

Dr. 12A - BK. 13

OFFICE OF COUNTY ENGINEER
RAMSEY CO. MINN.

_____ Plan _____ Survey

_____ HILL ST. _____

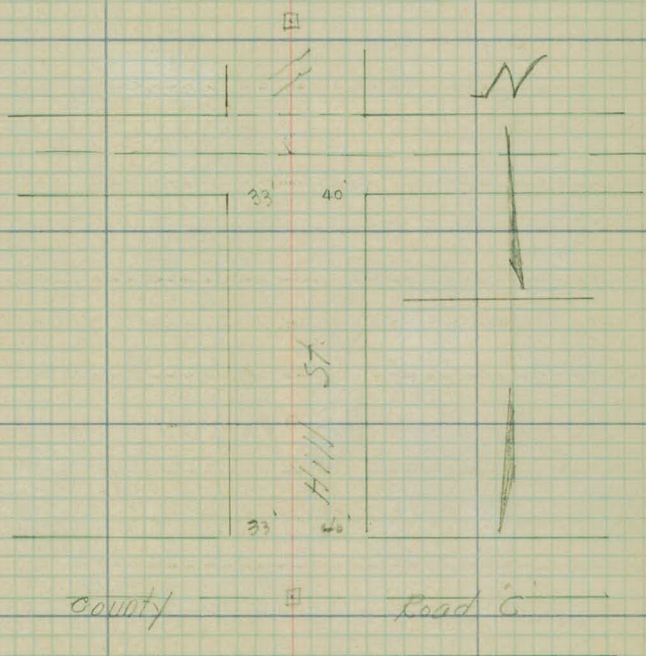
From Co. Rd. "C" To Kohlman Ave

Road Acc't. No. N21

Date Filed June 1936 File _____

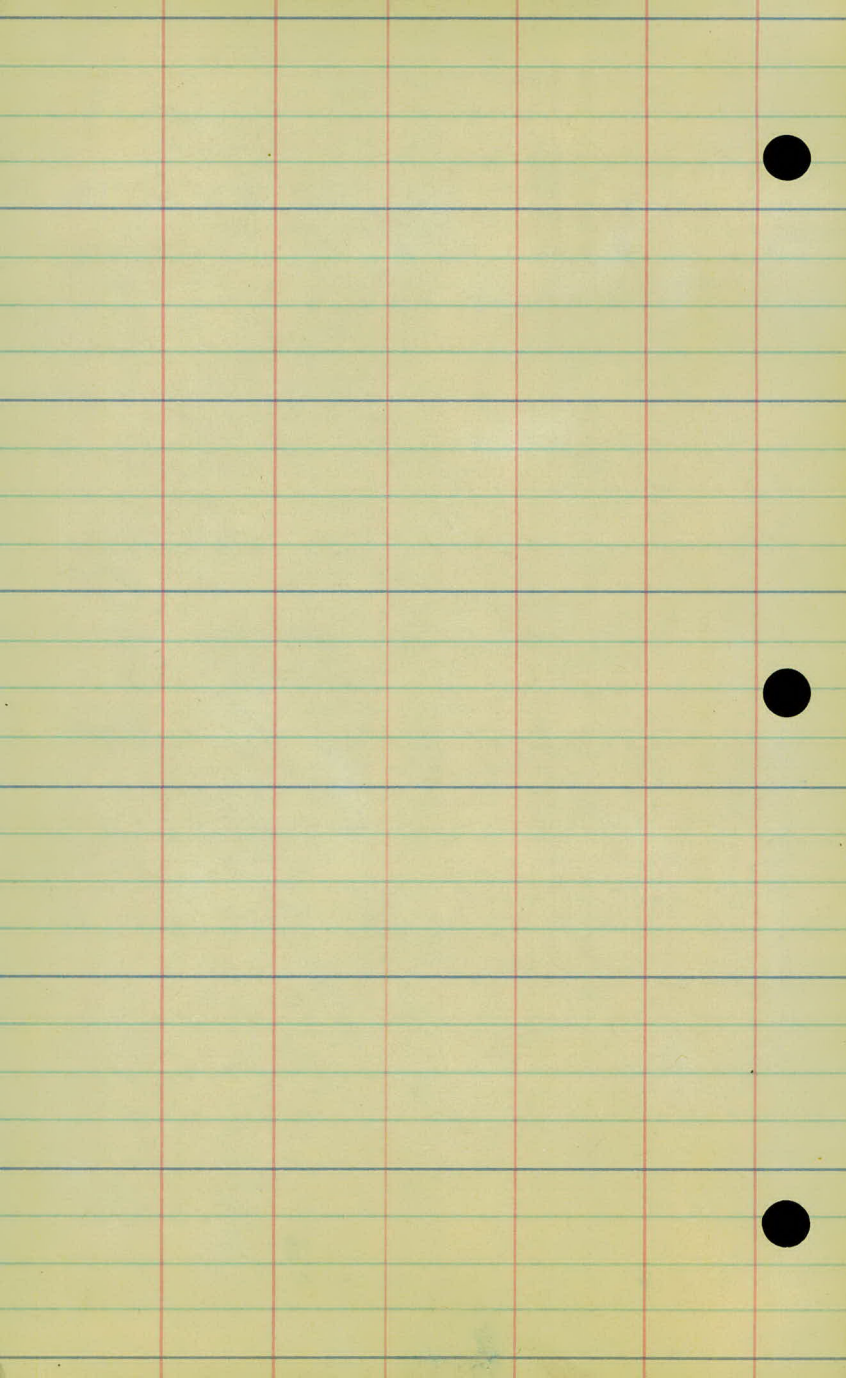
1

Plan Survey
Hill Street
County Road "C" to Kohlman Ave.



Index
alignment R. 1-3
Topography R. 4-5
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W. H. Carlson
7/6/36



alignement.

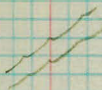
Sta.

Point

6+57.51 Boat Spike. $\pm$ Kohlman Ave.

0+00= Men $\pm$ Co. Rd "C"

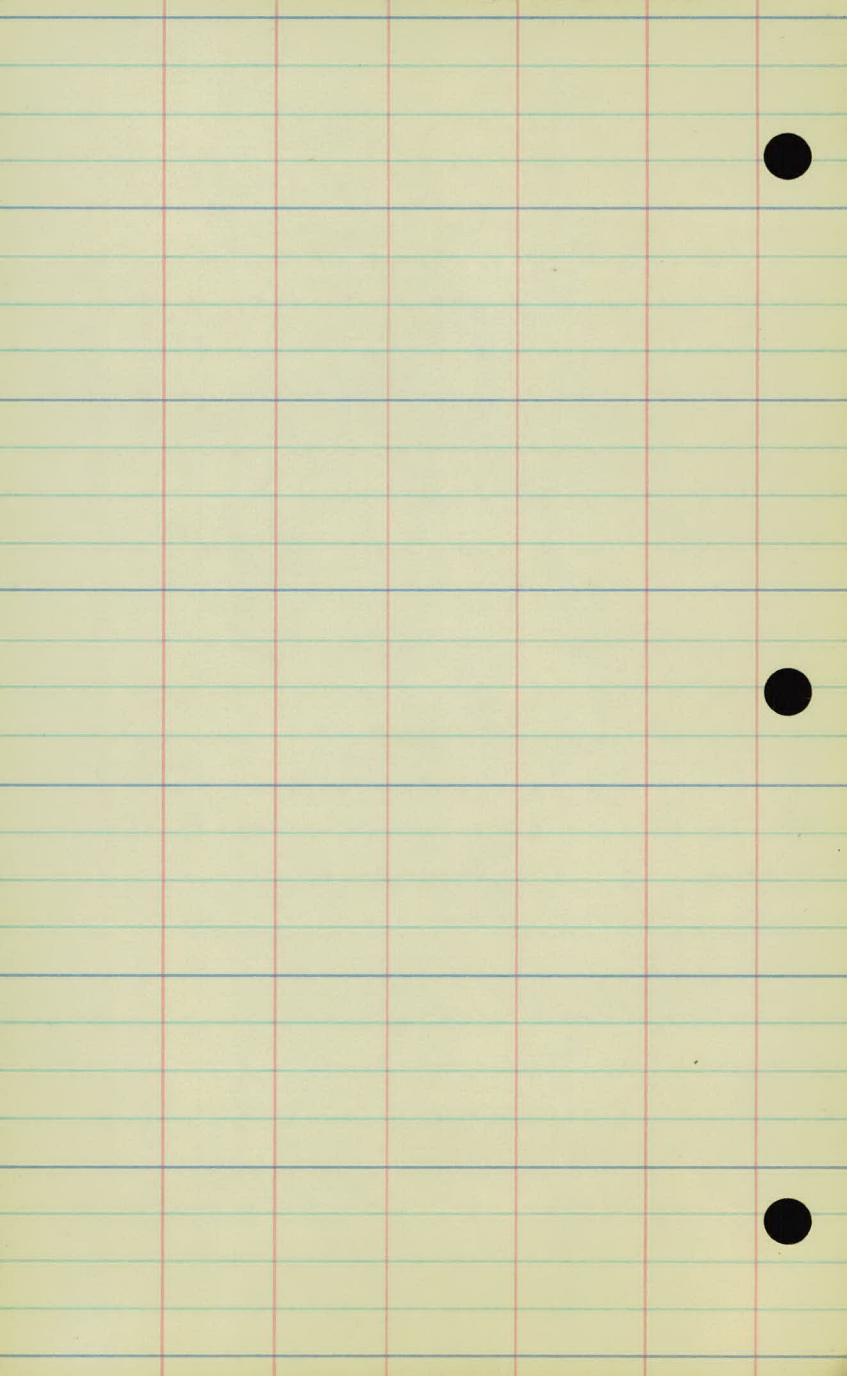
□



Santa Fe Ave.
Robinson Ave.

□

□



Topography.

6+57.51

6to

4-14'

5to

6-11'

4to 12'x24' C.M. 12-12'

4to

6-10

3to

6-10'

Gravel

2to

7-10

1to

6-10'

130 7-9'

1to d

12'x20' C.M. OK.

10+10'

cto

+39-A in Fence 21'
+34-A in Fence 17'

+05-RR 16'
F-16

+36-2" Poplar 17'
+36-Bag Fence 15'
+26-Ent. 12" X 6 C.M.

+06

+23-RR 15'
Cult. 15'

+50-Cult. 12'

Cult. 14'

+51-Pole 15'
No Wires

Cult. 16'

+15-F. Ent.
Pl. Cult. 10

+90-Pole 15'
No Wire

+70-RR 20'

Yard
Flowers

Corn Field

3 Wires

2 Wires

+83-5 3x4 36'

+59-S. W. cor. 30' 70'
+37-Ent.

Cult. 23'

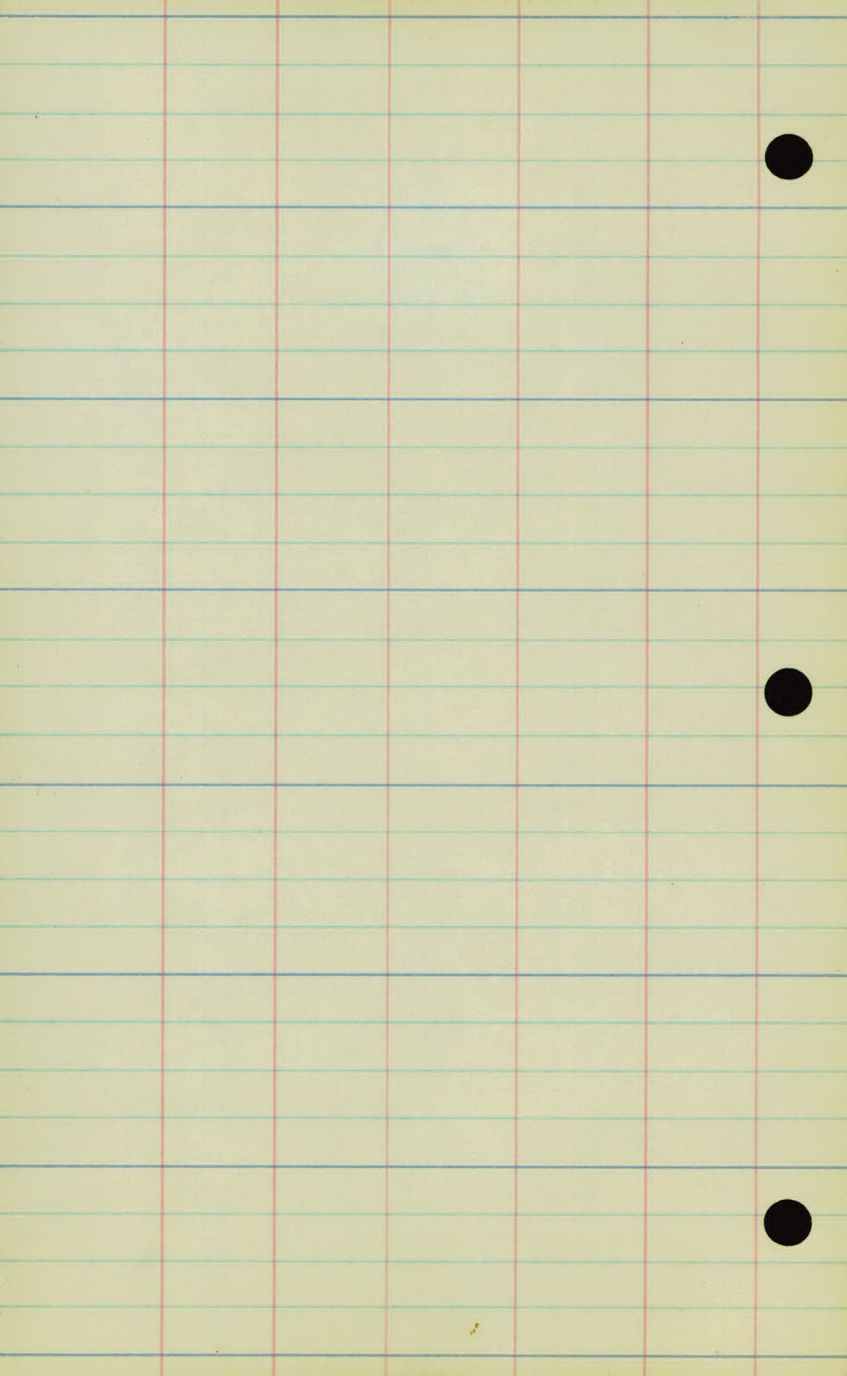
Cult.

Cult. 20'

Cult. 14'

Cult.

Cult. 17'



Cross Sections

Sta.	+	T ✓	-	Elev.
B.M.	11.05	903.86		892.81

0+0 = 1 Co Rd "C"				94.8
-------------------	--	--	--	------

0+17				94.8
------	--	--	--	------

0+22				94.6
------	--	--	--	------

0+35				94.8
------	--	--	--	------

+60				95.7
-----	--	--	--	------

1+0				97.3
-----	--	--	--	------

+50				98.7
-----	--	--	--	------

2+0				98.0
-----	--	--	--	------

+50				96.0
-----	--	--	--	------

3+0				93.8 ✓
-----	--	--	--	--------

T.P.	3.55	895.76 ✓	11.65	892.21
------	------	----------	-------	--------

+80				92.2
-----	--	--	--	------

Lt

E

Rt

7

Spike in P.P. So. Rt. Sta. 8495 - (Kohlman Ave.) W.N.C.

K.A.

7/6/36

L.B.H.

A.M.

$$\begin{array}{r} 9.1 \\ 50 \end{array}$$

$$\begin{array}{r} 9.1 \\ \hline \text{Total in} \end{array}$$

$$\begin{array}{r} 9.2 \\ 50 \end{array}$$

$$\begin{array}{r} 9.6 \\ 50 \end{array}$$

$$\begin{array}{r} 9.7 \\ 14 \end{array}$$

$$\begin{array}{r} 9.1 \\ \hline \end{array}$$

$$\begin{array}{r} 9.6 \\ 11 \end{array}$$

$$\begin{array}{r} 10.0 \\ 50 \end{array}$$

$$\begin{array}{r} 10.1 \\ 50 \end{array}$$

$$\begin{array}{r} 10.3 \\ 14 \end{array}$$

$$\begin{array}{r} 9.4 \\ 10 \end{array}$$

$$\begin{array}{r} 9.3 \\ \hline \end{array}$$

$$\begin{array}{r} 9.5 \\ 8 \end{array}$$

$$\begin{array}{r} 11.0 \\ 14 \end{array}$$

$$\begin{array}{r} 11.0 \\ 50 \end{array}$$

$$\begin{array}{r} 4.4 \\ 50 \end{array}$$

$$\begin{array}{r} 5.9 \\ 33 \end{array}$$

$$\begin{array}{r} 8.0 \\ 18 \end{array}$$

$$\begin{array}{r} 9.7 \\ 12 \end{array}$$

$$\begin{array}{r} 9.1 \\ 8 \end{array}$$

$$\begin{array}{r} 9.1 \\ \hline \end{array}$$

$$\begin{array}{r} 7.3 \\ 8 \end{array}$$

$$\begin{array}{r} 10.4 \\ 13 \end{array}$$

$$\begin{array}{r} 11.8 \\ 25 \end{array}$$

$$\begin{array}{r} 13.8 \\ 40 \end{array}$$

$$\begin{array}{r} 5.6 \\ 33 \end{array}$$

$$\begin{array}{r} 5.8 \\ 21 \end{array}$$

$$\begin{array}{r} 8.5 \\ 11 \end{array}$$

$$\begin{array}{r} 8.1 \\ 6 \end{array}$$

$$\begin{array}{r} 8.2 \\ \hline \end{array}$$

$$\begin{array}{r} 8.7 \\ 9 \end{array}$$

$$\begin{array}{r} 9.4 \\ 14 \end{array}$$

$$\begin{array}{r} 10.0 \\ 16 \end{array}$$

$$\begin{array}{r} 12.7 \\ 40 \end{array}$$

$$\begin{array}{r} 3.9 \\ 33 \end{array}$$

$$\begin{array}{r} 4.6 \\ 14 \end{array}$$

$$\begin{array}{r} 6.3 \\ 11 \end{array}$$

$$\begin{array}{r} 5.8 \\ 4 \end{array}$$

$$\begin{array}{r} 4.6 \\ 0 \end{array}$$

$$\begin{array}{r} 6.8 \\ 14 \end{array}$$

$$\begin{array}{r} 6.2 \\ 16 \end{array}$$

$$\begin{array}{r} 2.8 \\ 40 \end{array}$$

L.O

$$\begin{array}{r} 1.3 \\ 33 \end{array}$$

$$\begin{array}{r} 1.0 \\ 16 \end{array}$$

$$\begin{array}{r} 5.4 \\ 10 \end{array}$$

$$\begin{array}{r} 5.6 \\ 7 \end{array}$$

$$\begin{array}{r} 5.2 \\ \hline \end{array}$$

$$\begin{array}{r} 5.4 \\ 9 \end{array}$$

$$\begin{array}{r} 6.0 \\ 13 \end{array}$$

$$\begin{array}{r} 2.2 \\ 17 \end{array}$$

$$\begin{array}{r} 2.2 \\ 19 \end{array}$$

$$\begin{array}{r} 4.4 \\ 40 \end{array}$$

$$\begin{array}{r} 1.9 \\ 33 \end{array}$$

$$\begin{array}{r} 1.9 \\ 16 \end{array}$$

$$\begin{array}{r} 6.4 \\ 10 \end{array}$$

$$\begin{array}{r} 6.1 \\ 5 \end{array}$$

$$\begin{array}{r} 5.9 \\ \hline \end{array}$$

$$\begin{array}{r} 6.1 \\ 7 \end{array}$$

$$\begin{array}{r} 6.7 \\ 12 \end{array}$$

$$\begin{array}{r} 4.1 \\ 18 \end{array}$$

$$\begin{array}{r} 6.1 \\ 40 \end{array}$$

$$\begin{array}{r} 6.7 \\ 33 \end{array}$$

$$\begin{array}{r} 6.8 \\ 24 \end{array}$$

$$\begin{array}{r} 6.8 \\ 15 \end{array}$$

$$\begin{array}{r} 8.8 \\ 11 \end{array}$$

$$\begin{array}{r} 8.3 \\ 6 \end{array}$$

$$\begin{array}{r} 7.9 \\ \hline \end{array}$$

$$\begin{array}{r} 8.2 \\ 9 \end{array}$$

$$\begin{array}{r} 8.7 \\ 13 \end{array}$$

$$\begin{array}{r} 7.6 \\ 16 \end{array}$$

$$\begin{array}{r} 8.3 \\ 40 \end{array}$$

$$\begin{array}{r} 10.5 \\ 33 \end{array}$$

$$\begin{array}{r} 10.8 \\ 19 \end{array}$$

$$\begin{array}{r} 11.2 \\ 10 \end{array}$$

$$\begin{array}{r} 10.5 \\ 7 \end{array}$$

$$\begin{array}{r} 10.1 \\ \hline \end{array}$$

$$\begin{array}{r} 10.4 \\ 10 \end{array}$$

$$\begin{array}{r} 13.1 \\ 20 \end{array}$$

$$\begin{array}{r} 15.4 \\ 40 \end{array}$$

$$\begin{array}{r} 3.9 \\ 33 \end{array}$$

$$\begin{array}{r} 4.6 \\ 17 \end{array}$$

$$\begin{array}{r} 5.2 \\ 13 \end{array}$$

$$\begin{array}{r} 3.9 \\ 7 \end{array}$$

$$\begin{array}{r} 3.6 \\ \hline \end{array}$$

$$\begin{array}{r} 3.8 \\ 9 \end{array}$$

$$\begin{array}{r} 4.5 \\ 12 \end{array}$$

$$\begin{array}{r} 7.6 \\ 21 \end{array}$$

$$\begin{array}{r} 8.3 \\ 40 \end{array}$$

Sta.	+	π ✓	-	Elev.
		895.76		
440				91.2
+50				90.8
540				90.7
+50				90.9
640				91.3
+37				92.0
+57.51 = L. Kibbayan.				92.1
B.M.			2.95	✓ 892.81

4.

5

Rt.

8

$$\begin{array}{r} 65 \\ 33 \end{array} \quad \begin{array}{r} 68 \\ 17 \end{array} \quad \begin{array}{r} 72 \\ 13 \end{array} \quad \begin{array}{r} 48 \\ 7 \end{array}$$

$$\begin{array}{r} 4.6 \\ \hline \end{array}$$

$$\begin{array}{r} 5.1 \\ 9 \end{array}$$

$$\begin{array}{r} 5.5 \\ 12 \end{array}$$

$$\begin{array}{r} 8.3 \\ 18 \end{array}$$

$$\begin{array}{r} 8.6 \\ 22 \end{array}$$

$$\begin{array}{r} 8.9 \\ 40 \end{array}$$

12" X 24' CM 4+20

Drains Lt. - Pl. 24' CM.

$$\begin{array}{r} 6.7 \\ 33 \end{array}$$

$$\begin{array}{r} 7.1 \\ 18 \end{array}$$

$$\begin{array}{r} 8.0 \\ 15 \end{array}$$

$$\begin{array}{r} 7.3 \\ 14 \end{array}$$

$$\begin{array}{r} 5.6 \\ 9 \end{array}$$

$$\begin{array}{r} 5.9 \\ 6 \end{array}$$

$$\begin{array}{r} 5.0 \\ \hline \end{array}$$

$$\begin{array}{r} 5.3 \\ 11 \end{array}$$

$$\begin{array}{r} 8.3 \\ 19 \end{array}$$

$$\begin{array}{r} 8.4 \\ 40 \end{array}$$

$$\begin{array}{r} 5.8 \\ 33 \end{array}$$

$$\begin{array}{r} 6.6 \\ 18 \end{array}$$

$$\begin{array}{r} 6.9 \\ 14 \end{array}$$

$$\begin{array}{r} 5.7 \\ 9 \end{array}$$

$$\begin{array}{r} 5.2 \\ 6 \end{array}$$

$$\begin{array}{r} 5.1 \\ \hline \end{array}$$

$$\begin{array}{r} 5.3 \\ 11 \end{array}$$

$$\begin{array}{r} 6.8 \\ 15 \end{array}$$

$$\begin{array}{r} 7.3 \\ 19 \end{array}$$

$$\begin{array}{r} 7.0 \\ 25 \end{array}$$

$$\begin{array}{r} 7.0 \\ 40 \end{array}$$

$$\begin{array}{r} 4.3 \\ 33 \end{array}$$

$$\begin{array}{r} 5.2 \\ 13 \end{array}$$

$$\begin{array}{r} 6.0 \\ 11 \end{array}$$

$$\begin{array}{r} 5.3 \\ 8 \end{array}$$

$$\begin{array}{r} 4.9 \\ \hline \end{array}$$

$$\begin{array}{r} 5.3 \\ 14 \end{array}$$

$$\begin{array}{r} 6.0 \\ 16 \end{array}$$

$$\begin{array}{r} 6.2 \\ 21 \end{array}$$

$$\begin{array}{r} 5.7 \\ 26 \end{array}$$

$$\begin{array}{r} 5.8 \\ 40 \end{array}$$

$$\begin{array}{r} 4.0 \\ 33 \end{array}$$

$$\begin{array}{r} 4.7 \\ 14 \end{array}$$

$$\begin{array}{r} 5.5 \\ 12 \end{array}$$

$$\begin{array}{r} 4.5 \\ 7 \end{array}$$

$$\begin{array}{r} 4.5 \\ \hline \end{array}$$

$$\begin{array}{r} 4.9 \\ 14 \end{array}$$

$$\begin{array}{r} 5.8 \\ 20 \end{array}$$

$$\begin{array}{r} 6.0 \\ 28 \end{array}$$

$$\begin{array}{r} 6.3 \\ 40 \end{array}$$

$$\begin{array}{r} 3.2 \\ 33 \end{array}$$

$$\begin{array}{r} 3.9 \\ 20 \end{array}$$

$$\begin{array}{r} 4.4 \\ 15 \end{array}$$

$$\begin{array}{r} 3.8 \\ \hline \end{array}$$

$$\begin{array}{r} 4.2 \\ 10 \end{array}$$

$$\begin{array}{r} 5.3 \\ 25 \end{array}$$

$$\begin{array}{r} 5.8 \\ 40 \end{array}$$

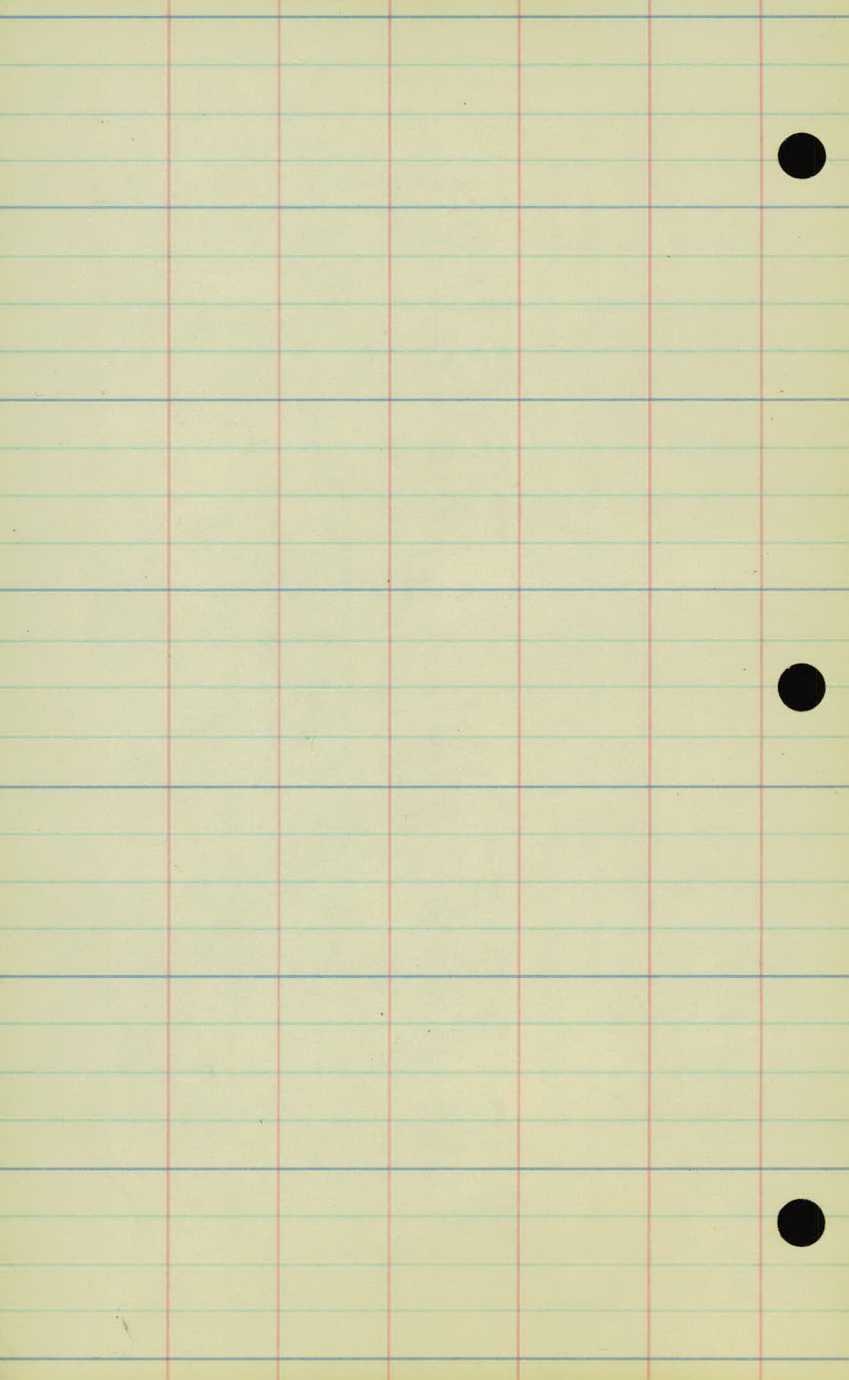
$$\begin{array}{r} 1.9 \\ 55 \end{array}$$

$$\begin{array}{r} 2.8 \\ 75 \end{array}$$

$$\begin{array}{r} 3.7 \\ \hline \end{array}$$

$$\begin{array}{r} 4.8 \\ 25 \end{array}$$

$$\begin{array}{r} 6.0 \\ 50 \end{array}$$



File Kohlman

8

892.81

Slope stakes.

Kohlman Ave.

Sta. to Sta.

Grade Lift.

Sta.	+	π	-	Elev.	Grade
B.M.	0.17	892.98		892.81	
10+0					
+50					
11+0					85.25
+50					84.18
12+0					83.4
	6.60	887.13	1245	880.53	
+50					82.96
13+0					82.85
+50					83.06
14+0					83.60
+50					84.48
15+0					85.65
T.P.	9.04	894.74	1.43	893.70	
15+30					87.16
16+0					89.0
			4.18	890.56	

Lt.

E

Rt.

W.H.G.

6/4/76

Spike in P.O. Kohlman & Hill St.

24' Road - Bed

2:1 Slope

Except fill over 4'

85.2

7.75

200/6.7
+1.07.8
-0.08.0
12.06.5/20.0
+1.3

8.8

20/9.5
12.0/12.0
12.8/9.2
-0.49.5
-0.710.0/14.4
-1.27.5/20.0
+1.3

9.58

200/8.6
-4.011.3
-1.711.8/14.4
-2.210.6/20.0
10.0

4.2

200/9.9
-5.76.5
-2.37.3/18.2
-3.1

4.28

200/9.9
-5.27.2
-2.97.9/19.2
-2.6

4.07

200/8.9
-4.88.0
-2.97.5/18.8
-2.4

3.53

200/8.0
-4.56.5
-2.06.6/18.2
-2.1

2.65

200/6.6
-4.05.6
-3.05.4/17.6
-2.8

1.48

18.0/4.5
-3.03.6
-2.13.6/16.2
-2.1

7.58

140/8.6
-1.08.1
-8.58.0/17.8
-0.47.7/20.0
-2.3

5.74

1.0 nail in Pole #12

5.3

10.4

5.3/12

10.4

4.9/20.0

10.8

Sta.

+

π

-

Elev

Grade

Kohlman Ave.

93.0
7.8
85.2

92.0
11.3
81.7

92.81

.17

892.98

12.45

880.53

6.60

887.13

1.43

885.70

5.1 9.04

78894.74

85 41.18

890.56

93.0

85.25

7.75

87.13

82.96

4.17

87.13

83.6

3.53

94.74

87.16

7.58

92.98

84.18

8.8

87.13

82.85

4.28

87.13

84.48

2.65

94.74

84.

92.98

83.4

9.58

81

4.3

3.8

87.13

85.65

1.48

94.7

87.13

83.06

4.07

7.4
4.1

53
2.8
.7

66

74
4.7

76

126
9.6

11.3
9.6
7

120
9.6
118
9.6

9.8 09.85

3.8

10+0	88.4	+0.0	88.4
+50	86.5	+0.16	86.66
11+00	84.6	+0.65	85.25
+50	82.7	+1.48	84.18
12+0	80.8	+2.60	83.4
12+80	78.9	+4.06	82.96
13	77.0	+5.85	82.85
+50	79.0	+4.06	83.06
14	81.0	+2.60	83.60
+50	83.0	+1.48	84.48
15	85.0	+0.65	85.65
+50	87.0	+0.16	87.16
16	89.0	+0.0	89.0

4/15/

Blue tops.

STA.	+	π	-	ELEV.	GRADE
------	---	-------	---	-------	-------

B.M.	4.36	895.00		890.64	
------	------	--------	--	--------	--

	6.92	898.72	-3.20	891.80	
--	------	--------	-------	--------	--

B.M.	7.24	902.54	-3.42	895.30	
------	------	--------	-------	--------	--

+35					895.3
-----	--	--	--	--	-------

+60					96.1
-----	--	--	--	--	------

1+00					97.1
------	--	--	--	--	------

+50					97.4
-----	--	--	--	--	------

2+00					97.1
------	--	--	--	--	------

+50					95.8
-----	--	--	--	--	------

3+00					94.0
------	--	--	--	--	------

+50					92.4
-----	--	--	--	--	------

4+00					91.3
------	--	--	--	--	------

	4.78	896.14	11.18	891.36	
--	------	--------	-------	--------	--

+50					90.6
-----	--	--	--	--	------

5+00					90.3
------	--	--	--	--	------

@ School Ho.

R.R. Spike in P.P.

S.W. of Hill St & Co Rd C.

5.4

4.9 6.9

5.4

6.7 - 8.7

8.5

10.5

10.1

11.2

5.5

5.8

STA

+

K

-

Elev.

GRADE

896.41

+50

90.5

6+00

91.2

B.M.

3.33

892.81

4.6

52
10.27

4.9

4.2

3.2

3.6

4.0

4.5

4.2

4.9

4.9

Kohlman Ave gutter

13.16 883.35

870.19

12.5

70.9

0+50

1+0

1+50

1+92.59

2+0

0.7

T.P

13.06 896.29

0.12

883.23

2+50

9.9

+75

3+0

3+25

3+50

2.0

T.P

11.70

907.25

0.74

895.55

4+00

4+25

Aug. 18, 1936

Gutter 9.20
 Grade
 Plan -
 87.2 12.15
 12.60 = Due to High. Exc.

873.7 9.65

877.3 6.05

80.7 2.65 ✓

81.3 2.05

85.3 10.99

87.3 9.00

740

88.2 8.1

Grade 9.20

91.3 5.0

90.3 6.0

93.3 3.0

93.3 3.0

97.3 10.0

97.3 10.0

99.3 8.3
 146

99.3 8.3
 146

907.25

4150

T.P.

5.51

910.77

1.99

905.26

4198 - Rt. - (End)

Stro - Lt.

5.3

905.5

stro - Lt. end

9.4.11
9.4.11 9.4.11

9013 6.0

904.3 6.5

904.3 6.5

904.8 6.0

6.8

