

Book- #5, Dr. 12

X

OFFICE OF COUNTY ENGINEER
RAMSEY CO. MINN.

PLAN Survey

COUNTY RD. G

From S.T.H. No. 1 To Birch Lake Blvd. S.

Road Acc't. No. W1

Date Filed 11-8-29 File W-B Twp.

PROJ. 29-W1

COUNTY ROAD G
Ramsaley Str.

White Bear Twp.

From S.T.H. H-1 to Birch Lake Blvd So.

29-W1

Sta. Point Δ Lt. Δ Rt.

64+68²

± So. Birch Lake Rd.

52+52²⁴

0°23' ± Otter Lake Rd.

33+72⁴⁷ P.O.T.

26+35²

0°26'

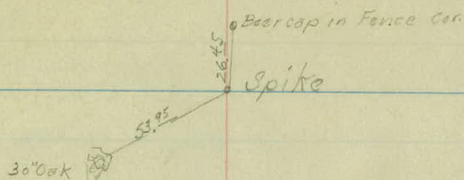
Rec.

20+72⁵⁸ P.O.T.

17+62⁸⁴ P.O.T.

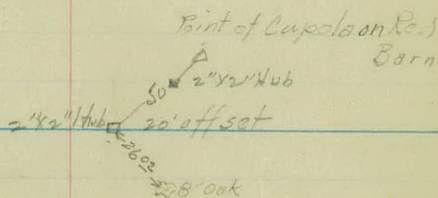
0+00

± Bald Eagle Ave.

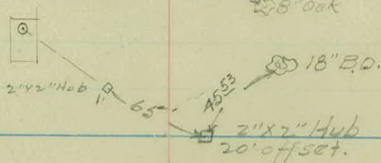


N. 1/4 Cor. Sec. 22

Ment.



Top of Vent.
on Barn.



N. W. 1/4 Sec. 23

Iron

Iron 40.

Hub

Iron

Iron 40.

Hub

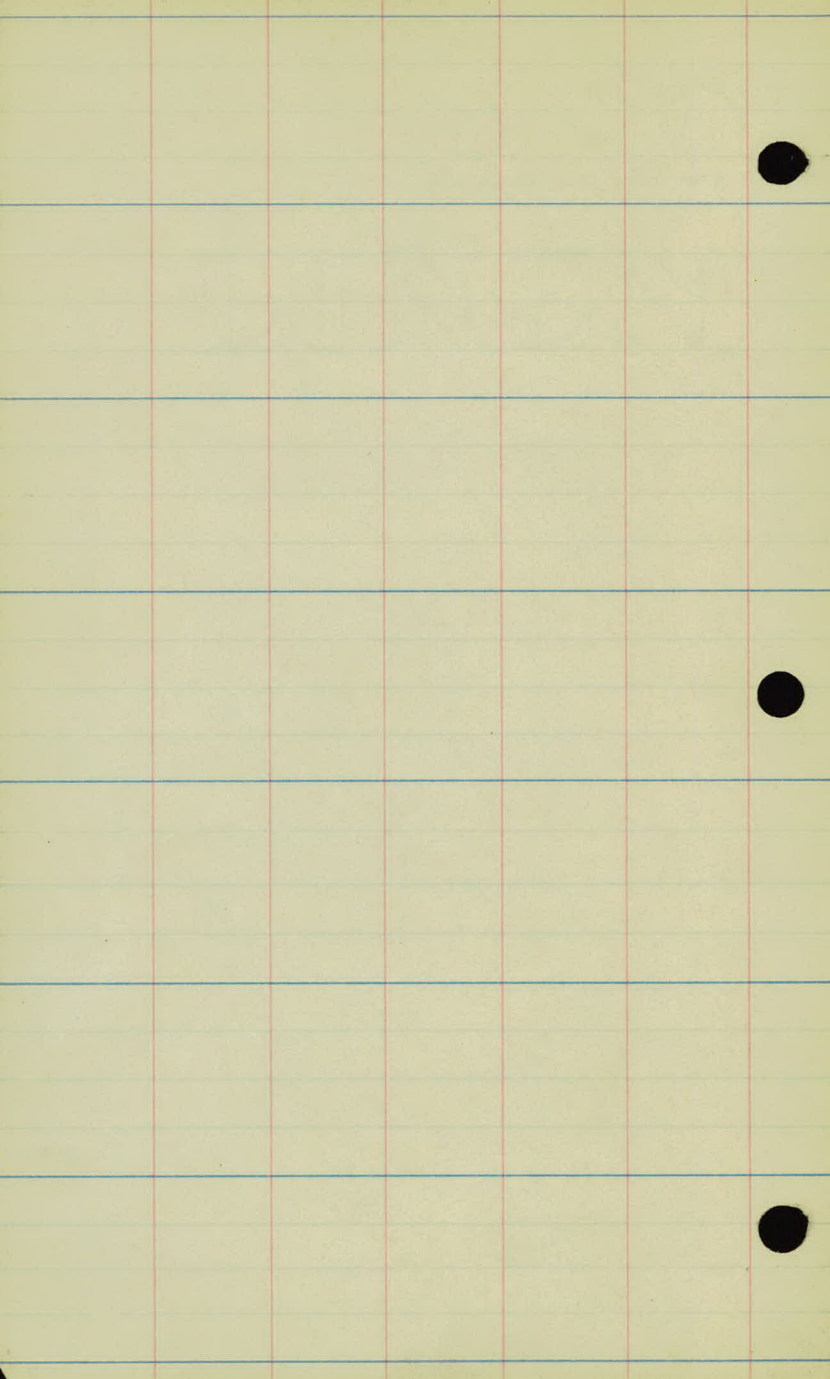
N. 1/4 Cor. Sec. 23

24" EE

Hub

54.79

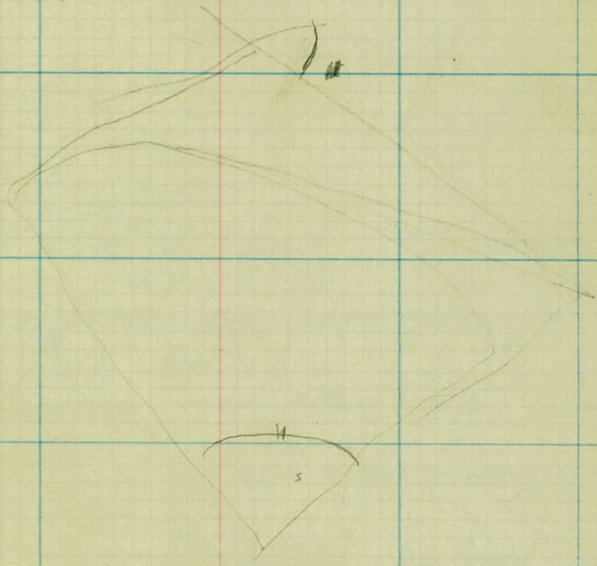
Rooting Nail in Tree.



Topog. Notes

H

C



6

5

4

3

2

1

0+00

+90 G. y Pole 31'

+34 Pr. Dr.

+ 15 Ctr 30" Conc. Walk 26'

+ 49 - T.R. 30'

+ 32 P.P. 31'

十 16 2

Cross St. ± 16 Ctr M.H. 2'

+41-T.R. 30'

+ 35 R. Dr.

+84 P.P. 32'

459-18" B.E. 40'

44-20" BE. 41'

+ 27 = 15" BE 40'

+ 10-12" BE 39'

+90-20" BE. 40"

+66-Ctr 4' Conc. Walk

+66 R.R. 33'

+ 53 Hyd 33'

+ 37 CTr. Manhole 2'

+ 37 Ctr Cross 54

+ 03. King Sqn. 15'

X 410/1

2. Сред

W. Edge Rd.

M.R.R.

+ Ctr Tract

+56 = Ctr Track

+394 Ctr Truck

+ 76 End Ring 12'

3"x10"x16' Planks

+30 Plank King 12'

14' to So. Edge traveled Rd 16' Wide.

+ 99' R.R. Xing 59.3'

+ 88 - Stop 59. 6'

+ 72. $\frac{1}{2}$ car tracks.

+ 67.	W. Edge Pav.
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+98-Guy Pole 3'

+ 96-T.F. 31'

S. T. H. #



16

15

14

13

12

11

10

9

8

7

155 145

+05-10"X32'CM.

11

+00. P.Dn.

8-6" C.W.
Sta. 11 To 12

Light
Clearing
Sta 9-10

+35-15" Triple C.W. 30'

⊕

+14 M.H. 2'

26

25

24

23

22

21

20

19

18

17

22

050
09
11 E

19 11

A blank sheet of graph paper with a light blue grid. A horizontal red line runs across the middle of the page. There are small black marks or artifacts along the right edge and bottom edge of the grid.

2

x x x x x

[illegible]

1477

Reddown

+52.24

52

50

✓
2.1

39

37

33

30

27

+80 Beg. Cultivation
+79 T.F. 25'

± Otter

+80 Beg. Cultivation

Lake Rd.

+29 T.F. 3'

52+25 End Woods +
Clearing.

Cultivated

49+80 Beg Wood

+20 Beg. Light Clearing
25'

Cultivated

+10 F. Cor. 8'

33+52

+62 = 8" Oak 40'
+46 = Cluster 5-4" Wilks.
Ditch 3 to 4' Wide.

+65 F. Cor. 10'

Cultivated

Cultivated

Clearing.

← Average 8' Thick.

64

63

62

53

Cultivated

Cultivated

Cultivated

134° 25'

Spike +68.12 ± So. Birch Lake Rd.



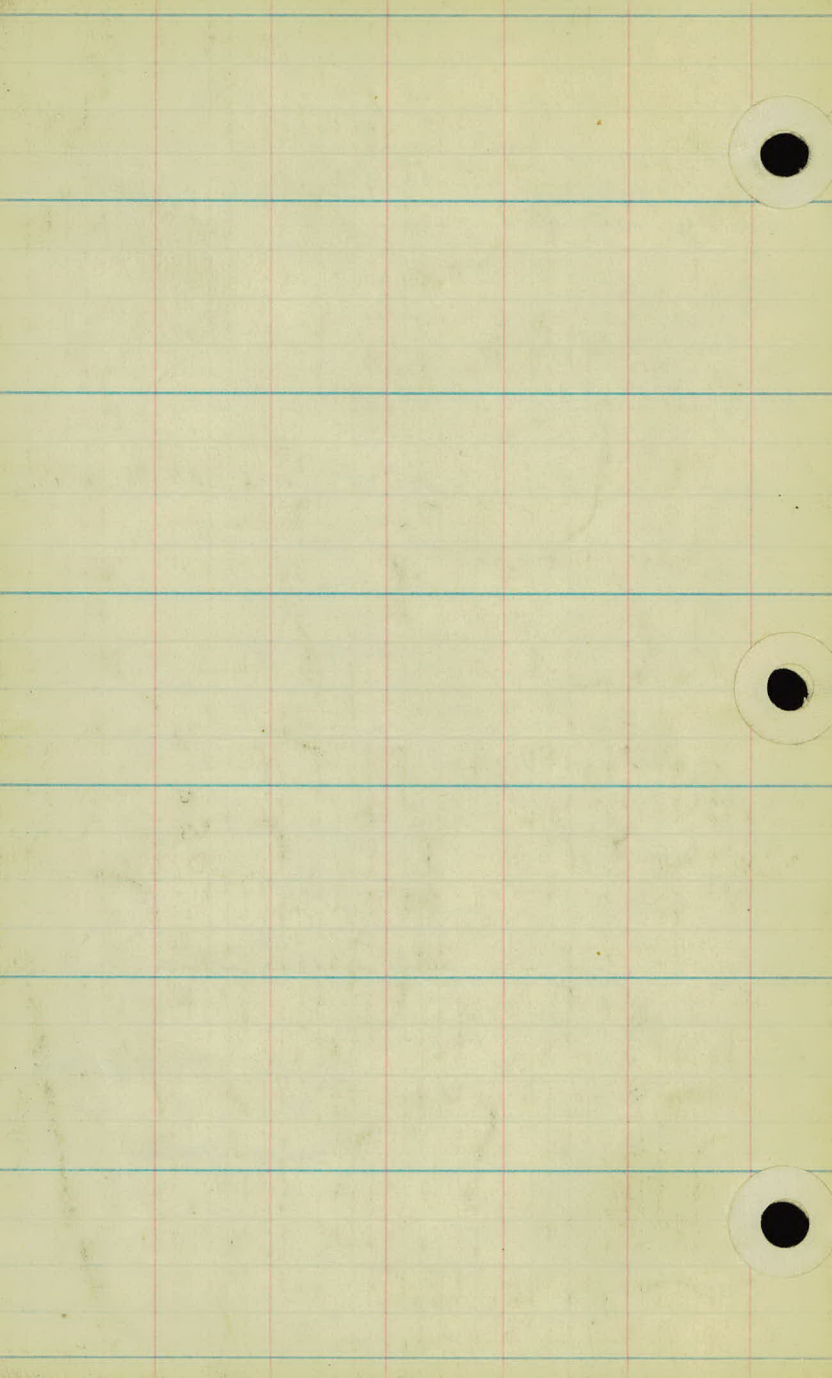
+27-24" Oak 10'

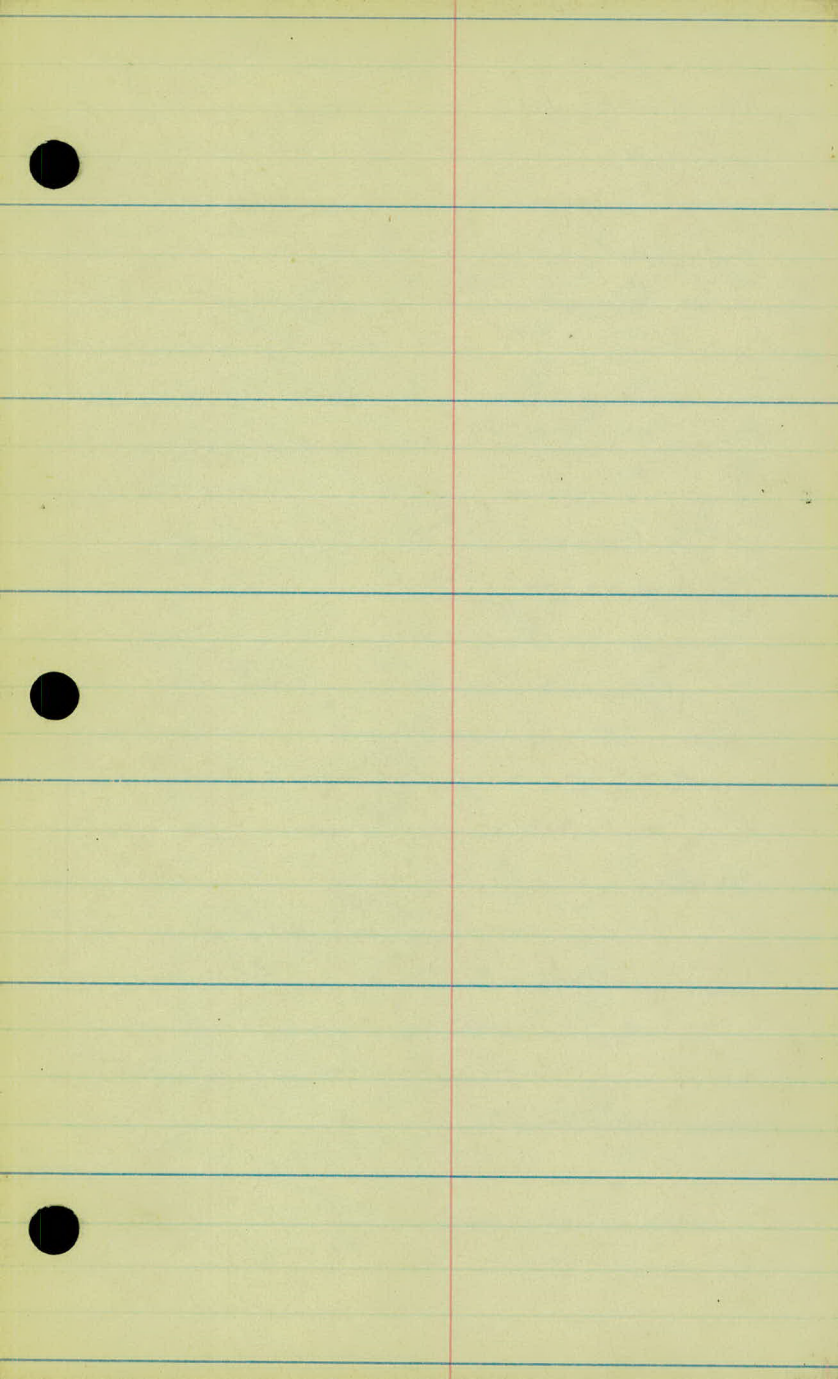


+93-12" Oak 12'



+85-18" Oak 12'





Sta.	+	H.I.	-	Elev
B.M.	3.66	929.32		925.66
T.P.	7.48	934.75	2.05	927.27
" "	3.07	929.52	8.30	926.45
" "	11.08	935.27	5.33	924.19
B.M.	4.14	935.93	3.48	931.79
T.P.	5.92	936.67	5.18	930.75
" "	3.65	933.86	6.46	930.21 (40)
" "	4.58	933.59	4.85	929.01 (35)
B.M.			2.71	930.88
T.P.	4.87	934.30	4.16	929.43 (29)
B.M.	0.72	933.74	1.28	933.02
T.P.	5.14	935.21	3.67	930.07
" "	6.62	936.50	5.33	929.88
B.M.			5.14	931.36
T.P.	10.44	942.07	4.87	931.63
B.M.			1.73	940.34
0+00				35.9

+67 Edge of Pave S.T.H. #1 35.82

+70 East Rail Steercor tracks 36.07

1 36.6

+56 Top of East Rail Mainline N.P.R.P. 36.0
Track #2

Lt £ K7

Spike in T.P. No. Birch LK + Otter LK. Road.

Spike in T.P. 100' No. Sta 52+25

Spike in 8" Oak 75' Rt Sta. 33+62

Spike in 18" Oak 38' Rt Sta. 26+50

R.R. spike in 24" B.E. 50' Rt. 12+25

Top Hyd. 33' Rt Sta. 2+55

6.2

$\frac{6.7}{50}$

6.25

$\frac{6.1}{50}$

$\frac{6.2}{50}$

6.0

$\frac{6.0}{50}$

$\frac{6.3}{40}$

$\frac{5.7}{20}$

5.5

$\frac{6.3}{14}$

$\frac{6.4}{30}$

$\frac{6.4}{40}$

$\frac{6.4}{40}$

$\frac{6.3}{20}$

6.06

$\frac{6.0}{11}$

$\frac{5.6}{14}$

$\frac{5.7}{28}$

$\frac{6.2}{40}$

Sta	+	942.07	-		
2				36.3	
+38		$\pm$ Cross Rd.		37.0	
3				38.1	
+50				38.6	
4				38.1	
5				36.1	
+16		$\pm$ Cross St.		35.7	
6				37.4	
7				32.8	
+14					33.6
8				31.4	
T.P.	4.53.	936.16	10.44	931.63	
9				31.3	
10				31.2	
11				31.8	

Lt

E

Rt

 $\frac{6.6}{40}$ $\frac{6.7}{20}$ $\frac{6.4}{14}$ $\frac{5.7}{11}$ 5.8 $\frac{5.7}{20}$ $\frac{5.7}{40}$
Top Manhole E
of Cross Rd.
 $\frac{5.0}{50}$ 5.1 $\frac{4.9}{2}$ $\frac{4.5}{50}$
 $\frac{3.4}{40}$ $\frac{3.4}{30}$ $\frac{4.0}{25}$ 4.0 $\frac{4.2}{16}$ $\frac{4.7}{22}$ $\frac{3.9}{35}$ $\frac{3.9}{40}$
 $\frac{2.9}{40}$ $\frac{3.0}{30}$ $\frac{3.8}{24}$ $\frac{3.4}{10}$ 3.5 $\frac{3.8}{8}$ $\frac{4.2}{28}$ $\frac{3.2}{34}$ $\frac{3.0}{40}$
 $\frac{2.8}{40}$ $\frac{3.1}{32}$ $\frac{4.2}{24}$ 4.0 $\frac{4.4}{24}$ $\frac{5.1}{27}$ $\frac{4.0}{34}$ $\frac{3.9}{40}$
 $\frac{5.9}{40}$ $\frac{6.6}{29}$ $\frac{5.7}{4}$ 6.0 $\frac{6.3}{25}$ $\frac{6.7}{40}$

Top of Manhole

 $\frac{6.1}{40}$ 6.4 $\frac{6.4^e}{2}$ $\frac{6.6}{40}$
 $\frac{6.7}{40}$ $\frac{7.6}{26}$ 7.7 $\frac{7.9}{26}$ $\frac{7.2}{33}$ $\frac{7.2}{40}$
 $\frac{8.7}{40}$ $\frac{9.5}{26}$ 9.3 $\frac{9.6}{18}$ $\frac{10.4}{30}$ $\frac{9.7}{34}$ $\frac{9.8}{40}$

8.5 ← Manhole 1' Rt

 $\frac{9.0}{45}$ $\frac{9.0}{40}$ $\frac{10.9}{27}$ 10.7 $\frac{11.0}{20}$ $\frac{11.3}{40}$
 $\frac{5.7}{45}$ $\frac{5.7}{40}$ $\frac{6.0}{32}$ $\frac{6.6}{29}$ $\frac{5.0}{4}$ 4.9 $\frac{5.0}{7}$ $\frac{6.0}{16}$ $\frac{6.4}{40}$ $\frac{6.4}{45}$
 $\frac{5.5}{45}$ $\frac{5.5}{40}$ $\frac{5.6}{33}$ $\frac{6.1}{28}$ $\frac{4.9}{7}$ 5.0 $\frac{5.1}{15}$ $\frac{6.2}{31}$ $\frac{6.2}{45}$
 $\frac{3.8}{45}$ $\frac{3.8}{40}$ $\frac{4.0}{18}$ $\frac{4.6}{16}$ 4.4 $\frac{4.7}{15}$ $\frac{6.3}{23}$ $\frac{6.3}{25}$ $\frac{5.6}{27}$ $\frac{5.0}{40}$ $\frac{5.9}{45}$

Sta	+	M.I.	-	Elev.
12		936.16		31.3
13				30.4
14				29.7
T.P.	5.56	935.43	6.29	929.87
15				29.4
16				29.7
17				30.5
18				30.4
19				29.5
20				29.7
T.P.	3.81	933.87	5.37	930.06
21				30.3
22				30.5
23				29.5
24				29.9

Lt

E

Rt.

$\frac{5.0}{45}$	$\frac{5.0}{40}$	$\frac{4.9}{26}$	4.9	$\frac{6.2}{19}$	$\frac{6.5}{29}$	$\frac{5.3}{33}$	$\frac{5.3}{45}$
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$\frac{6.1}{45}$	$\frac{6.1}{40}$	$\frac{6.3}{32}$	$\frac{7.0}{31}$	$\frac{7.0}{28}$	$\frac{6.1}{24}$	5.8	$\frac{5.5}{5}$	$\frac{7.4}{22}$	$\frac{6.3}{27}$	$\frac{6.3}{45}$
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$\frac{7.3}{45}$	$\frac{7.3}{40}$	$\frac{8.0}{30}$	$\frac{7.1}{19}$	$\frac{7.8}{18}$	6.5	$\frac{8.0}{17}$	$\frac{8.1}{23}$	$\frac{7.2}{25}$	$\frac{7.8}{29}$	$\frac{7.0}{40}$	$\frac{7.0}{45}$
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$\frac{7.1}{45}$	$\frac{7.1}{40}$	$\frac{6.8}{34}$	$\frac{7.4}{29}$	$\frac{6.1}{23}$	$\frac{6.5}{20}$	$\frac{7.4}{18}$	$\frac{6.6}{12}$	6.0	$\frac{6.6}{13}$	$\frac{7.5}{20}$	$\frac{6.4}{27}$	$\frac{6.2}{40}$	$\frac{6.2}{40}$
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$\frac{6.6}{45}$	$\frac{6.6}{40}$	$\frac{6.6}{17}$	5.7	$\frac{6.5}{13}$	$\frac{7.4}{18}$	$\frac{6.0}{21}$	$\frac{6.5}{25}$	$\frac{6.5}{45}$
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$\frac{5.5}{45}$	$\frac{5.5}{43}$	$\frac{5.3}{19}$	$\frac{6.2}{18}$	4.9	$\frac{5.1}{13}$	$\frac{5.9}{19}$	$\frac{4.8}{21}$	$\frac{5.0}{40}$	$\frac{5.0}{45}$
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$\frac{5.7}{45}$	$\frac{5.7}{40}$	$\frac{5.5}{19}$	$\frac{6.0}{17}$	5.0	$\frac{5.2}{11}$	$\frac{5.9}{16}$	$\frac{5.3}{18}$	$\frac{5.4}{40}$	$\frac{5.4}{45}$
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$\frac{6.3}{45}$	$\frac{6.3}{40}$	$\frac{6.1}{19}$	$\frac{6.8}{17}$	5.9	$\frac{6.2}{7}$	$\frac{6.7}{16}$	$\frac{6.0}{18}$	$\frac{5.9}{40}$	$\frac{5.9}{45}$
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$\frac{6.2}{45}$	$\frac{6.2}{40}$	$\frac{5.9}{19}$	$\frac{6.4}{18}$	5.7	$\frac{6.1}{10}$	$\frac{6.8}{16}$	$\frac{6.1}{18}$	$\frac{6.2}{40}$	$\frac{6.2}{45}$
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$\frac{3.8}{45}$	$\frac{3.8}{40}$	$\frac{3.9}{21}$	$\frac{4.7}{20}$	$\frac{4.1}{13}$	3.6	$\frac{4.5}{18}$	$\frac{4.0}{20}$	$\frac{4.0}{45}$
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$\frac{3.8}{45}$	$\frac{3.8}{40}$	$\frac{4.1}{20}$	$\frac{5.0}{19}$	3.4	$\frac{4.1}{12}$	$\frac{4.9}{18}$	$\frac{3.9}{20}$	$\frac{4.2}{40}$	$\frac{4.2}{45}$
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$\frac{5.1}{45}$	$\frac{5.1}{40}$	$\frac{5.2}{22}$	$\frac{5.6}{20}$	4.4	$\frac{5.7}{17}$	$\frac{5.3}{18}$	$\frac{5.7}{40}$	$\frac{5.7}{45}$
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$\frac{5.0}{45}$	$\frac{4.6}{40}$	$\frac{4.1}{21}$	$\frac{5.4}{20}$	$\frac{4.6}{18}$	4.0	$\frac{5.6}{18}$	$\frac{4.7}{20}$	$\frac{4.5}{40}$	$\frac{4.5}{45}$
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Sta 25	+	H.I. 933.67	—	Elev	29.9
26					29.5
+25		= E. Shoulder of Ditch			29.1
+34		E of County Ditch			28.7
+44		W. Shoulder of Co. Ditch.			29.2
B.M.	0.62	933.64	0.86	933.01	933.02
27					30.0
28					30.5
T.P.	422	933.65	421	929.43	
29					30.4
30					30.4
31					30.3
32					30.3
33					30.2
+50		E. Shoulder of Ditch			30.0
+52		Bottom "			28.0
+57		W. Shoulder of Ditch			29.9
+60					29.2

$$\frac{4.7}{4.5} \quad \frac{4.7}{4.0} \quad \frac{4.5}{2.2} \quad \frac{5.2}{2.1} \quad 4.0 \quad \frac{4.9}{1.6} \quad \frac{4.5}{4.0} \quad \frac{4.5}{4.5}$$

$$\frac{3.7}{4.5} \quad \frac{3.7}{4.0} \quad \frac{4.6}{2.2} \quad \frac{5.2}{1.9} \quad 4.4 \quad \frac{4.8}{1.6} \quad \frac{3.5}{4.0} \quad \frac{3.5}{4.5}$$

$$\frac{4.6}{4.5} \quad \frac{4.6}{4.0} \quad \frac{4.6}{2.0} \quad \frac{5.6}{1.7} \quad 4.8 \quad \frac{5.5}{1.2} \quad \frac{4.6}{1.6} \quad \frac{4.3}{4.0} \quad \frac{4.3}{4.5}$$

Bottom of Culvert

Bottom Culvert

$$\frac{10.1}{4.0} \quad \frac{10.9}{1.9} \quad \frac{5.9}{1.9} \quad 5.2 \quad \frac{5.8}{1.1} \quad \frac{10.8}{1.1} \quad \frac{9.9}{4.0}$$

$$\frac{4.4}{4.5} \quad \frac{4.4}{4.0} \quad \frac{4.6}{2.7} \quad \frac{5.6}{1.3} \quad 4.7 \quad \frac{4.8}{1.3} \quad \frac{4.0}{1.8} \quad \frac{4.2}{4.0} \quad \frac{4.2}{4.5}$$

$$\frac{3.6}{2} \quad \frac{4.6}{1.0} \quad \frac{4.8}{1.0} \quad \frac{4.8}{4.0}$$

Top of Stake Sta. 29 + 00

$$\frac{3.1}{3} \quad \frac{4.0}{3} \quad \frac{4.5}{7} \quad \frac{4.6}{4.0} \quad \frac{4.6}{4.5}$$

$$\frac{3.3}{6} \quad \frac{4.4}{6} \quad \frac{4.5}{1.6} \quad \frac{4.6}{4.0} \quad \frac{4.6}{4.5}$$

$$\frac{3.3}{4} \quad \frac{4.4}{4} \quad \frac{4.8}{4.0} \quad \frac{4.8}{4.5}$$

$$\frac{3.4}{8} \quad \frac{4.7}{8} \quad \frac{4.7}{4.5}$$

$$\frac{3.4}{9} \quad \frac{4.9}{9} \quad \frac{4.8}{4.5}$$

$$\frac{3.5}{3} \quad \frac{3.5}{3} \quad \frac{5.3}{5} \quad \frac{4.5}{1.0} \quad \frac{4.7}{4.5}$$

$$\frac{3.7}{4} \quad \frac{5.2}{4} \quad \frac{5.2}{2.0} \quad \frac{5.8}{4.0} \quad \frac{5.8}{4.5}$$

$$\frac{5.7}{2.0} \quad \frac{6.1}{2.0} \quad \frac{6.2}{4.0} \quad \frac{6.3}{4.5}$$

$$\frac{3.8}{3} \quad \frac{4.8}{3} \quad \frac{4.3}{8} \quad \frac{3.6}{2.0} \quad \frac{3.4}{4.0} \quad \frac{3.4}{4.5}$$

$$\frac{4.5}{2.0} \quad \frac{4.8}{2.0} \quad \frac{4.9}{4.5}$$

Sta.	+	H.I.	-	Orig Elev.
		933.65		
	2.78	933.66	2.77	930.88
34				28.9
35				29.7
36				30.2
37				30.4
38				29.9
39				30.0
40				29.9
T.P.	6.21	936.42	3.46	930.20
41				30.9
42				32.2
43				33.4
44				33.4
45				32.1
46				31.4

L1.

L

R1

$$4.8 \quad \frac{3.7}{3} \quad \frac{4.9}{20} \quad \frac{5.1}{40} \quad \frac{5.1}{45}$$

$$4.0 \quad \frac{4.9}{4} \quad \frac{4.9}{20} \quad \frac{4.7}{45}$$

$$3.5 \quad \frac{4.8}{3} \quad \frac{4.2}{20} \quad \frac{4.4}{40} \quad \frac{4.4}{45}$$

$$3.3 \quad \frac{4.7}{4} \quad \frac{4.7}{45}$$

$$3.8 \quad \frac{4.7}{5} \quad \frac{4.3}{9} \quad \frac{4.7}{45}$$

$$3.7 \quad \frac{4.9}{6} \quad \frac{4.0}{11} \quad \frac{4.4}{12} \quad \frac{4.9}{45}$$

$$3.8 \quad \frac{4.5}{6} \quad \frac{4.6}{40} \quad \frac{4.6}{45}$$

$$5.5 \quad \frac{5.8}{12} \quad \frac{6.2}{14} \quad \frac{6.5}{40} \quad \frac{6.5}{45}$$

$$4.2 \quad \frac{4.4}{10} \quad \frac{4.9}{13} \quad \frac{5.2}{40} \quad \frac{5.2}{45}$$

$$3.0 \quad \frac{3.7}{5} \quad \frac{4.7}{14} \quad \frac{4.5}{40} \quad \frac{4.5}{45}$$

$$3.0 \quad \frac{3.7}{3} \quad \frac{4.3}{15} \quad \frac{4.4}{45}$$

$$4.3 \quad \frac{4.9}{13} \quad \frac{5.1}{40} \quad \frac{5.1}{45}$$

$$5.0 \quad \frac{5.5}{14} \quad \frac{5.7}{40} \quad \frac{5.7}{45}$$

Sta.	+	H.I.	-	Elev	
47		936.42 ✓		30.5 ✓	
T.P.	5.65	936.38 ✓	5.69	930.73 ✓	
48				30.5 ✓	
49				31.4	
50				31.5	
51				31.4	
52				31.7	
B.M.	1.63	933.42 ✓	4.60	931.78 ✓	931.79 ✓
+ 52		± other Lk. Rd.		29.8	
53				29.0	
54				28.7	
55				28.6	
56				27.9	
57				27.5	
58				23.6	
T.P.	12.52	936.34 ✓	9.60	923.82 ✓	

$$\frac{5.9}{11} \quad \frac{5.3}{13} \quad \frac{5.8}{45}$$

$$\frac{5.9}{5} \quad \frac{5.4}{40} \quad \frac{5.8}{45}$$

$$\frac{5.0}{7} \quad \frac{4.7}{45}$$

$$\frac{4.9}{7} \quad \frac{4.3}{17} \quad \frac{5.0}{45}$$

$$\frac{5.0}{11} \quad \frac{4.8}{40} \quad \frac{5.2}{45}$$

$$\frac{4.7}{11} \quad \frac{6.1}{40} \quad \frac{6.1}{45}$$

Spike in T.P. 100' ~~N~~ of Sta. 52+25

$$\frac{2.1}{50} \quad \frac{3.3}{20} \quad \frac{3.6}{20} \quad \frac{3.4}{20} \quad \frac{3.7}{50}$$

$$\frac{4.7}{45} \quad \frac{4.7}{40} \quad \frac{4.6}{20} \quad \frac{4.4}{20} \quad \frac{4.5}{40} \quad \frac{4.3}{40} \quad \frac{4.3}{45}$$

$$\frac{5.0}{45} \quad \frac{5.0}{40} \quad \frac{4.8}{20} \quad \frac{4.7}{20} \quad \frac{4.9}{20} \quad \frac{4.6}{40} \quad \frac{4.6}{45}$$

$$\frac{5.4}{45} \quad \frac{5.4}{40} \quad \frac{5.2}{20} \quad \frac{4.8}{20} \quad \frac{5.3}{20} \quad \frac{5.6}{40} \quad \frac{5.6}{45}$$

$$\frac{6.3}{45} \quad \frac{6.3}{40} \quad \frac{6.0}{20} \quad \frac{5.5}{20} \quad \frac{5.8}{20} \quad \frac{6.2}{40} \quad \frac{6.2}{45}$$

$$\frac{7.3}{45} \quad \frac{7.0}{40} \quad \frac{6.5}{20} \quad \frac{5.9}{20} \quad \frac{6.0}{20} \quad \frac{6.3}{40} \quad \frac{6.3}{45}$$

$$\frac{10.1}{45} \quad \frac{10.1}{40} \quad \frac{10.3}{20} \quad \frac{9.8}{20} \quad \frac{10.3}{20} \quad \frac{10.3}{45}$$

Sta.	+	H.I.	-	Elev
59		936.34		23.6
60				27.9
61				31.3
62				32.5
63				32.0
64				32.0
+37				31.7
+43				29.6
+54				33.0

+68.12		End of Proj.		✓ 33.5
B.M.		✓ 3.38	932.96	
B.M.	1.10	934.12	933.02	
27				

28

29

Lt

±

Rt

$$\frac{12.4}{45} \quad \frac{12.4}{40} \quad \frac{12.8}{20} \quad 12.7 \quad \frac{13.0}{20} \quad \frac{13.0}{45}$$

$$\frac{8.2}{45} \quad \frac{8.2}{40} \quad \frac{8.5}{20} \quad 8.4 \quad \frac{8.0}{20} \quad \frac{7.6}{40} \quad \frac{7.4}{45}$$

$$\frac{6.7}{45} \quad \frac{6.3}{40} \quad \frac{5.9}{11} \quad 5.0 \quad \frac{6.1}{20} \quad \frac{6.2}{45}$$

$$\frac{4.5}{45} \quad \frac{4.4}{8} \quad 3.8 \quad \frac{3.5}{13} \quad \frac{4.2}{20} \quad \frac{4.7}{40} \quad \frac{4.7}{45}$$

$$\frac{4.6}{45} \quad \frac{4.6}{40} \quad \frac{4.8}{20} \quad 4.3 \quad \frac{3.0}{12} \quad \frac{4.2}{25} \quad \frac{4.3}{45}$$

$$\frac{4.9}{45} \quad \frac{4.9}{27} \quad \frac{4.1}{9} \quad 4.3 \quad \frac{3.6}{5} \quad \frac{5.0}{20} \quad \frac{4.4}{30} \quad \frac{5.1}{40} \quad \frac{6.5}{48}$$

$$\frac{4.5}{45} \quad \frac{4.5}{40} \quad \frac{4.1}{20} \quad 4.6 \quad \frac{6.7}{4} \quad \frac{6.4}{9} \quad \frac{3.3}{15} \quad \frac{2.9}{33} \quad \frac{3.4}{46}$$

$$\frac{4.1}{45} \quad \frac{4.1}{40} \quad \frac{4.7}{32} \quad \frac{4.2}{23} \quad \frac{4.7}{11} \quad \frac{6.6}{4} \quad 6.7 \quad \frac{6.2}{4} \quad \frac{3.5}{10} \quad \frac{2.8}{29} \quad \frac{3.4}{42}$$

$$\frac{4.5}{45} \quad \frac{4.1}{25} \quad \frac{7.1}{15} \quad 3.3 \quad \frac{2.8}{16} \quad \frac{3.3}{33} \quad \frac{4.8}{41} \quad \frac{4.8}{45}$$

$$\frac{4.1}{50} \quad \frac{4.5}{40} \quad \frac{6.3}{35} \quad \frac{5.3}{30} \quad \frac{5.4}{22} \quad 2.8 \quad \frac{5.3}{19} \quad \frac{4.8}{29} \quad \frac{4.5}{40}$$

R.R. spike in 20" oak 60' Lt Sta 64+43.

Spike in 18" oak 58' Rt Sta. 26+50.

$$\frac{5.0}{45} \quad \frac{5.0}{20} \quad \frac{4.8}{10} \quad \frac{5.0}{4} \quad (4.1)$$

$$\frac{4.5}{45} \quad \frac{4.5}{41} \quad \frac{4.9}{23} \quad \frac{4.7}{7} \quad \frac{5.5}{5} \quad (3.6)$$

$$\frac{5.0}{45} \quad \frac{5.0}{20} \quad \frac{4.8}{7} \quad \frac{5.4}{4} \quad (3.7)$$

+ H.I. - Elev.

30

934.12 ✓

31

T.P.

3.99

933.33 ✓

4.78

929.34 ✓

32

33

34

35

36

37

38

T.P.

7.29

936.71 ✓

3.91

929.42 ✓

39

40

41

42

43

Lt

$$\frac{5.0}{4.5} \frac{5.0}{4.0} \frac{5.2}{2.0} \frac{4.7}{8} \frac{5.7}{4} \quad (3.7)$$

$$\frac{4.7}{4.5} \frac{4.7}{4.0} \frac{5.1}{2.0} \frac{4.9}{6} \frac{5.6}{3} \quad (3.8)$$

$$\frac{4.3}{4.5} \frac{4.5}{1.8} \frac{4.5}{5} \frac{5.1}{3} \quad (3.0)$$

$$\frac{4.2}{4.5} \frac{4.2}{3.0} \frac{4.6}{1.8} \frac{4.4}{5} \frac{5.0}{3} \quad (3.1)$$

$$\frac{4.6}{4.5} \frac{4.6}{1.8} \frac{4.5}{8} \frac{5.5}{4} \quad (4.4)$$

$$\frac{4.6}{4.5} \frac{4.6}{4.0} \frac{5.0}{2.0} \frac{4.6}{7} \frac{5.7}{3} \quad (3.6)$$

$$\frac{4.4}{4.5} \frac{4.5}{2.2} \frac{4.4}{6} \frac{5.2}{4} \quad (3.1)$$

$$\frac{4.5}{4.5} \frac{4.7}{2.2} \frac{3.8}{9} \frac{5.3}{5} \quad (2.9)$$

$$\frac{4.2}{4.5} \frac{4.2}{4.0} \frac{4.7}{1.7} \frac{4.5}{6} \frac{5.5}{4} \quad (3.4)$$

$$\frac{7.8}{4.5} \frac{7.8}{1.6} \frac{7.6}{7} \frac{8.7}{4} \quad (6.7)$$

$$\frac{7.8}{4.5} \frac{7.6}{4.0} \frac{7.6}{6} \frac{8.3}{4} \quad (6.8)$$

$$\frac{6.8}{4.5} \frac{6.8}{4.0} \frac{7.0}{1.9} \frac{6.6}{8} \frac{7.0}{5} \quad (4.8)$$

$$\frac{6.0}{4.5} \frac{5.9}{4.0} \frac{5.4}{3.0} \frac{5.9}{2.2} \frac{5.5}{1.1} \quad (4.5)$$

$$\frac{4.6}{4.5} \frac{4.6}{2.0} \frac{5.0}{2.2} \frac{4.4}{9} \frac{3.1}{3} \quad (3.3)$$

936.71 ✓

44

T.P.

3.81

935.53 ✓

4.99

931.72 ✓

45

46

47

T.P.

6.49

937.12 ✓

4.80

930.73 ✓

48

49

50

51

52

T.P.

3.62

935.29 ✓

5.55

931.67 ✓

B.M.

3.52

931.77 ✓

931.79 orig

$$\frac{3.9}{45} \quad \frac{3.9}{40} \quad \frac{4.7}{20} \quad \frac{3.6}{5} \quad (3.3)$$

$$\frac{3.8}{45} \quad \frac{3.8}{40} \quad \frac{3.3}{30} \quad \frac{3.9}{22} \quad \frac{2.8}{6} \quad (3.4)$$

$$\frac{4.6}{45} \quad \frac{3.6}{35} \quad \frac{4.6}{23} \quad \frac{4.4}{14} \quad (4.1)$$

$$\frac{5.0}{50} \quad \frac{4.2}{40} \quad \frac{4.5}{30} \quad \frac{5.3}{21} \quad (5.0)$$

$$\frac{6.8}{50} \quad \frac{6.8}{45} \quad \frac{6.0}{35} \quad \frac{6.6}{30} \quad \frac{7.0}{18} \quad (6.7)$$

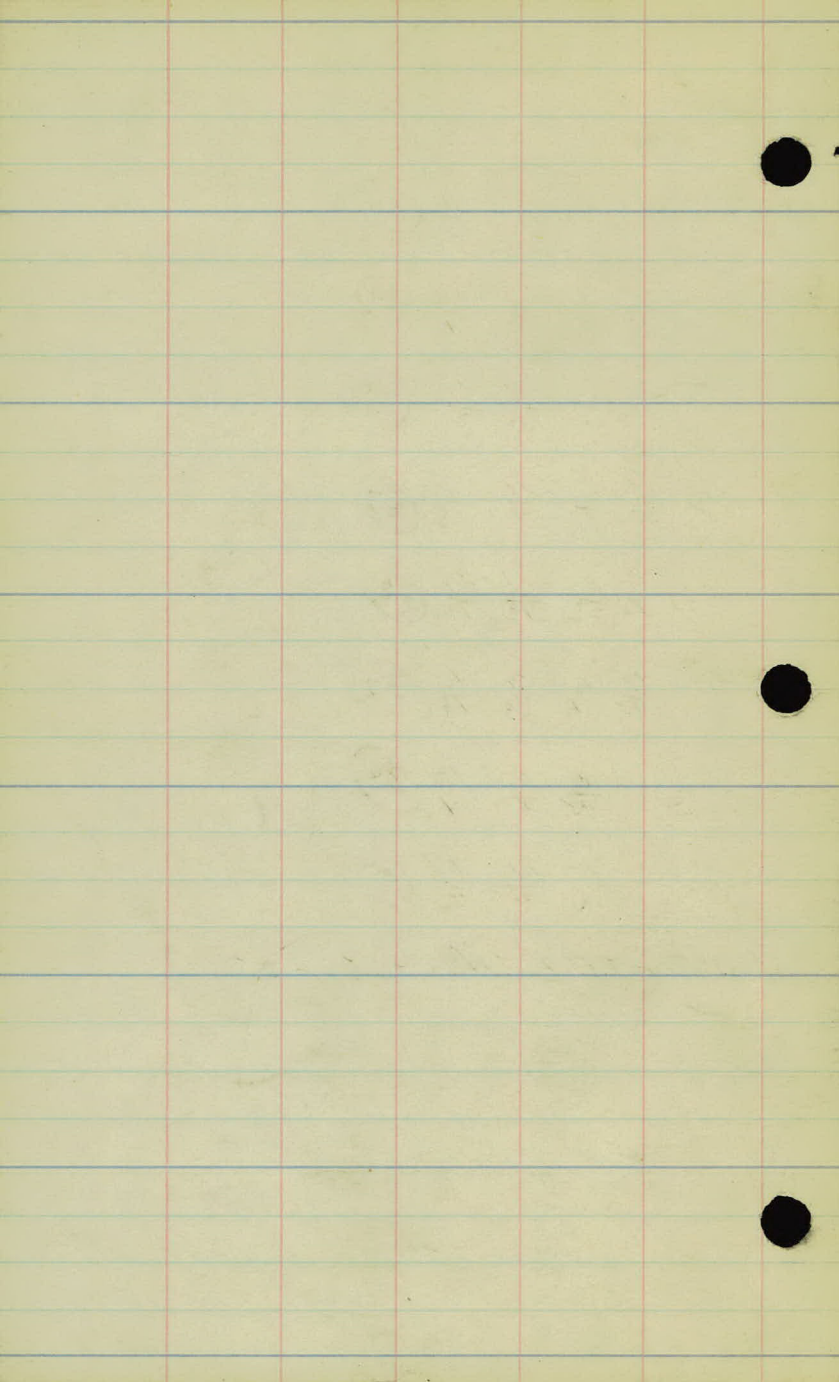
$$\frac{6.1}{45} \quad \frac{5.7}{40} \quad \frac{6.2}{22} \quad \frac{6.5}{19} \quad \frac{5.9}{13} \quad (5.8)$$

$$\frac{6.0}{45} \quad \frac{6.0}{40} \quad \frac{5.7}{23} \quad \frac{6.0}{18} \quad (5.7)$$

$$\frac{6.0}{45} \quad \frac{6.0}{40} \quad \frac{6.2}{14} \quad (5.8)$$

$$\frac{6.1}{45} \quad \frac{6.1}{30} \quad \frac{6.4}{20} \quad (5.5)$$

Spike in T.P. 100' No. 5 to 52 + 25



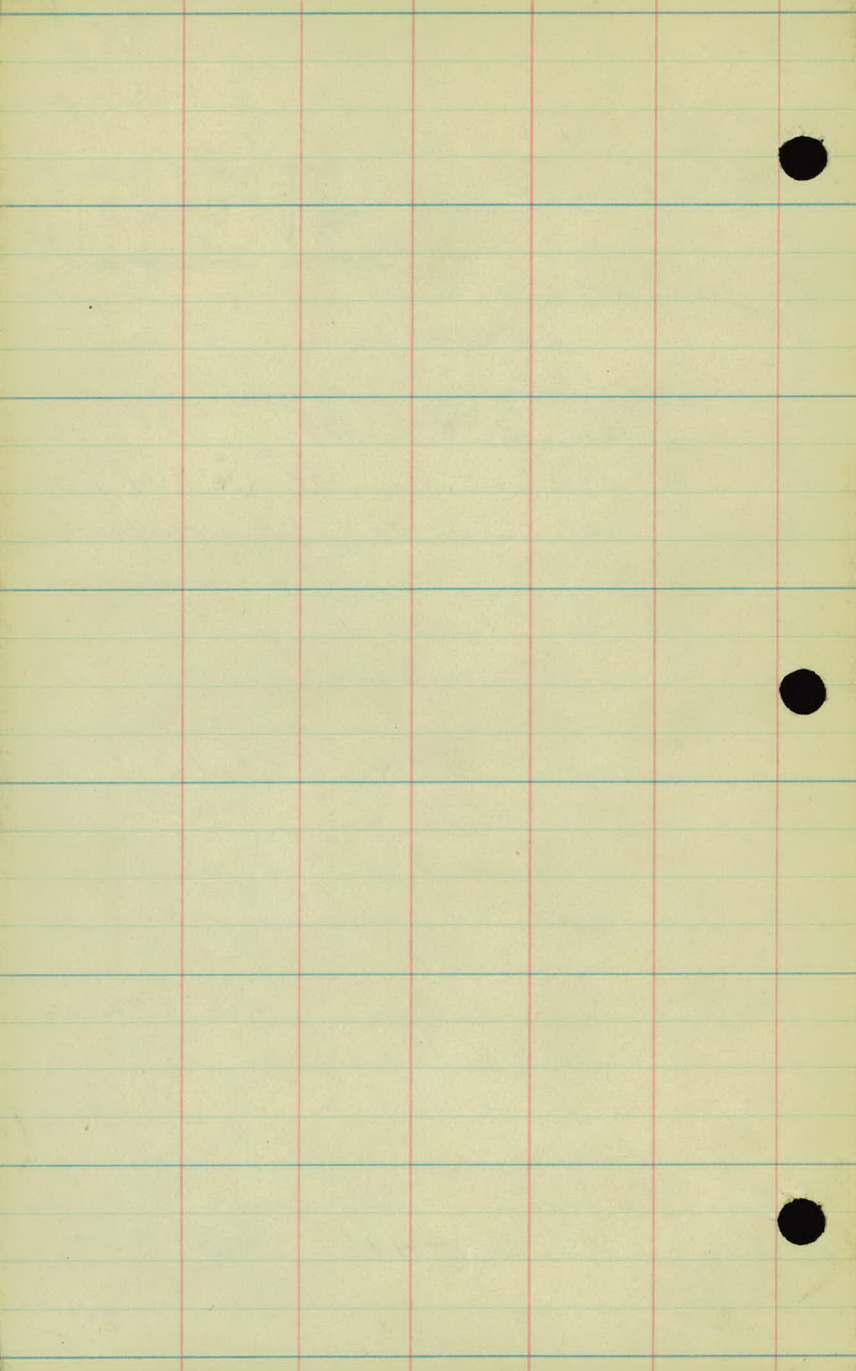
RAMBLEY AVE.

10/16/29

White Bear Twp.

O.R.V.K.
W.S.M.

- ✓ 9+00 to 12+00 - Cl. 20' wide. = 0.14 ac.
- ✓ 12+00 - R^t - P-15" X 20' C.M.
- ✓ 16+05 - Rem. - P-18" P₃ X 48' Haul 2.00
- * Pitch on R^t + L^t - 16+00 to 20+00
- ✓ 20+50 - R^t + L^t - No culv. req.
- * Ditch on R^t + L^t - 20+50 ahead to 23+50
- 23+50 - Rem. P-18" P₃ X 48' Haul 2.75
- ✓ 26+34 - Extend ~~on R^t~~ 36" X 10' C.M. L^t
36" X 16' C.M. R^t.
- ✓ 26+50 to 40+00 - Gr. 15' wide = 0.46 ac
- ✓ 25+00 - R^t - P-15" X 20'
- ✓ 25+00 - L^t - "
- ✓ 30+30 - R^t - "
- ✓ 27+00 - L^t - "
- * Ditch grades Sta. 34+00 back to Co. Ditch
- ✓ 37+00 - R^t - P-15" X 20'
- ✓ 37+00 - L^t - "
- ✓ 49+50 - R^t - "
- ✓ 49+50 - L^t - "
- ✓ 40+00 to 52+50 - Gr. 25' wide = 0.72 ac
- ✓ 52+52 - R^t - P-15" X 30'
- ✓ 53+52 - L^t - "
- ✓ 56+20 - R^t - P-15" X 20'
- ✓ 56+20 - L^t - "
- ✓ 58+50 - P-18" X P₃ 48' Haul 6.00
- ✓ 63+00 to 64 - Cl. & Gr. 0.03 ac
- ✓ 64+40 - P-18" P₃ X 48' Haul 6.56



29-W-1

B.NI.	2.35	942.69		940.34	
3		⁷⁹⁹ 93470		36.6	6.1
750				36.8	5.9
4				36.7	6.0
750				36.2	6.5
5				35.6	7.1
6				34.4	8.3
T.P.	1.39	936.09	7.99	93470	
7				33.3	2.8
8				32.5	3.60
9				31.8	4.3
10				31.4	4.7
11				31.1	5.0
T.P.	3.53	93537	4.25	93184	
12				30.9	4.5
13				30.7	4.7
			4.01		

$$\begin{array}{l} 3^{30}/\overset{\wedge}{4.1} \quad 1^{80}/\overset{\wedge}{4.7} \quad 4.2 \quad 4.1 \quad 4.7 \quad 5.0 \quad 4.7 \quad 4.8 \quad 5.3 \quad 4.6 \quad 4.7 \quad 6/\overset{\wedge}{4.8} \quad 1^{80}/\overset{\wedge}{4.8} \\ 3^{30}/\overset{\wedge}{7.20} \quad 1^{80}/\overset{\wedge}{7.24} \quad 40 \quad 30 \quad 15 \quad 10 \quad 11.4 \quad 18 \quad 22 \quad 34 \quad 40 \quad 3/\overset{\wedge}{7.13} \quad 1^{80}/\overset{\wedge}{7.23} \end{array}$$

$$\begin{array}{l} 3^{30}/\overset{\wedge}{7.5} \quad 1^{80}/\overset{\wedge}{7.4} \quad 3.6 \quad 3.6 \quad 4.5 \quad 4.1 \quad 4.2 \quad 4.4 \quad 4.9 \quad 3.9 \quad 3.7 \quad 5/\overset{\wedge}{4.0} \quad 1^{80}/\overset{\wedge}{4.4} \\ 3^{30}/\overset{\wedge}{7.14} \quad 1^{80}/\overset{\wedge}{7.25} \quad 40 \quad 31 \quad 24 \quad 18 \quad 11.7 \quad 18 \quad 28 \quad 34 \quad 40 \quad 3/\overset{\wedge}{7.19} \quad 1^{80}/\overset{\wedge}{7.25} \end{array}$$

$$\begin{array}{l} 3^{30}/\overset{\wedge}{7.6} \quad 1^{80}/\overset{\wedge}{4.9} \quad 3.4 \quad 3.8 \quad 4.9 \quad 4.9 \quad 4.7 \quad 5.0 \quad 5.7 \quad 4.6 \quad 5.1 \quad 4.5 \quad 0/\overset{\wedge}{5.2} \quad 2/\overset{\wedge}{4.9} \\ 3^{30}/\overset{\wedge}{7.24} \quad 1^{80}/\overset{\wedge}{7.12.1} \quad 40 \quad 30 \quad 24 \quad 12 \quad 11.3 \quad 23 \quad 27 \quad 34 \quad 37 \quad 40 \quad 1^{80}/\overset{\wedge}{7.11.8} \quad 3/\overset{\wedge}{7.11.1} \end{array}$$

$$\begin{array}{l} 0/\overset{\wedge}{6.0} \quad 1^{80}/\overset{\wedge}{6.0} \quad 4.9 \quad 3.3 \quad 6.0 \quad 6.1 \quad 5.6 \quad 6.1 \quad 6.5 \quad 6.0 \quad 6.0 \quad 0/\overset{\wedge}{6.2} \quad 0/\overset{\wedge}{6.5} \\ 3/\overset{\wedge}{7.0.5} \quad 1^{80}/\overset{\wedge}{7.0.5} \quad 40 \quad 33 \quad 28 \quad 17 \quad 10.9 \quad 24 \quad 27 \quad 33 \quad 40 \quad 1^{80}/\overset{\wedge}{7.0.3} \quad 2/\overset{\wedge}{7.0.0} \end{array}$$

$$\begin{array}{l} 9^{30}/\overset{\wedge}{7.2} \quad 1^{80}/\overset{\wedge}{7.1} \quad 6.6 \quad 7.3 \quad 7.2 \quad 6.5 \quad 6.7 \quad 7.0 \quad 7.3 \quad 7.3 \quad 0/\overset{\wedge}{7.0} \quad 9/\overset{\wedge}{7.3} \\ 9^{30}/\overset{\wedge}{7.0.1} \quad 1^{80}/\overset{\wedge}{7.11.0} \quad 40 \quad 68 \quad 19 \quad 5 \quad 10.4 \quad 24 \quad 31 \quad 40 \quad 1^{80}/\overset{\wedge}{7.11.1} \quad 2/\overset{\wedge}{7.0.2} \end{array}$$

$$\begin{array}{l} 9^{30}/\overset{\wedge}{7.9} \quad 1^{80}/\overset{\wedge}{8.2} \quad 7.4 \quad 7.7 \quad 8.3 \quad 8.2 \quad 8.4 \quad 8.4 \quad 8.4 \quad 7.8 \quad 7.7 \quad 0/\overset{\wedge}{8.5} \quad 2/\overset{\wedge}{8.4} \\ 9^{30}/\overset{\wedge}{7.0.4} \quad 1^{80}/\overset{\wedge}{7.11.1} \quad 40 \quad 33 \quad 25 \quad 18 \quad 9.1 \quad 19 \quad 29 \quad 33 \quad 40 \quad 1^{80}/\overset{\wedge}{7.0.8} \quad 2/\overset{\wedge}{7.0.1} \end{array}$$

$$\begin{array}{l} 3^{30}/\overset{\wedge}{3.3} \quad 1^{80}/\overset{\wedge}{3.5} \quad 2.6 \quad 3.1 \quad 3.7 \quad 3.5 \quad -3.3 \quad 3.6 \quad 4.4 \quad 3.8 \quad 3.8 \quad 3/\overset{\wedge}{4.2} \quad 1^{80}/\overset{\wedge}{3.8} \\ 3^{30}/\overset{\wedge}{-0.5} \quad 1^{80}/\overset{\wedge}{+0.3} \quad 40 \quad 32 \quad 26 \quad 18 \quad -0.5 \quad 1.8 \quad 3.1 \quad 3.4 \quad 4.4 \quad -1.4 \quad +0.7 \end{array}$$

$$\begin{array}{l} 3^{30}/\overset{\wedge}{4.4} \quad 1^{80}/\overset{\wedge}{4.7} \quad 4.2 \quad 4.3 \quad 5.0 \quad 4.7 \quad 4.7 \quad 4.9 \quad 5.5 \quad 5.2 \quad 5.1 \quad 3/\overset{\wedge}{5.4} \quad 1^{80}/\overset{\wedge}{4.9} \\ 3^{30}/\overset{\wedge}{-0.8} \quad 1^{80}/\overset{\wedge}{-0.1} \quad 40 \quad 32 \quad 25 \quad 18 \quad -1.1 \quad 1.8 \quad 2.9 \quad 3.5 \quad 4.0 \quad 1^{80}/\overset{\wedge}{4.0.18} \quad 1^{80}/\overset{\wedge}{-0.3} \end{array}$$

$$\begin{array}{l} 3^{30}/\overset{\wedge}{4.0} \quad 1^{80}/\overset{\wedge}{4.0} \quad 5.7 \quad 5.8 \quad 6.6 \quad 6.0 \quad 5.3 \quad 4.7 \quad 4.9 \quad 6.0 \quad 6.6 \quad 6.4 \quad 1^{80}/\overset{\wedge}{6.1} \quad 3/\overset{\wedge}{6.4} \\ 3^{30}/\overset{\wedge}{-1.7} \quad 1^{80}/\overset{\wedge}{-0.6} \quad 40 \quad 33 \quad 28 \quad 23 \quad 11 \quad -0.4 \quad 9 \quad 15 \quad 31 \quad 40 \quad 1^{80}/\overset{\wedge}{0.8} \quad 3/\overset{\wedge}{-2.1} \end{array}$$

$$\begin{array}{l} 3^{30}/\overset{\wedge}{5.7} \quad 1^{80}/\overset{\wedge}{5.5} \quad 5.5 \quad 5.5 \quad 6.0 \quad 5.4 \quad 5.0 \quad 4.9 \quad 6.2 \quad 6.2 \quad 6.1 \quad 1^{80}/\overset{\wedge}{5.6} \quad 3/\overset{\wedge}{6.7} \\ 3^{30}/\overset{\wedge}{0.10} \quad 1^{80}/\overset{\wedge}{0.02} \quad 40 \quad 32 \quad 27 \quad 22 \quad -0.3 \quad 1.4 \quad 2.1 \quad 2.9 \quad 4.0 \quad 4.0 \quad 1^{80}/\overset{\wedge}{4.0.1} \quad 1^{80}/\overset{\wedge}{-1.5} \end{array}$$

$$\begin{array}{l} 3^{30}/\overset{\wedge}{3.0} \quad 1^{80}/\overset{\wedge}{3.9} \quad 3.4 \quad 4.0 \quad 4.6 \quad 4.3 \quad 4.6 \quad 5.6 \quad 6.2 \quad 4.6 \quad 4.9 \quad 1^{80}/\overset{\wedge}{5.4} \quad 9^{30}/\overset{\wedge}{5.3} \\ 3^{30}/\overset{\wedge}{0.11} \quad 1^{80}/\overset{\wedge}{0.2.1} \quad 40 \quad 18 \quad 11 \quad 0.7 \quad 1.4 \quad 1.9 \quad 2.5 \quad 3.3 \quad 4.0 \quad 4.0 \quad 1^{80}/\overset{\wedge}{0.0.6} \quad 2/\overset{\wedge}{0.0.3} \end{array}$$

$$\begin{array}{l} 2^{30}/\overset{\wedge}{4.1} \quad 4.2 \quad 4.2 \quad 4.1 \quad 4.4 \quad 5.7 \quad 7.0 \quad 6.0 \quad 5.3 \quad 4.6 \quad 1^{80}/\overset{\wedge}{5.4} \\ 2^{30}/\overset{\wedge}{0.01} \quad 4.0 \quad 1.8 \quad 0.4 \quad 1.6 \quad 2.1 \quad 2.2 \quad 2.3 \quad 3.0 \quad 4.0 \quad 1^{80}/\overset{\wedge}{0.11} \end{array}$$

$$\begin{array}{l} 19^{30}/\overset{\wedge}{5.6} \quad 26^{30}/\overset{\wedge}{6.3} \quad 5.3 \quad 5.3 \quad 6.3 \quad 5.4 \quad 4.9 \quad 4.7 \quad 6.4 \quad 7.5 \quad 6.6 \quad 5.3 \quad 5.5 \quad 2^{30}/\overset{\wedge}{5.6} \quad 2^{30}/\overset{\wedge}{6.0} \\ 19^{30}/\overset{\wedge}{F.0.9} \quad 26^{30}/\overset{\wedge}{20.0.5} \quad 40 \quad 33 \quad 29 \quad 24 \quad F.0.2 \quad 5 \quad 22 \quad 23 \quad 24 \quad 27 \quad 40 \quad 1^{80}/\overset{\wedge}{0.0.11} \quad 1^{80}/\overset{\wedge}{F.1.3} \end{array}$$

925.37

14				30.5	4.9	
B.M.	334	934.70	4.01	931.36	✓	
15				30.3	4.4	
16			927.2	30.1	7.5	4.6 7.5
17			27.3	29.9	7.4	4.8 7.4
T.P.	3.20	934.28	3.62	931.08		
18			27.4	29.7	6.9	4.6 6.9
19			27.5	29.6	6.8	4.7 6.8
20			27.6	29.6	6.7	4.7 6.7
21			27.5	29.7	6.8	4.6 6.8
22			27.4	29.8	6.9	4.5 6.9
23			27.3	29.9	7.0	4.4 7.0
	4.61	934.58	4.31	929.97		
24			27.2	30.0	7.4	4.6 7.4
25			27.1	30.1	7.5	4.5 7.5
26			27.0	30.2	7.6	4.4 7.6
B.M.	1.54	934.56	1.54	933.04	933.02	

$$\begin{array}{r}
 10.6 \quad 6.5 \quad 7.2 \quad 6.1 \quad 7.0 \quad 5.6 \quad 7.0 \quad 7.1 \quad 7.8 \quad 7.2 \quad 6.4 \quad 20.7 \quad 1.6 \quad 6.6 \\
 2/12.1 \quad 40 \quad 23 \quad 29 \quad 21 \quad 17 \quad 5.7 \quad 17 \quad 21 \quad 22 \quad 23 \quad 40 \quad F_{2.1} \quad 0.0.3 \\
 50.1 \quad 10 \quad 25 \quad 50 \quad 24 \quad 2.8 \quad 12+25
 \end{array}$$

$$\begin{array}{r}
 20.7 \quad 5.9 \quad 20.7 \quad 5.6 \quad 6.0 \quad 5.8 \quad 5.8 \quad 6.8 \quad 5.1 \quad 5.9 \quad 6.8 \quad 5.7 \quad 5.7 \quad 20.7 \quad 5.6 \\
 20.0.5 \quad F_{1.2} \quad 40 \quad 26 \quad 20 \quad 17 \quad F_{2.1} \quad 15 \quad 24 \quad 29 \quad 40 \quad F_{2.1} \quad 0.0.2
 \end{array}$$

$$\begin{array}{r}
 20.7 \quad 4.9 \quad 18.6 \quad 4.1 \quad 5.7 \quad 6.0 \quad 5.0 \quad 5.8 \quad 6.6 \quad 5.5 \quad 5.5 \quad 20.6 \quad 5.9 \quad 3.1 \quad 4.7 \\
 20.0.26 \quad F_{2.3} \quad 40 \quad 17 \quad F_{2.4} \quad 13 \quad 16 \quad 20 \quad 40 \quad F_{1.3} \quad 0.0.2.8
 \end{array}$$

$$\begin{array}{r}
 29.7 \quad 4.9 \quad 18.6 \quad 5.1 \quad 4.9 \quad 4.6 \quad 5.5 \quad 4.1 \quad 4.5 \quad 5.4 \quad 4.1 \quad 4.3 \quad 18.6 \quad 5.1 \quad 20.7 \quad 4.2 \\
 20.0.2.5 \quad F_{2.3} \quad 40 \quad 19 \quad 18 \quad 20.7 \quad 12 \quad 18 \quad 22 \quad 40 \quad F_{2.3} \quad 0.0.2.2
 \end{array}$$

$$\begin{array}{r}
 20.7 \quad 4.7 \quad 18.6 \quad 4.7 \quad 4.5 \quad 4.4 \quad 4.7 \quad 3.8 \quad 4.9 \quad 4.2 \quad 4.2 \quad 20.7 \quad 4.2 \quad 20.7 \quad 4.5 \\
 2/12.3 \quad 18.6 \quad 0.0 \quad 40 \quad 19 \quad 18 \quad 10.8 \quad 16 \quad 18 \quad 40 \quad 18.6 \quad 0.1 \quad 20.7 \quad 4.5
 \end{array}$$

$$\begin{array}{r}
 8.5 \quad 5.2 \quad 6.5 \quad 5.1 \quad 5.1 \quad 5.1 \quad 5.6 \quad 4.8 \quad 5.5 \quad 4.9 \quad 4.7 \quad 20.7 \quad 4.9 \quad 20.7 \quad 4.9 \\
 2/11.7 \quad 18.6 \quad -0.3 \quad 40 \quad 19 \quad 17 \quad 0.0 \quad 15 \quad 17 \quad 40 \quad 18.6 \quad -0.1 \quad 20.7 \quad 4.9
 \end{array}$$

$$\begin{array}{r}
 20.7 \quad 4.7 \quad 4.5 \quad 5.0 \quad 5.0 \quad 4.8 \quad 5.2 \quad 4.5 \quad 5.5 \quad 4.9 \quad 5.1 \quad 20.7 \quad 5.0 \quad 20.7 \quad 4.9 \\
 2/12.1 \quad 18.6 \quad -0.2 \quad 40 \quad 17 \quad 18 \quad 10.2 \quad 8 \quad 18 \quad 40 \quad 20.7 \quad 4.8 \quad 18.6 \quad -0.1
 \end{array}$$

$$\begin{array}{r}
 20.7 \quad 4.4 \quad 4.3 \quad 5.1 \quad 4.0 \quad 5.0 \quad 4.5 \quad 4.4 \quad 4.4 \quad 4.9 \quad 4.4 \quad 20.7 \quad 4.9 \quad 20.7 \quad 4.4 \\
 2/12.0 \quad 18.6 \quad -0.4 \quad 40 \quad 21 \quad 20 \quad 10.7 \quad 17 \quad 20 \quad 40 \quad 18.6 \quad -0.2 \quad 20.7 \quad 4.4
 \end{array}$$

$$\begin{array}{r}
 20.7 \quad 4.5 \quad 4.6 \quad 4.6 \quad 5.6 \quad 5.8 \quad 5.3 \quad 4.4 \quad 4.6 \quad 6.4 \quad 4.9 \quad 20.7 \quad 4.5 \quad 20.7 \quad 4.5 \\
 2/12.5 \quad 18.6 \quad -0.8 \quad 40 \quad 21 \quad 20 \quad 10.7 \quad 17 \quad 20 \quad 40 \quad 18.6 \quad -0.3 \quad 20.7 \quad 4.5
 \end{array}$$

$$\begin{array}{r}
 20.7 \quad 5.9 \quad 5.5 \quad 5.7 \quad 6.1 \quad 4.9 \quad 6.2 \quad 5.8 \quad 6.0 \quad 6.5 \quad 5.8 \quad 20.7 \quad 5.8 \quad 20.7 \quad 6.0 \\
 2/11.2 \quad 18.6 \quad -1.4 \quad 40 \quad 22 \quad 20 \quad -0.5 \quad 17 \quad 19 \quad 40 \quad 20.7 \quad 5.3 \quad 20.7 \quad 6.0
 \end{array}$$

$$\begin{array}{r}
 20.7 \quad 5.1 \quad 5.3 \quad 5.0 \quad 6.1 \quad 4.7 \quad 6.5 \quad 5.3 \quad 5.3 \quad 6.5 \quad 4.4 \quad 20.7 \quad 5.1 \quad 20.7 \quad 5.1 \\
 2/12.3 \quad 18.6 \quad -1.3 \quad 40 \quad 21 \quad 19 \quad 0.1 \quad 17 \quad 20 \quad 40 \quad 18.6 \quad -0.8 \quad 20.7 \quad 5.1
 \end{array}$$

$$\begin{array}{r}
 20.7 \quad 5.4 \quad 5.4 \quad 5.2 \quad 5.9 \quad 4.8 \quad 5.5 \quad 5.4 \quad 5.2 \quad 6.5 \quad 4.4 \quad 20.7 \quad 5.4 \quad 20.7 \quad 5.3 \\
 2/12.1 \quad 18.6 \quad -1.3 \quad 40 \quad 23 \quad 21 \quad 0.3 \quad 15 \quad 20 \quad 40 \quad 18.6 \quad -0.9 \quad 20.7 \quad 5.3
 \end{array}$$

$$\begin{array}{r}
 20.7 \quad 5.6 \quad 4.3 \quad 5.2 \quad 5.8 \quad 5.1 \quad 5.5 \quad 4.7 \quad 3.7 \quad 20.7 \quad 5.6 \quad 20.7 \quad 5.6 \\
 2/13.0 \quad 18.6 \quad -1.2 \quad 40 \quad 22 \quad 19 \quad -0.7 \quad 15 \quad 22 \quad 40 \quad 18.6 \quad -0.6 \quad 20.7 \quad 5.6
 \end{array}$$

Sta.	+	H.I.	-	Elev	Gr. Rod.
		934.56			
27			26.8	30.2	78 4.4 78
B.M.	2.08	935.10	1.54	933.04	933.02
28			26.9	30.1	82 5.0 82
29			27.0	30.0	81 5.1 81
	4.20	933.67	5.63	929.47	
30			27.1	29.9	66 3.8 66
31			27.2	29.8	65 3.9 65
32			27.3	29.7	64 4.0 64
33			27.4	29.6	63 4.1 63
34			27.5	29.5	62 4.2 62
B.M.	2.94	933.82	2.81	930.86	930.88
35				29.5	4.3
36				29.5	4.3
37				29.6	4.2
38				29.7	4.1
T.P.	6.68	936.18	4.32	929.50	
39				29.8	6.4

$\frac{2^{\circ}5.4}{3/12.4}$	$\frac{4^{\circ}5.6}{2/7.2}$	$\frac{5.4}{33}$	$\frac{5.3}{18}$	$\frac{5.7}{5}$	$\frac{4.5}{-0.1}$	$\frac{5.5}{13}$	$\frac{5.2}{33}$	$\frac{0^{\circ}5.4}{2/7.0}$	$\frac{2^{\circ}5.2}{3/12.4}$
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$\frac{1^{\circ}7.5.7}{3/12.5}$	$\frac{0^{\circ}6.0}{2/7.0}$	$\frac{5.7}{33}$	$\frac{5.9}{17}$	$\frac{5.9}{5}$	$\frac{4.8}{10.2}$	$\frac{6.0}{8}$	$\frac{6.0}{33}$	$\frac{6^{\circ}5.9}{19/0.9}$	$\frac{1^{\circ}6.0}{4/12.2}$
---------------------------------	------------------------------	------------------	------------------	-----------------	--------------------	-----------------	------------------	-------------------------------	-------------------------------

$\frac{1^{\circ}6.0}{3/12.1}$	$\frac{8^{\circ}6.0}{19/0.9}$	$\frac{5.7}{33}$	$\frac{5.9}{8}$	$\frac{6.3}{5}$	$\frac{4.8}{10.3}$	$\frac{5.8}{7}$	$\frac{6.1}{33}$	$\frac{9^{\circ}5.9}{1/-0.8}$	$\frac{0^{\circ}6.1}{5/12.0}$
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ON STAKE 20 FT STR. 29100

$\frac{0^{\circ}8.4.4}{3/12.2}$	$\frac{0^{\circ}4.8}{2/7.0}$	$\frac{4.4}{33}$	$\frac{4.8}{17}$	$\frac{4.8}{8}$	$\frac{5.2}{5}$	$\frac{5.6}{10.2}$	$\frac{4.4}{3}$	$\frac{4.7}{15}$	$\frac{4.9}{33}$	$\frac{9^{\circ}4.6}{19/0.8}$	$\frac{0^{\circ}4.8}{3/12.8}$
---------------------------------	------------------------------	------------------	------------------	-----------------	-----------------	--------------------	-----------------	------------------	------------------	-------------------------------	-------------------------------

$\frac{0^{\circ}8.4.3}{3/12.2}$	$\frac{1^{\circ}4.7}{19/0.8}$	$\frac{4.1}{33}$	$\frac{4.7}{18}$	$\frac{4.5}{5}$	$\frac{5.2}{3}$	$\frac{5.5}{10.4}$	$\frac{4.6}{5}$	$\frac{4.6}{33}$	$\frac{2^{\circ}4.5}{19/0.6}$	$\frac{1^{\circ}4.7}{3/12.8}$
---------------------------------	-------------------------------	------------------	------------------	-----------------	-----------------	--------------------	-----------------	------------------	-------------------------------	-------------------------------

$\frac{0^{\circ}4.6}{3/12.8}$	$\frac{8^{\circ}4.9}{19/0.9}$	$\frac{4.8}{33}$	$\frac{4.8}{17}$	$\frac{4.9}{5}$	$\frac{5.4}{3}$	$\frac{5.4}{10.6}$	$\frac{5.3}{6}$	$\frac{4.6}{8}$	$\frac{4.8}{33}$	$\frac{1^{\circ}4.8}{19/0.8}$	$\frac{0^{\circ}4.8}{3/12.6}$
-------------------------------	-------------------------------	------------------	------------------	-----------------	-----------------	--------------------	-----------------	-----------------	------------------	-------------------------------	-------------------------------

$\frac{0^{\circ}4.5}{3/12.8}$	$\frac{0^{\circ}5.0}{19/0.9}$	$\frac{4.6}{33}$	$\frac{4.9}{18}$	$\frac{4.7}{5}$	$\frac{5.5}{3}$	$\frac{5.7}{10.4}$	$\frac{5.3}{5}$	$\frac{4.7}{8}$	$\frac{4.8}{33}$	$\frac{1^{\circ}4.9}{19/0.8}$	$\frac{0^{\circ}4.8}{3/12.5}$
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$\frac{0^{\circ}6.5.1}{3/12.1}$	$\frac{0^{\circ}5.3}{2/7.1}$	$\frac{5.2}{33}$	$\frac{5.2}{18}$	$\frac{5.0}{7}$	$\frac{5.8}{4}$	$\frac{4.0}{10.2}$	$\frac{5.0}{3}$	$\frac{5.0}{33}$	$\frac{1^{\circ}4.9}{19/0.7}$	$\frac{0^{\circ}5.1}{3/12.1}$
---------------------------------	------------------------------	------------------	------------------	-----------------	-----------------	--------------------	-----------------	------------------	-------------------------------	-------------------------------

$\frac{2^{\circ}7.3.4}{2/00.9}$	$\frac{1^{\circ}5.2}{19/0.9}$	$\frac{5.1}{33}$	$\frac{5.5}{22}$	$\frac{5.0}{6}$	$\frac{6.0}{3}$	$\frac{4.2}{0.1}$	$\frac{5.1}{3}$	$\frac{5.3}{13}$	$\frac{5.0}{33}$	$\frac{19^{\circ}5.1}{19/0.8}$	$\frac{3^{\circ}5.0}{3/-0.7}$
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$\frac{2^{\circ}7.2.8}{00.15}$	$\frac{1^{\circ}6.4.4}{19/0.9}$	$\frac{4.7}{33}$	$\frac{5.0}{22}$	$\frac{4.8}{6}$	$\frac{5.6}{4}$	$\frac{3.6}{0.7}$	$\frac{4.3}{3}$	$\frac{4.7}{15}$	$\frac{4.8}{33}$	$\frac{1^{\circ}6.4.5}{19/0.2}$	$\frac{2^{\circ}8.4.7}{2/00.6}$
--------------------------------	---------------------------------	------------------	------------------	-----------------	-----------------	-------------------	-----------------	------------------	------------------	---------------------------------	---------------------------------

$\frac{2^{\circ}7.4.4}{00.13}$	$\frac{1^{\circ}6.5.1}{19/0.9}$	$\frac{4.9}{33}$	$\frac{4.9}{15}$	$\frac{4.3}{10}$	$\frac{5.8}{5}$	$\frac{3.7}{0.5}$	$\frac{5.0}{5}$	$\frac{4.9}{33}$	$\frac{1^{\circ}6.4.7}{19/0.5}$	$\frac{2^{\circ}9.4.9}{00.13}$
--------------------------------	---------------------------------	------------------	------------------	------------------	-----------------	-------------------	-----------------	------------------	---------------------------------	--------------------------------

$\frac{2^{\circ}7.4.8}{00.13}$	$\frac{2^{\circ}6.5.2}{19/1.1}$	$\frac{4.7}{33}$	$\frac{5.2}{19}$	$\frac{5.0}{7}$	$\frac{5.8}{4}$	$\frac{3.9}{0.2}$	$\frac{4.0}{4}$	$\frac{4.9}{33}$	$\frac{1^{\circ}6.4.6}{19/0.5}$	$\frac{2^{\circ}7.4.6}{00.13}$
--------------------------------	---------------------------------	------------------	------------------	-----------------	-----------------	-------------------	-----------------	------------------	---------------------------------	--------------------------------

$\frac{2^{\circ}7.7.2}{00.12}$	$\frac{1^{\circ}6.7.2}{19/0.8}$	$\frac{7.2}{33}$	$\frac{7.3}{18}$	$\frac{7.0}{7}$	$\frac{8.1}{5}$	$\frac{6.2}{0.2}$	$\frac{7.4}{5}$	$\frac{6.5}{11}$	$\frac{7.4}{33}$	$\frac{1^{\circ}6.7.1}{19/0.7}$	$\frac{2^{\circ}7.7.3}{2/00.11}$
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936.18

40

30.1

6.1

41

30.9

5.3

42

31.7

4.5

43

32.2

4.0

T.P.

4.06

936.63

3.61

932.57

44

32.3

4.3

45

32.1

4.5

46

31.7

4.9

47

31.5

5.1

T.P.

5.03

936.14

5.52

931.11

48

38.6
5.5

31.3

4.84

F08

49

31.3

4.8

C0.1

50

31.2

4.9

C0.3

51

31.0

5.1

C0.1

52

30.6

5.5

C0.1

B.M.

1.60

933.39

4.37

931.77

931.79

$$\frac{27.6}{DC.11} / \frac{7.0}{F0.8} \quad \frac{19.6}{33} / \frac{6.7}{8} \quad \frac{6.7}{8} \quad \frac{8.7}{4} \quad \frac{6.2}{F0.1} \quad \frac{7.1}{7} \quad \frac{7.2}{33} \quad \frac{19.6}{F0.8} / \frac{6.9}{27.6} / \frac{7.0}{DC.11}$$

$$\frac{27.6}{DC.11} / \frac{6.2}{F1.5} \quad \frac{21.0}{6.8} \quad \frac{6.3}{19} \quad \frac{6.6}{4} \quad \frac{6.7}{0.1} \quad \frac{5.2}{12} \quad \frac{5.4}{15} \quad \frac{6.1}{33} \quad \frac{6.3}{F0.9} \quad \frac{9.3}{6.2} \quad \frac{7.1}{6.3} / \frac{27.6}{DC.10}$$

$$\frac{28.1}{DC.16} / \frac{4.9}{F1.1} \quad \frac{7.5}{5.6} \quad \frac{4.7}{33} \quad \frac{5.3}{22} \quad \frac{4.9}{10} \quad \frac{3.9}{0.6} \quad \frac{4.1}{9} \quad \frac{4.7}{14} \quad \frac{5.0}{33} \quad \frac{8.8}{4.9} / \frac{28.1}{F0.4} / \frac{5.0}{DC.15}$$

$$\frac{29.0}{DC.20} / \frac{4.0}{F0.8} \quad \frac{6}{9.4} \quad \frac{4.1}{33} \quad \frac{4.5}{21} \quad \frac{3.8}{8} \quad \frac{3.1}{0.9} \quad \frac{3.5}{12} \quad \frac{4.1}{15} \quad \frac{4.3}{33} \quad \frac{8.4}{4.2} / \frac{8.5}{4.3} / \frac{29.0}{DC.17}$$

$$\frac{29.4}{DC.23} / \frac{4.0}{F0.2} \quad \frac{18.4}{4.5} \quad \frac{4.0}{33} \quad \frac{4.5}{20} \quad \frac{4.1}{7} \quad \frac{3.3}{0.10} \quad \frac{3.7}{9} \quad \frac{4.5}{15} \quad \frac{4.6}{33} \quad \frac{18.4}{4.5} / \frac{29.4}{F0.2} / \frac{4.7}{DC.16}$$

$$\frac{29.0}{DC.20} / \frac{4.5}{F0.8} \quad \frac{19.6}{5.3} \quad \frac{4.5}{33} \quad \frac{5.1}{21} \quad \frac{4.8}{10} \quad \frac{4.2}{0.6} \quad \frac{4.5}{8} \quad \frac{5.3}{15} \quad \frac{5.3}{33} \quad \frac{19.6}{5.3} / \frac{29.0}{F0.8} / \frac{5.3}{DC.12}$$

$$\frac{28.1}{DC.14} / \frac{5.5}{F0.8} \quad \frac{19.6}{5.7} \quad \frac{5.1}{33} \quad \frac{5.6}{17} \quad \frac{5.3}{F0.4} \quad \frac{5.4}{11} \quad \frac{5.9}{15} \quad \frac{6.0}{33} \quad \frac{20.0}{6.0} / \frac{28.1}{F1.1} / \frac{6.0}{DC.0.9}$$

$$\frac{28.1}{DC.14} / \frac{5.7}{F1.1} \quad \frac{20.0}{6.2} \quad \frac{5.4}{33} \quad \frac{6.2}{20} \quad \frac{6.0}{F0.9} \quad \frac{6.1}{15} \quad \frac{6.1}{33} \quad \frac{20.0}{6.1} / \frac{28.1}{F1.0} / \frac{6.1}{DC.1.0}$$

$$\frac{27.8}{DC.12} / \frac{5.6}{F1.4} \quad \frac{20.8}{6.2} \quad \frac{5.3}{33} \quad \frac{6.1}{18} \quad \frac{5.6}{13} \quad \frac{5.6}{F0.8} \quad \frac{5.2}{10} \quad \frac{5.7}{15} \quad \frac{5.7}{33} \quad \frac{20.8}{5.8} / \frac{27.8}{F1.0} / \frac{5.7}{DC.1.1}$$

$$\frac{28.6}{DC.19} / \frac{4.1}{F0.1} \quad \frac{19.4}{5.5} \quad \frac{4.6}{33} \quad \frac{5.3}{18} \quad \frac{4.9}{13} \quad \frac{4.7}{0.1} \quad \frac{4.6}{8} \quad \frac{5.2}{19} \quad \frac{4.6}{33} \quad \frac{18.6}{5.2} / \frac{28.6}{F0.4} / \frac{4.6}{DC.2.2}$$

$$\frac{29.6}{DC.2.4} / \frac{4.5}{F0.1} \quad \frac{18.2}{5.0} \quad \frac{4.8}{33} \quad \frac{5.0}{20} \quad \frac{4.6}{14} \quad \frac{4.7}{0.2} \quad \frac{4.3}{8} \quad \frac{4.8}{33} \quad \frac{18.2}{5.0} / \frac{29.6}{F0.1} / \frac{4.7}{DC.2.2}$$

$$\frac{27.8}{DC.12} / \frac{4.9}{F0.4} \quad \frac{16.8}{4.7} \quad \frac{4.9}{33} \quad \frac{5.1}{14} \quad \frac{4.8}{0.3} \quad \frac{5.1}{33} \quad \frac{16.8}{4.7} / \frac{27.8}{F0.4} / \frac{4.8}{DC.1.3}$$

$$\frac{28.6}{DC.1.9} / \frac{5.7}{F0.1} \quad \frac{18.2}{5.6} \quad \frac{5.5}{33} \quad \frac{5.9}{15} \quad \frac{5.6}{F0.1} \quad \frac{5.9}{16} \quad \frac{5.7}{33} \quad \frac{18.2}{5.8} / \frac{28.6}{F0.3} / \frac{5.7}{DC.1.9}$$

spike in T.P. 100 V2. Sta. 52-25

Sta.	+	H. 1.	—	931.79		
		933.39				
53				930.00	3.4	F 1.0 F 0.6
54				29.3	4.1	F 0.6
55				28.6	4.8	0.0
56				27.9	5.5	0.0.
57				27.2	6.2	0.03
T.P.	6.20	934.11	5.48	927.91		
58				26.9	7.2	F 2.3
59				27.5	6.6	F 3.9
60				28.8	5.3	F 0.9
61				30.2	3.9	C 1.1
62				31.2	2.9	C 1.3
T.P.	5.26	938.01	1.36	932.75		
63				31.9	6.1	0.01
64				32.3	5.7	F 0.3
B.M.	5.13	938.15	5.02	932.99	933.02	
+37				Apr. 14-30		
			5.13	32.4	5.75	F 0.7

Left

L

Right

$$\begin{array}{r} 27^3/4.5 \\ \hline D.C. 0.9 \end{array} \quad \begin{array}{r} 27^3/4.5 \\ \hline F 1.1 \end{array} \quad \begin{array}{r} 4.5 \\ 33 \end{array} \quad \begin{array}{r} 4.4 \\ 15 \end{array} \quad \begin{array}{r} 4.4 \\ F 1.0 \end{array} \quad \begin{array}{r} 4.5 \\ 17 \end{array} \quad \begin{array}{r} 4.3 \\ 33 \end{array} \quad \begin{array}{r} 27^3/4.4 \\ \hline F 1.0 \end{array} \quad \begin{array}{r} 27^3/4.3 \\ \hline D.C. 1.1 \end{array}$$

$$\begin{array}{r} 28^3/4.8 \\ \hline D.C. 1.3 \end{array} \quad \begin{array}{r} 19^2/4.7 \\ \hline F 0.6 \end{array} \quad \begin{array}{r} 5.0 \\ 33 \end{array} \quad \begin{array}{r} 4.7 \\ 16 \end{array} \quad \begin{array}{r} 4.7 \\ F 0.6 \end{array} \quad \begin{array}{r} 4.9 \\ 17 \end{array} \quad \begin{array}{r} 4.7 \\ 33 \end{array} \quad \begin{array}{r} 19^2/4.7 \\ \hline F 0.6 \end{array} \quad \begin{array}{r} 28^3/4.8 \\ \hline D.C. 1.3 \end{array}$$

$$\begin{array}{r} 25^4/5.2 \\ \hline D.C. 1.6 \end{array} \quad \begin{array}{r} 18^6/5.1 \\ \hline F 0.3 \end{array} \quad \begin{array}{r} 5.4 \\ 33 \end{array} \quad 0.0 \quad \begin{array}{r} 5.3 \\ 16 \end{array} \quad \begin{array}{r} 5.5 \\ 33 \end{array} \quad \begin{array}{r} 19^2/5.4 \\ \hline F 0.6 \end{array} \quad \begin{array}{r} 29^1/5.4 \\ \hline D.C. 1.4 \end{array}$$

$$\begin{array}{r} 28^1/6.1 \\ \hline D.C. 1.4 \end{array} \quad \begin{array}{r} 19^0/5.9 \\ \hline F 0.5 \end{array} \quad \begin{array}{r} 6.1 \\ 33 \end{array} \quad 0.0 \quad \begin{array}{r} 6.1 \\ 33 \end{array} \quad \begin{array}{r} 18^4/5.7 \\ \hline F 0.2 \end{array} \quad \begin{array}{r} 25^4/5.9 \\ \hline D.C. 1.6 \end{array}$$

$$\begin{array}{r} 28^4/6.6 \\ \hline D.C. 1.6 \end{array} \quad 0.0 \quad \begin{array}{r} 6.8 \\ 33 \end{array} \quad \begin{array}{r} 5.8 \\ C 0.4 \end{array} \quad \begin{array}{r} 6.1 \\ 33 \end{array} \quad \begin{array}{r} 19^0/5.7 \\ \hline C 0.5 \end{array} \quad \begin{array}{r} 29^1/5.9 \\ \hline D.C. 2.3 \end{array}$$

$$\begin{array}{r} 25^4/10.9 \\ \hline F 3.7 \end{array} \quad \begin{array}{r} 10.6 \\ F 3.4 \end{array} \quad 10.9 \quad \begin{array}{r} 25^1/10.8 \\ \hline F 3.6 \end{array}$$

$$\begin{array}{r} 26^0/10.6 \\ \hline F 4.0 \end{array} \quad \begin{array}{r} 10.6 \\ 33 \end{array} \quad \begin{array}{r} 10.6 \\ F 4.0 \end{array} \quad \begin{array}{r} 11.0 \\ 33 \end{array} \quad \begin{array}{r} 26^8/11.0 \\ \hline F 4.4 \end{array}$$

$$\begin{array}{r} 27^3/6.1 \\ \hline D.C. 1.2 \end{array} \quad \begin{array}{r} 27^2/6.4 \\ \hline F 1.1 \end{array} \quad \begin{array}{r} 6.0 \\ 33 \end{array} \quad \begin{array}{r} 6.3 \\ F 1.0 \end{array} \quad \begin{array}{r} 5.9 \\ 28 \end{array} \quad \begin{array}{r} 19^4/6.0 \\ \hline F 0.7 \end{array} \quad \begin{array}{r} 28^0/6.0 \\ \hline D.C. 1.3 \end{array}$$

$$\begin{array}{r} 28^3/4.0 \\ \hline D.C. 1.9 \end{array} \quad \begin{array}{r} 18^4/4.1 \\ \hline F 0.2 \end{array} \quad \begin{array}{r} 4.1 \\ 33 \end{array} \quad \begin{array}{r} 4.0 \\ 15 \end{array} \quad \begin{array}{r} 2.7 \\ C 1.2 \end{array} \quad \begin{array}{r} 3.9 \\ 19 \end{array} \quad \begin{array}{r} 4.0 \\ 33 \end{array} \quad \begin{array}{r} 18^4/3.7 \\ \hline C 0.2 \end{array} \quad \begin{array}{r} 29^0/3.9 \\ \hline D.C. 2.0 \end{array}$$

$$\begin{array}{r} 30^0/2.2 \\ \hline D.C. 2.7 \end{array} \quad \begin{array}{r} 19^3/2.3 \\ \hline C 0.6 \end{array} \quad \begin{array}{r} 2.3 \\ 33 \end{array} \quad \begin{array}{r} 2.3 \\ 9 \end{array} \quad \begin{array}{r} 1.9 \\ C 1.0 \end{array} \quad \begin{array}{r} 1.2 \\ 13 \end{array} \quad \begin{array}{r} 2.2 \\ 33 \end{array} \quad \begin{array}{r} 2.0/1.9 \\ \hline C 1.0 \end{array} \quad \begin{array}{r} 30^3/2.0 \\ \hline D.C. 2.9 \end{array}$$

$$\begin{array}{r} 29^1/6.0 \\ \hline D.C. 2.1 \end{array} \quad \begin{array}{r} 18^6/6.4 \\ \hline F 0.3 \end{array} \quad \begin{array}{r} 6.0 \\ 33 \end{array} \quad \begin{array}{r} 6.1 \\ 9 \end{array} \quad \begin{array}{r} 6.0 \\ C 0.1 \end{array} \quad \begin{array}{r} 4.8 \\ 13 \end{array} \quad \begin{array}{r} 5.9 \\ 33 \end{array} \quad \begin{array}{r} 19^6/5.3 \\ \hline C 0.8 \end{array} \quad \begin{array}{r} 29^1/6.0 \\ \hline D.C. 2.1 \end{array}$$

$$\begin{array}{r} 27^3/6.5 \\ \hline D.C. 1.2 \end{array} \quad \begin{array}{r} 19^0/6.2 \\ \hline F 0.5 \end{array} \quad \begin{array}{r} 6.6 \\ 33 \end{array} \quad \begin{array}{r} 5.9 \\ 12 \end{array} \quad \begin{array}{r} 6.0 \\ F 0.3 \end{array} \quad \begin{array}{r} 5.4 \\ 10 \end{array} \quad \begin{array}{r} 6.6 \\ 18 \end{array} \quad \begin{array}{r} 6.6 \\ 33 \end{array} \quad \begin{array}{r} 19^0/6.7 \\ \hline F 1.0 \end{array} \quad \begin{array}{r} 28^2/6.3 \\ \hline D.C. 1.5 \end{array}$$

SP. 1 K 2 in 20" Tree

$$\begin{array}{r} 26^4/6.1 \\ \hline D.C. 1.1 \end{array} \quad \begin{array}{r} 19^4/6.4 \\ \hline F 0.7 \end{array} \quad \begin{array}{r} 6.2 \\ 33 \end{array} \quad \begin{array}{r} 6.2 \\ 16 \end{array} \quad \begin{array}{r} 7.05 \\ F 1.3 \end{array} \quad \begin{array}{r} 9.5 \\ 7 \end{array} \quad \begin{array}{r} 8.2 \\ 12 \end{array} \quad \begin{array}{r} 5.0 \\ 23 \end{array} \quad \begin{array}{r} 4.9 \\ 33 \end{array}$$

