

Book- 9, Dr. 12

X

OFFICE OF COUNTY ENGINEER
RAMSEY CO. MINN.

PLAN Survey

Ash St.

COUNTY RD. "F"

From S.T.H. 61 To White Bear Ave

Road Acc't. No. 33-N.4

Date Filed.....

File.....

Alignment

33-W4

33+53.60 E W. B. Ave

19+29.10 P.O.T.

7+25.85 P.O.T.

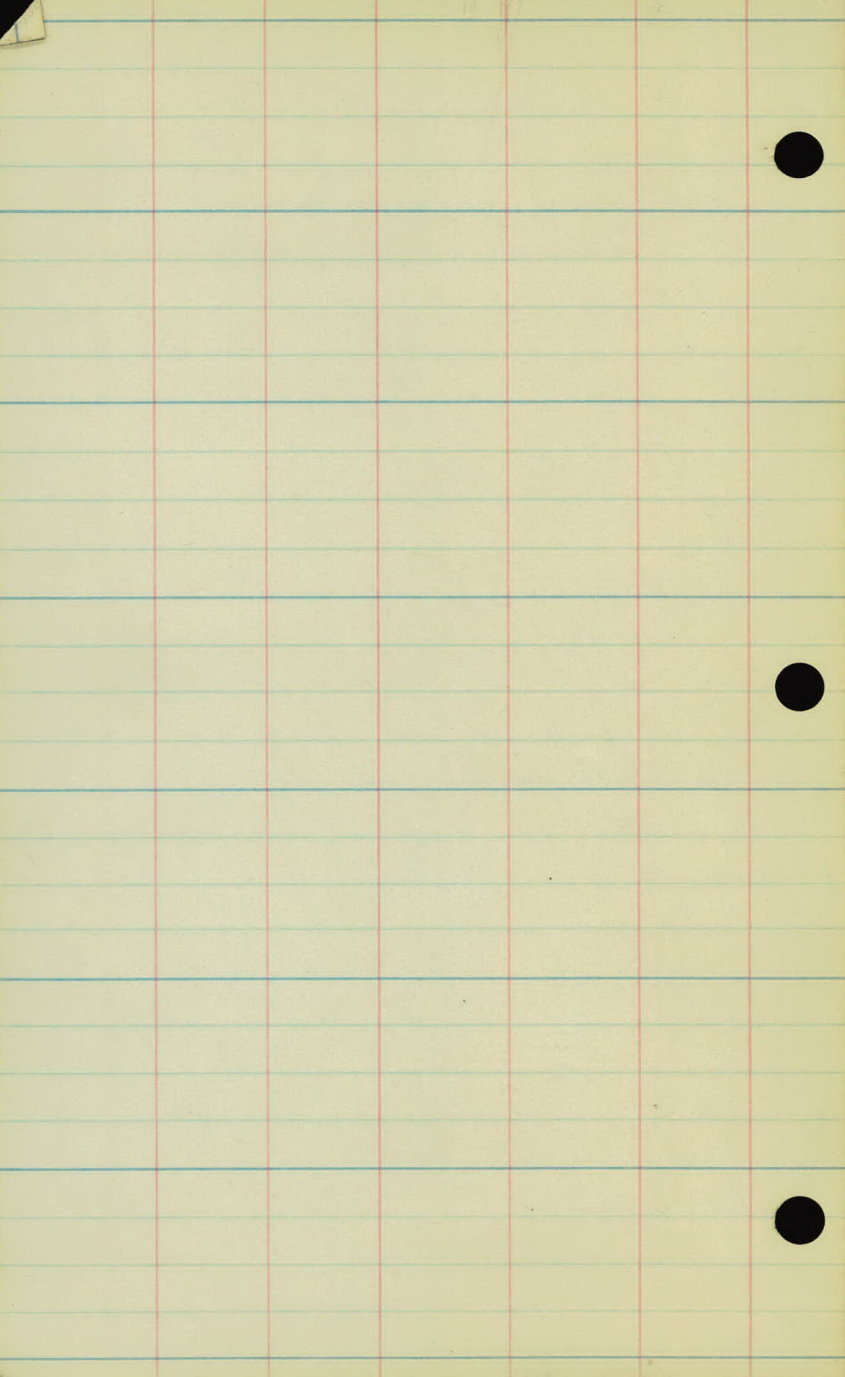
0+00 E S.T.H. #1

8" Elm @ 40.50 — Iron Mont. $5\frac{1}{4}$ Cor
 Iron Rel. Sq. @ 40.42 — Sec. 23

12" Elm @ 43.0 — Spt.
 10" Elm @ 49.87

18" Oak @ 57.03 — 10" Oak @ 66.16
 Mont. SW Cor 23
 30-22

T.P. @ 59.62 — Nail in Pavement
 19.48 — P.P.



Topog.

33-W4

5

4

3

2

1

0+00

+89-P.P.28'

+42-Rd Sq. 18'
+38-P.P.29'

+00-P.P.30'

+52-T.P.30'
+40-St. Sq. 26
£ S.T.H. #1

Cult.

Cult.

Orchard

Pasture

+49-T.P.19'

+08-F. Int.

+43-FC. 23'

+30-£ D.R.

+05-T.P.21'

+33-T.P.22'

+89-T.P.23'

12

11

10

9

8

7

6

+67-T. 29'

F. 33'

+76-Sq. 14'

+36-12"X26'C.M.

F. 33'

+64-F. Int.

F. 33'

+27-T. 30'

+67-F. 33'

+02-T. 30'

+42-P.P. 27'

+92-E Dr.

+79-T. 30'

+46-12"X32'C.M.

+35-P.P. 27'

Pasture

Cult.

Cult.

+71-T. 18'

+52-T.P. 16'

+04-T.P. 16'

+27-T. 18'

+44-T.P. 17'

+35-T. 24'

+03-T. 18'

+74-T. 24'

+67-T. 31'

+60-T. 30'

+42-T.P. 18'

+25-85-E Linden Ave

+91-F.C. 23'

F. 27'

Yard

Yard

19

18

17

16

15

14

13

F. 33'

+45-T. 27'

F. 33'

+61-T. 28'

+19-T. 28'

F. 33'

+80-T. 27'

+37-T. 28'

F. 33'

+96-T. 28'

+16-T. 29'

F. 33'

+74-T. 28'

F. 33'

+48-T. 28'

F. 33'

Cult.

+74-T.P. 15'
+66-T. 20'

+83-T. 21'

+50-F.C. 26'

+11-T.P. 15'
+01-T. 21'
F. 25'

+75-F.E.

+83-F.C. 25'

+52-T.P. 15'

+20-T. 20'

+81-T.P. 15'

+37-T. 19'

+95-T. 18'

+54-T. 19'

+25-T.P. 15'

Pasture

Cult.

26

25

24

23

22

21

20

+87-T.23'

+45-T.23'
+43-T.P.16'

+70-T.25'

+60-T.23'

+20-T.23'

+82-T.P.15'
+79-T.22'

+04-T.26'

Cult

Cult

+12-T.P.15'

+50-T.P.15'

+06-T.21'

+74-T.26'

+33-T.26'
+27-F.C.33'-P.P.33'



{10"X30' C.M. 14'
+01-E Highland Ave

33

32

31

30

29

28

27

+53.6 @ W.B. Ave

+23 - Rd. Sq. 26'

+75 - T. 24'

+91 - T. 24'

+50 - T. 25'

+09 - T. 25'

+71 - 12" x 32' C.M.

+69 - T. 25'

+26 - T. 25'

+99 - T. 26'

+57 - T. 26'

+75 - T. 26'

+54 - T. 26'

+26 - T.P. 19'
+25 - S + Sq. 18'

+68 - T. 23'
+58 - T.P. 16'

+26 - T. 24'

+40 - T.P. 17'

+02 - T. 24'

17 15'

Cut

Cut

+29 - Rd. Sq. 15'

+77 - T. 25'
+73 - T.P. 17'

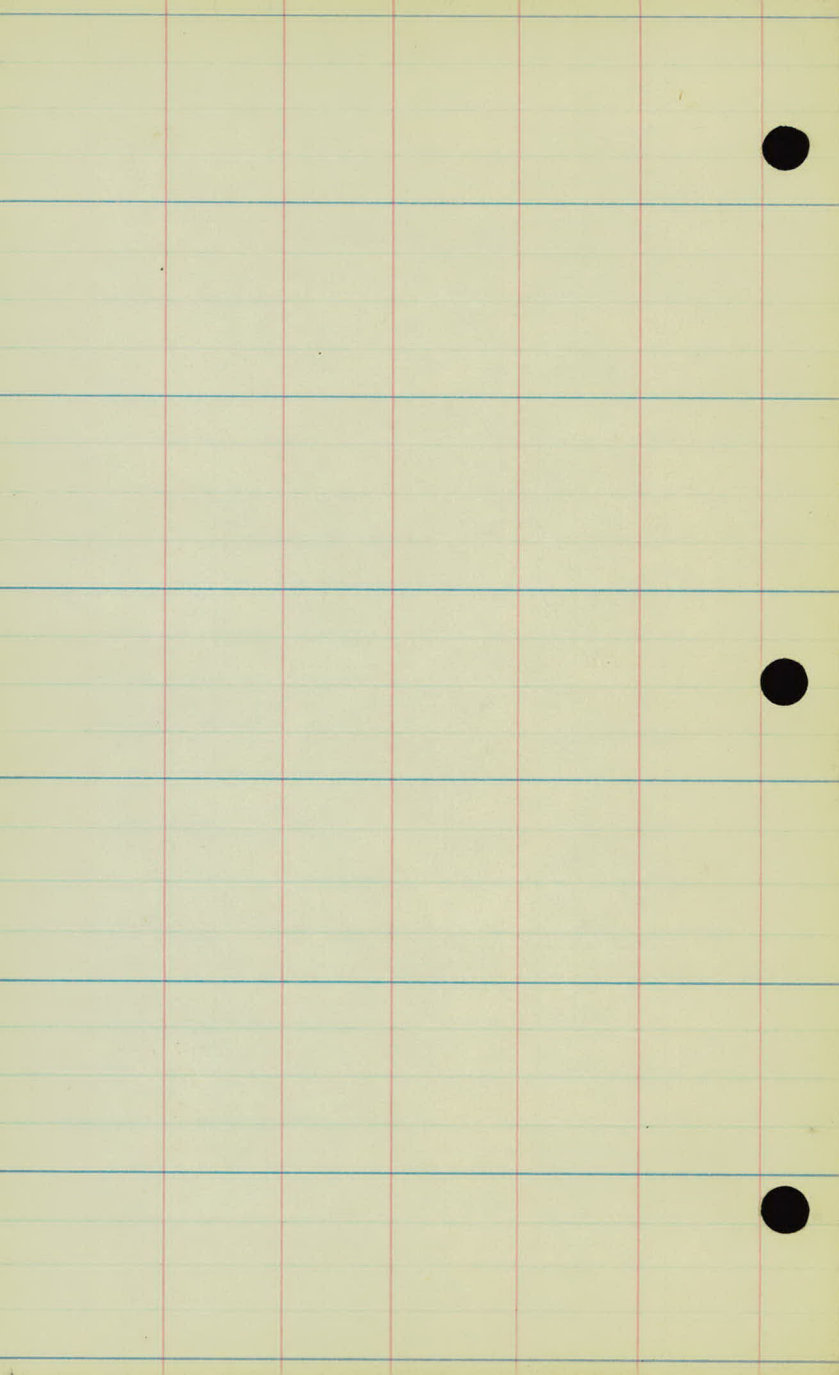
+28 - T. 24'

+53 - T. 24'

+08 - T.P. 14'

+70 - T. 23'

+27 - T. 23'



X-Sections

33-W4

B.M. 6.57 936.37

929.80

0+00 $\pm$ S.T.H. #1

29.5

+12

29.4

+25

29.2

+37

29.3

+50

29.6

1

30.4

+50

31.7

2

32.6

+20

32.5

+60

31.9

3

31.1

+20

30.6

+70

29.7

Spk. in P.P. 1' Lt. 0-23

$$\frac{7.1}{40} \quad 6.9 \quad \frac{6.8}{40}$$

$$\frac{7.0}{40} \quad 7.0 \quad \frac{7.3 \ 6.8}{16 \ 21} \quad \frac{7.0}{38}$$

$$\frac{7.5}{40} \quad \frac{7.3}{22} \quad 7.2 \quad \frac{7.8 \ 11.0}{11 \ 17} \quad \frac{12.4}{40}$$

$$\frac{8.6}{40} \quad \frac{8.4}{35} \quad \frac{7.6}{24} \quad 7.1 \quad \frac{7.0 \ 8.4}{4 \ 12} \quad \frac{11.0}{18} \quad \frac{12.5}{40}$$

$$\frac{7.5}{40} \quad \frac{7.7}{24} \quad \frac{7.2}{19} \quad \frac{6.7}{9} \quad 6.8 \quad \frac{7.3 \ 8.1}{6 \ 12} \quad \frac{11.2}{18} \quad \frac{12.2}{40}$$

$$\frac{5.6}{40} \quad \frac{5.7}{21} \quad \frac{6.0}{14} \quad \frac{5.6}{7} \quad 6.0 \quad \frac{6.2 \ 7.4}{8 \ 14} \quad \frac{10.1}{40}$$

$$\frac{2.4}{40} \quad \frac{2.4}{22} \quad \frac{3.7}{17} \quad \frac{4.6}{12} \quad \frac{4.5}{5} \quad 4.7 \quad \frac{4.7 \ 3.7}{2 \ 9} \quad \frac{6.8}{40}$$

$$\frac{1.4}{40} \quad \frac{1.0}{22} \quad \frac{3.0}{16} \quad \frac{3.9}{11} \quad \frac{3.7}{5} \quad 3.8 \quad \frac{3.8 \ 3.0}{4 \ 6} \quad \frac{1.1}{9} \quad \frac{1.2}{40}$$

$$\frac{2.5}{40} \quad \frac{1.6}{22} \quad \frac{2.0}{19} \quad \frac{4.0}{12} \quad \frac{3.8}{5} \quad 3.9 \quad \frac{4.0 \ 3.0}{3 \ 8} \quad \frac{1.8}{9} \quad \frac{1.0}{12} \quad \frac{0.0}{40}$$

$$\frac{6.0}{40} \quad \frac{4.6}{17} \quad \frac{4.3}{13} \quad \frac{4.7}{10} \quad 4.5 \quad \frac{4.6 \ 4.2}{4 \ 8} \quad \frac{3.2}{11} \quad \frac{3.2}{23} \quad \frac{2.2}{40}$$

$$\frac{9.4}{40} \quad \frac{8.2}{19} \quad \frac{5.5}{13} \quad \frac{5.5}{10} \quad 5.3 \quad \frac{5.5 \ 5.5}{4 \ 9} \quad \frac{5.0}{11} \quad \frac{5.5}{15} \quad \frac{5.0}{40}$$

$$\frac{10.0}{40} \quad \frac{9.8}{28} \quad \frac{8.8}{18} \quad \frac{5.8}{11} \quad 5.8 \quad \frac{6.0 \ 6.0}{4 \ 8} \quad \frac{5.2}{12} \quad \frac{6.0}{19} \quad \frac{6.0}{30} \quad \frac{5.4}{40}$$

$$\frac{8.2}{40} \quad \frac{6.8}{16} \quad \frac{6.6}{11} \quad \frac{7.0}{9} \quad 6.7 \quad \frac{7.0 \ 6.6}{5 \ 7} \quad \frac{6.6}{9} \quad \frac{5.3}{12} \quad \frac{5.7}{15} \quad \frac{5.4}{40}$$

936.37

4

29.2

+20

28.8

+27

28.6

+35

28.4

+42

28.3

5

27.4

T.P.

5.50

933.63

8.24

928.13

+50

27.3

6

27.0

+32

27.3

+50

27.5

+65

27.6

7

27.8

+35

28.2

$$\frac{8.2}{40} \quad \frac{7.0}{15} \quad \frac{7.4}{8} \quad 7.2 \quad \frac{7.3}{5} \quad \frac{7.2}{10} \quad \frac{5.5}{14} \quad \frac{5.8}{22} \quad \frac{5.2}{40}$$

$$\frac{2.0}{40} \quad \frac{8.2}{18} \quad \frac{7.6}{11} \quad \frac{7.8}{9} \quad 7.6 \quad \frac{7.8}{15} \quad \frac{6.2}{16} \quad \frac{5.2}{20} \quad \frac{4.8}{40}$$

$$\frac{2.4}{40} \quad \frac{8.4}{17} \quad \frac{7.8}{10} \quad \frac{8.0}{8} \quad 7.8 \quad \frac{8.0}{6} \quad \frac{7.7}{9} \quad \frac{8.0}{25} \quad \frac{7.6}{40}$$

$$\frac{2.8}{40} \quad \frac{8.8}{17} \quad \frac{7.9}{10} \quad \frac{8.2}{8} \quad 8.0 \quad \frac{8.2}{6} \quad \frac{7.8}{9} \quad \frac{8.0}{28} \quad \frac{7.7}{40}$$

$$\frac{10.2}{40} \quad \frac{7.5}{18} \quad \frac{8.1}{10} \quad \frac{8.5}{8} \quad 8.1 \quad \frac{8.4}{6} \quad \frac{8.0}{9} \quad \frac{7.5}{15} \quad \frac{6.5}{18} \quad \frac{5.5}{26} \quad \frac{5.5}{40}$$

$$\frac{13.0}{40} \quad \frac{12.0}{17} \quad \frac{9.3}{12} \quad \frac{9.2}{8} \quad 9.0 \quad \frac{9.0}{6} \quad \frac{8.8}{8} \quad \frac{9.5}{11} \quad \frac{8.2}{15} \quad \frac{5.7}{32} \quad \frac{5.5}{40}$$

$$\frac{10.3}{40} \quad \frac{9.3}{19} \quad \frac{6.6}{10} \quad 6.3 \quad \frac{6.4}{6} \quad \frac{7.1}{7} \quad \frac{5.3}{14} \quad \frac{3.0}{35} \quad \frac{2.8}{40}$$

$$\frac{10.0}{40} \quad \frac{8.8}{18} \quad \frac{6.8}{10} \quad 6.6 \quad \frac{6.4}{8} \quad \frac{7.1}{11} \quad \frac{6.0}{13} \quad \frac{5.0}{18} \quad \frac{3.2}{40}$$

$$\frac{9.2}{40} \quad \frac{8.5}{16} \quad \frac{6.6}{10} \quad 6.3 \quad \frac{6.4}{7} \quad \frac{7.0}{11} \quad \frac{6.0}{13} \quad \frac{5.0}{28} \quad \frac{3.8}{40}$$

$$\frac{6.7}{40} \quad \frac{6.7}{29} \quad \frac{6.2}{9} \quad 6.1 \quad \frac{6.3}{7} \quad \frac{7.0}{11} \quad \frac{5.0}{30} \quad \frac{4.0}{40}$$

$$\frac{7.0}{40} \quad \frac{7.4}{19} \quad \frac{6.4}{10} \quad 6.0 \quad \frac{6.2}{7} \quad \frac{7.4}{14} \quad \frac{5.7}{31} \quad \frac{4.8}{40}$$

$$\frac{5.5}{40} \quad \frac{6.0}{26} \quad \frac{6.5}{13} \quad \frac{6.1}{9} \quad 5.8 \quad \frac{5.8}{12} \quad \frac{5.8}{25} \quad \frac{6.2}{35} \quad \frac{5.5}{40}$$

$$\frac{4.0}{40} \quad \frac{4.0}{17} \quad \frac{5.9}{12} \quad \frac{5.5}{10} \quad 5.4 \quad \frac{5.4}{13} \quad \frac{5.0}{18} \quad \frac{4.6}{40}$$

933.63

7+40

28.3

B.M.

2.44

933.61

2.44

931.19 ✓

931.17

8

29.0

+50

28.8

9

27.6

+50

26.3

10

25.8

+50

25.4

11

25.2

T.P.

10.39

934.70 ✓

9.30

924.31 ✓

+50

25.3

12

25.8

+50

26.9

13

28.3

+50

30.1

$\frac{3.9}{40}$	$\frac{3.7}{17}$	$\frac{5.8}{13}$	$\frac{5.5}{9}$	5.3	$\frac{5.4}{12}$	$\frac{4.0}{16}$	$\frac{3.8}{40}$
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Spk. in 8" Oak 50' Rt. 7+67

$\frac{4.1}{40}$	$\frac{3.1}{18}$	$\frac{4.7}{13}$	$\frac{4.7}{9}$	4.6	$\frac{4.8}{11}$	$\frac{3.3}{17}$	$\frac{3.6}{40}$
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$\frac{5.6}{40}$	$\frac{4.3}{33}$	$\frac{3.9}{16}$	$\frac{5.0}{13}$	4.8	$\frac{5.3}{10}$	$\frac{4.7}{14}$	$\frac{3.5}{17}$	$\frac{2.9}{27}$	$\frac{3.6}{40}$
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$\frac{7.3}{40}$	$\frac{6.1}{26}$	$\frac{5.7}{16}$	$\frac{6.0}{14}$	$\frac{6.1}{9}$	6.0	$\frac{6.3}{7}$	$\frac{5.8}{15}$	$\frac{4.8}{17}$	$\frac{4.4}{40}$
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$\frac{8.0}{40}$	$\frac{7.8}{25}$	$\frac{7.5}{9}$	7.3	$\frac{7.5}{6}$	$\frac{7.3}{12}$	$\frac{8.0}{17}$	$\frac{7.5}{40}$
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$\frac{8.5}{40}$	$\frac{8.5}{25}$	$\frac{8.0}{9}$	7.8	$\frac{7.8}{6}$	$\frac{7.8}{11}$	$\frac{8.6}{13}$	$\frac{9.1}{21}$	$\frac{9.5}{40}$
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$\frac{10.0}{40}$	$\frac{9.8}{24}$	$\frac{9.0}{14}$	$\frac{8.4}{10}$	8.2	$\frac{8.3}{6}$	$\frac{7.7}{10}$	$\frac{8.8}{15}$	$\frac{8.6}{40}$
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$\frac{10.4}{40}$	$\frac{10.0}{18}$	$\frac{9.1}{15}$	$\frac{8.7}{9}$	8.4	$\frac{8.4}{5}$	$\frac{8.4}{10}$	$\frac{9.7}{23}$	$\frac{9.6}{40}$
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$\frac{12.0}{40}$	$\frac{11.4}{17}$	$\frac{9.5}{14}$	$\frac{9.5}{9}$	9.4	$\frac{9.5}{6}$	$\frac{9.8}{10}$	$\frac{11.0}{14}$	$\frac{11.0}{40}$
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$\frac{11.2}{40}$	$\frac{11.0}{16}$	$\frac{9.0}{13}$	$\frac{9.0}{10}$	8.9	$\frac{9.0}{6}$	$\frac{9.2}{10}$	$\frac{10.7}{15}$	$\frac{10.5}{22}$	$\frac{10.6}{40}$
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$\frac{9.7}{40}$	$\frac{9.0}{18}$	$\frac{8.0}{9}$	7.8	$\frac{7.8}{8}$	$\frac{8.4}{16}$	$\frac{7.8}{21}$	$\frac{8.0}{40}$
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$\frac{5.8}{40}$	$\frac{5.2}{20}$	$\frac{6.6}{18}$	$\frac{6.6}{10}$	6.4	$\frac{6.6}{6}$	$\frac{6.0}{13}$	$\frac{3.8}{18}$	$\frac{4.2}{40}$
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$\frac{3.7}{40}$	$\frac{3.5}{21}$	$\frac{5.0}{18}$	$\frac{4.8}{10}$	4.6	$\frac{4.7}{6}$	$\frac{4.8}{12}$	$\frac{3.0}{17}$	$\frac{2.5}{40}$
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934.70

14 30.2

+50 30.5

15 30.4

+50 30.9

16 31.9

+50 32.9

T.P. 7.71 941.01 1.40 933.30

17 33.9

B.M. 4.92 936.09 936.18

+50 35.6

18 37.9

T.P. 7.30 946.28 2.03 938.98

+50 39.7

19 40.7

+50 41.5

+92 41.7

2.8	2.5	4.7	5.5	4.6		4.7	2.6	2.5
40	21	18	19	11	45	10	17	40

4.8	3.7	5.1	5.2	4.5		4.3	5.0	4.2	3.0	3.3
40	20	17	13	10	42	5	10	12	17	40

4.7	5.5	4.5		4.4	5.7	5.5
40	18	7	43	6	21	40

5.8	5.4	4.0		4.1	4.6	4.0
40	18	10	3.8	7	10	40

4.0	3.0	3.8	3.0		2.8	3.3	2.0	1.7
40	21	15	9	2.8	6	9	30	40

2.0	2.2	2.1		1.8	2.4	2.2
40	27	10	1.8	5	10	40

9.0	9.5	7.4	7.2		7.5	9.5	10.2
40	19	13	8	7.1	11	15	40

Sph. in 15" Oak 200' Rth. 17+10

6.7	7.0	6.0	5.5		5.6	6.1	7.1	7.1
40	16	14	9	5.4	7	14	17	40

1.4	1.6	3.5	3.4		3.4	3.8	2.0	2.7	3.3
40	19	17	8	3.1	7	14	17	32	40

2.4	2.8	6.4	2.1	6.8		6.7	2.3	3.1	4.7
40	23	19	15	11	6.6	8	14	18	40

2.0	2.0	5.6	6.1	5.8		6.1	5.6	3.3	4.7
40	22	18	15	10	5.6	10	16	18	40

3.8	4.6	5.6	4.9		5.1	5.5	4.8	5.2
40	20	18	10	4.8	6	13	16	40

5.0	5.5	6.0	5.0		4.8	5.4	5.4
40	33	20	9	4.6	23	27	40

946.28

20

41.7

+10

41.8

T.P.

436 945.83 ✓ 4.81

941.47

+50

41.4

21

41.4

+50

41.4

22

40.8

+50

40.1

23

39.6

+50

38.6

24

37.8

+50

37.2

25

36.9

T.P.

360 941.65 ✓ 7.78 938.05

$\frac{5.4}{40}$	$\frac{6.2}{19}$	$\frac{5.0}{9}$	$\frac{4.6}{6}$	$\frac{4.1}{14}$	$\frac{4.8}{40}$
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$\frac{5.4}{40}$	$\frac{5.8}{33}$	$\frac{6.0}{19}$	$\frac{5.0}{11}$	$\frac{5.0}{45}$	$\frac{5.0}{18}$	$\frac{5.0}{22}$	$\frac{5.4}{31}$	$\frac{5.4}{40}$
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E. End Side Drain Rt. 20+

$\frac{4.0}{50}$	$\frac{4.0}{29}$	$\frac{4.1}{14}$	$\frac{5.2}{14}$	$\frac{4.6}{10}$	$\frac{4.7}{6}$	$\frac{5.4}{13}$	$\frac{4.4}{15}$	$\frac{4.2}{50}$
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$\frac{3.9}{40}$	$\frac{3.7}{33}$	$\frac{4.3}{16}$	$\frac{5.1}{15}$	$\frac{4.4}{11}$	$\frac{5.0}{9}$	$\frac{4.8}{25}$	$\frac{4.3}{50}$
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$\frac{4.6}{40}$	$\frac{3.9}{33}$	$\frac{3.7}{18}$	$\frac{5.1}{14}$	$\frac{4.5}{11}$	$\frac{4.9}{10}$	$\frac{3.3}{17}$	$\frac{3.4}{40}$
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$\frac{4.7}{40}$	$\frac{4.0}{35}$	$\frac{4.4}{19}$	$\frac{5.3}{14}$	$\frac{5.3}{50}$	$\frac{4.7}{9}$	$\frac{4.0}{15}$	$\frac{4.4}{33}$	$\frac{4.4}{40}$
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$\frac{4.5}{40}$	$\frac{3.7}{35}$	$\frac{4.4}{16}$	$\frac{5.9}{15}$	$\frac{5.7}{57}$	$\frac{6.2}{10}$	$\frac{5.2}{11}$	$\frac{4.3}{13}$	$\frac{4.0}{40}$
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$\frac{6.0}{40}$	$\frac{5.6}{34}$	$\frac{5.9}{16}$	$\frac{6.8}{13}$	$\frac{6.2}{6.2}$	$\frac{6.7}{10}$	$\frac{5.7}{12}$	$\frac{5.0}{23}$	$\frac{5.4}{40}$
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$\frac{8.4}{40}$	$\frac{7.8}{36}$	$\frac{7.4}{17}$	$\frac{8.0}{13}$	$\frac{7.4}{8}$	$\frac{7.2}{7.2}$	$\frac{7.5}{4}$	$\frac{7.9}{10}$	$\frac{7.1}{12}$	$\frac{6.9}{25}$	$\frac{7.4}{40}$
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$\frac{9.3}{40}$	$\frac{9.4}{14}$	$\frac{8.1}{10}$	$\frac{8.0}{8.0}$	$\frac{8.4}{7}$	$\frac{9.1}{13}$	$\frac{8.7}{24}$	$\frac{9.3}{40}$
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$\frac{8.7}{40}$	$\frac{9.2}{14}$	$\frac{9.6}{13}$	$\frac{8.6}{10}$	$\frac{8.6}{8.6}$	$\frac{8.8}{7}$	$\frac{10.2}{17}$	$\frac{10.1}{25}$	$\frac{10.7}{40}$
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$\frac{8.6}{40}$	$\frac{8.9}{28}$	$\frac{8.5}{19}$	$\frac{9.0}{14}$	$\frac{9.4}{12}$	$\frac{9.1}{11}$	$\frac{8.9}{8.9}$	$\frac{9.2}{8}$	$\frac{9.7}{10}$	$\frac{9.2}{11}$	$\frac{9.0}{25}$	$\frac{9.5}{40}$
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941.65

25+50

36.8

26

36.7

+50

36.8

27

37.0

+50

37.2

28

37.0

+50

36.7

29

36.0

+50

35.3

30

34.2

+50

33.8

T.P.

11.00 94299

946

931.99

31

33.6

+41

34.2

4.5 4.0 4.4 5.4 5.0 5.0 5.5 5.0 4.3 4.7
40 33 17 13 9 4.9 7 10 11 34 40

4.8 4.9 4.8 5.7 5.2 5.9 5.2 5.0 5.0
40 32 17 12 5.0 7 10 13 35 40

4.8 4.4 5.0 5.5 5.3 5.7 4.7 4.5 5.0
40 34 16 12 4.9 9 10 15 38 40

4.9 4.8 4.6 5.2 4.9 5.5 4.8 5.1 4.5
40 38 14 13 4.7 7 10 13 35 40

4.4 4.5 5.2 4.7 4.8 5.5 4.4 5.8 4.1
40 14 15 9 4.5 9 13 14 25 40

3.9 4.8 3.9 5.1 4.8 5.6 4.1 3.9 4.0
40 29 17 16 4.7 8 13 15 26 40

3.8 3.5 3.9 5.7 5.2 5.0 5.5 3.7 3.0 3.8
40 31 21 20 10 5.0 9 14 15 24 40

3.4 3.4 3.6 6.0 6.0 5.8 6.1 3.5 3.1 3.3
40 31 19 17 9 5.7 8 14 16 24 40

4.9 4.7 5.0 6.8 6.6 6.4 6.8 4.9 4.1 4.3
40 30 21 19 10 6.4 8 14 16 24 40

8.3 7.5 8.0 8.8 7.7 7.7 8.9 8.3 7.8 7.7
40 29 18 15 8 7.5 8 13 15 24 40

11.4 10.8 11.1 8.3 8.0 10.2 10.3 10.4
40 29 19 11 7.9 9 14 28 40

11.5 12.0 9.5 9.8 12.0 11.6
40 17 10 9.4 7 16 40

8.6 8.8 10.1 9.8 8.8 9.1 9.9 9.4 9.0 8.8
40 27 22 16 10 8.8 7 12 14 24 40

942.99

32

36.8

+50

39.0

33

40.2

+22

40.7

+32

40.9

+40 W. shoulder White Bear Ave

41.0

+53⁶⁰

41.1

BM.

1.85 941.14

$$\begin{array}{r} 43 \ 46 \ 7.0 \ 7.0 \ 6.5 \\ 40 \ 24 \ 21 \ 15 \ 13 \ 6.2 \end{array} \quad \begin{array}{r} 6.3 \ 6.8 \ 5.8 \ 4.8 \ 4.6 \\ 8 \ 11 \ 13 \ 23 \ 40 \end{array}$$

$$\begin{array}{r} 2.8 \ 2.2 \ 5.3 \ 5.4 \ 4.4 \\ 40 \ 24 \ 20 \ 16 \ 11 \ 4.0 \end{array} \quad \begin{array}{r} 4.1 \ 4.6 \ 4.1 \ 2.9 \ 2.8 \\ 7 \ 11 \ 13 \ 19 \ 40 \end{array}$$

$$\begin{array}{r} 2.0 \ 2.1 \ 4.2 \ 4.0 \ 3.0 \\ 40 \ 22 \ 19 \ 14 \ 10 \ 2.8 \end{array} \quad \begin{array}{r} 3.2 \ 2.7 \ 2.7 \\ 11 \ 13 \ 40 \end{array}$$

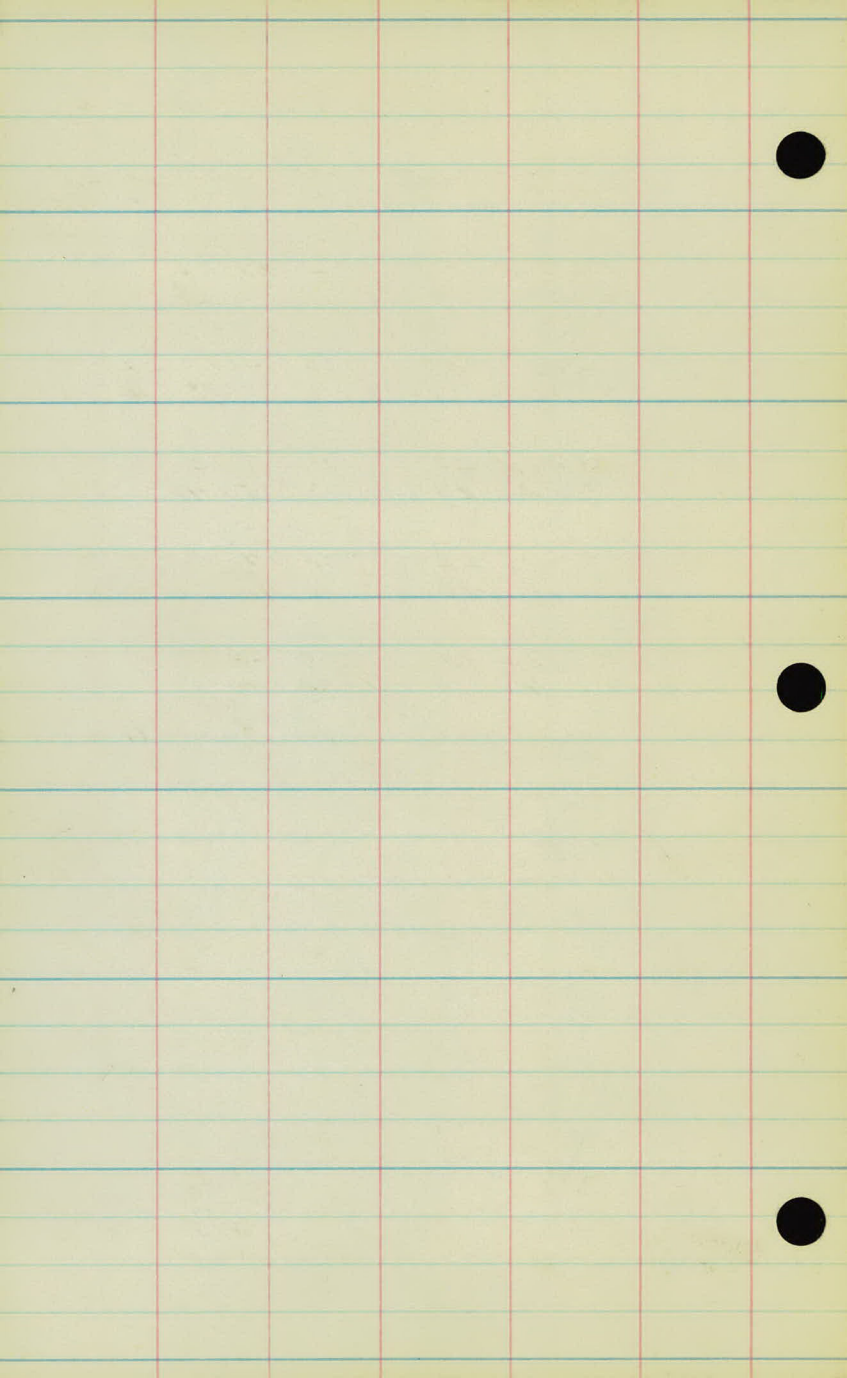
$$\begin{array}{r} 1.8 \ 1.8 \ 3.5 \ 3.4 \ 2.6 \\ 40 \ 22 \ 19 \ 16 \ 12 \ 2.3 \end{array} \quad \begin{array}{r} 2.6 \ 1.4 \ 1.2 \ 2.2 \\ 11 \ 14 \ 33 \ 40 \end{array}$$

$$\begin{array}{r} 3.7 \ 3.7 \ 2.3 \\ 40 \ 24 \ 20 \ 2.1 \end{array} \quad \begin{array}{r} 2.4 \ 2.0 \ 2.0 \\ 13 \ 15 \ 40 \end{array}$$

$$\begin{array}{r} 1.8 \ 2.2 \\ 40 \ 20 \ 2.0 \end{array} \quad \begin{array}{r} 2.0 \ 1.7 \\ 21 \ 40 \end{array}$$

$$\begin{array}{r} 1.6 \ 1.7 \\ 40 \ 19 \ 1.9 \end{array} \quad \begin{array}{r} 1.9 \ 2.0 \\ 22 \ 40 \end{array}$$

Top 1000 most & White Bear Arc



Level 5 - Ash St.

J.T.H. #1 - White Bear Ave.

BM.	7.18	936.98		929.80
T.P.	6.00	933.89	9.09	927.89
BM.			2.72	931.17 931.17
T.P.	8.43	934.17	8.15	925.74
T.P.	12.17	944.50	1.84	932.33
BM.			8.40	936.10 936.10
T.P.	1.90	943.57	2.83	941.67
T.P.	5.52	942.19	6.90	936.67
BM.			1.02	941.17 941.17

N.B.
H.W.
ET.
D.J.

9-18-33

SpK in PP 1' Lt St 0-23

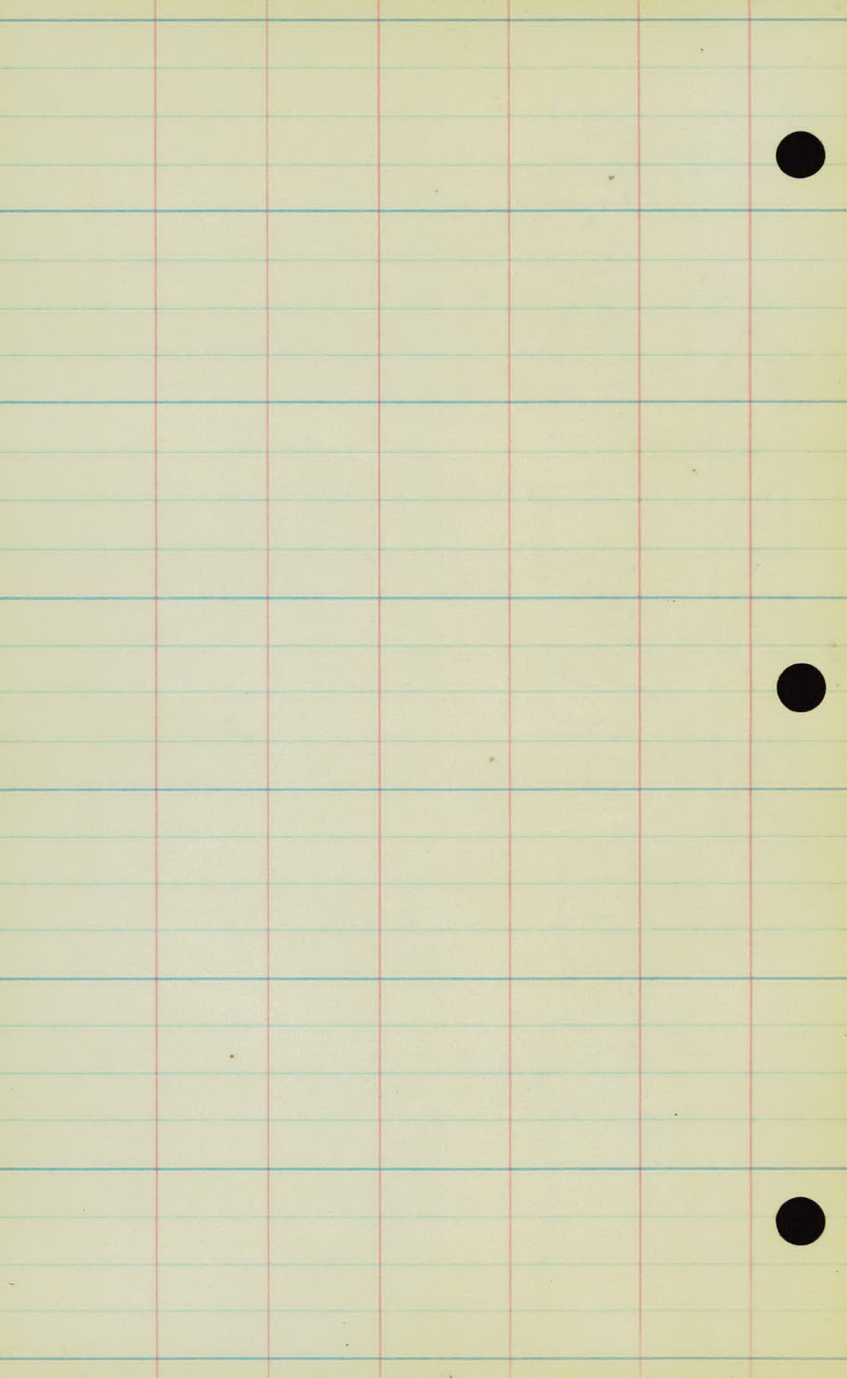
SpK in 8" oak 50' Rt St 7167

SpK in 15" oak 200' Rt St. 17410

on x sections this bench was made 936.09

Iron mon't E White Bear Ave.

on x sections this bench was made 941.14



Co. Rd. "F"

33-W. 4

0+30 No. culv. req.

4+30 Rt - Rep. 12" X 26' fr 177 11+36

X 6+00 Pl. 18" P₃ X 36'

2+50 Lt. No. culv. req.

6+92 Lt Rep. 12" X 32' C.M. fr 6+16

7+26 Rt No culv. req

7+50 - 10+00 Cl. 3 Gr. 9

11+00 - 11+50 Cl. 1 Gr. 1

X 11+26 Re 177. Pl. 18" P₃ X 36'

14+00 Rt. Pl. 15" X 20 C.M.

12+50 15+00 Cl. 4 Gr. 4

17+75 Rt Pl. 15" X 20' C.M.

17+50 - 20+00 Cl. 5 Gr. 5

20+01 Rt. Re 177. 170 culv. req

20+50 Lt. No culv. req

27+50 - 29+50 Cl. 5 Gr. 5

29+50 Rt. Rep. fr 177 - 30+71 - 32'

29+50 Lt Pl. 15" X 20

X 30+71 Re 177 Pl. 18" P₃ 42

32+00 - 33+00 Cl. 4 Gr. 4

32

26

30

32

120