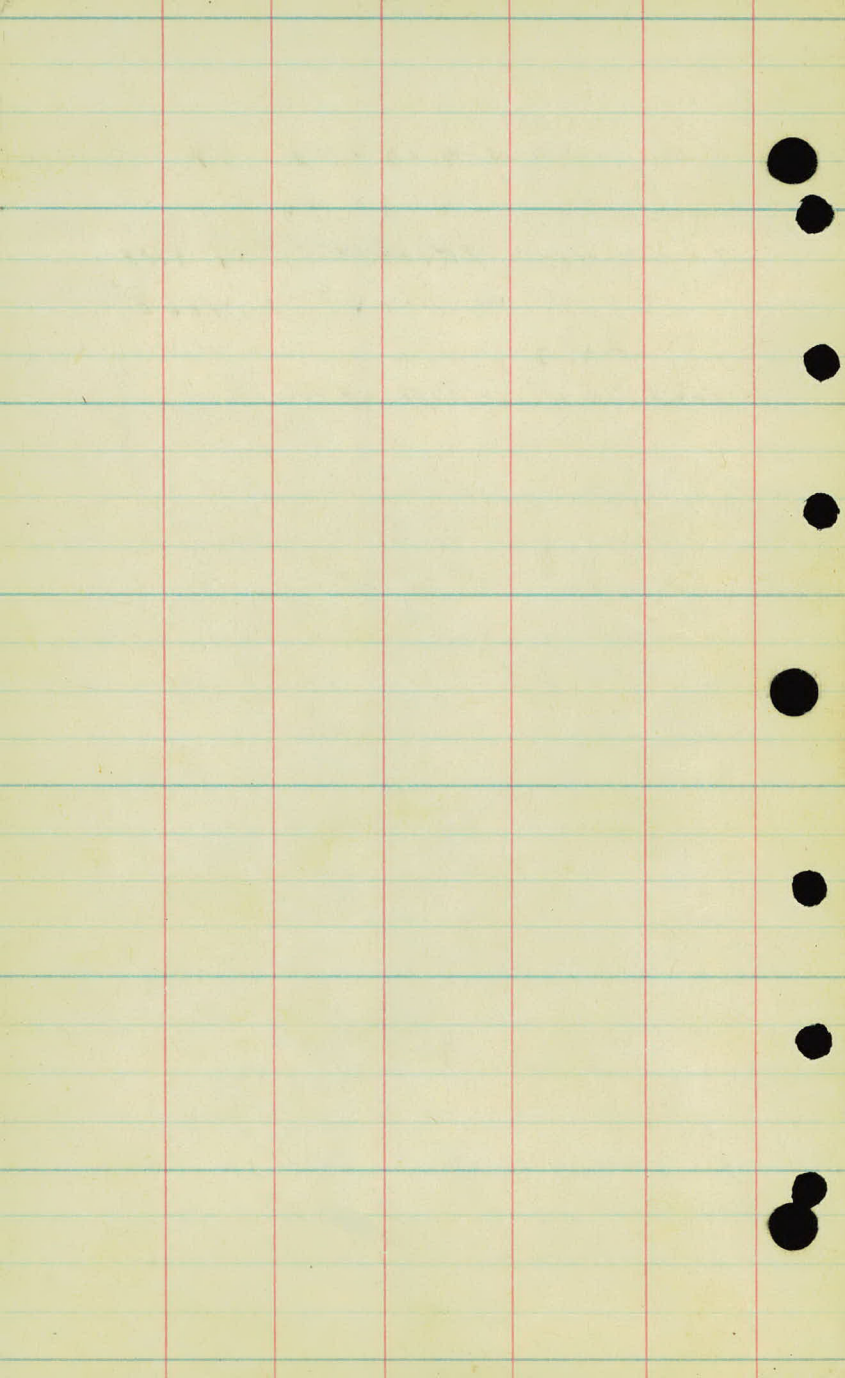
STA.	+	H.I	-	ELEV.
B.M.	11.23	923.01		911.78
T.P.	4.56	921.73	5.84	917.17
B.M.			6.62	915.11
T.P.	13.66	954.05	1.34	920.39
T.P.	12.84	944.98	1.91	932.14
B.M.			5.89	939.09
T.P.	11.88	956.10	0.76	944.22
B.M.			0.82	955.28 ✓

ON IRON MARKER 45 FT. STA. 0-18. ✓

SPK IN 8" OAK 30' LT. STA. 16+40 ✓

SPK IN FENCE COR. 100' LT. STA. 6+45 ✓

6+00 & HOLE IN PAVE. ✓



PROJ # 62-132-177

CLARK FV.

ALIGNMENT FROM RICE
ST. TO A POINT $\frac{1}{2}$ MILE
EAST.

STA. POINT Δ LT. Δ RT

24+13⁰⁰ P.I. 0°-10'

x

23+47¹⁷ P.O.T.

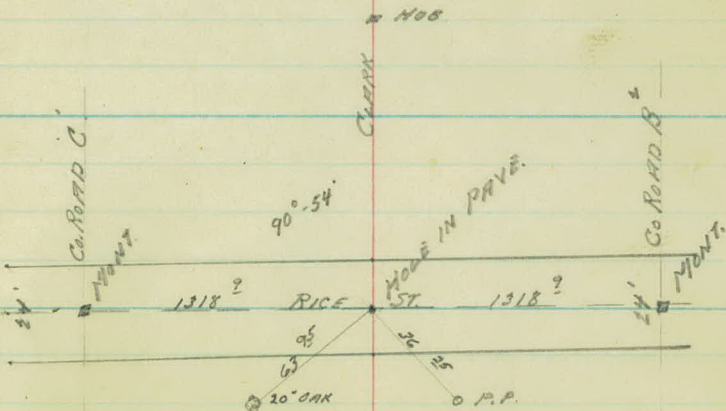
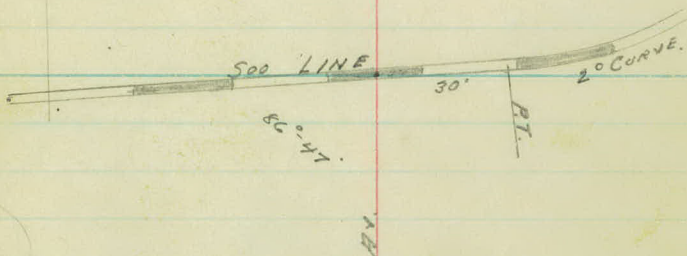
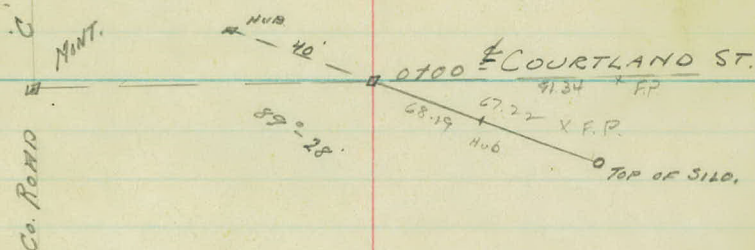
589°-06'E

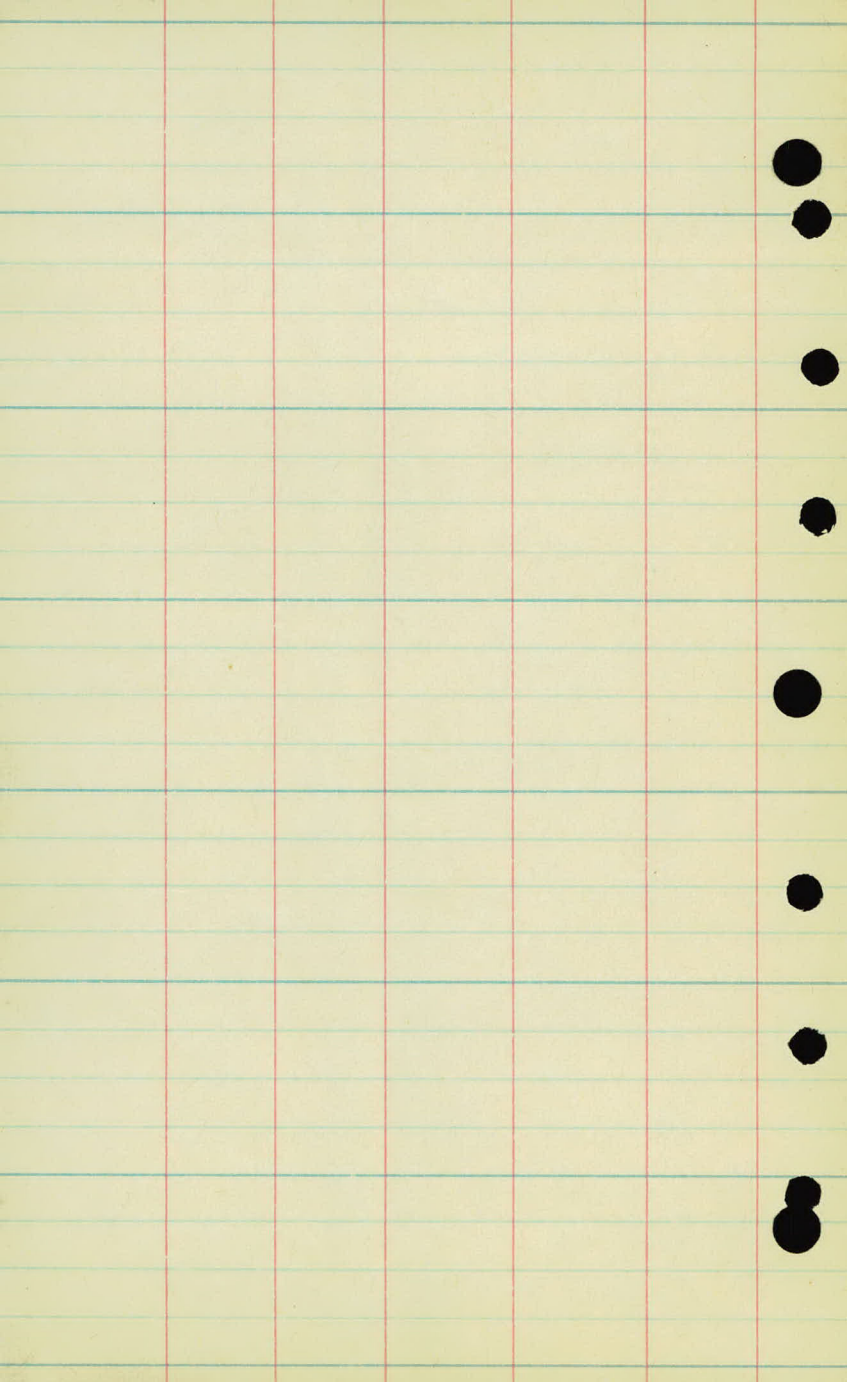
4+71⁵⁵ P.O.T.

0+00 P.O.T.

x

IRON
26 + 26.90





PROJ. #62-B2-177

CLARK AV.

ART. TOPOG. FROM RICE
ST. TO A. POINT $\frac{1}{2}$ MILE
EAST.

5

4

3

2

1

0 + 00

CULTIVATED.

CULTIVATED.

+29 X.F. 40'

+26 T.P. 43.

+12' EDGE OF PINE.

x x

x x x

+31 X.F. 22

24' P.M.V.E.

12

11

10

9

8

7

6

5

F. 20²

F. 25⁵

+28-6"-T-11
+81-6"-T-20

+40-14"-T-8

F. 20

F. 27

+51-30"-T-30

F. 20

PASTURE

CULTIVATED

F. 26

+60-6"-T-33

F. 20

+20-6"-T-22

F. 24

HAY FIELD

+91 F. COR. 22

F. 23

+38 F. COR. 22⁵

+29 PRI. ENZ

+21 F. COR. 22⁵

F. 23

CULTIVATED

FARM YARD

+06 F. COR. 23

+78-6"-T-21

19

18

17

16

15

14

13

12

F. 9.

+44 F. CoR. 22

F. 11⁵
F. 22

F. 18⁵
F. 22⁵

+20 F. 14

+125 TUNING 8
F. 22

F. 21

F. 21

F. 21

PASTURE

PASTURE

SCATTERED OAKS

PASTURE

CULTIVATED

HAY MEADOW

SWAMP

HAY FIELD

+96 X.F.
+70 F. 12

F. 15

F. 15

F. 15

+06 F. CoR 14⁵

25

24

23

22

21

20

19

700 F 21

795 X.F.

713 F.C.R. 14⁵

794 PIPE LINE 49
129 X DRAIN
EXTENDS 19 R. 65' L
16" X 24' V.I.T.

500 LINE.

710 T.P. 6⁵

796 F. 0.5' L
798 X.F.

700 F. ENT. 18

PASTURE.

PASTURE.

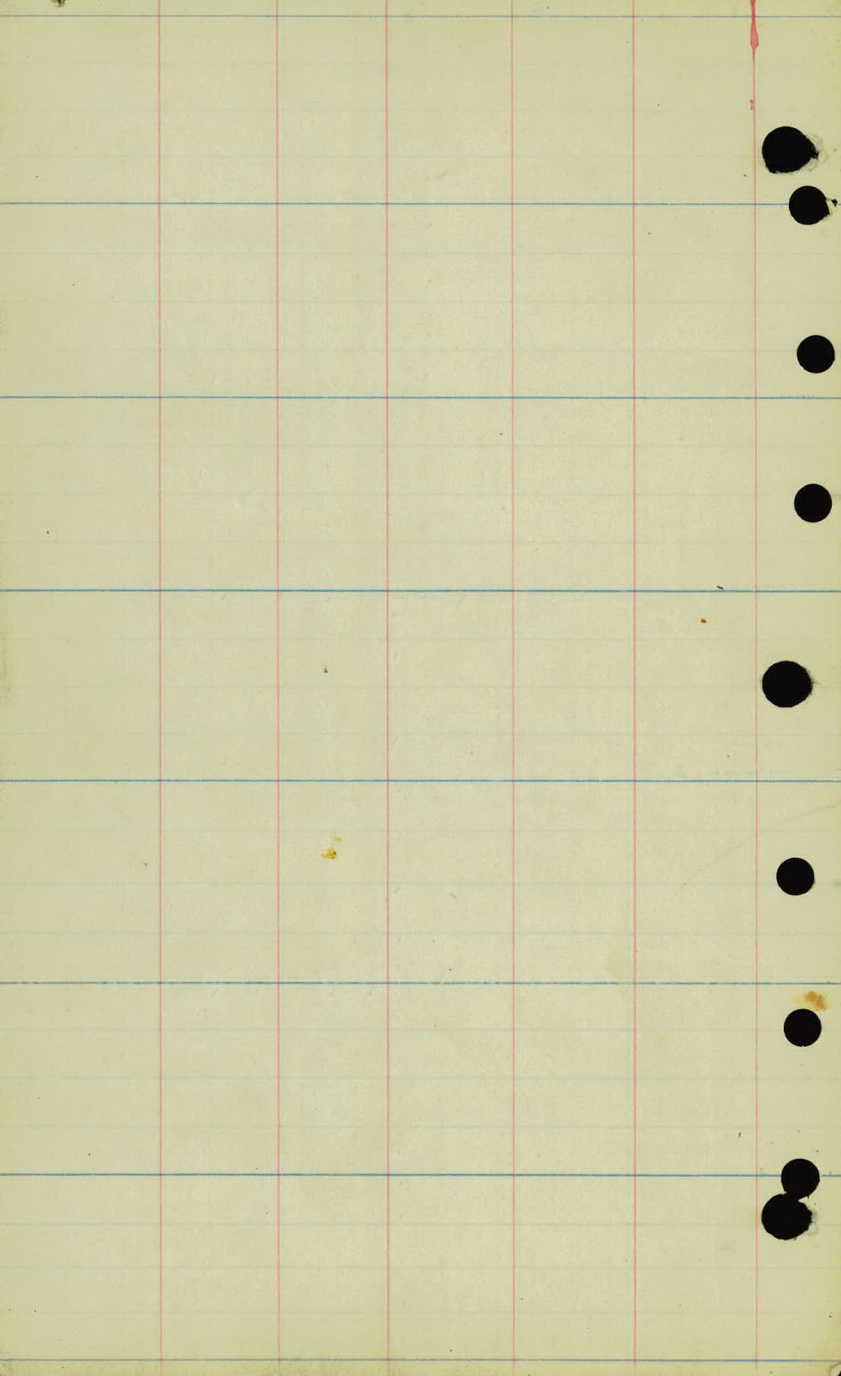
F. 2'

F. 4

785 X.F.

SWAMP

F. 6



1
Dumont Ave.

Ditch & Drainage

10 pages

drawn up -6-6-57

Sta	+	π	-	Elev
BM	3.90	941.85		937.95 100.00

Water Surface			6.13	935.72
---------------	--	--	------	--------

Bottom of Pond			8.7	933.15
----------------	--	--	-----	--------

6

+ 10

+ 25

+ 35

+ 50

FX
AM
Ed G

June 4, 1954

L

RT

2

Spt in PP 29' RT Sta 6+24

40.8
1.1 5.8
100

36.1
5.8
55

39.7 36.3 36.1 35.0 36.7
2.2 5.6 5.8 6.9 5.2
23 33 43 52

Pitch
(End Overflow
Drain)
36.0 35.4 35.7 36.6
5.9 6.5 6.2 5.3
20 29 31 53
Pitch

38.6
33

34.9
20
23
Pitch

Sta	+	x	-	Elev
-----	---	---	---	------

		941.85		
		103.90		

7

+15 W. End 15" x 20' CM

+35 E. End 15" x 20' CM

8

9

10

TP	1.34	929.75	928.41	928.41
		91.80	13.44	90.46

2

Ditch

3

.1
30
5.2

.1
30
8.2

.58
33
8.27
FL

.33
33
8.52
FL

.1
30
8.2

.14
31
10.5

.9
30
11.0

.1
28
13.2

.6
30
13.4

.3
26
15.6

Sta + X. - Elev

929.75

~~91.80~~

10+45 W End 15" x 20' CM

+65 E End 15" x 20' CM

11

12

13

14

917.97

916.54

TP 1.43 ~~80.02~~ 13.21 ~~78.59~~

2

Ditch

4

25.80

3.95
FL

24.99

4.76
FL

26.1

3.7

24.6

5.2

23.6

6.2

21.1

8.7

20.9

8.9

18.4

11.4

18.2

11.6

15.1

14.7

Sta + π - Elev

917.97
~~88.02~~

15

16

17

18

19

+36 24" X 38' CM X Drain

2

Ditch

15.8

13.2

2.2

4.8

14.6

12.0

3.4

6.0

13.4

11.1

4.6

6.9

13.0

10.5

5.0

7.5

12.6

09.7

5.4

8.3

09.33

08.57

12.2

08.99

8.64

9.40

5.8

8.98

Water
Surface

FL

FL

S. End

Sta + . π - Elev

917.97
~~80.02~~

20

21

+50

916.52

910.57

BM 5.95 ~~78.57~~ 7.40 ~~72.62~~

3+93 Cortland Ave

W. End 20" C.I. X-Drain Under R.R. Tracks

TP 5.58 ~~83.69~~ 0.46 ~~78.11~~

921.64

916.06

TP 0.78 ~~76.11~~ 8.36 ~~75.33~~

914.06

913.28

3+93 E End 20" C.I. X-Drain Under RR Tracks

L

Ditch

8.1

11.8

9.2

9.9

6.2

8.8

Bottom
Pond

8.2

11.9

9.2

9.8

6.1

8.8

Bottom
Pond

12.8

10.2

5.2

7.8

Top N. End 24" x 28" x Drain Sta 19 + 36

06.04

Ditch From Swamp

10.48

to Culvert Under

FL

R.R. Tracks Should

Be Cleaned. Would

Drain Marsh

05.05

9.01

Sta + π - Elev

914.06
~~76.11~~

CM

3+93 W End 24"X40" X Drain of Cortland

CM

3+93 E. End 24"X40" X Drain of Cortland

Water Surface E. of Cortland

		913.47		906.41	
BM	7.06	75.52	7.65	68.46	
		924.08		912.65	
TP	11.43	86.13	0.82	74.70	
		917.36		913.03	
TP	4.33	79.41	11.05	75.08	
				910.58	
BM			6.78	72.63	72.62
		924.67		914.45	
TP	10.22	86.72	2.91	76.50	
		934.54		924.66	
TP	9.88	96.59	0.01	86.71	
		942.23		933.15	
TP	9.08	104.28	1.39	95.20	
				937.95	
BM			4.28	100.00	

✓

FK
AM
LC
MMc
Ed G.

June 7, 1954

7

0485

9.21

0441

9.65

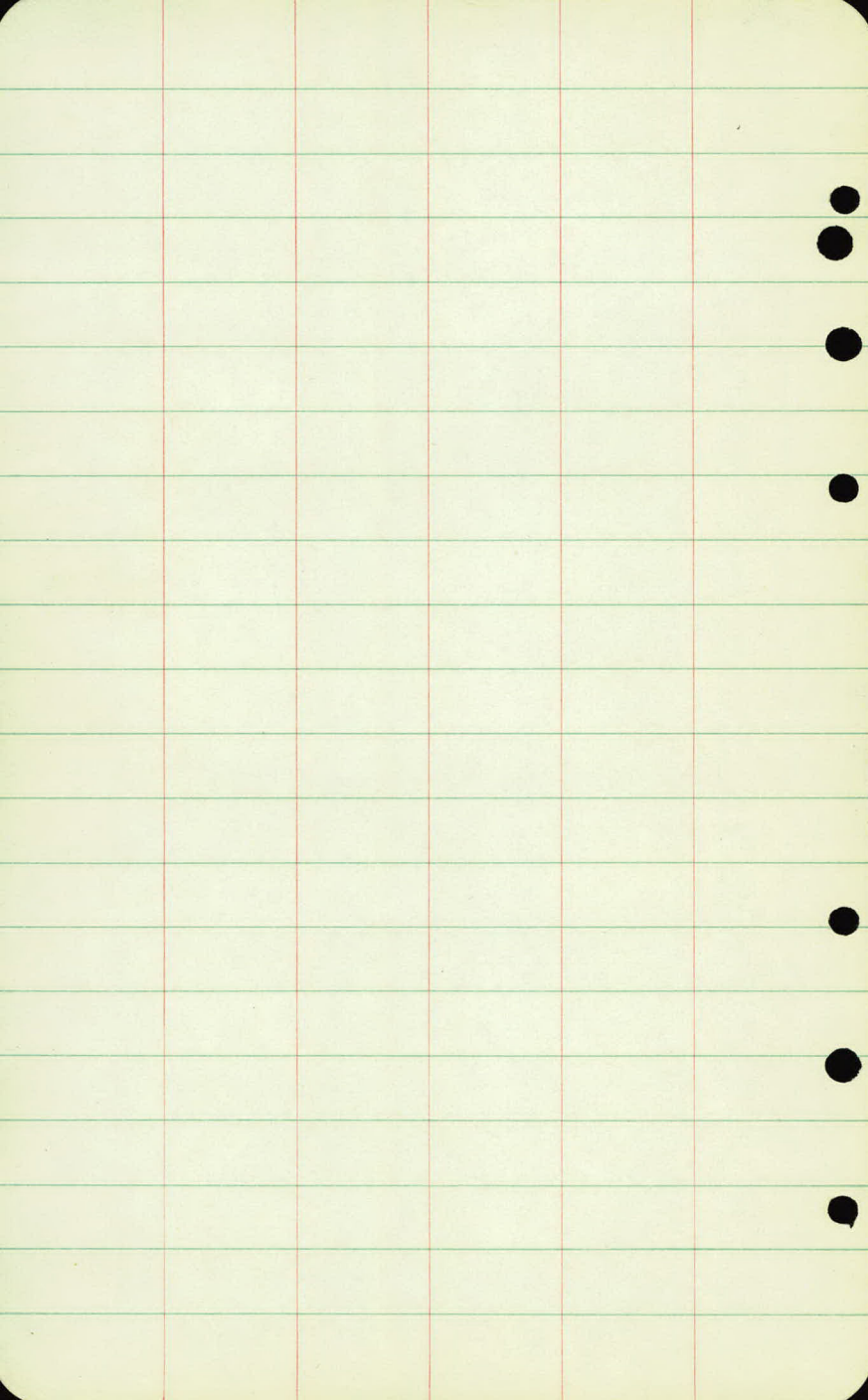
02.58

11.48

Top E. End 24" Culvert under Cortland Sta 2+93

Top N End Culvert Sta 19+36

Spt in PP 29' Rt Sta 6+24



DEMONT

Swamp

Topography

6

End Pothole
+95 96 to 150

3

Pothole
75 to 125

A

Pothole
80 to 150

Begin Pothole
+60 120'

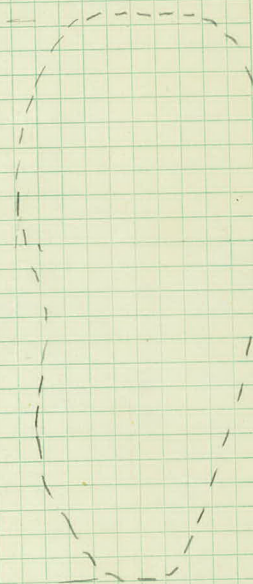
2

6

5

4

3



22 Edge Swamp
120'

Swamp
+40 22'

21 Swamp
20

20 Swamp
20' + 130
Swamp
+60 25 + 60

15

Marsh
+50 25 + 70

14 Edge Marsh
22'

+50 Edge Marsh
100'

13

22

21

20

15

14

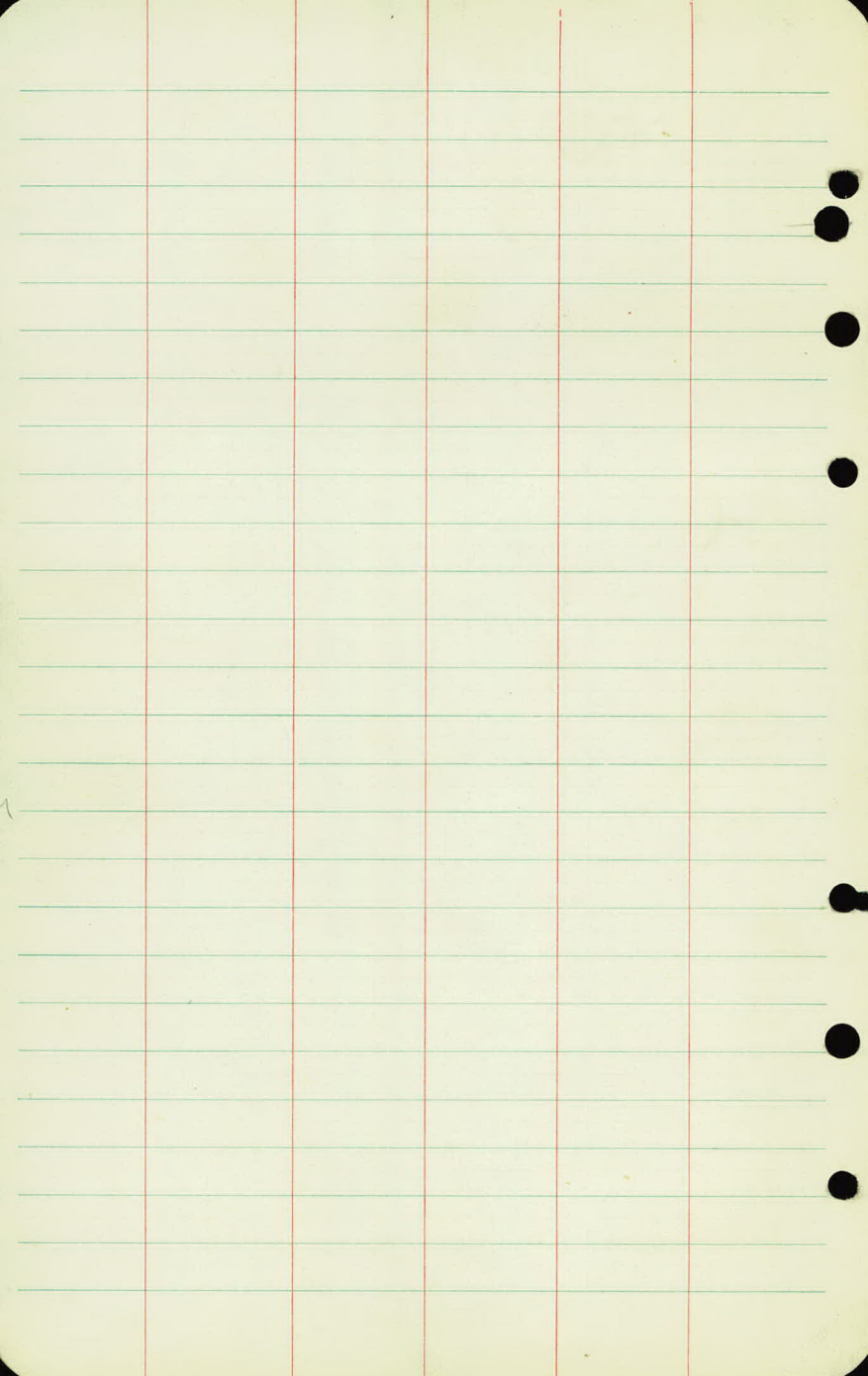
13

13

Dry

Spring

Swamp



FX
HG
DS
GA

Jan 8, 1973

1

~~CO. RD. C
RICE ST TO LAKESHORE DR.~~

BENCH LEVELS

FOR

Jackson & Demont
Sight Distances

12-181

STA	+	T	-	ELEV.
BM	10.26	959.25		(948.99)
	0.80	952.98	7.07	952.18
	2.86	945.31	10.53	942.45
			7.68	937.63
			13.05	932.26

BM	6.31	931.19		(924.88)
TP	9.31	938.76	1.74	929.45
	9.17	945.84	2.09	936.67
			3.30	942.54
			8.13	937.71
	1.90	938.56	9.18	936.66
	2.05	934.36	6.25	932.31
	0.37	924.14	10.59	923.77
	4.28	915.79	12.63	911.51
	7.77	916.01	7.55	908.24
			2.36	913.65
BM	8.32	921.97		
5+00			1.3	920.7
	E. Rail		1.35	920.62
	W Rail		1.26	920.71

FK
KP
DS
GA

Jan 8, 1973

DESCRIPTION

2

SPIKE IN PP NW COR STARK

SPIKE IN S.W. BRIDGE ABUTMENT

SPIKE IN ARC-LITE POLE S.E. COR ^{JACKSON}

TOP PK & STA 12+00 JACKSON ST.

TOP HYD RT STA 10+09

TOP HYD NW COR C: LAKESHORE DR

TOP STAKE 33' LT STA 305+50

TOP HYD 38' LT STA 302+63 Co. ROC

SPIKE IN PP SE COR JACKSON & C

JACKSON ST STA 12

TOP YEL Connector Post

TOP HYD RT STA 10+09 JACKSON ST

TOP ROCK

SPIKE IN ARC-LITE POLE ZOO'S LAKE

SPIKE IN PP 400' S. LAKE

SPIKE IN PP NE COR DEMONT

Sta	+	7 921.97	-	Elev	
4+75			1.2	920.8	1.3
+50			2.5	919.5	1.4
+25			3.9	918.1	1.3
A			5.2	916.8	
3+50			7.0	915.0	1.8
3			8.2	913.8	1.2
2+50			8.7	913.3	0.5
2			9.2	912.8	
1+50			9.2	912.8	
1			8.6	913.4	
0+50			8.7	913.3	
0+00			8.5	913.5	
5+25			2.2	919.8	
+50			4.0	918.0	
+75			5.5	916.5	
6			7.6	914.4	
+50			10.4	911.6	
7			12.4	909.6	

FK
KP
DS
GA

Jan 8, 1973
Cold - 7°F

3

Sta	+	π	-	Elev.
		921.97		
7+50			13.1	908.9
8			13.4	908.6
+50			13.2	908.8
9			12.6	909.4
+50			11.2	910.8
10			9.6	912.4

RR Track E. Rail

4			1.95	20.02
3			2.26	19.71
2			2.79	19.18
1			3.34	18.63
0			3.92	18.05
6			0.74	21.23
7			0.10	921.87
8				
9				
10				

Too High
Same Grade

BM 5,64916,59 11.02 910.95

FK
XP
DS
GA

Jan 8, 1973

Cold - 7°F

4

Top Hyd S.E. Cor Jackson + Demont.

Sta	+	π	-	Elev.
-----	---	-------	---	-------

		916.59		
--	--	--------	--	--

TP	7.55	915.79	8.35	908.24
----	------	--------	------	--------

TP	13.38	924.88	4.29	911.50
----	-------	--------	------	--------

TP	10.61	934.38	1.11	923.77
----	-------	--------	------	--------

			2.07	932.31
--	--	--	------	--------

				932.31
--	--	--	--	--------

FK
HP
DS
GA

Jan. 8, 1973
Cold -6°F

5

SPIKE IN PP 400' S LAKE ST.

SPIKE IN PP 200' S LAKE ST.

LOCK

TOP HYD. RT STA 10+09 JACKSON ST.

10	231
9 + 50	250
9	100
8 + 50	200
8	229
7 + 50	235
7	310
6 + 50	459
6	490
+ 50	560

Any Parking on S.E. Quadrant would obstruct Sight Distance.

SW Quad

0	95
1	106
2	132
+ 50	150
3	248
+ 50	326
4	493

FK
RP
DS
GA

West to East N. W. Quadrant
Jan 8, 1973 6

0 95

1 108

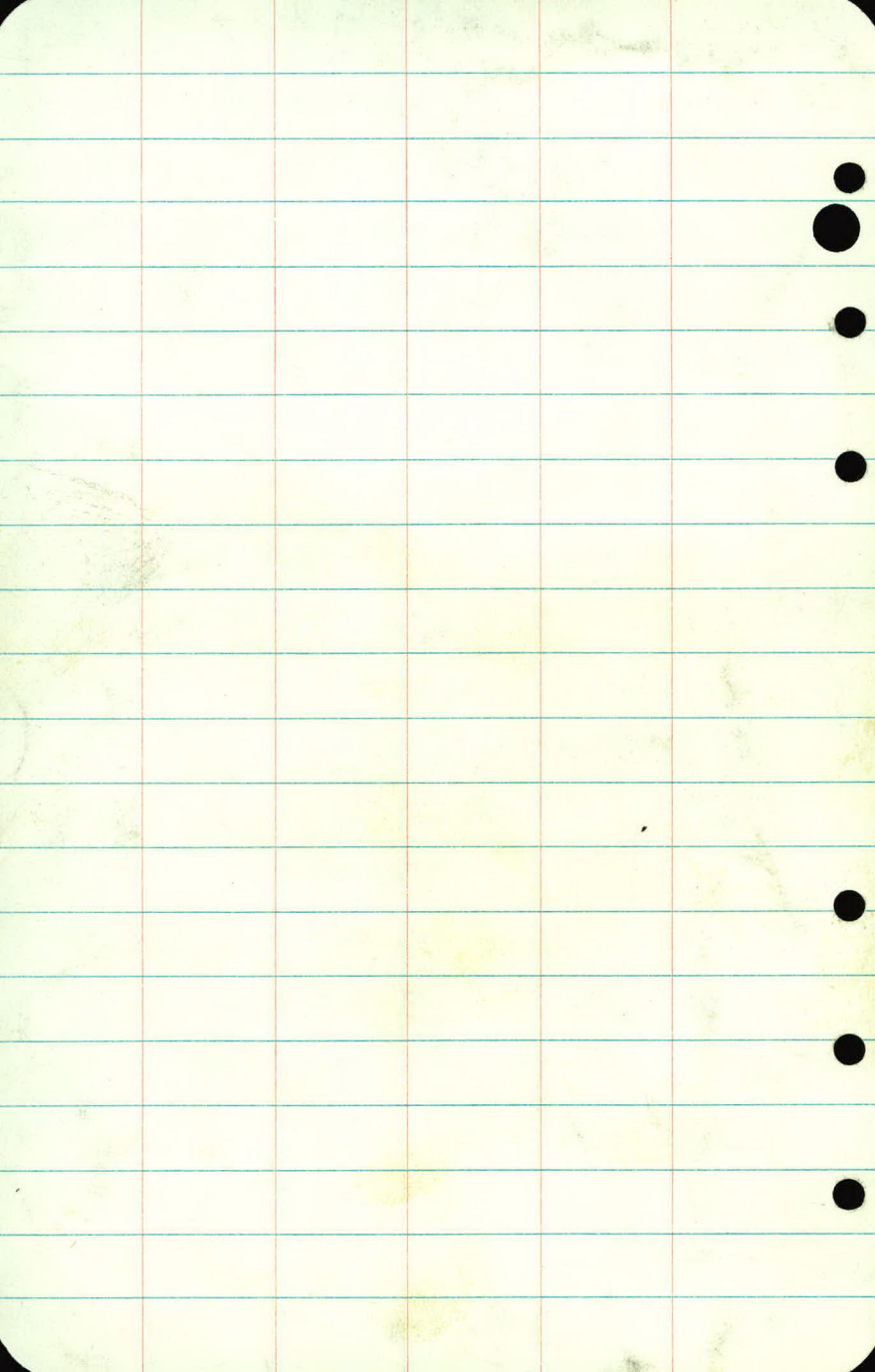
2 125

3 189

3450 300 to 323 only

4+50 325

4+75 550



KP
BF

23 MAY 1973 1.
SUNNY 50°

DEMONT ROAD

0+00 = 500' W OF RR TRACKS

£ TRACKS = 5+00

5+67 = £ JACKSON ST.

6+27 = £ ENT. RT

2+82 = £ ENT RT

0-177 = £ ENT. LT

10+43 = £ ENT LT.

PROFILE OF JACKSON. ST.

page 2

STA	+	T	-	ELEV.
BM	5.82	919.38		(913.56)
0+00			2.7	16.7
+50			4.8	14.6
1+00			6.9	12.5
+50			8.3	11.1
2+00			8.9	10.5
+50			9.0	10.4
3+00			8.9	10.5
BM			11.14	(908.24)
	6.38	919.94		(913.56)
			9.01	910.93 (910.95)

SPIKE IN PP N.E. COR DEMONT

£ DEMONT & JACKSON

SPIKE IN PP 400' S. LAKE ST ON JACKSON

SPIKE IN PP N.E. COR JACKSON & DEMONT

TOP HYD S.E. COR JACKSON & DEMONT

