

Book 3-A, Dr. 12 X

CONSTRUCTION NOTES

K&E
FIELD BOOK
360A

PROJ. 33-W4

KEUFFEL & ESSER CO.

DRAWING MATERIALS AND SURVEYING INSTRUMENTS.

NEW YORK.

CHICAGO. ST. LOUIS. SAN FRANCISCO. MONTREAL.

TABLES FOR EXCAVATIONS AND EMBANKMENTS.

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.

ROADWAY 18 FEET WIDE. SIDE SLOPES 1 TO 1.

FOR SINGLE TRACK EXCAVATION.

"Copyright, 1895, by Keuffel & Esser Co."

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	0
1	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	1
2	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	2
3	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	3
4	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	4
5	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	5
6	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	6
7	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	7
8	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	8
9	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	9
10	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	10
11	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	11
12	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	12
13	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	13
14	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	14
15	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	15
16	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	16
17	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	17
18	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	18
19	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	19
20	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	20
21	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	21
22	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	22
23	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	23
24	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	24
25	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	25
26	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	26
27	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	27
28	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	28
29	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	29
30	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	30
31	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	31
32	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	32
33	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	33
34	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	34
35	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	35
36	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	36

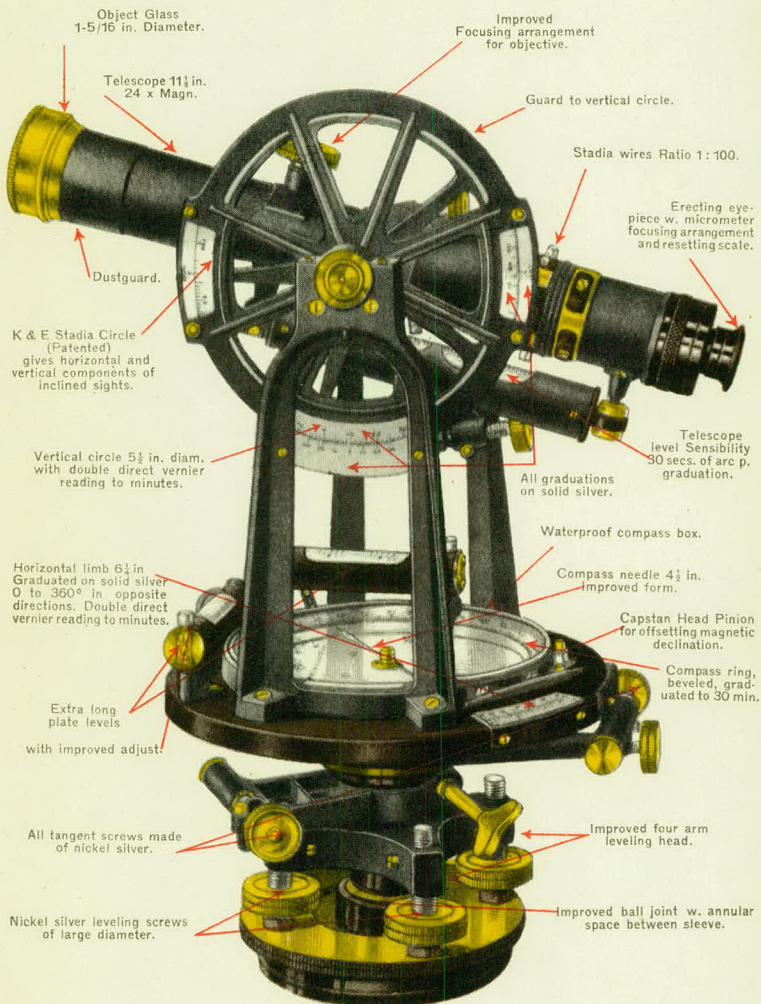
Calculated by Julien A. Hall, M. Am. Soc. C. E.

For Keith's Railroad Curve Tables see end of book.

EXTRA FINE ENGINEERS' TRANSIT

No. 5060 S

KEUFFEL & ESSER CO., N.Y.



ALSO MADE WITH

INTERNAL FOCUSING TELESCOPE
PRACTICALLY DUST AND MOISTURE PROOF.

PROJ. # 33-W4

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33+53⁶⁰

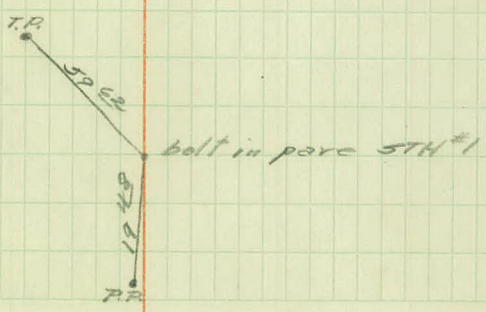
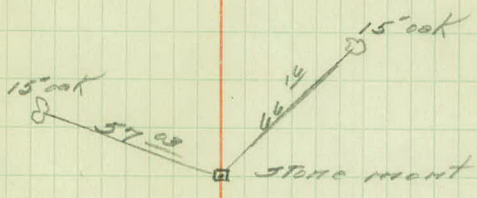
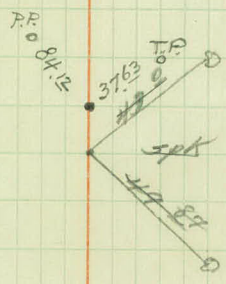
19+50⁰ F.O.T.

~~19+29¹⁰~~

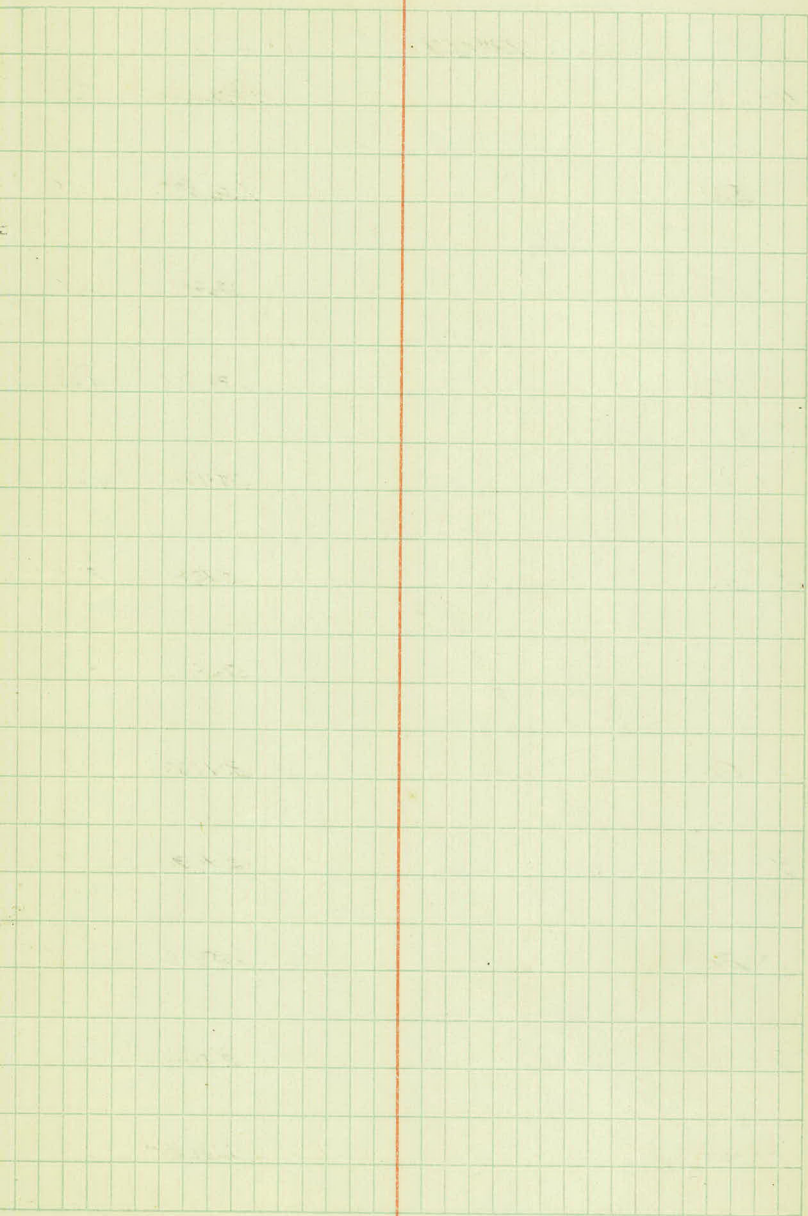
7+25⁸⁵

0+00

• brass plug in pare. N.B. Ave



BM	7.13	936.99	959.80	
0+37			29.30	7.6
+50			29.4	7.3
1+00			30.4	6.5
+50			31.1	5.8
2+00			32.2	4.7
+20			32.5	4.4
3+60			31.9	5.0
3			31.1	5.8
+20			30.6	6.3
+70			29.7	7.2
4			29.2	7.7
+30			28.8	



B.M.	7.46	937.24	929.80	
0+00				
+25				
+37			929.5	7.8
+50			29.7	7.6
1			30.7	6.6
+50			31.4	5.7
2			31.9	5.4
+20			32.0	5.3
+40			31.8	5.5
3			31.3	6.0
+20			31.0	6.3
+70			30.3	7.0
4			29.9	7.4

SPK in PP 1 No. of sta. 0-

$\frac{8.0}{40}$		$\frac{7.7}{40}$				
8.3	8.0	7.8	8.5	11.3	12.4	12.4
40	10	8.1	11	17	22	40
9.4	7.9	7.8	8.5	11.9	13.5	
40	11	8.0	10	18	40	

DC12		$\frac{16}{-0.1}$		$\frac{-5.2}{12.0}$		
8.4	8.4	8.5	7.6	8.8	12.0	13.3
40	28.8	23	10	7.7	11	18
						29.4
						40

$\frac{+0.0}{6.5}$		$\frac{6.0}{6.6}$		$\frac{-2.3}{6.9}$		$\frac{10.5}{8.1}$	
6.5	6.6	6.9	6.5	-0.2	7.0	8.1	8.9
33	240	15	8	6.8	7	12	17.6
							40

$\frac{+2.8}{28}$		$\frac{5.7}{5.7}$		DC13		
28	29	32	5.5	5.4	5.0	5.7
33	28.2	22	12	7	5.6	2
						8
						22.9
						33

$\frac{+3.8}{2.1}$		$\frac{5.4}{1.6}$		$\frac{+3.8}{1.5}$		$\frac{1.4}{4.0}$	
2.1	1.6	1.5	4.0	4.8	4.6	4.0	4.8
33	29.5	24	16	12	4	4.8	3
							6
							9
							29.5
							33

$\frac{32}{33}$		$\frac{2.7}{22}$		$\frac{4.3}{15}$		$\frac{4.9}{11}$	
32	2.7	4.3	4.9	5.3	4.9	4.3	2.6
33	22	15	11	4.8	3	6	8
							29
							33

DC14		$\frac{5.5}{5.9}$		$\frac{+1.5}{5.7}$		$\frac{4.0}{4.2}$	
6.4	5.9	5.7	5.2	5.6	4.0	4.2	4.0
33	23.4	19	12	11	5.4	3	8
							11
							17
							26.2
							33

$\frac{-3.0}{10.0}$		$\frac{6.0}{9.0}$		$\frac{-0.7}{6.4}$		$\frac{6.3}{6.3}$	
10.0	9.0	6.4	6.3	-0.7	6.3	5.9	6.5
33	19.0	13	10	6.1	4	13	17
							23.2
							33

$\frac{10.9}{33}$		$\frac{9.6}{18}$		$\frac{6.8}{12}$		$\frac{6.3}{6.4}$	
10.9	9.6	6.8	6.8	6.1	7.0	6.4	
33	18	12	6.4	4	13	22	33

DC18		$\frac{7.0}{8.2}$		$\frac{7.7}{7.7}$		$\frac{-0.6}{7.8}$	
8.7	8.2	7.7	7.7	-0.6	7.8	7.4	6.1
33	22.2	17	9	7.6	5	9	13
							19
							24.8
							33

DC13		$\frac{7.4}{8.1}$		$\frac{8.2}{8.2}$		$\frac{-0.6}{8.0}$	
8.7	8.1	7.7	8.2	-0.6	8.0	6.4	6.4
33	22.9	17	9	8.0	10	14	25.5
							33

STA.	+	H.I	-	ELEV.	GR. ROD.
		937.24			
4120.				929.60	7.7
+27				29.5	7.8
+35				29.4	7.9
+42				29.4	7.9
5				28.8	8.5
+50				28.4	8.7
T.P.	622	933.56	9.92	937.34	
6				28.4	5.2
+32				28.5	5.1
+50				28.5	5.1
+65				28.5	5.1
7				28.7	4.9
+35				28.9	4.7

LT

RT

$$\begin{array}{r} 9.6 \ 8.5 \ 8.7 \ 7.7 \\ 33 \ 15 \ 9 \ 8.4 \end{array} \quad \begin{array}{r} 8.7 \ 6.6 \ 5.8 \\ 13 \ 15 \ 33 \end{array}$$

$$\begin{array}{r} 9.9 \ 8.8 \ 7.8 \\ 33 \ 15 \ 8.4 \end{array} \quad \begin{array}{r} 8.8 \ 8.0 \ 8.7 \\ 4 \ 10 \ 33 \end{array}$$

$$\begin{array}{r} 10.3 \ 9.9 \ 9.1 \ 7.9 \\ 33 \ 19 \ 15 \ 8.8 \end{array} \quad \begin{array}{r} 9.1 \ 8.7 \ 8.7 \\ 6 \ 8 \ 33 \end{array}$$

$$\begin{array}{r} -2.4 \ 7.9 \\ 11.0 \ 10.3 \ 9.1 \ -1.1 \ 9.2 \ 5.8 \ 8.3 \ 6.9 \ 6.6 \ 6.1 \\ 33 \ 178 \ 12 \ 9.0 \ 6 \ 8 \ 16 \ 21 \ 25.9 \ 33 \end{array}$$

$$\begin{array}{r} -4.3 \ 8.5 \\ 13.4 \ 12.8 \ 12.7 \ 10.3 \ -1.3 \ 9.8 \ 10.3 \ 9.1 \ 7.9 \ 6.6 \\ 33 \ 21.6 \ 17 \ 12 \ 9.8 \ 8 \ 11 \ 15 \ 24.9 \ 33 \end{array}$$

$$\begin{array}{r} -3.9 \ 8.7 \\ 13.3 \ 12.6 \ 10.2 \ -1.2 \ 9.8 \ 10.7 \ 9.0 \ 7.8 \ 6.4 \\ 33 \ 20.9 \ 10 \ 9.9 \ 9 \ 11 \ 15 \ 25.4 \ 33 \end{array}$$

$$\begin{array}{r} -3.5 \ 8.2 \\ 9.6 \ 8.7 \ 6.8 \ -1.3 \ 6.3 \ 7.0 \ 4.9 \ 4.4 \ 3.6 \\ 33 \ 20.0 \ 10 \ 6.5 \ 9 \ 11 \ 18 \ 25.2 \ 33 \end{array}$$

$$\begin{array}{r} 9.6 \ 8.3 \ 6.4 \ 5.1 \\ 33 \ 16 \ 9 \ 6.2 \end{array} \quad \begin{array}{r} 6.3 \ 6.8 \ 5.8 \ 4.4 \\ 9 \ 11 \ 14 \ 33 \end{array}$$

$$\begin{array}{r} DC0.5 \ 5.1 \\ 6.6 \ 6.6 \ 6.2 \ -1.0 \ 6.2 \ 6.9 \ 6.2 \ DC0.9 \ 4.8 \\ 33 \ 21.8 \ 11 \ 6.1 \ 9 \ 11 \ 22 \ 22.4 \ 33 \end{array}$$

$$\begin{array}{r} 7.5 \ 7.2 \ 6.3 \ 5.1 \\ 33 \ 18 \ 10 \ 6.0 \end{array} \quad \begin{array}{r} 6.1 \ 7.2 \ 6.8 \ 5.8 \\ 7 \ 14 \ 25 \ 33 \end{array}$$

$$\begin{array}{r} DC0.9 \ 4.3 \ DC1.2 \\ 5.5 \ 6.8 \ 6.1 \ 6.5 \ 6.1 \ -0.8 \ 5.7 \ 6.1 \\ 33 \ 22.4 \ 16 \ 14 \ 10 \ 5.7 \ 22.8 \ 33 \end{array}$$

$$\begin{array}{r} 4.0 \ 3.9 \ 3.8 \ 5.3 \ 4.7 \\ 33 \ 19 \ 12 \ 10 \ 5.3 \end{array} \quad \begin{array}{r} 5.3 \ 4.6 \\ 12 \ 33 \end{array}$$

933.54

7 + 40

928.90 4.7

8
BNP28.9 4.7
238 931.18

+ 50

28.4 5.0

9

28.2 5.4

+ 50

27.7 5.9

10

27.2 6.4

+ 50

26.8 6.8

11

26.7 6.9

+ 50

26.9 6.7

12

27.1 6.5

+ 50

27.5 6.1

13
TP28.1 5.5
496 928.40

+1.2 4.7
3.6 3.5 3.6 5.8 5.5 -0.5 5.4 3.0 3.0 3.6
 33 25.8 17 12 10 5.2 11 17 25.4 33

+1.3 4.7 +1.7
3.4 3.4 3.1 4.8 -0.2 4.9 3.3 3.0 3.4
 33 26.0 18 12 4.5 11 17 20.5 33

8" 03K 50.1 Rt. 7+6.7 50
4.6 3.9 3.7 5.0 10.3 5.2 4.8 3.3 2.9 3.2
 33 25.7 14 13 4.7 10 13 10 27.2 33
 +1.1

DC1.8 5.4
6.6 5.4 5.6 6.1 -0.5 6.1 5.8 4.7 4.3 4.4
 33 23.7 16 14 5.9 8 14 17 25.4 33

DC0.2 5.9
7.6 7.7 -1.3 7.2 7.8 9.9 7.6
 33 21.3 7.2 10 16 21.3 33

DC0.2 6.4
8.3 8.2 -1.4 7.6 8.4 8.6 9.2
 33 21.3 7.8 10 15 19.4 33

-2.0 6.8
9.6 8.8 8.5 -1.4 8.3 7.6 8.7 8.4 8.5
 33 19.0 12 8.2 6 10 15 21.6 33

-2.8 6.9
9.8 9.7 8.7 -1.5 8.4 9.7 9.7 9.4
 33 18.6 11 8.4 10 14 18.0 33
 18.6

-3.7 6.7
10.6 10.4 10.2 8.4 -1.3 8.4 9.8 10.0 10.0
 33 20.4 17 14 8.2 10 14 19.6 33

-3.2 6.5
9.7 9.7 9.6 7.8 -1.2 8.0 9.5 9.6 9.5
 33 19.4 15 13 7.7 9 14 19.2 33

DC0.2 6.1 DC1.2
8.1 7.9 7.8 7.0 -0.5 7.0 6.9 6.7
 33 21.3 18 11 6.6 16 22.8 33

5.5 +1.1 +2.9
4.5 4.4 4.0 5.6 5.8 5.4 4.2 5.2 4.7 2.7 2.6 2.7
 33 25.7 20 17 13 10 5.3 9 13 18 28.4 33

T.P.	844	934.94		926.50	
13+50				928.90	0.0
14				29.9	5.0
+50				30.9	4.0
15				31.8	3.1
+50				32.7	2.2
T.P.	863	937.23		928.60	
16				33.8	3.4
+50				35.0	3.2
17				35.9	1.3
+50				37.0	0.2
BN7	894	945.06	1.12	936.11	936.10
18				38.1	7.0
+50				39.2	5.9
T.P.	526	946.68	364	941.42	
19				40.2	6.5

$$\begin{array}{r}
 +2.2 \\
 \hline
 3.9 \quad 3.8 \quad 3.5 \quad 5.3 \quad 5.2 \quad +1.2 \quad 5.1 \quad 3.1 \quad 2.8 \quad 2.9 \\
 40 \quad 27.3 \quad 21 \quad 17 \quad 12 \quad 4.8 \quad 12 \quad 18 \quad 28.8 \quad 40
 \end{array}$$

$$\begin{array}{r}
 +2.3 \\
 \hline
 5.0 \quad 2.7 \quad 2.8 \quad 5.5 \quad 4.9 \quad +0.3 \quad 5.0 \quad 2.5 \quad 2.7 \quad 2.8 \\
 40 \quad 27.4 \quad 19 \quad 14 \quad 11 \quad 4.7 \quad 9 \quad 14 \quad 27.4 \quad 40
 \end{array}$$

$$\begin{array}{r}
 +4.0 \\
 \hline
 4.8 \quad 4.1 \quad 3.8 \quad 5.1 \quad 5.4 \quad 4.8 \quad -0.5 \quad 4.6 \quad 5.2 \quad 3.3 \quad 3.3 \quad 3.5 \\
 40 \quad 23.8 \quad 20 \quad 18 \quad 14 \quad 11 \quad 4.5 \quad 5 \quad 10 \quad 17 \quad 25.1 \quad 40
 \end{array}$$

$$\begin{array}{r}
 -2.6 \\
 \hline
 7.1 \quad 5.7 \quad 4.8 \quad -1.5 \quad 4.6 \quad 5.6 \quad 5.7 \\
 40 \quad 18.2 \quad 12 \quad 4.6 \quad 6 \quad 18.0 \quad 40
 \end{array}$$

$$\begin{array}{r}
 -3.4 \\
 \hline
 6.2 \quad 5.6 \quad 4.3 \quad -1.8 \quad 4.4 \quad 4.8 \quad -2.4 \quad 4.6 \quad 4.0 \\
 40 \quad 19.8 \quad 10 \quad 4.0 \quad 8 \quad 10 \quad 17.8 \quad 40
 \end{array}$$

$$\begin{array}{r}
 -2.5 \\
 \hline
 6.2 \quad 5.9 \quad 5.8 \quad 6.1 \quad 5.6 \quad -1.9 \quad 5.3 \quad 5.9 \quad 4.4 \\
 33 \quad 18.0 \quad 17 \quad 14 \quad 9 \quad 5.3 \quad 5 \quad 9 \quad 21.8 \quad 33
 \end{array}$$

$$\begin{array}{r}
 -2.4 \\
 \hline
 4.6 \quad 4.6 \quad 4.9 \quad 4.4 \quad -2.1 \quad 4.4 \quad 4.8 \quad 4.8 \quad 4.6 \\
 33 \quad 17.8 \quad 14 \quad 11 \quad 4.3 \quad 5 \quad 10 \quad 15.2 \quad 33
 \end{array}$$

$$\begin{array}{r}
 -4.4 \\
 \hline
 5.5 \quad 5.7 \quad 5.6 \quad 3.5 \quad -2.0 \quad 3.6 \quad 5.5 \quad 6.2 \quad 6.4 \\
 33 \quad 21.8 \quad 18 \quad 15 \quad 3.3 \quad 11 \quad 15 \quad 22.8 \quad 33
 \end{array}$$

$$\begin{array}{r}
 -3.0 \\
 \hline
 3.1 \quad 3.2 \quad 3.0 \quad 2.0 \quad -1.4 \quad 2.2 \quad 3.4 \quad 3.6 \quad 3.4 \\
 33 \quad 18.0 \quad 17 \quad 13 \quad 1.4 \quad 13 \quad 17 \quad 19.8 \quad 33
 \end{array}$$

Spk. 17 15" Oak 200' Rt. 17+10

$$\begin{array}{r}
 +1.5 \\
 \hline
 5.5 \quad 5.5 \quad 7.5 \quad 7.5 \quad -0.1 \quad 7.3 \quad 7.7 \quad 6.0 \quad 6.4 \quad 6.8 \\
 33 \quad 26.8 \quad 17 \quad 8 \quad 7.1 \quad 6 \quad 15 \quad 17 \quad 24.9 \quad 33
 \end{array}$$

$$\begin{array}{r}
 +4.5 \\
 \hline
 1.4 \quad 1.4 \quad 1.5 \quad 3.1 \quad 5.7 \quad 5.5 \quad +0.6 \quad 5.4 \quad 6.1 \quad 1.9 \quad 2.7 \quad 2.8 \\
 33 \quad 30.8 \quad 23 \quad 19 \quad 14 \quad 12 \quad 5 \quad 3 \quad 7 \quad 14 \quad 18 \quad 28.8 \quad 33
 \end{array}$$

$$\begin{array}{r}
 +4.3 \\
 \hline
 2.2 \quad 2.2 \quad 2.2 \quad 5.8 \quad 6.4 \quad +0.5 \quad 6.4 \quad 6.1 \quad 3.5 \quad 4.1 \quad 4.6 \\
 33 \quad 30.8 \quad 22 \quad 19 \quad 14 \quad 6.0 \quad 8 \quad 14 \quad 17 \quad 27.6 \quad 33
 \end{array}$$

946.68

19+50

940.9

5.8

+92

41.2

5.5

20

41.2

5.5

+10

41.1

5.6

+50

41.0

5.7

21

40.7

6.0

+50

40.4

6.3

T.P.

1.25

944.43

3.50

943.18

22

40.1

4.3

+50

39.8

4.6

23

39.5

4.9

+50

39.2

5.2

24

38.9

5.5

$$\begin{array}{r}
 +1.2 \\
 \hline
 4.3 \quad 4.6 \quad 4.9 \quad 6.1 \quad 5.3 \quad 40.7 \quad 5.4 \quad 6.0 \quad 5.3 \quad 5.2 \quad 5.3 \\
 33 \quad 25.821 \quad 18 \quad 10 \quad 5.1 \quad 7 \quad 12 \quad 16 \quad 24.9 \quad 33
 \end{array}$$

$$\begin{array}{r}
 5.8 \\
 \hline
 5.9 \quad 6.4 \quad 5.2 \\
 33 \quad 20 \quad 18 \quad 5.0 \quad 5.1 \quad 4.8 \quad 5.2 \quad 4.8 \\
 5 \quad 9 \quad 24 \quad 33
 \end{array}$$

$$\begin{array}{r}
 DC1.2 \\
 \hline
 6.1 \quad 6.3 \quad 6.5 \quad 5.3 \quad 10.6 \quad 5.0 \quad 4.6 \quad 4.9 \quad 5.0 \\
 33 \quad 22.8 \quad 20 \quad 11 \quad 4.9 \quad 5 \quad 9 \quad 24.9 \quad 33
 \end{array}$$

$$\begin{array}{r}
 5.6 \\
 \hline
 6.1 \quad 6.4 \quad 5.3 \\
 33 \quad 19 \quad 10 \quad 4.9 \quad 5.2 \quad 5.7 \\
 21 \quad 33
 \end{array}$$

$$\begin{array}{r}
 10.7 \\
 \hline
 4.9 \quad 5.0 \quad 4.9 \quad 5.9 \quad 5.4 \quad 10.5 \quad 5.4 \quad 6.0 \quad 5.1 \quad 5.1 \quad 5.2 \\
 33 \quad 25.1 \quad 17 \quad 14 \quad 10 \quad 5.2 \quad 6 \quad 13 \quad 15 \quad 24.9 \quad 33
 \end{array}$$

$$\begin{array}{r}
 +1.3 \\
 \hline
 4.4 \quad 4.7 \quad 5.0 \quad 5.8 \quad 5.2 \quad 10.8 \quad 5.8 \quad 5.6 \quad 5.5 \\
 33 \quad 25.9 \quad 16 \quad 15 \quad 10 \quad 5.2 \quad 9 \quad 24.6 \quad 33
 \end{array}$$

$$\begin{array}{r}
 +1.6 \\
 \hline
 4.7 \quad 4.7 \quad 4.5 \quad 5.9 \quad 5.2 \quad 11.1 \quad 5.2 \quad 4.2 \quad 4.2 \quad 4.3 \\
 33 \quad 26.4 \quad 18 \quad 14 \quad 10 \quad 5.2 \quad 12 \quad 17 \quad 27.3 \quad 33
 \end{array}$$

$$\begin{array}{r}
 4.3 \\
 \hline
 4.1 \quad 4.1 \quad 2.7 \quad 3.8 \quad 3.7 \quad 3.5 \quad 3.6 \quad 4.0 \quad 3.4 \quad 2.7 \quad 2.8 \\
 33 \quad 26.0 \quad 18 \quad 14 \quad 11 \quad 10.8 \quad 6 \quad 10 \quad 14 \quad 26.4 \quad 33
 \end{array}$$

$$\begin{array}{r}
 4.6 \\
 \hline
 2.3 \quad 2.6 \quad 2.9 \quad 4.0 \quad 4.3 \quad 4.7 \quad 3.7 \quad 2.8 \quad 2.5 \quad 2.6 \\
 33 \quad 27.0 \quad 16 \quad 13 \quad 10.3 \quad 10 \quad 11 \quad 15 \quad 27.2 \quad 33
 \end{array}$$

$$\begin{array}{r}
 4.9 \\
 \hline
 4.3 \quad 4.5 \quad 4.4 \quad 5.5 \quad 4.9 \quad 4.8 \quad 4.9 \quad 5.3 \quad 4.1 \quad 3.7 \quad 4.0 \\
 33 \quad 24.6 \quad 13 \quad 13 \quad 5 \quad 10.1 \quad 5 \quad 10 \quad 12 \quad 25.8 \quad 33
 \end{array}$$

$$\begin{array}{r}
 DC1.1 \\
 \hline
 6.3 \quad 6.1 \quad 6.0 \quad 6.5 \quad 6.0 \quad 5.8 \quad 5.9 \quad 6.4 \quad 6.0 \quad 5.4 \quad 6.0 \\
 33 \quad 22.7 \quad 17 \quad 14 \quad 10 \quad 10.6 \quad 5 \quad 10 \quad 12 \quad 23.7 \quad 33
 \end{array}$$

$$\begin{array}{r}
 5.5 \\
 \hline
 8.0 \quad 8.4 \quad 8.0 \quad 6.7 \quad 6.5 \quad 6.9 \quad 7.6 \quad 7.5 \quad 7.4 \quad 7.8 \\
 33 \quad 18.8 \quad 14 \quad 9 \quad 10 \quad 6 \quad 12 \quad 17.0 \quad 25 \quad 33
 \end{array}$$

944.43

24+50

38.4

5.8

25

38.3

6.1

+50

38.0

6.4

26

37.7

6.7

T.P.

4.50

941.29

7.64

936.79

+50

37.4

3.9

27

37.1

4.2

+50

36.8

4.5

28

36.5

4.8

+50

36.2

5.1

29

35.9

5.4

+50

35.6

5.7

30

35.3

6.0

$$\begin{array}{r} \text{DCA.5} \\ \hline 7.0 \quad 7.3 \quad 7.2 \quad 7.9 \quad 7.1 \quad 7.1 \quad 7.4 \quad 8.1 \quad 8.7 \quad 9.1 \\ 33 \quad 21.8 \quad 17 \quad 13 \quad 9 \quad -1.3 \quad 7 \quad 11 \quad 18.8 \quad 33 \end{array}$$

$$\begin{array}{r} \text{DCO.8} \\ \hline 7.0 \quad 7.3 \quad 7.1 \quad 2.9 \quad 7.5 \quad 7.5 \quad 7.5 \quad 8.3 \quad 7.7 \quad 7.5 \quad 7.9 \\ 33 \quad 22.2 \quad 18 \quad 13 \quad 10 \quad -1.4 \quad 8 \quad 10 \quad 11 \quad 24.9 \quad 33 \end{array}$$

$$\begin{array}{r} \text{DCA.3} \\ \hline 6.9 \quad 7.1 \quad 7.1 \quad 8.2 \quad 7.8 \quad 7.7 \quad 7.8 \quad 8.3 \quad 7.8 \quad 7.4 \quad 7.4 \\ 33 \quad 22.0 \quad 18 \quad 13 \quad 9 \quad -1.3 \quad 6 \quad 10 \quad 11 \quad 22.5 \quad 33 \end{array}$$

$$\begin{array}{r} \text{DCL.0} \\ \hline 7.8 \quad 7.7 \quad 7.5 \quad 8.0 \quad 7.2 \quad 7.8 \quad 7.9 \quad 8.6 \quad 8.0 \quad 7.6 \quad 7.9 \\ 33 \quad 22.5 \quad 18 \quad 15 \quad 9 \quad -1.1 \quad 6 \quad 10 \quad 11 \quad 22.7 \quad 33 \end{array}$$

$$\begin{array}{r} \text{DCL.6} \\ \hline 4.1 \quad 4.3 \quad 4.4 \quad 5.1 \quad 4.7 \quad 4.5 \quad 4.7 \quad 5.4 \quad 4.9 \quad 4.5 \quad 4.4 \\ 33 \quad 23.4 \quad 16 \quad 12 \quad 8 \quad -0.6 \quad 7 \quad 10 \quad 11 \quad 23.1 \quad 33 \end{array}$$

$$\begin{array}{r} \text{DCL.9} \\ \hline 4.3 \quad 4.3 \quad 4.2 \quad 4.9 \quad 4.4 \quad 4.3 \quad 4.5 \quad 5.1 \quad 4.5 \quad 3.9 \quad 4.1 \\ 33 \quad 23.9 \quad 14 \quad 13 \quad 10 \quad -0.1 \quad 7 \quad 11 \quad 12 \quad 24.5 \quad 33 \end{array}$$

$$\begin{array}{r} +0.5 \\ \hline 3.6 \quad 4.0 \quad 4.2 \quad 5.0 \quad 4.3 \quad 4.1 \quad 4.3 \quad 5.1 \quad 4.1 \quad 4.0 \quad 3.5 \quad 3.8 \\ 33 \quad 24.8 \quad 16 \quad 14 \quad 10 \quad +0.4 \quad 6 \quad 11 \quad 13 \quad 19 \quad 25.5 \quad 33 \end{array}$$

$$\begin{array}{r} +0.9 \\ \hline 3.2 \quad 3.9 \quad 3.2 \quad 5.0 \quad 4.6 \quad 4.3 \quad 4.4 \quad 5.3 \quad 3.8 \quad 3.4 \quad 3.4 \\ 33 \quad 25.4 \quad 17 \quad 15 \quad 10 \quad +0.5 \quad 6 \quad 13 \quad 15 \quad 26.1 \quad 33 \end{array}$$

$$\begin{array}{r} +1.6 \\ \hline 3.1 \quad 3.5 \quad 3.4 \quad 5.4 \quad 4.8 \quad 4.6 \quad 4.6 \quad 5.1 \quad 3.4 \quad 3.6 \quad 2.8 \quad 3.4 \\ 33 \quad 26.4 \quad 22 \quad 18 \quad 10 \quad +0.5 \quad 10 \quad 14 \quad 15 \quad 21 \quad 27.5 \quad 33 \end{array}$$

$$\begin{array}{r} +2.1 \\ \hline 3.0 \quad 3.3 \quad 3.2 \quad 5.6 \quad 5.5 \quad 5.3 \quad 5.4 \quad 5.9 \quad 3.2 \quad 2.6 \quad 2.8 \\ 33 \quad 27.2 \quad 20 \quad 18 \quad 11 \quad +0.1 \quad 9 \quad 14 \quad 16 \quad 28.2 \quad 33 \end{array}$$

$$\begin{array}{r} +0.8 \\ \hline 4.9 \quad 4.9 \quad 5.1 \quad 6.9 \quad 6.4 \quad 6.1 \quad 6.3 \quad 6.7 \quad 5.1 \quad 4.9 \quad 4.2 \quad 4.6 \\ 33 \quad 25.2 \quad 21 \quad 18 \quad 11 \quad -0.4 \quad 8 \quad 14 \quad 16 \quad 21 \quad 26.3 \quad 33 \end{array}$$

$$\begin{array}{r} \text{DCO.4} \\ \hline 7.2 \quad 7.5 \quad 7.6 \quad 7.7 \quad 8.4 \quad 7.4 \quad 7.1 \quad 7.3 \quad 8.4 \quad 7.8 \quad 7.7 \quad 7.2 \quad 6.7 \quad 7.4 \\ 33 \quad 27 \quad 21.6 \quad 17 \quad 15 \quad 10 \quad -1.1 \quad 7 \quad 12 \quad 15 \quad 19 \quad 22.2 \quad 25 \quad 33 \end{array}$$

941.29

30 +50

35.2

6.1

31

35.5

5.8

+41

36.2

5.1

32

37.3

4.0

T.P.

7.93

945.59

3.63

937.66

+50

38.6

7.0

33

39.9

5.7

+22

40.5

5.1

+32

40.7

4.9

+40

40.9

4.7

+53.6

4 W. B. Ave

B.M.

4.41

941.18

941.17

$$\begin{array}{r} -4.6 \\ \hline 10.5 \\ 33 \end{array} \quad \begin{array}{r} 10.7 \\ \hline 22.2 \end{array} \quad \begin{array}{r} 10.3 \\ \hline 17 \end{array} \quad \begin{array}{r} 7.9 \\ \hline 11 \end{array} \quad \begin{array}{r} 6.1 \\ \hline 7.5 \\ -1.4 \end{array} \quad \begin{array}{r} 7.7 \\ \hline 8 \end{array} \quad \begin{array}{r} 9.7 \\ \hline 14 \end{array} \quad \begin{array}{r} -4.3 \\ \hline 10.4 \\ 21.6 \end{array} \quad \begin{array}{r} 9.9 \\ \hline 33 \end{array}$$

$$\begin{array}{r} -4.8 \\ \hline 10.0 \\ 33 \end{array} \quad \begin{array}{r} 10.6 \\ \hline 22.6 \end{array} \quad \begin{array}{r} 9.9 \\ \hline 15 \end{array} \quad \begin{array}{r} 7.8 \\ \hline 10 \end{array} \quad \begin{array}{r} 5.8 \\ \hline 7.6 \\ -1.8 \end{array} \quad \begin{array}{r} 8.2 \\ \hline 7 \end{array} \quad \begin{array}{r} 9.3 \\ \hline 11 \end{array} \quad \begin{array}{r} -4.7 \\ \hline 10.2 \\ 16 \end{array} \quad \begin{array}{r} 10.5 \\ \hline 22.4 \end{array} \quad \begin{array}{r} 10.0 \\ \hline 33 \end{array}$$

$$\begin{array}{r} 6.8 \\ \hline 33 \end{array} \quad \begin{array}{r} 7.1 \\ \hline 27 \end{array} \quad \begin{array}{r} 8.3 \\ \hline 21 \end{array} \quad \begin{array}{r} -3.3 \\ \hline 8.4 \\ 19.6 \end{array} \quad \begin{array}{r} 8.0 \\ \hline 15 \end{array} \quad \begin{array}{r} 7.1 \\ \hline 9 \end{array} \quad \begin{array}{r} 5.1 \\ \hline 7.0 \\ -1.9 \end{array} \quad \begin{array}{r} 7.2 \\ \hline 8 \end{array} \quad \begin{array}{r} 8.1 \\ \hline 11 \end{array} \quad \begin{array}{r} 7.7 \\ \hline 13 \end{array} \quad \begin{array}{r} -2.7 \\ \hline 7.8 \\ 18.4 \end{array} \quad \begin{array}{r} 7.1 \\ \hline 23 \end{array} \quad \begin{array}{r} 7.2 \\ \hline 33 \end{array}$$

$$\begin{array}{r} 2.8 \\ \hline 33 \end{array} \quad \begin{array}{r} 3.0 \\ \hline 25.5 \end{array} \quad \begin{array}{r} 5.3 \\ \hline 20 \end{array} \quad \begin{array}{r} 4.7 \\ \hline 12 \end{array} \quad \begin{array}{r} 5.1 \\ \hline 8 \end{array} \quad \begin{array}{r} 4.0 \\ \hline 4.5 \\ -0.5 \end{array} \quad \begin{array}{r} 4.6 \\ \hline 8 \end{array} \quad \begin{array}{r} 5.0 \\ \hline 11 \end{array} \quad \begin{array}{r} 4.2 \\ \hline 13 \end{array} \quad \begin{array}{r} 3.0 \\ \hline 25.5 \end{array} \quad \begin{array}{r} 2.8 \\ \hline 33 \end{array}$$

$$\begin{array}{r} 5.0 \\ \hline 33 \end{array} \quad \begin{array}{r} +2.0 \\ \hline 5.0 \\ 27.0 \end{array} \quad \begin{array}{r} 6.2 \\ \hline 23 \end{array} \quad \begin{array}{r} 8.0 \\ \hline 18 \end{array} \quad \begin{array}{r} 7.6 \\ \hline 14 \end{array} \quad \begin{array}{r} 7.0 \\ \hline 11 \end{array} \quad \begin{array}{r} 7.0 \\ \hline 6.6 \\ +0.4 \end{array} \quad \begin{array}{r} 6.6 \\ \hline 6 \end{array} \quad \begin{array}{r} 7.3 \\ \hline 11 \end{array} \quad \begin{array}{r} 6.6 \\ \hline 13 \end{array} \quad \begin{array}{r} 5.6 \\ \hline 18 \end{array} \quad \begin{array}{r} +1.5 \\ \hline 5.5 \\ 26.3 \end{array} \quad \begin{array}{r} 5.8 \\ \hline 33 \end{array}$$

$$\begin{array}{r} 4.7 \\ \hline 33 \end{array} \quad \begin{array}{r} +1.2 \\ \hline 4.5 \\ 25.8 \end{array} \quad \begin{array}{r} 4.6 \\ \hline 22 \end{array} \quad \begin{array}{r} 6.7 \\ \hline 18 \end{array} \quad \begin{array}{r} 6.6 \\ \hline 15 \end{array} \quad \begin{array}{r} 5.6 \\ \hline 9 \end{array} \quad \begin{array}{r} 5.7 \\ \hline 5.4 \\ +0.3 \end{array} \quad \begin{array}{r} 5.6 \\ \hline 7 \end{array} \quad \begin{array}{r} 5.9 \\ \hline 10 \end{array} \quad \begin{array}{r} 5.3 \\ \hline 12 \end{array} \quad \begin{array}{r} +0.4 \\ \hline 5.3 \\ 24.6 \end{array} \quad \begin{array}{r} 5.2 \\ \hline 33 \end{array}$$

$$\begin{array}{r} 4.3 \\ \hline 33 \end{array} \quad \begin{array}{r} 4.3 \\ \hline 22 \end{array} \quad \begin{array}{r} 6.3 \\ \hline 18 \end{array} \quad \begin{array}{r} 5.9 \\ \hline 14 \end{array} \quad \begin{array}{r} 5.2 \\ \hline 12 \end{array} \quad \begin{array}{r} 5.1 \\ \hline 4.9 \\ +0.2 \end{array} \quad \begin{array}{r} 5.2 \\ \hline 10 \end{array} \quad \begin{array}{r} 4.1 \\ \hline 15 \end{array} \quad \begin{array}{r} 3.8 \\ \hline 33 \end{array}$$

$$\begin{array}{r} 6.2 \\ \hline 33 \end{array} \quad \begin{array}{r} 5.8 \\ \hline 20 \end{array} \quad \begin{array}{r} 4.7 \\ \hline 17 \end{array} \quad \begin{array}{r} 5.0 \\ \hline 14 \end{array} \quad \begin{array}{r} 4.9 \\ \hline 4.7 \\ +0.2 \end{array} \quad \begin{array}{r} 4.9 \\ \hline 13 \end{array} \quad \begin{array}{r} 4.6 \\ \hline 17 \end{array} \quad \begin{array}{r} 4.3 \\ \hline 33 \end{array}$$

$$\begin{array}{r} 4.2 \\ \hline 33 \end{array} \quad \begin{array}{r} 4.8 \\ \hline 22 \end{array} \quad \begin{array}{r} 4.7 \\ \hline 4.6 \\ +0.1 \end{array} \quad \begin{array}{r} 4.8 \\ \hline 20 \end{array} \quad \begin{array}{r} 4.3 \\ \hline 33 \end{array}$$

$$\begin{array}{r} 4.26 \\ \hline 33 \end{array} \quad \begin{array}{r} 4.41 \\ \hline 33 \end{array} \quad \begin{array}{r} 4.55 \\ \hline 33 \end{array}$$

Brass Plug in Pavement & W.B. Arc

B.M.	3.23	939.34		936.11	
17+50				37.2	2.14 ✓
17				36.2	3.14 ✓
+50				35.3	4.04 ✓
16				34.1	5.24 ✓
+50				33.0	6.34 ✓
15				32.1	7.24 ✓
+50				30.9	8.44 ✓
14				29.9	9.44 ✓
+50				28.9	10.44 ✓
13				28.1	11.24 ✓
T.P.	3.64	931.76	11.22	928.12	
+50				27.5	4.26 ✓
12				27.3	4.46 ✓
+50				27.2	4.56 ✓
11				27.0	4.76 ✓
+50				27.1	4.66 ✓
10				27.5	4.26 ✓
+50				27.9	3.86 ✓
					4.26
					4.66

0.2 H_i

0.2 H_i

31.8

7.5

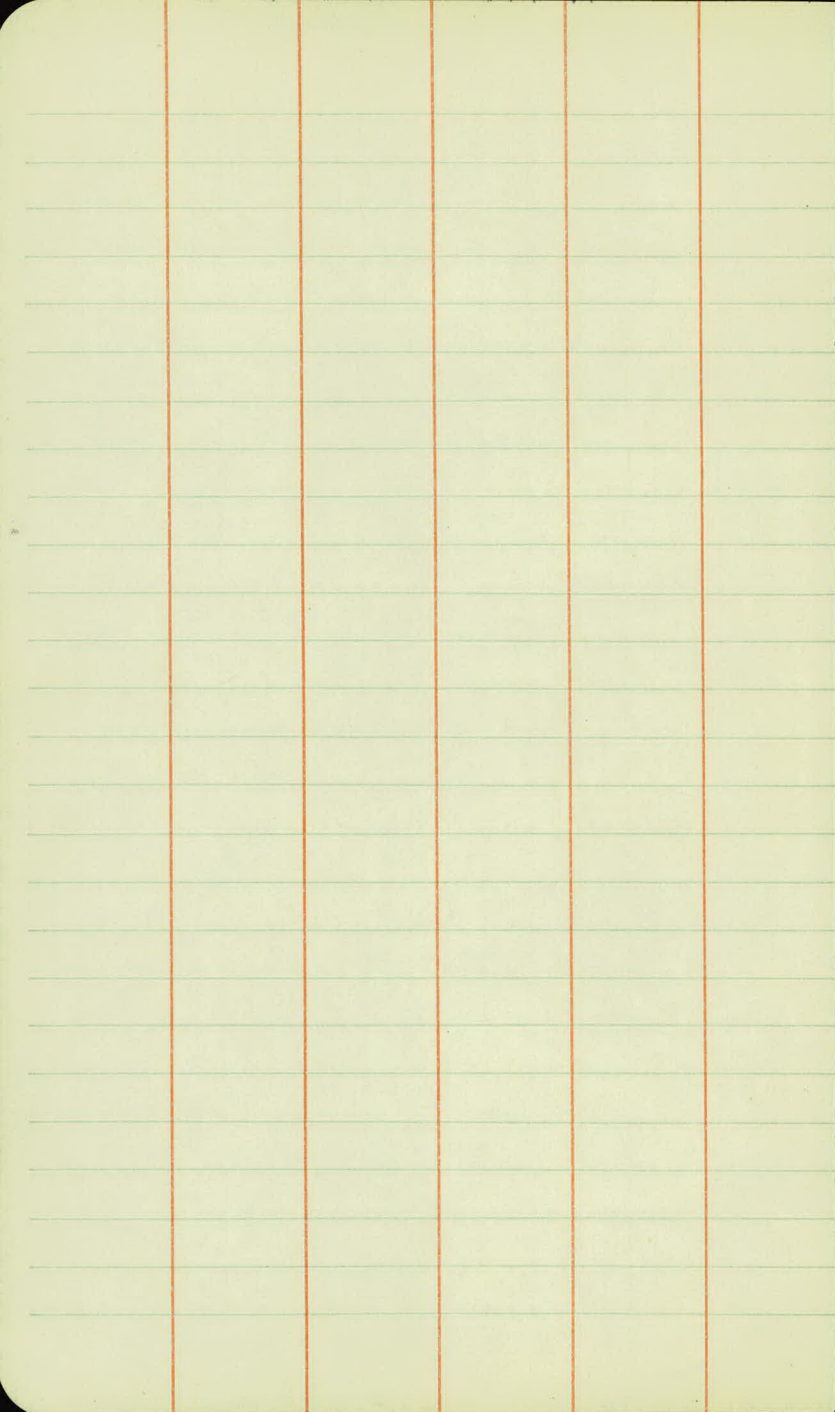
6.26

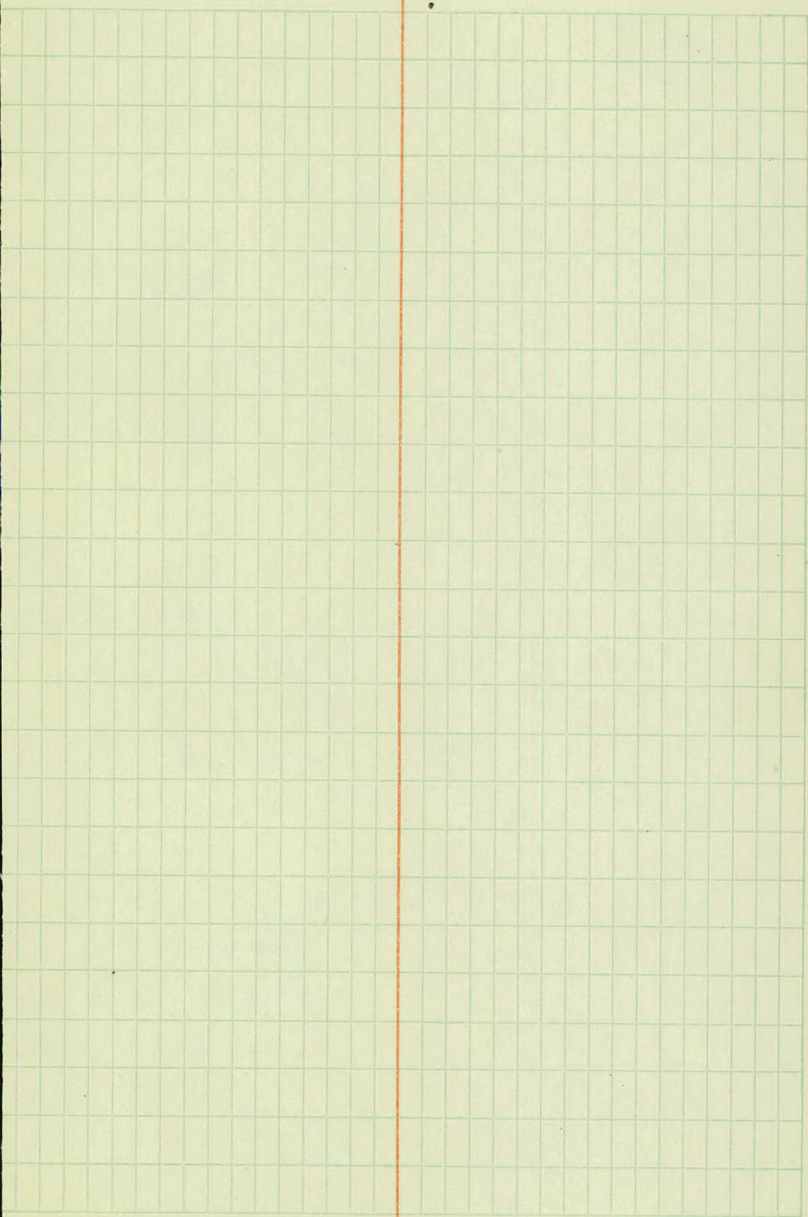
4.06

0.2 H_i

0.3 H_i

0.2 H_i





B.M.	6.58	936.38		929.80	
+50		<u>27</u>		929.7	✓6.68
1		28.68		30.7	✓5.68
+50				31.6	✓4.78
2				31.9	✓4.48
+50				31.8	✓4.58
3				31.3	✓5.08
+50				30.6	✓5.78
4				29.9	✓6.48
+50				29.3	✓7.08
5				28.8	✓7.58
+50				28.6	✓7.78
6				28.4	✓7.98
+50				28.5	✓7.88
7	3.48	932.16	7.70	28.7	✓7.68
+50				28.9	✓3.26
8				28.9	✓3.26
+50				28.6	✓3.56
9				28.2	✓3.96
+50					
10	28.68				
+50	3.48		7.70		
11	<u>32.16</u>				
+50					
12					

SPK IN PAI No. OF STA 0-23

+50

13

+50

14

+50

15

+50

16

+50

17

+50

94260

18

+50

38.1 ✓ 2.5

39.2 ✓ 3.4

19

+50

94447

40.2 ✓ 2.4

40.9 ✓ 3.57

20

+50

41.2 ✓ 3.27

41.0 ✓ 3.47

21

+50

40.7 ✓ 3.77

40.4 ✓ 4.07

22

+50

40.1 ✓ 4.37

39.8 ✓ 4.67

23

+50

39.5 ✓ 4.97

39.2 ✓ 5.27

B.M. spt in Elm.

941.87

26.0

23' Lt 20 + 40

944.47

- 7.98

936.49

5.00

41.63

24

+50

25

+50

26

+50

27

+50

28

+50

29

+50

30

+50

31

+50

32

+50

33

+50

34

+50

35

38.9

38.6

38.3

38.0

37.7

37.4

37.1

36.8

36.5

36.2

35.9

35.6

35.3

35.2

35.5

36.2

37.3

38.6

39.9

✓5.57

✓5.87

✓6.17

✓6.47

✓6.77

✓7.07

✓7.37

✓7.67

✓7.97

✓✓4.3

✓5.73

✓6.03

✓6.33

✓6.43

✓6.13

✓5.43

✓4.33

✓3.03

✓1.73

941.17

Fair 68°F.

4-30-34

15

{ Weber
Stooglund
Wilke
Bell.
Steinman

Final Survey

Sta.	+	H.I. ✓	-	Elev.
B.M.	7.09	936.89		929.80
0+00				

+17

+37

+50

1

+50

2

+20

+60

3

+20

+70

4-30-34

16

LEFT

E

RIGHT.

Spk. in P.P. 1' No 0-23'

$$\begin{array}{r} 7.6 \\ 50 \end{array} \quad \begin{array}{r} 7.4 \\ 50 \end{array}$$

$$\begin{array}{r} 7.6 \\ 50 \end{array} \quad \begin{array}{r} 7.7 \\ 27 \end{array} \quad \begin{array}{r} 7.11 \\ 7.6 \end{array} \quad \begin{array}{r} 7.5 \\ 28 \end{array} \quad \begin{array}{r} 11.4 \\ 35 \end{array} \quad \begin{array}{r} 11.3 \\ 50 \end{array}$$

$$\begin{array}{r} 9.4 \\ 50 \end{array} \quad \begin{array}{r} 9.0 \\ 28 \end{array} \quad \begin{array}{r} 7.3 \\ 23 \end{array} \quad \begin{array}{r} 7.14 \\ 7.2 \end{array} \quad \begin{array}{r} 7.3 \\ 22 \end{array} \quad \begin{array}{r} 12.8 \\ 34 \end{array} \quad \begin{array}{r} 12.6 \\ 50 \end{array}$$

$$\begin{array}{r} 8.0 \\ 40 \end{array} \quad \begin{array}{r} 8.1 \\ 29 \end{array} \quad \begin{array}{r} 8.9 \\ 27 \end{array} \quad \begin{array}{r} 9.0 \\ 24 \end{array} \quad \begin{array}{r} 7.3 \\ 20 \end{array} \quad \begin{array}{r} 7.12 \\ 7.0 \end{array} \quad \begin{array}{r} 7.2 \\ 19 \end{array} \quad \begin{array}{r} 12.4 \\ 30 \end{array} \quad \begin{array}{r} 12.4 \\ 40 \end{array}$$

$$\begin{array}{r} 6.0 \\ 40 \end{array} \quad \begin{array}{r} 6.3 \\ 25 \end{array} \quad \begin{array}{r} 8.0 \\ 21 \end{array} \quad \begin{array}{r} 8.2 \\ 17 \end{array} \quad \begin{array}{r} 6.2 \\ 13 \end{array} \quad \begin{array}{r} 6.12 \\ 6.2 \end{array} \quad \begin{array}{r} 6.2 \\ 13 \end{array} \quad \begin{array}{r} 8.5 \\ 18 \end{array} \quad \begin{array}{r} 10.8 \\ 40 \end{array}$$

$$\begin{array}{r} 2.9 \\ 40 \end{array} \quad \begin{array}{r} 2.8 \\ 28 \end{array} \quad \begin{array}{r} 7.2 \\ 21 \end{array} \quad \begin{array}{r} 7.3 \\ 17 \end{array} \quad \begin{array}{r} 5.3 \\ 13 \end{array} \quad \begin{array}{r} 5.13 \\ 5.3 \end{array} \quad \begin{array}{r} 5.3 \\ 13 \end{array} \quad \begin{array}{r} 7.3 \\ 17 \end{array} \quad \begin{array}{r} 7.3 \\ 21 \end{array} \quad \begin{array}{r} 6.2 \\ 23 \end{array} \quad \begin{array}{r} 7.3 \\ 40 \end{array}$$

$$\begin{array}{r} 2.2 \\ 40 \end{array} \quad \begin{array}{r} 1.4 \\ 30 \end{array} \quad \begin{array}{r} 6.8 \\ 21 \end{array} \quad \begin{array}{r} 6.8 \\ 17 \end{array} \quad \begin{array}{r} 5.0 \\ 13 \end{array} \quad \begin{array}{r} 5.0 \\ 4.8 \end{array} \quad \begin{array}{r} 5.0 \\ 13 \end{array} \quad \begin{array}{r} 6.8 \\ 17 \end{array} \quad \begin{array}{r} 6.8 \\ 21 \end{array} \quad \begin{array}{r} 1.2 \\ 30 \end{array} \quad \begin{array}{r} 1.7 \\ 40 \end{array}$$

$$\begin{array}{r} 3.1 \\ 40 \end{array} \quad \begin{array}{r} 2.6 \\ 28 \end{array} \quad \begin{array}{r} 6.7 \\ 21 \end{array} \quad \begin{array}{r} 6.6 \\ 17 \end{array} \quad \begin{array}{r} 4.8 \\ 13 \end{array} \quad \begin{array}{r} 4.9 \\ 4.7 \end{array} \quad \begin{array}{r} 4.9 \\ 13 \end{array} \quad \begin{array}{r} 6.7 \\ 17 \end{array} \quad \begin{array}{r} 6.5 \\ 21 \end{array} \quad \begin{array}{r} 0.5 \\ 29 \end{array} \quad \begin{array}{r} 0.5 \\ 40 \end{array}$$

$$\begin{array}{r} 6.7 \\ 40 \end{array} \quad \begin{array}{r} 6.2 \\ 23 \end{array} \quad \begin{array}{r} 6.4 \\ 18 \end{array} \quad \begin{array}{r} 5.0 \\ 13 \end{array} \quad \begin{array}{r} 5.1 \\ 5.0 \end{array} \quad \begin{array}{r} 5.2 \\ 13 \end{array} \quad \begin{array}{r} 7.3 \\ 17 \end{array} \quad \begin{array}{r} 7.2 \\ 21 \end{array} \quad \begin{array}{r} 3.6 \\ 26 \end{array} \quad \begin{array}{r} 2.8 \\ 40 \end{array}$$

$$\begin{array}{r} 9.8 \\ 40 \end{array} \quad \begin{array}{r} 8.5 \\ 19 \end{array} \quad \begin{array}{r} 5.6 \\ 13 \end{array} \quad \begin{array}{r} 5.6 \\ 5.6 \end{array} \quad \begin{array}{r} 5.6 \\ 13 \end{array} \quad \begin{array}{r} 7.7 \\ 17 \end{array} \quad \begin{array}{r} 7.2 \\ 21 \end{array} \quad \begin{array}{r} 6.2 \\ 23 \end{array} \quad \begin{array}{r} 5.3 \\ 40 \end{array}$$

$$\begin{array}{r} 10.6 \\ 40 \end{array} \quad \begin{array}{r} 9.3 \\ 19 \end{array} \quad \begin{array}{r} 6.1 \\ 13 \end{array} \quad \begin{array}{r} 5.9 \\ 5.8 \end{array} \quad \begin{array}{r} 5.8 \\ 13 \end{array} \quad \begin{array}{r} 8.1 \\ 17 \end{array} \quad \begin{array}{r} 8.0 \\ 21 \end{array} \quad \begin{array}{r} 6.6 \\ 24 \end{array} \quad \begin{array}{r} 5.9 \\ 40 \end{array}$$

$$\begin{array}{r} 8.7 \\ 40 \end{array} \quad \begin{array}{r} 7.6 \\ 23 \end{array} \quad \begin{array}{r} 8.5 \\ 21 \end{array} \quad \begin{array}{r} 8.6 \\ 17 \end{array} \quad \begin{array}{r} 6.6 \\ 13 \end{array} \quad \begin{array}{r} 6.6 \\ 6.7 \end{array} \quad \begin{array}{r} 6.7 \\ 13 \end{array} \quad \begin{array}{r} 8.7 \\ 17 \end{array} \quad \begin{array}{r} 8.6 \\ 21 \end{array} \quad \begin{array}{r} 6.1 \\ 25 \end{array} \quad \begin{array}{r} 5.8 \\ 40 \end{array}$$

Sta	+	H.I. ✓	-	Elev
4		936.89		

+20

+27

+35

+42

5

+50

6

T.P.	7.00	✓ 933.72	10.17	✓ 926.72
------	------	----------	-------	----------

+32

+50

+65

7

+35

LEFT

五

RIGHT

$\frac{8.7}{40}$	$\frac{7.9}{28}$	$\frac{8.9}{21}$	$\frac{9.0}{17}$	$\frac{7.0}{13}$	$\frac{7.0}{13}$	$\frac{9.1}{17}$	$\frac{8.9}{21}$	$\frac{6.1}{26}$	$\frac{5.7}{40}$
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$\frac{9.4}{40}$	$\frac{8.6}{23}$	$\frac{9.1}{21}$	$\frac{9.0}{17}$	$\frac{7.2}{13}$	$\overset{1.3}{7.2}$	$\frac{7.3}{13}$	$\frac{9.1}{17}$	$\frac{9.1}{21}$	$\frac{5.8}{27}$	$\frac{5.5}{40}$
------------------	------------------	------------------	------------------	------------------	----------------------	------------------	------------------	------------------	------------------	------------------

$\frac{9.9}{40}$	$\frac{9.0}{22}$	$\frac{9.3}{21}$	$\frac{9.3}{17}$	$\frac{7.3}{13}$	$7^{1.4}$	$\frac{7.3}{13}$	$\frac{8.0}{40}$
------------------	------------------	------------------	------------------	------------------	-----------	------------------	------------------

$$\frac{10.4}{40} \quad \frac{9.5}{18} \quad \frac{7.4}{13} \quad \overset{1.1}{7.2} \quad \frac{7.4}{13} \quad \frac{8.0}{40}$$

$\frac{10.8}{40}$	$\frac{9.8}{18}$	$\frac{7.5}{13}$	$\frac{1.5}{73}$	$\frac{7.5}{13}$	$\frac{9.3}{17}$	$\frac{9.3}{21}$	$\frac{7.3}{26}$	$\frac{6.0}{40}$
-------------------	------------------	------------------	------------------	------------------	------------------	------------------	------------------	------------------

$$\frac{13.4}{40} \quad \frac{12.4}{22} \quad \frac{8.1}{13} \quad 7.1 \quad \frac{8.0}{13} \quad \frac{10.1}{17} \quad \frac{10.0}{21} \quad \frac{7.5}{25} \quad \frac{6.0}{40}$$

$$\frac{13.4}{40} \quad \frac{12.0}{21} \quad \frac{8.4}{13} \quad \frac{8.3}{13} \quad \frac{10.4}{17} \quad \frac{10.3}{21} \quad \frac{7.4}{25} \quad \frac{5.9}{40}$$

$\frac{13.1}{40}$	$\frac{12.0}{20}$	$\frac{8.5}{13}$	$\frac{8.5}{13}$	$\frac{11.0}{17}$	$\frac{10.9}{21}$	$\frac{7.7}{25}$	$\frac{6.5}{40}$
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$$\frac{9.4}{40} \quad \frac{8.5}{19} \quad \frac{5.4}{13} \quad \overset{12}{52} \quad \frac{5.3}{13} \quad \frac{7.5}{17} \quad \frac{7.5}{21} \quad \frac{5.3}{24} \quad \frac{4.1}{40}$$

$$\frac{6.8}{40} \quad \frac{6.7}{22} \quad \frac{7.3}{21} \quad \frac{7.2}{17} \quad \frac{5.2}{13} \quad 5.1 \quad \overset{12}{5.1} \quad \frac{5.2}{13} \quad \frac{7.4}{17} \quad \frac{5.3}{24} \quad \frac{3.6}{40}$$

$\frac{76}{40}$	$\frac{73}{18}$	$\frac{52}{13}$	$5^{1/2}$	$\frac{53}{13}$	$\frac{72}{17}$	$\frac{69}{25}$	$\frac{49}{40}$
-----------------	-----------------	-----------------	-----------	-----------------	-----------------	-----------------	-----------------

$\frac{54}{40}$	$\frac{61}{22}$	$\frac{71}{21}$	$\frac{70}{17}$	$\frac{50}{13}$	$\frac{60}{49}$	$\frac{50}{20}$	$\frac{66}{25}$	$\frac{57}{40}$
-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------

$$\frac{4.3}{40} \quad \frac{3.7}{26} \quad \frac{7.0}{21} \quad \frac{7.0}{18} \quad \frac{4.9}{13} \quad 4.8 \quad \frac{4.6}{21} \quad \frac{5.3}{27} \quad \frac{4.7}{40}$$

✓
933.72

7 + 40

8

B.M.

2.51 931.21 931.18

+ 50

9

+ 50

10

+ 50

11

+ 50

12

T.P.

9.86

✓
936.51

7.07

✓
926.65

+ 50

13

+ 50

LEFT					$\pm$	RIGHT				
$\frac{40}{40}$	$\frac{3.7}{26}$	$\frac{6.9}{21}$	$\frac{6.8}{17}$	$\frac{4.9}{13}$	$\frac{4.8}{48}$	$\frac{4.7}{16}$	$\frac{6.3}{19}$	$\frac{5.9}{23}$	$\frac{3.8}{27}$	$\frac{3.7}{40}$
$\frac{4.1}{40}$	$\frac{3.5}{26}$	$\frac{6.5}{21}$	$\frac{6.6}{17}$	$\frac{4.8}{13}$	$\frac{4.8}{49}$	$\frac{7.0}{13}$	$\frac{6.9}{17}$	$\frac{3.1}{21}$	$\frac{3.6}{27}$	$\frac{3.6}{40}$
$\frac{5.8}{40}$	$\frac{4.1}{26}$	$\frac{7.0}{21}$	$\frac{7.1}{17}$	$\frac{5.1}{13}$	$\frac{5.1}{51}$	$\frac{5.1}{13}$	$\frac{7.0}{17}$	$\frac{7.0}{21}$	$\frac{3.0}{28}$	$\frac{3.8}{40}$
$\frac{7.3}{40}$	$\frac{6.0}{24}$	$\frac{7.8}{21}$	$\frac{7.8}{17}$	$\frac{5.5}{13}$	$\frac{5.5}{54}$	$\frac{5.5}{13}$	$\frac{7.5}{17}$	$\frac{7.4}{21}$	$\frac{4.5}{26}$	$\frac{4.5}{40}$
$\frac{8.0}{40}$	$\frac{7.7}{22}$	$\frac{8.2}{21}$	$\frac{8.1}{17}$	$\frac{6.0}{13}$	$\frac{6.0}{59}$	$\frac{6.0}{13}$	$\frac{8.0}{17}$	$\frac{8.1}{20}$	$\frac{7.8}{21}$	$\frac{7.6}{40}$
$\frac{8.5}{40}$	$\frac{8.4}{22}$	$\frac{8.7}{21}$	$\frac{8.5}{17}$	$\frac{6.5}{13}$	$\frac{6.5}{62}$	$\frac{6.5}{13}$	$\frac{8.9}{17}$	$\frac{9.4}{25}$	$\frac{9.5}{40}$	
		$\frac{10.0}{40}$	$\frac{9.2}{18}$	$\frac{6.8}{13}$	$\frac{6.9}{66}$	$\frac{6.8}{13}$	$\frac{9.0}{17}$	$\frac{9.1}{20}$	$\frac{8.5}{22}$	$\frac{8.7}{40}$
		$\frac{10.3}{40}$	$\frac{9.8}{19}$	$\frac{7.0}{13}$	$\frac{7.0}{67}$	$\frac{7.1}{13}$	$\frac{9.9}{19}$	$\frac{9.5}{40}$		
		$\frac{10.9}{40}$	$\frac{10.4}{21}$	$\frac{6.8}{13}$	$\frac{6.8}{65}$	$\frac{6.8}{13}$	$\frac{10.1}{19}$	$\frac{10.2}{40}$		
		$\frac{10.1}{40}$	$\frac{9.8}{20}$	$\frac{6.7}{13}$	$\frac{6.6}{63}$	$\frac{6.7}{13}$	$\frac{9.6}{19}$	$\frac{9.7}{40}$		
west end Col. v.										
$\frac{11.4}{40}$	$\frac{10.8}{21}$	$\frac{11.2}{20}$	$\frac{11.2}{17}$	$\frac{9.1}{13}$	$\frac{9.0}{90}$	$\frac{9.1}{13}$	$\frac{11.1}{17}$	$\frac{11.1}{21}$	$\frac{9.9}{24}$	$\frac{9.7}{40}$
$\frac{7.7}{40}$	$\frac{7.3}{26}$	$\frac{10.5}{21}$	$\frac{10.5}{17}$	$\frac{8.5}{13}$	$\frac{8.4}{83}$	$\frac{8.5}{13}$	$\frac{10.5}{17}$	$\frac{10.4}{21}$	$\frac{5.6}{29}$	$\frac{6.2}{40}$
$\frac{5.3}{40}$	$\frac{5.1}{28}$	$\frac{9.7}{21}$	$\frac{9.7}{17}$	$\frac{7.7}{13}$	$\frac{7.6}{75}$	$\frac{7.6}{13}$	$\frac{9.4}{17}$	$\frac{9.4}{21}$	$\frac{4.4}{29}$	$\frac{4.4}{40}$

✓
936.51

14

+50

15

+50

16

+50

17

T.P.

9.55

✓
945.65

0.43

✓
936.08

936.10

+50

18

+50

19

+50

LEFT $\pm$ RIGHT

$\frac{4.7}{40}$	$\frac{4.3}{27}$	$\frac{8.7}{21}$	$\frac{8.7}{17}$	$\frac{6.6}{13}$	$\frac{6.6}{6.4}$	$\frac{6.6}{13}$	$\frac{8.6}{17}$	$\frac{8.6}{21}$	$\frac{4.3}{28}$	$\frac{4.5}{40}$
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$\frac{6.2}{40}$	$\frac{5.6}{24}$	$\frac{7.7}{21}$	$\frac{7.7}{17}$	$\frac{5.6}{13}$	$\frac{5.6}{5.5}$	$\frac{5.6}{13}$	$\frac{7.6}{17}$	$\frac{7.6}{21}$	$\frac{4.9}{26}$	$\frac{4.6}{40}$
------------------	------------------	------------------	------------------	------------------	-------------------	------------------	------------------	------------------	------------------	------------------

$\frac{8.4}{40}$	$\frac{7.2}{18}$	$\frac{4.5}{13}$	$\frac{4.7}{4.4}$	$\frac{4.4}{13}$	$\frac{7.2}{19}$	$\frac{7.3}{40}$
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$\frac{7.7}{40}$	$\frac{7.2}{20}$	$\frac{3.5}{13}$	$\frac{3.8}{3.5}$	$\frac{3.5}{13}$	$\frac{6.0}{18}$	$\frac{5.6}{40}$
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$\frac{5.4}{40}$	$\frac{5.0}{18}$	$\frac{2.4}{13}$	$\frac{2.7}{2.4}$	$\frac{2.5}{13}$	$\frac{4.4}{18}$	$\frac{4.4}{21}$	$\frac{4.2}{22}$	$\frac{3.6}{40}$
------------------	------------------	------------------	-------------------	------------------	------------------	------------------	------------------	------------------

$\frac{3.5}{40}$	$\frac{3.8}{18}$	$\frac{1.3}{13}$	$\frac{1.3}{1.1}$	$\frac{1.3}{13}$	$\frac{3.9}{18}$	$\frac{4.0}{40}$
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$\frac{4.4}{40}$	$\frac{4.8}{22}$	$\frac{0.4}{13}$	$\frac{0.6}{0.2}$	$\frac{0.4}{13}$	$\frac{5.5}{23}$	$\frac{5.5}{40}$
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Spt in 15" Oak 200' R+

$\frac{11.1}{40}$	$\frac{11.5}{20}$	$\frac{8.5}{13}$	$\frac{17+10}{8.4}$	$\frac{12.1}{20}$	$\frac{12.1}{40}$
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$\frac{5.8}{40}$	$\frac{6.0}{27}$	$\frac{9.4}{21}$	$\frac{9.5}{17}$	$\frac{7.5}{13}$	$\frac{7.3}{7.3}$	$\frac{7.6}{13}$	$\frac{9.9}{17}$	$\frac{9.7}{21}$	$\frac{7.0}{25}$	$\frac{8.2}{40}$
------------------	------------------	------------------	------------------	------------------	-------------------	------------------	------------------	------------------	------------------	------------------

$\frac{1.9}{40}$	$\frac{1.9}{31}$	$\frac{8.3}{21}$	$\frac{8.4}{17}$	$\frac{6.4}{13}$	$\frac{6.2}{6.2}$	$\frac{6.5}{13}$	$\frac{8.6}{17}$	$\frac{8.5}{21}$	$\frac{3.3}{29}$	$\frac{3.9}{40}$
------------------	------------------	------------------	------------------	------------------	-------------------	------------------	------------------	------------------	------------------	------------------

$\frac{1.4}{40}$	$\frac{1.2}{31}$	$\frac{7.4}{22}$	$\frac{7.5}{18}$	$\frac{5.5}{13}$	$\frac{5.3}{5.3}$	$\frac{5.4}{13}$	$\frac{7.5}{17}$	$\frac{7.4}{21}$	$\frac{3.1}{28}$	$\frac{3.9}{40}$
------------------	------------------	------------------	------------------	------------------	-------------------	------------------	------------------	------------------	------------------	------------------

$\frac{3.1}{40}$	$\frac{3.5}{26}$	$\frac{6.8}{21}$	$\frac{6.8}{17}$	$\frac{4.7}{13}$	$\frac{4.4}{4.4}$	$\frac{4.7}{13}$	$\frac{6.7}{17}$	$\frac{6.6}{21}$	$\frac{4.4}{25}$	$\frac{4.5}{40}$
------------------	------------------	------------------	------------------	------------------	-------------------	------------------	------------------	------------------	------------------	------------------

✓
945.65

+92

20

+10

+50

21

+50

22

+50

23

T.P.

3.33

✓
942.60

6.38

✓
939.27

+50

24

+50

L

E

R.

$\frac{4.5}{40}$	$\frac{5.0}{23}$	$\frac{6.1}{21}$	$\frac{6.3}{17}$	$\frac{4.5}{13}$	$\frac{4.5}{43}$	$\frac{4.3}{13}$	$\frac{6.1}{17}$	$\frac{6.2}{21}$	$\frac{4.6}{24}$	$\frac{4.8}{40}$
			$\frac{4.5}{40}$	$\frac{4.5}{13}$	$\frac{4.5}{43}$	$\frac{4.4}{13}$	$\frac{4.1}{40}$			
$\frac{4.9}{40}$	$\frac{5.3}{24}$	$\frac{6.1}{22}$	$\frac{6.1}{18}$	$\frac{4.5}{13}$	$\frac{4.6}{44}$	$\frac{4.3}{13}$	$\frac{6.1}{17}$	$\frac{6.1}{21}$	$\frac{4.5}{23}$	$\frac{4.4}{40}$
$\frac{3.4}{40}$	$\frac{4.1}{25}$	$\frac{6.6}{21}$	$\frac{6.6}{17}$	$\frac{4.6}{13}$	$\frac{4.7}{45}$	$\frac{4.6}{13}$	$\frac{6.7}{17}$	$\frac{6.6}{21}$	$\frac{4.0}{25}$	$\frac{4.3}{40}$
$\frac{3.7}{40}$	$\frac{3.7}{27}$	$\frac{6.8}{21}$	$\frac{7.0}{17}$	$\frac{5.0}{13}$	$\frac{5.0}{48}$	$\frac{5.1}{13}$	$\frac{7.3}{17}$	$\frac{7.2}{21}$	$\frac{4.5}{25}$	$\frac{4.4}{40}$
$\frac{4.6}{40}$	$\frac{3.8}{27}$	$\frac{7.3}{21}$	$\frac{7.2}{17}$	$\frac{5.3}{13}$	$\frac{5.3}{50}$	$\frac{5.2}{13}$	$\frac{7.2}{17}$	$\frac{7.2}{21}$	$\frac{3.2}{28}$	$\frac{3.1}{40}$
$\frac{4.5}{40}$	$\frac{4.2}{27}$	$\frac{7.6}{21}$	$\frac{7.6}{17}$	$\frac{5.6}{13}$	$\frac{5.6}{54}$	$\frac{5.5}{13}$	$\frac{7.5}{17}$	$\frac{7.5}{21}$	$\frac{4.2}{27}$	$\frac{4.2}{40}$
$\frac{4.4}{40}$	$\frac{3.9}{28}$	$\frac{7.7}{21}$	$\frac{7.8}{17}$	$\frac{5.9}{13}$	$\frac{5.9}{56}$	$\frac{5.9}{13}$	$\frac{8.0}{17}$	$\frac{7.8}{21}$	$\frac{3.7}{28}$	$\frac{3.8}{40}$
$\frac{5.8}{40}$	$\frac{5.8}{25}$	$\frac{8.2}{21}$	$\frac{8.3}{17}$	$\frac{6.2}{13}$	$\frac{6.2}{60}$	$\frac{6.2}{13}$	$\frac{8.1}{17}$	$\frac{8.0}{21}$	$\frac{5.0}{26}$	$\frac{5.3}{40}$
$\frac{4.9}{40}$	$\frac{4.2}{24}$	$\frac{5.5}{21}$	$\frac{5.5}{17}$	$\frac{3.5}{13}$	$\frac{3.4}{33}$	$\frac{3.3}{13}$	$\frac{5.3}{17}$	$\frac{5.4}{21}$	$\frac{3.6}{24}$	$\frac{4.2}{40}$
		$\frac{6.4}{40}$	$\frac{6.5}{20}$	$\frac{3.8}{13}$	$\frac{3.7}{35}$	$\frac{3.7}{13}$	$\frac{5.8}{18}$	$\frac{5.8}{21}$	$\frac{5.3}{24}$	$\frac{6.0}{40}$
$\frac{5.4}{40}$	$\frac{5.5}{22}$	$\frac{6.1}{21}$	$\frac{6.0}{17}$	$\frac{4.1}{13}$	$\frac{4.0}{38}$	$\frac{4.1}{13}$	$\frac{7.0}{19}$	$\frac{7.4}{40}$		

✓
942.60

25 +50

+50

26

+50

27

+50

28

+50

29

+50

T.P.

7.31

✓
941.68

8.23

✓
934.37

30

+50

Lt

±

Rt.

$$\begin{array}{ccccccccc} \frac{5.6}{40} & \frac{5.4}{22} & \frac{6.4}{21} & \frac{6.4}{17} & \frac{4.3}{13} & \begin{array}{c} 4.3 \\ 4.2 \end{array} & \frac{4.4}{13} & \frac{6.5}{17} & \frac{6.5}{21} & \frac{5.7}{23} & \frac{6.3}{40} \end{array}$$

$$\begin{array}{ccccccccc} \frac{5.5}{40} & \frac{5.3}{23} & \frac{6.7}{21} & \frac{6.6}{17} & \frac{4.7}{13} & \begin{array}{c} 4.6 \\ 4.5 \end{array} & \frac{4.6}{13} & \frac{6.7}{17} & \frac{6.6}{21} & \frac{5.4}{23} & \frac{5.8}{40} \end{array}$$

$$\begin{array}{ccccccccc} \frac{6.0}{40} & \frac{5.9}{23} & \frac{7.0}{21} & \frac{7.0}{17} & \frac{4.9}{13} & \begin{array}{c} 4.9 \\ 4.8 \end{array} & \frac{4.9}{13} & \frac{6.9}{17} & \frac{6.8}{21} & \frac{5.8}{23} & \frac{5.9}{40} \end{array}$$

$$\begin{array}{ccccccccc} \frac{6.0}{40} & \frac{5.7}{23} & \frac{7.2}{21} & \frac{7.3}{17} & \frac{5.2}{13} & \begin{array}{c} 5.2 \\ 5.1 \end{array} & \frac{5.2}{13} & \frac{7.3}{17} & \frac{7.3}{21} & \frac{5.7}{24} & \frac{5.8}{40} \end{array}$$

$$\begin{array}{ccccccccc} \frac{6.1}{40} & \frac{5.6}{24} & \frac{7.5}{21} & \frac{7.5}{17} & \frac{5.5}{13} & \begin{array}{c} 5.5 \\ 5.6 \end{array} & \frac{5.6}{13} & \frac{7.5}{17} & \frac{7.5}{21} & \frac{5.1}{25} & \frac{5.5}{40} \end{array}$$

$$\begin{array}{ccccccccc} \frac{5.4}{40} & \frac{5.4}{25} & \frac{7.8}{21} & \frac{7.8}{17} & \frac{5.8}{13} & \begin{array}{c} 5.8 \\ 5.8 \end{array} & \frac{5.8}{13} & \frac{7.8}{17} & \frac{7.8}{21} & \frac{4.8}{26} & \frac{5.2}{40} \end{array}$$

$$\begin{array}{ccccccccc} \frac{4.9}{40} & \frac{5.2}{25} & \frac{8.0}{21} & \frac{8.0}{17} & \frac{6.0}{13} & \begin{array}{c} 6.1 \\ 6.0 \end{array} & \frac{6.0}{13} & \frac{8.0}{17} & \frac{8.0}{21} & \frac{4.7}{27} & \frac{4.7}{40} \end{array}$$

$$\begin{array}{ccccccccc} \frac{4.9}{40} & \frac{4.9}{26} & \frac{8.5}{21} & \frac{8.5}{17} & \frac{6.5}{13} & \begin{array}{c} 6.4 \\ 6.3 \end{array} & \frac{6.4}{13} & \frac{8.2}{17} & \frac{8.2}{21} & \frac{4.4}{27} & \frac{4.8}{40} \end{array}$$

$$\begin{array}{ccccccccc} \frac{4.4}{40} & \frac{4.3}{28} & \frac{8.7}{21} & \frac{8.7}{17} & \frac{6.8}{13} & \begin{array}{c} 6.7 \\ 6.7 \end{array} & \frac{6.8}{13} & \frac{8.8}{17} & \frac{8.8}{21} & \frac{4.1}{28} & \frac{4.4}{40} \end{array}$$

$$\begin{array}{ccccccccc} \frac{6.4}{40} & \frac{6.5}{26} & \frac{9.2}{21} & \frac{9.2}{17} & \frac{7.2}{13} & \begin{array}{c} 7.0 \\ 6.9 \end{array} & \frac{7.2}{13} & \frac{9.2}{18} & \frac{9.2}{21} & \frac{5.5}{26} & \frac{5.8}{40} \end{array}$$

$$\begin{array}{ccccccccc} \frac{8.0}{40} & \frac{7.9}{22} & \frac{8.7}{21} & \frac{8.6}{18} & \frac{6.5}{13} & \begin{array}{c} 6.4 \\ 6.2 \end{array} & \frac{6.6}{13} & \frac{8.5}{17} & \frac{8.5}{21} & \frac{7.4}{23} & \frac{7.5}{40} \end{array}$$

$$\begin{array}{ccccccc} \frac{11.2}{40} & \frac{11.1}{23} & \frac{6.6}{13} & \begin{array}{c} 6.5 \\ 6.5 \end{array} & \frac{6.5}{13} & \frac{10.4}{22} & \frac{10.2}{40} \end{array}$$

Sta

941.68 ✓

31

+41

32

+50

33

+22

+32

+40

+53.6

B.M.

E. W. B. Ave Pavement ✓

0.54 941.14 941.17

Left

X

RIGHT

$$\frac{10.5}{40} \quad \frac{11.0}{23} \quad \frac{6.4}{13} \quad \frac{6.2}{62} \quad \frac{6.4}{13} \quad \frac{10.9}{23} \quad \frac{10.3}{40}$$

$$\frac{7.3}{40} \quad \frac{8.1}{24} \quad \frac{8.7}{23} \quad \frac{8.7}{19} \quad \frac{5.8}{13} \quad \frac{5.5}{5.9} \quad \frac{5.8}{13} \quad \frac{8.1}{18} \quad \frac{8.0}{23} \quad \frac{7.6}{25} \quad \frac{7.7}{40}$$

$$\frac{3.0}{40} \quad \frac{3.4}{26} \quad \frac{6.6}{21} \quad \frac{6.5}{18} \quad \frac{4.5}{13} \quad \frac{4.4}{4.7} \quad \frac{4.4}{13} \quad \frac{6.5}{17} \quad \frac{6.4}{21} \quad \frac{3.4}{26} \quad \frac{3.3}{40}$$

$$\frac{1.2}{40} \quad \frac{1.0}{27} \quad \frac{5.0}{21} \quad \frac{5.0}{17} \quad \frac{3.1}{13} \quad \frac{3.1}{3.1} \quad \frac{3.1}{13} \quad \frac{5.1}{17} \quad \frac{5.1}{21} \quad \frac{1.7}{26} \quad \frac{1.7}{40}$$

$$\frac{1.0}{40} \quad \frac{0.7}{26} \quad \frac{3.8}{21} \quad \frac{3.8}{17} \quad \frac{1.8}{13} \quad \frac{1.8}{1.9} \quad \frac{1.8}{13} \quad \frac{3.9}{17} \quad \frac{4.0}{21} \quad \frac{1.4}{26} \quad \frac{1.3}{40}$$

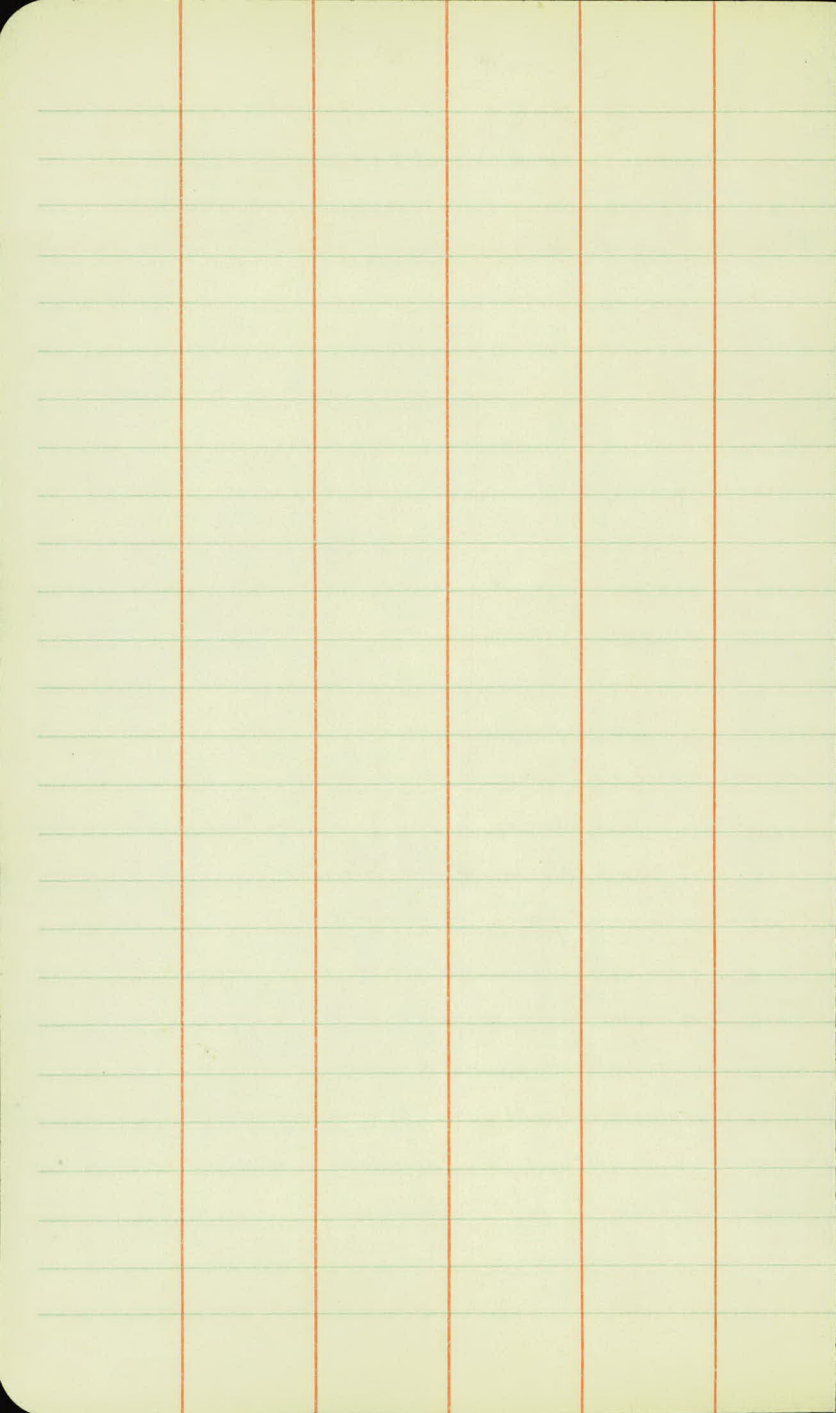
$$\frac{0.6}{40} \quad \frac{0.5}{26} \quad \frac{2.8}{22} \quad \frac{2.9}{19} \quad \frac{1.2}{14} \quad \frac{1.2}{1.3} \quad \frac{1.3}{14} \quad \frac{2.8}{19} \quad \frac{2.7}{22} \quad \frac{2.2}{27} \quad \frac{1.0}{40} \quad + 2 \text{ over H.I.}$$

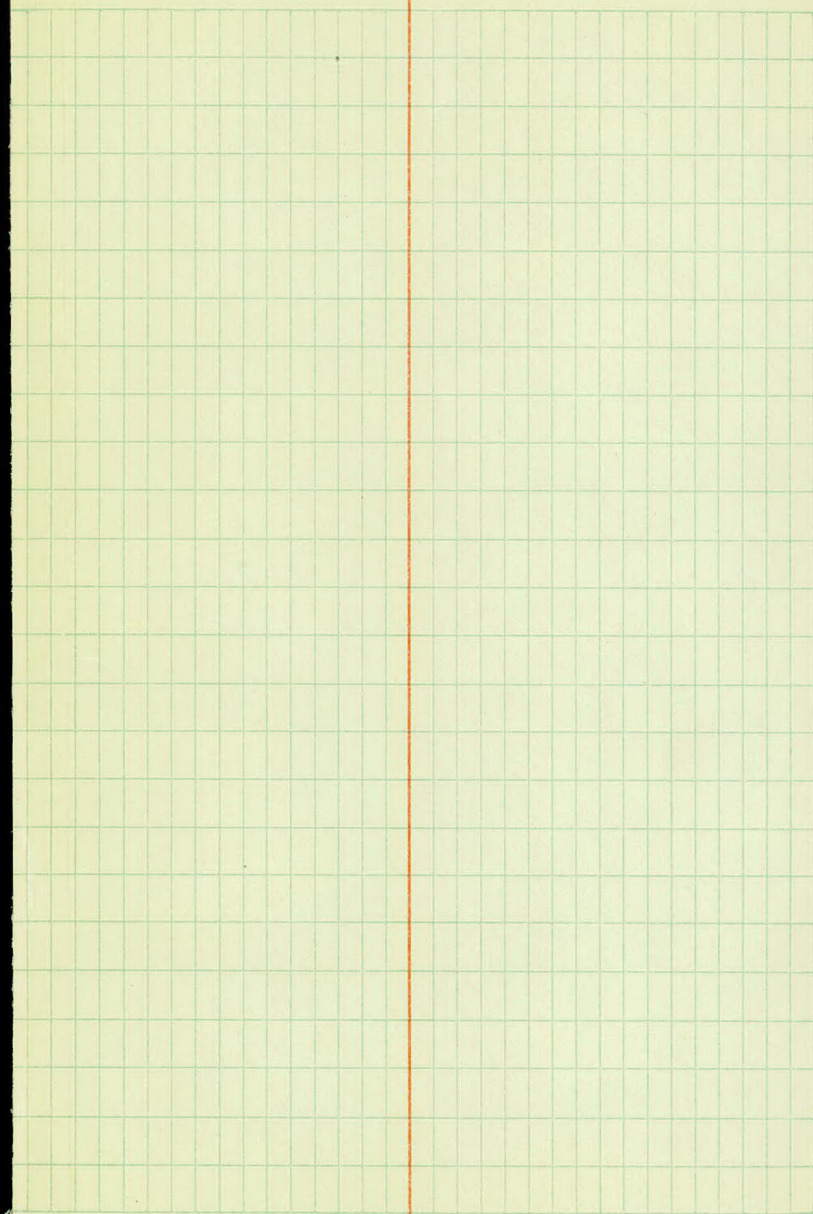
$$\frac{2.3}{40} \quad \frac{2.3}{26} \quad \frac{0.7}{20} \quad \frac{1.0}{1.0} \quad \frac{1.1}{19} \quad \frac{1.6}{22} \quad \frac{1.0}{30} \quad \frac{0.6}{34} \quad \frac{0.6}{40}$$

$$\frac{0.6}{40} \quad \frac{0.6}{20} \quad 0.8 \quad \frac{0.8}{20} \quad \frac{0.5}{40}$$

$$\frac{0.4}{40} \quad \frac{0.4}{20} \quad 0.54 \quad \frac{0.6}{20} \quad \frac{0.7}{40}$$

Brass plug in Pave. W.B. Ave + "F"





T.P.	1.09	938.75	937.66
		930.10	930.10
		8.65	8.65
30+73	18" X 42' P3	21' Lt.	21' Rt.
		Grade	1' Down
		10' O.S.	10' O.S.

T.P.	6.15	930.46	924.31
		923.20	923.40
		7.26	7.06
11+36	18" X 36' P3	18' Lt.	18' Rt.
		Grade	Grade
		10' O.S.	10' O.S.

B.M.	0.95	932.13	931.18
		924.80	925.90
		7.33	6.23
6+00	18" X 36' P3	19' Lt.	17' Rt.
		Grade	4' Down
		10' O.S.	10' O.S.

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.

ROADWAY 14 FEET WIDE. SIDE SLOPES 1½ TO 1.

FOR SINGLE TRACK EMBANKMENT.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	7.0	7.2	7.3	7.5	7.6	7.8	7.9	8.1	8.2	8.4	0
1	8.5	8.7	8.8	9.0	9.1	9.3	9.4	9.6	9.7	9.9	1
2	10.0	10.2	10.3	10.5	10.6	10.8	10.9	11.1	11.2	11.4	2
3	11.5	11.7	11.8	12.0	12.1	12.3	12.4	12.6	12.7	12.9	3
4	13.0	13.2	13.3	13.5	13.6	13.8	13.9	14.1	14.2	14.4	4
5	14.5	14.7	14.8	15.0	15.1	15.3	15.4	15.6	15.7	15.9	5
6	16.0	16.2	16.3	16.5	16.6	16.8	16.9	17.1	17.2	17.4	6
7	17.5	17.7	17.8	18.0	18.1	18.3	18.4	18.6	18.7	18.9	7
8	19.0	19.2	19.3	19.5	19.6	19.8	19.9	20.1	20.2	20.4	8
9	20.5	20.7	20.8	21.0	21.1	21.3	21.4	21.6	21.7	21.9	9
10	22.0	22.2	22.3	22.5	22.6	22.8	22.9	23.1	23.2	23.4	10
11	23.5	23.7	23.8	24.0	24.1	24.3	24.4	24.6	24.7	24.9	11
12	25.0	25.2	25.3	25.5	25.6	25.8	25.9	26.1	26.2	26.4	12
13	26.5	26.7	26.8	27.0	27.1	27.3	27.4	27.6	27.7	27.9	13
14	28.0	28.2	28.3	28.5	28.6	28.8	28.9	29.1	29.2	29.4	14
15	29.5	29.7	29.8	30.0	30.1	30.3	30.4	30.6	30.7	30.9	15
16	31.0	31.2	31.3	31.5	31.6	31.8	31.9	32.1	32.2	32.4	16
17	32.5	32.7	32.8	33.0	33.1	33.3	33.4	33.6	33.7	33.9	17
18	34.0	34.2	34.3	34.5	34.6	34.8	34.9	35.1	35.2	35.4	18
19	35.5	35.7	35.8	36.0	36.1	36.3	36.4	36.6	36.7	36.9	19
20	37.0	37.2	37.3	37.5	37.6	37.8	37.9	38.1	38.2	38.4	20
21	38.5	38.7	38.8	39.0	39.1	39.3	39.4	39.6	39.7	39.9	21
22	40.0	40.2	40.3	40.5	40.6	40.8	40.9	41.1	41.2	41.4	22
23	41.5	41.7	41.8	42.0	42.1	42.3	42.4	42.6	42.7	42.9	23
24	43.0	43.2	43.3	43.5	43.6	43.8	43.9	44.1	44.2	44.4	24
25	44.5	44.7	44.8	45.0	45.1	45.3	45.4	45.6	45.7	45.9	25
26	46.0	46.2	46.3	46.5	46.6	46.8	46.9	47.1	47.2	47.4	26
27	47.5	47.7	47.8	48.0	48.1	48.3	48.4	48.6	48.7	48.9	27
28	49.0	49.2	49.3	49.5	49.6	49.8	49.9	50.1	50.2	50.4	28
29	50.5	50.7	50.8	51.0	51.1	51.3	51.4	51.6	51.7	51.9	29
30	52.0	52.2	52.3	52.5	52.6	52.8	52.9	53.1	53.2	53.4	30
31	53.5	53.7	53.8	54.0	54.1	54.3	54.4	54.6	54.7	54.9	31
32	55.0	55.2	55.3	55.5	55.6	55.8	55.9	56.1	56.2	56.4	32
33	56.5	56.7	56.8	57.0	57.1	57.3	57.4	57.6	57.7	57.9	33
34	58.0	58.2	58.3	58.5	58.6	58.8	58.9	59.1	59.2	59.4	34
35	59.5	59.7	59.8	60.0	60.1	60.3	60.4	60.6	60.7	60.9	35
36	61.0	61.2	61.3	61.5	61.6	61.8	61.9	62.1	62.2	62.4	36

Calculated by Julien A. Hall, M. Am. Soc. C. E.

MADE IN GERMANY.

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