

OFFICE OF COUNTY ENGINEER
RAMSEY COUNTY, MINN.

PLAN

Survey

Co. Rd. "C"

From T. H. 8 To CLEVELAND

Road Acc't. No. 23

Date Filed 1-21-82

Dr. 12
File Pl. 36

KP
DS
RJ
VC

30 Nov, 1973
Sunny 37°

Co. RD C

SILVER LAKE ROAD TO W. CO. LINE
T.H. No 8

ALINEMENT

STA	POINT	ΔLT	ΔRT	CURVE DATA
-----	-------	-----	-----	---------------

L²

13+00

PI

0°27.0

0+00

0+00^L P.O.T

0-122752

PI

± SILVER LAKE RD.

30 Nov. 1973

LT

E

RT

S.E. Cor. Sec 6



STONE MONT.

89° 28.0'

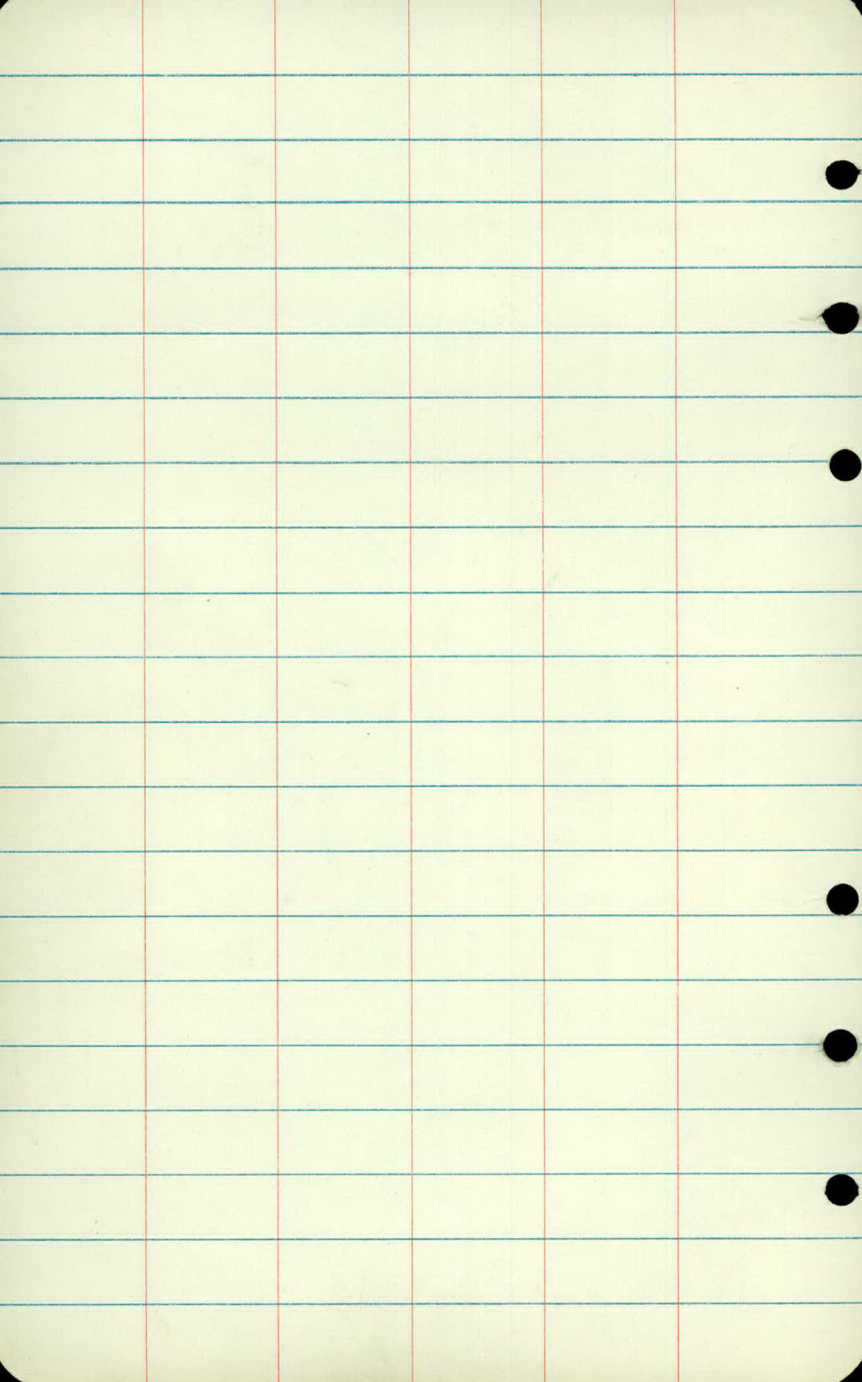


DRILL HOLE

S $\frac{1}{4}$ Cor Sec. 6 - T29-R²³



Iron MONT



Co. RD. C

W. Co. LINE TO FAIRVIEW AVE

PLANS SURVEY

Title	Page
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Alinement	"
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Sta	Point	ΔL	ΔR	CURVE DATA
-----	-------	------------	------------	---------------

26+51.24	P1	0°04'		
----------	----	-------	--	--

26+35.44	= E	MAIN TRACK		
----------	-----	------------	--	--

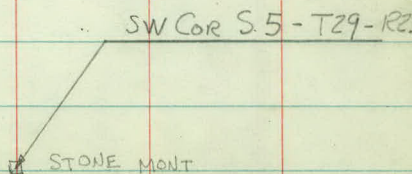
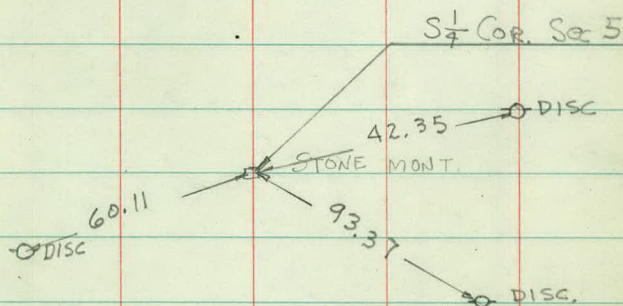
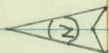
25+52.30	= E	SPUR TRACK		
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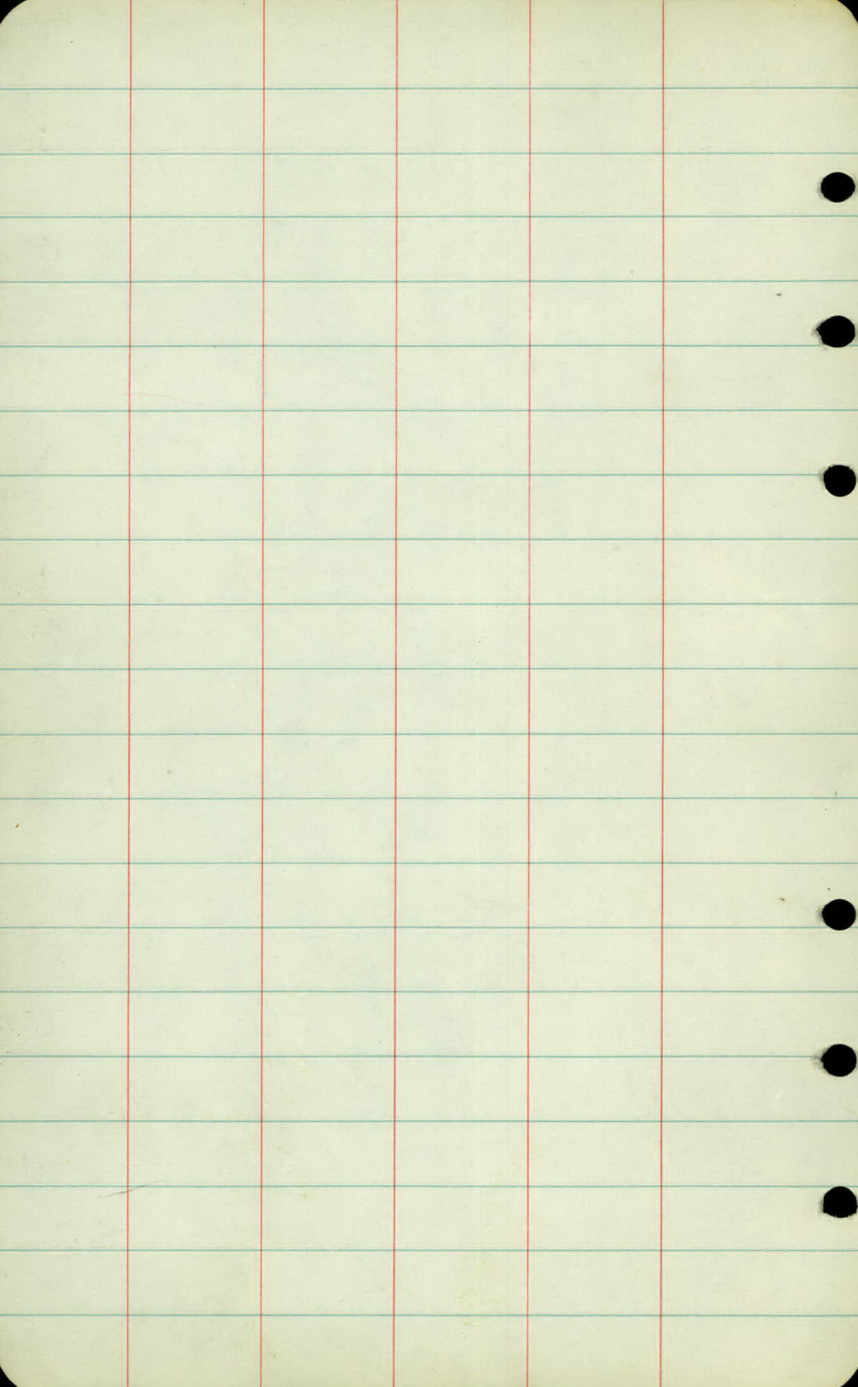
0+00	= W. Co. LINE			
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Lt

E

Rt





13 NOV. 1973

2,

ALINEMENT

S. LINE Sec. 5 - T28 - R23

STA	POINT	Δ LT	Δ RT	CURVE DATA
-----	-------	-------------	-------------	---------------

53+02. ⁶⁰				
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38+80.60	P.O.T.	LONG LAKE RD.		
----------	--------	---------------	--	--

26+52. ¹⁵	PI	0°04.8		
----------------------	----	--------	--	--

0+00				
------	--	--	--	--

LT

13 Nov, 1973
RT

3.

S.E. Cor.

Iron mont.

H.P.

S 1/4 Cor.

3N - - - - 143.57

DISC

169.36 - - - - 34.90 - - - - 3N

PK - 42.11 - - - -



TOP RIVER
N.W. Cor

3N - - - -

3N - - - - PK

SW Cor

STONE MONT.

BLDG

STA	POINT	DLT	Δ RT	CURVE DATA
-----	-------	-----	------	------------

26+52. ¹⁵	PI	0°04.8		
----------------------	----	--------	--	--

26+36. ³⁹	=	Δ	MAIN TRACK	
----------------------	---	---	------------	--

25+53. ²³	=	Δ	SPUR TRACK	
----------------------	---	---	------------	--

15+00	P.O.T.			
-------	--------	--	--	--

		0°27.0		
--	--	--------	--	--

0+00	=	WEST CO. LINE		
------	---	---------------	--	--

LT

E

14 Nov. 1973

RT

4.

$5\frac{1}{4}$ Cor

PK

SPIKE

SW Cor.

□ STONE MONT

STA	POINT	ΔLT	ΔRT	CURVE DATA
-----	-------	-------------	-------------	---------------

		$0^{\circ}36.5$		
--	--	-----------------	--	--

53+02.60	= E	CLEVELAND AVE.		
----------	-----	----------------	--	--

38+80.60	P.O.T.	LONG LAKE RO.		
----------	--------	---------------	--	--

33+00	P.O.T.			
-------	--------	--	--	--

26+52 ¹⁵	PI	$0^{\circ}04.8$		
---------------------	----	-----------------	--	--

LT

14 Nov. 1973

Rt

5.

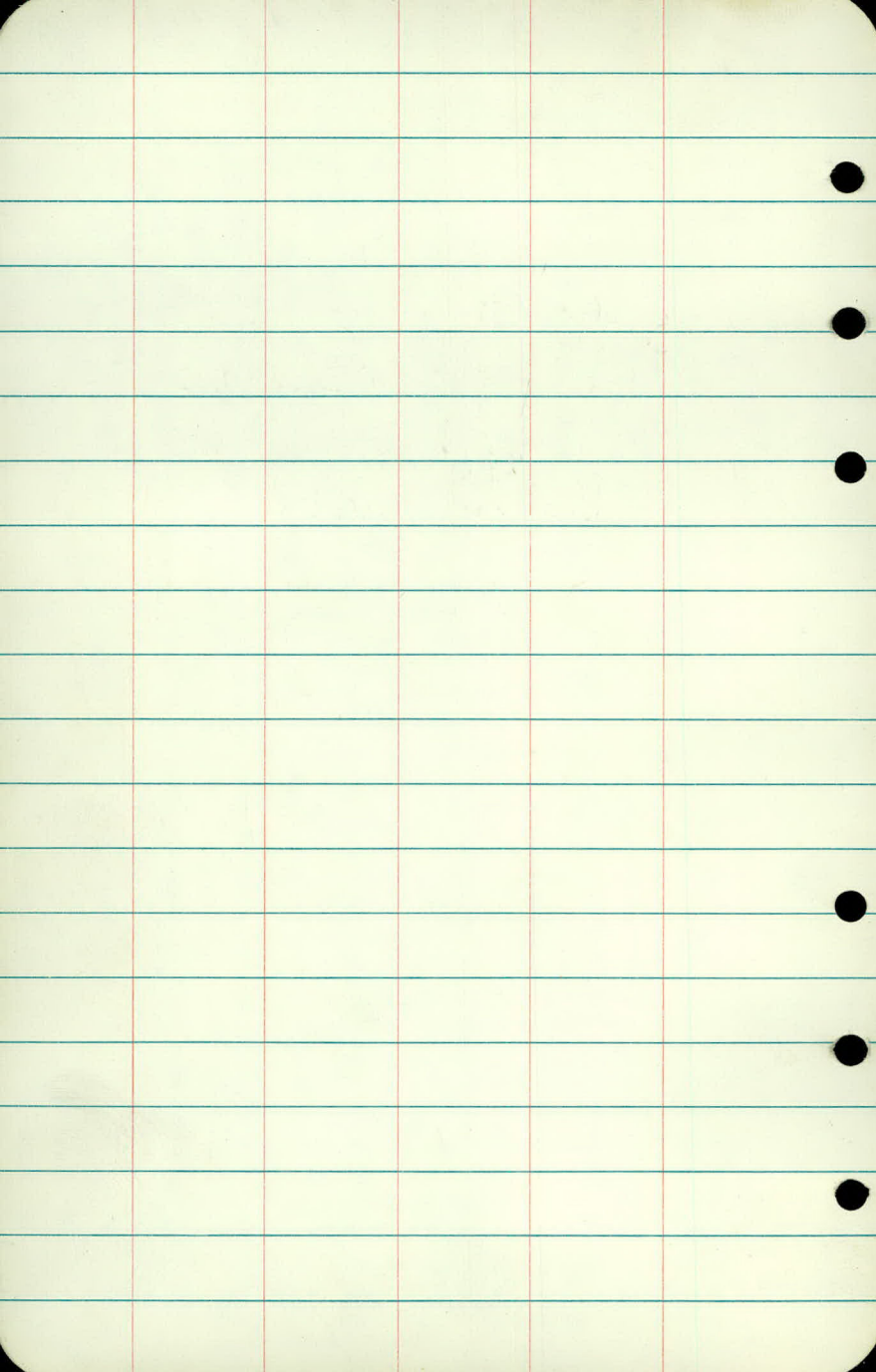
S.E. Cor

• Iron mont.

• SPIKE

S $\frac{1}{4}$ Cor.

• PK



W.S
G.A
P.S
EX

10-29-76
CLERMONT

CO. RD "C"

W. CO LINE TO CLEVELAND

ADDITIONAL

CROSS-SECTIONS - TOPO - PROFILE

BASE LINE OFF OF CO. RD "C" NORTH OF
ANTHONY LANE.

ANTHONY LANE

0+00



7+35

CO. RD "C"

1A

LT

Q

RT

2 +00

$$+75 \frac{\text{LOT}}{0.100}$$

$$+80 \frac{\text{RD}}{35}$$

$$+75 \frac{\text{RD}}{0}$$

$$+76 \frac{\text{RD}}{10}$$

$$+75 \frac{\text{RD}}{23}$$

+50 ✓

$$+43 \frac{5" \text{ ASD}}{11}$$

$$+33 \frac{\text{LOT}}{34.66}$$

$$+33 \frac{\text{RD}}{47}$$

$$+19 \frac{\text{COR LOT}}{48}$$

$$+33 \frac{\text{RD}}{0}$$

$$+13 \frac{6" \text{ POPULAR}}{29}$$

$$+06 \frac{15" \text{ POPULAR}}{23}$$

1 +00

$$\text{RD} \frac{12}{32}$$

$$\text{RD} \frac{32}{32}$$

$$+98 \frac{3" \text{ m}}{55}$$

$$+77 \frac{5" \text{ m}}{54}$$

$$+60 \frac{\text{SW COR BLDG}}{70}$$

$$+60 \frac{3" \text{ MAPLE}}{44}$$

$$+65 \frac{\text{S.T.P.}}{20}$$

+50

$$+45 \frac{\text{RD}}{16}$$

$$+45 \frac{\text{RD}}{16}$$

$$+27 \frac{\text{MH}}{2}$$

0 +00

W.S
G.A
R.S
E.H

LT

⊕

10-29-76
RT
CLIM: 57°

2

PARKING LOT



⊙ MH

MH

E

L

SECTION NUMBER

2A STA	+	π	-	ELEV.
-----------	---	-------	---	-------

BM	2.29	943.41		941.12
----	------	--------	--	--------

0+25

+40

+45

+75

1+00

+33

KP
DS
RJ
JC

30 NOV. 1973
SUNNY 40°

1A

Adj. topo pt. 8 Nov '76

Co. Rd C

SILVER LAKE RD TO W. CO. LINE

TOPOGRAPHY

1 + 31.62

LT

E

RT

1+50

1+00

+50

0+00

0-50

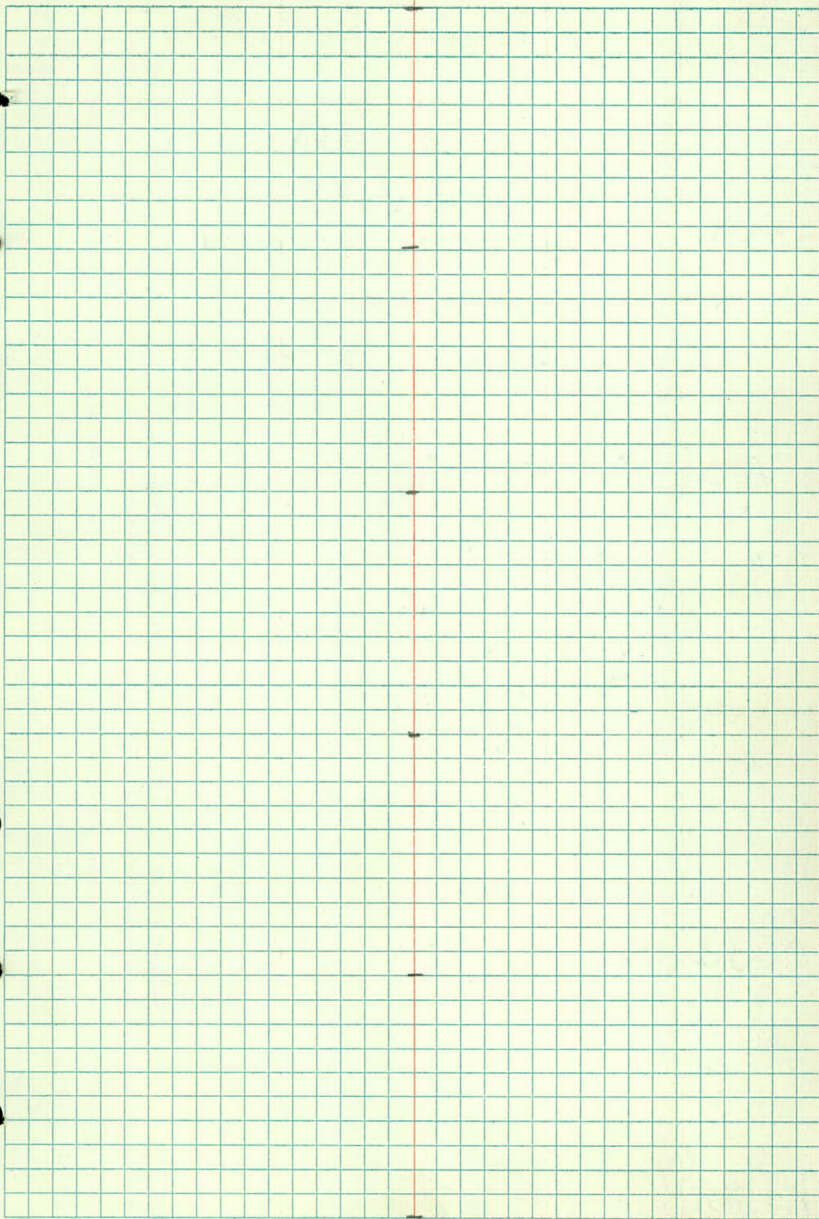
0-100

LT

E

RT

2A



4+00

BIT

11-21

CONC

11 11

N.W. Cor Bldg

+77

160

+64 Conc Curb
153

+50

CONC

11 11

+51 Conc Curb
98

+41 CONC

11-13

+41 BIT

13-21

+25 CONC

11-14

+25 BIT

14-24

3+00

BIT

CONC

CONC

25-37

11-25

11 11

+96 MH

33

+75 BIT

+75 CONC

+75 CURB

17-59

11-17

+70 Pull Box

+70 CONC

11 11

+60 CURB

+42 +70 CURB

117

+70 CURB

+50

24 +70 CONC

14

CONC

124

12 12

+47 CURB (R)

88

+47 CURB

14

+25 CURB

69

+25 CURB

14

+08 MH (TEL)

29

+21 MH (TEL)

29

2+00

Curb

Pull Box

Curb

CONC

45

26

14

12 12

BIT

12-22

Box Bit

154

+82 LITE STD

21

+71 CURB

16

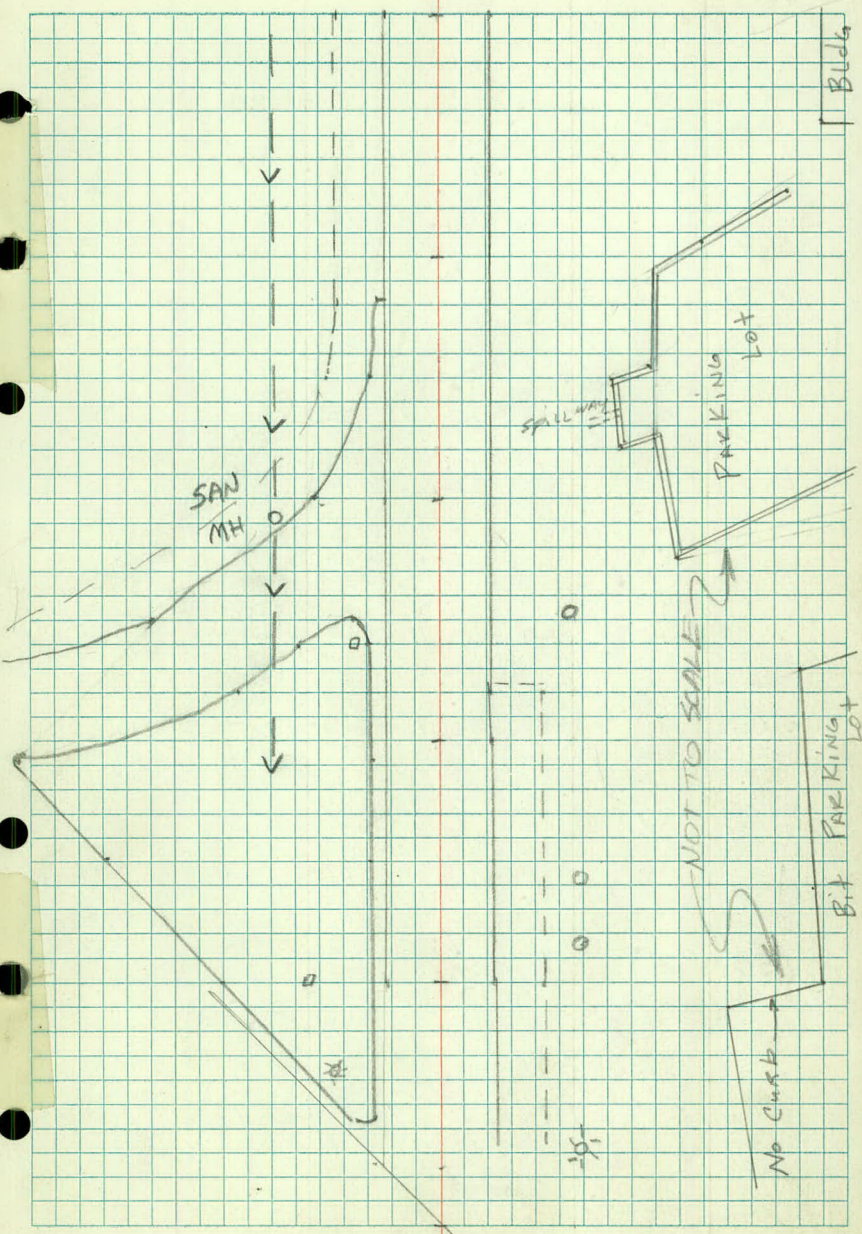
+95 Conc Bit Parking Lot
138

+65 SIGNAL STD

28

1+50

Bldg



+50

BIT

11-21

CONC

11 11

+33 E END 24" CM

35

+25 RT E END ENT.

SEE NEW NOTES

+36 BT

11-19

+32

Curb Bit

102-125 100-100

+14 LITE

+25 SIGN

+101 BT

11-13

6+00

38

BIT

11-64

52

CONC.

11 11

+84 BIT

94

+84 S.E. Con Bldg

100

+71

Aprm (24" RCP)

40

+74 MH

35

+57 Conc slab

33-100

+50

CONC

11 11

+42 Curb

100-122

Bit

102-102 +

+38 SW Con Bldg

100

+38 Conc slab

+38 BIT

96

33-100

+22

Curb

122-142

N.E.

Core B Ldg

162

5+00

BIT

11-79

CONC

11 11

+82 PHONE

46

+82 LITE

39

+70 RT BIT

+72 W. END 24" CM

36

+50

BIT

11-21

CONC

11 11

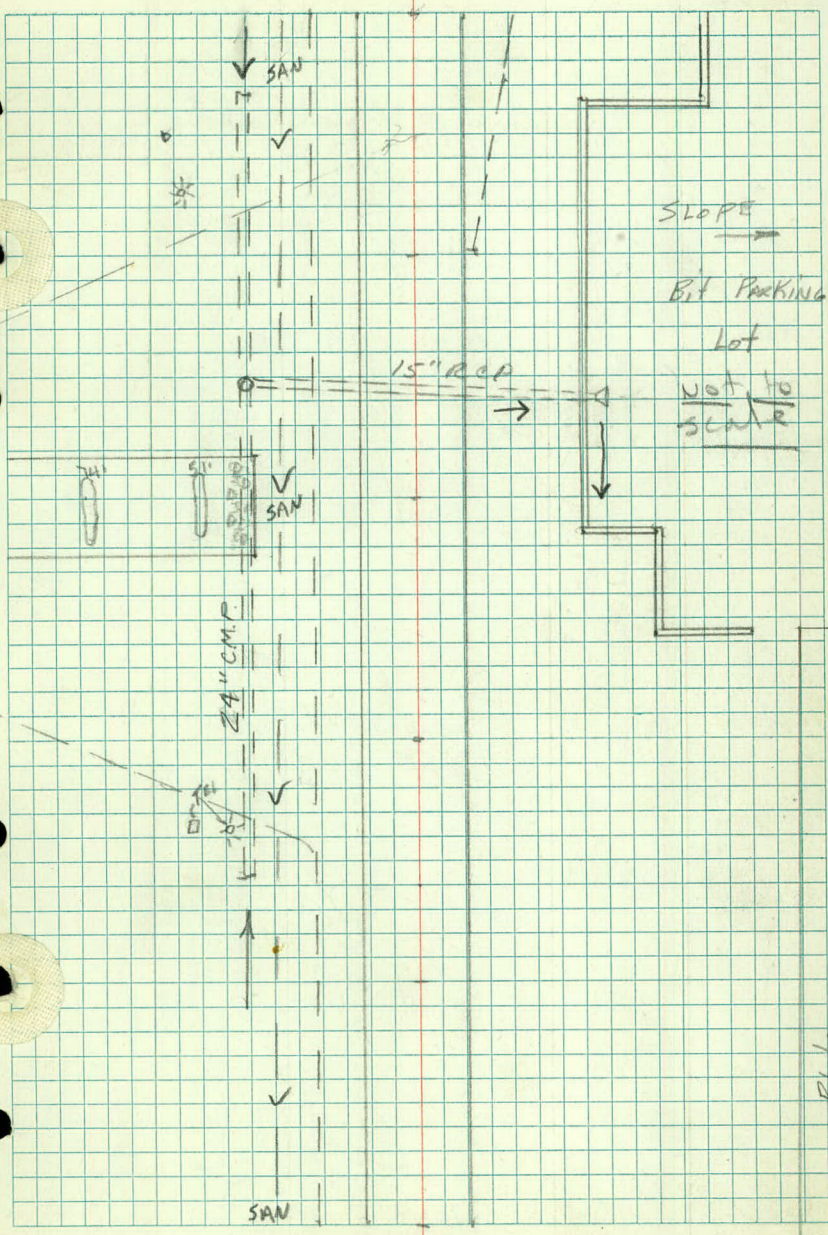
4+00

BIT

11-21

CONC

11 11



BLdg

9+00

LT

BLDG

63

CONC.

11 11

+83 iron
68

RT

+81 iron
43+81 BT
11-13+73 4" M
47+68 WSO
34+57 BUSH
61

+50

BIT

CONC.

11-21

11 11

+30 BUSH
61+38 BUSH
61+47 BUSH
61+09 SW CO-BLDG
63+21 BUSH
60+22 4" M
46+48 BIT
11-15+05 BUSH
65+06 BUSH
60+11 BUSH
59+23 BIT
11-19+02 BUSH
52+02 BUSH
62+04 BUSH
56+97 ER BIT
23

8+00

BIT

CONC.

11-21

11 11

+81 4" M
43+75 ER
21+92 4" M
79+82 E END 18" SCF
39+80 POR BIT
33+62 POR
26+69 CONC Curb
57-5+69 BR
57+54 BR
37+58 E END 18" CM
40+58 CONC RD
57

+50

+37 MH
27

CONC.

11 11

+47 ER
57+47 Curb
57-5+20 BUSH
63+24 ER
38+31 MH
15+36 CONC Curb
116+25 BR
57+16 W END 18" CM
40+11 CONC RD
57+25 Curb
57-5+16 HYD
31+16 WSO
29+16 POR
26+07 BUSH
37+03 ER
57+03 CONC Curb
57-5+03 BR
21

7+00

BIT

CONC.

11-21

11 11

+93 W END 15" SCF
39+92 POR
31+75 BT
11-23SEE NEW
NOTES

6+50

BIT

CONC.

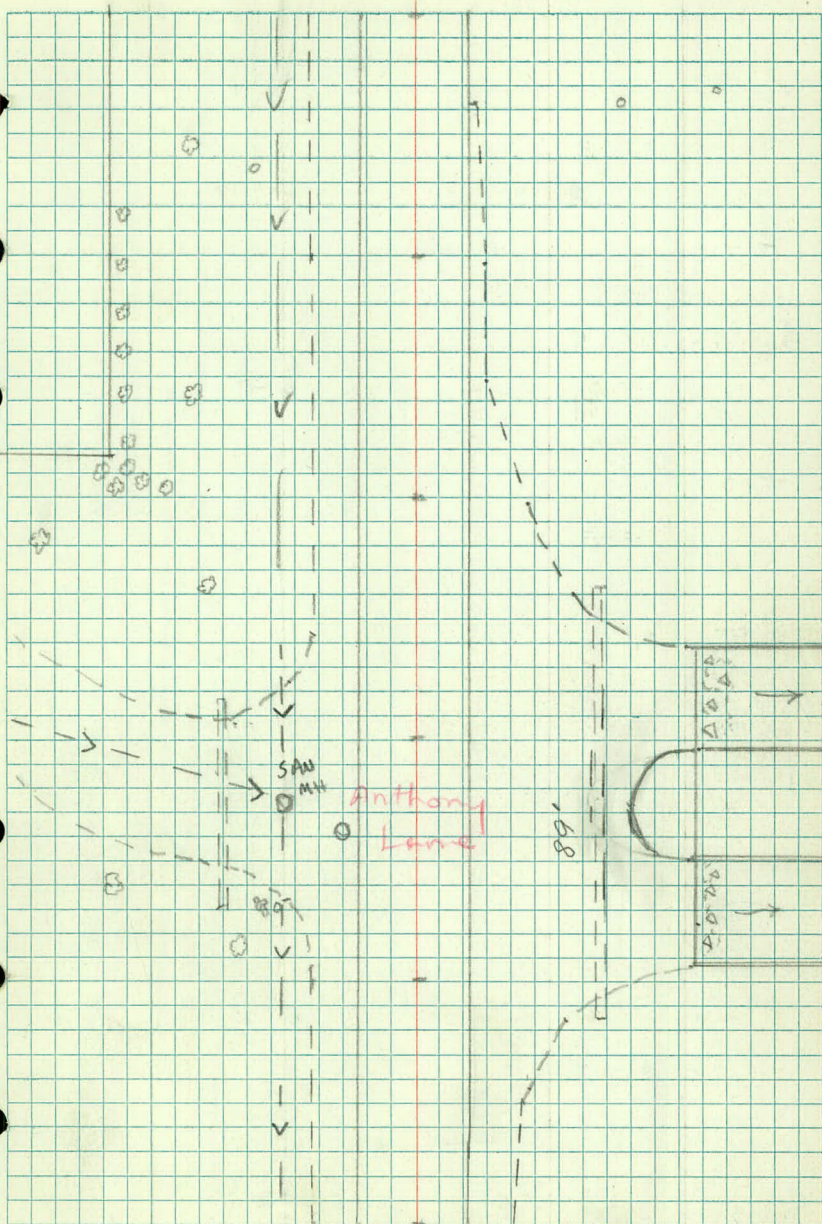
11-21

11 11

LT

30 Nov. 1973

5A



+50

LT

E

RT

11+00

+50

10+00

BIT

11-21

15' ENT

+99 PP + SL END CONC.

31

31

11

11

+71 E 25.0' ENT

+84 Post

35

+57 Post

36

+54 W. END 15" CM

31

+50

+39 SE Cor Bldg CONC.

+32 4" M

63

11

11

+37 END BUSH

+16 4" M

46

+21 4" M

37

58

+10 Begin Bush

58

9+00

BLOG BIT

63

11-21

CONC.

11

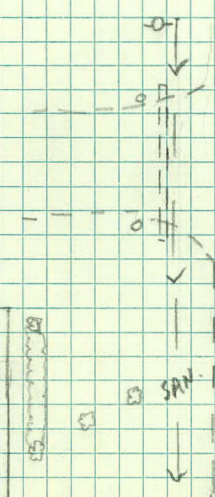
11

LT

30 Nov. 1973

RT

6A



13+00

+50

12+00

11+50

KP
DS
LPD.

12 NOV. 1974
CLOUDY & WINDY
34°

CO. RD. C

Sta 7+00 Henn. Co.

STH #8 TO ~~CLEVELAND AVE~~

ADDITIONAL TOPOGRAPHY

E

+50

conc
11-37

Curb
37

+06 conc
11-24-42

Curb
42

3+00

+05 NOSE
22-24

Curb
43

+50

B624

Curb
22

MED

B6

Curb
35

B6
Curb
53

2+00

B624

Curb
22

B6

Curb
51

B6

Curb
70

B624

+65 Curb LITE
22 28

B6 B6
Curb Curb
64 83

B624

B6

+50

Curb
25

Curb
72

Curb
94

1+00

Curb

Curb

Curb

12 NOV. 1974

LT

E

RT

75

20

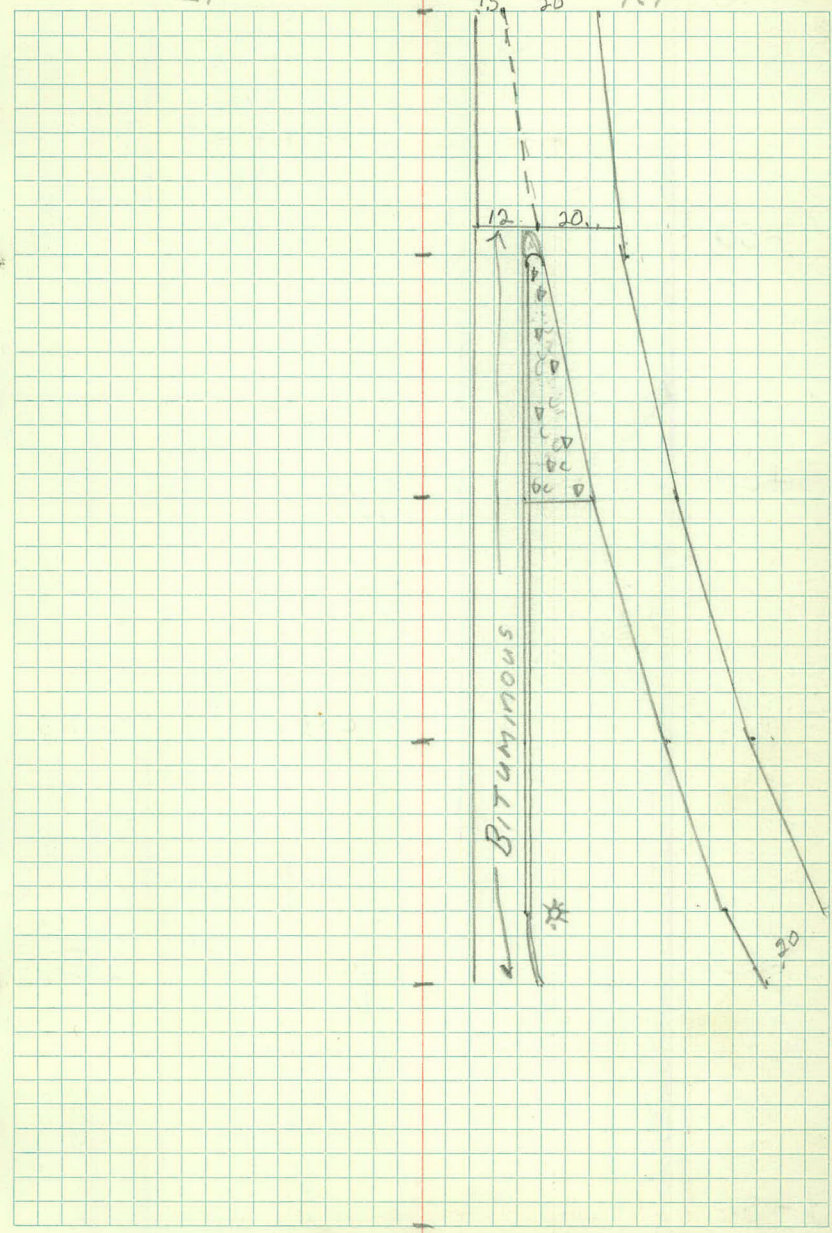
12

20

1

BITUMINOUS

20



6+00

£

Conc.
11-22

+72 Conc.
11-22

+50

Conc
11-23

5+00

Conc
11-27

+77 END Curb
28

+65 ^{12" amapcon}
53

+65 CB
28

+65 Curb
29

+50

Conc.
11-30

Curb
30

4+00

Conc
11-33

Curb
33

3+50

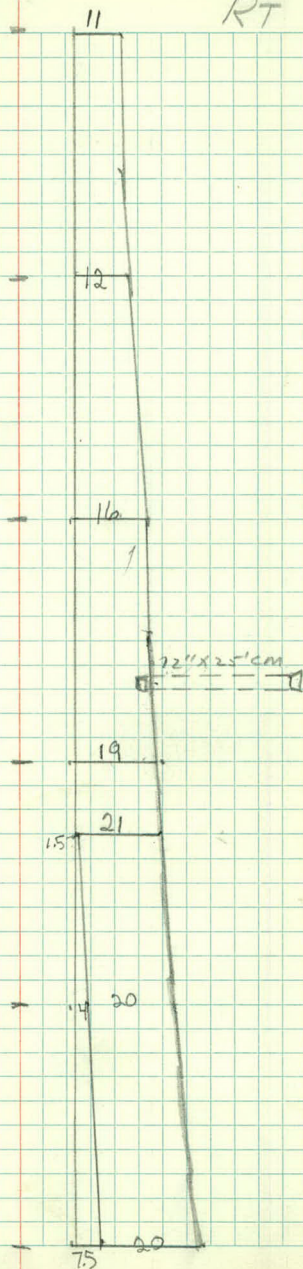
Conc
11-37

Curb
37

LT

12 NOV. 1974

RT



£

7+00

+62 END. Conc
11-22

+50

Conc
11-22

6+00

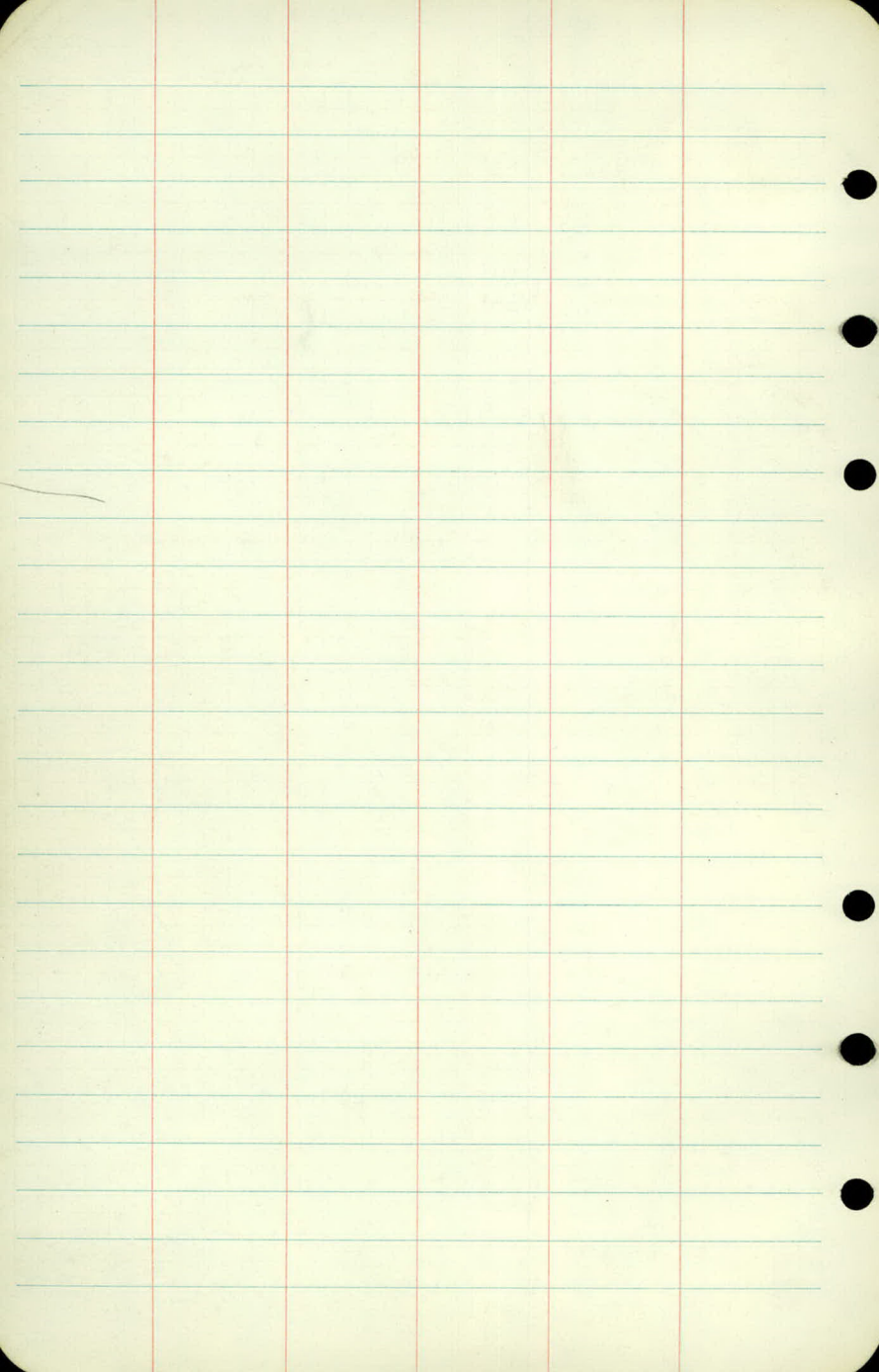
Conc
11-22

L7

£ 12 NOV 1974

R7





28 Nov. 1973
SUNNY 30°

9A

Co. Rd. C

W. Co. Line To 300' W.

ADDITIONAL TOPOGRAPHY

0-100

B.T. LT

11-21

✓
CONC.
11 11

RT

0-134 MH
280-110 LITE
36

0-175 E. END 15" CM

0-150

B.T.

11-21

31

CONC.

11 11

0-180 SW Cor Bldg
63

0-189 E 19.0 BT ENT.

+00 B.T. / 0-203 W. END 15" CM

0-200

0-203 PP

31

CONC.

0-208 SEG 11 11

0-218 BLUSH

63

62

0-209 6" P

61

0-229 4" P

62

0-247

4" M

31

Ash

0-250

B.T.

11-21

CONC.

11 11

0-251 SW Cor BLDG

63

0-271 E END 15" CM

0-277 GATE POST

0-284 E 22.0 BT ENT

31

0-300

B.T.

11-21

CONC.

11 11

0-302 GATE POST

32

0-301 W. END 15" CM

0-301 PP
28

0-350

B.T.

11-21

CONC.

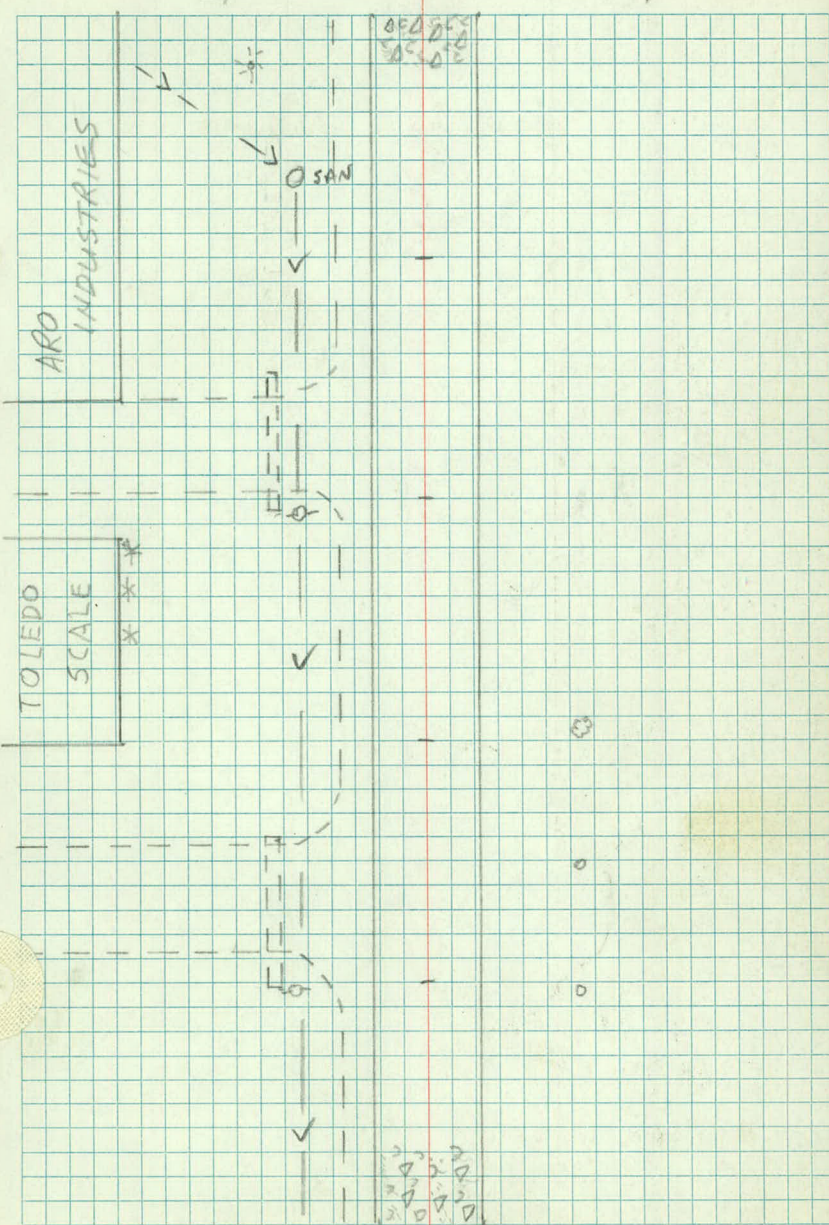
11 11

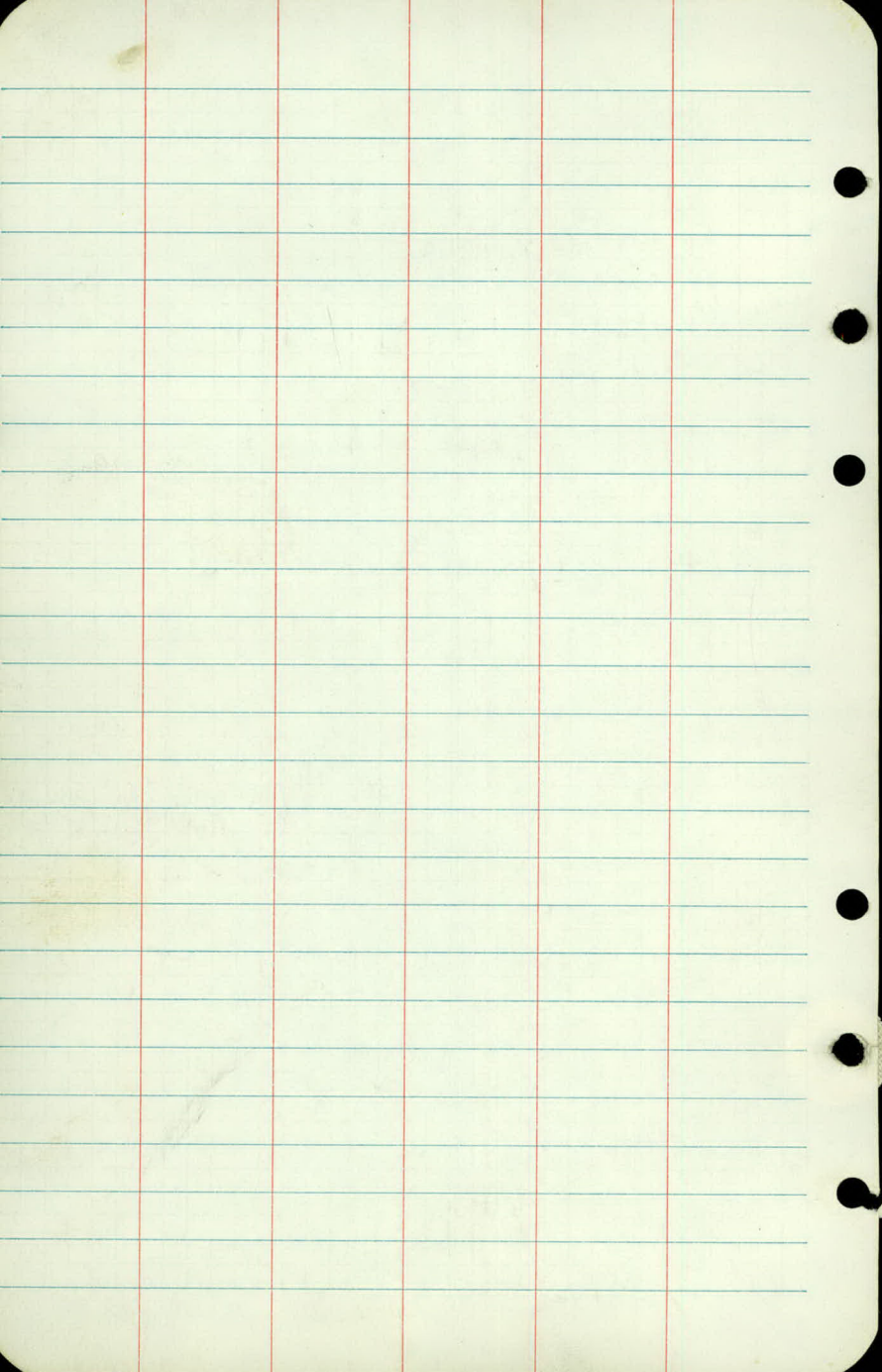
28 NOV, 1973

9B

RT

LT

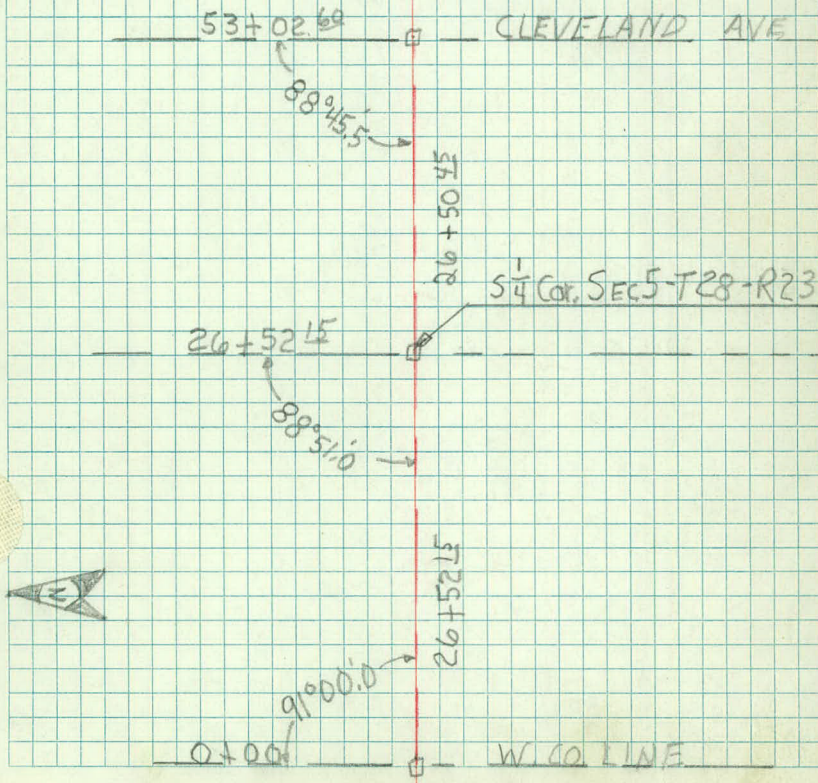




Co. Rd C

W. CO. LINE TO CLEVELAND

TOPOGRAPHY



LT

E

RT

+50

CONC.

$$\begin{array}{r} 12 \text{ CM} \\ +39 \text{ W. END} \\ +47 \text{ RT ENT} \end{array}$$

11 11

+36 Row of Trees

+41 GV (S)

$$\begin{array}{r} 30 \\ 63 - N \\ +27 \text{ PP} \\ 29 \end{array}$$

29

1+00

CONC.

11 11

+85 GV (S)

29

+50

CONC.

11 11

+29 GV (S)

29

+21 MH

+27 MH

Tel. 28

+09 MH

28

24

0+00

Iron

33

MONT.

0-5 PP

29

0-30 E. END 15" CM

0-31 GV

0-32 HYD

18

0-46 E 22' ENT.

0-50

CONC.

11 11

0-60 W END 15" CM

0-80 SE Cor Bl 29.

64

0-93 Triple 2" Birch

41

0-100

BIT

CONC.

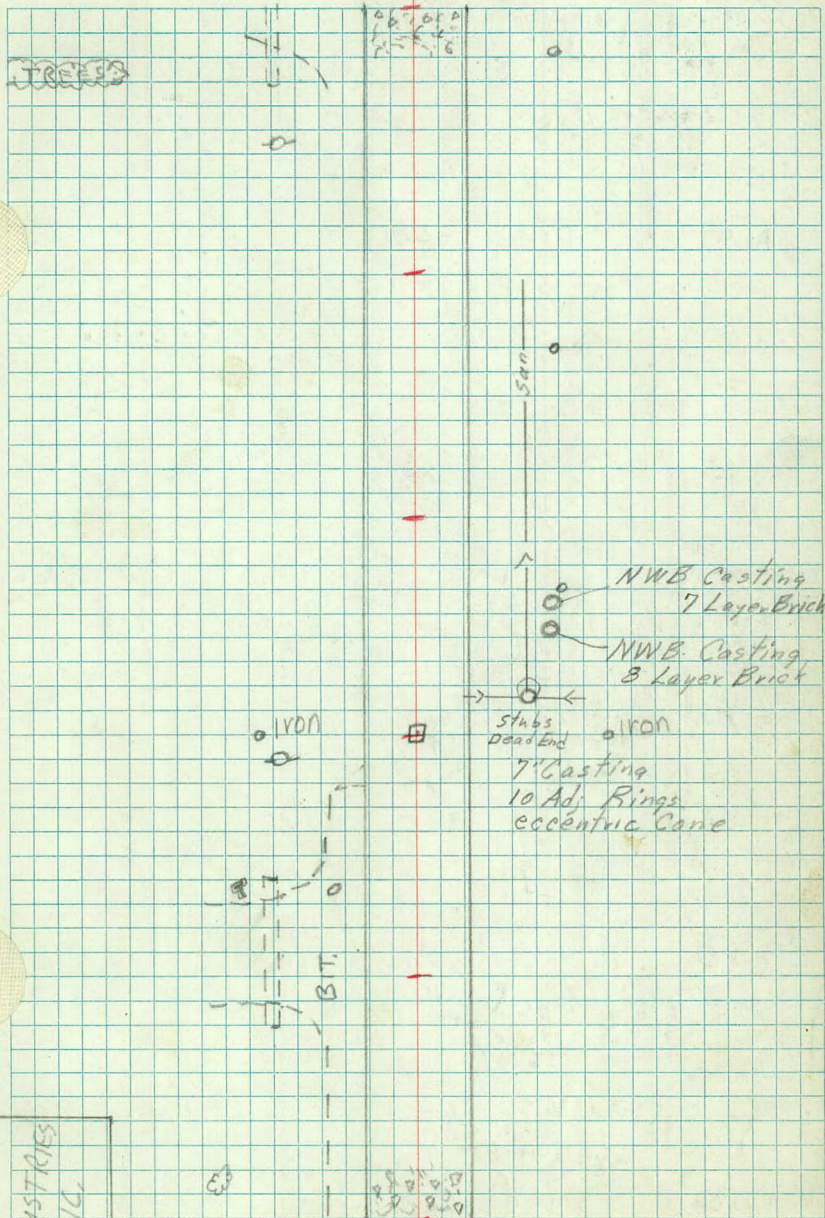
11-21

11 11

LT

26 Nov. 1973 RT

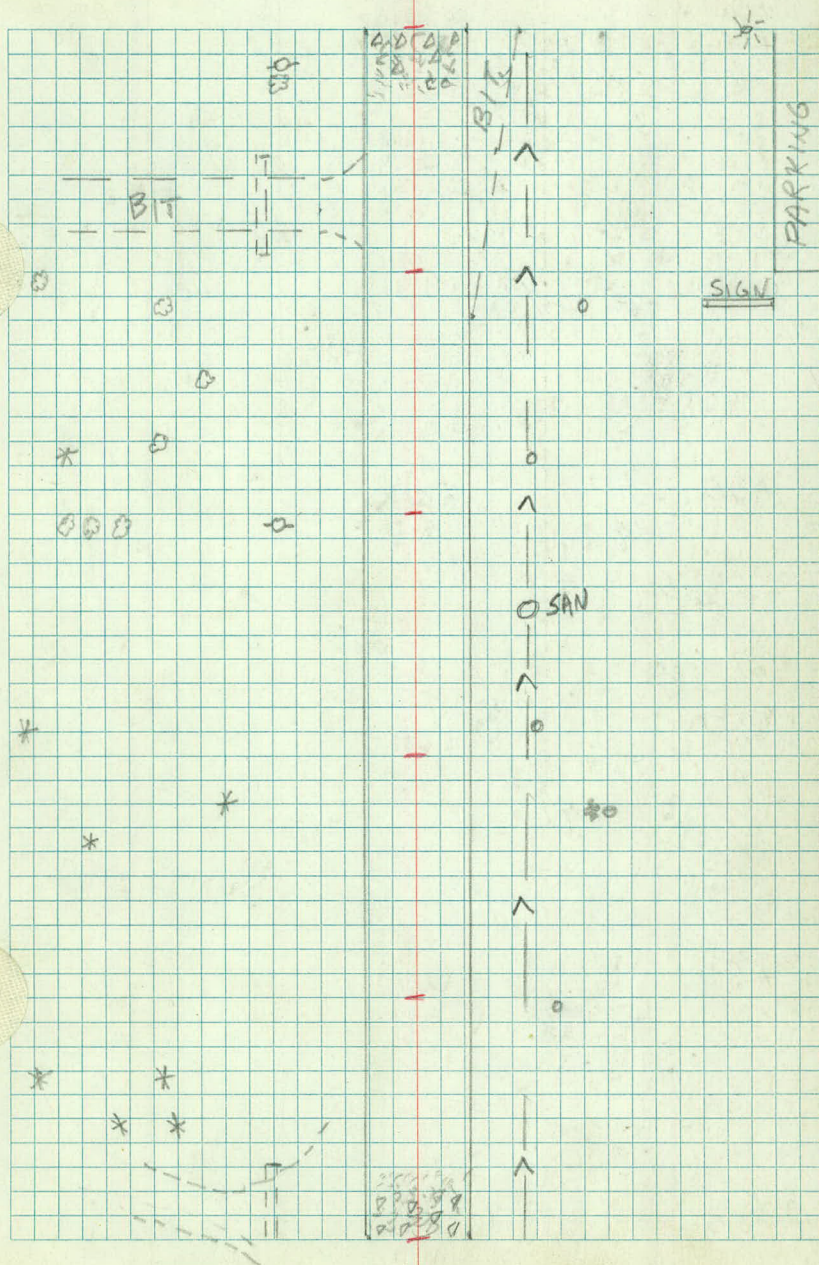
11,



ARO
INDUSTRIES
INC.

LT

26 Nov 1973 RT 12



LT

E

RT

+50

CONC.

11 11

+20 PP

17

+32 E WALNUT ST.

+26 5"CE

36

+28 6"CE

39

+06 CONC CEG

59-5

+14 4"CE

38

+16 5"CE

37

+04 CB

44

+06 ER

59

6+00

CONC.

11 11

POR

40

+89 TW 5"CE

33

+90 POR

29

+67 5"CE

37

+71 BR

24

+76 MH

28

+50 8"CE

CONC.

11 11

+49 6"CE

31

+30 PP

28

+31 PP

33

+98 6"CE

31

+95 4"CE

31

+26 GV(S)

34

5+00

CONC.

11 11

+68 10"CE

34

+89 8"CE

49

+97 END Parking

74

+78 6"CE

47

+80 MH

22

+56 6"CE

41

+67 LITE

68

+50

CONC.

11 11

BIT

11-22

PARKING Lot

74

+47 4"CE

31

+11 7"CE

32

+14 4"CE

29

+35 LITE

68

+17 GV(S)

33

+05 6"CE +08 7"CE

33

29

CONC.

11 11

BIT

11-22

LITE

69

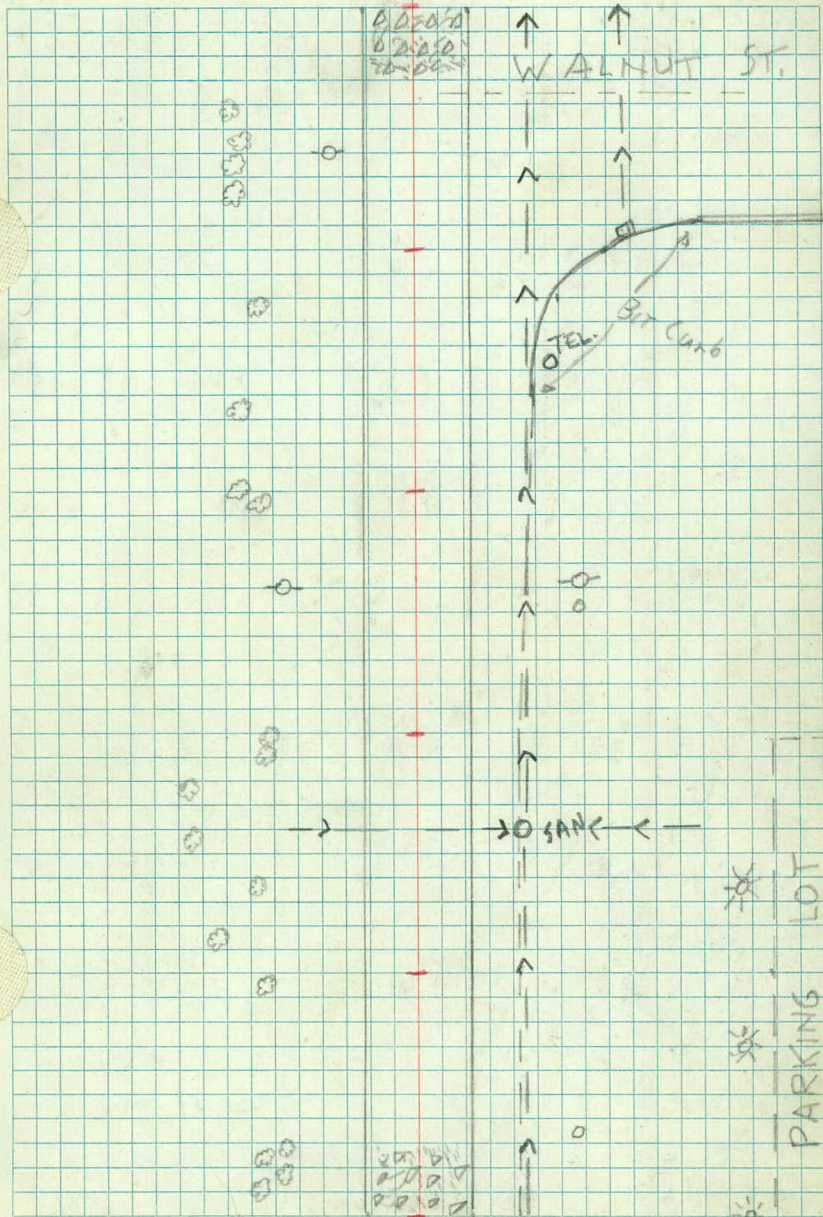
4+00

LT

26 Nov 1973

RT

13



9+00	LT FE 37	E CONC. 11 11	RT BIT 11-16	BLDG 83
+84 SPILLWAY				
34-39	+72 PP 28			
			+55 N.W. Cor	BLDG 83
+50	FE 37	CONC. 11 11	BIT 11-23	Cor. PARKING LOT 83
8+00	FE 37	CONC. 11 11	BIT 11-23	PARKING LOT 83
			+79 MH 24	
+50	FE 37	CONC. 11 11	BIT 11-23	PARKING LOT 83
			+33 MH 33	
	+11 CB 32		+12 SD 43	+22 MH 29
7+00	FE 37	CONC. 11 11	+80 ER 26	PARKING LOT 83
	+65 FE Cor		+68 POR 34	+81 PAV BOX 31
+64 PP 28	37-N			+65 PP 38
			+61 CB A3	+58 BR 57
6+50	+54 (12 6" TREES	CONC. 28-39 11 11	+58 CONC. CEG 57-5	

LT

26 Nov 1973 R7

14

6.0 CYCLONE

0000
0340
0000

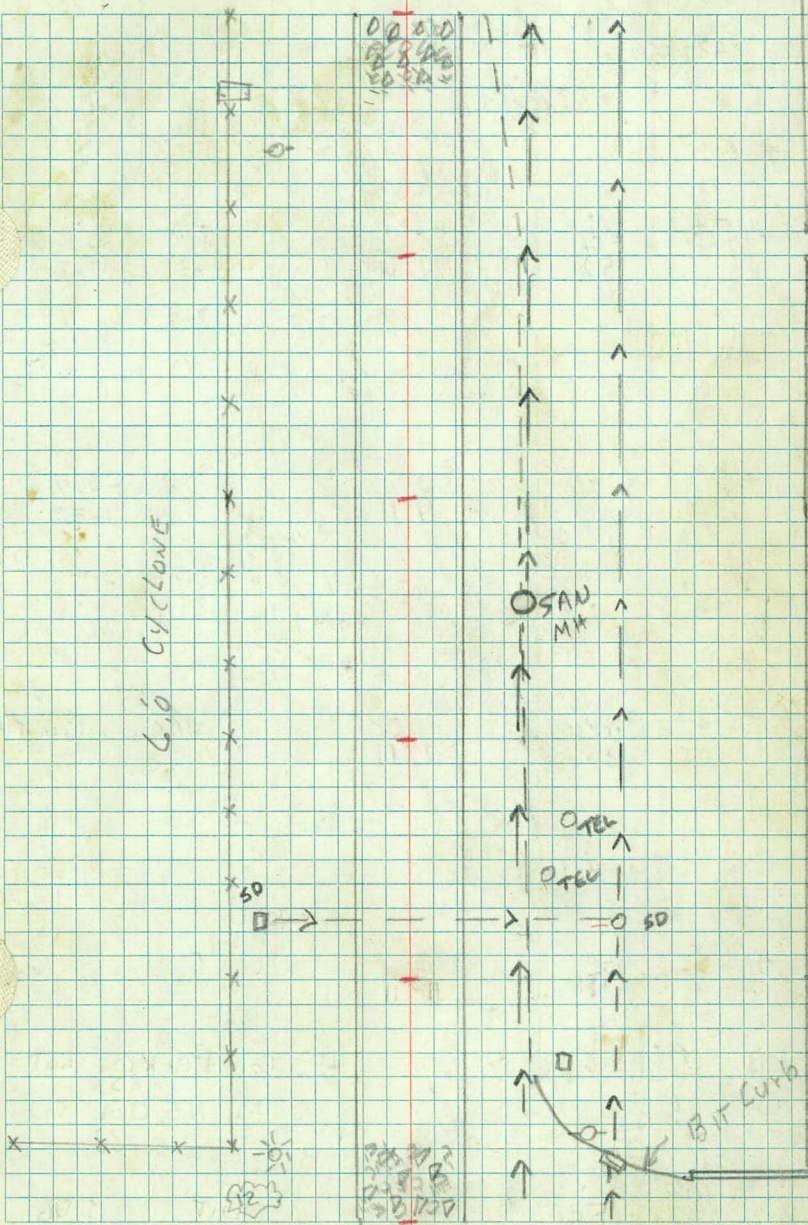
SAN
MX

0REV

0REV

50

BIT Curb



LT

E

RT

+50

CONC.

Conc.

11-22

+27 GATE POST

+44 E ENT.

+23 POR

+11 Cor ENT HI CUMB

+10 POR

+06 Mont. BM

61

+03 MH

35

11+00

POR

FE

CONC.

ER

+99 HND

Conc.

50

118

11

11

29

45

11-22

+87 POR

+91 SD

+94 MH

+84 MH

36

+58 POR

+68 MH

+65 E EUSTIS

19

+54 ER

+50

CONC.

38

Conc

11 11

+46 POR

11-22

+34 MH

+43 PP

+41 Cor Parking Lot

+43 PP

35

27

31

33

+30 Conc

+41 SD

85

+41 PP

11-13

+34 MH

23

+36 BR

83

10+00 FE Parking Lot

CONC.

CONC.

Parking Lot

36-118

11 11

11-22

83

+75 E 16' ENT

+74 Conc

11-22

+70 Conc

11-14

+50

FE

CONC.

+16 Parking Lot

+13 W. END 18' SCP +16 FE Cor

+32 Cor Parking Lot

37-118

118

11

83

+05 HND

+07 MH

+21 N.E. Cor Bldg.

+15 HEADWALL

35

45

+17 BIT

83

9+00

FE

CONC.

BIT

BLDG

37

11 11

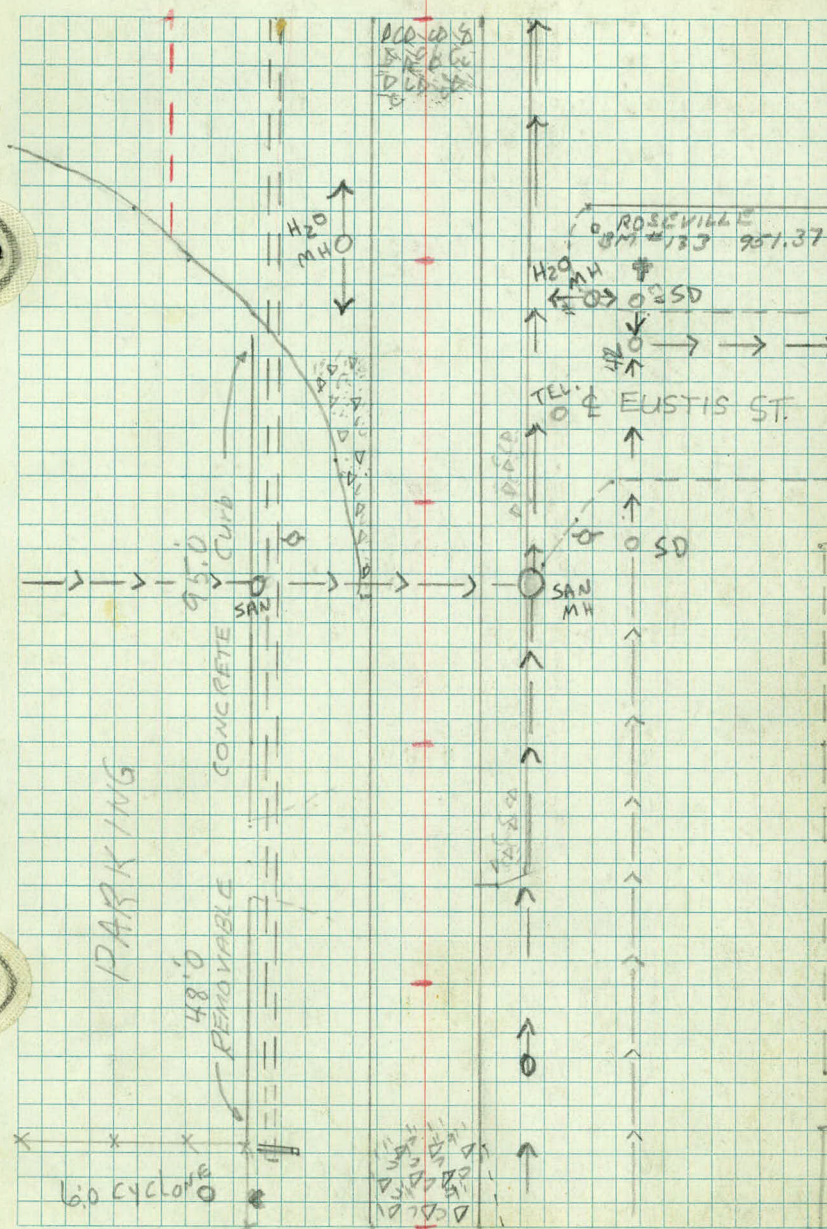
11-16

83

24

26 Nov 1973 RT

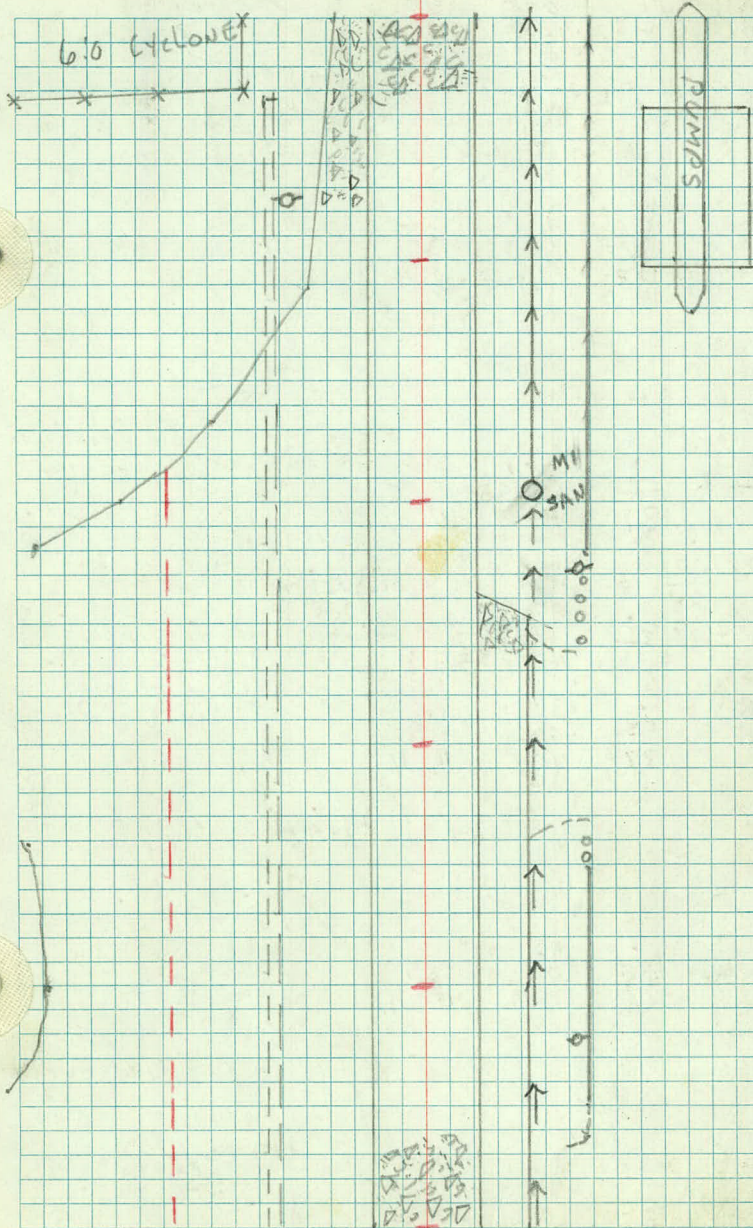
15



L7		F		RT	
14+00	FE	Conc	CONC.	Curb	BLDG
	37	11-18	11 11	35	133
+85	FE Cor				
	37				
+84	E END 18" SCP				+81 Roof
	31				46-67
	+64 PP	+82 FE Cor			
	28	118			
+50		CONC.		ISLAND	+48 Roof
		11 11		53-59	46-67
+44	ER				
	24				
	+16 POR			+38 W. END IS.	
	44			56	
				+02 MH	
				23	
13+00	FE	POR	CONC.	+86 PP	+87 Curb
	118	63	11 11	33	24
	+91 POR			+76 Conc	+81 Conc.
	81			11-22	11
				+80 Post	+83 Post
				33	33
	+85 GATE Post			+72 Post	+76 Post
	118			33	33
+50	FE	CONC.			
	118	11 11			
				+30 Post	+27 Post
				33	33
+46	GATE Post	+38 LITE		+23 Curb	
	118	98		34	
	+29 POR				
	83				
12+00	FE	POR	CONC.	CONC.	
	118	78	11 11	11-22	
				+89 NW Cor BLDG	
				133	
	+78 POR			+68 END ENT	+87 PP
	89				32
	+65 GATE Post			+75 Beg Curb	
	118			34	
11+50		CONC.		CONC	
		11 11		11-22	

16

6:0 CYCLONEX



	LT		E		RT	+50 LITE 107
+50	FE	CONC	CONC.		PARKING LOT	FE
	37	11-16	11 11		44-102	105

16+00	FE	CONC	CONC.		PARKING LOT	FE
	37	11-17	11 11		45-102	105

+64 LITE
107

+50	FE	CONC	CONC.
	37	11-17	11 11

+60 PARKING LOT
43-102

+28 PP
25

+19 WSD
30

+19 HYD
32

+22 FE COR
105-5
+21 POST
33

+21 POST
34

+21 POST
36

+24 CURB
25

+18 CURB
32-38

15+00	FE	CONC.	CONC.
	37	11-18	11 11

+01 COR FE
78-5

+60 MH
22

+83 FE
78

+54 POST
33

+58 POST
33

+50	FE	CONC	CONC.
	37	11-18	11 11

+48 END CURB
35

+44 COR BLD
133

+44 FE
133

+44 FE
113

+02 FE END IS
56

14+00	FE	CONC.	CONC.
	37	11-18	11 11

CURB
34

BLDG
133

LT

26 Nov 1973 RT

17

66 CYCLONE

Parking

11/28/73
Cyclone
66
11/28/73

11/28/73
Cyclone
66
11/28/73

11/28/73
Cyclone
66
11/28/73

11/28/73
Cyclone
66
11/28/73

19+00

LT

E

RT

FE

CONC.

$$\begin{array}{r} 37 \\ +94 \text{ PP} \\ \hline 28 \end{array}$$

11 11

+88 E ENT

+61

$$\begin{array}{r} \text{HYD} \\ 31 \end{array}$$

$$\begin{array}{r} +61 \text{ WSO} \\ 24 \end{array}$$

$$\begin{array}{r} +69 \text{ GATE Post} \\ 36 \end{array}$$

$$\begin{array}{r} +53 \text{ Cor SD} \\ 50 \end{array}$$

+50

$$\begin{array}{r} \text{FE} \\ 37 \end{array}$$

$$\begin{array}{r} \text{CONC.} \\ 11 \quad 11 \end{array}$$

$$\begin{array}{r} \text{Cor SD (5x8)} \\ 46 \end{array}$$

$$\begin{array}{r} +46 \text{ Cor SD} \\ 54 \end{array}$$

$$\begin{array}{r} +43 \text{ Cor SD + 26 LITE} \\ 50 \quad 107 \end{array}$$

$$\begin{array}{r} +28 \text{ BIT} \\ 36 \end{array}$$

$$\begin{array}{r} +13 \text{ BIT} \\ 11 \end{array}$$

$$\begin{array}{r} +28 \text{ FE Cor.} \\ 36-105 \end{array}$$

18+00

$$\begin{array}{r} \text{FE} \\ 37 \end{array}$$

$$\begin{array}{r} \text{CONC.} \\ 11 \quad 11 \end{array}$$

$$\begin{array}{r} \text{Parking Lot} \\ 38-102 \end{array}$$

$$\begin{array}{r} \text{FE} \\ 105 \end{array}$$

$$\begin{array}{r} +60 \text{ Open End 18" CM} \\ 106 \end{array}$$

$$\begin{array}{r} +66 \text{ MH} \\ 23 \end{array}$$

+50

$$\begin{array}{r} \text{FE} \\ 37 \end{array}$$

$$\begin{array}{r} \text{CONC.} \\ 11 \quad 11 \end{array}$$

$$\begin{array}{r} \text{Parking Lot} \\ 41-103 \end{array}$$

$$\begin{array}{r} \text{FE} \\ 105 \end{array}$$

$$\begin{array}{r} +39 \text{ LITE} \\ 107 \end{array}$$

$$\begin{array}{r} +07 \text{ PP STUMP} \\ 33 \end{array}$$

17+00

$$\begin{array}{r} \text{FE} \\ 37 \end{array}$$

$$\begin{array}{r} +89 \text{ PP} \\ 28 \end{array}$$

$$\begin{array}{r} \text{CONC.} \\ 11 \quad 11 \end{array}$$

$$\begin{array}{r} \text{Parking Lot} \\ 42-102 \end{array}$$

$$\begin{array}{r} \text{FE} \\ 105 \end{array}$$

+60 CONC

$$\begin{array}{r} +54 \text{ CONC} \\ 11-16 \end{array}$$

16+50

$$\begin{array}{r} \text{FE} \\ 37 \end{array}$$

$$\begin{array}{r} \text{CONC.} \\ 11 \quad 11 \end{array}$$

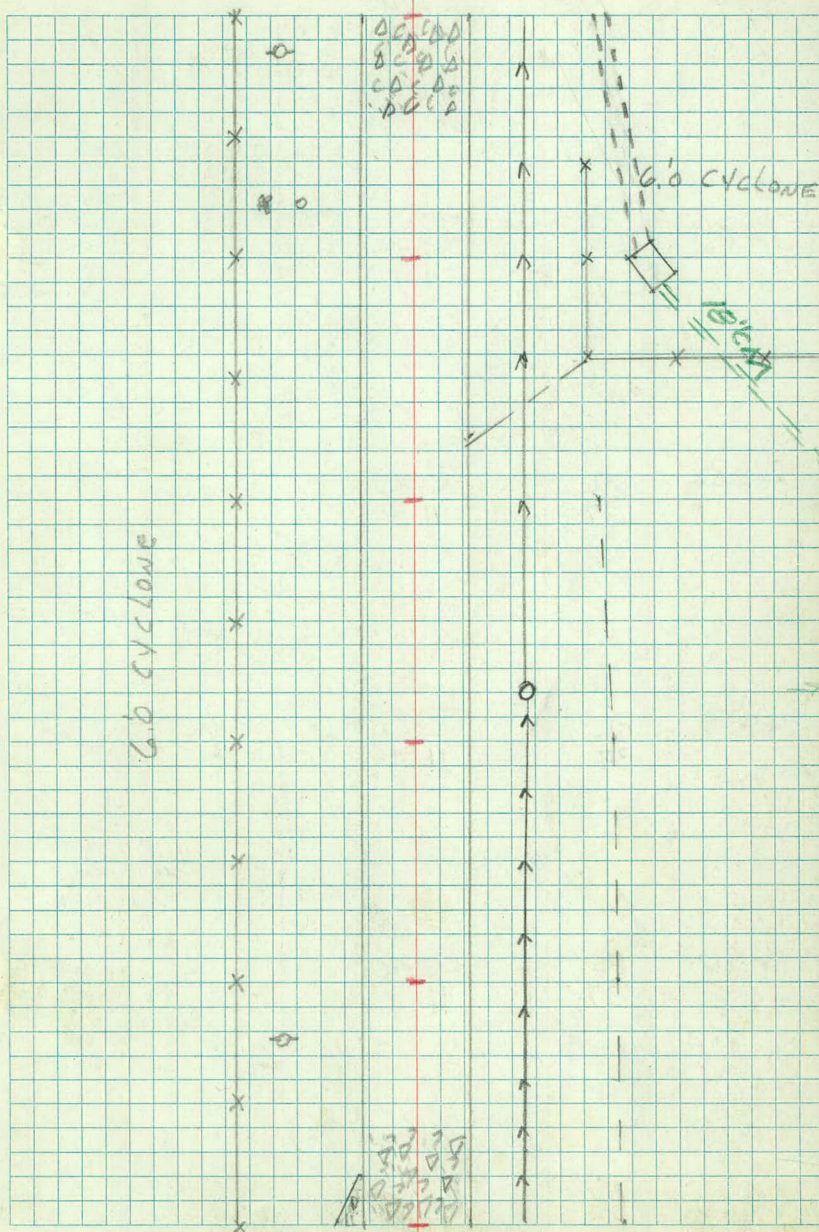
$$\begin{array}{r} \text{Parking Lot} \\ 44-102 \end{array}$$

$$\begin{array}{r} \text{FE} \\ 105 \end{array}$$

LT

26 NOV 1973 R1

18



LT

E

RT

+50

FE
37CONC.
11 11FE
35+47 BIT
11

+25 M14

+21 GATE POST
36+24 BIT
36

21+00

FE

CONC.
11 1137+96 AP
27+77 BIT +82 GATE
34 36+77 END WALL
24+76 W. END 15" CM
32+52 FIRE BOX
34

Tell Con. Post

+50

FE
37CONC.
11 11+42 TEL MH
26+45 BIT
11+23 N.E. Cor Bldg
103

20+00

FE
37CONC.
11 11WALL
34FE
35+66 P.I.P.
29

+50

FE
37CONC.
11 11WALL
34FE
35

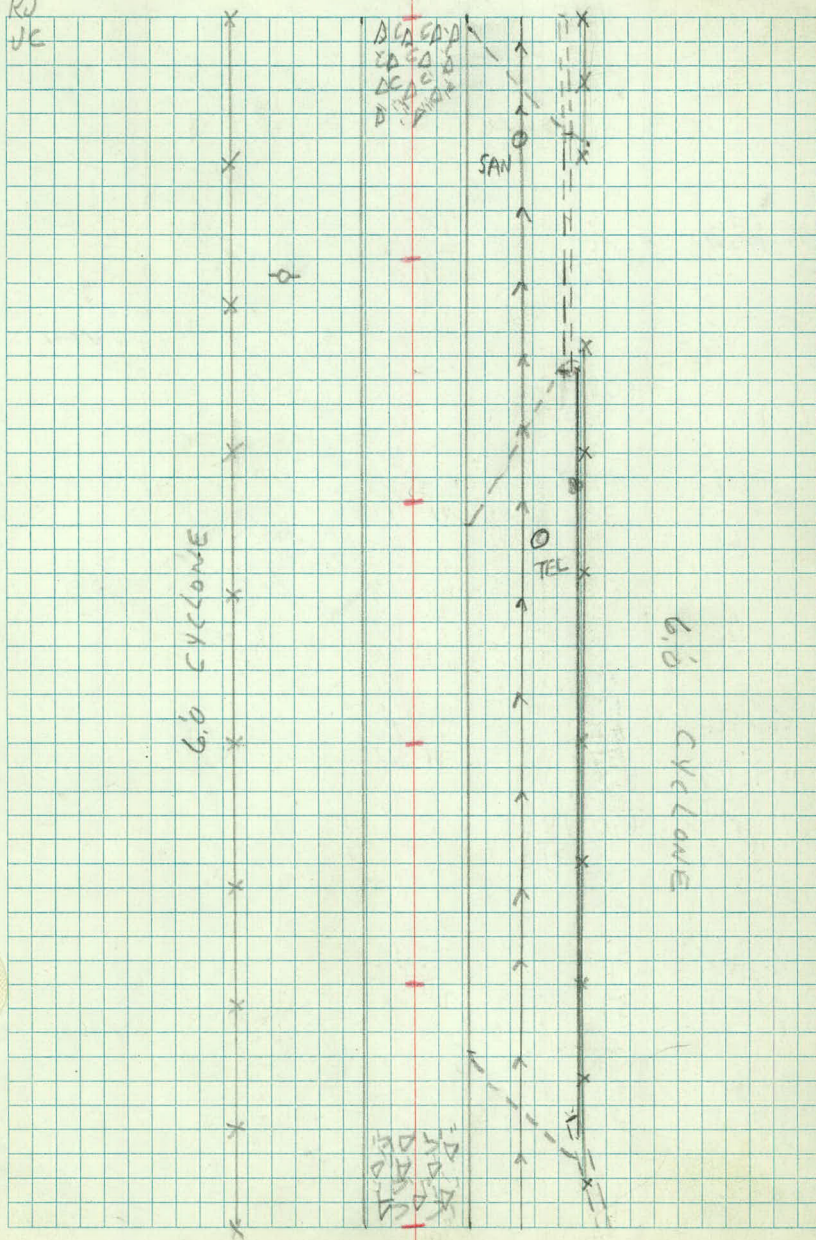
+21 E. END 24" CM

+36 BIT
11+18 Begin 3.0 Black Wall
35+14 BR
34+09 GATE POST +11 NW Cor Bldg.
36 103

19+00

FE
37CONC.
11 11

19



24+00

FE
37CONC.
11 11FE
34

+50

FE
37CONC.
11 11FE
34+08 PP
28+27 PP WITH LITE
36+02 N.E. Cor BLDG
109

23+00

FE
36CONC.
11 11FE
34+98 MH
24+77 E END 12" SCP
32

15" Jk

+41 NW Cor Bldg.
109

+50

FE
37CONC.
11 11FE
34+19 PP
27+10 HYD
31+21 APE
34

22+00

FE
37CONC.
11 11FE
35+75 GV
35

21+50

FE
37CONC.
11 11FE
35

LT

27 NOV. 1973 RT.

20

G.D. CYCLONE

G.D. CYCLONE

A. A. A. A.
E. A. A. A.
A. C. S. S.
A. C. S. S.

A. A. A. A.
E. A. A. A.
A. C. S. S.
A. C. S. S.

LIFE

SAN

LT

E

RT,

+50 E TRACKS CONC.
79 11 11

+50 POLE BASES
425 81

+37 Switch
44

+36.39 E MAIN TRACKS

+25 E TRACKS
78

26+00 +97 PP 43 CONC.
26 11 11

+07 MH
23

+92 PP
26

+70 E TRACKS
70

+77 PP
105

+66 ER
11

+53.23 E SPUR TRACKS

+50 +49 POR 30 CONC.
11 11

+34 E RD +46 BR 41

+35 E TRACKS
79

+20 POR
30

+25 ER
39

+65 PIPE LINE

+25 E TRACKS
107

+20 RT FE

+24 RT E RD +07 BR 61

+11 MH
23

+16 FE COR
34

+06 FE COR +05 PIPE LINE 16
37 39 +05 PP 28

25+00

FE
37

CONC.
11 11

FE
34

+94 RT FE

+72 FE COR
34

+84 E END 12" G
30

+51 FE COR
34

+50

FE
37

CONC.
11 11

+46 W END 12" CIP
30

24+00

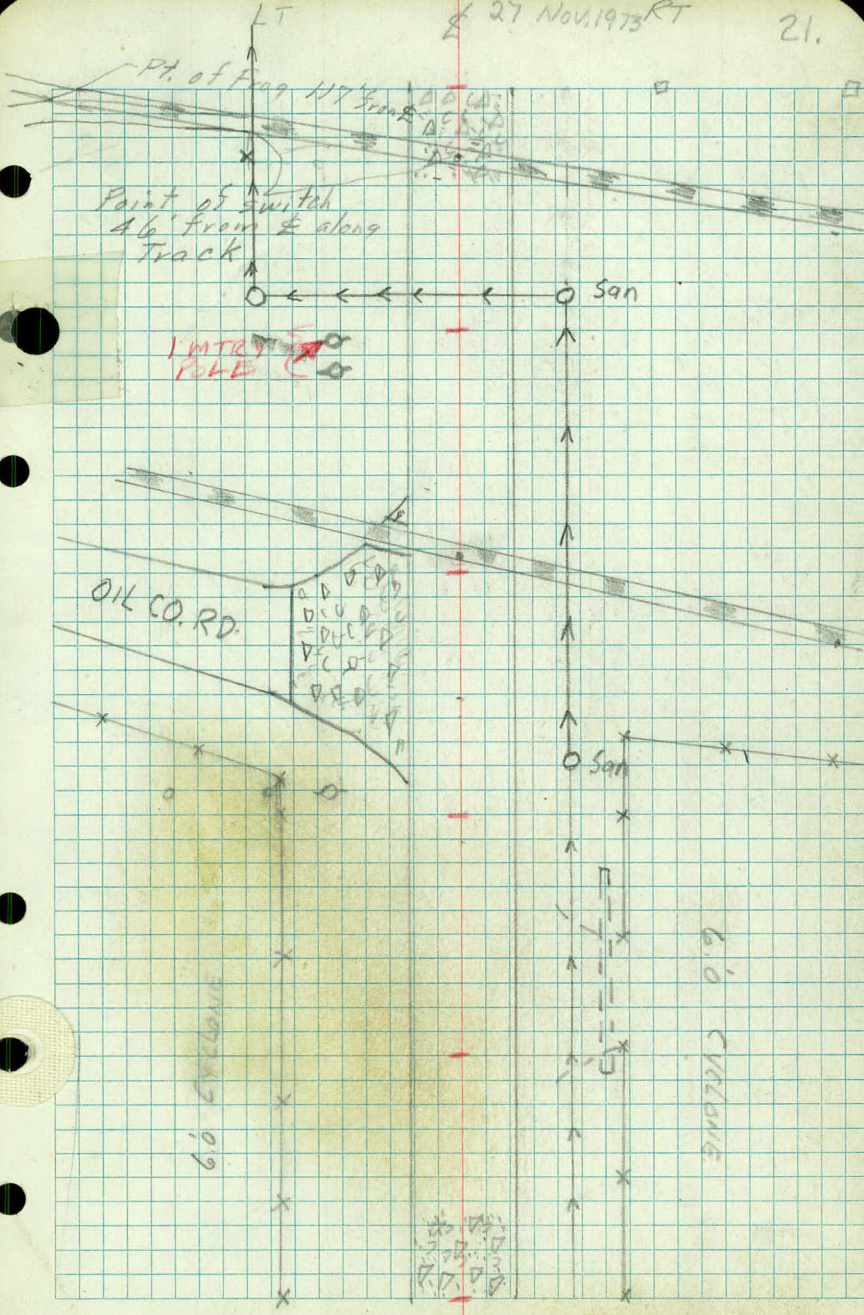
FE
37

CONC.
11 11

FE
34

27 Nov. 1973 RT

21.



29+00

LT

Conc.

11 11

RT

FE

41

Bldg

154-162

End Tile

37

+88 30" BE

36

+71 28" STP

35

+55 30" BE

35

+77

beg. Tile

111

+81

Cor Bit

106

Cor Bit

+70

123-154

+50

Conc.

11 11

FE

41

+39 30" BE

35

+23 1/4"

+18 WSO

24

+18 HYD

31

+14 control pole

31

37

28+00

Conc.

11 11

FE

41

+63 conduit

37

+61 PIPE LINE

+63 8" P

+55 12" P

+52 VENT

42

+50

PP

28

Conc.

11 11

FE

41

+43 PIPE LINE

+38 PP

28

+31 FE Cor

41-5

+36 RT FE

+29 Power Cable

32

+17 PIPE LINE + 21 PP

38

53

27+00

Conc.

11 11

+96 PIPE LINE

40

+89 POLE BASE

43+82

Power Cable

+88 29-22

+83 PP

18

+86 N. END 84" Arch Apron

67

A-3-M

+52.15 MONT.

+61 S. END 84" Arch

102

APR

26+50

Conc.

11 11

120.6
41.5

LT

27 NOV 1973 RT

22

ADCA
ADCA
ADCA
ADCA

TEL

G.O. CYCLONE

MTREY RLE

MTREY RLE

HIGH LINE

TOWER

ADCA
ADCA
ADCA

+50

LT

E

RT

POR
15

FE
41

+46 W. END 15" CM
29

+34 FP
38

+17 30" BE
34

+41 E END 15" SCP

+25 POR
27

+14 FE COR
41

31+00

38" BE
34

CONC
11 11

POR
58

+94 FP
39

+93 GATE POST
88

+78 FP
39

+72 FP
39

+73 E COR. ENT. +53 ER
88

+52 LITE
88

+53 GATE POST
88

+50

+48 FP
39

CONC
11 11

+44 POR
52

+32 FP
39

+20 30" BE
84

+29 6" P
57

+38 7" P
75

+24 POR
29

+15 FE COR
39

+16 PP
28

+33 FE COR
41

+26 8" P
70

+13 TW 6" CE
39

+08 W. END 12" SCP
35

+02 18" Pine
154 40.8

30+00

CONC.
11 11

POR
17

FE
41

+98 E 11.0 ENT

+95 41 Cor. Bldg
161.6

+82 MH
43

+85 36" BE
54

+74 Bit
123-154

+64 S.P
63

+77 BR
11-13

+82 MH
32

+55 Bush
73

+50

CONC.
11 +43 ER
11-13 +38

FE
41

+42 E END 12" SCP
35

+18 30" BE
34

+34 BR
8

+11 ER
21

+45 154-162
Bldg

+02 BR
11-13

+08 GATE POST
41

+04 PP
28

+02 12" SCP W END
35

29+00

CONC.
11 11

FE
41.5

CT

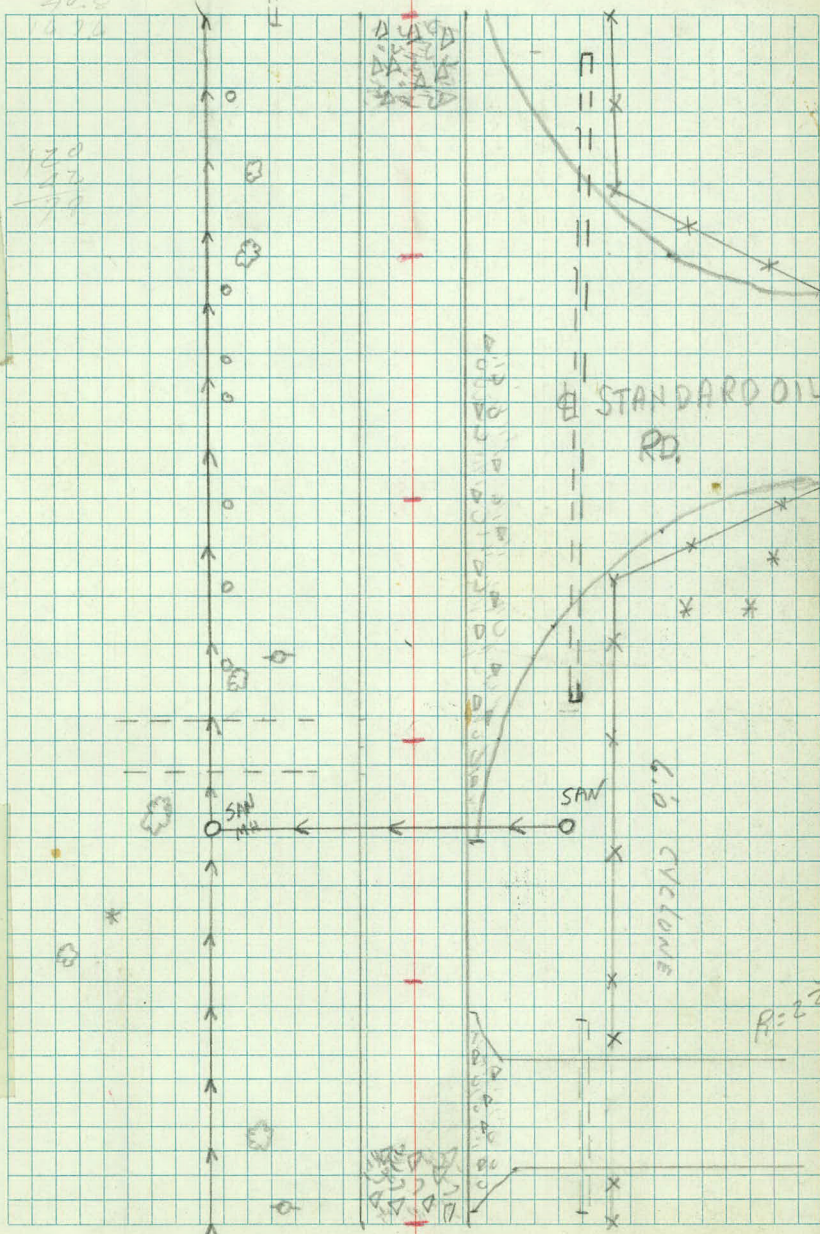
27 NOV 1973 RT

23

120.8
20.2

10.10

120
20
10

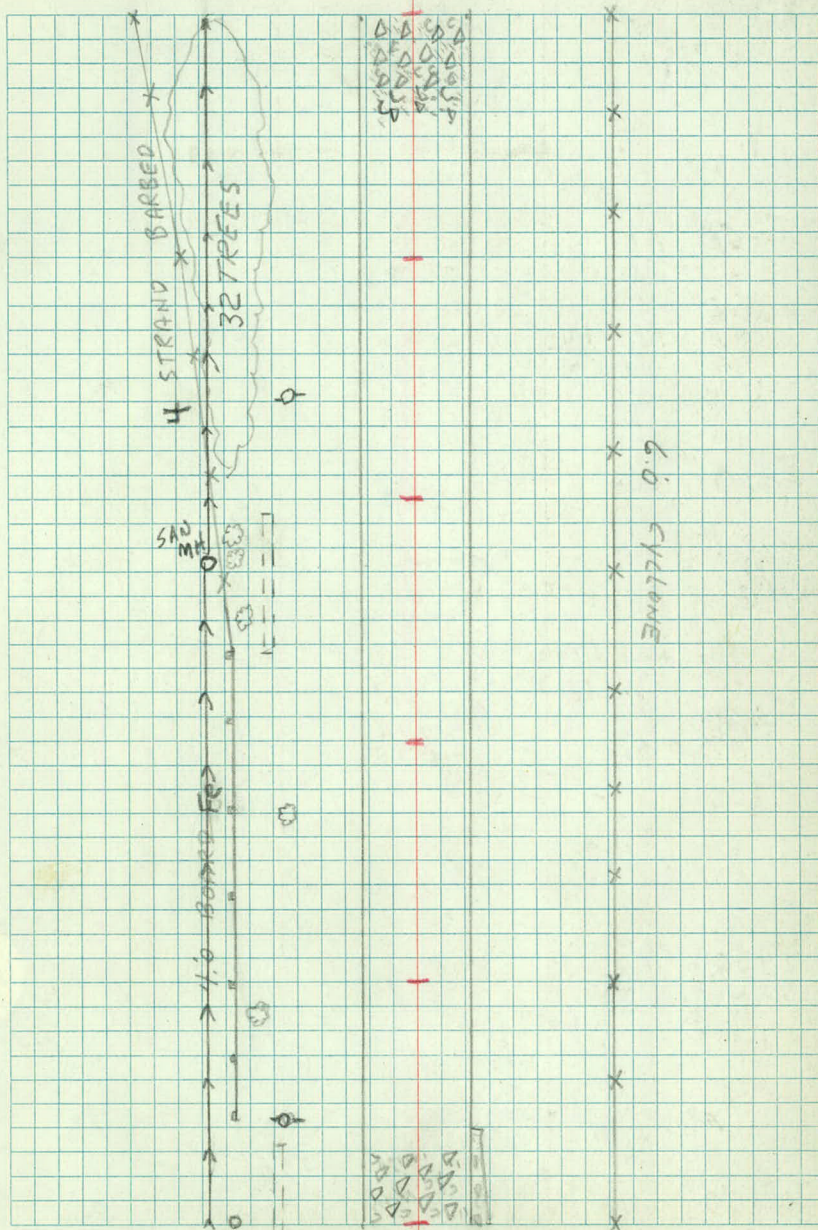


+67 4" CE 34+100	LT +70 4" CE 39 FE (59)	+71 4" CE 51	+88 4" CE 42	RT	FE 41
+62 7" PP 4" CE 38	+64 4" CE 34	+52 4" CE 48			
+44 4" CE 38	+45 6" CE 42	+41 4" CE 40			
+38 4" CE 38	+39 4" CE 42	+35 4" CE 41			
+35 4" CE 33	+31 4" CE 36	+29 4" CE 27			
+50	FE 49	+26 4" CE 38			FE 41
+19 5" CE 38	+19 6" CE 36	+25 4" CE 38			
+19 4" CE 34	+13 4" CE 27	+22 PP 28			
+07 6" CE 40	+09 4" ELM 37	+27 4" CE 39			
	+96 E END 15" SCP 31				
33+00	+94 8" CE 39	Conc 11 11			FE 41
+68 END WOOD FE MA ³⁹	+75 7" POR 36				
+67 1/3	+67 W. END 15" SCP 31				
+68 Bay Wive Fe 39	+87 6" CE 39				
+50		Conc 11 11			FE 41
	+35 4" ELM 27				
32+00	FE 39	Conc 11 11			FE 41
+94 30" O 34	+72 BEGUN BOARD FE 39				
+64 FP 38	+72 PP 28				
	+66 E END 15" CM 29				
+51 FP 38		+69 ER 11-13			
31+50		Conc 11 11			POR 15
					FE 41

LT

27 Nov 1973 R1

24



+50

L7
FE
71E
Conc
27 27RT
BIT
27-33FE
76

36+00

FE
71Conc
23 23BIT
23-29FE
76✓
+84 MH
43 *+86 FE Cor
75 -5.

+50

FE
71Conc
19 19BIT
19-25+31 Cable x
62
+31 Cable v
62+43 PP
38+04 Angle Point
59 x

35+00

FE
71Conc
15 15BIT
15-21FE
75+81 N.E. END 12° CIP
41+90 PP
28+53 FE Cor
41-75

+50

FE
68

Conc

FE
41+40 Conc
11 11BIT
11-17+26 HYD
31+36 TEL VENT
32

34+00

FE
59Conc
11 11FE
41

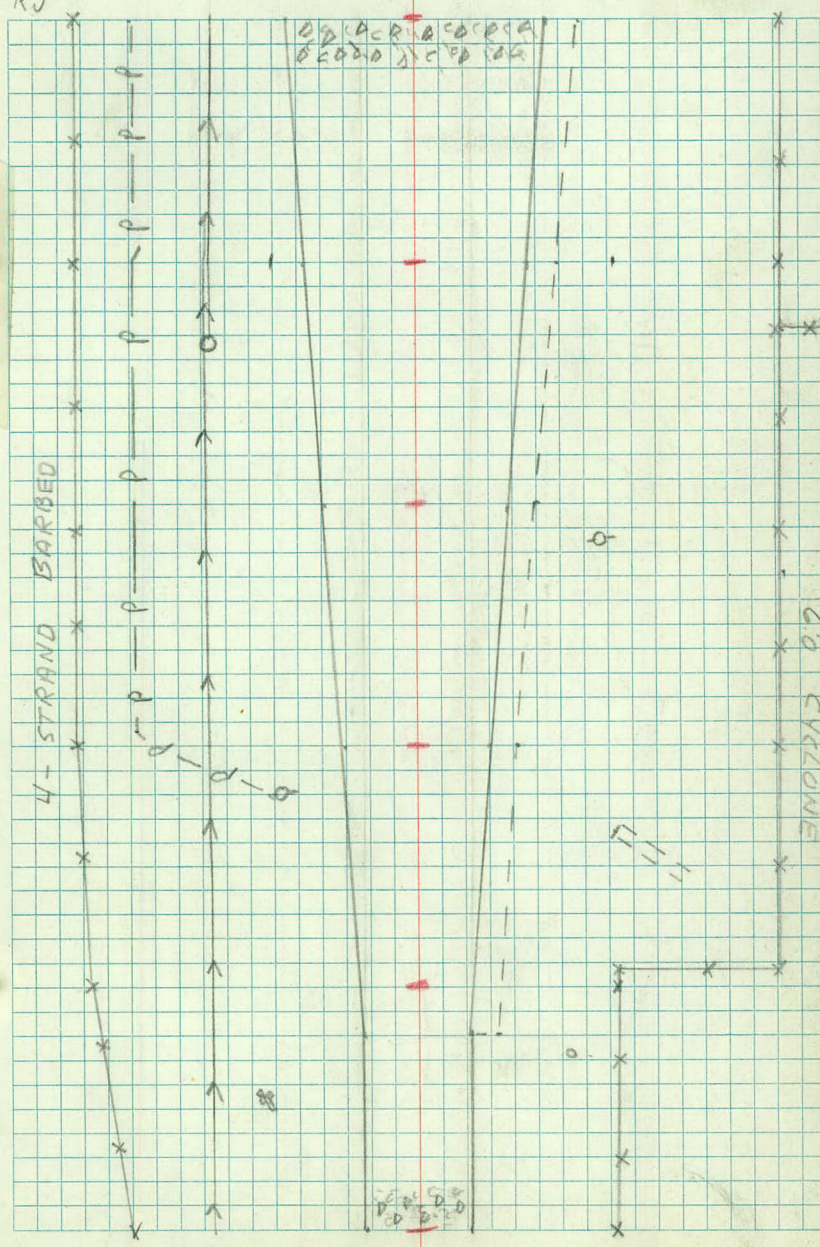
KP
DS
RJ

LT

28 NOV. 1973 RT
CLOUDY 25°

25

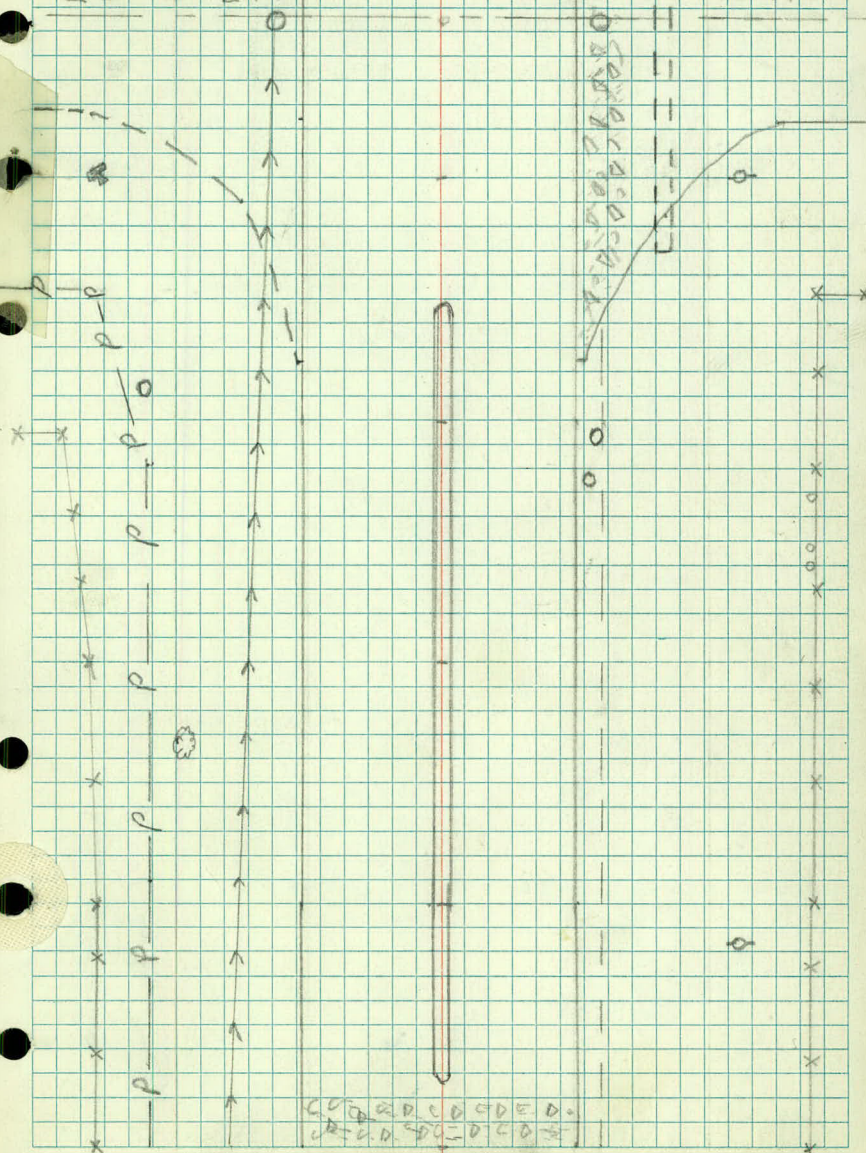
4-STRAND BARBED



39+00	LT	±	Rt	
				+95 MH 102
+82	MH 35	+81 = ±	LONG LANE RD	+82 MH 32
+63 ER 74		+61 ER 70		+61 CB 150
+50	+A1 Hyd 72 *			+57 PP 90
+45 POR 42 *	+27 Cable 70 - N. END	+24 END MEDIAN		+40 W.E 18" SCP 50 *
+12 BR 28	+07 MH 61			+26 FE COR 77 - S
				+41 POR 47
				+12 BR 29
38+00		CONC MED CONC BIT		FE
	+90 Cable *	28 2 2	28 28.34 + 96	MH 77
	+96 FE 78 - N		+84 OIL LINE 76	+74 OIL LINE 76
			+70 OIL LINE 76	
+50	FE 73	MED 2 2		FE 77
+32	5" TWCE 52 *			
	+05 Cable 61			
37+00	FE 71	CONC MED 28 2 2	CONC 28	+91 PP FE 41 77
		+63 BOD IN MED 2 2		
		+60 CONC 28 28		
36+50	FE 71		BIT 27-33	FE 76

26

ROAD



LT
+50 FE BIT CONC MED
45 28-34 28 22

RT
CONC.
28

41+00 FE BIT CONC. MED
45 28-34 28 22

CONC. BIT
28 28-34

+50 FE BIT CONC MED
45 28-34 28 22

CONC.
28

+17 PP
+11 Curb Line 60
76

+03 Curb Line
76

40+00 FE BIT CONC. MED
45 28-34 28 22

CONC. BIT
28 28-34

+63 FE Cor
45

+83 MH
24

+68 ER
29

+50 ER CONC. MED
34 28 22

+54 MH
61

+20 FE Cor
84-N

+42 Begin Med
22

+32 Apron
49

+20 POR
44

+08 HYD
121

+06 BR
74

+05 CB
110
+05 MH
50

+06 BR
92

+25 POR
41

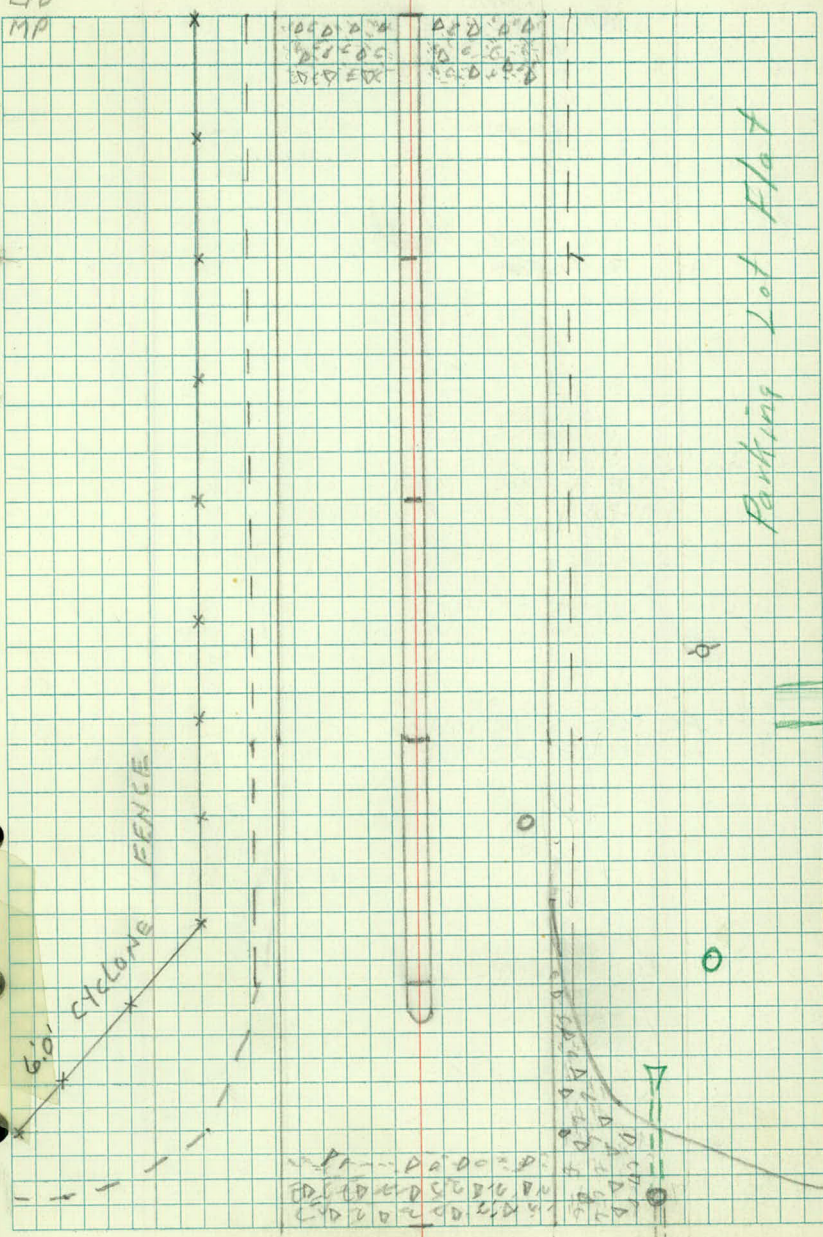
39+00

KP
DS
LPD
MP

LT

10 JAN 1974 KT
cloudy -16°

27.



44+00

FE
63CURB
51MED
2 2CONC.
28BIT
28-34+78 ARC-LITE.
62+54 MH
31

+50

CONC
28MED
2 2CONC.
28+40 NW CON B/DG
84+47 FE
76+47 CURB
65+47 MED NOSE
38

+37 PP

+27 NOSE 61 MEDIAN
CONC CURB+12 MH
23

+05 HYD.

43+00

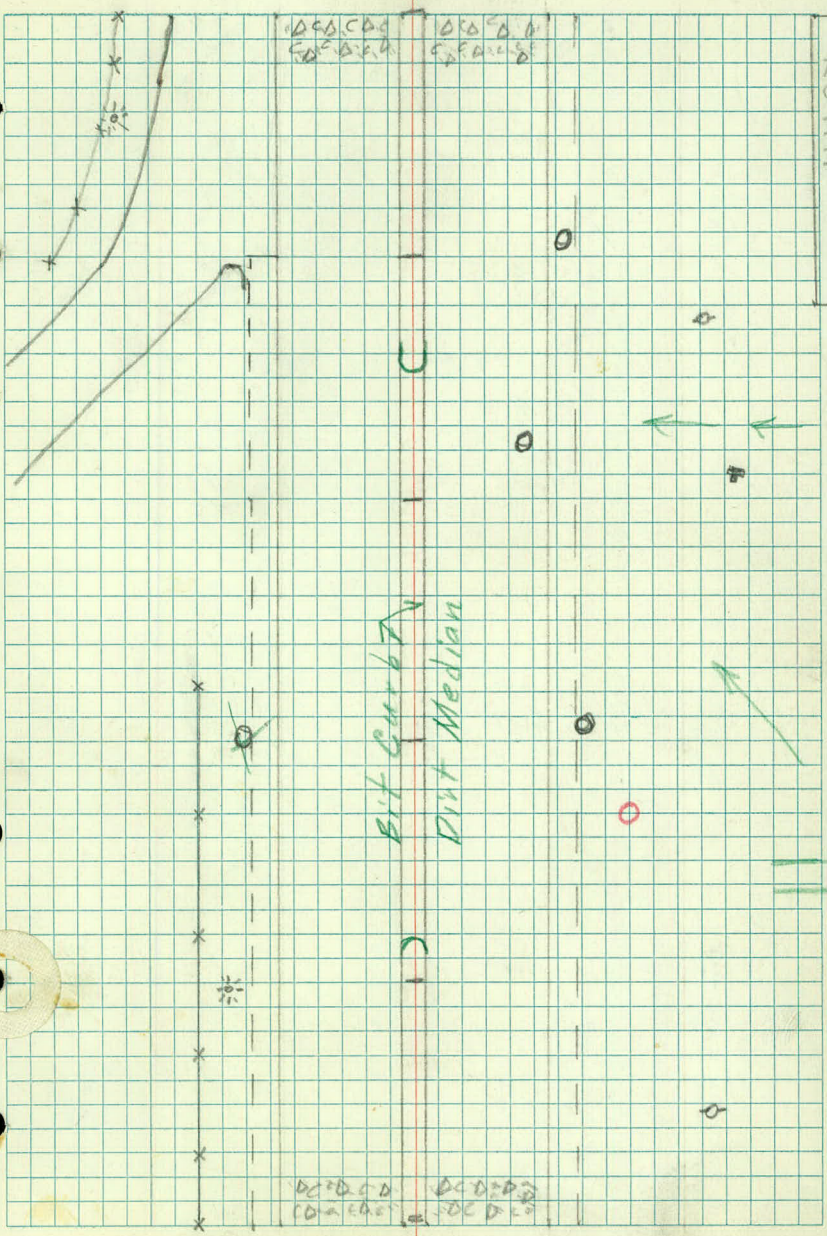
BIT
28-34CONC
28MED
2 266 CONC.
28BIT
28-34+62 END FE
45+54 MH Tell
35+35 Tell MH
45+50 FE BIT
45 28-34CONC
28MED
2 2CONC.
28+25 CURB LINE
75+18 CURB LINE
75+08.5 NOSE CONC
MED CURB42+00 FE BIT
45 28-34CONC
28MED
2 2CONC.
28BIT
28-34+97 ARC-LITE
39+74 PP
6241+50 FE BIT
45 28-34CONC
28MED
2 2CONC.
28

LT

2

11/10/74 RY

28



Bit Curve
Dirt Median

+50

FE
51Curb
37MED
2 2CONC.
28GR
34

+27 RT FE

46+00

FE
51Curb
38MED
2 2CONC.
28GR Bit
38 28-34

+81 Begin GR

+75 ARC-LITE
44

41

+59 E. END ¹⁸ 15" CM
54

+50

FE
51Curb
39MED
2 2CONC.
28+29 W. END ¹⁸ 15" CM
54

45+00

FE
51Curb
39MED
2 2CONC.
28Bit
28-34
+98 PP
62

+50

FE
53Curb
43MED
2 2CONC.
28

+00 N.E. Cor Bldg

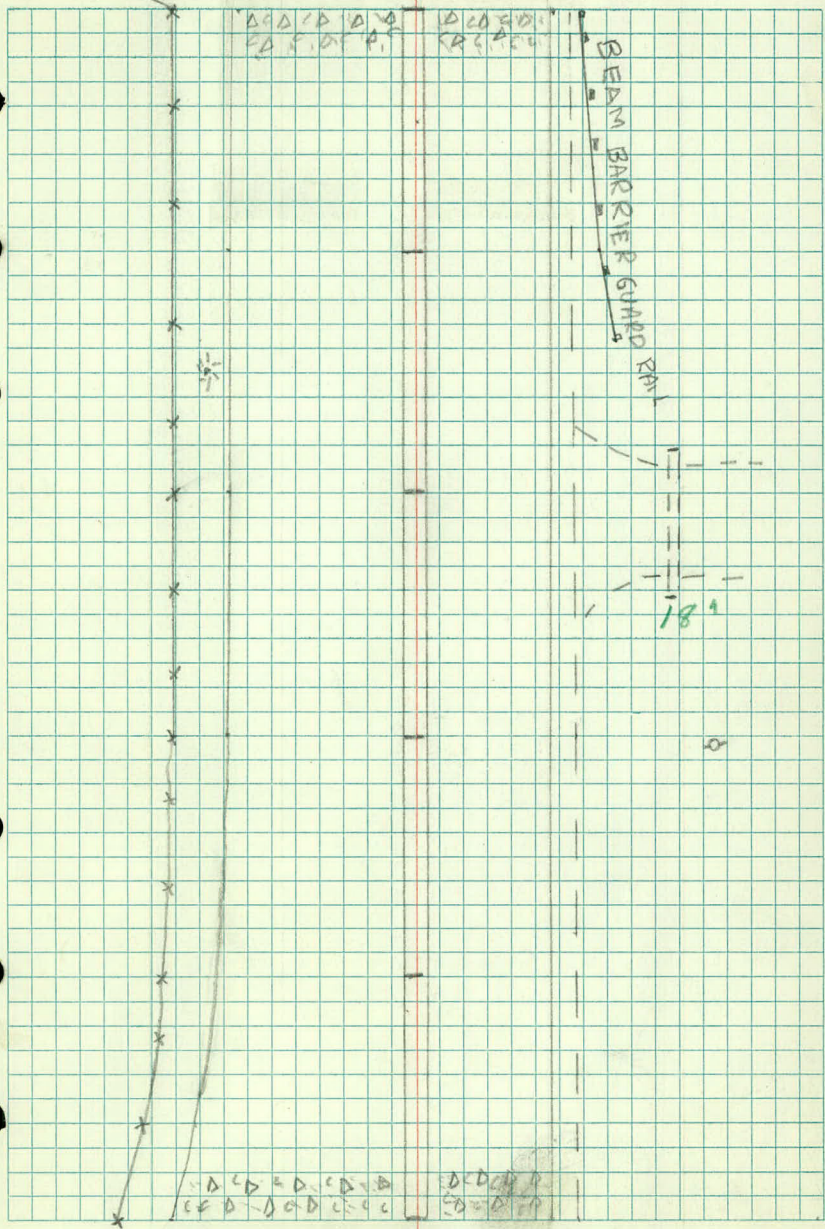
44+00

FE
63Curb
51MED
2 2CONC.
28Bit
28-34

RT 29

27

3



49+00	GR 43	Curb 37	MED 2 2	Conc. 28	GR 33	BIT 28-34
				83		
	+53 Pillar 44			+70 Pillar 35		
				+52 Pillar 35		
+50	GR 41	Curb 37	MED 2 2	Conc. 28	GR 33	
	+35 Pillar 44			+33 Pillar 35		
	+16 Pillar 44			+14 Pillar 35		
48+00	GR 41	Curb 37	MED 2 2	Conc. 28	GR 33	BIT 28-34
	+96 Pillar 44					
	+61 Pillar 44			+79 Pillar 35		
				+61 Pillar 35		
+50		Curb 37	MED 2 2	Conc. 28	GR 33	
	+23 Pillar 44	+42 Pillar 44		+42 Pillar 35	+24 Pillar 35	
	+05 Pillar 44			+02 PP 63		
				+19		
47+00	GR 41	Curb 37	MED 2 2	Conc. 28	GR 33	BIT 28-34
	+88 GR (Bog) 41			+92 Corner 40		
	+52 PE 51				+51	W. END 30" SCP 48
46+50	FE 51	Curb 37	MED 2 2	Conc. 28	GR 34	

APPRO

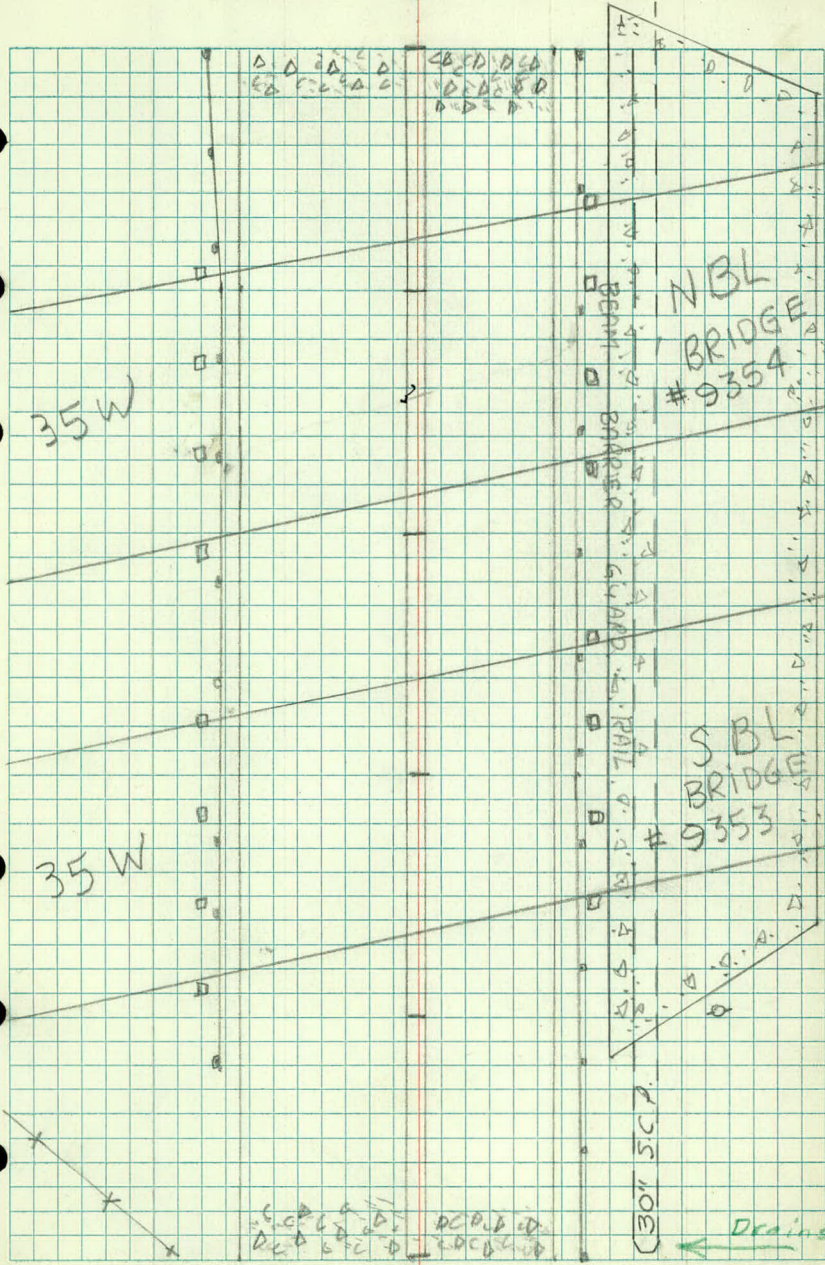
LT

2

1/10/74

RT

30



+50

LT

£

RT

51+00

+50

50+00

+90 GR
60

+79 CB
29

+50

GR
50

MED
2 2

+47 END GR
32

+29 MH
32

+12 PD
63

Slope Paring Corner

+18

40

49+00

GR
43

CONC
37

MED
2 2

CONC
28

GR
33

KP
DS
LWD
MP

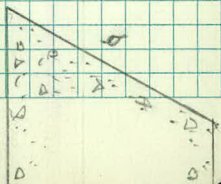
LT

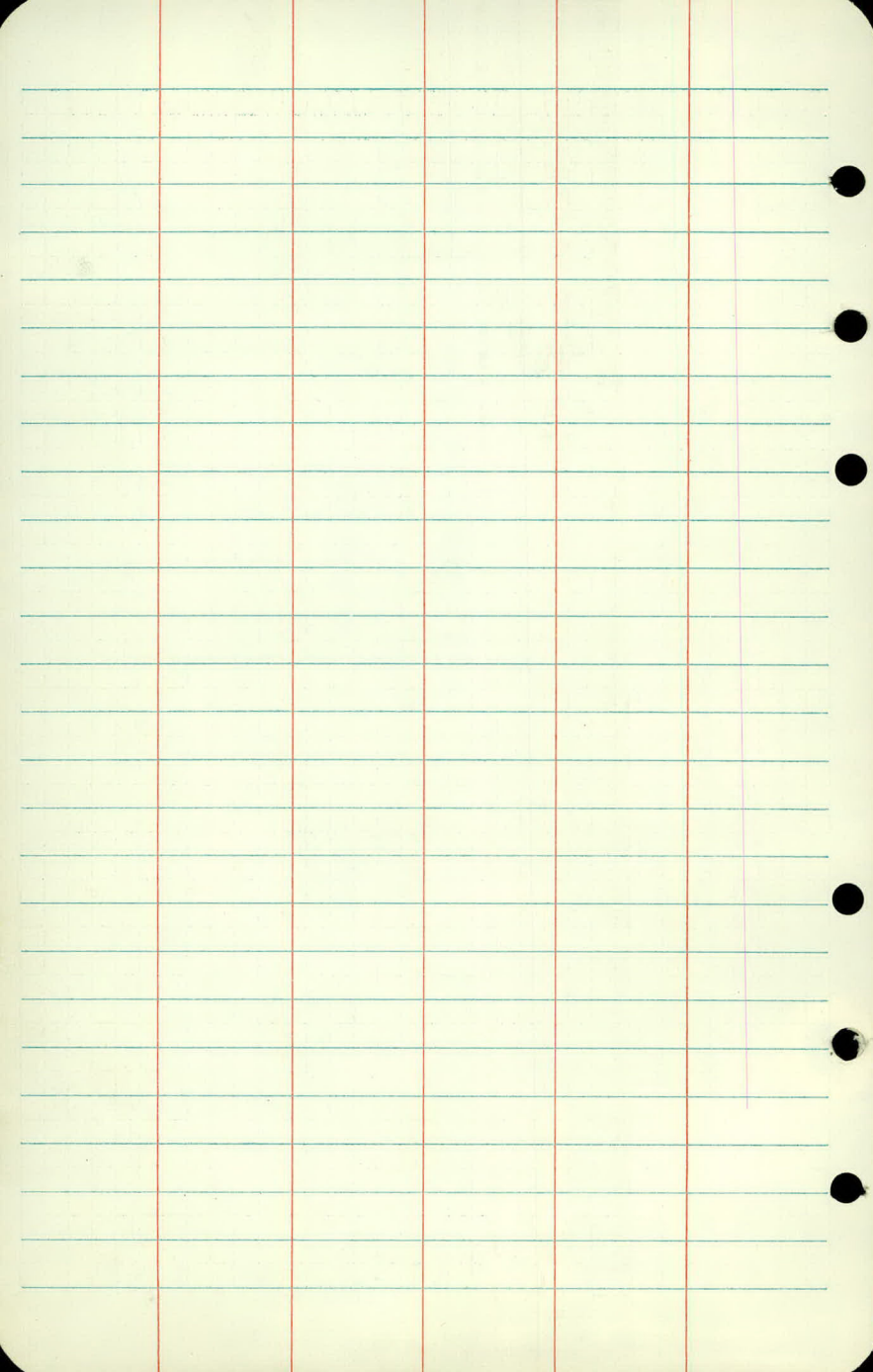
E

11 JAN 1974
-120
SUNNY

RT

31





W.S
R.C
E.Y

6-22-76
CL 90°

ADDITIONAL TOPOGRAPHY

CORD "C"

STA. 14+00 → STA. 18+00

BASE LINE

IS

50' NORTH OF $\perp$

+50

L.T.

E

RT

+30 TANK
160+41 RD RD
0-9 26-3516 RD RD TANK
93-114 38-44 126RD
3RD
7FE
14+20 RD
38-75-107+74 RD
75

+50

TANK
114RD
3RD
6

15

RD
6+97 TANK
182+82
0-9RD
3FE
14

+50

RD
13-23

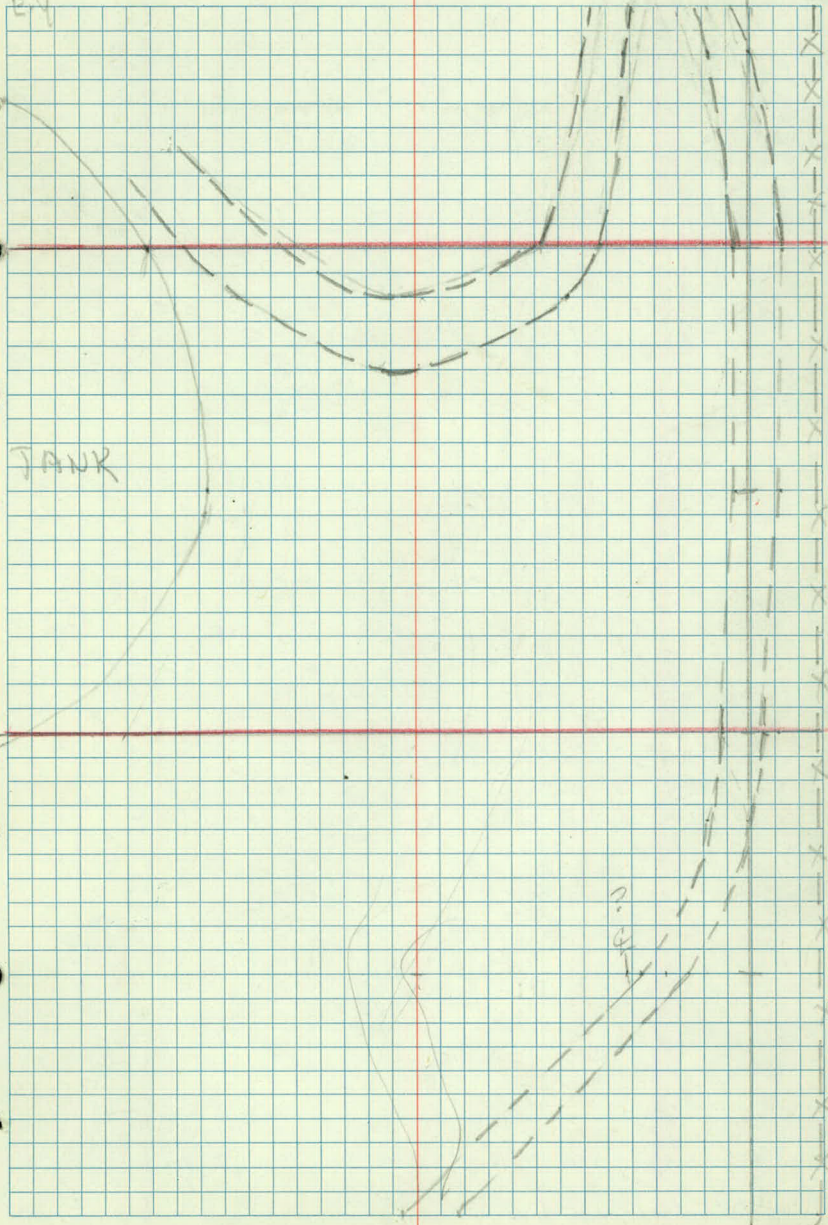
14+00

RD
61-73FE
14

WIS
RIC
BY

6-22-76
CL: 90°

2



LT

⊥

RT

18 RD
76-86

FE
145

+50 RD +51 R B W L T I E TO DRIVE (14+64)
54-65

17 RD
29-40

FE
145

+64 RD +64 ~~FE~~
11-21-29? 2

16 +50

W.S
R.L
E.Y

6-2-76
CL-90°

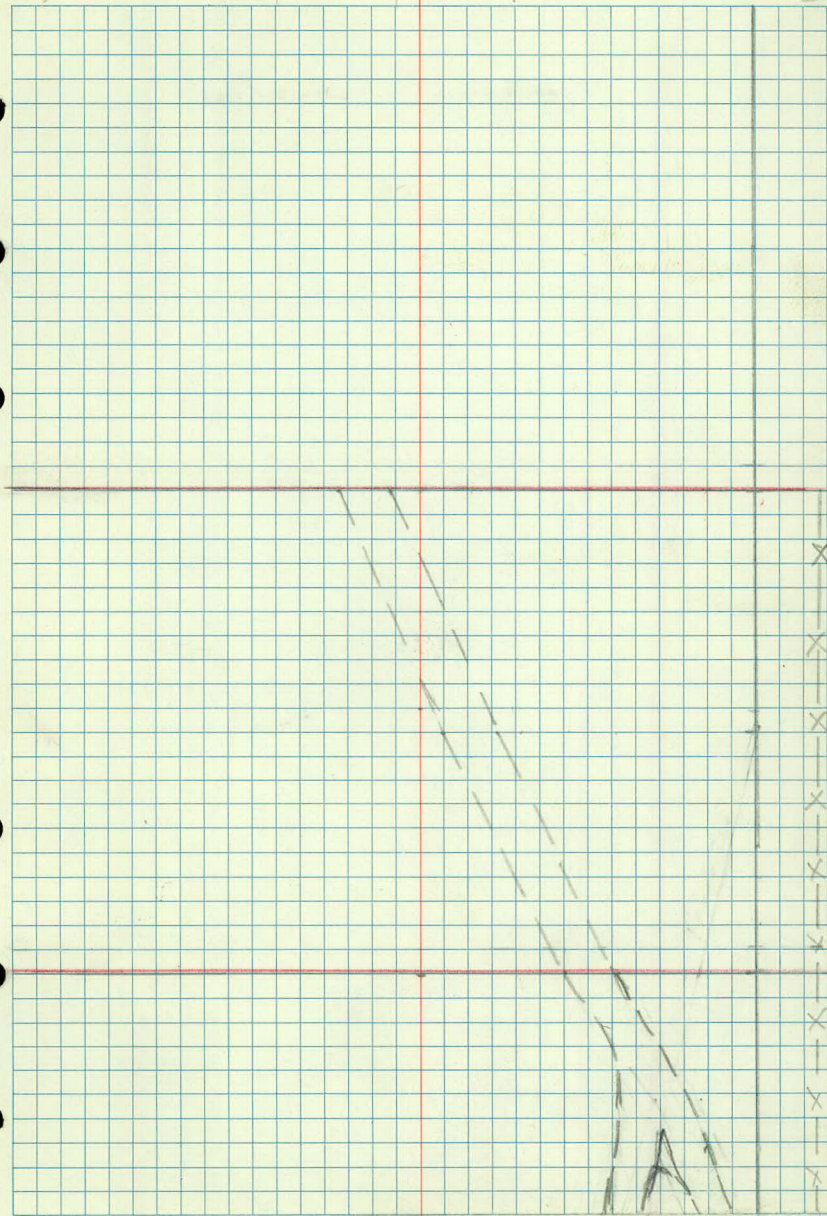
E

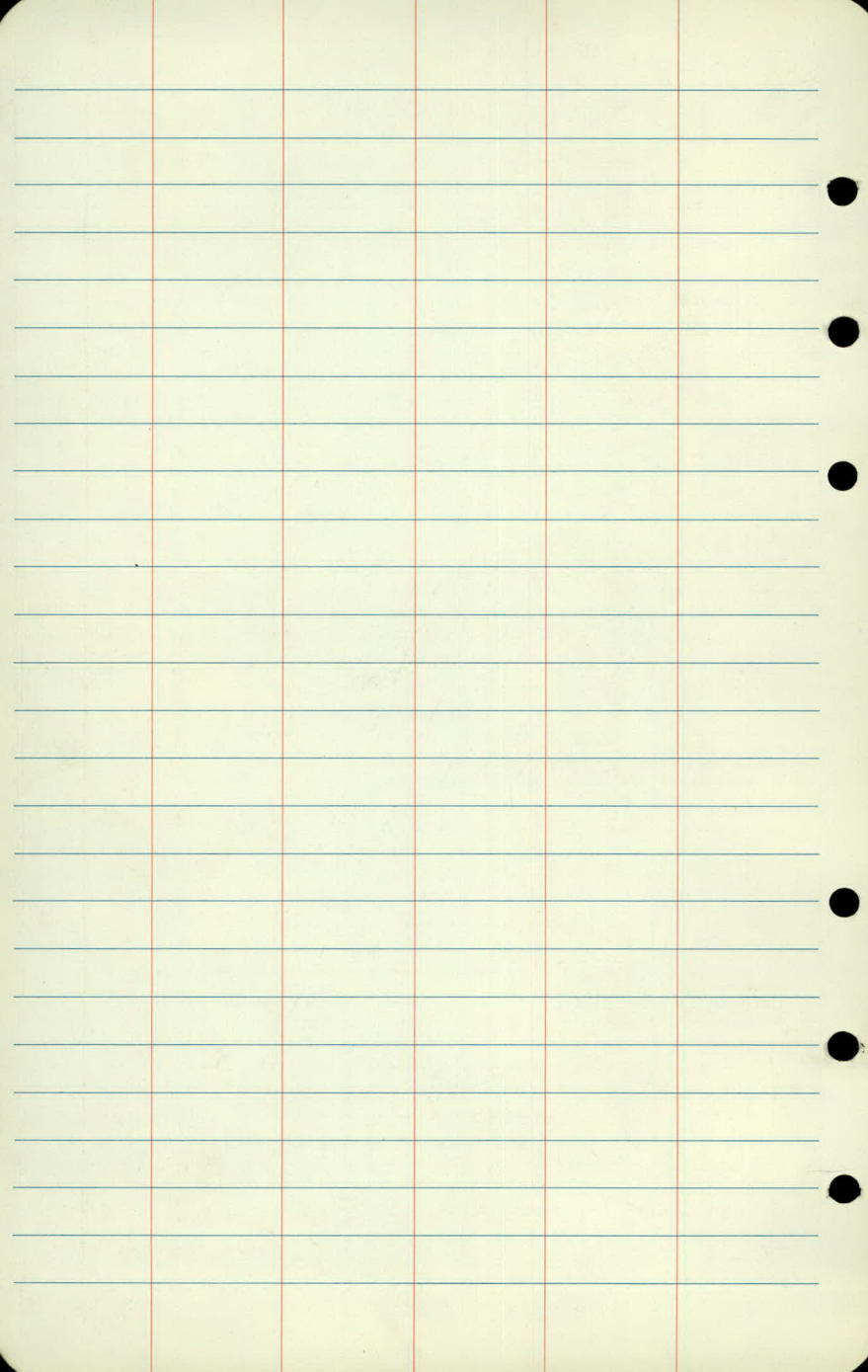
3

-100

-75

-50





W.S
B.W
E.Y
D.W

8-15-16
CLEVELAND 74°

1

ADDITIONAL
TOPOGRAPHY
(NEW GATE)
Amoco Oil Facility
COUNTY ROAD 1

CLEVELAND
TO
FREEWAY

2 PAGES

LT E RT

31+00

$$\begin{array}{r} \text{COR FE} \\ +15 \quad 41 \end{array}$$

$$\begin{array}{r} \text{NEW FE} \\ +93 \quad 108-120 \end{array}$$

$$\begin{array}{r} \text{COR FE} \quad \text{CONC} \\ +93 \quad 88 \quad 88 \end{array}$$

$$\begin{array}{r} \text{OLD GATE} \\ +93 \quad 88-108 \end{array} +$$

$$\begin{array}{r} \text{NEW FE} \\ +33 \quad 108-120 \end{array} \begin{array}{r} +22 \\ +53 \end{array}$$

$$\begin{array}{r} 31+24 \\ \uparrow \text{SLIDING GATE} \\ +93 \quad 120 \end{array}$$

$$\begin{array}{r} \text{SLIDING GATE} \\ 120 \end{array}$$

+50

$$\begin{array}{r} \text{COR FE} \quad \text{CONC} \\ +53 \quad 88 \quad 88 \end{array}$$

$$\begin{array}{r} \text{GATE} \\ 88-108 \end{array}$$

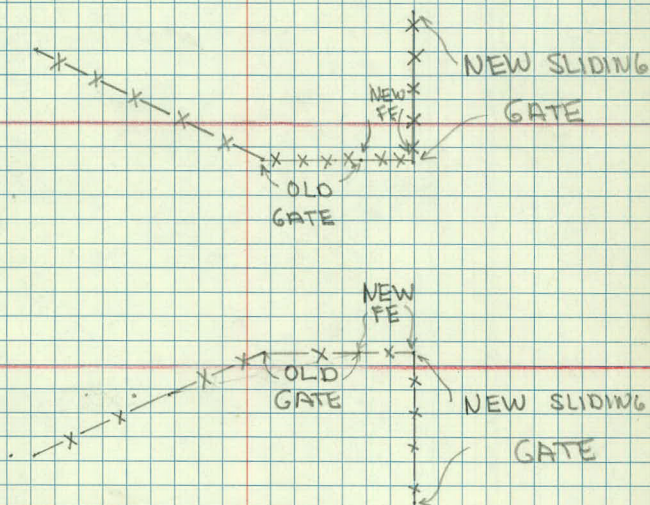
$$\begin{array}{r} \text{COR FE} \quad \text{CONC} \\ +32 \quad 41 \quad 36 \end{array}$$

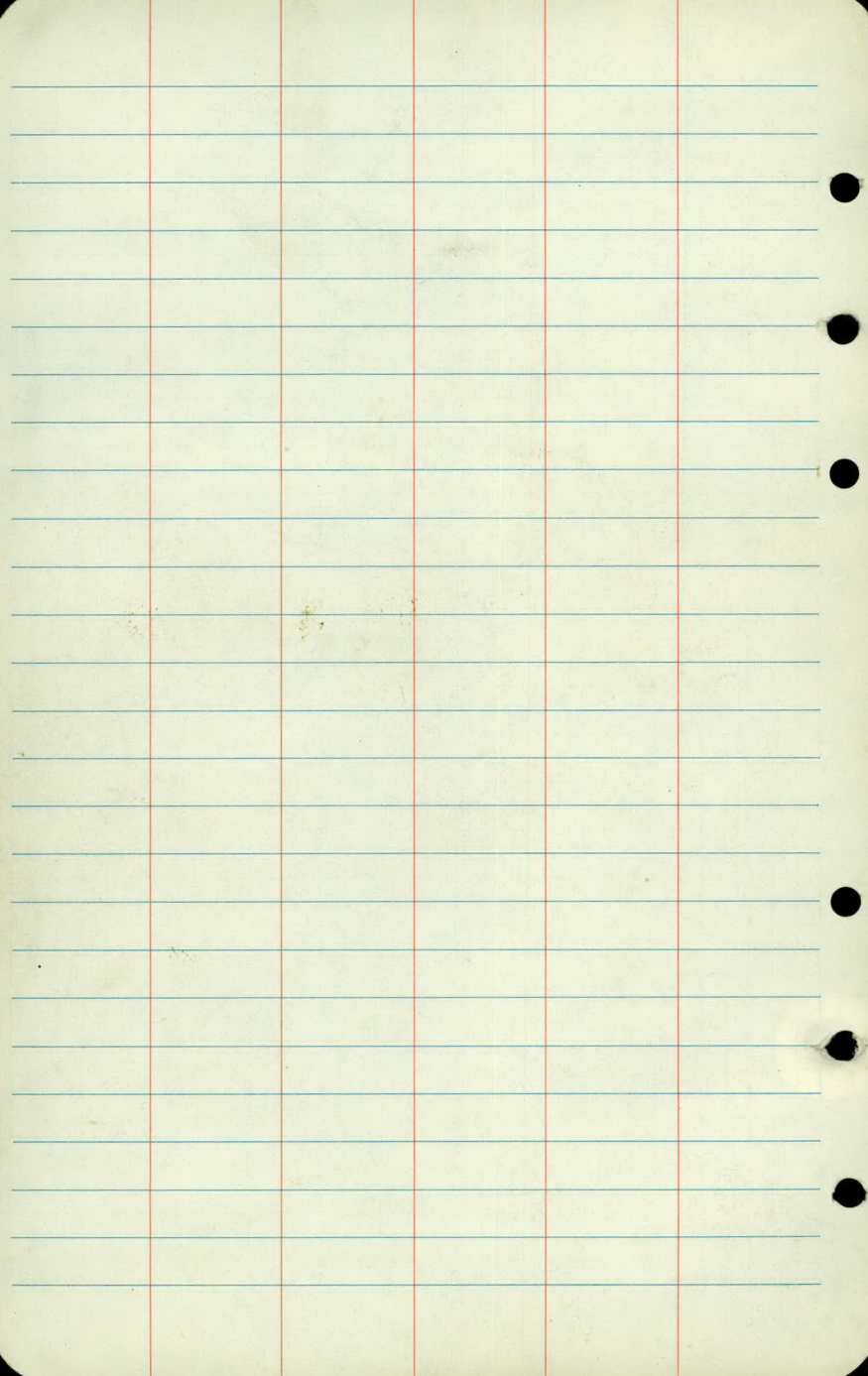
$$\begin{array}{r} \text{FE \& CONC} \\ +4469 \quad 52 \end{array}$$

30+00

WIS
L Biw
E.V
RW

8-13-76
CLEARING





W.S.
K.G.
B.W.
E.Y.

6-29-16
CLEAR 78°

CLEVELAND AVE ADDITIONAL TOPOGRAPHY

~~6~~

~~CROSS SECTIONS~~

900' SOUTH to
600' S. OF
COUNTY ROAD "C"

Co. Rd. "C" □ 15+00

6+00
Oakcrest

+50

LT

C

RT

+29 $\frac{SD}{58}$

✓
+36 $\frac{36" Elm}{55}$ ✓
+50 $\frac{40" Elm}{21}$ ✓
+24 $\frac{86-12 Curb}{51-69}$ ✓
+18 $\frac{Reg 86-18}{33-69}$ ✓
+10 $\frac{8" Mulled Rail Wall}{43}$ ✓
+35 $\frac{PP}{24}$ ✓
+22 $\frac{S.W. Coy. Road}{122}$ ✓
+31 $\frac{12" RCP}{41}$ ✓
+34 $\frac{WSO}{32}$ ✓
+21 $\frac{Lamp Post (25')}{64}$ ✓
+22 $\frac{24" RCP}{36}$ ✓
+14 $\frac{CR}{37}$ ✓

8

+99 $\frac{NE COR. FE}{34}$ ✓
+61 $\frac{24" Elm}{19}$ ✓
+99 $\frac{12" EMP}{29}$ ✓
+92 $\frac{CURB}{98-E}$ ✓
+89 $\frac{NOSE}{96}$ ✓
+84 $\frac{20" R.C.P.}{34}$ ✓
+77 $\frac{COR BLOC}{122-133}$ ✓
+75 $\frac{RD}{14}$ ✓
+92 $\frac{CURB}{33-68}$ ✓
+87 $\frac{POSE}{70+87}$ ✓
+84 $\frac{SW COR BLOC}{133}$ ✓
+88 $\frac{CURB}{98-117}$ ✓
+89 $\frac{CURB}{51-68}$ ✓
+77 $\frac{CURB}{51-117}$ ✓

+50

+130 $\frac{STP}{18}$

+13 $\frac{STP}{17}$

+28 $\frac{20" \frac{24" RCP}{32}}{32}$

7

FE 34 RD 10 RD 14

UGTC 28

+85 $\frac{STP}{18}$

+84 $\frac{CURB}{49}$ ✓
+84 $\frac{CURB}{94-115}$ ✓

+64 $\frac{BLOC}{122-135}$ ✓
+60 $\frac{RD}{15}$ ✓

+64 $\frac{86-12}{49}$ ✓
+64 $\frac{86-12}{94-115}$ ✓

+50

+58 $\frac{MK}{38}$ ✓
+40 $\frac{86-12 CURB}{49}$ ✓
+40 $\frac{SW COR BLOC}{135}$ ✓
UGTC 31

+10 $\frac{36" ELP}{14}$

+06 $\frac{SD}{69}$

6+00

FE (4' CHANNEL) RD 34 RD 10 PARKING LOT (CURB 86-12) 49 UGTC 35

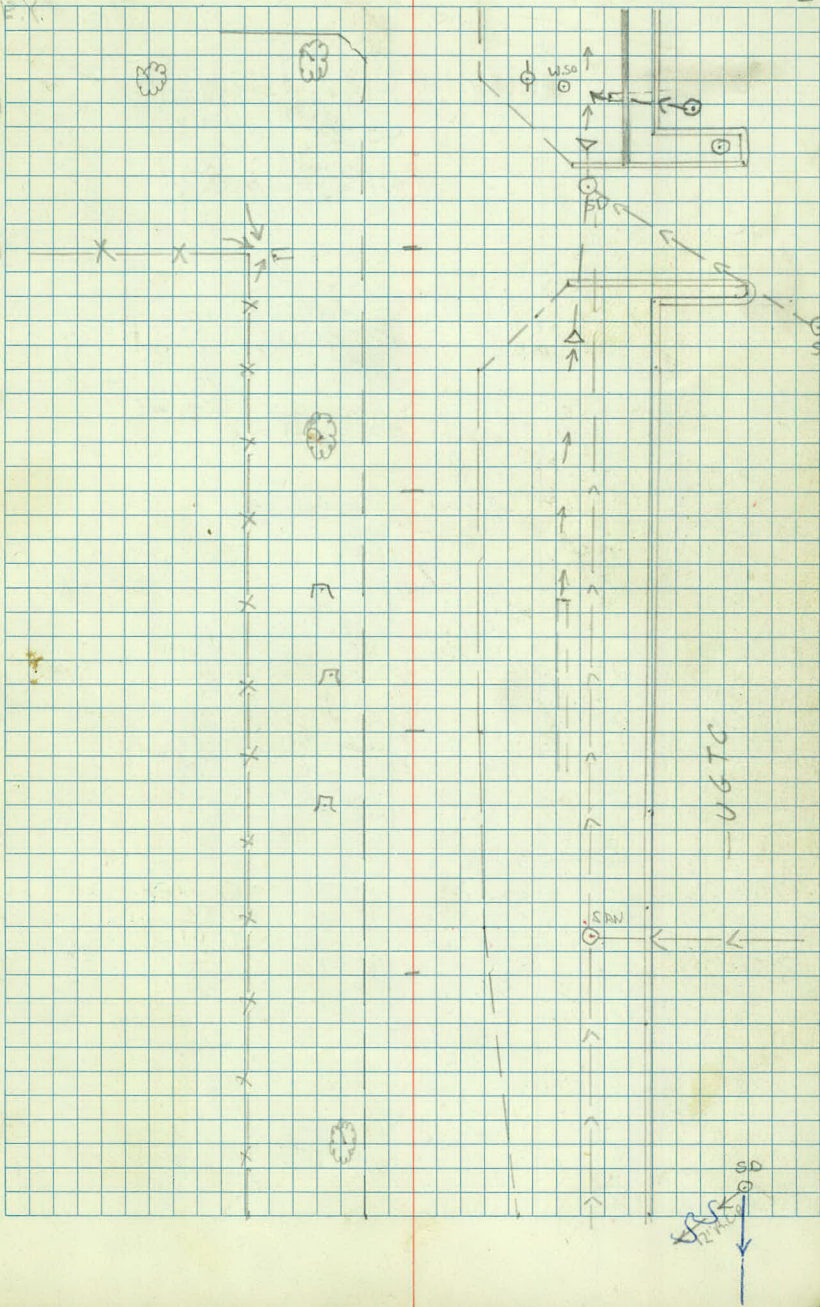
W.S.
R.G.
B.W.
E.Y.

LT

L

RTR. 6-29-76
CLEAR 75°

2



11

LT

E

RT

End Rad
14

+50

DIDN'T
CHANGE3'x2' CMP
+82 42Bag Rad
+71 49POR
+79 32S. Edge Ent.
+41 33-400PP
+29 243'x2' CMP
+31 44STP
+34 37N. Cor. Build
+09 56-2494' Cottonwood
+24 55

10 +00

RD
10Lot 1 ran
+93 336" Cottonwood
+96 5236" Elm
+87 66STP
+75 20PP
+70 28RD
+72 1432" Elm
+60 21N. Edge Ent.
+60 29-543'x2' CMP
+65 36Hyd.
+70 27

+50

S. Edge Ent.
+39 32-249SW Cor. Build
+39 249CB
+09 59conc. Wall 14'x4'
+21 3315" RCP
+21 363'x2' CMP
+34 36N. Edge Ent.
+17 5948" Elm
+13 21conc. Steps
+01 52-58cor. BG-12 curb
+27 77-100cor. Wood Wall
+31 47-200conc. Steps
+01 52-5812" RCP
+09 41N. Cor. Build
+10 122cor. BG-12 curb
+5 52-70RD
+10 10RD Build
+14 122wood Rail Wall
+44 44cor. Build
+86-12
52SE Cor. Ho.
+82 5844" Elm
+81 20cor. Build
+82 107-122Pine Bush
+67 29conc. Wall
+53 33-100Begin conc. Wall
+57 27(25)
ULBS Post
+64 48cor. Build
+65 107-122Twin 2" Pine
+59 32

8 +50

W.S
K.G
B.Y

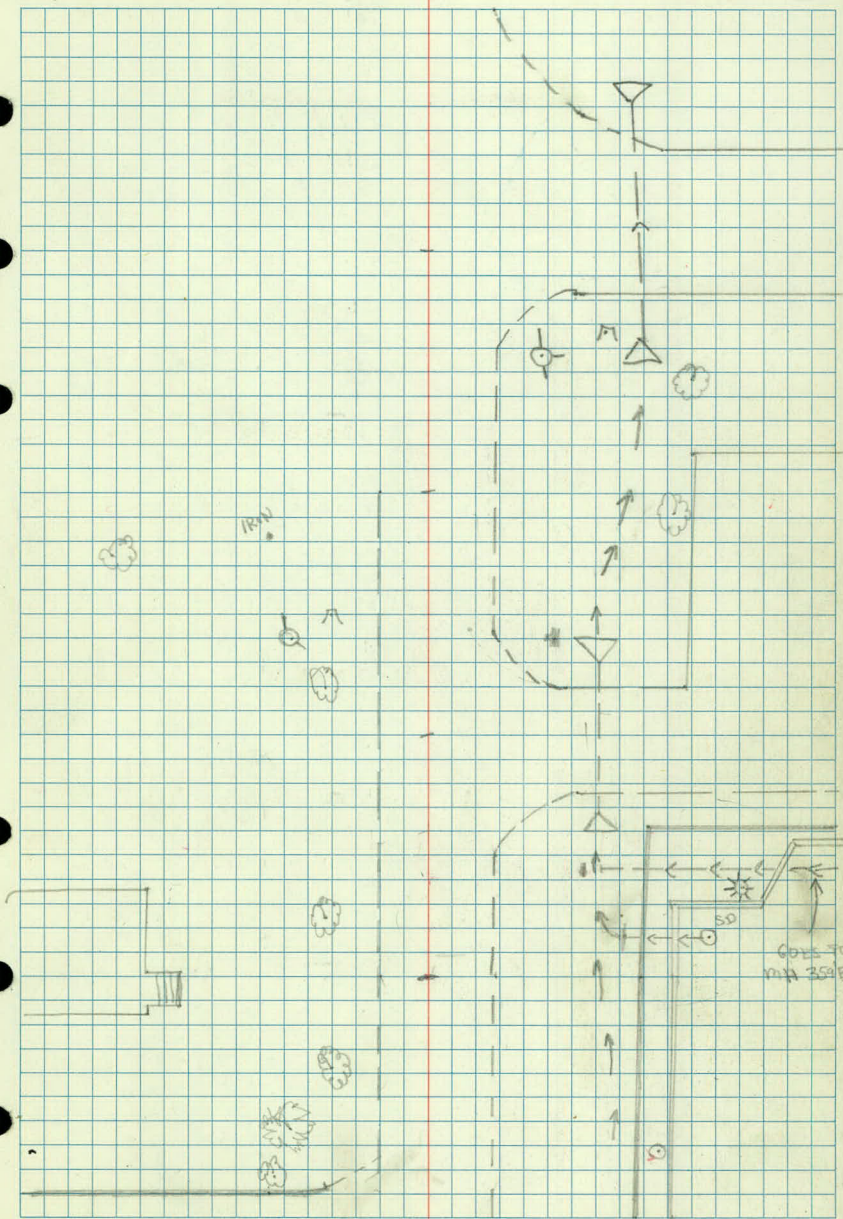
LT

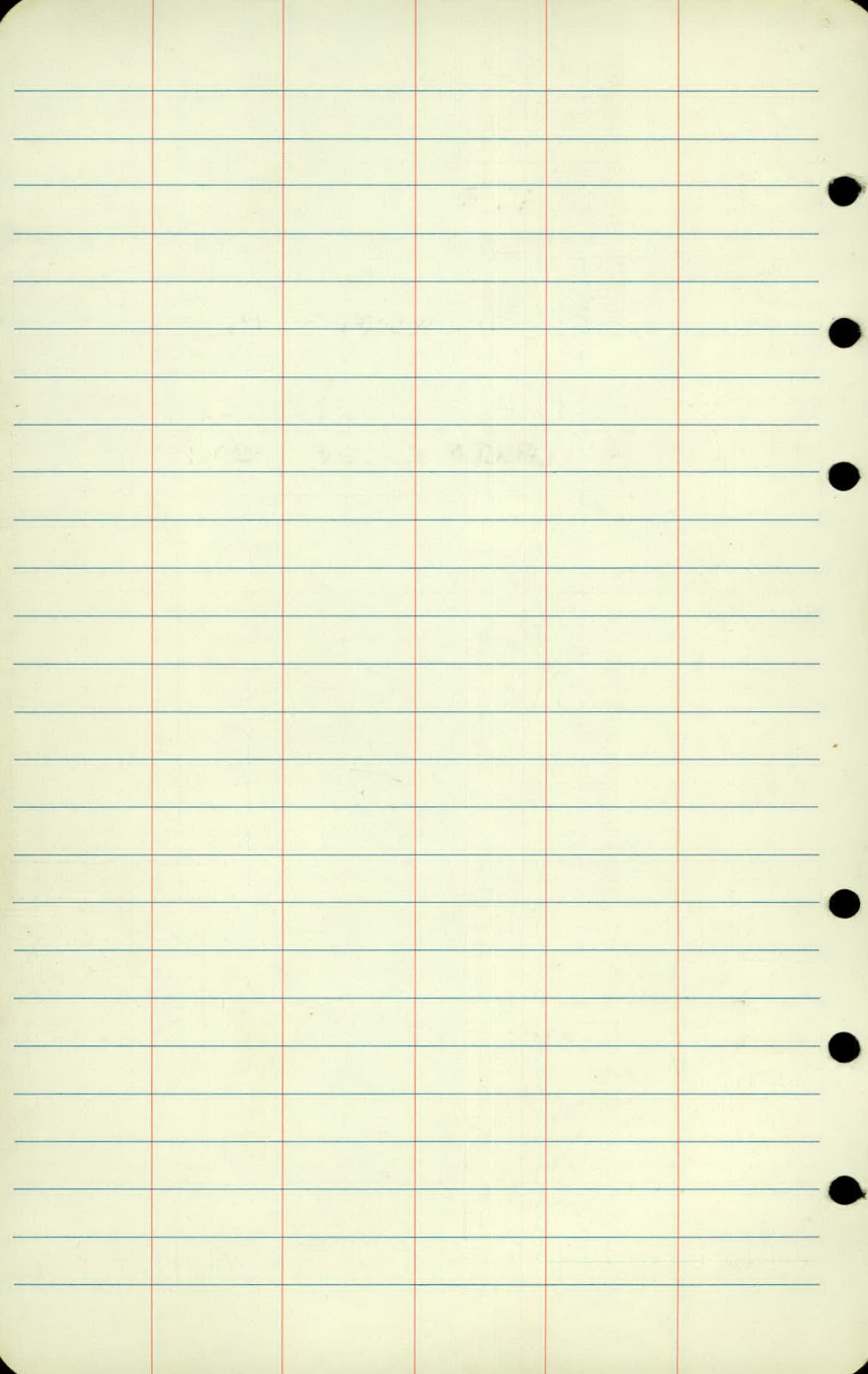
E

RT

6-30-76
clear: 80°
7-1-76

3





25°-chd-

NOV. 22, 1971

1

KG
DS
K
H

TOPOGRAPHY

CLEVELAND AVE

600' SOUTH & NORTH

OF COUNTY RD. "C"

11

Lt. J

Rd

Rd.

+93 N. End Cn. V. 17-11
+61 E Drive 14' 29'

+96 Cor Bldg 87'

+72 bag Conc. Wall
27 - back of Ho

+63 15" CMP 29'

+81 N. End Turn 182. m.p. 39'-41'

+63 12" Maple 39'

+63 N.E. Cor Ho. 77'

+55 E 30' Dr.

+29 10" ELM. 38'

+29 S.E. Cor Ho. 77'

+27 PP. 20'

+29 18" Twin Cn. V. CMP 41'-43'

+09 Cor. Bit Pklot 59'

10

Rd
14-11

+75 24" ELM. 22'

+71 ER. 10'

+69 Hyd 25'

+68 PP 31'

+54 Bev R. 33'

+60 POR. 20'

+59 30" ELM 23'

+56 N.E. Cn. V. 23'

+37 S. End 18" Arch Pipe C. V.P. 33'

+15 N.E. Cor Ho (25' wide) 12'

+27 PP. 52'

+37 ER. 22'

+12 30" ELM 24'

+21 18 RCP 31'

+21 POR 20'

9

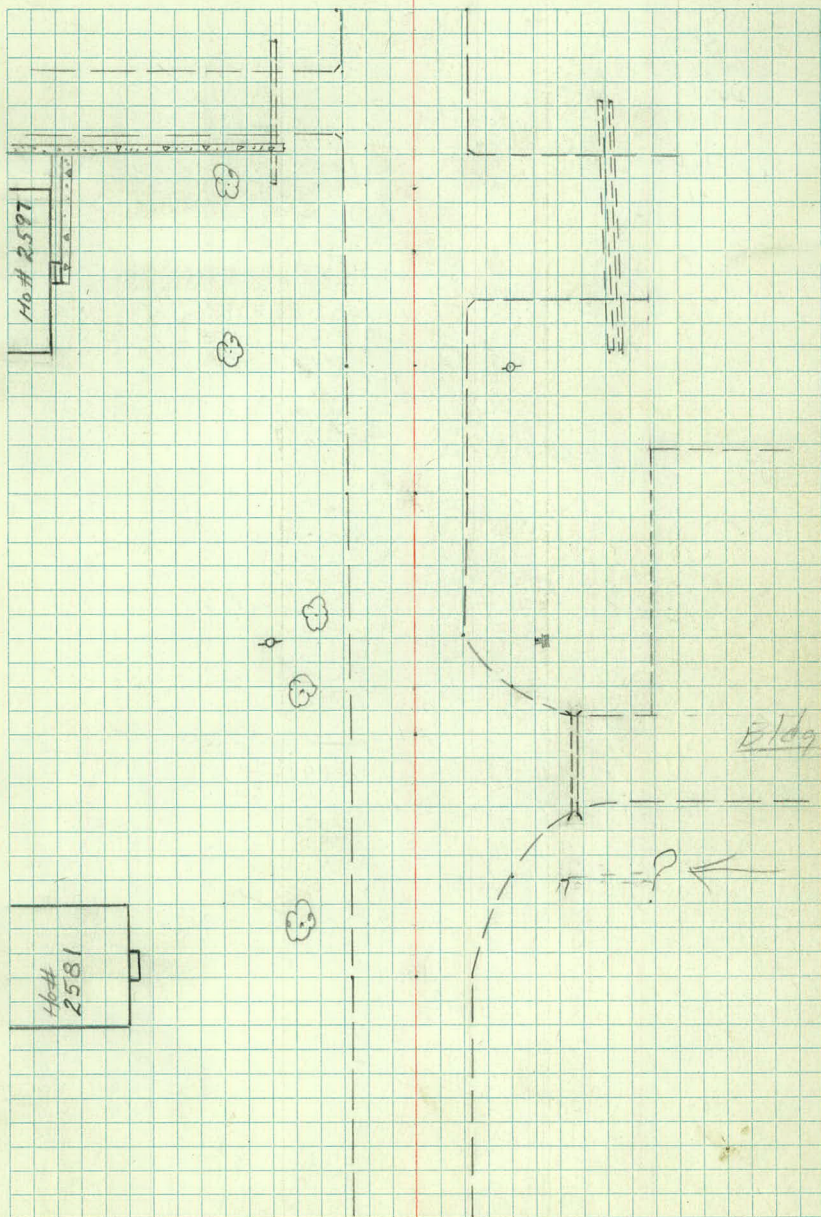
Rd
13-12

See also new notes LKF

8+50

NOV. 22, 1971

2



+46 U.S.M. Box
28

+48 PP
30

+48 C. Blg
84

+49 Cor. Blt
30

+13 GP
20

+13 GP
24

+09 Sig. box
21

+09 GP
25

+12 GP
29

36
30" R.P.
+18
24

+21 MH
24

13

Road
13-11

ERR ✓

+96 36
30" R.C.P.

ROSEVILLE BEACH

+85 21
Sig. box

+76 Sig. box
36

(24" x 60")
(30" x 20")
+76 Sig. box
40

+77 30
30" R.C.P.

+83 20
Sig. box

+62 36
M.H. (sewer)

BRK ✓ +67 PP
33

+58 E. Rod
15

+46 Cor. Blg
80

+45 vent pipe
25

+44 PP
31

+44 Hyd.
22

+44 W.S.O
21

+39 P.O.R
26

+26 Bas. P.
68

+32 P.O.R
38

12

+100 E. Rod
62

Road
13-11

+81 P.O.R
23

+91 P.O.R
32

+94 Cor. Blg
70

+59 24" E.M.
41

+64 3. Rod
19

+53 47
5sm. Willow

+47 39
14" E.M.

+50 38
5" E.M.

+40 50
15" Willow

+41 46
6" Willow

+17 PP
29

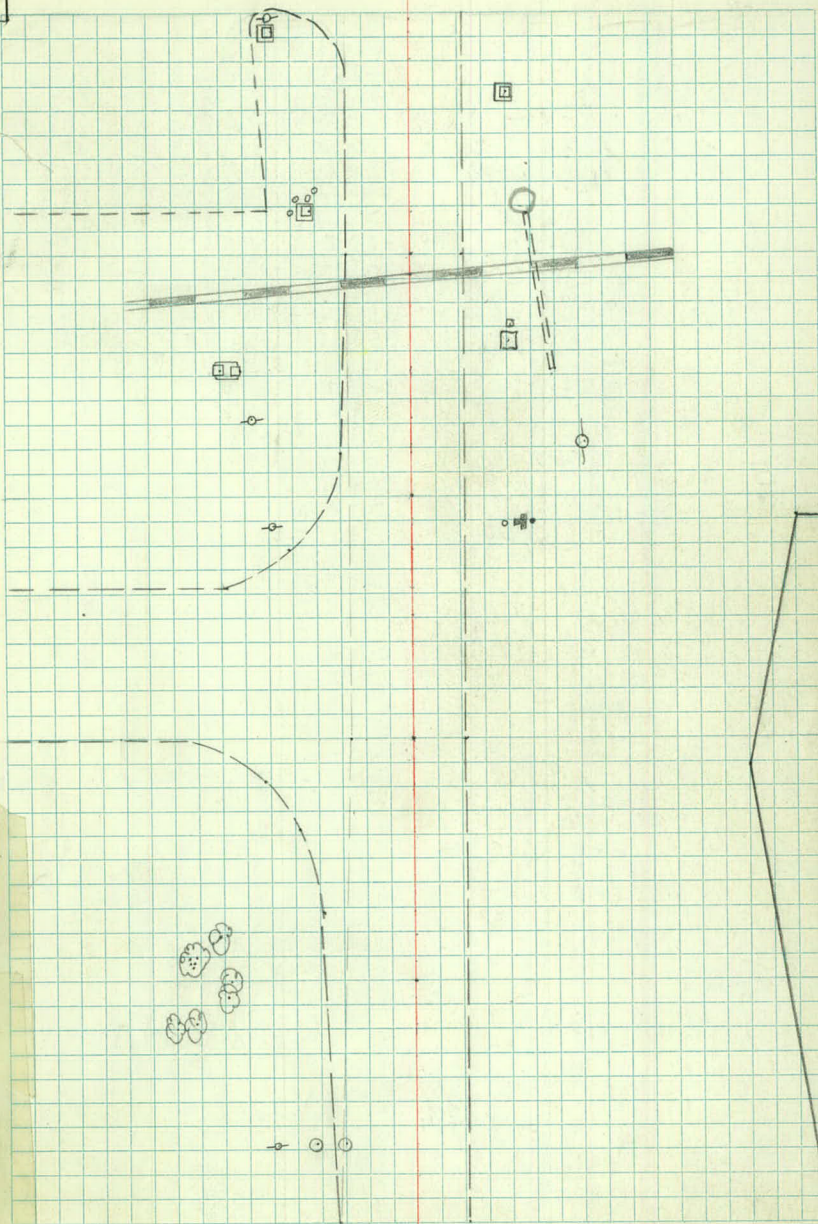
+17 MH (tele)
15

+17 Tele M.H.
21

Road
17-11

NOV. 22, 1971

3



16

$$+100 \frac{ER}{23} + 100 \frac{C.F. Road}{42 \cdot 23}$$

$$+99 \frac{B.R}{23}$$

$$+90 \frac{24" MP}{S.E. 99'}$$

$$+162 \frac{Tele MH}{23}$$

$$+56 \frac{MH (Tele)}{16}$$

$$+42 \frac{C.F.}{102'}$$

$$+42 \frac{POK}{47}$$

$$+30 \frac{B.R.}{54}$$

$$+38 \frac{MH}{51}$$

$$+60 \frac{POK}{31} + 100 \frac{24" RCP}{49}$$

$$+50 \frac{MH}{22}$$

$$+50 \frac{MH}{38}$$

$$+30 \frac{ER}{95}$$

$$+49 \frac{POK}{36}$$

15

$$+100 \frac{End 9' Mod.}{59}$$

$$+100 \frac{mont.}{59}$$

$$+100 \frac{End 4' Mod.}{59}$$

$$+76 \frac{Conc.}{E}$$

$$+176 \frac{MH}{50}$$

$$+136 \frac{T.M.H.}{26} + 66 \frac{T.M.H.}{19}$$

$$+152 \frac{MH (Tele)}{26} + 160 \frac{ER Tele MH}{53' \cdot 26}$$

$$+66 \frac{ER}{52}$$

$$+58 \frac{24" RCP}{48}$$

$$+52 \frac{POK}{26}$$

$$+42 \frac{MH (water)}{49'}$$

$$+37 \frac{POK}{18}$$

$$+26 \frac{C.Conc.}{59'}$$

$$+32 \frac{PO}{29'}$$

$$+48 \frac{PO.R.}{23}$$

$$+15 \frac{PO}{24'}$$

$$+23 \frac{PO R.}{15'}$$

$$+23 \frac{Sign}{38'}$$

$$+11 \frac{C.Conc}{40'}$$

$$+11 \frac{End 15.}{88}$$

$$+06 \frac{C.Conc}{80}$$

$$+08 \frac{C.Conc}{72'}$$

14

$$+93 \frac{C.Conc.}{54}$$

$$+13 \frac{Road}{12}$$

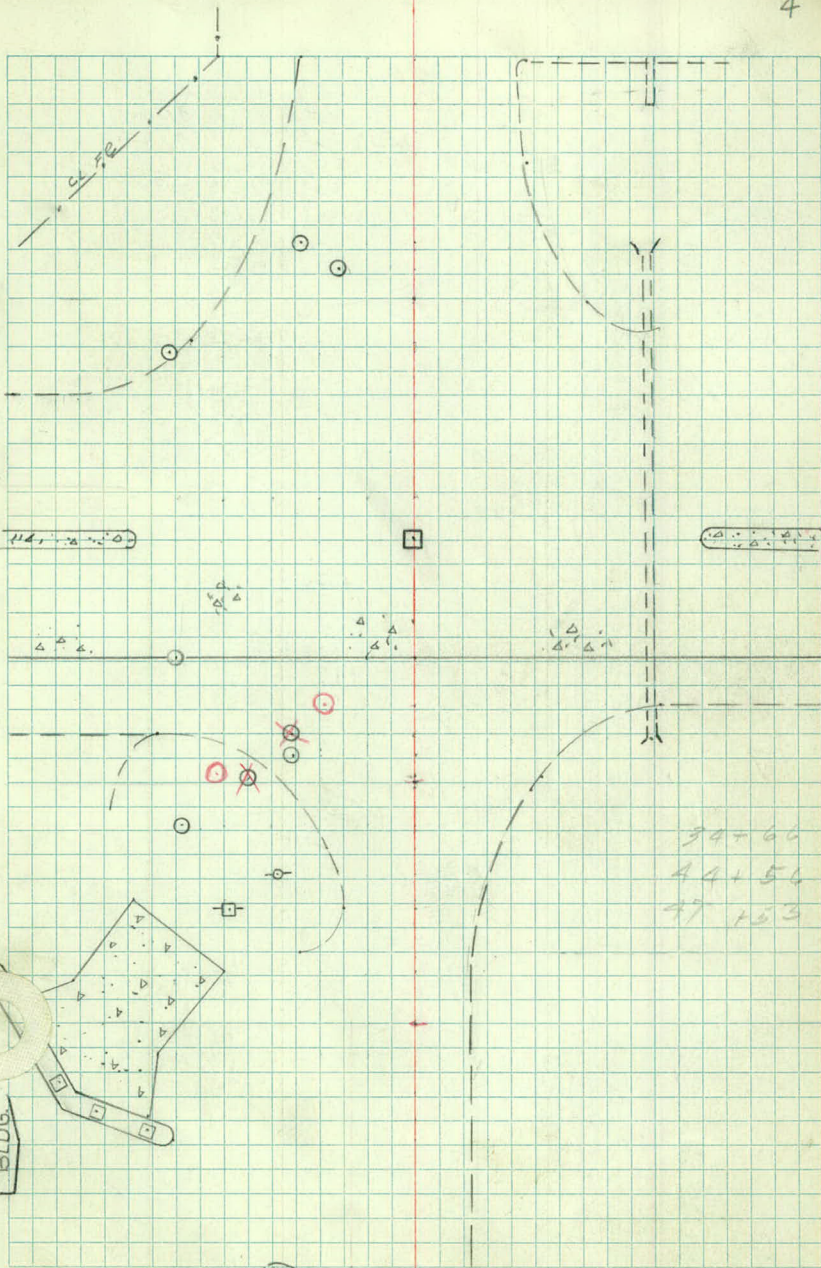
$$+81 \frac{C.Conc Dr.}{56}$$

$$+86 \frac{Bend in ls.}{71'}$$

$$+77 \frac{End 15. (7' wide)}{51}$$

$$+65 \frac{C.Bldg}{84'}$$

$$+77 \frac{Car Bldg}{83}$$



34 + 66
44 + 56
47 + 53

BLDG.

LT

E

RT

$$+148 \frac{B.R.}{12} + 66 \frac{POR}{30} + 66 \frac{24' CMP}{41}$$

$$+109 \frac{PP}{27}$$

$$+108 \frac{C.F.E.}{42}$$

$$Road \checkmark \\ 12 \ 12$$

$$+147 \frac{Edge Rd.}{13}$$

$$+35 \frac{24' CMP}{43}$$

$$+17 \frac{29' Drive}{44}$$

17

$$+100 \frac{Fe}{42}$$

$$Road \checkmark \\ 16 \ 14 + 94 \frac{24' CMP}{44}$$

$$+32 \frac{PR}{28}$$

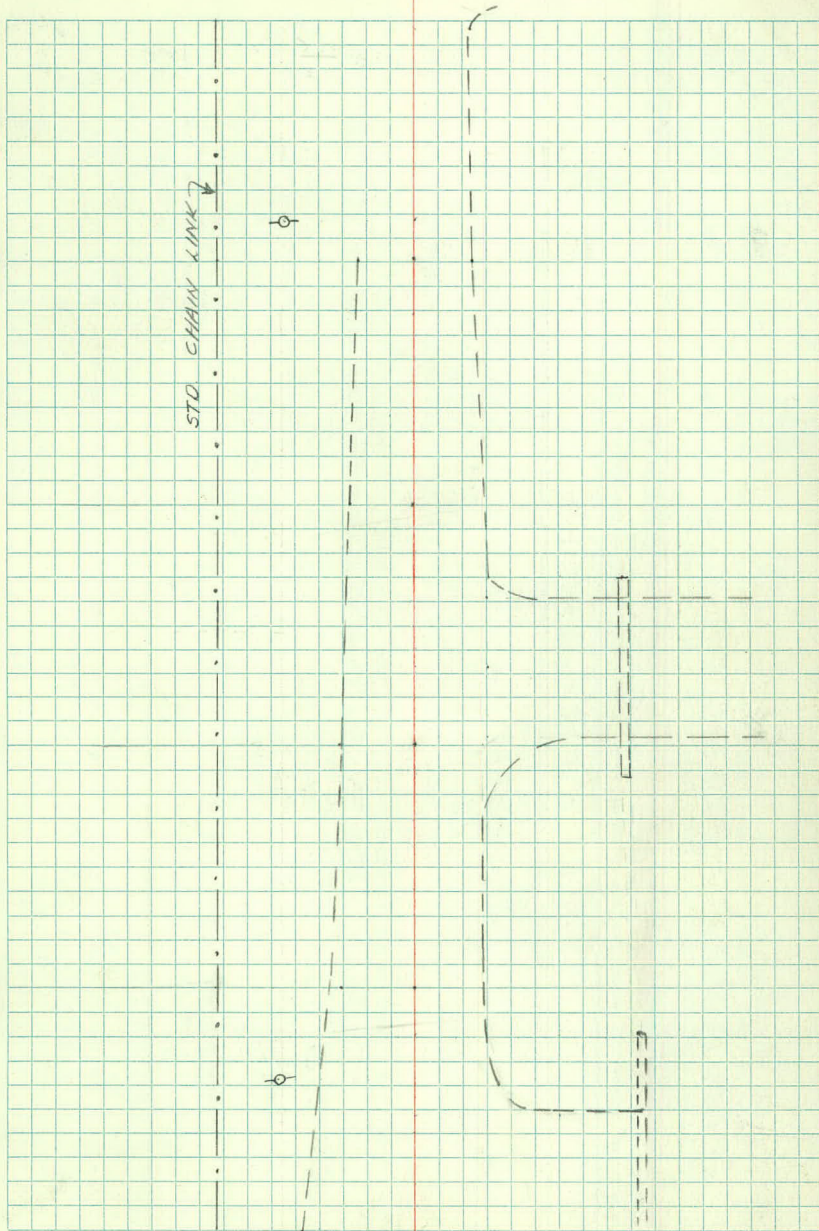
$$+41 \frac{24' CMP}{46} + 27 \frac{ER}{30}$$

16

$$Road \\ 23 \ 25$$

Nov. 22, 1971

5



21

$+16 \frac{5.0}{97}$ ✓
 $+72 \frac{36" \text{ Arch Pipe}}{77}$ ✓
 $+76 \frac{P.O.R.}{30}$ ✓
 $+56 \frac{12' \text{ C.M.P.}}{67}$ ✓
 $+76 \frac{E.R.}{84}$ ✓
 $+93 \frac{24' \text{ C.M.P. Culv.}}{38}$ ✓
 $+00 \frac{\text{Acc Life}}{25}$ ✓

$+46 \frac{\text{End F.C.}}{42}$ ✓
 $+40 \frac{P.O.R.}{17}$ ✓
 $+19 \frac{B.R.}{12}$ ✓
 $+44 \frac{M.H.}{30}$ ✓
 $+37 \frac{H.Y.D.}{49}$ ✓
 $+37 \frac{W.S.O.}{51}$ ✓

20

$+92 \frac{P.O.R.}{28}$ ✓
 $\text{Road } 12/12$ ✓

$+15 \frac{P.O.R.}{38}$ ✓
 $+32 \frac{E.R.}{12}$ ✓
 $+24 \frac{24' \text{ C.M.P.}}{42}$ ✓
 $+04 \frac{B.R.}{62}$ ✓

19

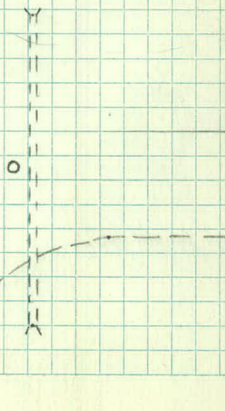
$+00 \frac{C.I.F.C.}{42}$ ✓
 $\text{Road } 12/12$ ✓

$+94 \frac{M.H. (\text{Sewer})}{37}$ ✓
 $+78 \frac{E.R.V.}{57}$ ✓
 $+66 \frac{P.O.R.}{30}$ ✓
 $+60 \frac{24' \text{ C.M.P.}}{41}$ ✓

NOV 22, 1971

6

0



5

7

J.A.
L.P.D
D.S.

DEC 10, 1976

RR SIGNAL LOCATION
ON CLEVELAND AVE 200± SO.
OF Co Rd "C"

2 PAGES

15

0+00

14

13+09

1+91

RR SIGNAL
20'

12+96.5

2+03.5

RR

12+82

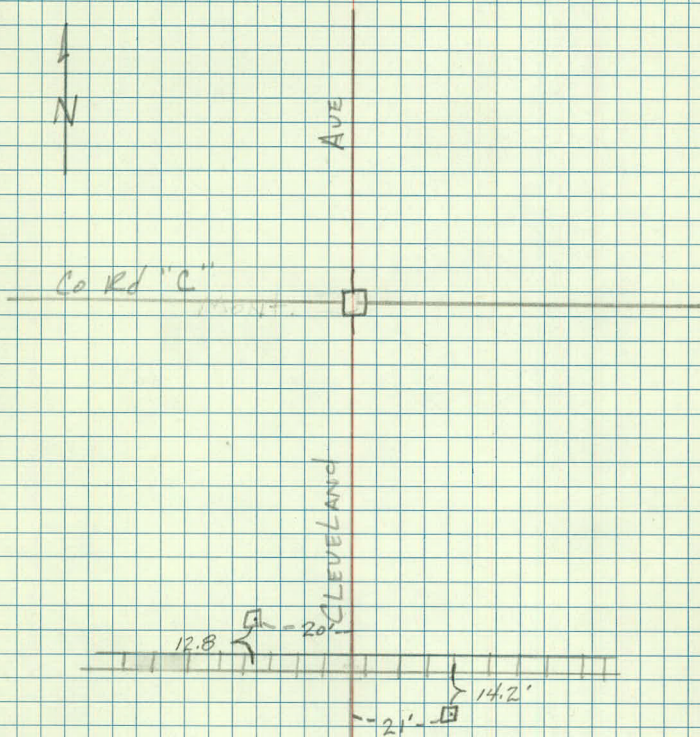
2+18

RR SIGNAL
21'

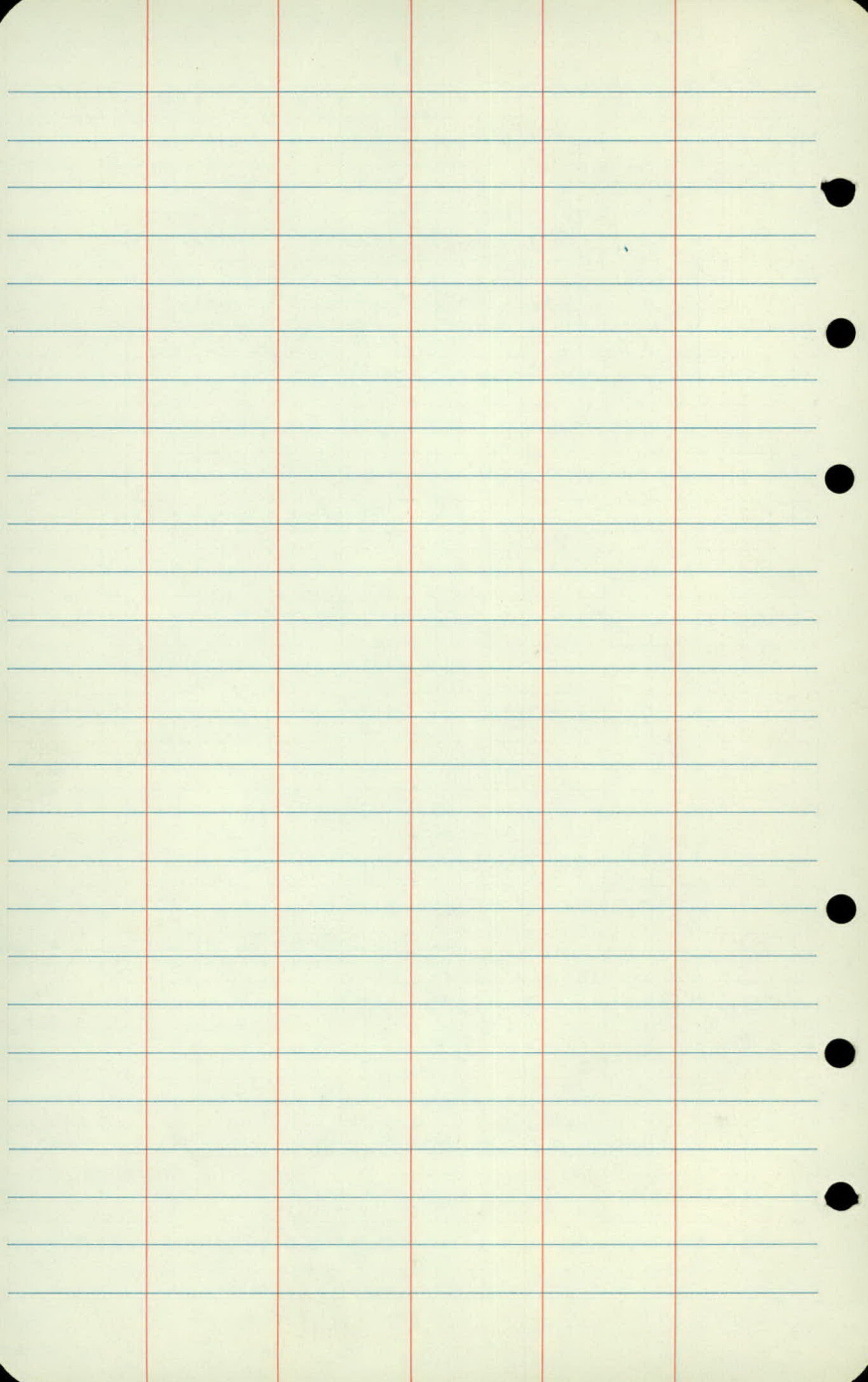
J.A.
L.P.D.
D.S.

DEC 10, 1976
CLR 00'

2



Signals Checked to be in
the same Location
as on Nov. 22, 1971
Jk



JH
LPD
ML
GA
BW.

12-19-77
CLR 150

1

SIGNAL EQUIPMENT

LOCATION AT INTERSECTION

Co Rd "C" & CLEVELAND

PAGES 2

Section
Line?
&
Cleveland Ave

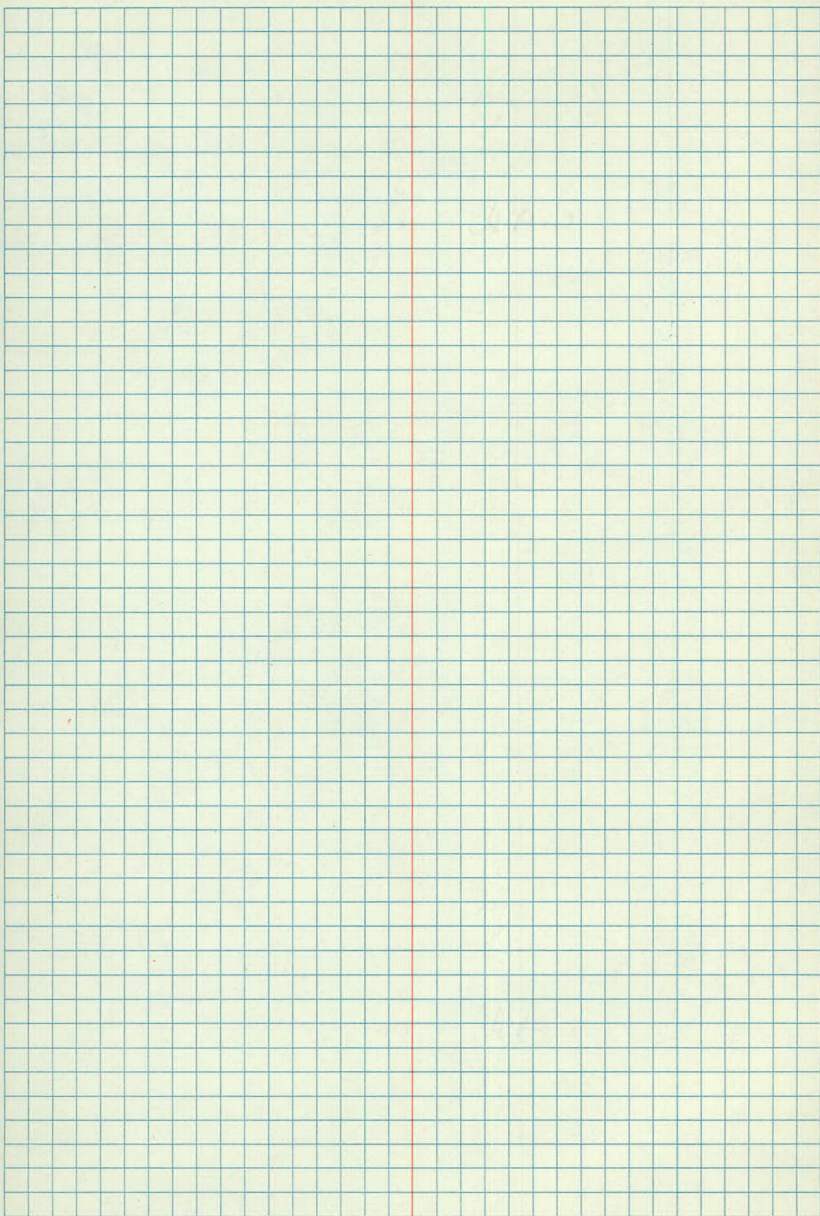
5+00

+50 +54 $\frac{HH}{45}$ +55 $\frac{HH}{45}$ +60 $\frac{Signal}{69}$
+44 $\frac{HH}{42}$

+34 $\frac{Curve}{40}$ +39 $\frac{Signal}{32}$
+30 $\frac{SOP}{29}$

4+00

= 'S Co Rd "C"



11-16-77

11-18-77

JA
LPD
DS

DAN GREEN

633-1555 Dist office

636-2733 Warehouse

For 62-623-14

WILLIAMS Bros. Pipe Location

And Ground cover from WILLIAMS

Track to Long Lake Rd

Along Co. Rd "C"

Baseline is 50' S. of

S. line of 5-29-23

27+00

28+00

+50

29+00

+50

30+00

31+00

31+50

32+00

32

Lt

BASE
LINE

Rt

Top No. Distance from Base Line

Bottom No. is Amount of Ground COVER

4.8'

30"

5.4'

30"

0.6

32"

2

21"

5.1

35"

5.9

33"

2

20"

0.8

0.8

37"

0.2

5.6'

36"

0.2'

45"

6.3'

32"

2.5'

38"

1.0'

41"

5.6'

33"

3.0

33"

0.8'

38"

5.6'

38"

2.7

24"

0.7

30"

32 + 50

33

+ 50

34

+ 50

35

+ 50

36

+ 50

37

+ 50

Lt.

BASE
LINE

Rt.

6.2"

2.5

0.5

31"

24"

31"

6.2'

2.4

1.1

31"

24"

32"

5.6'

1.4

1.9

34"

15"

21"

5.5'

0.33'

2.9'

32"

14"

23"

5.8'

0.8

4.0'

47"

14"

24"

5.8'

1.8

39"

20"

7.4'

1.7'

1.7'

38"

17"

8.2

4.0'

38"

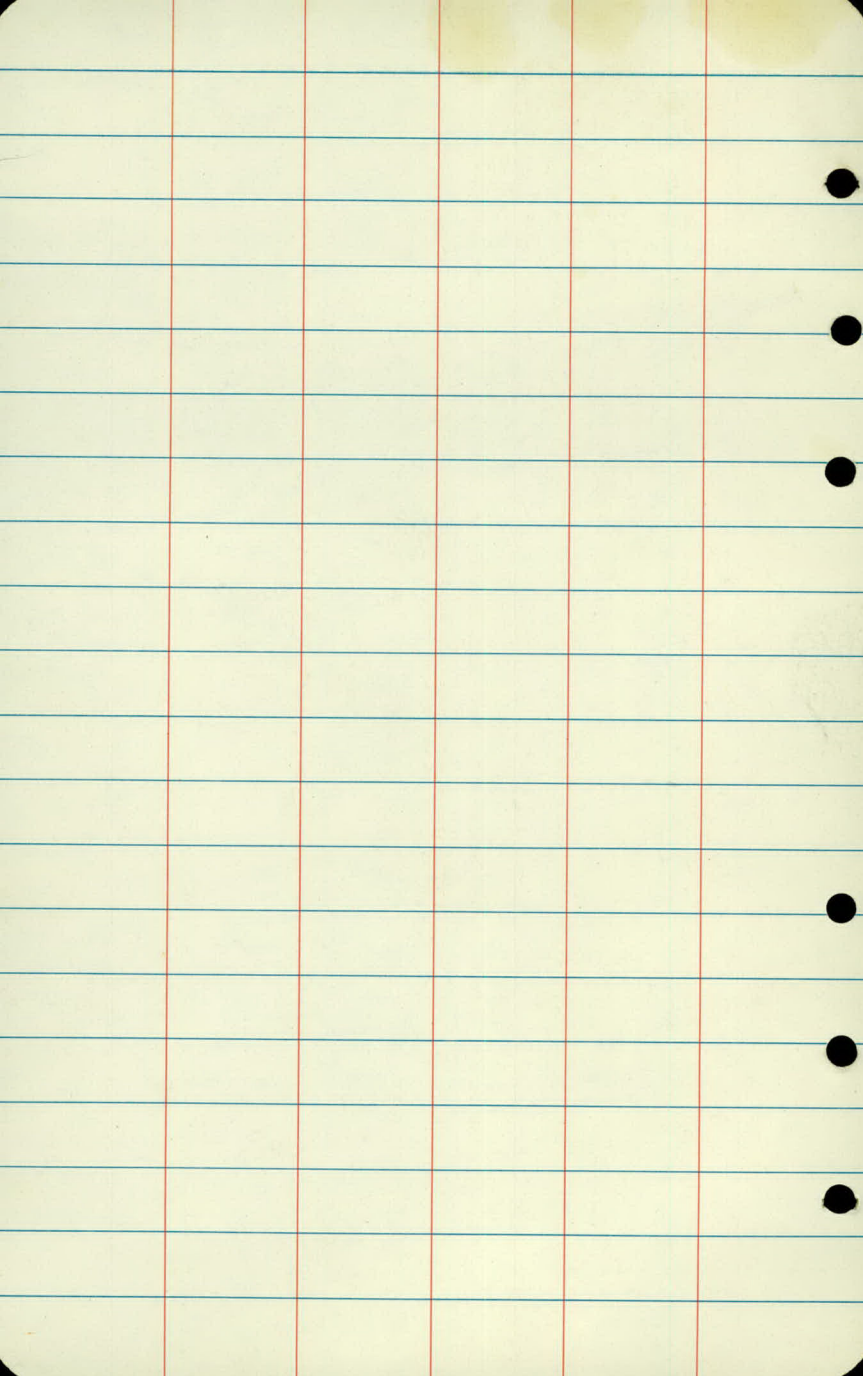
33"

4.5'

52"

9.5'

56"



CLEVELAND STRUCTURAL DATA TYPE

STORM	☒	ELECTRIC		WATER	
SANITARY		TELEPHONE		OTHER	
STATION	RIGHT	LEFT	SIZE	9 INCH CASTING	
6+06	☒ 69'		9		

TYPE OF CONST.	COMMENTS
BLOCK	1' high precast bottom
BRICK	
SECTIONAL	

ADJUSTING RINGS	TYPE	NO.	DEPTH	COMMENTS
BLOCK				
BRICK				
CONC. RINGS	☒	2	.4'	

DEPTH FROM BOTTOM OF M.H. TO TOP OF CASTING	ELEV.
3.15'	
DISTANCE FROM HIGHEST FLOW LINE TO TOP OF CASTING	
ETC.	
INV.	

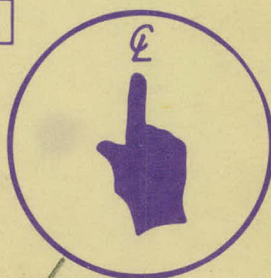
SIZES OF ALL
PIPES AND
DIRECTION OF
FLOW

DESIGN

ELEVATION - TOP
FINAL ELEVATION
DIFFERENCES

ADJUST

RECONSTRUCT



12" RCP

CLEVELAND

STRUCTURAL DATA TYPE

STORM

ELECTRIC

WATER

SANITARY

TELEPHONE

OTHER

STATION

RIGHT

LEFT

SIZE

6+58

38'

7

INCH CASTING

TYPE OF CONST.

COMMENTS

BLOCK

BRICK

SECTIONAL

Concentric

3.5 bottom section

3.0 middle section

4.5

ADJUSTING RINGS

TYPE

NO.

DEPTH

COMMENTS

BLOCK

BRICK

CONC. RINGS

17

3.1'

DEPTH FROM
BOTTOM OF M.H.

ELEV.

TO TOP OF CASTING

13.8'

DISTANCE
FROM HIGHEST
FLOW LINE TO
TOP OF CASTING

13.2

ETC.

INV.

SIZES OF ALL
PIPES AND
DIRECTION OF
FLOW

DESIGN

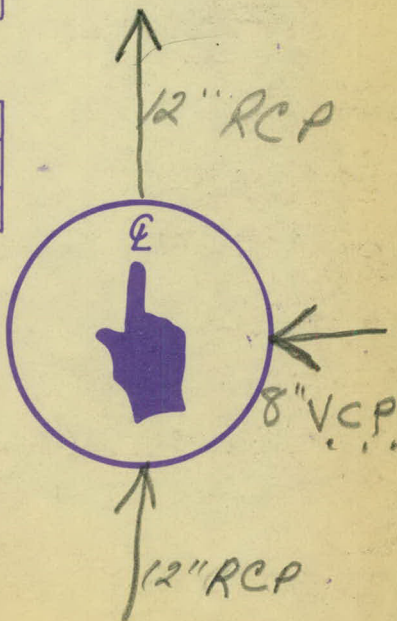
ELEVATION - TOP

FINAL ELEVATION

DIFFERENCES

ADJUST

RECONSTRUCT



CLEVELAND

STRUCTURAL DATA TYPE

142

STORM

ELECTRIC

WATER

SANITARY

TELEPHONE

OTHER

STATION

RIGHT

LEFT

SIZE

7484

75'

9

INCH CASTING

TYPE OF CONST.

COMMENTS

BLOCK

Concentric

BRICK

3' section

SECTIONAL

ADJUSTING RINGS

TYPE

NO.

DEPTH

COMMENTS

BLOCK

BRICK

CONC. RINGS

In
ELEV.DEPTH FROM
BOTTOM OF M.H.

TO TOP OF CASTING

4.0'

DISTANCE
FROM HIGHEST
FLOW LINE TO
TOP OF CASTING

ETC.

INV.

12" RCP

SIZES OF ALL
PIPES AND
DIRECTION OF
FLOW

DESIGN

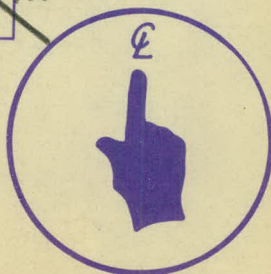
ELEVATION - TOP

FINAL ELEVATION

DIFFERENCES

ADJUST

RECONSTRUCT



CLEVELAND STRUCTURAL DATA TYPE

STORM	☒	ELECTRIC	☐	WATER	☐
SANITARY	☐	TELEPHONE	☐	OTHER	☐
STATION	RIGHT	LEFT	SIZE	INCH CASTING	
8+14	37'	-	7		

TYPE OF CONST.	COMMENTS
BLOCK	Built into 30" RCP with conc blocks
BRICK	
SECTIONAL	

ADJUSTING RINGS	TYPE	NO.	DEPTH	COMMENTS
BLOCK				
BRICK				
CONC. RINGS				

DEPTH FROM BOTTOM OF M.H TO TOP OF CASTING	ELEV.	
DISTANCE FROM HIGHEST FLOW LINE TO TOP OF CASTING	3.4' 929.44 L&F	
ETC.	2.4'	
INV.		
SIZES OF ALL PIPES AND DIRECTION OF FLOW		
DESIGN		
ELEVATION - TOP	932.34 L&F	
FINAL ELEVATION		
DIFFERENCES		
ADJUST		
RECONSTRUCT		

61602000

STRUCTURAL DATA

140

TYPE

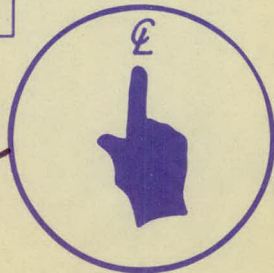
STORM	☒	ELECTRIC		WATER	
SANITARY		TELEPHONE		OTHER	
STATION	RIGHT	LEFT	SIZE		
8+29	58		7	INCH CASTING	

TYPE OF CONST.	COMMENTS				
BLOCK					
BRICK					
SECTIONAL	☒				

ADJUSTING RINGS	TYPE	NO.	DEPTH	COMMENTS
BLOCK				
BRICK				
CONC. RINGS				

DEPTH FROM BOTTOM OF M.H. TO TOP OF CASTING	ELEV.
2.6'	
DISTANCE FROM HIGHEST FLOW LINE TO TOP OF CASTING	
ETC.	
INV.	

SIZES OF ALL PIPES AND DIRECTION OF FLOW	12" RCP
---	---------



DESIGN	
ELEVATION - TOP	
FINAL ELEVATION	
DIFFERENCES	

ADJUST	
RECONSTRUCT	

STRUCTURAL DATA TYPE

STORM

ELECTRIC

WATER

SANITARY

TELEPHONE

OTHER

STATION

RIGHT

LEFT

SIZE

9+09

59'

9

INCH CASTING

TYPE OF CONST.

COMMENTS

BLOCK

BRICK

SECTIONAL

2' precast

ADJUSTING RINGS

TYPE

NO.

DEPTH

COMMENTS

BLOCK

BRICK

CONC. RINGS

2

2

.35

DEPTH FROM
BOTTOM OF M.H.

ELEV.

TO TOP OF CASTING

2.9

DISTANCE

FROM HIGHEST

FLOW LINE TO

TOP OF CASTING

ETC.

INV.

SIZES OF ALL

PIPES AND

DIRECTION OF

FLOW

DESIGN

ELEVATION - TOP

FINAL ELEVATION

DIFFERENCES

ADJUST

RECONSTRUCT

12" RCP



STRUCTURAL DATA 12-14-77

TYPE

STORM	ELECTRIC	WATER	
SANITARY ☒	TELEPHONE	OTHER	
STATION	RIGHT	LEFT	SIZE
14+76		50'	11 INCH CASTING

TYPE OF CONST.	COMMENTS
BLOCK	2-2'
BRICK	1-4'
SECTIONAL ☒	2' Block Const Top

ADJUSTING RINGS	TYPE	NO.	DEPTH	COMMENTS
BLOCK				
BRICK				
CONC. RINGS				

DEPTH FROM BOTTOM OF M.H. TO TOP OF CASTING	ELEV.	
	10.	35
DISTANCE FROM HIGHEST FLOW LINE TO TOP OF CASTING		
ETC.		
INV.		

SIZES OF ALL PIPES AND DIRECTION OF FLOW	

DESIGN ELEVATION - TOP	
FINAL ELEVATION	
DIFFERENCES	

ADJUST RECONSTRUCT	

W.S
R.G
E.Y

7-1-76
CLEAN: 800

4

CLEVELAND AVE

900' SOUTH OF CORO "C"

BENCH LEVELS $\frac{1}{2}$
ADDTL X SECT

STA	+	Σ	-	ELEV
B.M.	13.36	935.34		921.98
			10.68	924.66
T.P.			2.63	932.71
	6.52	939.23		
T.P.			0.39	938.84
	0.81	939.65		
			6.95	932.70
	2.33	935.03		
			10.37	924.66
			13.07	921.96

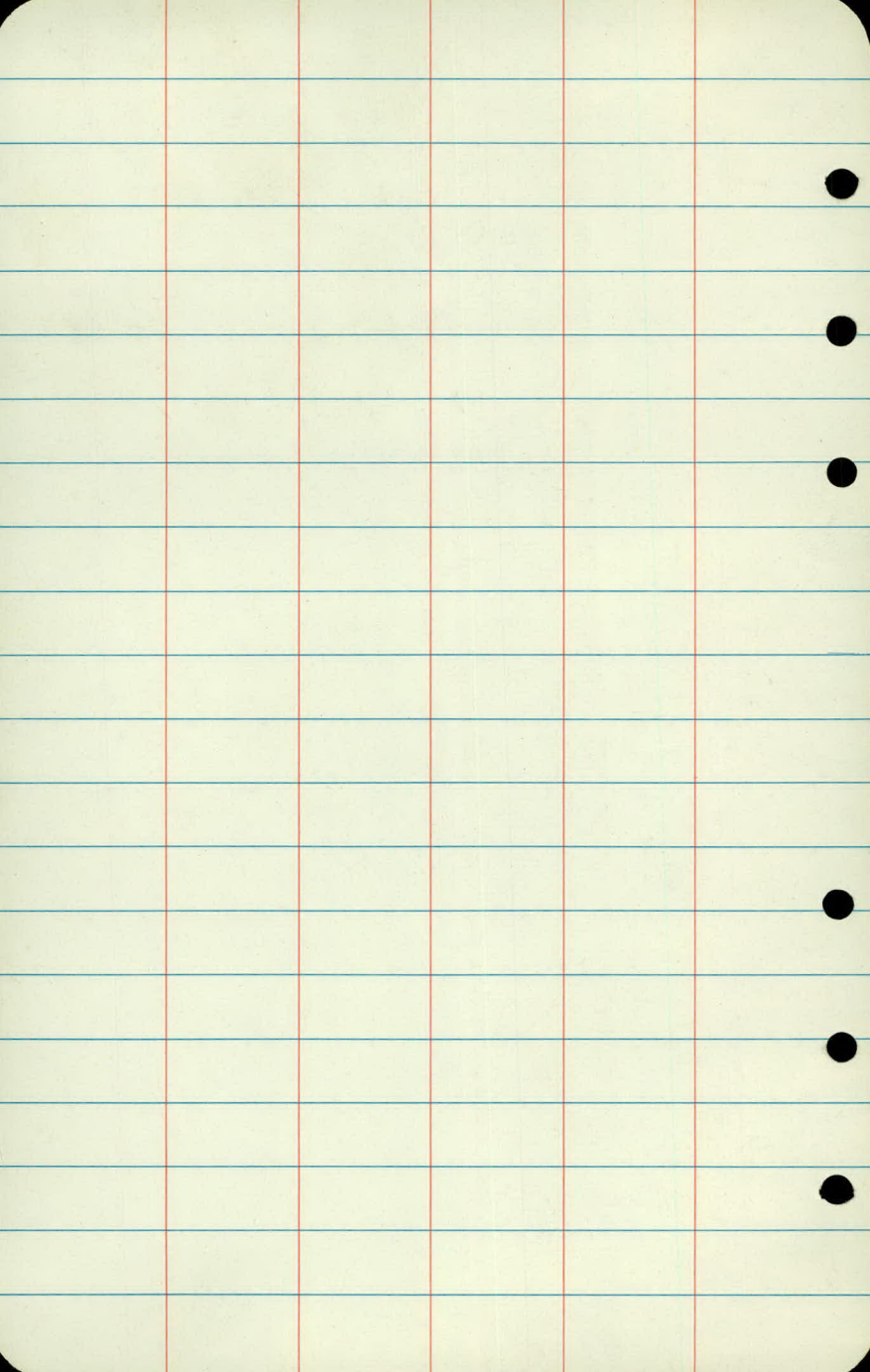
TOP OF CONC. REFERENCE PT BY R/R TRACKS

TOP OF AVD 50' SOUTH OF R/R TRACKS

TOP AVD 9270 RT 27'

TOP AVD 5791 RT 27'





FK
KE
EX.

7-2-76
CLEAR 71°
6

CLEVELAND AVENUE

900' SOUTH OF CO. RD. "C"

ADDITIONAL
CROSS SECTIONS

STA.

+

π

-

ELEV

B.M.

938.84

6+00

✓

+50

✓

7+00

✓

FA
KG
EAY

LT

July 2, 1976

Rt

7

Top Hyd Rt Sta 5+91 NE Cor Oak Crest

35.6	36.3	36.6	36.7	35.9	36.0	38.4	38.61
19	16	10		22	27	43	C 48

35.0					37.9	38.15
33					60	G 48
Fe						

34.5	35.1	35.3	35.5	35.2	34.6	35.5
18	16	11		14	22	27

34.2	34.1			38.5	38.27	38.74	37.6
28	33			72	G	C	38
					49		

32.0	32.1	34.1	34.4	34.2	33.5	36.2	37.8
33	29	10		14	22	35	44

37.6	37.78	38.23
75	G	C
	49	

Sta

7 +29

81

93 ✓

+81

32.39

32.93

314

29.79

✓

TP sta 8

932.80

932.71

+93

✓

FK
KG
Ed Y

Lt

July 2, 1976

RT

8

32.1 33.3 33.7 33.8 33.6 32.8 29.90
24 16 10 14 23 Inv
32

31.7 31.9
30 33

36.6 36.86 37.35 32.8
75 6 C 35
49

31.3 32.5 32.9 33.0 32.9 32.4 29.79 32.5
33 16 10 14 23 Inv 40
34

34.3 34.28 34.75
60 6 C
50

30.0 32.5 32.7 32.9 32.6 32.5 33.89 33.44
22 15 10 13 22 C G
33

29.7
33

33.76 34.22 33.64 34.10
6 C 6 C
66 50

Sta

8 Ent Rt

✓

+14 S.D. 36' Rt 932.84

+17

✓

+27

+31 Inv 12" SCP 40' Rt 930.10

FK
HG
EdY

July 2, 1976

RT

9

Lt

29.3 32.2 32.6 32.8 32.5 32.4 33.5 33.9
22 16 10 14 21 50 75

26.5 27.9 26.09
29 34 1nV
28

28.3 32.1 32.4 32.6 32.2 32.1 33.52 33.06
25 15 10 14 20 $\frac{0}{35}$ $\frac{0}{35}$

27.8 28.2 $\frac{1}{2}$
~~37.8~~ ~~38.2~~
33 61

33.50 33.96
 $\frac{0}{53}$ $\frac{0}{53}$

29.0 31.9 32.2 32.4 32.1 32.1 32.3 29.55
24 16 10 13 21 28 1nV
34

28.3 29.4
30 51

#143
33.55 33.41 33.89 33.6
55 $\frac{0}{49}$ $\frac{0}{49}$ 42
SD

Sta	+	π	-	Elev.
-----	---	---	---	-------

8+54		Ent Lt		
------	--	--------	--	--

✓

BM		Top Hyd Rt @ 9+70		
----	--	-------------------	--	--

932.71

9+00

✓

+09	Inv	12" RCP 41' Rt	929.79
-----	-----	----------------	--------

+21	Inv	18" RCP 36' Rt	928.35
-----	-----	----------------	--------

+31

FK
KG
EdY

Lt

July 2, 1976

10

30.6 31.2 32.0 32.0 31.7 31.0 30.0 29.3 33.5
24 17 10 14 22 31 36 44

340. 33.68 34.11
58 G 50
50 C

30.58 30.22 30.54 30.02 30.49 29.84
C G C G C G
37 55 25

31.7 31.0 31.3 31.4 31.1 30.7 30.4 28.8
25 17 10 14 20 27 33

32.59
50
Conc @ Ho

33.8 33.53 33.98 33.2
60 G C 44
51

32.1 31.3 30.7 30.9 31.0 30.6 30.1 29.1 27.93
61 37 16 10 14 30 34 35

1mV
2' X 3' area
cm

32.2 34.6 31.2 33.5 30.9 33.2 30.5
G W G W G W 40
99 58 43

Sta

BM

932.71

7+84 SD 75' Rt 933.73

9+09 SD 5⁸8' Rt 933.4211+09 Tell MH 15' Lt 927.64
928.0511+17 Tell MH 15' Lt 927.41
927.8211+17 Tell MH 21' Lt 927.25
927.65

TP

927.62

~~12+62 MH Rt 36'~~~~2.35~~ 921.94

12+62 MH Rt 36' 917.99

13+20 MH 24' Rt 919.70

(14+42 Lt 40' 917.50 water comp.
14+52 MH in 0.00 notes)Tell
14+56 MH 26' Lt 913.86Tell
14+66 MH 19' Lt 913.90

14+40 Rt 32 CB 914.29

14+60 Rt 43' CB 914.68

13+00 N. Rail 921.16

FK
LKF

April 28, 1977
Clear 40°

11

Top Hyd Rt Sta 9+70[±]

2.8' Deep Invert Elev. 930⁶²

sta

Lenker Rod

-

+

BM

2.82 919.16

(921.98)

13+21

0.58 919.74

-

2.14

(910.60) ? $\frac{1}{2}$

5.7

914.04

12+83

9.45 918.61 - 3.96

3.96

12+83

914.65

BM

5.50 924.66

12+98

2.01 921.17 (921.16)

FK
LF

May 2, 1971
Clear 60°

12

Top Roseville BM

• Top MH Rt 24'

Inv North

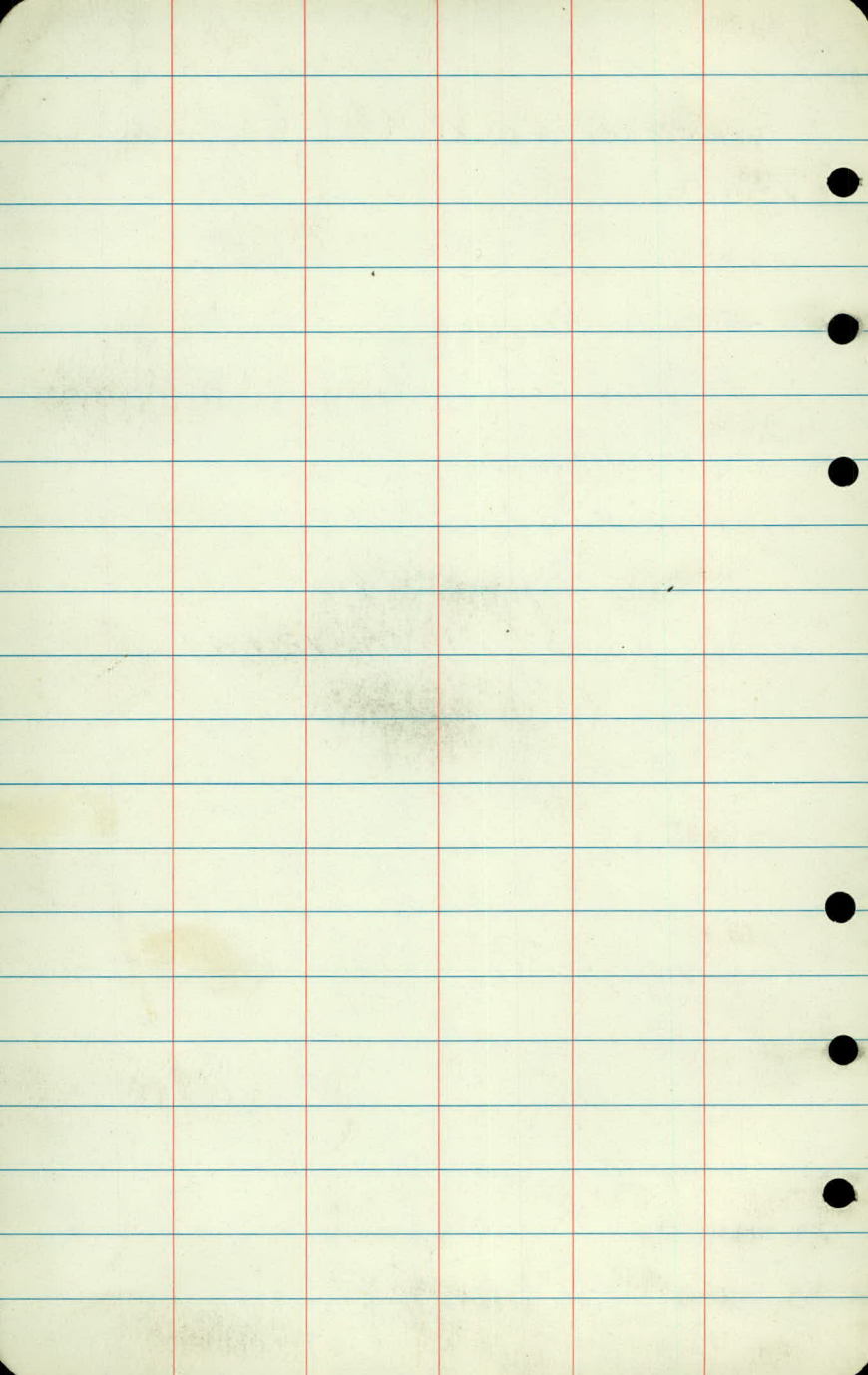
• Inv South

Top S End Pipe 29' Rt

• Inv S. End Pipe 29' Rt

Top Hyd 22' Rt Sta 12+44

Top N. Rail at



KP
DS
RJ
JC

30 NOV 1973

CO. RD. C

SILVER LAKE RD TO W. CO. LINE

BENCH LEVELS

STA	+	π	-	ELEV.
BM	0.24	947.39		947.15
	3.95	945.20	6.14	941.25
	3.61	944.66	4.15	941.05
	8.64	949.62	3.68	940.98
	3.48	949.99	3.19	946.43 946.51
	3.34	944.42	8.91	941.08 941.06
	2.80	943.96	3.26	941.16 941.12
	6.46	947.78	2.64	941.32 941.26
			0.57	947.21 947.15

30 NOV. 1973

DESCRIPTION

TOP HYD. LT STA 12+68 L'

SW COR ENT SLAB TOLEDO SCALE CO.

TOP HYD. NW COR ANTHONY & CO. R.D.C

E STA 4+00 L'

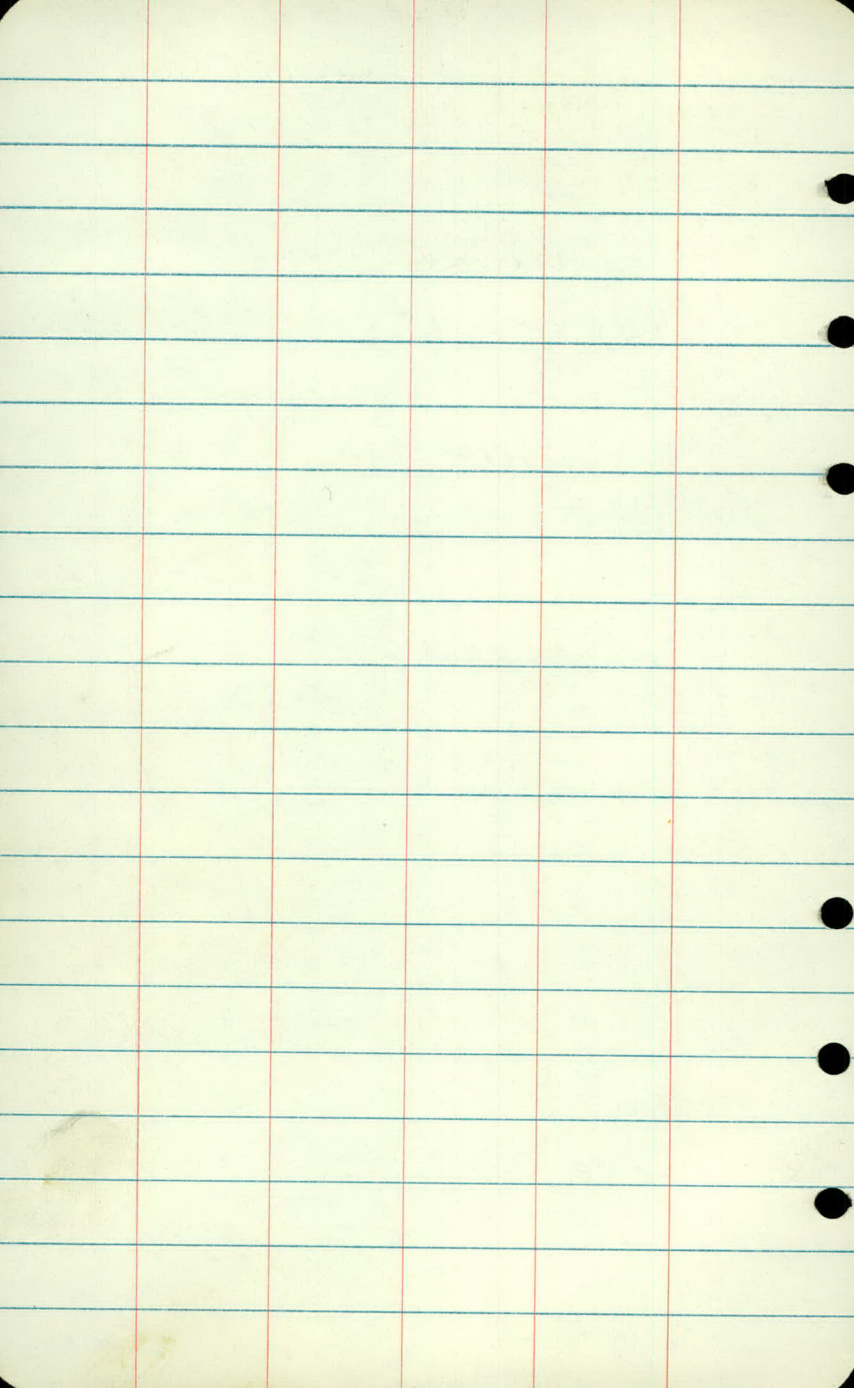
TOP HYD NW COR. RANKIN & CO. R.D.C

E STA 4+00

TOP HYD. NW COR ANTHONY & CO. R.D.C

SW COR ENT SLAB TOLEDO SCALE CO.

TOP HYD LT STA 12+68 L'



KP
DS
LPD

13 NOV. 1974
CLOUDY 30° 1

Add. X-Sections Nov 4, 1976-FRK

CORD C

STH#8 TO CLEVELAND AVE

ADDITIONAL X-SECTIONS

Rt.

computed LRF 11-26-74

STA + π - ELEV.

BM 2.75 949.26

946.51

2+00

✓
2+06

+08

5.29 43.97

+20

+21

5.52 43.74

3+50

✓
4+50

+76

6.20 943.06

13 NOV. 1974 RT 2

TOP HYD, NW COR CO. RD & RANKIN

44.21 43.79 44.24 44.2 43.15
5.05 5.47 5.02 5.1 5.81
22 23 37 51
6 TC TC

37.6 41.4 42.32 41.80 42.86
8.7
34.6 34.6 31.6 32.0 11.7 7.9 6.94 7.46 6.40
145 125 111 109 91 79 71 70 52
TC 6 6

TOP MH 28.0' RT

TOP MH 28.0' RT

43.36 43.02 43.50 43.26
5.90 6.24 5.76 6.00
22 23 35
6 TC TC

38.5 41.3 42.13 41.67 42.67
35.0 35.5 32.5 32.5 10.8 8.0 7.13 7.59 6.59
133 107 94 88 72 63 55 54 36
MH 26' RT TC 6 6

STA + π - ELEV.

949.26

3+00

✓

+50

✓

8.16 941.10 (941.06)

TBM Lenker Rod

941.10

+66

✓

13 NOV 1974
RT

3

42.62 42.26 42.70 42.72 42.20

6.64 7.00 6.56 6.54 7.06
22 23 25 26
G TC TC G

34.4 38.8 41.1 41.7 41.24

GUTTER	TIC.								
3552	36.01	35.6	32.9	32.6	14.9	105	8.2	7.55	8.02
114	113	95	83	79	74	60	52	43	43
								TC	G

41.93 40.94 41.42 40.06 36.7

7.33 8.32 7.84 9.2 12.6
37 38 46 60
G TC

B/T	GUTTER	TIC.			
35.9	35.61	36.04	35.9	32.9	32.9
144	101	100	86	72	70

STA 4100

Sta 4100

RG
KCP
LPD

Dec 4, 1974
clay 22°

41.68 41.54 40.80 41.26 40.9
11 35 36 43
BC TC

36.7 36.8 36.8 33.8 33.6 36.9
124 106 87 73 66 59

STA + π - ELEV.

Lenker Rod

941.10

4+00

✓

+50

✓

+65

39.72

+65

34.51

+72

✓

Q

X

Dec 4, 1974
RT

4

41.10	41.00	40.50	40.99	40.8	37.1	33.9
	11	34 BC	35 TC	39	53	63

37.1	41.9	40.4	36.9	34.1
140	115	102	84	69

40.40	40.27	40.00	40.41	40.1	36.9	34.1
	11	30 BC	31 TC	36	47	56

38.0	41.6	41.8	37.1	36.4	34.2
124	117	109	93	75	62

F-L CB RT 27'

F-L 12' CM RT 53'

40.14	39.95	39.69	40.16	39.9	36.4	34.1	34.1
	12	27 BC	28 TC	34 FL	46	53	58

37.1	39.6	40.4	36.9	36.5
129	117	102	87	74

STA + π - ELEV

Lenker Rod

941.10

4483

✓

BM

41.14

(941.12)

Lenker Rod

1.12 (41.12)

5+00

✓

+50

+71

34.37

Dec 4, 1974

RT

5

40.00	39.82	39.51	39.5	36.4	34.2	34.3
"	28.5	35	46	53	58	
	end curb					

37.3	38.8	39.3	36.7	36.3
121	113	97	79	72

Top Hyd @ St. Anthony (NW cor)

"

"

"

"

39.75	39.61	39.32	39.0	34.3	34.2	36.3	37.6
"	27	35	49	59	72	84	

36.4	36.9
120	107

39.33	39.22	38.99	38.6	34.7	34.8	37.5	39.0
"	23.5	32	44	50	67	36.4	36.9
						80	

T.C.

38.86	39.83
100	99

FL Apron 24" RCP R+40'

STA	+	π	-	ELEV.
-----	---	-------	---	-------

41.12

6+00				
------	--	--	--	--

✓

+25				
-----	--	--	--	--

✓

+33				
-----	--	--	--	--

✓

L

Dec 4, 1974
RT

6

38.97 38.92 38.74 38.5 35.1 35.1
11 22 27 40 46

Gutter	T.C.		39.2	37.3
38.88	39.34	39.5	36.4	36.8
102	101	90	78	61 60

38.90 38.82 38.59 38.3 35.2 ^{35.1} ~~36.8~~ 38.7 36.7
11 22 28 40 48 ~~58~~ 67 75

Gutter	T.C.	
38.88	39.33	39.4
101	100	85

38.91 38.82 38.57 38.3 35.2 35.9 39.0
11 22 27 39 ~~59~~ ~~78~~
50 69

38.88	39.30	39.4
102	101	85

STA

+

π

-

ELEV

41.12

6+50

✓

+62

✓

+92

7+00

38.85

P

Dec 4, 1974
RT

7

38.86	38.76	38.54	38.2	35.2	36.2	39.4
	11	22	27	38	36.7	37.6
					51	70
					51	70

39.2	39.2
110	95

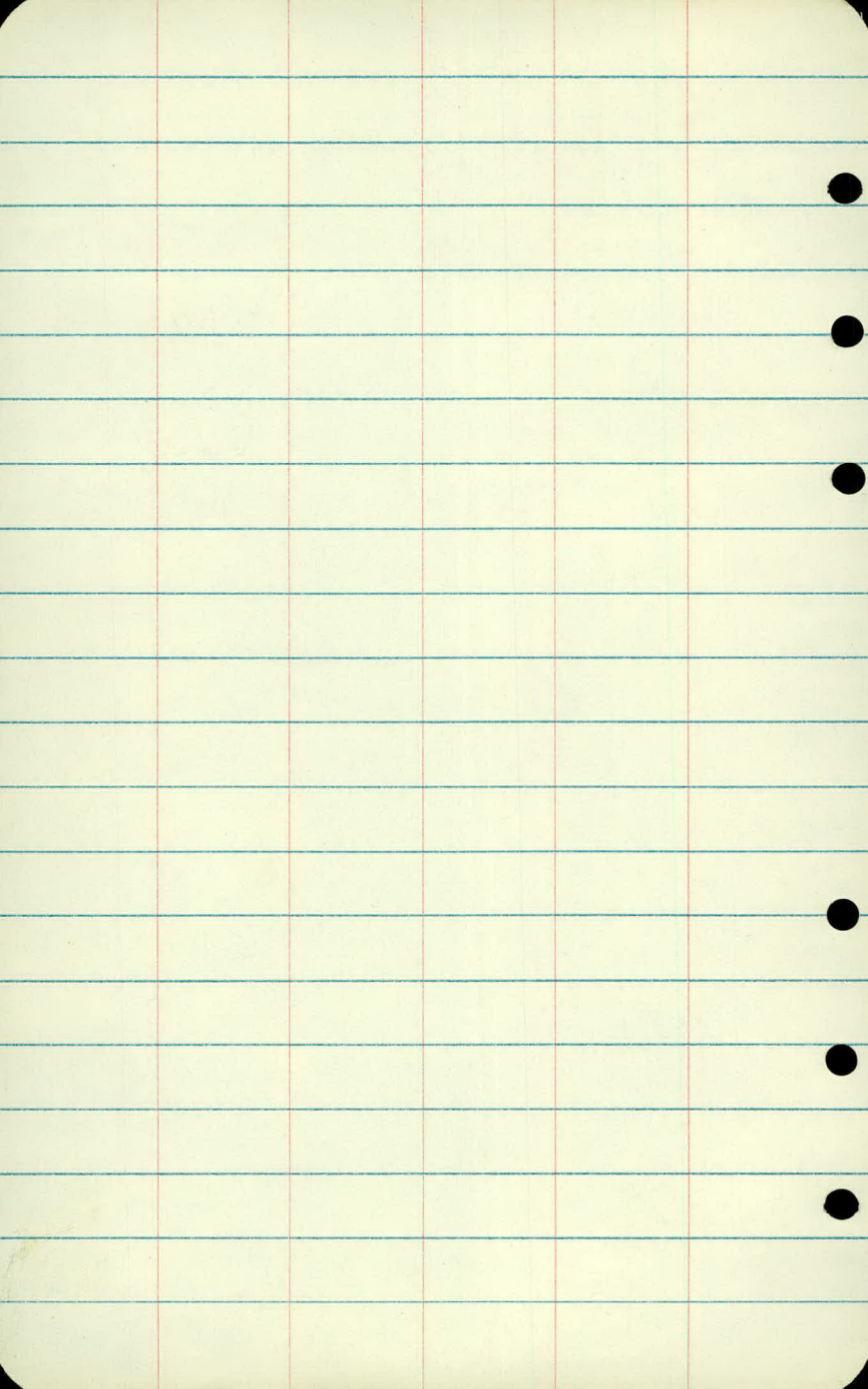
38.84	38.72	38.56	38.3	35.3	36.8	37.3
	11	22	24	37	55	74.
		end emc				

/ / / / / / / / / / / / / /

38.86	38.75	37.90	34.37	36.6	37.2
	11	32	40	47	62
	BT	BT	FL		

W. end
15" RCP

Sta 7+00



KP
LPD

DS
JC

13 NOV. 1973

1.

CO. RD. C.

W. CO. LINE TO CLEVELAND AVE
PLAN SURVEY

PAGE

TITLE;

1

~~ALINEMENT.~~

~~2-5~~

TOPOGRAPHY

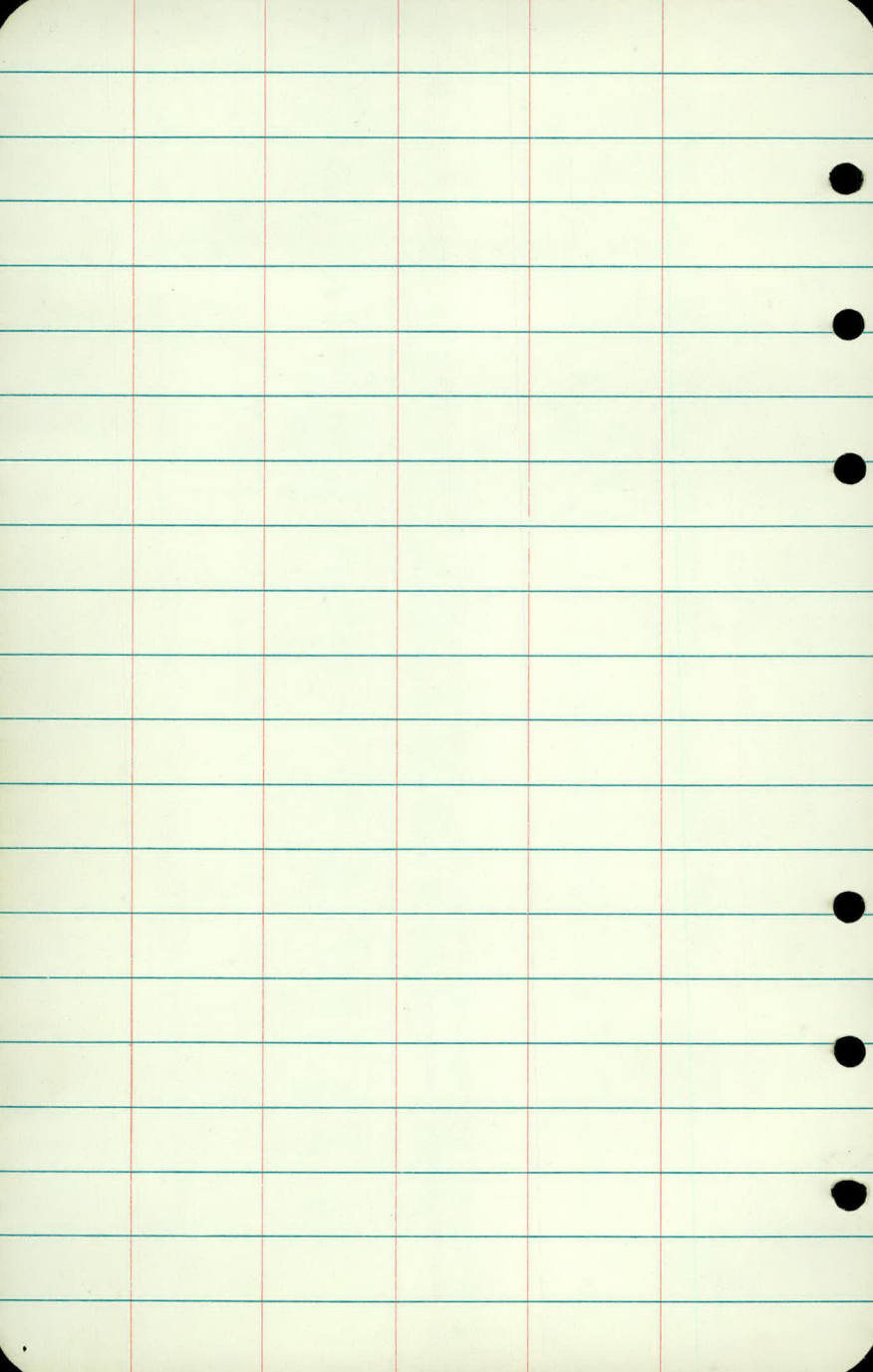
10-26

BENCH LEVELS

6-9

X- SECTIONS

27-



15 NOV. 1973

16

Co. RD C

W. Co. LINE TO CLEVELAND

BENCH LEVELS

STA	+	T	-	ELEV
BM	3.60	929.19		925.59
	2.72	929.67	2.24	926.95
	2.75	931.00	1.42	928.25
	2.55	932.02	1.53	929.47
	1.94	931.56	2.40	929.62
	1.15	928.80	3.91	927.65
	2.20	925.77	5.23	923.57
	3.08	917.51	11.34	914.43
	5.26	917.42	5.35	912.16
	3.72	918.79	2.35	915.07
	8.87	926.09	1.57	917.22
	6.82	931.66	1.25	924.84
	6.40	937.06	1.00	930.66
	4.57	940.11	1.52	935.54
	9.37	945.95	3.53	936.58
	7.63	953.40	0.18	945.77
	6.72	958.99	1.13	952.27
	2.18	959.59	1.58	957.41
	2.83	954.24	8.18	951.41
	4.95	955.78	3.41	950.83

16 Nov, 1973

7.

DESCRIPTION

TOP HYD. NW COR. E & FAIRVIEW

TOP HYD. AT RAMSEY ENG. CO.

TOP HYD. BY CLARK FENCE CO.

TOP HYD. N.W. COR PRIOR & CO. RD. C

TOP HYD. AT INDIAN HEAD TRUCKING

TOP HYD. AT MOUNT RIDGE RD.

TOP HYD AT ANIMAL HOSPITAL

TOP IRON MONT & CLEVELAND

TOP CB 70' E. OF BRIDGE S. SIDE OF RD

TOP HYD. AT RUAN TRUCKING

SPIKE IN PP SW COR. LONG LAKE RD.

TOP HYD. LT STA 34+30

& STA 30+00

TOP HYD LT STA 28+25

SPIKE IN ARC-LITE POLE N.W. COR ENT LT 25+00

TOP HYD. LT STA 22+10

TOP HYD. LT STA 18+60

TOP HYD. LT STA 15+10

C & GS MONT RT STA 11+05 # 19

TOP HYD LT STA 9+10

STA	+	π	-	ELEV.
-----	---	-------	---	-------

		955.78		
--	--	--------	--	--

1.05	954.03	2.80	952.98	
------	--------	------	--------	--

		7.21	946.82	
--	--	------	--------	--

6.83	953.97	6.89	947.1A	
------	--------	------	--------	--

		7.16	946.81	
--	--	------	--------	--

2.43	955.40	1.00	952.97	use
------	--------	------	--------	-----

3.44	954.31	4.53	950.87	950.86
------	--------	------	--------	--------

		2.26	952.05	
--	--	------	--------	--

7.83	959.27	2.87	951.44	951.37
------	--------	------	--------	--------

1.62	959.09	1.85	957.42	
------	--------	------	--------	--

1.62	953.88	6.78	952.26	
------	--------	------	--------	--

0.93	946.70	8.11	945.77	
------	--------	------	--------	--

3.63	940.20	10.13	936.57	
------	--------	-------	--------	--

		4.68	935.52	
--	--	------	--------	--

		4.70	935.50	
--	--	------	--------	--

		5.00	935.20	
--	--	------	--------	--

		5.04	935.16	
--	--	------	--------	--

1.85	937.38	4.67	935.53	
------	--------	------	--------	--

2.16	932.89	6.70	930.68	930.67
------	--------	------	--------	--------

0.48	925.34	7.98	924.86	924.85
------	--------	------	--------	--------

21 Nov. 1973

8.

DESCRIPTION

TOP HYD. RT STA 2+38

TOP STONE MONT. STA 0+00

TOP HYD. LT STA 0+32 ✓

TOP STONE MONT. STA 0+00 ✓

TOP HYD. RT STA 2+38

TOP HYD. LT STA 9+10

TOP HYD. RT STA 11+00

C&GS MONT. RT STA 11+05

TOP HYD. LT STA 15+10

TOP HYD. LT STA 18+60

TOP HYD. LT STA 22+10

SPIKE IN ARC-LITE BLEND W. Cor Ent LT²⁵⁺⁴⁰

W. Track Spur Line

E. Track Spur Line

W. Track MAIN Line

E. Track MAIN Line

TOP HYD. LT STA 28+25

£ STA 30+00

TOP HYD LT STA 34+30

STA	+	π	-	ELEV.
-----	---	-------	---	-------

		925.34		
--	--	--------	--	--

1.94	919.16	8.12	917.22	
------	--------	------	--------	--

2.30	917.37	4.09	915.07	
------	--------	------	--------	--

6.42	918.03	5.76	911.61	
------	--------	------	--------	--

10.70	925.15	3.58	914.45	(914.44)
-------	--------	------	--------	----------

5.33	928.93	1.55	923.60	(923.59)
------	--------	------	--------	----------

4.17	931.85	1.25	927.68	(927.67)
------	--------	------	--------	----------

2.69	932.33	2.21	929.64	(929.63)
------	--------	------	--------	----------

1.37	930.86	2.84	929.49	(929.49)
------	--------	------	--------	----------

1.67	929.91	2.62	928.24	
------	--------	------	--------	--

2.52	929.40	2.95	926.96	(926.95)
------	--------	------	--------	----------

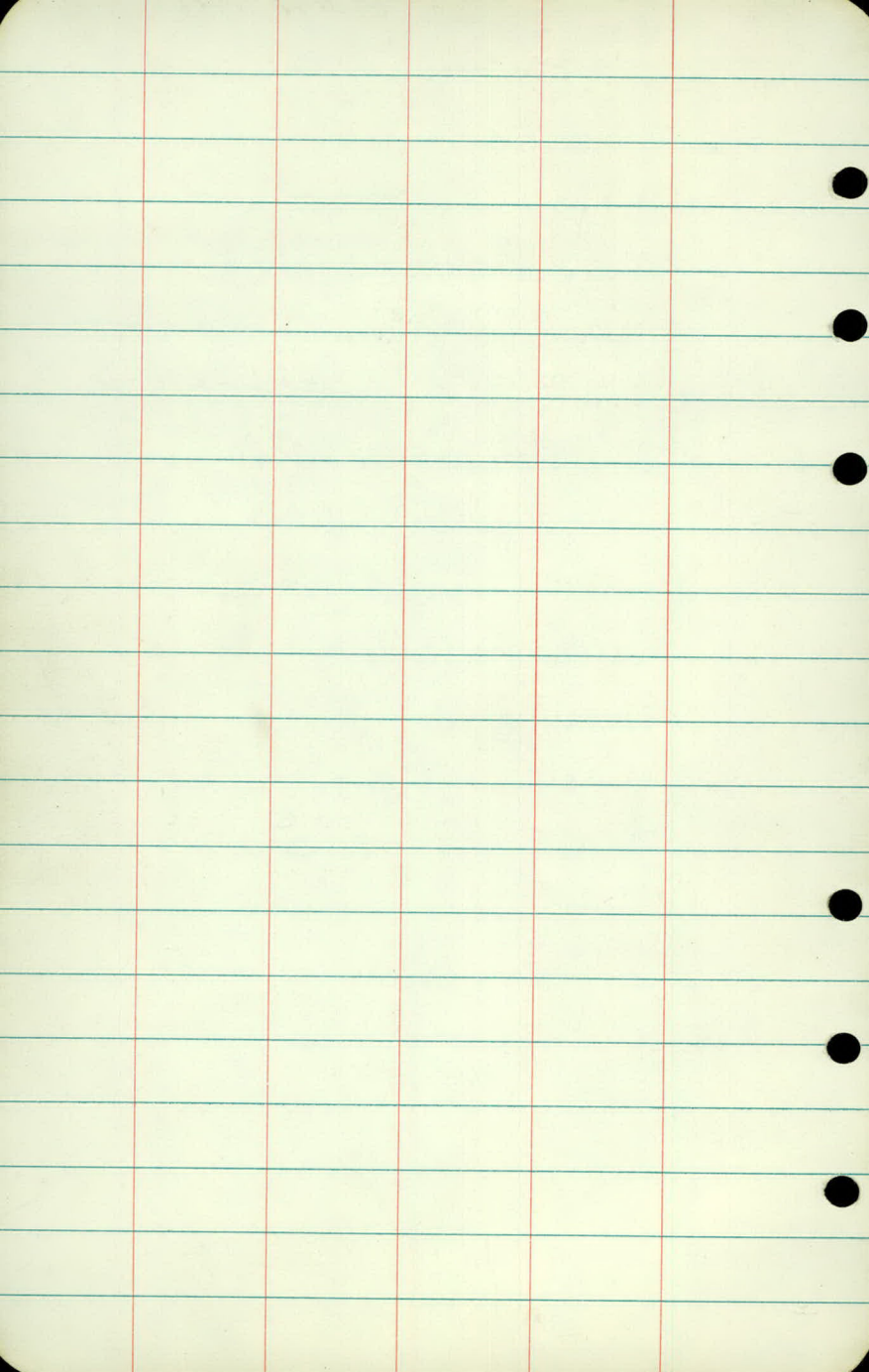
		3.88	925.60	(925.59)
--	--	------	--------	----------

21 Nov. 1973

9.

DESCRIPTION

- SPIKE IN ARC-LITE POLE SW COR LONG LAKERD
- TOP HYD. AT RUAN TRUCKING
- TOP CB (FL)
- TOP IRON MONT. & CLEVELAND
- TOP HYD. AT ANIMAL HOSPITAL
- TOP HYD. AT MOUNT RIDGE RD.
- TOP HYD. AT INDIANHEAD TRUCKS
- TOP HYD. NW COR PRIOR & CO. RD C
- TOP HYD. BY CLARK FENCE CO.
- TOP HYD. BY RAMSEY ENG CO.
- TOP HYD. NW. COR. FAIRVIEW



3 DEC 1973

KP
WS
DS
LPD

CO. RD. C

~~SILVER LAKE RD~~ TO. W. CO. LINE
T.H.B

X- SECTIONS

STA + π - ELEV.

BM 3.73 950.24

(946.51)

9.15

~~941.06~~
941.09

(941.06)

1+49 = E. EDGE SLAB NBL STH 8

✓

2+00

+08

6.99 943.25

+21

7.16 943.08

+50

LT

4 DEC. 1973

RT

TOP HYD. NW COR CO. RDC - RANKIN

STA 4+00 L¹ AA.72 AA.13 A3.49 A3.29

4.20	4.51	4.68	5.12	5.52	6.11	6.75	7.00
150	100	75	32		40	80	100

A6.26

3.98

200

See
new
Kseels
LKF

A1.20

A2.27

9.04

7.97

200

150

37.19

A0.44

A2.82

A3.96

A4.22

A4.47

A4.92

A6.05

A6.56

13.1

9.8

7.42

6.28

6.02

5.77

5.32

4.19

4.68

61

38

33

12

13

13

48

48

Rt. Jk

Lt. Jk

TOP MH 28' RT

TOP MH 28' RT

A5.18

A3.52

A3.82

A3.29

A3.35

A3.27

A2.89

A3.39

A3.79

5.06

4.72

6.42

6.95

6.89

6.97

7.4

10.9

13.5

58

58

13

13

12

26

35

52

G

A5.55 TC

TC

G

4.69

75

STA + π - ELEV.

950.24

2+96

7.10

943.14

3+00

✓

+50

✓

TP

2.95

944.01

9.15

941.09
~~941.06~~

941.06

LT

4 DEC. 1973
RT

TOP MH 31' LT

A2.5A

A2.8A

A2.87

A2.96

A2.6A

A2.51

A1.7A

37.3A

7.7

7.4

7.37

7.78

7.60

7.73

8.5

12.9

63

48

31

11

11

33

52

39.5A

10.7

85

37.3A

A1.1A

A1.3A

A1.80

A1.93

A1.79

90.9A

37.8A

12.9

9.1

8.9

8.44

8.31

8.45

9.3

12.4

42

28

20

11

11

21

35

38.6A

39.3A

11.6

10.9

57

75

STA 4+00

STA

+

π

-

ELEV

944.01

4+00

✓

+50

✓

+72

✓

LT

4 DEC. 1973

RT

37.31

40.91

40.81

40.99 ✓

41.06

40.99

40.61

37.81

35.51

6.7

3.6

3.2

3.02

2.95

3.02

3.4

6.2

8.5

38

27

22

11

11

23

36

59

38.11

38.01

5.9

6.0

50

75

37.81

36.71

36.91

39.61

40.29

40.39 ✓

40.25

39.91

36.61

34.61

6.2

7.3

7.1

4.4

3.72

3.62

3.76

4.1

7.4

9.4

50

40

30

26

11

11

22

40

50

38.21

5.8

75

36.38

39.21

39.61

40.01

40.11 ✓

39.99

39.91

36.81

34.71

7.63

4.8

4.4

4.00

3.87

4.02

4.6

7.2

9.3

36

28

22

11

11

23

38

50

FL

37.91

38.41

38.51

6.6

5.6

5.5

38

44

75

STA	+	π	-	ELEV.
-----	---	-------	---	-------

		944.01		
--	--	--------	--	--

4+83				
------	--	--	--	--

✓				
---	--	--	--	--

5+00				
------	--	--	--	--

✓				
---	--	--	--	--

+38				
-----	--	--	--	--

		5.00	939.01	
--	--	------	--------	--

+50				
-----	--	--	--	--

LT

4 DEC. 1

RT

39.01

39.31

39.91

39.86

39.99

39.83

39.31

36.61

34.51

5.0

4.7

4.6

4.15

4.02

4.18

4.7

7.4

9.5

75

50

26

11

11

24

38

50

39.51

39.21

39.31

39.67

39.79

39.63

38.81

39.61

34.41

4.5

4.8

4.7

4.34

4.22

4.38

5.2

7.4

9.6

75

50

34

11

11

24

38

50

SW Cor Conc. ✓ slab 33.0 LT

39.72

39.29

38.92

38.71

39.01

39.20

39.39

39.24

38.91

35.81

34.51

4.29

4.77

5.09

5.3

5.0

4.81

4.67

4.77

5.6

8.2

9.5

75

50

33

28

21

11

11

24

38

50

Conc

Conc

Conc

STA	+	π	-	ELEV.
-----	---	-------	---	-------

		944.01		
--	--	--------	--	--

5+57				
------	--	--	--	--

			5.12	
--	--	--	------	--

				938.89
--	--	--	--	--------

+74				
-----	--	--	--	--

			4.93	
--	--	--	------	--

				939.08
--	--	--	--	--------

+100				
------	--	--	--	--

+25				
-----	--	--	--	--

+33				
-----	--	--	--	--

✓				
---	--	--	--	--

BM	209	943.21	2.88	941.13
----	-----	--------	------	--------

				941.12
--	--	--	--	--------

LT

4 DEC. 1973

RT

S.E. Cor Conc. Slab 33.0 LT

TOP MH 34.0 LT

38.91	38.71	38.51	38.86	38.96	38.93	38.41	35.91	35.01	36.71
5.1	5.3	5.5	5.15	5.05	5.08	5.6	8.1	9.0	7.3
75	50	24	11		11	23	35	50	75

38.31	38.61	37.91	38.01	38.78	38.96	38.89	38.41	35.31	36.31	36.81
5.7	5.4	6.6	6.0	5.23	5.05	5.17	5.6	8.7	8.7	7.2
75	50	33	24	11		11	24	38	50	75

34.7	36.41	37.01	38.11	38.78	38.93	38.82	38.51	35.71	35.01	35.81	36.61
9.26	7.60	7.0	5.9	5.23	5.08	5.19	5.5	8.3	9.0	8.2	7.4
36	34	30	24	11		11	23	35	46	60	75
FL											

36.51	38.21	38.11
7.5	5.8	5.9
38	50	75

TOP HYD. N.W. Cor Co. RDC & ANTHONY

STA + π - ELEV.

943.21

6+50

+92

7+00

+03 = Curb RT

+15 = $\frac{1}{2}$ RD. RT

+26 = Curb RT

LT

4 DEC. 1973
CLOUDY RT
20°

37.11	37.21	36.11	35.41	38.31	38.73	38.87	38.76	38.51	36.61	35.21	36.11	37.11
5.8	6.0	7.1	7.8	4.9	4.48	4.34	4.45	4.7	6.6	8.0	7.1	5.8
75	49	44	36	25	11		11	22	32	38	50	75

37.11	36.81	36.01	36.11	38.51	38.71	38.92	38.79	37.91	34.59	36.81	37.11
6.1	6.4	7.2	7.1	4.7	4.47	4.29	4.42	5.3	8.62	6.4	5.8
75	50	44	35	23	11		11	33	40	50	75

FL

37.01	37.21	36.31	36.51	38.41	38.71	38.89	38.79	38.11	37.11	38.31
6.2	6.0	6.9	6.7	4.8	4.44	4.32	4.42	5.1	5.8	4.9
75	50	46	32	23			11	40	50	75

SAME AS 7+00

38.93	38.79	38.21	38.21	38.54	38.09	38.92
4.28	4.42	5.0	5.0	4.67	5.12	4.21
	11	38	50	57	57	75

TC 6 6

36.21	36.01	34.77	37.81	38.41	38.81	38.25	38.81	38.41	38.40	38.21
7.0	7.2	8.44	5.4	4.8	4.40	4.26	4.40	4.8	4.81	5.00
75	50	40	30	23	11		11	40	57	75

FL CONC CONC

37.71	38.11	38.41	38.86	38.96	38.84	38.57	35.65	38.18	38.40	37.97
5.5	5.1	4.8	4.35	4.25	4.37	4.7	4.56	5.03	4.81	5.24
75	50	30	11		11	36	57	57	75	75

TC 6 TC 6

STA + π - ELEV.

943.21

7+31

4.50 938.71

+38 = ~~E~~ ANTHONY

+48 = Curb Rt B6 (INTREGRANT)

+59 = ~~E~~ RD RT

+71 = Curb Rt

+81

TP 4.46 943.81 3.86 939.35

LT

4 DEC. 1973
RT

TOP MH 14.0 LT

38.01	38.21	38.63	38.91	39.02	38.91	38.51	38.41	38.82	38.51
5.2	5.0	4.58	4.30	4.19	4.30	4.7	4.8	4.39	4.7
75	50	27 MH	11		11	30	46	46 TC	75

37.71	37.91	38.31	38.92	39.05	38.95	38.51	38.73	38.21	38.41	38.04
5.5	5.3	4.9	4.29	4.16	4.26	4.7	4.48	4.94	4.74	5.17
75	50	36	11		11	34	57 TC	57 G	75 TC	75 G

36.51	36.61	35.41	38.01	38.92	39.04	38.99	38.41	38.65	38.38
6.7	6.6	7.80	5.2	4.29	4.12	4.22	4.8	4.56	4.83
75	50	41 FL	29	11		11	34	57 conc.	75 conc.

37.21	37.41	37.21	37.21	39.00	39.16	39.05	38.31	38.68	38.24	38.46	38.00
6.0	5.8	6.0	4.9	4.21	4.05	4.16	4.9	4.53	4.97	4.75	5.21
75	50	35	22	11		11	34	57 TC	57 G	75 TC	75 G

38.01	38.11	38.21	37.21	38.51	39.09	39.21	39.10	38.11	35.09	37.51	37.91
5.2	5.1	5.0	6.0	4.7	4.12	4.00	4.11	5.1	8.12	5.7	5.3
75	50	44	33	21	11		11	33	40 FL	50	75

± STA 8+00

STA	+	T	-	ELEV.
-----	---	---	---	-------

		943.81		
--	--	--------	--	--

BM	2.53	943.79	2.53	941.28	941.26
----	------	--------	------	--------	--------

8+00

+50

9+00

+54

+58

+71 = & ENT LT.

LT

4 DEC 1974
RT

S.W. Cor Ent Slab TOLEDO SCALE CO.

^{38.67} 5.1 50
^{38.89} 4.9 35
^{37.29} 6.5 32
^{38.89} 4.9 21
^{39.21} 4.58 11
^{39.33} 4.46 11
^{39.19} 4.60 24
^{38.89} 4.9 37
^{35.99} 8.3 45
^{35.29} 8.5 59
^{37.89} 5.4 75
^{37.89} 5.9 75

^{38.99} 4.8 63
^{38.59} 5.2 43
^{37.69} 6.1 31
^{39.99} 4.3 21
^{39.69} 4.15 11
^{39.71} 4.08 11
^{39.59} 4.20 23
^{39.29} 4.5 33
^{36.39} 7.4 42
^{35.49} 8.3 56
^{37.99} 5.8 75
^{38.49} 5.3 75

BLDG

^{38.79} 5.0 63
^{38.69} 5.1 42
^{37.69} 6.1 31
^{39.89} 3.9 22
^{40.27} 3.52 11
^{40.40} 3.39 11
^{40.26} 3.53 11
^{39.79} 4.0 22
^{36.49} 7.3 35
^{36.39} 7.4 44
^{38.69} 5.1 56
^{38.89} 4.9 75

BLDG

^{38.93} 4.86 60
^{39.19} 4.6 41
^{38.09} 5.70 31
^{40.59} 3.2 21
^{41.26} 2.53 11
^{41.28} 2.51 11
^{41.12} 2.67 11
^{40.39} 3.4 22
^{38.29} 5.5 34
^{38.09} 5.7 50
^{39.19} 4.6 56
^{39.29} 4.5 75

SW FL

^{38.86} 4.93 60
^{39.29} 4.5 50
^{40.39} 3.4 25
^{41.31} 2.48 11
^{41.27} 2.42 11
^{41.21} 2.58 11
^{40.39} 3.4 21
^{38.29} 5.2 36
^{37.99} 5.8 45
^{38.69} 5.1 50
^{39.09} 4.7 56
^{39.39} 4.4 75

SW

^{38.79} 5.0 75
^{39.49} 4.3 50
^{40.99} 2.8 18
^{41.41} 2.38 11
^{41.52} 2.27 11

SAME AS 9+83

STA

+

π

-

ELEV.

943.79

9483

487

10400

BM

2.53

941.26

941.26

LT

4 DEC. 1973

RT

38.99	39.69	41.09	41.61	41.70	41.55	40.69	38.99	38.69	39.59	39.29
4.8	4.1	2.7	2.18	2.09	2.24	3.1	4.8	5.1	4.2	4.5
75	50	20	11		11	22	33	50	57	75

39.19	39.99	40.19	38.96	40.99	41.64	41.75	41.60	40.69	38.99	38.79	39.59	39.29
4.6	3.8	3.6	4.83	2.8	2.15	2.04	2.19	3.1	4.8	5.0	4.2	4.5
75	50	38	31	21	11		11	21	33	50	57	75

41.99
1.80

S.W. Cor ENT SLab TOLEDO SCALE CO.

STA

+

π

-

ELEV.

KP
DS
RU
VC

28 Nov. 1973
SUNNY 30°

27

CO. RD. C.

30' x 1'

W. CO. LINE TO CLEVELAND AVE.

X- SECTIONS

STA + π - ELEV

BM 2.80 949.62

(946.82)

-3+01 = 9+99

9.55 940.07

✓

-3+00 = 10+00 = 13+00

-2+84 $\overset{10+16}{=}$ ENT. LT

10+16

TP 2.61 949.74 2.48 947.14

(947.15)

-2+71 = 10+29
Gutter Lt

16+29

LT

28 Nov. 1973

28

TOP MONT & STA 0+00

FL W. END 15" CM 31.0 LT 0-301

939.52	40.12	40.12	41.22	41.89	42.01	41.89	41.62	40.82	39.72	38.82	38.42
10.1	9.5	8.9	8.4	7.73	7.61	7.78	8.0	8.8	9.9	10.8	10.1
75	52	33	21	11		11	16	23	36	53	75

39.82	40.32	41.12	42.13	42.28	42.13	41.32	40.62	39.22	39.12	39.62
9.8	9.3	8.5	7.49	7.34	7.49	8.3	9.0	10.4	9.9	10.0
75	56	33	11		11	21	33	40	51	75

TOP HYD LT-0+32

40.06	40.56	41.06	41.86	42.39	42.53	42.55	41.60	39.70	40.2	40.1
9.7	9.2	8.7	7.9	7.39	7.23	7.41	8.2	10.1	9.6	9.7
75	58	31	21	11		11	20	35	49	75

BT TWP 154CM

STA + π - ELEV.

949.74

$$-2+50 = 10+50$$

10+50

$$-2+05 = 10+95$$

Gutter Lt

10+05

$$-2+00 = 11+00$$

W edge ENT

11+00

$$-1+90 = 11+10$$

ENT Lt.

11+10

$$-1+80 = 11+20$$

E. EDGE ENT

11+20

$$-1+75 = 11+25$$

GUTTER LEFT

11+25

RG
DS
RJ
JC

LT

E

Nov 29 1973
PC 20° 40' RT

29

A1.1	A1.0	A0.5	A2.3	A2.7A	A2.88	A2.7A	A2.3	39.6	A0.3	A0.5
8.7	8.8	9.3	7.5	7.02	6.88	7.02	7.5	10.2	9.5	9.3
57	42	30	20	11		11	20	34	49	75
BT	BT		BT							

A1.8	A1.8	A1.9	A1.3A	A3.1	A3.4A	A3.38	A3.6	A3.1	A0.9	A1.1	A0.8
8.0	8.0	7.9	8.42	6.7	6.32	6.38	6.40	6.7	9.4	8.7	9.0
75	63	41	32	21	11		11	21	36	48	75
FL15"CM											

A1.8	A1.8	A2.6	A3.2	A3.53	A3.5A	A3.45	A3.1	A0.9	A1.1	A0.8
8.0	8.0	7.2	6.6	6.23	6.22	6.31	6.7	9.4	8.7	9.0
75	63	34	21	11		11	21	36	48	75

0	A0.8	A1.3	A0.2	A1.3	A3.2	A3.6A	A3.72	A3.70	A3.5	A2.8	A2.3	A2.0
9.1	8.5	9.6	8.5	6.6	6.12	6.64	6.06	6.3	7.0	7.5	7.8	
75	65	48	39	30	21	11		11	20	29	47	75

0	A1.6	A0.4	A1.4	A3.5	A3.4	A3.90	A3.75	A3.92	A2.5	A3.0	A2.8	A2.5	A2.3
8.8	8.2	9.4	8.4	6.3	6.4	5.86	6.01	5.84	6.3	6.8	7.0	7.3	7.5
75	48	41	30	23	21	11		11	20	25	33	49	75

A2.8	A2.4	A2.2	A1.7	A3.5	A3.72	A3.90	A3.75	A3.5	A3.7	A1.5	A0.5	A1.7	A1.1
7.0	7.4	7.6	8.59	6.3	6.04	5.86	6.01	6.3	6.1	8.3	9.3	8.1	8.7
75	63	40	36	31	21	11		11	21	23	30	41	48

BLDG

15"
C.M

STA + T - ELEV.

949.76

$$-1+50 = 11+50$$

$$-1+34 = 11+66$$

7.37 942.39

$$-1+00 = 12+00$$

T.P. 4.83 951.65 2.94 946.82 (946.82)

$$-0+72 = 12+28$$

$$-0+60 = 12+40$$

gutter left

$$-0+45 = 12+55$$

& drive

LT

E

RT

30

^{A2.9} ^{A2.6} ^{A2.3} ^{A2.0} ^{A3.1} ^{AA.0} ^{AA.30} ^{AA.40} ^{AA.26} ^{A2.7} ^{AA.0} ^{AA.8} ^{A1.7} ^{A1.6}
 6.9 7.2 7.5 7.8 6.7 5.8 5.46 5.36 5.50 6.1 5.8 9.0 8.1 8.2
 63 49 34 32 27 20 11 11 20 24 36 48 75
 BLOC

TOP M.H 28' LT.

^{A2.9} ^{A2.7} ^{A2.8} ^{AA.7} ^{A5.11} ^{A5.19} ^{A5.00} ^{AA.4} ^{AA.6} ^{A2.3} ^{A1.8} ^{A2.5} ^{A2.6}
 6.9 7.1 7.0 5.1 4.65 4.57 4.76 5.4 5.2 7.5 8.0 7.3 7.27
 63 48 30 22 11 11 22 25 34 41 49 62 63

B/Hg

TOP MONT 0+00

^{A2.95} ^{A2.37} ^{A2.36} ^{AA.98} ^{A5.03} ^{A5.52} ^{A5.5A} ^{A5.47} ^{A4.96} ^{A3.73} ^{A2.50} ^{A2.14} ^{A2.9}
 SW 8.70 8.28 8.29 6.67 6.62 6.13 6.11 6.18 6.69 7.92 7.15 9.51 8.7
 63 38 32 25 23 11 11 22 29 35 42 75

^{A2.9} ^{A2.326} ^{AA.00} ^{A3.17} ^{AA.98} ^{A5.75} ^{A5.76} ^{A5.64} ^{A5.3} ^{A3.9} ^{A2.6} ^{A3.4} ^{A3.0} ^{A2.3}
 SW 8.73 8.29 7.65 8.48 6.67 5.90 5.89 6.01 6.4 7.8 9.1 8.3 8.7 8.4
 59 45 36 30 24 11 11 22 29 37 41 47 75

^{A2.6} ^{A2.8} ^{A3.3} ^{AA.5} ^{A5.5} ^{A5.98} ^{A6.01}
 9.1 8.9 8.4 7.2 6.2 5.67 5.64
 100 72 57 39 22 11

STA	+	π	-	ELEV.
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		9.51.65		
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-0+29	=	12+71		
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-0+03	=	12+97		
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0+02				
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+09				
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		5.26	946.39	
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+21				
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		5.47	946.18	
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+28				
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		5.41	946.24	
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LT

£

RT

31.

42.9	43.2	AA.0	AA.7	43.86	FL	45.95	46.20	46.29	46.17	46.0	AA.5	43.6	AA.5	AA.2
2.8	2.5	7.7	7.0	7.79	6.3	5.70	5.45	5.36	5.48	5.7	7.2	8.1	7.2	7.5
5	63	51	57	31	25	18	11	11	22	30	34	47	75	

43.9	43.6	45.1	44.8	46.3	46.3	46.71	46.77	46.65	46.5	45.5	45.9	48.5	49.8	50.2
2.8	7.1	6.3	6.9	5.4	5.4	4.94	4.88	5.00	5.2	6.2	5.8	3.2	1.9	1.5
65	53	39	30	24	20	11	11	21	28	39	47	54	75	

49.2	49.1	49.2	46.8	44.8	44.7	46.5	46.19	46.86	46.73	46.5	45.7	45.6	47.1	50.8	50.3
2.5	2.6	3.5	4.9	6.9	7.0	5.2	4.86	4.79	4.92	5.2	6.0	6.1	4.6	0.9	0.4
75	63	51	44	54	29	22	11	11	22	29	38	44	54	75	

TOP MH 23.0 RT

TOP MH 28.0 RT

TOP MH 28.0 RT

STA + π -

951.65

0+50

1+00

1+40

TP 2.43 953.18 0.90 950.75

1+40

FN ✓

LT

E

RT

32.

[•]47.3 [•]47.9 [•]47.2 [•]45.3 [•]45.6 [•]47.0 [•]47.43 [•]47.55 [•]47.47 [•]46.7 [•]46.7 [•]46.0 [•]46.0 [•]51.3 [•]51.3
 4.4 3.8 4.5 6.4 6.1 4.7 4.22 4.10 4.18 5.0 5.0 5.7 5.7 0.4 0.4
 75 61 49 34 27 22 11 11 21 25 32 37 56 - 75

[•]47.6 [•]48.3 [•]47.8 [•]46.7 [•]46.2 [•]47.7 [•]48.02 [•]48.14 [•]48.05 [•]47.7 [•]46.5 [•]46.3 [•]51.1 [•]51.1
 4.1 3.4 3.9 5.0 5.5 4.0 3.62 3.51 3.60 4.3 5.2 5.4 0.3 0.3
 75 61 48 38 30 22 11 11 22 30 36 52 - 75

[•]48.60 [•]48.19 [•]48.0 [•]47.1 [•]6.8 [•]51.6 [•]51.8 [•]51.1
 3.05 3.16 3.7 4.6 4.9 0.1 +0.1 +0.1
 11 22 31 36 50 51 75

TOP POST 0+90

[•]47.7 [•]47.2 [•]46.5 [•]46.7 [•]48.3 [•]48.50 [•]48.59
 5.5 6.0 6.7 6.5 4.9 4.68 4.59
 60 41 33 32 22 11

[•]5.9
 75

[•]47.3

[•]5.9
 75

STA + π - ELEV.

953.18 0.21

1+54 ENT LT.

✓

+66

TP 4.06 957.04 0.21 952.97 (952.98)

2+00

2+50

LT

Z

RT

33

47.68	48.18	48.28	48.28	48.48	48.69	48.75	48.61	48.18	47.18	46.98	52.48	52.58
5.5	5.0	4.9	4.9	4.7	4.49	4.43	4.57	5.0	6.0	6.2	0.7	0.6
100	75	57	39	21	11		11	23	31	36	54	68

51.88
5
1.3
75

48.28	48.08	47.28	47.08	46.68	48.58	48.79	48.87	48.75	48.38	47.08	53.18	53.18	52.38
4.9	5.1	5.9	6.1	6.5	4.6	4.39	4.31	4.43	4.8	6.1	0.0	0.0	0.8
75	56	39	32	21	21	11		11	23	36	56	68	75

Top Hyd Rt sta 2+38

49.74	47.64	46.64	48.74	49.06	49.25	49.65	48.69	47.34	47.94	54.54	54.54	53.64
8.3	9.4	10.4	8.3	7.98	7.29	7.39	8.4	9.7	9.6	2.5	2.5	3.4
75	46	29	20	11		11	22	32	35	57	68	75

49.64	48.64	47.04	47.54	48.74	49.14	49.53	49.42	49.04	48.04	48.04	55.94	55.94
7.4	8.4	10.0	9.5	8.3	7.60	7.51	7.62	8.0	9.0	9.0	1.1	1.1
75	50	31	26	22	11		11	22	30	34	58	75

STA + π - ELEV

959.04

2+81

7.55 949.49

3+00

3+54

3+63 E of ENTRANCE LT.

✓

3+72

LT

8

RT

34

So. rim M.H. RT 23'

9.54	8.64	8.14	7.24	8.24	9.70	9.82	9.71	9.14	9.44	5.54	5.74
7.5	8.4	8.9	9.8	8.1	7.34	7.22	7.33	7.9	8.4	0.5	0.3
75	61	45	30	22	11		11	22	30-32	69	75

9.84	9.64	9.89	9.54	9.04	9.84	9.94	9.86	9.96	9.89	9.54	9.64	9.74	5.74	5.04	5.34
9.2	9.4	9.2	9.5	9.0	7.2	7.1	7.8	7.08	7.15	7.5	8.4	7.3	1.3	1.0	1.7
75	53	38	32	32	24	19	11		11	21	29	37	55	63	67

Top 15" CM	9.54	9.34	9.54	9.34	9.93	9.89	9.92	9.74	9.84	9.04	5.34	5.74	5.34
	2.5	8.7	8.5	7.7	7.11	7.05	7.12	7.3	8.2	8.0	1.7	1.3	3.2
	100	80	45	28	11		11	21	28	35	56	61	72

52.94
4.1
75 Bit.

9.04	9.04	9.14	9.64	9.14	9.84	5.04	9.92	9.94	9.94	9.64	9.84	9.94	5.54	5.34	5.24
9.0	9.0	8.9	9.4	8.9	7.2	7.0	7.12	7.05	7.10	7.4	8.2	8.1	1.6	1.7	4.1
75	57	39	31	31	25	22	11		11	22	30	36	58	64	72-75

Top
15"
CM

STA

+

PI

-

ELEV.

957.04

4+00

4+50

T.P.

4.50

954.03

7.51

949.53

5+00

5+50

+77

4.36 949.67

+92

4.95

LT

20

RT

35

48.54	48.74	49.26 ³⁴	49.09	49.84	49.93	50.04	49.96	49.84	48.94	48.84	51.74	52.24	52.64
8.5	8.3	7.78	10.72	7.11	7.00	7.08	7.2	8.1	8.2	2.3	3.8	4.4	
75	53	36	26	22	11	11	22	31	36	50	69	75	

Bit

48.44	48.84	49.14	49.74	50.00	50.10	50.03	50.02 ³⁴	49.04	49.04	52.44	52.04	51.94
8.6	8.2	7.97	7.3	7.04	6.94	7.01	7.2	8.0	8.0	4.6	5.0	5.1
75	50	29	23	11		11	24	33	38	61	70	75

Bit

NORTH RIM of M.H. 22' LT. 4+80

47.93	48.43	48.83	49.33	49.88	50.02	49.90	49.63	49.13	50.83	51.03
6.1	5.6	5.2	4.7	4.15	4.01	4.13	4.4	4.9	3.2	3.0
75	56	33	23	11		11	24	40	58	75

47.93	48.33	48.93	49.43	49.74	49.93	49.77	49.43	49.13	49.93	50.23
6.1	5.7	5.1	4.6	4.29	4.20	4.26	4.6	4.9	4.1	3.8
75	52	31	23	11		11	23	41	60	75

No. rim MH RT 27'

Top of CONC. HH COVER 32' RT.

STA + π - ELEV.

954.03

6+00

T.P. 5.88 954.56 5.35 948.68

BM 3.67 954.53 3.67 950.89 (950.86)

6+02

6.00 948.53

+03 = GUTTER RT

+28(RT)

+32 = $\frac{1}{2}$ WALNUT ST

+56 = GUTTER RT.

+60

5.82

948.71

LT

4 DEC, 1973
RT

36

17.93	18.63	18.83	19.23	19.43	19.56	19.52	19.11	18.93	19.33	19.43	19.53	
6.1	5.4	5.2	4.8	4.6	4.47	4.51	4.92	5.10	4.7	4.6	4.5	
75	50	23	22	11		11	26	39	39	52	75	
							B.T	B.C T.C.				

No. Cor. CB GRATE S.W. RAD. WALNUT + C.
TOP HYD. LT STA 9+10

FL CB 44.0 RT

17.93	18.63	19.23	19.44	19.54	19.48	18.93	19.43	18.98	18.59	19.15
6.6	5.9	5.3	5.09	4.99	5.05	5.6	5.10	5.55	4.94	5.3
75	50	23	11		11	40	60	60	100	100
							TC	G	TC	G

17.63	18.43	18.93	19.28	19.41	19.30	19.33	19.53	19.63	19.73
6.9	6.1	5.6	5.25	5.12	5.23	5.2	5.0	4.9	4.8
75	50	26	11		11	50	100	150	200

17.03	17.23	18.33	18.73	19.11	19.22	19.15	18.93	19.38	18.93	19.49	19.00
7.5	7.3	6.2	5.8	5.42	5.31	5.38	5.6	5.15	5.60	5.04	5.53
75	50	42	25	11		11	41	57	57	100	100
							TC	G	TC	G	

FL CB 44.0' RT

STA	+	π	-	ELEV.
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		954.53		
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6+65 = DITCH LT

7+00

+ 10

8.75

945.78

+11

6.43

948.10

+22

6.32

948.21

+34

6.42

948.11

LT

4 DEC, 1973

RT

37

46.43	46.23	46.53	48.83	49.03	49.14	49.03	48.73	49.23	49.33	49.43
8.1	8.3	8.0	5.7	5.48	5.39	5.50	5.8	5.30	5.2	5.1
75	50	33	23	11		11	38	38	50	75
							G	TC		
46.53	46.33	49.43	48.82	48.87	48.78		48.63	48.23	49.53	
8.0	8.2	6.1	5.71	5.66	5.75	5.9	6.3	5.0		
35	31	24	11		11	24	39	75		
FE										

FL SD 31' Lt

FL SD 44.0 Rt

MH 28' Rt

MH 32' Rt

STA	+	π	-	ELEV.
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		954.53		
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7+50				
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+81				
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		6.14	948.39	
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8+00				
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+50				
-----	--	--	--	--

9+00				
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BM				
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	6,39			
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		957.25		
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			3.67	
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				950.86
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				950.86
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LT

4

4 DEC. 1973 38
RT.

47.03	46.63	48.23	48.78	48.82	48.67	48.23	47.83	48.63	49.83
7.5	7.9	6.3	5.75	5.71	5.86	6.2	6.7	5.9	4.7
37	31	23	11		11	23	39	50	75
FE									

MH 23.0 RT.

47.33	47.13	48.33	48.63	48.69	48.63	48.43	47.93	50.13
7.2	7.4	6.2	5.88	5.84	5.90	6.1	6.6	4.4
37	28	24	11		11	23	33	75
FE								

47.93	47.23	48.43	48.72	48.80	48.73	48.43	48.23	50.73
6.6	7.3	6.1	5.81	5.73	5.80	6.1	6.3	3.8
37	30	25	11		11	23	35	75
FE								

48.33	47.83	48.63	48.87	48.96	48.86	48.33	47.93	48.93	50.73
6.2	6.7	5.9	5.66	5.57	5.67	6.2	6.6	5.6	3.8
37	31	25	11		11	24	34	44	75
FE									

TOP HYP. LT STA. 9+10

STA + π - ELEV.

957.25

9+12

11.13 946.12

+50

10+00

+42

9.30 947.95

+50

+76 = $\neq$ EUSTIS ST.

LT

E

6 DEC 1973
SUNNY
10° RT

39

FL 18" SCP 31.0 LT

19.55	19.85	19.95	19.95	19.13	19.25	19.05	18.75	18.05	18.85	19.55	19.85
7.7	7.8	7.8	8.3	8.12	8.00	8.20	8.5	9.2	8.4	7.7	6.4
75	50	39	22	11		11	21	31	42	50	75

19.95	19.85	19.65	19.35	19.98	19.63	19.93	19.15	18.35	19.25	19.95
7.3	7.4	7.6	7.9	7.77	7.62	7.92	8.1	8.9	8.0	7.3
75	50	37	25	11		11	22	34	50	75

FL SD 43.0 RT

50.25	50.35	49.95	50.01	50.11	49.83	49.55	48.95	49.35
7.0	6.9	7.3	7.24	7.14	7.42	7.7	8.3	7.9
75	50	26	11		11	31	50	75

50.45	50.53	50.30	50.43	50.21	49.75	49.65	49.65	49.55
6.8	6.7	6.95	6.82	7.04	7.5	7.6	7.6	7.7
75	39	11		11	32	50	75	100

STA	+	π	-	ELEV.
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		957.25		
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+91				
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	7.39	949.86		
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11+00				
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BM	7.27	959.33	5.23	952.02	952.06
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BM			1.89	957.44	957.43
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11+50	ENT. LT & RT			
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12+00				
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+50	ENT RT			
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LT

E

6 DEC. 1973

40

RT

FL 50 44.0 RT

50.85	50.85	50.67	50.83	50.63	50.25	49.25	49.35
6.4	6.4	6.58	6.42	6.62	7.0	8.0	7.9
75	36	11		11	39	50	75

TOP HYD RT STA 11+00

TOP HYD LT STA 15+10

50.93	50.94	51.10	51.31	51.35	51.39	51.48	51.16	50.83	51.13	51.13
8.4	8.39	8.23	8.02	7.98	7.94	7.85	8.17	8.5	8.2	8.2
125	100	75	50	27	11		11	28	50	75

51.44	51.67	51.89	52.07	52.21	52.11	51.73	52.23	52.03	51.73
7.89	7.66	7.44	7.26	7.12	7.22	7.6	7.1	7.3	7.6
75	50	27	11		11	23	33	50	75

51.77	52.14	52.44	52.84	52.92	52.77	52.43	52.93	53.03	52.93
7.56	7.19	6.89	6.49	6.41	6.56	6.9	6.4	6.3	6.4
75	50	35	11		11	21	35	50	75

STA	+	π	-	ELEV.
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		959.33		
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12+68 = $\angle$ ENT. LT				
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13+00				
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+50				
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+86				
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14+00				
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BM	2.85	960.28	1.89	957.44	957.43
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LT

6 DEC. 1973 41
RT

50.53	51.16	51.71	52.28	52.52	53.06	53.15	52.99	52.63	53.23	53.23	53.33
8.4	8.17	7.62	7.05	6.81	6.27	6.18	6.34	6.7	6.1	6.1	6.0
125	100	75	50	35	11		11	23	36	50	75

53.15	52.47	52.95	53.51	53.65	53.49	53.33	53.53	53.83	53.83
6.18	6.86	6.38	5.82	5.68	5.84	6.0	5.8	5.5	5.5
75	50	34	11		11	25	36	50	75

51.33	51.73	53.83	53.74	54.18	54.33	54.21	54.13	54.23	54.43	55.05	54.5
8.0	7.6	5.5	5.59	5.15	5.00	5.12	5.2	5.1	4.9	4.28	4.8
75	45	26	21	11		11	26	36	52	52	75

Island

51.43	51.33	51.73	50.03	54.13	54.59	54.67	54.76	54.55	54.53	54.53	54.63	55.03	54.73
7.9	8.0	7.6	9.30	5.2	4.74	4.66	4.57	4.78	4.8	4.8	4.7	4.36	4.6
75	50	37	32	25	18	11		11	26	36	52	52	75

FL-18" SCP

Island

52.03	54.13	54.83	54.91	54.93	54.80	54.73	54.63	54.73	55.11	54.83
7.3	5.2	4.5	4.42	4.40	4.53	4.6	4.7	4.6	4.22	4.5
36	24	18	11		11	26	36	52	52	75

FE

Island

TOP HND. LT STA 15+10

STA + π - ELEV.

960.28

14+50

15+00 = ENT. RT

+40 = ENT. RT

+50

16+00

+50

LT

6 DEC. 1973

42

RT

	5 ^{2.98}	5 ^{5.16}	5 ^{5.16}	5 ^{5.17}	5 ^{5.20}	5 ^{5.08}	5 ^{5.08}	5 ^{5.08}
	7.8	5.12	5.12	5.00	5.08	5.2	5.2	5.2
	37	17	11		11	28	50	75
FE								
5 ^{2.88}	5 ^{4.68}	5 ^{5.26}	5 ^{5.30}	5 ^{5.43}	5 ^{5.33}	5 ^{5.08}	5 ^{5.08}	5 ^{4.78}
7.4	5.6	5.02	4.98	4.85	4.95	5.2	5.2	5.5
37	25	17	11		11	22	50	75
FE								
5 ^{3.28}	5 ^{5.08}	5 ^{5.40}	5 ^{5.40}	5 ^{5.47}	5 ^{5.26}	5 ^{4.57}	5 ^{4.68}	5 ^{2.98}
7.0	5.2	4.88	4.88	4.81	5.01	5.7	5.6	7.3
37	23	17	11		11	31	50	75
FE								
5 ^{3.28}	5 ^{5.18}	5 ^{5.40}	5 ^{5.38}	5 ^{5.43}	5 ^{5.26}	5 ^{4.45}	5 ^{4.28}	5 ^{3.48}
7.0	5.1	4.88	4.90	4.85	5.02	6.0	6.8	7.4
37	23	17	11		11	31	50	75
FE								
5 ^{2.98}	5 ^{4.78}	5 ^{5.05}	5 ^{5.03}	5 ^{5.12}	5 ^{4.93}	5 ^{4.38}	5 ^{3.28}	5 ^{3.58}
7.3	5.5	5.23	5.25	5.16	5.35	5.9	7.0	6.7
37	24	17	11		11	26	35	42
FE								
5 ^{1.98}	5 ^{4.28}	5 ^{4.53}	5 ^{4.51}	5 ^{4.66}	5 ^{4.47}	5 ^{3.98}	5 ^{2.88}	5 ^{2.78}
8.3	6.0	5.75	5.77	5.62	5.81	6.3	7.4	7.5
37	22	15	11		11	26	33	42
FE								
	5 ^{1.58}	5 ^{1.38}	5 ^{1.38}	5 ^{1.38}	5 ^{1.38}	5 ^{1.38}	5 ^{1.38}	5 ^{1.38}
	8.7	8.9	9.4					
	44	50	75					

STA	+	π	-	ELEV.
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		960.28		
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17+00				
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+50				
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18+00				
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BM	1.76	954.03	7.98	952.30	952.27
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18+26					
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+50					
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LT

E

6 DEC 1973

43

RT

50.88	53.08	53.81	53.87	53.75	53.28	50.98	50.48	50.28
9.4	7.2	6.47	6.41	6.53	7.0	9.3	9.8	10.0
37	25	11		11	31	37	50	75
FE								

49.68	52.28	52.79	52.94	52.79	51.98	50.98	50.18	49.98	49.98
10.6	8.0	7.49	7.34	7.49	8.3	9.3	10.1	10.3	10.3
37	22	11		11	28	35	39	50	75
FE									

48.98	51.38	51.84	51.91	51.81	51.28	49.88	49.68	49.78
11.8	8.9	8.44	8.37	8.47	9.0	10.4	10.6	10.5
37	23	11		11	26	35	50	75
FE								

TOP HYD. LT STA 18+60

48.03	48.33	51.33	50.73	51.19	51.31	51.21	51.03	49.13	49.73	49.63
6.0	5.7	2.7	3.3	2.84	2.72	2.82	3.0	4.9	4.3	4.4
37	33	23	21	11		11	25	36	50	75
FE										

47.63	49.63	50.23	50.73	50.81	50.71	49.93	49.29	49.93
6.4	4.4	3.8	3.30	3.22	3.32	4.1	4.79	4.1
37	26	22	11		11	35	47	75
FE						FE	SD	

STA	+	π	-	ELEV.
-----	---	-------	---	-------

		954.03		
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18+90	=	$\frac{1}{2}$	ENT	RT
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19+00				
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+18				
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+50				
-----	--	--	--	--

20+00				
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+42				
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		8.09		
--	--	------	--	--

			945.94	
--	--	--	--------	--

LT

E

6 DEC 1973

RT

44

16.33	19.93	19.79	19.95	19.88	19.83	19.83	50.03
7.7	4.6	4.24	4.08	4.15	4.2	4.2	4.0
37	21	11	11	33	50	75	
FE							

16.93	19.33	19.66	19.70	19.63	19.53	19.63	19.93
7.6	4.7	4.37	4.33	4.40	4.5	4.4	4.1
37	21	11	11	35	50	75	
FE							

16.23	19.03	19.36	19.39	19.23	18.93	18.73	19.73	18.89	19.43	19.83
7.8	5.0	4.67	4.64	4.80	5.1	5.3	9.30	5.16	4.6	4.2
37	22	11	11	29	34	34	35	50	75	
FE							FL 24" CM	TOP WALL		

15.63	18.33	18.66	18.70	18.60	17.63	16.23	18.47	19.03	19.43
8.4	5.7	5.37	5.33	5.43	6.4	7.8	5.56	5.0	4.6
37	23	11	11	27	34	35	50	75	
FE							TOP WALL		

14.53	17.33	17.66	17.72	17.60	16.83	14.93	18.04	18.63	18.93
9.5	6.7	6.37	6.31	6.43	7.2	9.1	5.99	5.4	5.1
37	22	11	11	26	34	35	50	75	
FE							TOP WALL		

TOP MH 27' RT

STA

+

π

-

ELEV.

954.03

20+50

+77

21+00

$\pm$ ENT RT

BM

8.24

945.79

(945.78)

LT

E

6 DEC. 1973

45

RT

13.73	16.03	16.52	16.69	16.56	16.13	14.43	17.5	18.13	18.53
10.3	8.0	7.51	7.34	7.47	7.9	9.6	6.28	5.9	5.5
37	24	11		11	27	34	35	50	75
FE							TOPWALL		

13.73	15.13	15.97	16.12	15.99	16.23	13.67	16.75	17.33	18.03
10.7	8.6	8.06	7.91	8.04	7.8	10.36	7.28	6.7	6.0
37	25	11		11	34	35	35	50	75
FE						FL/RT	TOPWALL		

13.23	15.03	15.16	15.58	15.51	16.33	17.03	17.63
10.8	9.0	8.57	8.45	8.52	7.5	7.0	6.4
37	23	11		11	35	50	75
FE							

TOP HYD. RT STA 22+10

SEE PAGES 46-50 FOR

ADDITIONAL X-SECTIONS

STA	+	π	-	ELEV.
BM	3.42	954.28		950.86

7+00

+50

8+00

+50

9+00

BM	7.23	959.29	2.25	952.03	952.06
----	------	--------	------	--------	--------

BM	1.86	959.29	1.86	957.43	957.43
----	------	--------	------	--------	--------

LT

7 DEC, 1973
SUNNY 10° RT

46.

TOP HYD LT STA 9+10

19.08

18.88

5.2

5.4

75

51

19.28

18.68

5.1

5.6

75

51

19.08

18.78

5.2

5.5

75

47

19.08

18.58

5.2

5.7

75

45

18.78

18.68

5.5

5.6

75

45

TOP HYD. RT STA 11+00

TOP HYD. LT STA 15+10

STA	+	π	-	ELEV
-----	---	-------	---	------

		959.29		
--	--	--------	--	--

14+00				
-------	--	--	--	--

+50				
-----	--	--	--	--

15+00				
-------	--	--	--	--

+40				
-----	--	--	--	--

+50				
-----	--	--	--	--

16+00				
-------	--	--	--	--

BM	1.57	959.00	1.86	957.43 (957.43)
----	------	--------	------	-----------------

LT

7 DEC 1973
RT

47

19.99

51.39

9.3

7.9

75

50

50.99

51.79

8.3

7.5

75

50

47.69

52.79

52.99

11.6

6.5

6.3

75

62

50

19.09

52.79

10.2

6.5

67

59

48.29

52.89

11.0

6.4

67

57

48.69

52.59

10.6

6.7

70

60

TOP HYD LT STA 15+10

STA + π - ELEV

959.00

BM

6.72 952.28 (952.27)

14+50

17+00

+50

18+00

+26

LT

E

7 DEC, 1973

RT

48

TOP HYD LT STA 18+60

50.70

51.80

8.3

7.2

75

50

50.00

51.00

9.0

8.0

75

50

48.70

49.30

10.3

9.7

75

50

48.30

48.30

10.7

10.7

75

50

53.60

47.90

47.80

5.4

11.1

11.2

75

65

50

STA + π - ELEV.

959.00

18+50

+90

19+00

+18

+50

20+00

BM

1.48

953.75

6.72

952.28

952.27

LT

7 DEC. 1973
RT 49

55.20 17.20
3.8 11.8
70 55
TOP EMB.

55.30 17.10
3.7 11.9
61 41
TOP EMB.

55.50 16.80
3.5 12.2
58 51
TOP EMB.

55.70 17.20
3.3 11.8
56 40
TOP EMB.

55.80 16.50
3.2 12.5
58 39
TOP EMB.

55.00 16.90
4.0 12.1
70 50
TOP EMB.

TOP HYD LT STA 18+60

STA + π - ELEV.

953.75

BM 7.98 953.76 7.98 945.77 (945.78)

20+50

+77

21+00

BM 2.95 948.73 7.98 945.78 (945.78)

21+50

LT

7 DEC. 1973

RT

50

TOP HYD. LT STA 22+10

 $\begin{matrix} \cdot & \cdot \\ 45.76 & 46.46 \end{matrix}$
 $\begin{matrix} 8.0 & 7.3 \\ 75 & 45 \end{matrix}$
 $\begin{matrix} \cdot & \cdot \\ 45.36 & 45.36 \end{matrix}$
 $\begin{matrix} 8.4 & 8.4 \\ 75 & 44 \end{matrix}$
 $\begin{matrix} \cdot & \cdot \\ 44.96 & 44.66 \end{matrix}$
 $\begin{matrix} 8.8 & 9.1 \\ 75 & 44 \end{matrix}$

TOP HYD. LT STA 22+10

$\begin{matrix} \cdot & \cdot \\ 45.73 & 44.63 \end{matrix}$	$\begin{matrix} \cdot & \cdot \\ 43.33 & 41.93 \end{matrix}$	$\begin{matrix} \cdot & \cdot \\ 42.23 & 43.93 \end{matrix}$	$\begin{matrix} \cdot & \cdot \\ 44.29 & 44.37 \end{matrix}$	$\begin{matrix} \cdot & \cdot \\ 44.27 & 43.63 \end{matrix}$	$\begin{matrix} \cdot & \cdot \\ 43.43 & 44.43 \end{matrix}$	$\begin{matrix} \cdot & \cdot \\ 44.73 & 46.03 \end{matrix}$	$\begin{matrix} \cdot & \cdot \\ 47.13 & \end{matrix}$
3.0 4.1 5.4 6.8 6.5 4.8 4.49 4.36 4.46 5.1 5.3 4.3 4.0 2.7 1.6							
75 50 43 37 33 25 11 11 20 26 32 35 42 75							
FE						FE	

STA

+

T

-

ELEV.

948.73

22+00

✓

+50

✓

+76

✓

LT

7 DEC. 1973
RT

51

A1.73	A1.13	A3.03	A3.27	A3.44	A3.32	A2.83	A3.23	A4.53	A4.93
7.0	7.6	5.7	5.46	5.29	5.41	5.9	5.5	4.2	3.8
41	37	23	11		11	22	35	42	50
	FE						FE		

A5.13	A6.33
3.6	2.4
50	75

A5.13
3.3
75

A1.93	A0.73	A1.73	A2.11	A2.29	A2.15	A2.03	A1.03	A2.23
6.8	8.0	7.0	6.62	6.49	6.58	6.7	7.7	6.5
41	36	23	11		11	20	25	35
								FE

A6.53	A8.33	A1.03
2.2	0.4	+2.3
52	58	63

TOP EMB.

A2.03	A1.93
6.7	6.8
75	50

A1.03	A9.53	A0.93	A1.35	A1.49	A1.37	A1.23	A0.23	A9.05
7.7	9.2	7.8	7.38	7.24	7.36	7.5	8.5	9.68
37	30	23	11		11	20	25	33
FE								FL 15" SLP

A3.93	A6.13	A8.73	A1.13
4.8	2.6	0.0	+2.4
41	47	52	59
			TOP EMB

A1.73	A1.23	A1.03	A1.53
7.0	7.5	7.7	7.2
75	50	35	33
		FE	

STA	+	π	-	ELEV.
-----	---	-------	---	-------

		948.73		
--	--	--------	--	--

22+98				
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		8.39	940.34	
--	--	------	--------	--

23+00				
-------	--	--	--	--

✓				
---	--	--	--	--

+50				
-----	--	--	--	--

✓				
---	--	--	--	--

LT

E

7 DEC. 1973

RT

52

TOP MH 23' RT

48.73	40.33	38.93	40.33	40.78	40.89	40.78	40.63	39.53	39.53	41.02
0.0	8.4	9.8	8.4	7.95	7.84	7.95	8.1	9.2	9.2	7.7
50	37	28	24	11		11	20	26	35	50

FE

50.33

+ 1.6

55

TOP EMB.

41.03

7.7

75

48.73	37.03	36.43	38.93	39.30	39.46	39.25	39.33	38.53	38.13	39.33
0.0	11.7	12.3	9.8	9.43	9.27	9.48	9.4	10.2	10.6	9.4
50	37	31	24	11		11	20	26	35	50

FE

FE

49.73

+ 1.0

61

TOP EMB.

39.83

8.9

75

STA	+	π	-	ELEV.
-----	---	-------	---	-------

		948.73		
--	--	--------	--	--

24+00				
-------	--	--	--	--

✓				
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BM	3.64	940.22	12.13	936.60 (936.58)
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24+48				
-------	--	--	--	--

✓				
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LT

E

7 DEC

1973

RT

53

33.53	34.33	37.53	37.77	37.93	37.82	37.73	37.03	37.03
15.2	14.4	11.2	10.96	10.80	10.91	11.0	11.7	11.7
50	37	24	11		11	20	27	35
	FE							FE

39.23	46.63					38.83	38.13	38.03
9.5	2.1					9.9	10.0	10.7
63	75					75	65	44

SPIKE IN ARC-LITE POLE N.W. CORE ENT LT 25+40

32.12	32.52	36.62	36.67	36.79	36.68	36.62	39.72	36.72
8.1	7.7	3.6	3.55	3.43	3.54	3.6	5.50	3.5
50	37	23	11		11	23	33	33
	FE						FL 12" CIP	

32.02						37.92	37.22	36.82
8.2						2.3	3.0	3.4
75						75	50	37

STA + K - ELEV.

940.22

24462 = ~~E~~ ENT RT.

+ 82

✓

25400

✓

BM 2.38 937.92 4.69 935.53 (935.54)

LT

7 DEC. 1973 54
RT.

31.72	31.62	32.02	36.32	36.42	36.60	36.47	36.62	37.02	37.52
8.5	8.6	8.2	3.9	3.80	3.62	3.75	3.6	3.2	2.7
75	50	37	24	11		11	35	50	75

FE

31.32	31.42	32.52	35.62	36.01	36.28	36.16	36.22	34.49	35.42
8.9	8.8	7.7	4.6	4.21	3.94	4.06	4.0	5.73	4.8
75	50	37	26	11		11	26	33	35

FE

12/2°C/P

36.92	36.72
3.3	3.5
75	50

30.82	31.42	31.62	35.52	35.93	36.01	35.90	36.02	35.02	35.32	36.22
9.4	8.8	8.6	4.7	4.29	4.15	4.32	4.2	5.2	4.9	4.0
75	50	37	26	11		11	23	26	34	35

FE

36.72	36.62
3.5	3.6
75	50

TOP HYD LT STA 28+25

STA + π - ELEV

937.92

25+08 = DITCH LT

+10

2.23 935.69

+19 = SHOULDER LT

+29 = ENT LT

+52 = W. TRACK SPUR LINE Profile

+57

LT

E

7 DEC 1973

RT

55

30.42	31.72	31.82	35.32	35.77	35.92	35.80	35.72	35.02	36.22	36.72	36.02
7.5	6.2	6.1	2.6	2.15	2.00	2.12	2.2	2.9	1.7	1.2	1.0
75	50	38	28	11		11	23	29	35	50	75

TOP MH 23.0' RT

35.02	35.22	35.42	35.64	35.80	35.72	35.52	36.12	36.42
2.9	2.7	2.5	2.28	2.12	2.20	2.4	1.8	1.5
75	50	28	11		11	34	50	75

33.92	34.37	34.96	35.30	35.38	35.59	35.70	35.68	35.42	35.52	34.82
4.00	3.55	2.96	2.62	2.54	2.33	2.22	2.24	2.5	2.4	3.1
200	150	100	50	33	11		11	26	50	75

33.67	33.99	34.49	35.07	35.52	35.39	33.98	34.07
4.25	3.93	3.43	2.85	2.40	2.53	3.94	3.85
200	150	100	50		50	100	200

34.42	34.82	35.12	35.42	35.50	35.57	35.12	34.72	34.22
3.5	3.1	2.8	2.50	2.42	2.35	2.8	3.2	3.7
75	50	36	11		11	27	50	75

STA + π - ELEV.

937.92

25+62

+75

+81

26+00

+18

+28

LT

7 DEC. 1973

56

RT

34.62	34.92	35.22	35.32	35.48	35.32	35.22	35.32	35.62	35.72	35.02
3.3	3.0	2.7	2.60	2.44	2.60	2.7	4.6	5.3	5.2	4.9
75	50	26	11		11	22	33	39	50	75

34.42	34.52	35.12	35.22	35.42	35.29	35.32	34.22	34.22	34.82	35.02
3.5	3.4	2.8	2.70	2.50	2.63	2.6	3.7	5.1	5.7	6.1
75	50	26	11		11	22	26	31	35	50

35.2	33.12	33.22	33.82	35.02	35.17	35.29	35.22	34.92	32.22	31.32	30.72
4.4	4.8	4.7	4.1	2.9	2.75	2.63	2.70	3.0	5.7	6.6	7.2
75	50	44	33	25	11		11	24	35	50	75

32.22	31.32	32.92	34.62	35.02	35.17	35.14	35.02	32.72	31.92	31.12	31.52
5.7	4.6	5.0	3.3	2.90	2.75	2.78	2.9	5.2	6.0	6.8	6.4
75	58	30	23	11		11	25	33	37	50	75

31.92	31.42	32.42	34.82	35.10	35.20	35.08	34.92	34.02	34.62
6.0	6.5	5.5	3.1	2.82	2.72	2.84	3.0	3.9	3.3
75	50	37	24	11		11	30	50	75

32.32	32.52	33.42	35.12	35.09	35.16	35.14	35.22	35.29	34.54
5.6	5.4	4.5	2.8	2.83	2.76	2.78	2.70	2.63	3.38
75	50	35	24	11		11	33	60	75

RAIL

STA + π - ELEV.

937.92

26+32

+34 = W. RAIL MAIN LINE *Note: RR Profile*

+40

+50

+67

+87

STA	+	π	-	ELEV.
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		937.92		
--	--	--------	--	--

27+00				
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BM	4.19	934.86	7.25	930.67	(930.67)
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BM	10.05	934.90	10.05	924.81	(924.85)
----	-------	--------	-------	--------	----------

27+50				
-------	--	--	--	--

28+00				
-------	--	--	--	--

+ 23			2.30	932.60
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+ 50				
------	--	--	--	--

LT

7 DEC 1973

RT

58.

27.42 30.87	32.02	33.22	34.42	34.13	34.90	34.69	34.02	31.22	30.62	30.42
10.5	5.9	4.7	3.5	3.19	3.02	3.23	3.9	6.7	7.3	7.5
75	50	40	24	11		11	22	37	50	75

STA 30+00

TOP HYD. LT STA 34+30

30.50	31.70	32.20	33.90	34.19	34.37	34.13	33.60	31.50	30.60	30.80	32.10
4.4	3.2	2.7	1.0	0.71	0.53	0.77	1.3	3.4	4.3	4.1	2.1
75	50	34	25	11		11	26	33	40	65	75

30.80	31.30	30.70	32.10	33.54	32.65	33.48	33.10	30.80	31.00	31.60	31.80
4.1	3.6	4.2	1.8	1.36	1.25	1.42	1.8	4.1	3.9	3.3	3.1
75	50	32	23	11		11	27	35	40	50	75

TOP MH 27' RT

30.90	30.40	30.90	32.60	32.85	32.94	32.80	32.60	30.90	31.50	31.50	31.50
4.0	4.5	4.5	2.3	2.05	1.96	2.10	2.3	4.0	3.4	3.4	3.4
75	50	36	23	11		11	29	35	40	50	75

STA	+	π	-	ELEV.
-----	---	-------	---	-------

		934.90		
--	--	--------	--	--

29+00 = W. END 12" SEP

✓

+21 = $\nless$ ENT RT (CONG.)

✓

+41 = E. END 12" SEP

✓

LT

E

10 DEC 1973

59.

RT

30.10

4.8

29

31.70

3.2

23

32.00

2.9

19

32.12

2.78

11

32.20

2.70

11

32.06

2.84

11

32.00

2.9

26

30.05

4.85

36

31.50

3.4

36

FL 12' SCP

30.00

4.9

50

30.00

4.9

75

31.70

3.2

75

31.30

3.6

41

FE

30.30

4.6

75

29.70

5.2

50

30.30

4.6

31

31.70

3.2

21

31.82

3.08

11

31.88

3.02

11

31.76

3.14

11

31.58

3.32

27

31.48

3.42

50

31.56

3.34

75

31.62

3.28

100

29.90

5.0

75

29.80

5.1

50

30.50

4.4

29

31.40

3.5

21

31.57

3.33

11

31.63

3.27

11

31.52

3.38

11

31.30

3.6

19

31.80

3.1

27

31.20

3.7

35

31.50

3.4

75

31.40

3.5

41

FE

28.88

6.02

35

FL 12' SCP

STA	+	T	-	ELEV.
-----	---	---	---	-------

		934.90		
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29+50				
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✓				
---	--	--	--	--

+82				
-----	--	--	--	--

		5.46	929.44	
--	--	------	--------	--

30+00 = 4		ENT. (LT.)		
----------------------	--	------------	--	--

✓				
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BM				
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8.85				
------	--	--	--	--

933.70				
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10.05				
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924.85				
--------	--	--	--	--

924.85				
--------	--	--	--	--

LT

E

10 DEC 1973

RT

60

29.90	29.60	30.50	31.30	31.44	31.53	31.41	31.20	31.60	29.50	31.90
5.0	5.3	4.4	3.6	3.46	3.37	3.49	3.7	3.3	5.4	4.0
75	50	29	19	11		11	20	27	35	39
										FE

31.40
3.5
75

TOP MH 31' RT

28.90	29.60	30.10	30.71	30.76	30.58	30.40	30.40	27.70
6.0	5.3	4.8	4.19	4.14	4.32	4.5	4.5	7.2
75	50	33	11		11	21	27	35-38

31.00
3.9
75

29.60
5.3
39
FE

TOP HYD. LT STA 34+30

STA	+	π	-	ELEV.
-----	---	-------	---	-------

		933.70		
--	--	--------	--	--

30+08				
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✓				
---	--	--	--	--

+15				
-----	--	--	--	--

✓				
---	--	--	--	--

+50				
-----	--	--	--	--

✓				
---	--	--	--	--

LT

10 DEC. 1973

RT.

61

$\begin{matrix} 29.20 \\ 4.5 \\ 75 \end{matrix}$
 $\begin{matrix} 29.30 \\ 4.4 \\ 50 \end{matrix}$
 $\begin{matrix} 29.90 \\ 3.8 \\ 28 \end{matrix}$
 $\begin{matrix} 30.53 \\ 3.17 \\ 11 \end{matrix}$
 $\begin{matrix} 30.60 \\ 3.10 \\ 11 \end{matrix}$
 $\begin{matrix} 30.44 \\ 3.26 \\ 11 \end{matrix}$
 $\begin{matrix} 30.10 \\ 3.6 \\ 29 \end{matrix}$
 $\begin{matrix} 30.36 \\ 7.34 \\ 35 \end{matrix}$
 $\begin{matrix} 30.30 \\ 3.4 \\ 42 \end{matrix}$
 $\begin{matrix} 30.50 \\ 3.2 \\ 50 \end{matrix}$

FL 15" FE

$\begin{matrix} 31.30 \\ 2.4 \\ 75 \end{matrix}$

$\begin{matrix} 28.30 \\ 5.4 \\ 75 \end{matrix}$
 $\begin{matrix} 28.50 \\ 5.2 \\ 50 \end{matrix}$
 $\begin{matrix} 28.90 \\ 4.8 \\ 28 \end{matrix}$
 $\begin{matrix} 29.20 \\ 3.5 \\ 22 \end{matrix}$
 $\begin{matrix} 30.44 \\ 3.26 \\ 11 \end{matrix}$
 $\begin{matrix} 30.50 \\ 3.20 \\ 11 \end{matrix}$
 $\begin{matrix} 30.35 \\ 3.35 \\ 11 \end{matrix}$
 $\begin{matrix} 30.10 \\ 3.6 \\ 21 \end{matrix}$
 $\begin{matrix} 30.50 \\ 3.2 \\ 41 \end{matrix}$
 $\begin{matrix} 31.30 \\ 2.4 \\ 75 \end{matrix}$

FE

$\begin{matrix} 27.50 \\ 6.2 \\ 75 \end{matrix}$
 $\begin{matrix} 28.00 \\ 5.7 \\ 50 \end{matrix}$
 $\begin{matrix} 28.00 \\ 5.7 \\ 29 \end{matrix}$
 $\begin{matrix} 29.60 \\ 4.1 \\ 23 \end{matrix}$
 $\begin{matrix} 29.95 \\ 3.75 \\ 11 \end{matrix}$
 $\begin{matrix} 30.01 \\ 3.69 \\ 11 \end{matrix}$
 $\begin{matrix} 29.90 \\ 3.80 \\ 11 \end{matrix}$
 $\begin{matrix} 29.94 \\ 3.76 \\ 34 \end{matrix}$
 $\begin{matrix} 30.46 \\ 3.24 \\ 50 \end{matrix}$
 $\begin{matrix} 31.10 \\ 2.6 \\ 75 \end{matrix}$

STA + π - ELEV

933.70

30+74 = $\nless$ ENT. RT. (ST. OIL RJ.)

31+00

+41

+47

+59 = $\nless$ ENT LT

+69

LT

10 DEC. 1973
RT

62

26.60	26.80	26.70	29.30	29.61	29.66	29.55	29.27	29.92	29.60
7.1	6.9	6.0	4.4	4.09	4.04	4.15	4.43	3.78	3.10
75	50	28	21	11		11	23	50	75

26.00	26.70	27.50	29.10	29.26	29.21	29.16	28.88	29.69	30.80
7.7	7.0	6.2	4.6	4.44	4.39	4.54	4.82	4.01	2.9
75	41	29	22	11		11	22	50	75

25.90	27.20	26.40	26.40	28.65	28.72	28.56	28.34	25.51	28.50	29.00
7.8	6.5	7.3	5.3	5.05	4.98	5.14	5.34	8.13	52.35	2.4
75	36	30	21	11		11	18	36	44	48

FL 15" FE

25.70	26.90	25.96	28.30	28.57	28.64	28.51	28.33	27.70	27.50	28.10	29.00
8.0	6.8	7.74	5.4	5.13	5.06	5.19	5.37	6.0	6.2	5.6	3.324
75	37	28	20	11		11	16	26	35	41	48

FL 12" CM FE

25.40	26.90	27.20	28.00	28.40	28.49	28.30	28.10	27.50	26.90	30.60	31.40
8.3	6.8	6.5	5.7	5.30	5.23	5.40	5.6	6.2	6.8	3.1	2.3
75	36	29	20	11		11	19	29	37	50	75

25.40	26.50	25.62	27.90	28.28	28.37	28.21	28.00	26.60	28.70	30.50	31.10
8.3	7.2	8.08	5.8	5.42	5.33	5.49	5.7	7.1	5.0	3.2	2.6
75	37	29	21	11		11	17	37	43	50	75

FL 12" CM

STA + π - ELEV.

933.70

32+00

+50

+68

+83 = ~~E~~ ENT, LT

+97

33+00

LT

F

10 DEC. 1973
RT

63

25.30	26.10	25.80	27.90	27.80	27.89	27.47	27.10	25.80	28.50	30.10	31.20
8.4	7.6	7.9	6.3	5.90	5.81	5.93	6.6	7.9	5.2	3.6	2.5
75	38	29	21	11	11	20	34	43	50	75	

25.50	25.90	25.10	26.90	27.05	27.14	26.97	26.90	24.80	27.60	30.10	31.00
8.2	7.8	8.6	6.8	6.65	6.56	6.73	7.3	8.9	6.1	3.6	2.7
75	37	30	21	11	11	21	34	43	50	75	

25.60	26.50	23.95	27.00	26.50	26.70	26.80	26.63	26.10	24.30	27.50	30.10	30.80
8.1	7.2	9.75	6.7	7.2	7.00	6.90	7.07	7.6	9.4	6.2	3.6	2.9
75	37	29	24	20	11	11	20	33	43	50	75	

FL 18" SCP

26.10	26.70	26.90	26.30	26.40	26.53	26.37	25.80	24.10	27.50	30.00	30.50
7.6	7.0	6.8	7.4	7.30	7.17	7.33	7.9	9.6	6.2	3.7	3.0
75	38	25	21	11	11	21	32	45	50	75	

26.50	26.70	25.60	23.55	26.00	26.25	26.32	26.18	25.60	24.00	25.40	27.00	29.60
7.2	7.0	8.1	10.15	7.7	7.45	7.38	7.52	8.1	9.7	8.3	6.7	4.12
75	50	37	30	21	11	11	20	30	41	46	50	75

FL 18" SCP

26.60	27.10	25.60	24.00	25.90	25.90	26.22	26.29	26.14	25.60	24.00	25.40	26.70	29.90	30.80
7.1	6.6	8.1	9.7	7.8	7.8	7.48	7.41	7.56	8.1	9.7	8.3	7.0	3.8	2.9
75	50	38	30	25	21	11	11	20	30	41	45	50	75	

STA + π - ELEV.

933.70

33+50

34+00

BM 2.14 926.99 8.87 924.83 (924.85)

34+50

✓

+82

5.90 921.09

LT

10 DEC. 1973

RT

64

26.30	25.90	24.00	23.30	25.10	25.46	25.55	25.37	24.80	23.40	24.60	25.90	29.00
7.4	7.8	9.7	10.4	8.6	8.24	8.15	8.33	8.9	10.3	9.1	7.8	47.3
75	50	40	30	22	11		11	21	33	41	43	50

23.40	23.70	22.60	22.40	24.00	24.54	24.65	24.47	24.10	22.40	23.90	25.00	27.90
10.3	10.0	11.1	11.3	9.7	9.13	9.05	9.23	9.6	11.3	9.8	8.7	58.2
75	50	42	32	21	11		11	21	33	41	45	50

TOP HYD, LT STA 34430

20.69	21.49	21.99	22.89	23.19	23.59	23.56	23.64	23.49	21.69	23.29	26.99	30.00
6.3	5.5	5.5	4.1	3.8	3.42	3.23	3.35	3.5	5.3	3.7	0.0	4.0
75	50	33	26	21	11		11	22	25	41	50	75

23.29
30.00
23.29
+ 3.9
75

N.E. END 12" CIP 40' RT.

STA	+	π	-	ELEV.
-----	---	-------	---	-------

		926.99		
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35+00				
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+50				
-----	--	--	--	--

+71				
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*				
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+86				
-----	--	--	--	--

*+84				
------	--	--	--	--

		7.62	919.37	
--	--	------	--------	--

36+00				
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LT

11 DEC, 1973
Partly cldy RT

65

19.69	20.29	20.99	22.59	22.85	22.87	22.76	22.39	19.99	20.79	20.59	20.79
7.3	6.7	6.5	4.4	4.14	4.12	4.23	4.6	7.0	6.2	1.4	+3.8
75	50	45	27	16	✓	15	26	29	38	50	75

18.69	19.89	20.89	21.87	21.99	21.84	21.49	19.19	21.49	23.99	20.69	20.69
8.3	7.1	6.1	5.12	5.00	5.15	5.5	7.8	5.5	3.0	+3.7	+3.7
75	43	33	20	✓	19	28	32	39	50	71	76

18.69	19.59	20.39	21.53	21.64	21.45	21.09	18.99	21.69	23.89	20.59	20.59
8.3	7.4	6.6	5.46	5.33	5.54	5.9	8.0	5.3	3.1	+3.6	+3.6
75	44	36	22	✓	19	30	35	43	50	68	76

19.29	19.19	20.09	21.19	21.34	21.14	20.89	18.39	22.39	24.29	24.59	24.59
7.7	7.8	6.9	5.80	5.65	5.85	6.1	8.6	4.6	2.7	2.4	2.4
75	50	36	21	✓	23	33	38	50	60	65	75

TOP MH 43' LT

19.09	18.99	19.99	21.01	21.15	20.94	20.59	17.99	21.09	23.79	24.19	24.19
7.9	8.0	7.0	5.98	5.84	6.05	6.4	9.0	5.9	3.2	2.8	2.8
75	50	37	24	✓	24	34	40	50	65	75	75

STA	+	π	-	ELEV.
-----	---	-------	---	-------

		926.99		
--	--	--------	--	--

36+50				
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37+00				
-------	--	--	--	--

✓				
---	--	--	--	--

+50				
-----	--	--	--	--

✓				
---	--	--	--	--

+87				
-----	--	--	--	--

		9.83		
--	--	------	--	--

			917.16	
--	--	--	--------	--

LT

11 DEC. 1973 66
RT

18.39	18.19	18.99	19.89	20.27	20.02	19.69	16.79	21.79	22.49
8.6	8.8	8.0	7.10	6.72	6.97	7.3	10.2	5.2	4.5
75	50	42	29		26	37	43	57	75 FE

16.99	18.39	19.09	19.33	20.09	20.16	20.09	19.37	19.03	18.79	16.19
10.0	8.6	7.95	7.64	6.90	6.83	6.90	7.62	7.96	8.2	10.8
50	40	28	2 G	2 TC		2 TC	2 G	28	38	47

16.29

10.7

75

21.09

5.9

75
FE

20.59

6.4

61

16.09	17.79	18.14	18.46	19.21	19.30	19.19	18.43	18.10	17.89	15.19
10.9	9.2	8.85	8.53	7.78	7.69	7.80	8.56	8.89	9.1	11.8
46	35	28	2 G	2 TC		2 TC	2 G	28	37	50

15.29

11.7

75

19.89

7.1

75
FE

19.29

7.7

66

TOP MH 32 RT

STA + π - ELEV.

926.99

38+00

✓

+07

12.82 914.17

+40

✓

+61 = GUTTER (S)

LT

11 DEC. 1973
RT

67.

14.69	16.69	17.26	17.56	18.36	18.91	18.35	17.60	17.27	16.39
12.3	10.3	9.73	9.43	8.63	8.58	8.64	9.39	9.72	10.6
50	38	28	2	2		2	2	28	39
			G	TC		TC	G		

14.59	18.19	17.79	14.99	15.19
12.4	8.5	9.2	12.0	11.5
75	75	68	50	42

TOP MH 61' LT

13.19	15.29	15.99	16.56	16.92	16.26	12.77	16.99
13.5	11.7	11.0	10.43	10.07	10.73	14.22	10.0
75	50	46	27		40	50	57
						FL W. END	
						18° SCP	

14.77	15.86	16.33	16.62	16.35	15.96	15.90	16.91
12.22	11.13	10.66	10.37	10.64	11.03	11.09	10.58
100	50	27		27	56	75	150
							CB

STA + π - ELEV.

926.99

38+83 = $\neq$ LONG LAKE RD

✓

BM 1.41 918.63 9.77 917.22 (917.22)

39+00

✓

BM 3.54 918.61 3.54 915.09 (915.07)

LT

Z

11 DEC. 1973 68.
R7

15.72

15.83

16.00

16.31

15.92

16.06

15.95

11.27

11.16

10.99

10.68

11.07

10.93

11.04

50

35

27

27

31

55

MH

MH

14.93

14.10

13.39

18.59

16.39⁴

16.07

12.06

12.89

13.60

8.40

10.65

10.92

100

150

200

150

100

75

SPIKE IN PP SW / COR LONG LAKE RD.

14.8

15.4

15.84

16.14

15.80

15.91

16.11

3.8

3.3

2.79

2.49

2.83

2.72

2.52

100

60

28

28

56

88

16.42
2.21
100

TOP HYDRANT AT RUAN TRUCKING CO.

STA	+	π	-	ELEV.
-----	---	-------	---	-------

		918.61		
--	--	--------	--	--

39+05	=	GUTTER	RT	
-------	---	--------	----	--

✓				
---	--	--	--	--

+26				
-----	--	--	--	--

✓				
---	--	--	--	--

+50				
-----	--	--	--	--

✓				
---	--	--	--	--

KP
RG
DS
RJ

LT

E

26 FEB 1974
CLOUDY
30° RT

69.

14.1	14.9	15.3	15.74	16.05	15.72	15.74	15.88
3.9	3.7	3.3	2.87	2.56	2.89	2.87	2.73
100	186	63	28		28	50 MIT	78

16.29
2.32
100

13.2	14.1	15.3	15.38	15.68	15.32	15.31	15.72	15.1
5.4	3.9	3.3	3.23	2.93	3.29	3.30	5.89	3.5
85	65	44	28		28	32	49	59

FL 18" SCP

12.5
6.1
100

15.1
2.9
100

13.1	14.9	15.01	15.44	16.18	16.23	16.18	15.39	15.03	15.10
5.5	3.7	3.60	3.17	2.43	2.38	2.43	3.22	3.58	3.6
58	37	28	2 G	2 TC		2 TC	2 6	28	39

15.0
14.8
14.7
12.4
3.6
3.8
3.9
6.2
100
80
59
49.50

STA

+

π

-

ELEV.

918.61

39+83

3.89 14.72

40+00

✓

+50

✓

LT

26 FEB 1974 70
RT

TOP MH 24' RT

14.1	14.55	14.81	15.55	15.66	15.55	14.76	14.44	14.3
4.5	4.06	3.80	3.06	2.95	3.06	3.85	4.17	4.3
39	28	2 G	2 TC		2 TC	2 G	28	38

13.9

4.7

4.4
FF

14.7

3.9

100

14.0

4.6

72

13.4

5.2

59

12.2

6.4

51-53

13.6	14.03	14.33	15.06	15.11	15.05	14.28	13.96	13.81
5.0	4.58	4.28	3.55	3.50	3.56	4.33	4.65	4.8
37	28	2 G	2 TC		2 TC	2 G	28	36

13.1

5.5

4.5
FF

13.8

4.8

100

13.4

5.2

66

12.4

6.2

59

11.7

6.9

50-52

STA	+	π	-	ELEV.
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		918.61		
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41+00				
-------	--	--	--	--

✓				
---	--	--	--	--

+50				
-----	--	--	--	--

✓				
---	--	--	--	--

42+00				
-------	--	--	--	--

✓				
---	--	--	--	--

LT

✓

26 FEB 1974

RT

71.

12.91	13.56	13.88	14.61	14.69	14.61	13.87	13.61	13.41
5.7	5.05	4.73	4.00	3.92	4.00	4.74	5.00	5.2
39	28	2	2		2	2	28	38
		G	TC		TC	G		

12.81
5.8
45
FE

13.31 13.21 12.21 11.51
5.3 5.4 6.4 7.1
100 83 59 50-53

13.01	13.17	13.58	14.35	14.43	14.32	13.57	13.31	13.01
5.6	5.44	5.03	4.26	4.18	4.29	5.04	5.31	5.6
37	28	2	2		2	2	28	38
		G	TC		TC	G		

12.51
6.1
45
FE

12.81 12.71 12.01 11.41
5.8 5.9 6.6 7.2
100 81 54 48-51

12.81	13.00	13.28	14.05	14.09	14.05	13.28	12.88	12.81
5.8	5.61	5.33	4.56	4.52	4.56	5.33	5.73	5.8
36	28	2	2		2	2	28	37
		G	TC		TC	G		

12.11
6.5
45
FE

12.31 11.81 11.31
6.3 6.8 7.3
100 64 45 48

STA + π - ELEV

918.61

42+35

7.04 911.57

✓

+53

✓

43+00

✓

LT

E

26 FEB 1974

RT

72

TOP MH 45' RT

12.51

12.69

12.99

13.60

13.56

13.63

13.01

12.66

12.49

6.1

5.92

5.62

5.01

5.05

4.98

5.60

5.95

6.12

37

28

2

2

2

2

28

34

G

TC

TC

G

MH

12.01

6.6

45

FE

11.71

11.71

11.41

11.83

12.41

6.9

6.9

7.2

6.78

6.2

100

74

55-57

49

38

12.51

12.59

12.87

13.47

13.41

13.48

12.86

12.53

12.21

6.1

6.07

5.74

5.14

5.20

5.13

5.75

6.08

6.4

37

28

2

2

2

2

28

38

G

TC

TC

G

11.51

12.81

12.11

7.1

5.8

6.50

45

55

61

conc.

11.21

11.61

10.21

7.4

7.0

8.4

100

61

50-53

STA + π - ELEV.

918.61

43+13

6.00 912.61

+53

✓

44+00

✓

BM 1.70 916.77 3.54 915.07 915.07

LT

£

26 FEB 1974

RT

73.

TOP MH 23' RT ✓

12.23 12.44 12.77 13.52 13.56 13.59 12.73 12.44 12.44

6.38 6.17 5.84 5.09 5.05 5.06 5.88 6.17 6.17
 42 28 2 2 2 2 28 31
 G TC TC G MH

11.22 11.18
 7.39 7.43
 62 73

12.21 11.31 9.91 12.11
 6.4 7.3 8.7 6.5
 84 59 50-53 39
 BLTG

11.36 12.39 12.69 13.47 13.54 13.46 12.71 12.41 12.31

7.25 6.22 5.92 5.14 5.07 5.15 5.90 6.20 6.3
 49 28 2 2 2 2 28 37
 G TC TC G

11.71 11.41
 6.9 7.2
 50 62
 FE

11.61 11.31 9.91
 7.0 7.3 8.7
 84 63 49-52

TOP HYD. AT RUAN TRUCKING CO.

STA

+

π

-

ELEV.

916.77

44+50

✓

45+00

✓

+29

✓

LT

E

26 FEB. 1974

RT

74.

11.89	11.46	12.64	13.41	13.53	13.41	12.69	12.35	12.07
4.88	5.31	4.13	3.36	3.24	3.36	4.08	4.42	4.7
41	41	2	2	2	2	2	28	36
TC	G	G	TC	TC	G			

11.57
5.2
54
FE

10.77 10.77 9.67
6.0 6.0 7.1
100 61 49-51

12.32	11.88	12.55	13.31	13.37	13.33	12.59	12.35	11.87
4.45	4.89	4.22	3.46	3.40	3.44	4.18	4.42	4.9
40	40	2	2	2	2	2	28	36
TC	G	G	TC	TC	G			

11.27
5.5
51
FE

10.27 10.17 10.27 9.07
6.5 6.6 6.5 7.7
100 85 67 51-53

12.49	12.04	12.57	13.35	13.40	13.32	12.57	12.28	11.67
4.28	4.73	4.20	3.42	3.37	3.45	4.20	4.49	5.1
40	40	2	2	2	2	2	28	40
TC	G	G	TC		TC	G		

11.57
5.2
51
FE

9.57 9.97 10.57 8.51
7.2 6.8 6.2 8.26
100 66 53 53
FL 18"

STA + π - ELEV.
916.77

45+45 = $\neq$ ENT RT

✓

+59

✓

46+00

✓

LT

E

26 FEB

1974 75.
RT

12.5A

12.0A

12.51

13.3A

13.36

13.29

12.55

12.25

4.23

4.73

4.20

3.43

3.41

3.48

4.22

4.52

39

39

2

2

2

2

28

TC

G

G

TC

TC

G

11.57

5.2

50

FE

9.17

9.97

10.57

11.17

7.3

6.8

6.2

5.3

100

57

48

40

12.5A

12.05

12.49

13.25

13.31

13.26

12.50

12.22

11.17

4.23

4.72

4.28

3.52

3.46

3.51

4.27

4.55

5.3

39

39

2

2

2

2

28

40

TC

G

G

TC

TC

G

11.57

5.2

51

FE

9.17

9.17

8.38

10.17

7.6

7.3

8.39

6.6

100

72

53-55

53

FL 18" M

12.50

12.01

12.43

13.19

13.25

13.17

12.10

12.19

12.17

4.27

4.76

4.34

3.58

3.52

3.60

4.37

4.58

4.6

40

40

2

2

2

2

28

36

TC

G

G

TC

TC

G

28

36

11.57

4.9

51

FE

8.97

9.17

8.57

9.97

7.8

7.6

8.2

6.8

100

75

53-55

44

STA + π - ELEV.

916.77

46+56

✓

47+00

✓

+50

✓

TP 4.56 917.55 3.78 912.99

LT

26 FEB. 1974 76.
RT

12.53	12.02	12.31	13.05	13.16	13.13	12.39	12.14	12.37
4.24	4.75	4.40	3.72	3.61	3.64	4.38	4.63	4.4
40	40	2	2		2	2	28	34
TC	G	G	TC		TC	G		

12.07
4.7
55

8.64
8.73
153
FL 30" SR (W. END)

12.33	11.91	12.32	13.10	13.13	13.09	12.33	11.98	11.97
4.44	4.86	4.45	3.67	3.64	3.68	4.44	4.79	4.8
40	40	2	2		2	2	28	33
TC	G	G	TC		TC	G		

12.57
4.2
50

11.67
2.1
55

13.57
32
44

11.87
4.9
40

12.57	11.83	12.21	13.06	13.05	13.00	12.21	11.90	12.17
4.2	4.94	4.56	3.77	3.72	3.77	4.56	4.87	4.6
42	40	2	2		2	2	28	34
		G	TC		TC	G		

12.97
3.8
45

¢

STA 48+00

STA

+

K

-

ELEV

917.55

49+00

✓

+50

✓

+66

9.24

48+63

6.21

BM

3.13

914.42

914.44

LT

E

26 FEB 1974 77.

RT

11.48	11.03	11.95	12.70	12.75	12.69	11.91	11.67	11.65
6.07	6.52	5.60	4.85	4.80	4.86	5.64	5.88	5.9
41	41	2	2		2	2	28	36
TC	G	G	TC		TC	G		
11.95	10.15							12.85
56	7.4							4.7
44	54							43

11.25	10.82	12.01	12.78	12.85	12.80	12.00	11.86
6.30	6.73	5.54	4.77	4.70	4.75	5.55	5.75
45	45	2	2		2	2	28
TC	G	G	TC		TC	G	
11.35	10.15					11.75	10.95
							11.95
6.2	7.4					5.8	6.6
51	57					53	43

FL E. END 24" SCP 63' RT

FL CB 39' LT

TOP Iron Mont E CLEVELAND

STA + TOWER ELEV. 26+52±
 ↑ - ELEV.

BM 2.99 939.57 (936.58)

Pier NW Cor 7.21 932.37

" SW Cor 7.27 932.30

" SE Cor 7.28 932.29

" NE Cor 7.27 932.30

BM 7.30 932.27 NE Cor. of NE Pier P.P.

BM Lt Sta 28+25 4.03 935.54 (935.54)

27 4.69 934.88 (34.90)

W.S.
K.6
R.C.
E.Y.

6-23-76
CLEAR: 85'

4

WMS
DPS

ADDITIONAL
CROSS SECTIONS

BASE LINE 50' N. OF SEC. LINE

CORD "C"

14+00 TO 18+00

STA	+	Δ	-	ELEV
BM	0.57	958.00		957.43
14+00				
✓				
+50				
✓				
15+00				
✓				

W.S
K.G
R.C
E.Y

BASE
LINE

6-23-76
CLEAR: 80"

5

TOP HYD LT. STA 15+10

48.9	44.0	49.2	50.1	51.4	51.9
9.1	9.0	8.8	7.9	6.6	6.1
71	63	50	25	0	14
	ERO				FE

50.1	50.3	46.1	43.1	40.3	39.6
7.3	7.7	11.3	14.9	17.7	18.4
77	81	90	100	107	150

51.9	52.4	51.1	51.5	51.9	51.7
6.1	5.6	6.9	6.5	6.1	6.3
42	33	26	23	0	14
			RA Edge		FE

48.1	44.3	41.1	39.7	39.4	39.6
9.9	13.7	14.9	18.3	18.6	18.6
50	57	61	100	150	200

41.0	46.9	52.5	52.8	53.0	52.9
17.0	11.1	5.5	5.2	5.0	5.1
37	27	16	7	14 RO	14
					FE

39.8	39.8	39.8
18.2	18.2	18.2
78	100	140
		TANK

STA

+

π

-

ELEV

958.00

15+50

✓

16

✓

920

17

16+50

W.S
K.6
R.C
E.Y

BASE
LINE

6-23-76
CLEAR 80°

6

41.0	46.3	52.7	53.1	53.2
17.0	11.7	5.3	4.9	4.8
28	21	11	RD	14 FE

39.9	39.9
18.1	18.1
69	114 TANK

47.1	52.3	52.8	52.0	52.9
10.9	5.7	5.2	5.0	5.1
20	10	4	RD	14 FE

43.6	41.8	41.0	39.9	39.9
14.4	16.2	17.0	18.1	18.1
29	40 RD	49	100 RD	126

49.8	51.4	51.5	52.0	51.9	52.2
8.2	6.6	6.5	6.0	6.1	5.8
25	22	16	9	0	14 FE
50.0	49.9	50.1	RD 41.9	40.4	39.9
80	8.1	7.9	16.1	17.6	18.1
31 RD	36	40	54	100	130

STA	+	π	-	ELEV
		958.00		
17+00				
✓				
T.P	5.02	956.14	6.88	951.12
17+50				
✓				
18+00				
END				

51.4	51.4	49.1	50.0	51.1	51.0
6.6	6.6	8.9	8.0	6.9	7.0
74	67	52	33		14
			Φ RD		FE

47.7	41.6	40.1
10.3	16.4	17.9
82	90	150

TOP SPNCE STA. 17+00

47.6	48.9	48.8	49.4	50.1
8.5	7.2	7.3	6.7	6.0
78	56	30		14
	Φ RD			FE

47.7	47.5	51.7	50.4	45.7	51.8
8.4	8.6	4.4	5.7	10.4	11.3
100	112	125	150	165	180

50.6	50.1	52.2	48.8	48.4	48.5
10.5	9.0	2.9	7.3	7.7	7.6
84	69	52	37		14
					FE

STA

+ π - ELEV
PROFILE & OF ROADS

956.14

0+00

5.1

951.0

+25

5.6

950.5

+50

9.2

946.9

+75

13.4

942.7

+86

14.6

941.5

0+00

7.1

949.0

+25

4.6

944.4

+50

0.2

955.9

Bm

3.84

952.30

952.27

6-23-76

CLARE 90°

8

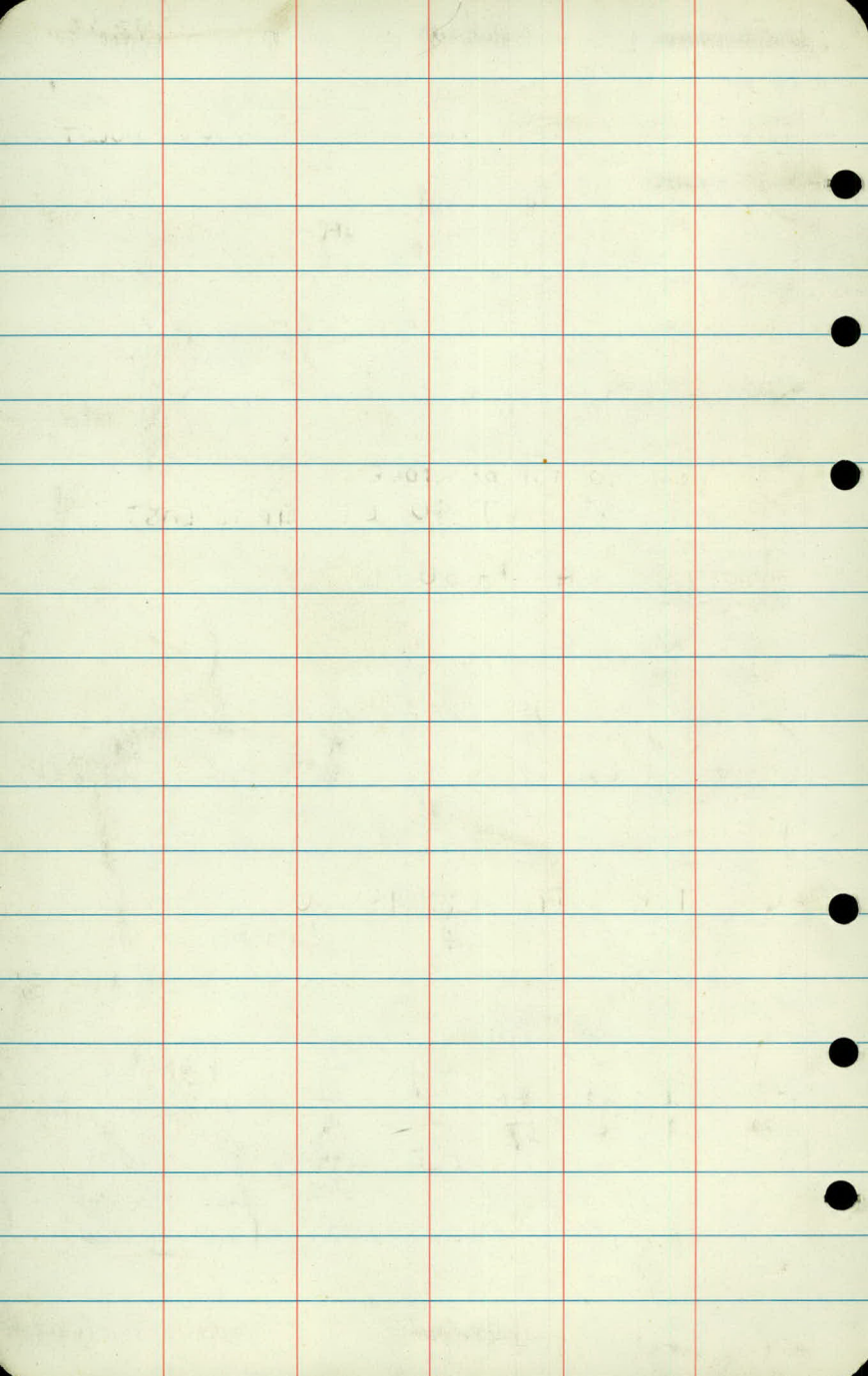
ROAD DOWN TO HOLDING AREA AROUND TANK

STA. 16+64 LT. DOWN TO WEST

ROAD TO TOP OF RIDGE

STA 17+50 LT UP TO EAST

TOP AWD LT. 18+60



W.S
G.A
R.S
E.V

10-29-76
CLEAR: 55°

1

CO. RD "C"

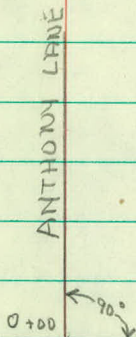
W. CO LINE TO CLEVELAND

ADDITIONAL

CROSS-SECTIONS - TOPO - PROFILE

BASE LINE OFF OF CO. RD "C" NORTH OF
ANTHONY LANE.

DIETZEN NO. 384-S



CO. RD "C"

1A

LT

Q

RT

2 + 00

$$+75 \frac{\text{LOT}}{0-100}$$

$$+80 \frac{\text{MH}}{35}$$

$$+75 \frac{\text{86 LOT}}{0}$$

$$+76 \frac{6" \text{ ASH}}{10}$$

$$+75 \frac{\text{RD}}{23}$$

+50 ✓

$$+43 \frac{5" \text{ ASH}}{11}$$

$$+33 \frac{\text{LOT}}{34-66}$$

$$+33 \frac{\text{RD}}{47}$$

$$+19 \frac{\text{COR LOT}}{48}$$

$$+33 \frac{\text{RD}}{0}$$

$$6" \text{ POPULAR}$$

$$+13 \frac{}{29}$$

$$+06 \frac{15" \text{ POPULAR}}{23}$$

1 + 00

$$\text{RD} \frac{}{12}$$

$$\text{RD} \frac{}{32}$$

$$+98 \frac{3" \text{ m}}{55}$$

$$+77 \frac{5" \text{ m}}{54}$$

$$\text{SW COR BLDG}$$

$$+60 \frac{}{70}$$

$$+60 \frac{3" \text{ MAPLE}}{44}$$

$$+65 \frac{\text{S.T.P.}}{20}$$

+50

$$+45 \frac{\text{POD}}{16}$$

$$+45 \frac{\text{RD}}{16}$$

$$+27 \frac{\text{MH}}{2}$$

0 + 00

W.S
G.A
R.J
24

LT

E

RT

10-29-16
CLEAR: 57°

2

PARKING LOT

MA

MA

DIETZGEN NO. 384-5

2A
STA

+

π

-

ELEV.

BM

2.29

943.41

941.12

0+25

+40

+45

+75

1+00

+33

W.S
G.A
R.J
E-4

LT

Q

RT

10-24-16
CLEAR 56"

3

TOP HYD N.W COR CO. RD "C" : ANTHONY LANE

38 ²	38 ²	38 ¹	38 ⁴	938 ⁶	38 ⁴	37 ²	38 ⁵	38 ⁷
5.2	5.2	5.3	5.0	4.8	5.0	5.5	4.9	4.7
75	46	26 BIT RD	17 BIT RD		15 BIT RD	28 BIT RD	45	67

34 ⁸	35 ²	37 ¹	36 ⁸	38 ²	38 ³	37 ²	35 ³¹	36 ⁶	38 ²	38 ⁶
8.6	8.2	8.70	6.6	5.2	5.1	5.7	8.10	6.8	5.2	4.8
75	44	24 F.L 18" emp.	21	16 BIT RD		15 RD BIT	20 F.L 18" emp.	27	44	75

36 ⁷	37 ¹	35 ⁷	38 ²	38 ²	37 ⁶	36 ³	37 ²	38 ⁸
6.7	6.3	7.7	5.2	5.2	5.8	7.1	5.7	4.6
51	31	24	16 BIT RD		16	24	37	60

36 ²	37 ⁰	36 ¹	37 ⁶	38 ⁰	37 ³	36 ⁵	38 ¹	38 ²
6.5	6.4	7.3	5.8	5.4	6.1	6.9	5.3	4.7
65	39	23	16 BIT RD		22 BIT RD	30	47	67 BLDG.

37 ⁰	36 ⁵	37 ²	36 ⁰	37 ⁶	37 ²	37 ³	36 ⁵	38 ²	38 ²
6.4	6.9	6.1	7.4	5.8	5.6	6.1	6.9	5.2	4.6
75	50	24	19	13 BIT RD		32 BIT RD	38	54	68 BLDG.

37 ²	37 ³	37 ⁶	37 ²	37 ¹	38 ²	37 ⁴	36 ⁶	37 ²	38 ²
6.2	6.1	5.8	7.4	5.7	5.4	6.0	6.8	5.7	4.7
66	36	12	8	BIT RD LEAVE	24 RD	45	51	61	69

DIETZEN NO. 384-5

3A

STA

+

π

-

ELEV

943.41

1+50

✓

+75

+80

5.51

37⁹⁰
—

✓

2+00

✓

W.S
C.D
R.W
R.Y

LT

£

RT

10-29-76
CLEAR: 59°

4

37² 37⁷ 37⁸ 36⁷ 36³ 37⁷ 38¹ 37³ 36⁸

6.2 5.7 5.6 6.7 7.1 5.7 5.3 6.1 6.6
60 22 3 2 11 33 58 67
LOT BIT RD BIT RD

37⁹
5.5
76

37⁷ 38² 38² 38⁴ 36³ 37⁸ 38²

5.7 5.4 5.2 5.0 7.1 5.6 5.2
53 21 9 17 25 48
LOT BIT RD

TOP MA RT. 35'

37⁴ 36⁸ 37⁴
6.0 6.6 6.0
86 79 73
BIT RD

38⁴ 38³ 38³ 38⁵ 36⁶ 37²

5.0 5.1 5.1 4.9 6.8 5.5
25 19 33 38 46
LOT BIT RD

37² 38²
5.7 5.2
91 69
BIT RD

DIETZGEN NO. 384-S

CROWN
4A
STA

PROFILE OF ANTHONY LAKE GOING NORTH

ELEV

0

943.41

+50

5.2

38²

1

5.5

37⁹

+50

5.3

38¹

2

5.2

38²

+50

5.2

38²

+80

5.0

38⁴

+50

FROM

—

ELEV

2+05 RT. 42

6.79

36⁶³

12" cnp

6.46

36⁹⁵

W.S
G.A
R.J
B.Y

10-29-76

5

DIETZEN NO. 384-S

SOUTH F.L.

NORTH END

} 40' CULVERT

5A

ML
MR

Nov 27, 78
Cloudy 26° 1.

62-623-14

CoRoC

X SECTIONS

84" R.C.P.A.

DITCH TO THE NORTH 150'

E 15 E of culvert.

not
used in plan (not)
L&R
11.30.78

STA	+	π	-	ELLEV
B.M	2.23	938.81		936.58

0+00 No. END 84" RCPA

0+25

0+50

0+75

ML
MR

Nov 27, 78

✱

LT

RT

2.

SPIKE IN ARC LITE 25+40 LT

34.1	29.5	20.8	20.3	21.3	30.1	31.2
4.7	9.3	18.0	18.5	17.5	8.1	7.6
31	14	6		14	19	34

33.9	26.2	19.2	19.1	20.3	28.6	30.0
4.9	12.6	19.6	19.7	18.5	10.2	8.8
31	13	4		10	18	33

33.1	20.1	20.8	20.4	20.5	28.1	29.4
5.1	12.7	18.0	18.4	18.3	10.7	9.4
31	16	3		8	17	32

34.0	25.5	20.5	20.2	20.7	27.9	28.5
4.8	13.3	18.3	18.6	18.1	10.9	10.3
31	16	2		8	17	32

STA

+

π

-

ELEV

938.81

1+00

1+25

1+50

B.M.

2.23

936.58

(936.58)

ML
MR

Nov 27, 78

LT

4

RT

3

33.3 33.3	25.0 25.0	20.5 20.5	20.2 20.2	26.8 26.8	27.4 27.4
5.5	13.8	18.3	18.6	12.0	11.4
31	16		9	17	32

33.3 33.3	24.7 24.7	20.2 20.2	20.0 20.0	19.9 19.9	26.3 26.3	26.9 26.9
5.3	14.1	18.6	18.8	18.9	12.5	11.9
31	16	8		8	15	30

33.3 33.3	25.3 25.3	20.0 20.0	20.0 20.0	20.1 20.1	26.1 26.1	26.8 26.8
5.5	13.5	18.8	18.8	18.1	12.7	12.0
31	16	3		8	15	30

SPIKE IN ARC LITE 25+40 LT

