

Book - 1, Dr. 12-A

OFFICE OF COUNTY ENGINEER
RAMSEY CO. MINN.
PLAN Survey

DE SOTO ST.

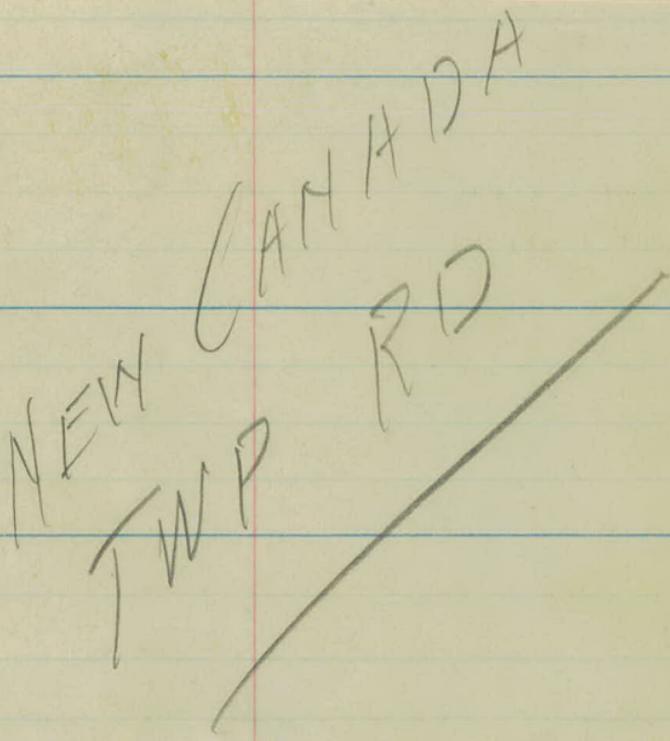
From St. Paul City Limits To Co. Rd A2

Road Acc't. No. N5

Date Filed 11-8-29 File NC. Twp.

700 207
15 98 58
10 98

ALIGNMENT FROM STA 0+00
TO STA 26+64.



STA POINT Δ LT Δ RT

STA	POINT	Δ LT	Δ RT
8+12	P.T.	7°-34'	
8100		7°-04"	
750		5°-04"	
7+18	P.I.		A-15°08'
7700		3°-04"	D-8°R
750		1°-04"	T-95 ²²
6+23	P.C.	0°-00	L-189 ¹¹
			R-716 ⁷⁸

5+84⁹ P.O.T.

5+72⁸ P.O.T

0+00

2×2 " HOB.

H HOB.

2×2 " HOB.

H HOB.

H HOB.

$93^{\circ}-29'$

150.5 ft

THREE NAILS
IN BRIDGE.

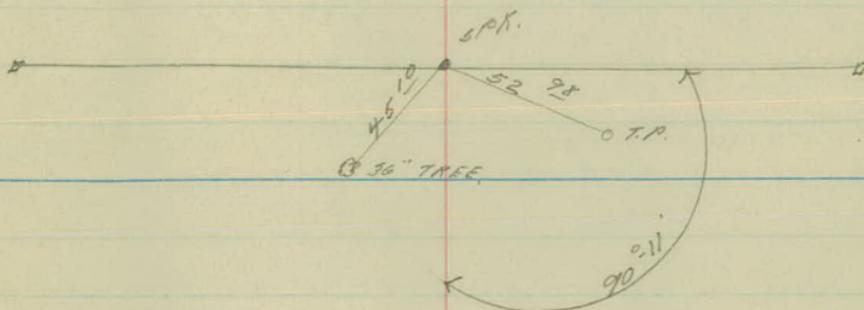
STA POINT ALT A RT

26+64³ P.O.T.

17+71 ²¹	P.T.	$0^{\circ} - 58^{\circ}$	
1800		$0^{\circ} - 52^{\circ}$	
17400		$0^{\circ} - 37^{\circ}$	
16+74 ³	P.I.		$\Delta - 1^{\circ} 57'$
1800		$0^{\circ} - 22^{\circ}$	$P - 1^{\circ} R$
16400		$0^{\circ} - 07^{\circ}$	$T - 97^{\circ} 49'$
15+76 ²¹	P.O.	$0^{\circ} - 00^{\circ}$	$L - 195^{\circ} 00'$
			R

13+47²⁵ P.O.T.

6-8-29

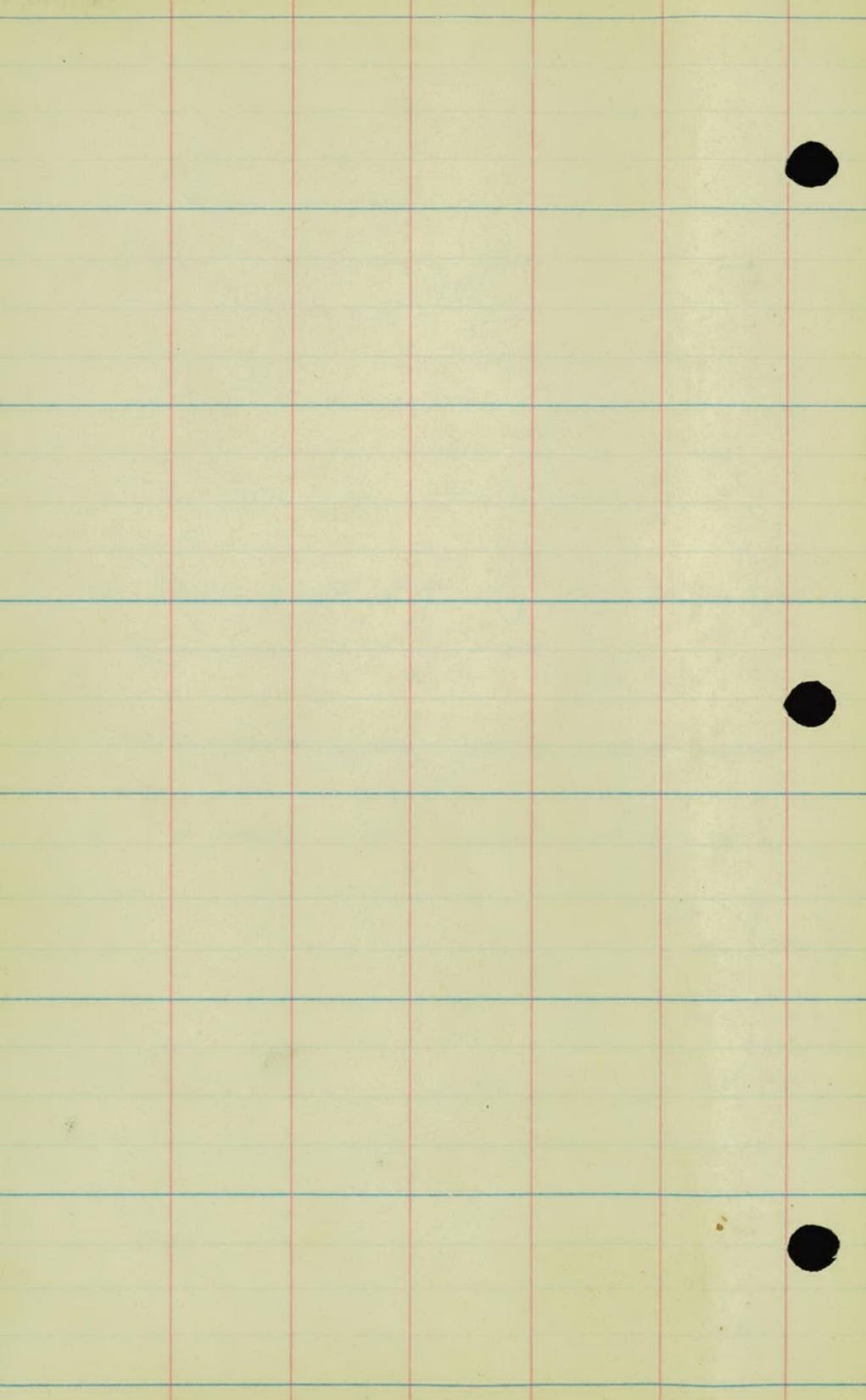


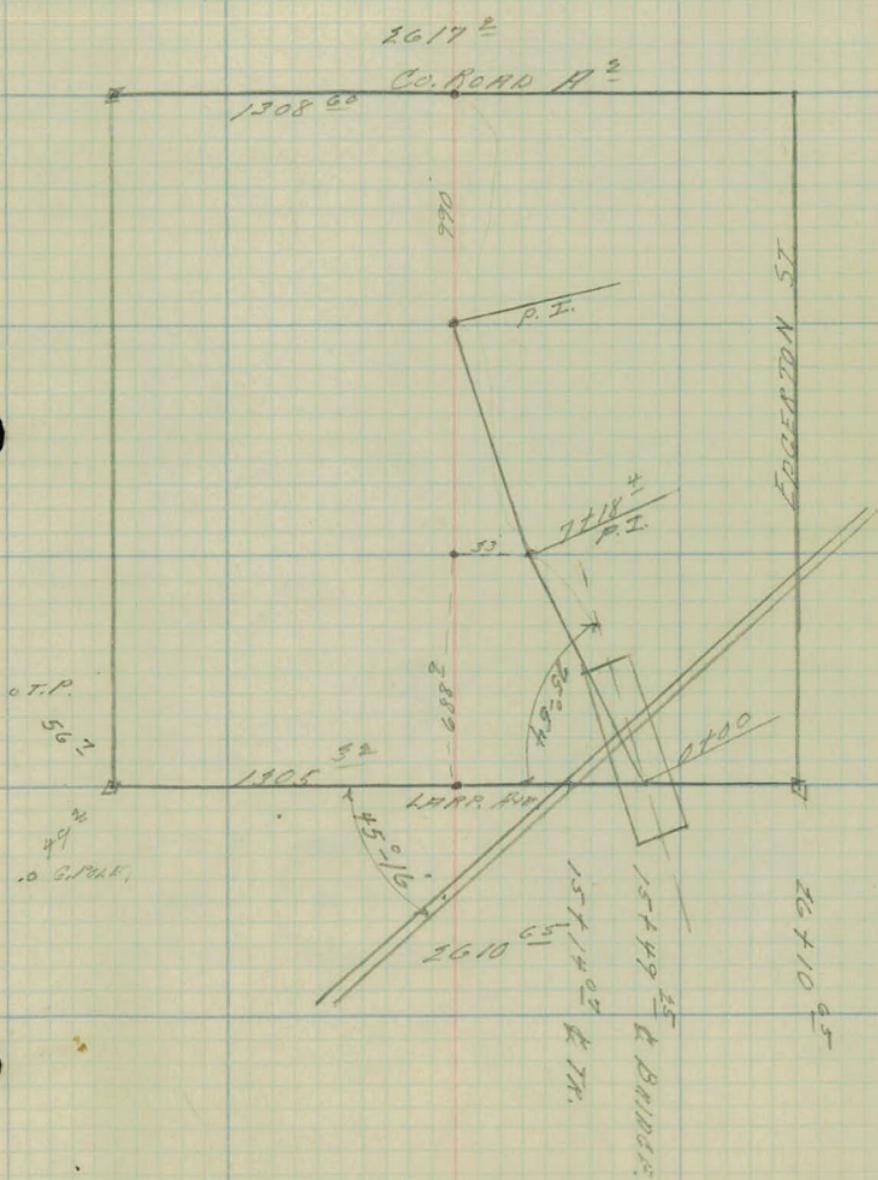
A HUB.

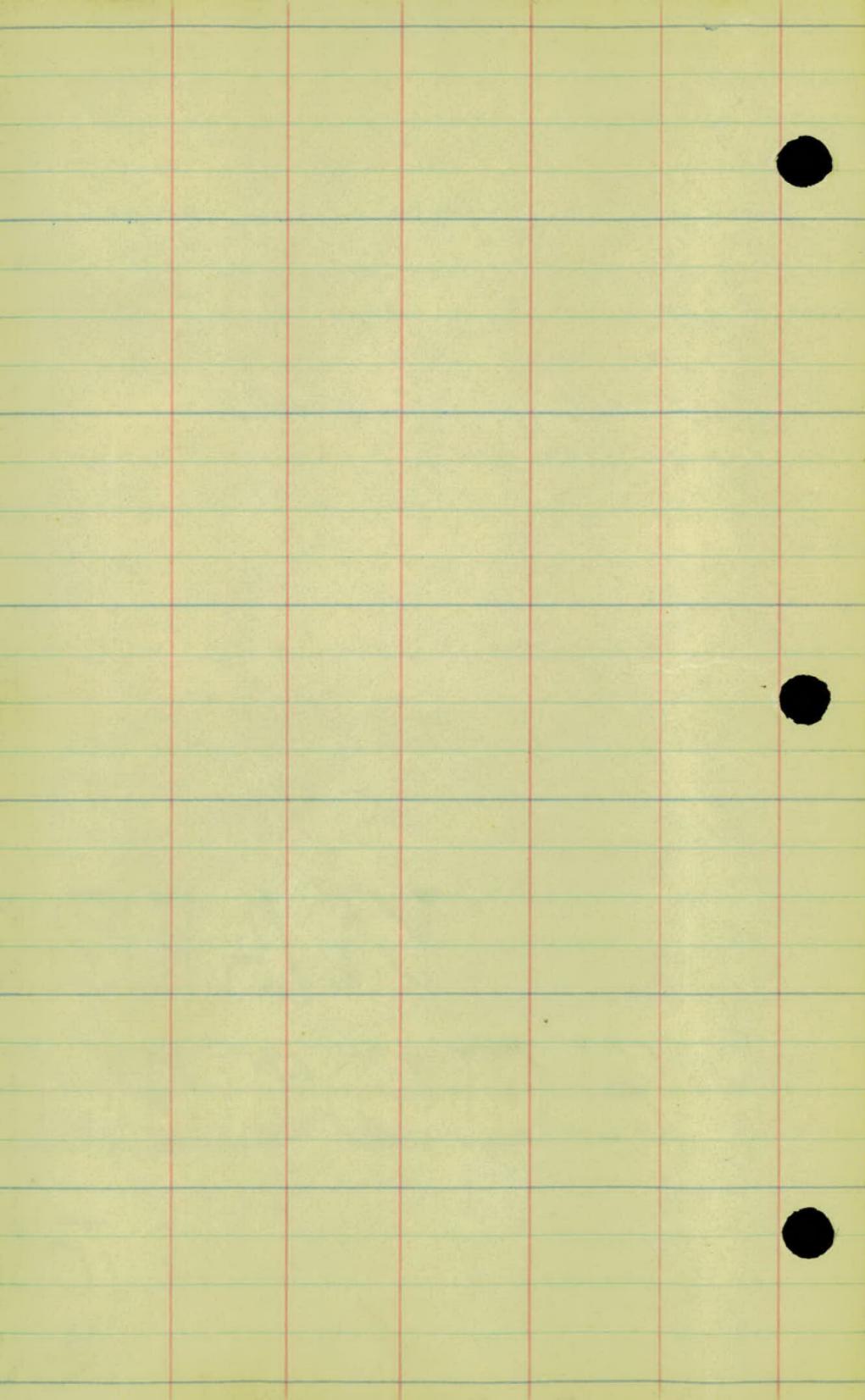
HUB.

A HUB.

A HUB.







ART TOPOG.

2700

+50

1700

69
60
154

+50

0700

-50

6-8-29

F. 7
F. 31
P. ROAD 14

F. 64
F. 7
P. ROAD 9

F. 3

PARTURE

HOG. P. 24
F. 7

0-75 F. 11

0-61 F. 16

0-67 PRIMOC. Ø.

0-65 7 RAD. Ø. 6²

750 F. CIR. 39.5

0-11 BRIDGE Ø.
0-16 RAD. Ø. 10²

118 F. CIR. 24
Ø RAD. 5'
100 P.P. 17

0-75² BRIDGE 12²

0-06² BRIDGE 9

8

7

6

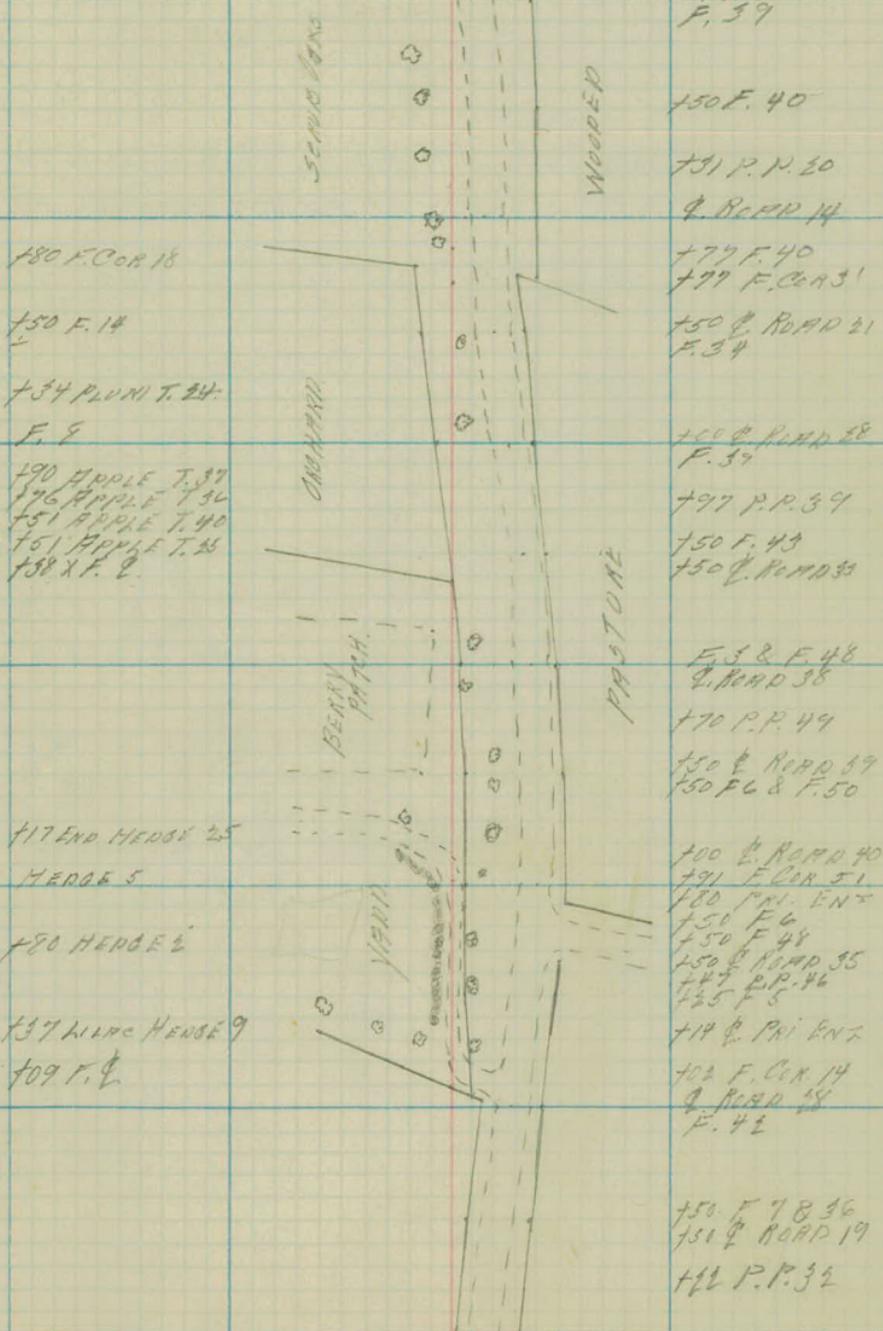
5

4

3

2

6-11-29



14

13

12

11

10

9

8

6-11-27

CROCHERO

Φ ROMD 9
F. 27

CULTIVATED

BERRY / 27004

+47 F. 31⁵
+47 P.P. 19

Φ ROMD 6

+44 P.P. 15

CULTIVATED

YANOS

Φ ROMD

+79 PRI ENT

F. 22

106 F.COR 29

CULTIVATED

WOODS

SHL & H.

WOODED PASTURE

+94 F. 41
+74 F. 28
+50 Φ. ROMD 12

+94 F. 28 & 35
+87 P.P. 28

Φ ROMD 9
F 31

+05 P.P. 30

20

19

18

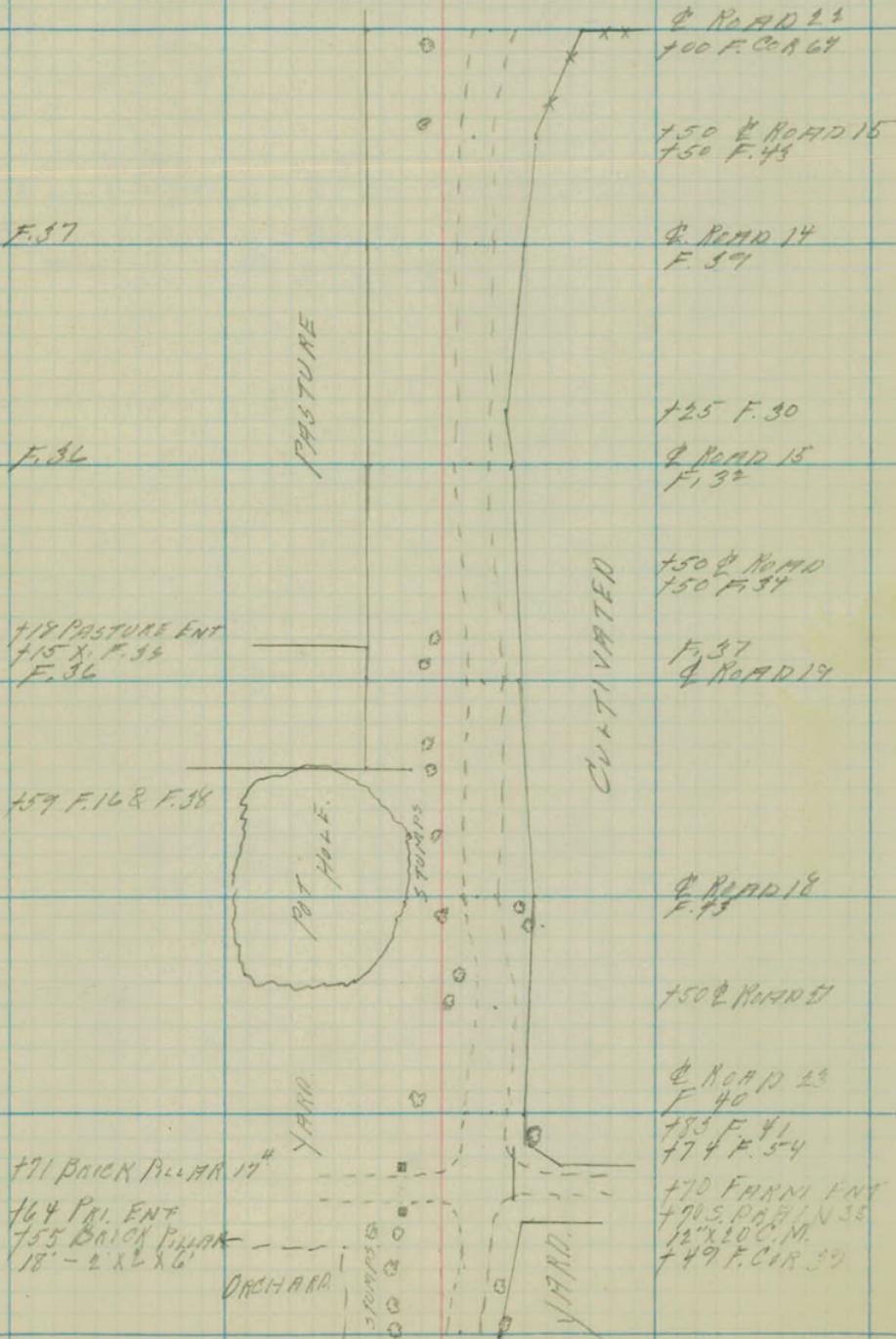
17

16

15

14

6-11-27



26

25

24

23

22

21

20

6-11-29

+784 FARM RAIL 13
+776 G MARCH 17
+794 G APRIL 24
+47 F.CORN 18

700 E 110 19
739 F 4

150 G ROAD 56
130 F 16

113 F. 30

700 G ROAD 56
+60 HIGE F. 38
756 FARM END
+53 S. DRAIN
12" X 20' C.M. 62
150 G ROAD 47
130 X F.
135 F 67
130 F. 40

F 76
2 RD 100

150 G ROAD 105
150 F 85

F. 29
2 RD 115

+24 EDGE OF FONDO

PONP.

PASTURE

F 52
G ROAD 84

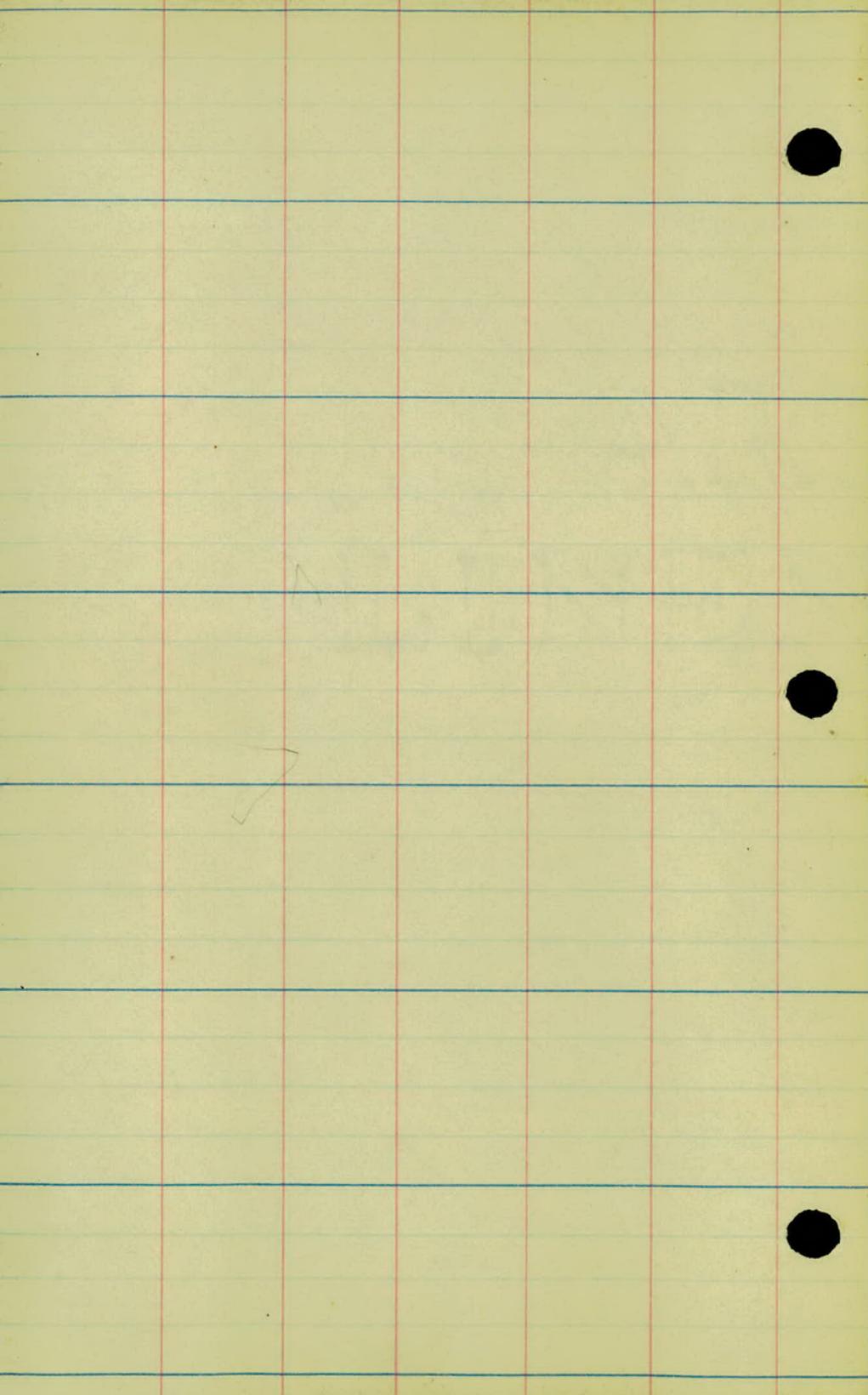
160 G ROAD 68
160 F 41

G ROAD 41
F. 30

135 F. 4

108 F. 6 & 38

151 G ROAD 28



13400

12400

12492 HOUSE 55³/8.

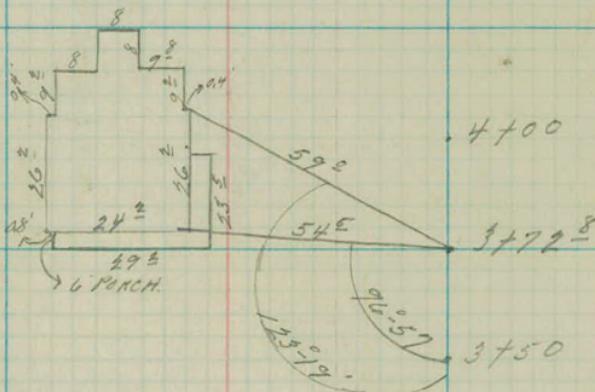


2- STORY BRICK
HOUSE.

12,407 HOUSE 54³/8.

24

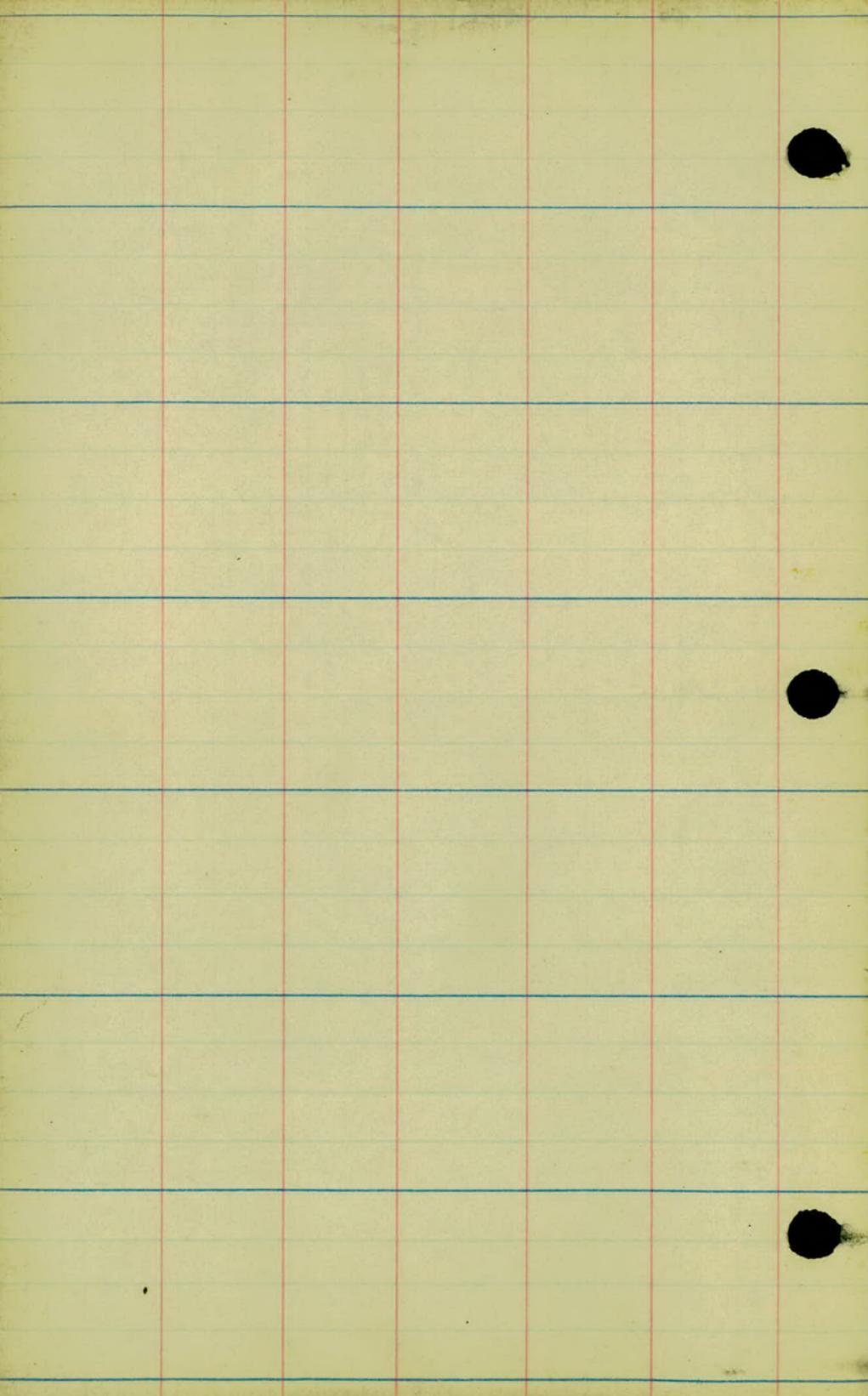
1 1/2 STORY
FRAME HOUSE.



4700

3472 8

3450



CHECK LEVELS

B.N.	3.18	914.38	911.20	
	4.55	913.19	5.74	908.64
B.N.			4.48	908.71
	4.39	916.76	0.82	912.37
	4.61	910.79	10.58	906.18 ✓
	4.30	904.40	10.69	900.10
B.N.			1.57	902.83 ✓
	8.44	879.36	13.48	870.92
	9.11	906.15	2.32	877.04 ✓
B.N.			3.02	903.13
	4.62	910.11	0.66	905.49
	2.85	903.41	9.55	900.56
	0.29	899.16	4.54	898.87
	12.30			886.86

7-12-29

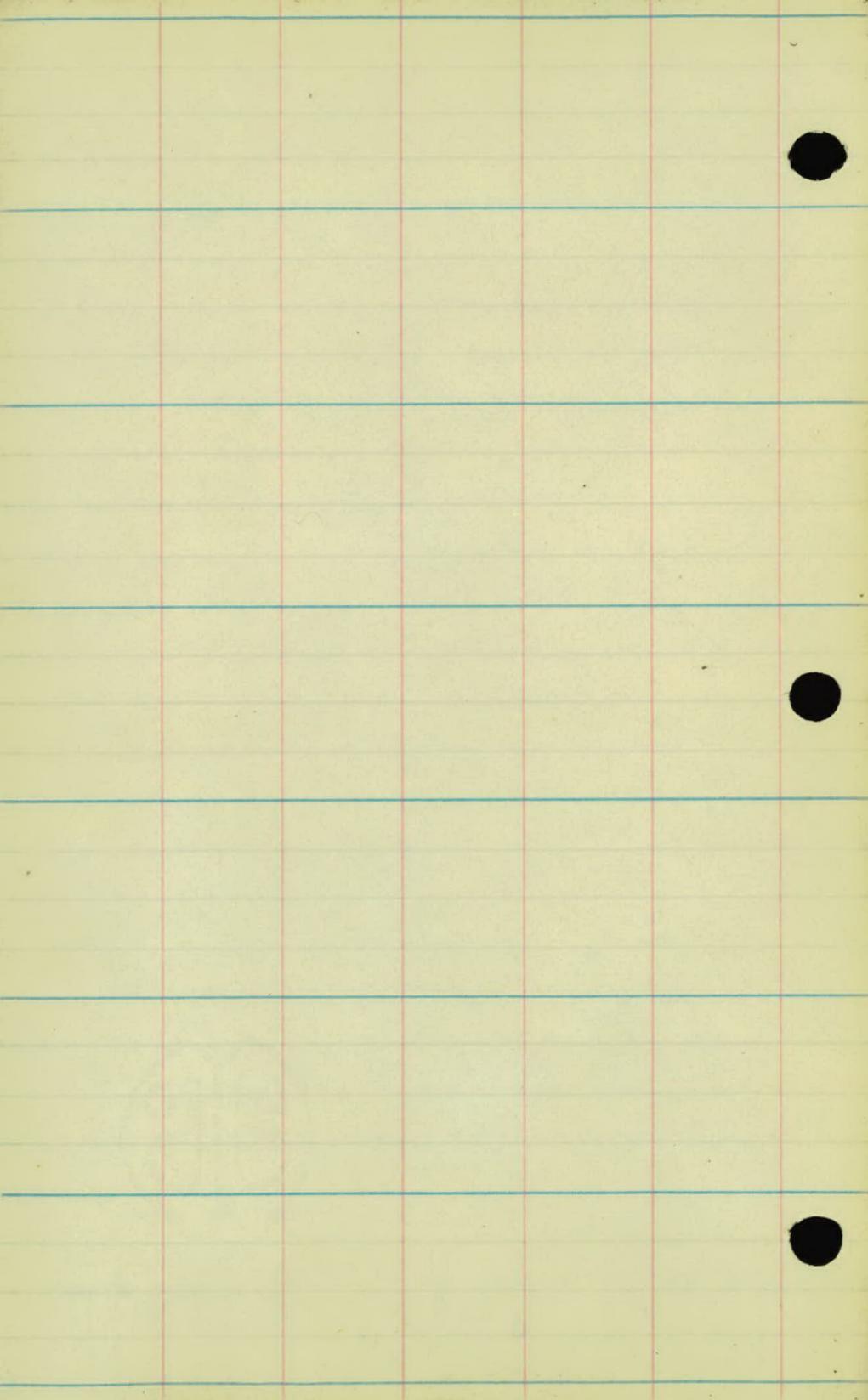
NAIL IN T.P. A 171 IN FRONT OF MC NEMEMY GRAYEL P.T.

SPK IN P.P. SW COR OF INT COLORADA R² & MC NEMEMY 39

SPK IN 24" OAK 50 RT STA 26705

SPK IN 24" OAK 40 RT STA 14185

SPK. IN CAP ON BRIDGE LT STA. 0+65



X SECTIONS.

B.M.	12.30	899.16	✓	886.86	
0-11	END OF BRIDGE			10.93	88.23
0+00				2.66	89.90
0+19				7.25	91.91
0+39				7.15	92.01
0+69				1	88.78
0+85					88.4
1+00					88.6
1+50					88.7
2+00					91.2
2+50			✓		96.8
	12.58	911.44	0.30	898.86	✓
3+00					900.4
3+50					05.7
4+00					09.7
4+50			✓		08.7
5+00	12.44	912.44	11.44	900.00	✓
					09.7

15.4 15.4 15.9 15.9 13.6 11.4 10.6 9.80 ^{7 ERASE OF PRACTICE} 17.6
40 35 21 21 13 7 4 10.38 12 12
31

19.8 15.6 13.2 11.0 10.7 10.8 12.5 14.3 13.1
40 30 10 4 10.8 9 20 34 28 40

20.0 14.7 13.4 14.9 10.8 10.6 10.8 11.0 12.2 13.1
40 26 18 14 3 10.6 9 18 26 37 40

17.5 14.0 11.9 11.5 10.8 10.0 9.8 10.0 8.4 8.3 9.0
40 25 15 11 5 10.5 2 13 19 21 27 40

17.4 14.4 10.6 2.0 8.0 8.3 8.1 7.4 4.0 2.7 2.7
40 29 14 6 8.0 8 15 19 23 32 32 40

8.6 7.7 5.3 6.4 3.7 4.1 5.0 4.8 1.0 0.0
40 32 14 24 4 9 11 18 27 35 40
4.0
2.7

9.6 10.0 10.5 11.6 10.5 11.5 13.4 14.0 13.4 12.7
40 31 14 11.0 4 10 14 22 33 35 40

0.6 2.3 4.1 4.6 5.6 6.6 7.3 12.4 12.9
40 23 9 6 4 5.7 7 14 24 40

12.7 11.0 0.0 0.6 1.2 2.2 2.9 3.6 11.5 12.0
40 21 10 5 4 1.7 6 7 17 31 40

14.1 10.3 0.2 0.7 4.9 11.1 11.7 11.5
40 18 13 9 27 17 28 38 40

15.5 13.8 + 8.0 0.3 1.5 3.9 5.2 6.3 9.0 14.4 14.0
50 25 20 10 6 27 5 11 14 17 26 40

	✓	912.44	
5+50			09.4
6+00			08.0
6+50			✓ 05.0
	2.34	✓ 703.07	11.71 900.93
7+00			99.6
7+50			✓ 98.1
	6.48	✓ 904.71	4.64 898.43
8+00			98.3
8+50			99.4
9+00			00.4
9+50			02.7
10+00			✓ 02.6
	0.19	✓ 70775	3.35 901.56
10+50			00.9
11+00			01.0
11+50			01.8

$$\begin{array}{r} +4.5 +3.0 .05 2.5 \\ 4.0 \quad 21 \quad 13 \quad 5 \quad 3.0 \end{array} \begin{array}{r} 5.0 12.8 14.7 14.3 14.4 \\ 6 \quad 19 \quad 23 \quad 32 \quad 40 \end{array}$$

$$\frac{15.7}{40}$$

$$\begin{array}{r} +6.0 +3.0 .07 2.4 3.5 \\ 3.0 \quad 28 \quad 14 \quad 8 \quad 3 \end{array} \begin{array}{r} 5.5 13.3 14.9 14.4 14.3 14.7 \\ 2 \quad 14 \quad 15 \quad 25 \quad 30 \quad 32 \end{array}$$

$$\begin{array}{r} +4.5 0.0 1.9 2.3 3.5 4.7 \\ 4.0 \quad 25 \quad 18 \quad 14 \quad 10 \quad 5 \end{array} \begin{array}{r} 14.4 13.8 13.4 13.8 18.8 \\ 7.4 \quad 10 \quad 18 \quad 24 \quad 32 \end{array} \frac{40}{40}$$

$$\begin{array}{r} +10.3 +7.6 +4.7 \\ 4.0 \quad 27 \quad 17 \end{array} \begin{array}{r} 5.7 5.1 4.6 4.9 5.5 7.6 14.0 \\ 3.5 \quad 4 \quad 6 \quad 12 \quad 17 \quad 25 \quad 28 \end{array} \frac{40}{40}$$

$$\begin{array}{r} +5.0 7.7 0.3 2.3 4.8 6.0 \\ 4.0 \quad 26 \quad 17 \quad 12 \quad 7 \quad 5 \end{array} \begin{array}{r} 4.9 5.6 8.5 10.4 12.4 14.0 \\ 5.0 \quad 8.1 \quad 16 \quad 21 \quad 24 \quad 30 \end{array} \frac{40}{40}$$

$$\begin{array}{r} +6.4 +5.9 0.3 6.4 \\ 4.0 \quad 24 \quad 12 \quad 4 \end{array} \begin{array}{r} 7.1 11.7 13.9 \\ 6.6 \quad 18 \quad 32 \end{array} \frac{40}{40}$$

$$\begin{array}{r} +8.2 +4.5 +1.6 4.9 \\ 4.0 \quad 23 \quad 12 \quad 3 \end{array} \begin{array}{r} 5.5 6.3 10.6 12.0 \\ 5.5 \quad 32 \quad 34 \quad 40 \end{array}$$

$$\begin{array}{r} +4.7 +1.7 +0.5 0.2 4.4 \\ 4.0 \quad 18 \quad 12 \quad 9 \quad 3 \end{array} \begin{array}{r} 4.8 7.5 9.8 \\ 4.5 \quad 20 \quad 26 \end{array} \frac{40}{40}$$

$$\begin{array}{r} +4.1 12.2 +2.6 +2.2 4.0.6 2.0 \\ 4.0 \quad 53 \quad 28 \quad 21 \quad 6 \quad 2 \quad 2.2 \end{array} \begin{array}{r} 3.0 3.4 2.5 3.2 6.1 \\ 1 \quad 19 \quad 20 \quad 27 \end{array} \frac{40}{40}$$

$$\begin{array}{r} +0.9 1.3 \\ 4.0 \quad 13 \end{array} \begin{array}{r} 3.3 3.5 2.5 1.9 2.0 0.9 \\ 2.3 \quad 2 \quad 19 \quad 20 \quad 27 \end{array} \frac{40}{40}$$

$$\begin{array}{r} 11.5 11.5 11.4 11.1 2.5 \\ 4.0 \quad 59 \quad 19 \quad 10 \quad 2 \end{array} \begin{array}{r} 6.7 6.7 6.5 5.6 4.3 4.8 \\ 6.9 \quad 5 \quad 20 \quad 23 \end{array} \frac{40}{40}$$

$$\begin{array}{r} 10.4 10.8 10.9 8.4 7.3 \\ 4.0 \quad 26 \quad 18 \quad 12 \quad 5 \end{array} \begin{array}{r} 6.9 8.5 8.9 \\ 6.8 \quad 15 \quad 26 \end{array} \frac{50}{50}$$

$$\begin{array}{r} 5.0 2.7 1.7 3.0 0.0 \\ 4.0 \quad 27 \quad 21 \quad 13 \quad 7 \end{array} \begin{array}{r} 6.0 7.6 8.0 8.2 \\ 6.0 \quad 12 \quad 18 \quad 20 \end{array} \frac{40}{40}$$

	907.75		
12+00			04.1
	6.67	913.68	0.74
12+50		907.01	07.0
13+00			09.0
13+46			09.2
13+58			09.1
14+00			00.6
14+50			01.2
B.M.	2.92	906.05	11.59
		903.09	903.13
15+00			98.8
15+50			97.4
16+00			97.8
16+50			96.9
17+00			97.4
17+50			98.0

$$\frac{+60}{40} \frac{+64}{69} \frac{+21}{16} \frac{52}{8} \frac{57}{37} \frac{27}{7} \frac{25}{12} \frac{25}{40}$$

$$\frac{0.0}{40} \frac{0.9}{23} \frac{0.0}{18} \frac{5.9}{7} \frac{6.5}{4.7} \frac{1.8}{9} \frac{1.6}{15} \frac{1.6}{40}$$

$$\frac{0.5}{40} \frac{0.3}{19} \frac{+0.2}{12} \frac{4.1}{5} \frac{4.5}{4.7} \frac{2.4}{8} \frac{0.8}{10} \frac{+0.3}{15} \frac{0.3}{50} \frac{0.3}{40}$$

$$\frac{5.1}{40} \frac{4.8}{29} \frac{3.3}{33} \frac{2.8}{16} \frac{2.1}{9} \frac{4.1}{5} \frac{4.2}{4.5} \frac{0.7}{10} \frac{+0.9}{15} \frac{+1.0}{27} \frac{1.0}{40}$$

$$\frac{2.8}{40} \frac{5.0}{26} \frac{3.4}{8} \frac{2.4}{6} \frac{4.5}{4.6} \frac{4.5}{12} \frac{3.4}{23} \frac{5.2}{40}$$

$$\frac{10.1}{40} \frac{9.0}{20} \frac{7.8}{5} \frac{8.3}{3} \frac{8.1}{81} \frac{7.9}{3} \frac{7.8}{20} \frac{4.1}{27} \frac{3.4}{40}$$

$$\frac{14.4}{40} \frac{14.5}{86} \frac{13.5}{15} \frac{12.5}{125} \frac{11.4}{10} \frac{11.7}{30} \frac{6.2}{37} \frac{4.8}{40}$$

$$\frac{8.9}{40} \frac{8.8}{21} \frac{8.4}{11} \frac{7.5}{7.5} \frac{6.8}{6} \frac{5.0}{13} \frac{3.1}{33} \frac{5.7}{35} \frac{4.9}{40}$$

$$\frac{11.8}{40} \frac{11.0}{28} \frac{10.3}{16} \frac{8.7}{8.7} \frac{8.0}{5} \frac{5.5}{12} \frac{4.9}{23} \frac{5.3}{32} \frac{6.2}{35} \frac{7.5}{40}$$

(TOP OF WATER)

$$\frac{14.1}{40} \frac{12.1}{21} \frac{10.9}{8} \frac{10.0}{4} \frac{7.4}{8.3} \frac{5.2}{3} \frac{4.6}{11} \frac{4.8}{21} \frac{5.9}{29} \frac{3.5}{33} \frac{1.4}{37} \frac{1.4}{40}$$

$$\frac{14.1}{40} \frac{12.1}{18} \frac{11.3}{15} \frac{10.4}{7} \frac{9.8}{2} \frac{9.0}{9.2} \frac{6.5}{3} \frac{6.0}{9} \frac{6.4}{17} \frac{7.1}{26} \frac{2.0}{30} \frac{1.8}{37} \frac{1.8}{40}$$

$$\frac{9.5}{40} \frac{7.7}{26} \frac{9.0}{11} \frac{8.7}{8.7} \frac{8.4}{7} \frac{9.8}{10} \frac{7.4}{18} \frac{7.4}{67} \frac{7.7}{31} \frac{5.9}{40}$$

$$\frac{8.4}{40} \frac{8.0}{30} \frac{9.6}{17} \frac{7.8}{8} \frac{7.4}{6} \frac{8.1}{8.1} \frac{7.9}{11} \frac{7.6}{17} \frac{7.5}{23} \frac{8.3}{28} \frac{7.7}{36} \frac{7.7}{40}$$

	906.05	✓	
18+00			99.8
18+50			98.1
19+00			97.9
19+50			98.0
20+00	6.84	✓	97.6
	901.52	11.37	894.68
20+00			
20+50			94.3
21+00			96.1
21+30	1.40	✓	94.0
	892.94	9.98	891.59
21+60	2.02	✓	88.2
	883.15	11.81	881.13
22+00			80.5
22+21			71.8
22+28	FOOE OF PONO ✓		70.2
	5.05	876.63	11.57
			871.58

6.7 5.8 5.1 4.7 6.6 7.7 7.3 7.4 8.1 8.4 8.5
40 30 19 8 63 3 7 15 23 28 34 50

7.2 7.2 5.8 6.9 8.2 7.8 8.2 7.8 5.4 3.4
40 21 7 3 8.0 6 19 23 28 34 40

9.7 9.2 7.5 6.2 6.7 9.3 9.8 9.1 9.0 4.1 3.1
40 35 22 7 1 8.2 5 13 21 26 35 40

6.6 6.8 6.2 5.5 6.8 10.9 10.5 10.8 11.1 4.4 9.4
40 36 12 9 2 8.1 5 11 24 27 40 41

4.9 5.6 6.2 7.3
40 18 7 1 8.5

(9.1) 8.5 8.0 8.0 9.1 10.6 10.9
9 21 32 40 37 40

5.1 4.8 5.7 7.9 7.9 9.8
40 34 17 7.2 6 7 26

7.7 6.1 5.0 6.5 7.7 9.2 11.8 10.5
40 31 18 5.4 8 18 22 26 40

9.4 8.9 7.5 8.2 10.7 15.1 15.1
40 31 15 7.5 14 31 37 40

TOR OF BOOK 15 LT 57 AD 21 + 50

7.2 6.7 5.7 4.3 5.4
40 30 15 4.7 14 40

6.6 5.5 3.8 1.8 1.0
40 59 13 2.7 16 40

11.4 10.4 7.2 5.3 4.7
12.3 12.3 8.4 6.7
(13.0 14 30 40)
TOR OF WATER

876.63

22+21

22+28

22+50

(70.1)
(68.5)

23+00

(70.1)
(67.5)

23+50

(70.1)
(67.9)

23+75

(70.1)
(68.6)

24+00 EDGE OF POND
11.34 887.15 1.82 875.81

✓ 70.1

24+30
9.31 894.54 1.92 885.23

✓ 79.2

24+50

86.3

25+00

89.5

25+50
12.26 905.02 1.78 892.76

✓ 92.5

25+50

26+00

98.7

13.M. 3.22 905.05 2.22 903.80 902.83

$$\begin{array}{c} 64 \\ 40 \end{array} \begin{array}{c} 6.2 \\ 21 \end{array} \begin{array}{c} 5.4 \\ 10 \end{array} \quad (4.8)$$

$$\begin{array}{c} 7.5 \\ 40 \end{array} \begin{array}{c} 7.5 \\ 29 \end{array} \begin{array}{c} 66 \\ 10 \end{array} \quad 6.5 - \text{Top of WINTER}$$

$$\begin{array}{c} 8.1 \\ 40 \end{array} \quad \begin{array}{c} 6.5 \\ 8.1 \end{array} \quad \begin{array}{c} 8.1 \\ 40 \end{array}$$

$$\begin{array}{c} 6.5 \\ 9.0 \end{array}$$

$$\begin{array}{c} 6.5 \\ 8.7 \end{array}$$

$$\begin{array}{c} 6.5 \\ 8.0 \end{array}$$

$$\begin{array}{c} 5.9 \\ 40 \end{array} \begin{array}{c} 6.9 \\ 27 \end{array} \begin{array}{c} 6.9 \\ 15 \end{array} \begin{array}{c} 6.5 \\ 6.5 \end{array} \begin{array}{c} 6.5 \\ 14 \end{array} \begin{array}{c} 6.1 \\ 30 \end{array} \begin{array}{c} 5.5 \\ 40 \end{array}$$

$$\begin{array}{c} 6.2 \\ 40 \end{array} \begin{array}{c} 7.5 \\ 28 \end{array} \begin{array}{c} 7.9 \\ 14 \end{array} \begin{array}{c} 8.0 \\ 8.0 \end{array} \begin{array}{c} 6.8 \\ 11 \end{array} \begin{array}{c} 4.4 \\ 31 \end{array} \begin{array}{c} 2.8 \\ 40 \end{array}$$

$$\begin{array}{c} 8.7 \\ 40 \end{array} \begin{array}{c} 8.7 \\ 33 \end{array} \begin{array}{c} 9.0 \\ 24 \end{array} \begin{array}{c} 8.4 \\ 25 \end{array} \begin{array}{c} 7.8 \\ 8.2 \end{array} \begin{array}{c} 7.2 \\ 19 \end{array} \begin{array}{c} 7.2 \\ 40 \end{array}$$

$$\begin{array}{c} 8.4 \\ 40 \end{array} \begin{array}{c} 6.9 \\ 27 \end{array} \begin{array}{c} 6.1 \\ 14 \end{array} \begin{array}{c} 5.0 \\ 5.0 \end{array} \begin{array}{c} 3.2 \\ 15 \end{array} \begin{array}{c} 2.4 \\ 25 \end{array} \begin{array}{c} 1.2 \\ 35 \end{array} \begin{array}{c} 2.0 \\ 40 \end{array}$$

$$\begin{array}{c} 4.3 \\ 40 \end{array} \begin{array}{c} 4.0 \\ 25 \end{array} \begin{array}{c} 2.9 \\ 11 \end{array} \begin{array}{c} 2.0 \\ 20 \end{array}$$

$$(12.5) \begin{array}{c} 11.6 \\ 9 \end{array} \begin{array}{c} 7.9 \\ 11 \end{array} \begin{array}{c} 9.7 \\ 21 \end{array} \begin{array}{c} 10.2 \\ 25 \end{array} \begin{array}{c} 9.6 \\ 31 \end{array} \begin{array}{c} 7.9 \\ 40 \end{array}$$

$$\begin{array}{c} 8.4 \\ 40 \end{array} \begin{array}{c} 7.8 \\ 29 \end{array} \begin{array}{c} 7.3 \\ 14 \end{array} \begin{array}{c} 6.3 \\ 6.5 \end{array} \begin{array}{c} 6.3 \\ 6 \end{array} \begin{array}{c} 5.0 \\ 11 \end{array} \begin{array}{c} 4.7 \\ 20 \end{array} \begin{array}{c} 5.5 \\ 28 \end{array} \begin{array}{c} 6.8 \\ 31 \end{array} \begin{array}{c} 5.8 \\ 37 \end{array} \begin{array}{c} 3.8 \\ 40 \end{array}$$

✓
90505

26730

✓ 02.9

674 910.80 0.99 ✓ 904.06

26753

✓ 05.6

26764³

✓ 05.7

10.32 916.05 ✓ 507 905.73 ✓

2.50 91281 5.74 910.31 ✓

B.NL

✓ 4.08 908.73 ✓

6.47 915.14 4.14 908.67 ✓

B.NL

✓ 3.93 911.21 911.20

6-13-29

36 46 43

$\frac{54}{40}$ $\frac{3.7}{26}$ $\frac{33}{14}$ $\frac{34}{70}$ $\frac{39}{5}$ 2.2 $\frac{1.7}{10}$ $\frac{2.5}{19}$ $\frac{40}{25}$ $\frac{3.4}{28}$ $\frac{3.4}{40}$

$\frac{5.4}{40}$ $\frac{5.4}{15}$ $\frac{5.2}{5.2}$ $\frac{5.2}{19}$ $\frac{5.2}{40}$

$\frac{5.1}{100}$ $\frac{5.1}{40}$ 5.1 $\frac{4.9}{40}$ $\frac{4.6}{100}$

