

Book- 6, Dr. 12

X

OFFICE OF COUNTY ENGINEER
RAMSEY CO. MINN.

PLAN

Survey

SOUTH ST.

From Otter Lake Rd. To Railroad Ave.

Road Acc't. No. W2

Date Filed. 11-8-29

File. W-B Twp.

PROJ. 29-W2

Transit Notes
South St.
White Bear Twp.

T Weber
Rod Beaton.
Chas. Bell

Offer Lake Rd to Railroad Ave

Sta.

$\Delta R + 0^{\circ}19'$

23+00.65

West 1/4 Cor. Sec. 22-30-22

17+45.28

14+06.8

P.O.T.

10+22.91

= West Line of Margaret St.
~~East~~

1003.64

+ 19.27 Iron. 30' Lt.

0+00

6" Pop.

Q

58°06'

$\Delta R. 0^{\circ}19'$

2" x 2" Hub

15'

2" x 2" Hub

Mont Gene.

Orig. Iron

Street

12" Oak

50.67

2" x 2" Hub

53.9

18" Oak

Found Orig Iron

60

South

orig. Iron

30'

35.50

1927

6'30"

Road

R.R. Spike

to Otter Lake

Orig. Iron

30'

44.18

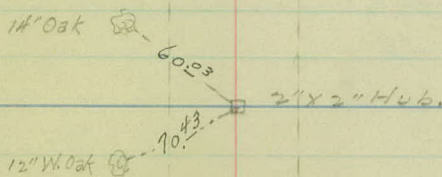
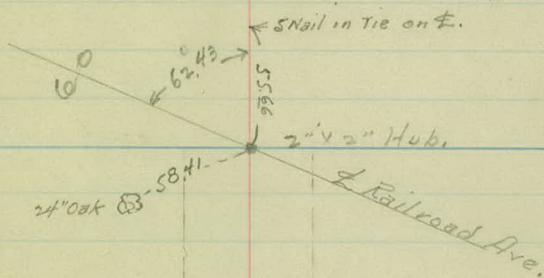
56.73

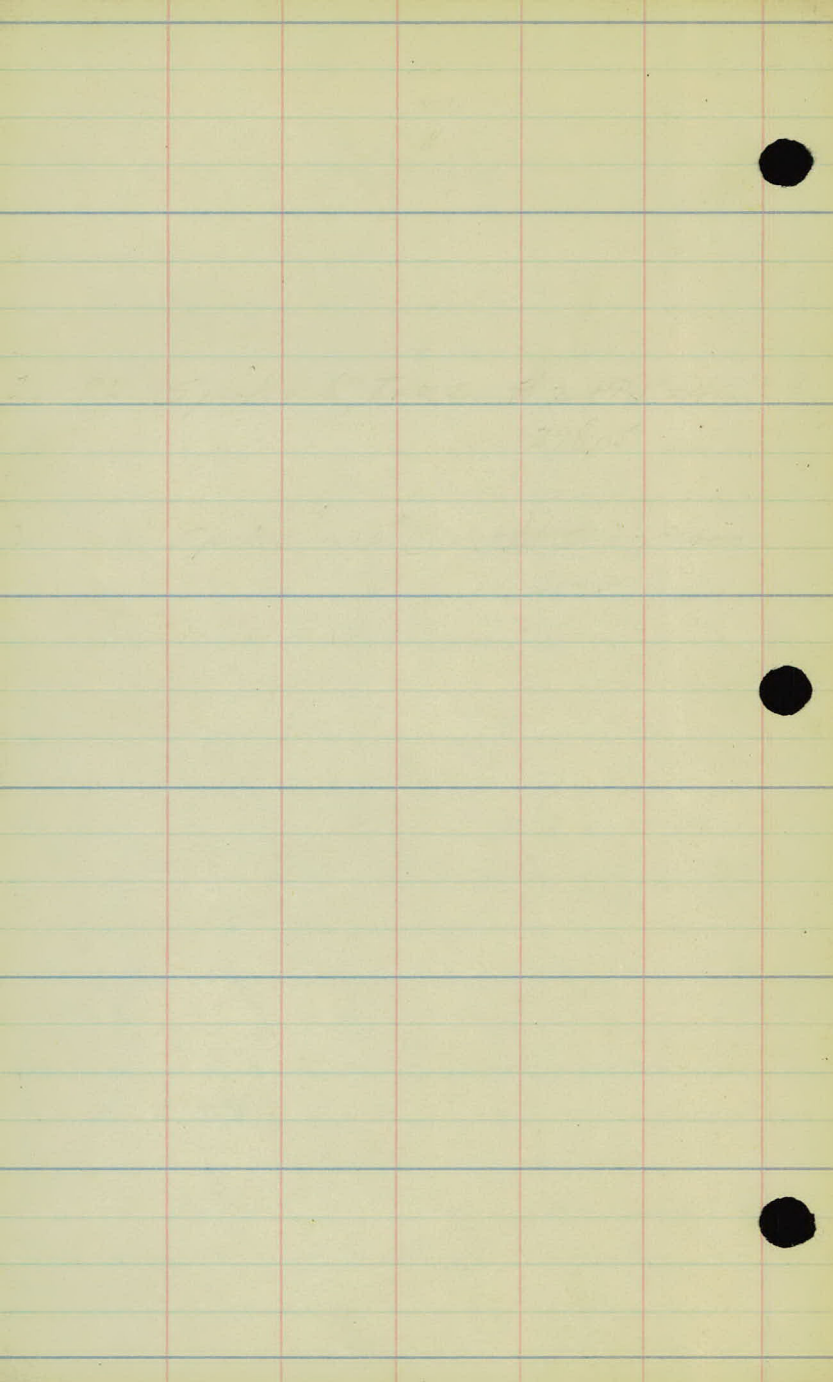
40+13.5

± P.R. Ave. End of Proj.

29+13.59

10-16-29





10-19-29

Topog Notes
South ----- St

White Bear Twp.

926.75

16

15

10+00

(Co. Ditch.)

2

1

0+00

22

21

20

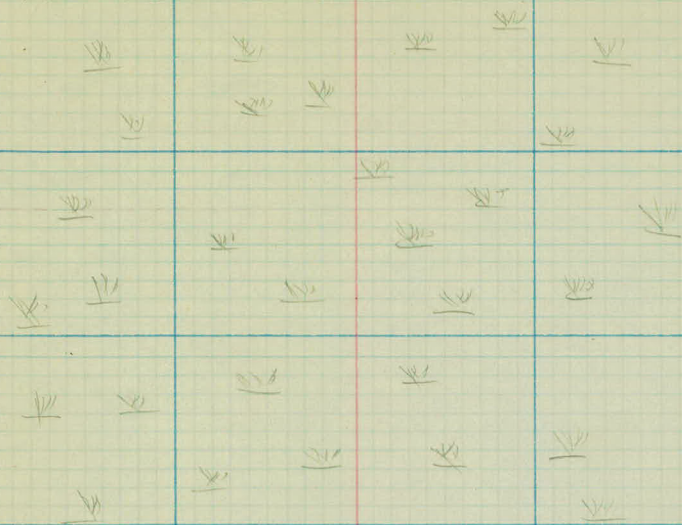
19

18

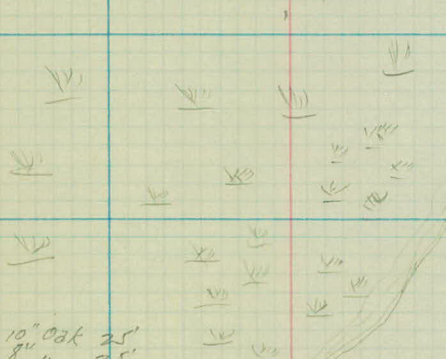
17+00

10-19-29

+95=12" x 16' C.M.



+28-12" x 24' C.M.



+22'-10" Oak 25'
+15= 8" " 25'

+00 = Bag.

450

28

27

26

25

24

23

+50-12" Oak 24'

+00 = End Swamp.

VV

PP

VV

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10-19-29

+42 = 15" x 18" Cul. C.M. + V.P. 25'



+17 = Manhole 9' ⊕

+11 = Conc. Steps 20' 

Dry Swamp.

+43 = 8" Oak 26'

+30 = 10" Oak 26'

+24 = 1" Cor. 28'

+76 = 1" Cor. 28'

+67 = 10" x 36" C.M.

Plotted



29+30
Box Cultivated Field

Uncultivated

+38 = 12" Oak 18'

+36 = 10" Oak 25'

+30 = 8" Oak 25'

40 + 13⁵ End of Proj.

38

37

36

10-19-29

Cultivated to End of Proj.

+++++

+87 = Fcn Cor. 3'
+72 = 8" Oak 18'

Fence = 1' R +00

+92 = 12" Oak 17'

Pasture

+37 = 14" Oak 8'
+26 = 6" Oak 6'

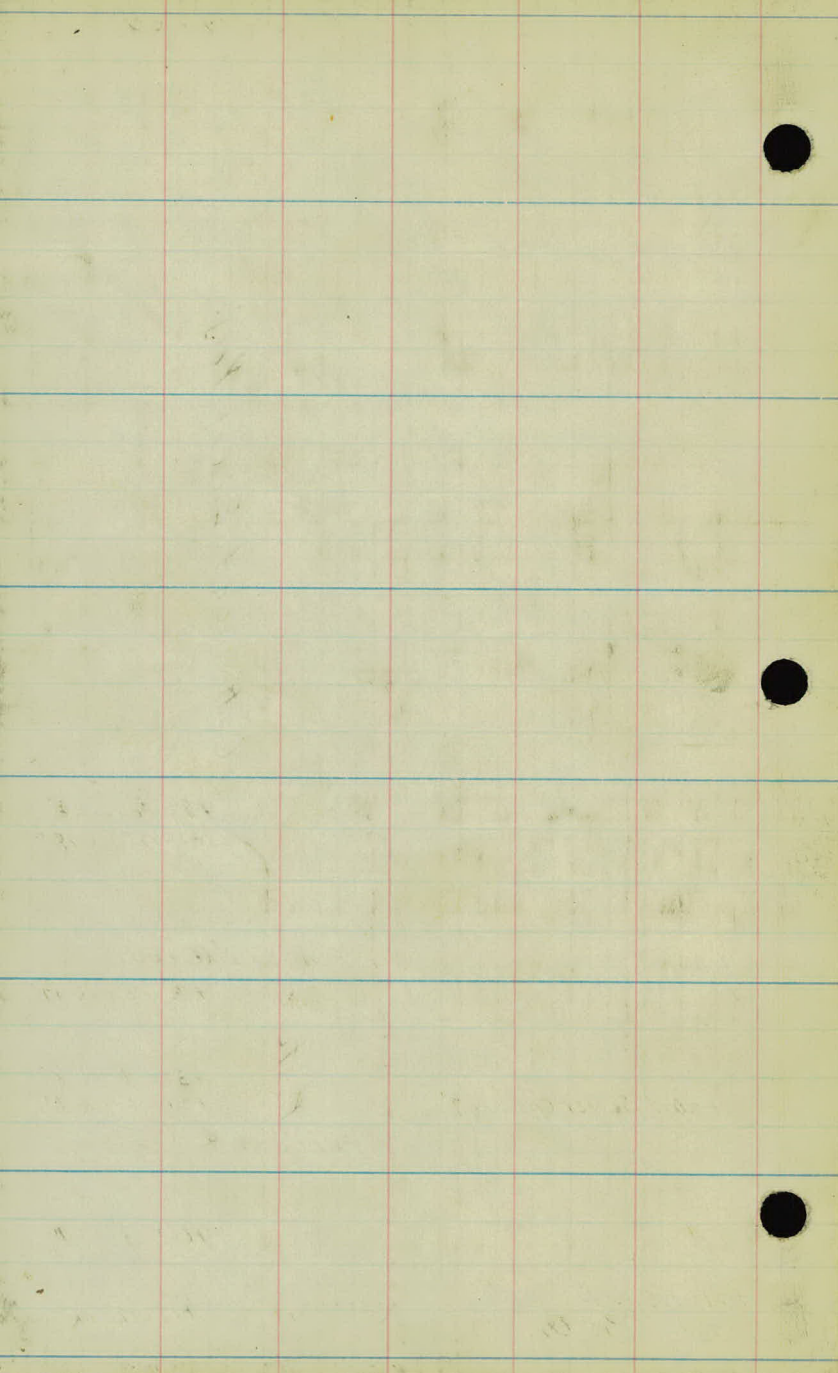
Fence on R 37 +00

+20 = 8" Sewer Opening 7'

+66 = 18" Oak 16'

+21 = F. Cor. 1'
+00 = Pr. Dr.

+19 = 12" Oak 23'



Original
X section Notes
South St.
White Bear Trip.

Sta.	+	H.I.	-	931.79 [✓]
	3.48	935.27 [✓]		
T.P.	4.83	933.04 [✓]	7.06	928.21 [✓]
" "	5.17	934.65 [✓]	3.56	929.48 [✓]
" "	4.02	933.84 [✓]	4.83	929.82 [✓]
B.M.			2.94	930.90 [✓]
		933.84 [✓]		

0+00 ~~L~~ Lt and Rt on Other Lk. Rd. 929.8

~~0+10~~ ~~29.8~~

0+27 29.6

1 30.2

2 29.6

3 30.1

4 30.9

5 31.4

T.P. 3.42 935.04[✓] 2.22 931.62[✓]

6 31.6

7 31.9

Spike in T.P. 100' No. Sta. 52+25. Ramaley +
 Otter Lake Pds.

10-17-29

Spike in T.P. 70' Rt Sta. 0+50

Lt

£

Rt.

$\frac{4.2}{50}$ $\frac{4.0}{25}$ $\frac{4.0}{25}$ $\frac{3.9}{25}$ $\frac{3.8}{50}$

$\frac{4.0}{10}$ $\frac{4.8}{12}$ $\frac{5.3}{15}$ $\frac{5.3}{15}$ $\frac{4.6}{16}$ $\frac{4.6}{33}$

$\frac{4.4}{33}$ $\frac{4.5}{17}$ $\frac{5.4}{16}$ $\frac{5.4}{13}$ $\frac{4.2}{13}$ $\frac{5.2}{15}$ $\frac{4.7}{15}$ $\frac{4.2}{22}$ $\frac{4.2}{33}$

$\frac{4.7}{33}$ $\frac{4.4}{17}$ $\frac{5.3}{16}$ $\frac{3.6}{11}$ $\frac{5.5}{11}$ $\frac{4.5}{33}$

$\frac{5.0}{33}$ $\frac{4.7}{18}$ $\frac{5.8}{16}$ $\frac{4.2}{18}$ $\frac{4.6}{18}$ $\frac{4.4}{33}$

$\frac{4.7}{33}$ $\frac{4.5}{19}$ $\frac{5.2}{17}$ $\frac{3.7}{10}$ $\frac{4.4}{10}$ $\frac{4.4}{33}$

$\frac{4.2}{33}$ $\frac{4.1}{18}$ $\frac{4.9}{17}$ $\frac{2.9}{10}$ $\frac{3.8}{10}$ $\frac{3.2}{11}$ $\frac{4.2}{33}$

$\frac{4.5}{33}$ $\frac{4.1}{18}$ $\frac{4.8}{17}$ $\frac{2.4}{11}$ $\frac{3.6}{11}$ $\frac{3.2}{12}$ $\frac{4.5}{33}$

$\frac{5.0}{33}$ $\frac{4.8}{19}$ $\frac{5.6}{18}$ $\frac{3.4}{11}$ $\frac{4.4}{11}$ $\frac{3.8}{12}$ $\frac{5.1}{30}$ $\frac{5.1}{33}$

$\frac{4.8}{33}$ $\frac{4.6}{19}$ $\frac{5.3}{17}$ $\frac{3.1}{12}$ $\frac{4.7}{12}$ $\frac{5.0}{30}$ $\frac{5.0}{33}$

	+	H.I.	-		
8		935.04			931.3
9					30.9
10					30.0
+14	}	West Shoulder			30.1
+19		Co. Ditch ±			29.9
+23		East Shoulder			29.8
B.M.	3.72	933.77	4.99	930.05	
11					29.7
12					29.8
13					29.8
14					29.1
+22					29.0
15					26.9
16					25.2
T.P.	2.15	927.53	8.39	925.38	

Lt Lt Rt.

$\frac{5.6}{33}$ $\frac{5.4}{20}$ $\frac{6.0}{19}$ 3.7 $\frac{4.9}{11}$ $\frac{5.5}{30}$ $\frac{5.5}{33}$

$\frac{5.7}{33}$ $\frac{5.6}{19}$ $\frac{6.4}{17}$ 4.1 $\frac{4.7}{10}$ $\frac{5.4}{30}$ $\frac{5.4}{33}$

$\frac{5.7}{33}$ $\frac{5.7}{30}$ $\frac{5.0}{20}$ $\frac{6.0}{19}$ 5.0 $\frac{5.4}{13}$ $\frac{5.0}{30}$ $\frac{5.0}{33}$

$\frac{5.0}{40}$ $\frac{5.4}{30}$ $\frac{7.0}{25}$ $\frac{5.5}{24}$ $\frac{5.2}{20}$ $\frac{6.2}{19}$ 4.9 $\frac{6.2}{14}$ $\frac{5.1}{16}$ $\frac{4.2}{30}$ $\frac{4.2}{40}$

$\frac{8.2}{40}$ (8.2) $\frac{8.0}{18}$ $\frac{6.1}{16}$ 5.1 $\frac{5.9}{7}$ $\frac{8.4}{9}$ (8.6) $\frac{8.6}{30}$ $\frac{8.6}{40}$ → Flow line.

$\frac{5.5}{40}$ $\frac{5.5}{30}$ $\frac{5.3}{21}$ $\frac{6.3}{19}$ 5.2 $\frac{6.1}{9}$ $\frac{5.5}{30}$ $\frac{5.9}{40}$

Spike in Twin Oak 35' Rt Sta. 10 + 70. So. side of Tree.

$\frac{4.3}{33}$ $\frac{4.5}{22}$ $\frac{5.6}{19}$ $\frac{3.5}{5}$ 4.1 $\frac{5.6}{12}$ $\frac{4.4}{14}$ $\frac{4.3}{33}$

$\frac{4.4}{33}$ $\frac{4.3}{22}$ $\frac{5.3}{20}$ $\frac{4.2}{14}$ 4.0 $\frac{5.6}{12}$ $\frac{4.4}{13}$ $\frac{4.3}{33}$

$\frac{4.9}{33}$ $\frac{4.8}{23}$ $\frac{5.7}{21}$ $\frac{4.6}{15}$ 4.0 $\frac{5.3}{11}$ $\frac{4.3}{12}$ $\frac{4.4}{33}$

$\frac{5.5}{33}$ $\frac{5.2}{24}$ $\frac{6.5}{23}$ $\frac{5.0}{15}$ 4.7 $\frac{5.7}{9}$ $\frac{4.7}{10}$ $\frac{4.7}{33}$

$\frac{5.1}{33}$ $\frac{4.8}{25}$ $\frac{5.8}{23}$ $\frac{4.7}{17}$ 4.8 $\frac{5.7}{8}$ $\frac{4.5}{10}$ $\frac{4.4}{33}$

$\frac{4.7}{33}$ $\frac{4.7}{24}$ $\frac{7.3}{22}$ 6.9 $\frac{7.2}{11}$ $\frac{4.5}{12}$ $\frac{4.7}{33}$

$\frac{5.8}{33}$ $\frac{6.4}{20}$ $\frac{9.2}{18}$ 8.6 $\frac{9.4}{12}$ $\frac{8.6}{13}$ $\frac{9.7}{33}$

		927.53			
B.M.	3.87	928.30	3.10	924.43	
16+50					923.0

17					20.3
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18					19.3
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19					19.1
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20					19.1
----	--	--	--	--	------

T.P	4.71	924.22	8.79	919.51	
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21					19.1
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22					19.0
----	--	--	--	--	------

23					19.3
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24					19.4
----	--	--	--	--	------

25					19.2
----	--	--	--	--	------

26					19.8
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T.P	9.91	930.33	3.80	920.42	
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27					20.4
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10-18-29

Spike in Twin Oak #5' Lt Sta. 16+80

$$\frac{3.2}{33} \quad \frac{4.2}{20} \quad \frac{6.0}{17} \quad \frac{5.3}{10} \quad \frac{6.2}{30} \quad \frac{8.0}{33}$$

$$\frac{6.3}{33} \quad \frac{8.2}{11} \quad \frac{7.8}{8} \quad \frac{8.0}{6} \quad \frac{9.8}{8} \quad \frac{10.3}{33}$$

$$\frac{10.6}{33} \quad \frac{10.6}{10} \quad \frac{9.2}{7} \quad \frac{9.0}{4} \quad \frac{9.3}{7} \quad \frac{10.4}{33}$$

$$\frac{10.3}{33} \quad \frac{10.3}{6} \quad \frac{9.3}{5} \quad \frac{9.2}{3} \quad \frac{9.4}{4} \quad \frac{10.2}{33}$$

$$\frac{10.4}{33} \quad \frac{10.4}{6} \quad \frac{9.4}{5} \quad \frac{9.2}{4} \quad \frac{9.4}{5} \quad \frac{10.5}{33}$$

$$\frac{6.5}{33} \quad \frac{5.9}{5} \quad \frac{5.2}{4} \quad \frac{5.1}{3} \quad \frac{5.2}{5} \quad \frac{6.5}{33}$$

$$\frac{6.3}{33} \quad \frac{6.3}{4} \quad \frac{5.2}{2} \quad \frac{5.2}{5} \quad \frac{6.4}{7} \quad \frac{6.4}{33}$$

$$\frac{6.0}{33} \quad \frac{6.0}{3} \quad \frac{4.9}{1} \quad \frac{4.9}{6} \quad \frac{5.1}{7} \quad \frac{6.1}{33}$$

$$\frac{5.9}{33} \quad \frac{5.9}{4} \quad \frac{4.9}{2} \quad \frac{4.8}{5} \quad \frac{4.9}{7} \quad \frac{5.7}{33}$$

$$\frac{6.1}{33} \quad \frac{6.1}{3} \quad \frac{5.1}{1} \quad \frac{5.0}{6} \quad \frac{4.9}{9} \quad \frac{5.8}{33}$$

$$\frac{5.2}{33} \quad \frac{5.2}{5} \quad \frac{4.5}{3} \quad \frac{4.4}{12} \quad \frac{4.5}{14} \quad \frac{5.4}{33}$$

$$\frac{10.8}{33} \quad \frac{10.8}{7} \quad \frac{9.9}{14} \quad \frac{10.1}{18} \quad \frac{11.1}{33}$$

27	✓ 930.33				
+ 37					921.2
+ 60					22.6

28					24.8
+ 75					27.1

29					26.7
+ 80					26.5

30					26.2
+ 25					27.0

31					24.2
T.F.	2.33	✓ 926.75	5.91	✓ 924.42	
+ 50					22.6

32					21.3
+ 60					20.3

33					20.7
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10-18-29

$$\frac{11.6}{33} \quad \frac{11.6}{12} \quad 9.1 \quad \frac{9.0}{18} \quad \frac{8.0}{22} \quad \frac{6.4}{24} \quad \frac{5.8}{33}$$

$$\frac{10.5}{33} \quad \frac{7.7}{9} \quad \frac{8.3}{7} \quad 7.7 \quad \frac{7.4}{8} \quad \frac{8.0}{21} \quad \frac{4.3}{26} \quad \frac{4.0}{33}$$

$$\frac{6.0}{33} \quad \frac{5.0}{15} \quad \frac{6.1}{14} \quad \frac{6.9}{11} \quad 5.5 \quad \frac{6.0}{19} \quad \frac{3.1}{23} \quad \frac{2.8}{33}$$

$$\frac{2.1}{33} \quad \frac{2.3}{20} \quad \frac{3.9}{18} \quad \frac{4.7}{13} \quad 3.2 \quad \frac{4.4}{18} \quad \frac{1.7}{20} \quad \frac{2.0}{33}$$

$$\frac{1.5}{33} \quad \frac{1.6}{17} \quad \frac{3.8}{15} \quad \frac{4.5}{13} \quad 3.6 \quad \frac{4.6}{18} \quad \frac{1.9}{20} \quad \frac{2.0}{33}$$

$$\frac{3.5}{33} \quad \frac{2.8}{15} \quad \frac{4.6}{14} \quad 3.8 \quad \frac{4.7}{17} \quad \frac{3.2}{19} \quad \frac{3.0}{33}$$

$$\frac{3.0}{33} \quad \frac{3.0}{16} \quad \frac{5.0}{14} \quad 4.1 \quad \frac{4.9}{11} \quad \frac{3.2}{13} \quad \frac{3.6}{33}$$

$$\frac{3.0}{33} \quad \frac{3.4}{17} \quad \frac{5.2}{14} \quad 3.3 \quad \frac{4.9}{11} \quad \frac{3.9}{14} \quad \frac{4.6}{27} \quad \frac{4.8}{33}$$

$$\frac{3.7}{33} \quad \frac{4.3}{20} \quad \frac{5.7}{19} \quad \frac{7.4}{13} \quad 6.1 \quad \frac{7.2}{11} \quad \frac{8.8}{33}$$

$$\frac{1.9}{33} \quad \frac{2.7}{20} \quad \frac{5.5}{17} \quad \frac{4.1}{14} \quad 4.2 \quad \frac{5.8}{14} \quad \frac{7.5}{27} \quad \frac{8.2}{33}$$

$$\frac{3.5}{33} \quad \frac{4.3}{22} \quad \frac{6.7}{19} \quad \frac{5.6}{11} \quad 5.5 \quad \frac{6.3}{9} \quad \frac{7.8}{12} \quad \frac{7.8}{33}$$

$$\frac{2.7}{33} \quad \frac{5.6}{21} \quad \frac{7.5}{18} \quad \frac{6.4}{8} \quad 6.5 \quad \frac{7.1}{7} \quad \frac{8.4}{11} \quad \frac{8.4}{33}$$

$$\frac{3.6}{33} \quad \frac{5.2}{22} \quad \frac{7.4}{19} \quad \frac{6.1}{9} \quad 6.1 \quad \frac{6.7}{7} \quad \frac{7.9}{11} \quad \frac{7.7}{33}$$

926.75

B.M.

2.13

924.62

34

921.8

35 + 17 = M.H. 9' Lt Elev = 923.65

35

931.80

22.0

T.R

9.61

934.23

4.56

922.19

+ 20

23.0

36

23.8

37

25.8

38

26.8

39

27.3

40

27.4

+ 13.5

927.7

B.M.

1.71

930.09

10-18-29

Spike in 10" W.O. 36' Lt Sta. 33+50

$$\frac{2.0}{33} \quad \frac{4.0}{25} \quad \frac{6.1}{20} \quad \frac{4.7}{9} \quad 5.0 \quad \frac{5.6}{9} \quad \frac{7.0}{14} \quad \frac{7.8}{33}$$

$$\frac{1.6}{33} \quad \frac{2.4}{26} \quad \frac{4.9}{23} \quad \frac{4.4}{15} \quad 4.8 \quad \frac{5.0}{7} \quad \frac{6.8}{14} \quad \frac{6.8}{33}$$

$$\frac{6.9}{35} \quad \frac{7.5}{27} \quad \frac{9.2}{25} \quad \frac{8.2}{12} \quad 8.8 \quad \frac{10.2}{15} \quad \frac{11.0}{33}$$

$$\frac{5.7}{35} \quad \frac{5.7}{33} \quad \frac{7.6}{22} \quad \frac{6.8}{17} \quad 8.0 \quad \frac{9.2}{15} \quad \frac{10.0}{33}$$

$$\frac{4.4}{35} \quad \frac{4.4}{33} \quad \frac{5.3}{25} \quad \frac{5.2}{14} \quad 6.0 \quad \frac{8.3}{33}$$

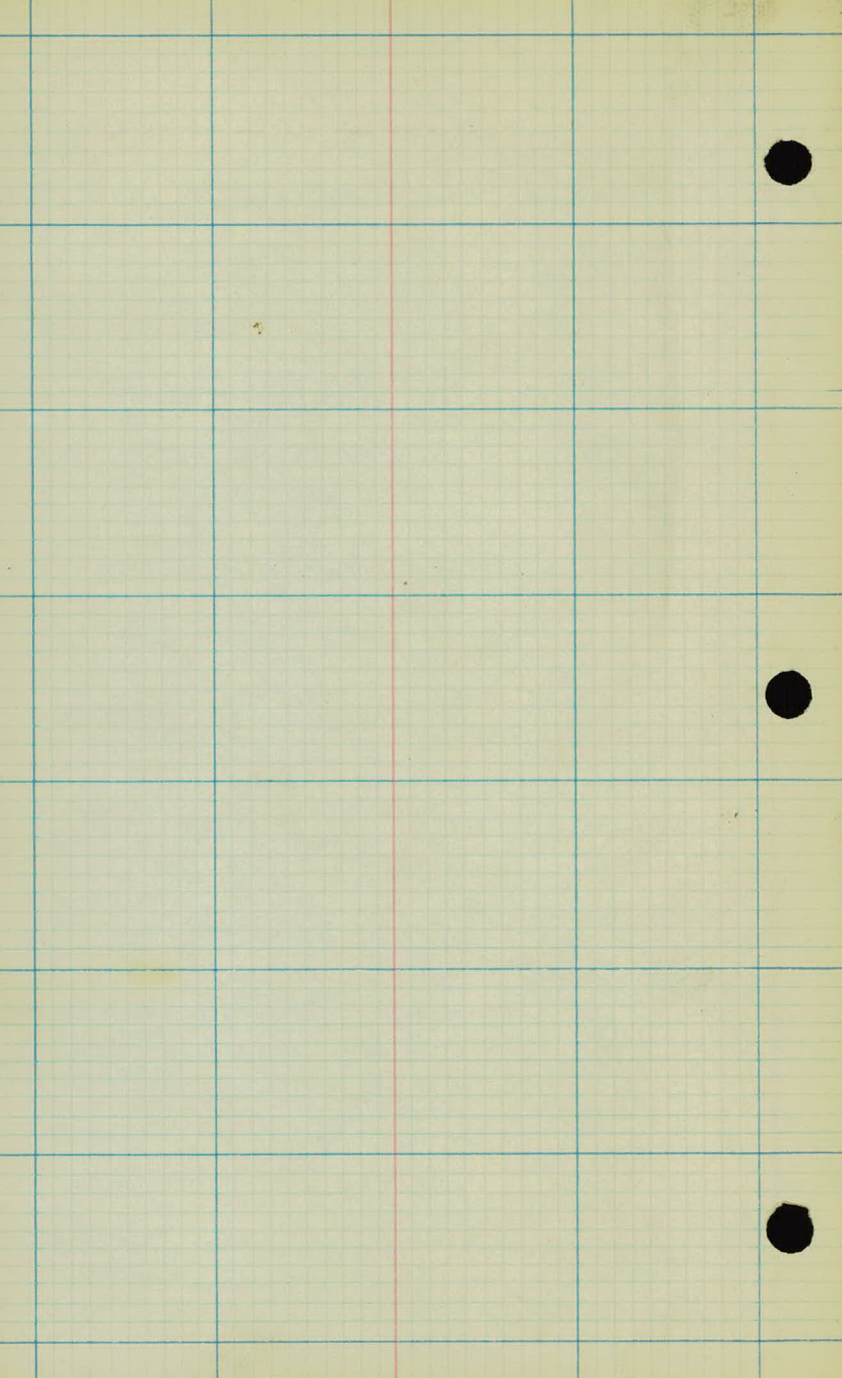
$$\frac{3.3}{33} \quad \frac{4.2}{24} \quad \frac{4.1}{14} \quad 5.0 \quad \frac{6.9}{33}$$

$$\frac{3.0}{33} \quad \frac{4.2}{21} \quad \frac{3.7}{13} \quad 4.5 \quad \frac{5.8}{33}$$

$$\frac{2.3}{33} \quad \frac{3.2}{14} \quad 4.4 \quad \frac{6.4}{32}$$

$$\frac{2.3}{33} \quad \frac{2.6}{24} \quad 4.1 \quad \frac{6.2}{33}$$

Spike in 36" Oak Sta 39+60 - 35' Lt.



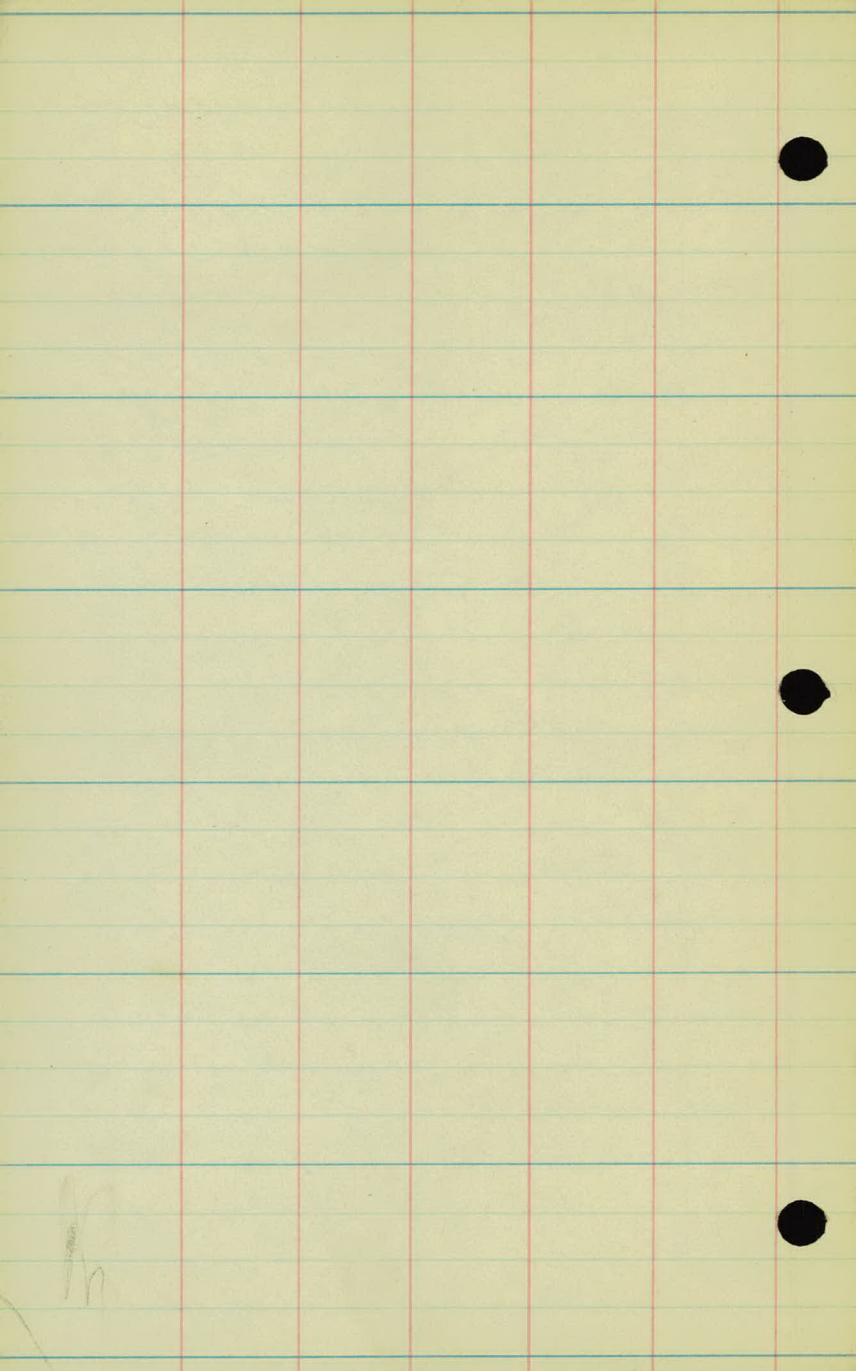
Plans in hand - South Street

O.R.V.K.

W.S.M.

10/31/29

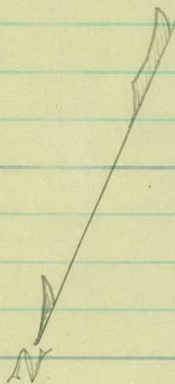
- ✓ 0+00 to 3+00 - Gr. 5 T.
- ✓ 0+40 - P-18" C.M. X 32'
- ✓ 4+00 - R^t - P-15" X 20' C.M.
- ✓ 7+00 - L^t - No culv. req.
- ✓ 10+18 - Extend on R^t (15" X 8' C.M.)
band
- ✓ 10+50 - R^t No culv. req.
- ✓ 10+50 - L^t " " "
- ✓ 14+00 to 17+00 - Gr. 15 T. Cl. 1 T.
- ✓ 18+00 to 26+00 - ~~Gr.~~ by acre - top width
0.28 AC of hand ditch on both sides
0.17 AC Cl. on R^t side ~~to 20+00~~
- ✓ 21+00 - 26+00 →
- ✓ 19+28 - Remove to 26+00
- ✓ 22+95 "
- ✓ 27+00 to 30+00 Cl. 9 T. Gr. 23 T.
- ✓ 32+67 - Remove P-18" C.M. X 36'
- ✓ 32+50 - L^t - Rep. 12" X 24' from 19+28
- ✓ 33+80 - L^t - Rep. 12" X 16' " 22+95
- ✓ 35+42 - L^t Rem & rep.
- ✓ 35+75 - R^t No culv. req.
- ✓ 36+80 - L^t - Rep 10" X 20' from 32+67
- ✓ 36+00 to 39+00 - Cl. 6 T. Gr. 8 T.
- ✓ 38+10 - L^t - P-12" X 20' C.M.
- ✓ 38+10 - R^t - P-12" X 20' C.M.
- ✓ 39+50 to 40+00 - Gr. 3 T.



X Sections of Ditch
Running South from Sta. 0 + 20
on Proj. 29-W.2

4+12 End of Ditch

0+00 So. End X Drain



Ditch

& Otter Lake Rd.

Sea St

Sta.	+	H.I.	-	Elev
	4.14	935.04		930.90
0+00	= So. End of X Drain.			

+25

+50

+75

1+00

+25

+50

+75

2+00

+25

+50

+75

3+00

Left

✱

Right.

$$\frac{5.4}{10} \frac{5.6}{4} \frac{7.2}{2} \quad 7.8 = \text{Flowline.} \quad \frac{7.2}{10} \frac{5.8}{3} \frac{5.2}{5} \frac{5.2}{10}$$

$$\frac{6.0}{10} \frac{5.4}{5} \frac{5.7}{4} \frac{7.6}{2} \quad 7.7 \quad \frac{7.6}{2} \frac{5.4}{4} \frac{4.9}{6} \frac{4.9}{10}$$

$$\frac{5.4}{10} \frac{4.9}{5} \frac{5.3}{4} \frac{7.3}{2} \quad 7.5 \quad \frac{7.3}{2} \frac{4.6}{4} \frac{4.7}{10}$$

$$\frac{5.7}{10} \frac{5.5}{4} \frac{7.5}{2} \quad 7.6 \quad \frac{7.4}{2} \frac{5.5}{4} \frac{4.8}{10}$$

$$\frac{5.6}{10} \frac{5.3}{3} \frac{7.3}{2} \quad 7.5 \quad \frac{7.3}{2} \frac{5.1}{4} \frac{4.7}{10}$$

$$\frac{5.5}{10} \frac{5.5}{3} \frac{7.2}{2} \quad 7.4 \quad \frac{7.1}{2} \frac{5.3}{4} \frac{4.7}{6} \frac{4.5}{10}$$

$$\frac{5.2}{10} \frac{5.1}{5} \frac{5.7}{3} \frac{7.6}{2} \quad 7.7 \quad \frac{7.4}{2} \frac{5.6}{4} \frac{4.8}{6} \frac{4.4}{10}$$

$$\frac{4.9}{10} \frac{4.9}{5} \frac{7.5}{3} \quad 7.5 \quad \frac{7.2}{2} \frac{5.7}{3} \frac{4.9}{6} \frac{4.5}{10}$$

$$\frac{4.6}{10} \frac{4.5}{4} \frac{7.1}{2} \quad 7.3 \quad \frac{7.0}{2} \frac{5.4}{3} \frac{4.6}{7} \frac{4.6}{10}$$

$$\frac{4.5}{10} \frac{4.3}{4} \frac{7.0}{2} \quad 7.2 \quad \frac{6.8}{2} \frac{5.3}{3} \frac{4.7}{6} \frac{4.8}{10}$$

$$\frac{4.5}{10} \frac{4.5}{5} \frac{7.1}{2} \quad 7.2 \quad \frac{6.5}{2} \frac{6.4}{3} \frac{5.5}{5} \frac{4.8}{7} \frac{4.7}{10}$$

$$\frac{4.8}{10} \frac{4.8}{6} \frac{7.2}{3} \quad 7.3 \quad \frac{6.5}{3} \frac{5.5}{5} \frac{4.9}{7} \frac{4.9}{10}$$

$$\frac{4.0}{10} \frac{4.6}{5} \frac{7.3}{2} \quad 7.4 \quad \frac{7.2}{2} \frac{5.7}{6} \frac{5.2}{8} \frac{5.2}{10}$$

935.04

+25

+50

+75

4

+12

So. End Ditch

B.M.

4.14 930.90 ✓

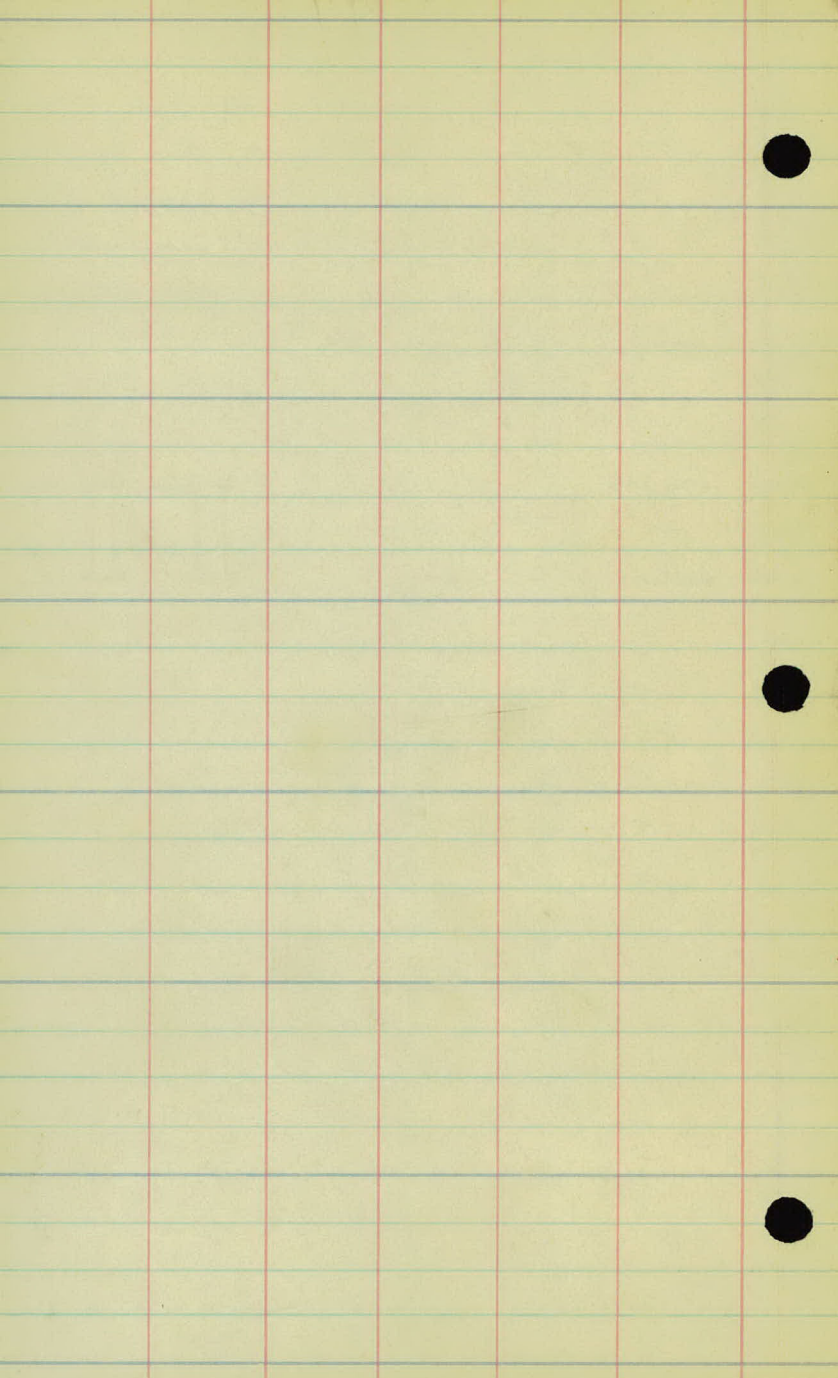
$$\begin{array}{r} \times \\ 4.7 \\ \hline 10 \end{array} \quad \begin{array}{r} \times \\ 5.1 \\ \hline 5 \end{array} \quad \begin{array}{r} 7.5 \\ \hline 2 \end{array} \quad 7.6 \quad \begin{array}{r} \times \\ 6.0 \\ \hline 6 \end{array} \quad \begin{array}{r} 5.7 \\ \hline 10 \end{array}$$

$$\begin{array}{r} \times \\ 5.2 \\ \hline 10 \end{array} \quad \begin{array}{r} \times \\ 5.2 \\ \hline 4 \end{array} \quad \begin{array}{r} 7.6 \\ \hline 2 \end{array} \quad 7.8 \quad \begin{array}{r} \times \\ 6.4 \\ \hline 6 \end{array} \quad \begin{array}{r} 6.1 \\ \hline 10 \end{array}$$

$$\begin{array}{r} \times \\ 6.0 \\ \hline 10 \end{array} \quad \begin{array}{r} \times \\ 5.8 \\ \hline 4 \end{array} \quad \begin{array}{r} 7.8 \\ \hline 2 \end{array} \quad 7.9 \quad \begin{array}{r} \times \\ 6.8 \\ \hline 6 \end{array} \quad \begin{array}{r} 6.7 \\ \hline 10 \end{array}$$

$$\begin{array}{r} \times \\ 7.2 \\ \hline 10 \end{array} \quad \begin{array}{r} \times \\ 7.1 \\ \hline 4 \end{array} \quad \begin{array}{r} 7.7 \\ \hline 2 \end{array} \quad 7.8 \quad \begin{array}{r} 7.7 \\ \hline 3 \end{array} \quad \begin{array}{r} \times \\ 7.2 \\ \hline 4 \end{array} \quad \begin{array}{r} 7.5 \\ \hline 10 \end{array}$$

$$\begin{array}{r} 7.6 \\ \hline 10 \end{array} \quad 8.1 \quad \begin{array}{r} 8.1 \\ \hline 10 \end{array}$$



29-W2

South St.
E Level

Sta.	+	H.I. ✓	-	Elev	Red.
	338	934.28		930.90	
0+00				929.88	4.4
+27				929.68	4.6
+50				929.88	4.4
1				930.18	4.1
+50				929.88	4.4
2				929.48	4.8
+50				929.68	4.6
3				929.98	4.3
+50				930.28	4.0
4				930.78	3.5
+50				931.08 30.98	3.3
5				931.08 30.98	3.3
+50				931.08	3.2
6				931.48	2.8
+50				931.88	2.4
7				931.78	2.5
	312	934.05 ✓	335	930.93 ✓	
+50				931.55	2.5
8				931.15	2.9
+50				931.05	3.0
9				930.65	3.2
+50				931.75	3.3
10				929.85	4.2
+23				929.35	4.7
11				929.25 ✓	4.8
B.M.			3.98	930.07	930.05

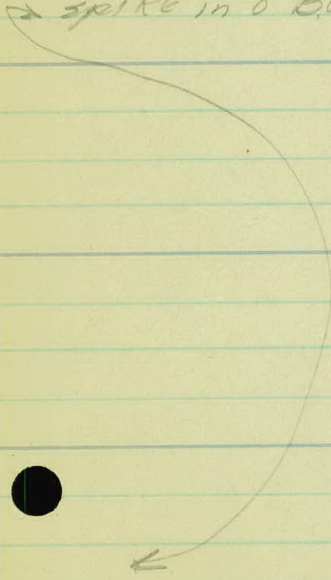
Spike in T.P. 100. Rt Sta 0+50

Spike in Twin O. Rt Sta 10+70 (So side)

934.05 ✓

11	+50				928.95	5.1
12					28.65	5.4
	+50				28.75	5.3
13					928.05	6.0
	+50				27.65	6.4
14					26.95	7.1
T.P.	0.23	927.43	685	927.20		
	+50				26.33	1.1
15					25.73	1.7
	+50				24.73	2.7
16					23.83	3.6
	+50				22.93	4.5
B.M.			2.98	924.45	924.43	
17					21.93	5.5
	+50				21.83	5.6
18					21.23	6.2
	+50				20.63	6.8
19					20.23	7.2
	+50				20.13	7.3
20					20.03	7.4
	+50				920.23	7.2
21					20.23	7.2
	+50				20.83	6.6
22					21.03	6.4
B.M.			2.98		924.45	

→ spike in 8" B.O. 40' Lt Sta 16+80.



South St.

£ Levels

0+00 To 22+00

Apr. 28-30.