

Book 28 Dr. 12

OFFICE OF COUNTY ENGINEER
RAMSEY CO. MINN.

Plan.....Survey

Matoska Park.....

From White Bear Lake, Minn......

Road Acc't. No.

Date Filed 11-7-45.....

File

Plan Survey

Matocha Park

White Bear Lake Minn

From Approx So Line Johnson

To No Line of 6th str

Index

Align

Page
1 to 6

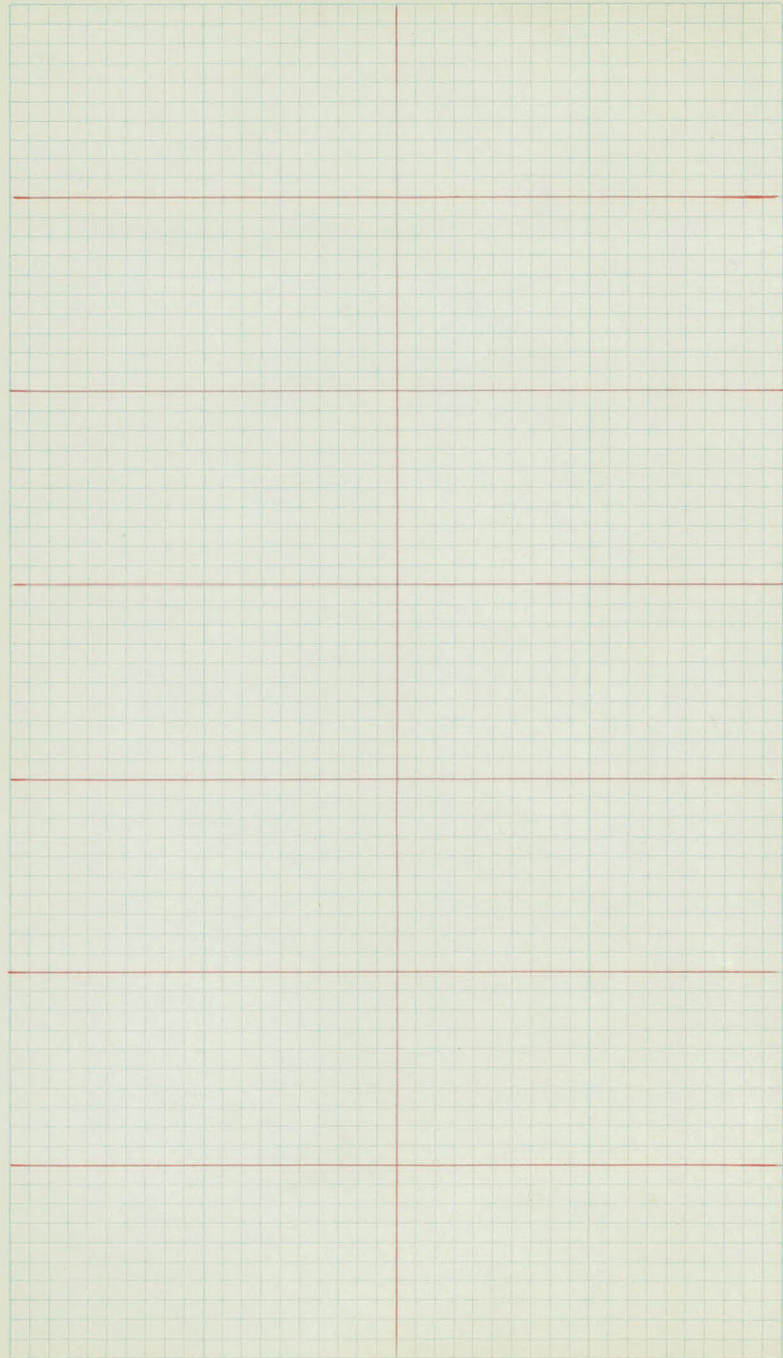
Topog

7 to 14

X Section

15 to 27

In Office 7/11/45



Align

"A" Line

Sta	Pt	ALT	ARt.
10+28.65	P.O.T	Approx	Shore Line

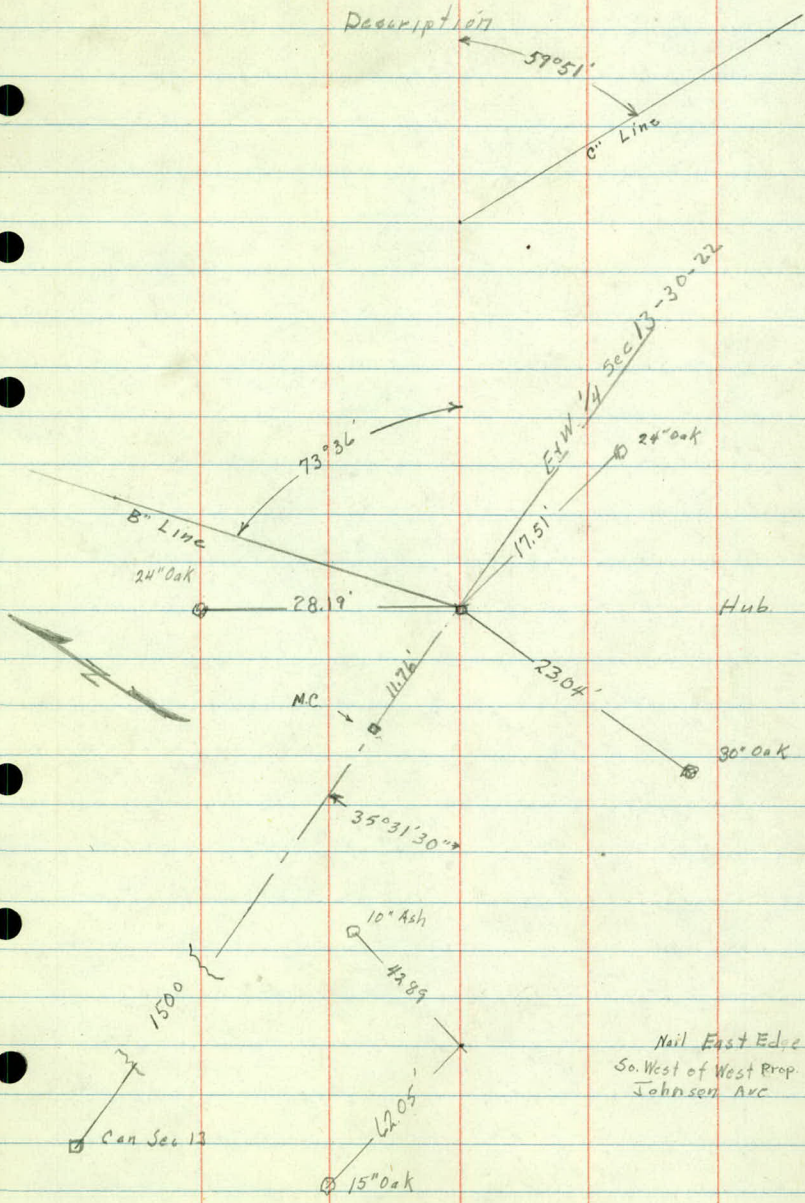
10+28.65

9+70.80	P.O.T	0+00 C" Line
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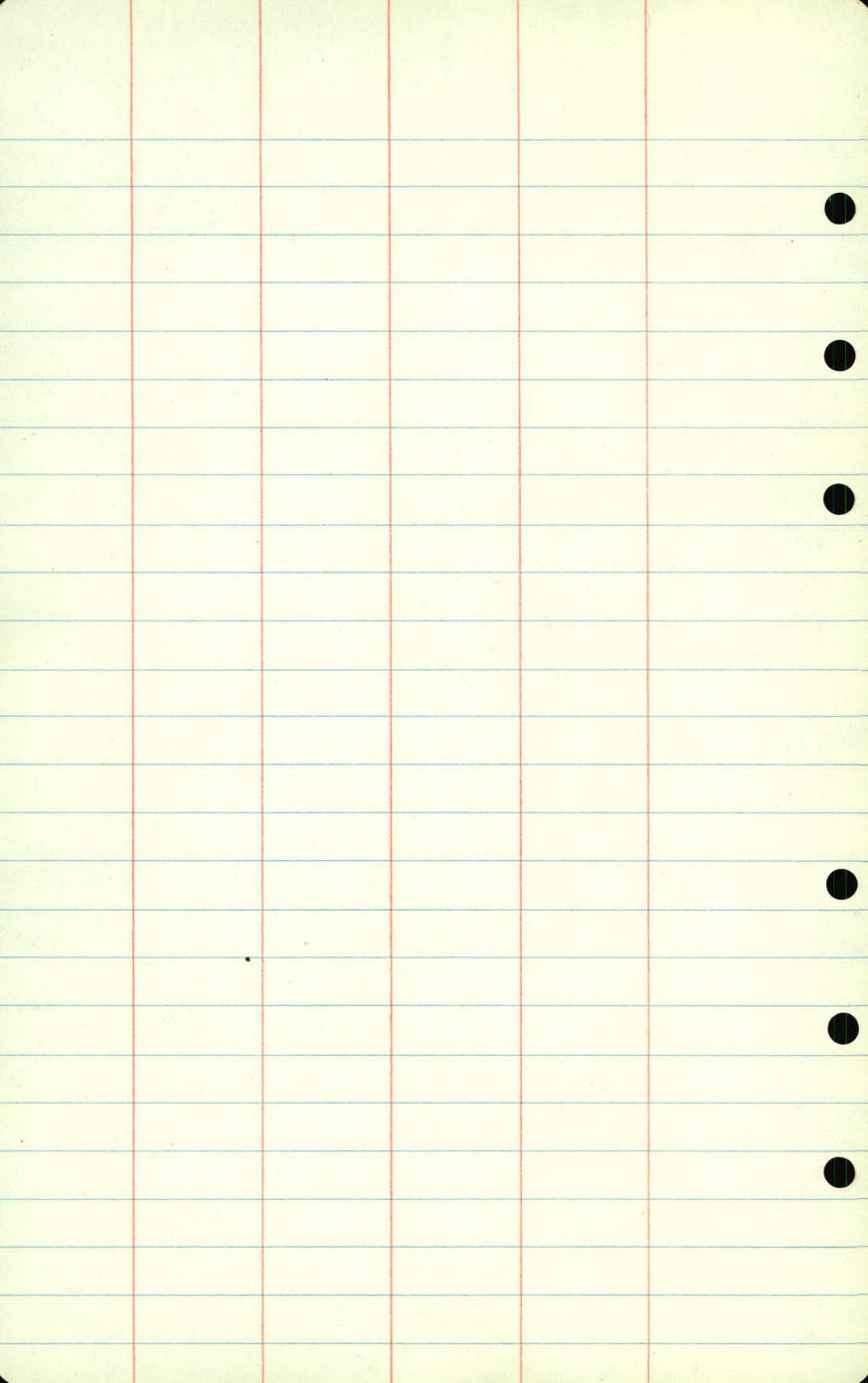
8+84.05	P.O.T =	0+00 "B" Line
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0+00

Description



Nail East Edge Parc
So. West of West Prop. Line
Johnson Arc



4
Align
"B" Line

From P.O.T "A" Line Sta 8+8405 To No Line 6th

579

P4

Δ L+

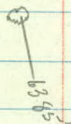
Δ R+

4+15.35

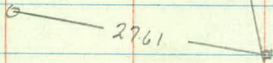
0+00 = 8+8405

Description

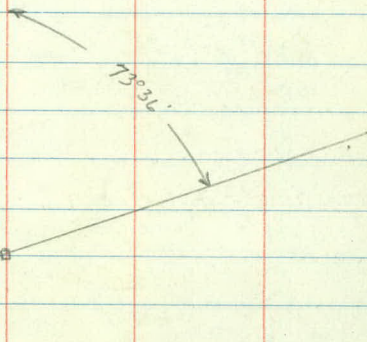
30" oak



Arch L.P.



Hub East Edge Pavc
On No Prop Line 6th



Sta	Pt	Alt	Art
-----	----	-----	-----

3+80.65			
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0+00 = 9+70.80 A Line	* Manitow Island Rd East		
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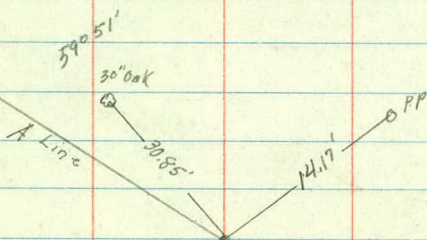
"C" Line

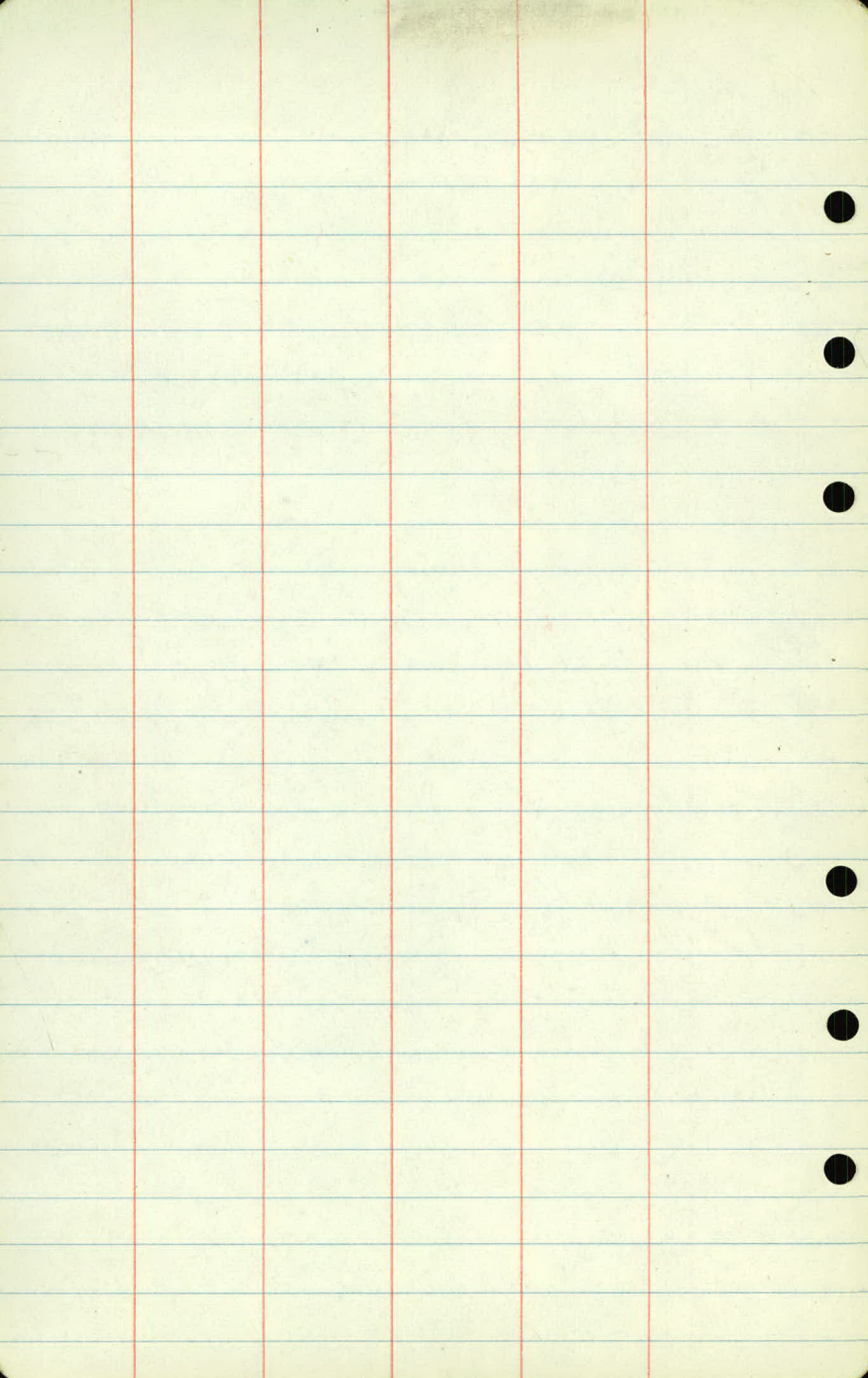
No. Edie Bridge

9.0'

14.0

Nail in Cen Travelled
Portion of Bridge

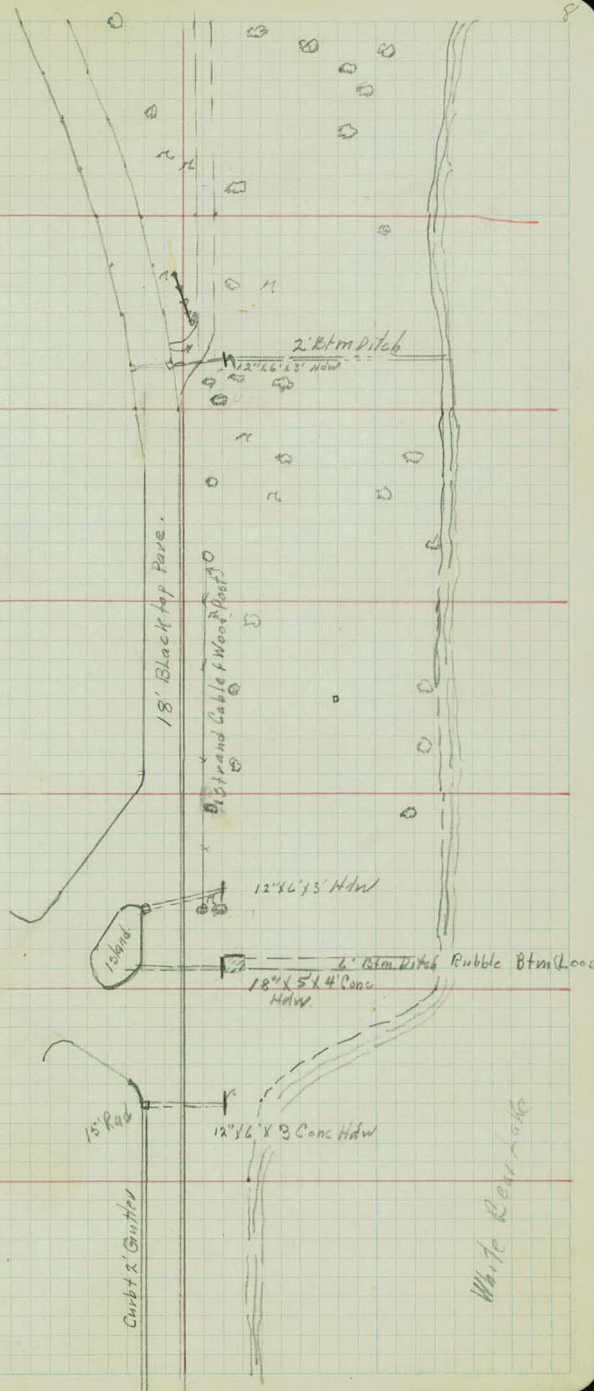




Topography

Matoska Park

6	100	24" Elm 37'	845'	60'	139'	12'	+93 18" Ash 37'
							+90 15" Elm 61'
							+85 15" Bass 108'
+52	18" Oak 18'	+75	73'	49'			+78 4" Oak 85'
		+50	62.5'	38.5'			+66 12" Bass 95'
+32	5th 10'						+44 30" W. 11' 88'
		+25	53'	29'			+27 5th 2'
5			45'	22'	127'	12'	+14 5" Oak 28'
							+63 5th 46'
+68	5th 8'	+75	37'	15'			+54 10" Oak 34'
							+48 5th 7'
+70	End Barricade 5'						+44 Beg Barricade 2'
		+50	315'	9.5'	+94	Tri Oak 106'	+31 5th 1'
							+25 End 12" CM 21.5'
+24	C.B. 65'	+25	27'	5'	+66	24" Bass 27'	+19 15" Oak 32'
+21	C.B. 26'				+16	Trail 100'	+12 15" Oak 11'
4			24' - 22' - 4' - 2.0	133'			+10 36" Oak 51'
							+04 15" Oak 21'
							+76 12" Oak 51'
							+67 Tw. 18" Oak 120'
							+62 15" Oak 14'
							+61 5th 45'
							+59 12" Oak 32' + 15" Oak 120'
							+55 18" Oak 108'
							+29 10" Oak 130'
							+24 12" Oak + End Fe 11'
							+16 Arch Pa. 7'
3					132'		+00 5th 16' Fe 8'
							+96 5th 16'
							+90 20" Oak 34'
							+56 12" Elm 122'
							+54 10" Oak 25'
							+51 Martin No. 77 on 15' Pole
+11	End Curb Rad 22'						+25 12" Elm 116'
2+01	Beg 10' Curb Rad 255'				137'		+24 18" Oak 27'
							Fe 10'
+50	No Curb Line 4th St 65'						+93 12" Oak 13'
+45	C.B. 25'						+90 12" Elm 117'
+41	End 6' Rad 32'						
+37	Beg 6' Curb Rad 22'				139'	+50	+52 End 12" CM 195'
+19	End 15' Curb Rad 465'						+47 5th 14'
+12	End 10' Rad 22'				139'	+25	+41 36" Oak 27'
+01	Beg 15' Rad 41'						+46 12" Oak + Beg Oak Fence 10'
+100	Beg 10' Curb Rad 375'				131'		+10 End 6' Elm Spillway 31'
							+10 End 24" Pit Storm Sewer
+55	Curb Rad 28'						
+35	Rye Trc West Curb Line				96'	+45	+46 5th 28'
+42	Beg Curb Rad 22'				40'		+40 End 12" CM 22'
+38	Con C.B. 38'				34'		
0			22' 20' 2				



10

+43.7 Edge Walk

x x

9

Trail LK 210
4'

+99 30" Oak 12

+22 End Side Walk Rad 159

+17 18" Oak 148'

+14 Stn 58

+100 24" Oak 128'

+78 Water Faucet 84

+67 15" W. Oak 59

+64 24" Oak 126'

+58 48" Coll 25-10" Elm 65'

+53 18" Elm 57'

+54 56" Coll 57'

+27 10" Birch 107'

+13 24" Elm 64'

+06 15" Ash 14'

+90 15" Elm 77'

+86 15" Ash 52'

+84 15" Elm 31'

+80 15" Oak 81'

+69 24" Elm 69'

+65 24" Elm 45'

+45 18" Elm 57'

+40 18" Oak 72'

6

205' 180-18'

+94 15" Elm 6'

+90 Beg Rad 6 Conc Walk 164'

+90 Stn 158'

+139 Coy L' Conc Walk 130

+31 Coy L' Conc Walk 137'

+107 End Rad 162'

+78 Beg 10" Rad 158'

+73 108

+70 End Rad 135'

+65 Beg Curb Rad 124'

+56 119' 94'

+25 97' 72'

845' 60'

139 84'

+76 20" Pop 121'

+64 30" Oak 16'

+63 Stn 46'

+71 NW Cor Teller 58

+61 SW Cor Teller 58'

+59 12" BE 55'

+52 24" BE 85'

+23 24" Will 116'

+11 24" BE 81'

+10 15" BE 129'

+69 6" Tr 182'

+64 10" BE 138'

+64 18" Ash 101'

+61 20" Pop 156'

+54 2-24" Pop 118-149'

+48 24" Will 9'

+47 15" Pop 166'

+23 30" Elm 49 15" Pop 162'

+10 12" Pop 149'

+05 24" Elm 10'

+91 15" Pop 149'

+70 36" Coll 33+20" Pop 142'

+43 15" Will 61'

+40 15" Pop 129'

+28 18" Elm 90'

+16 36" Coll 76'

+07 15" Pop 140'

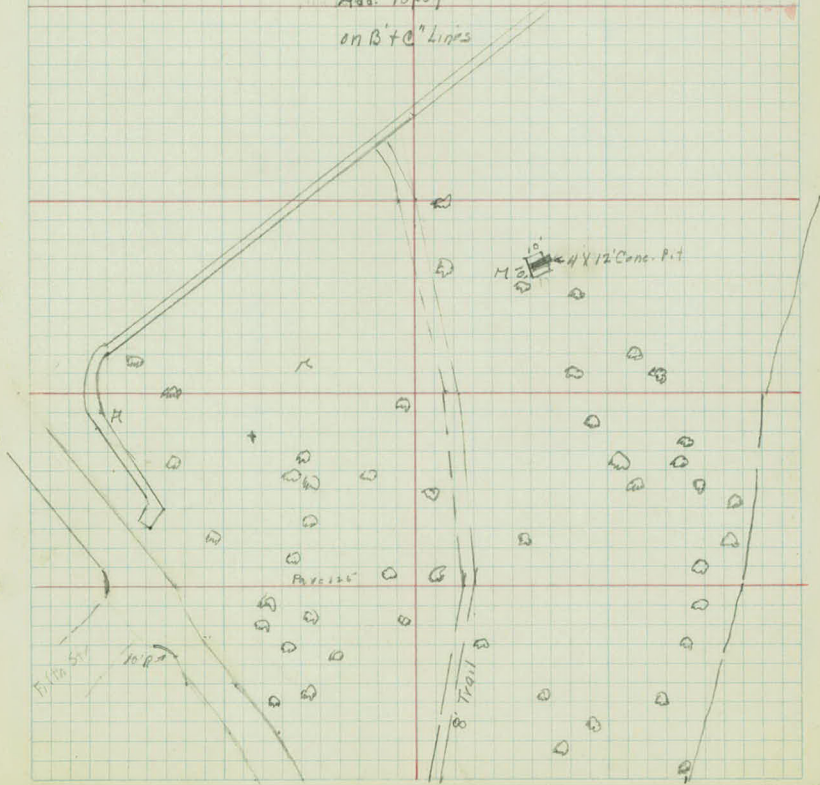
Add. Topog
on B+C Lines

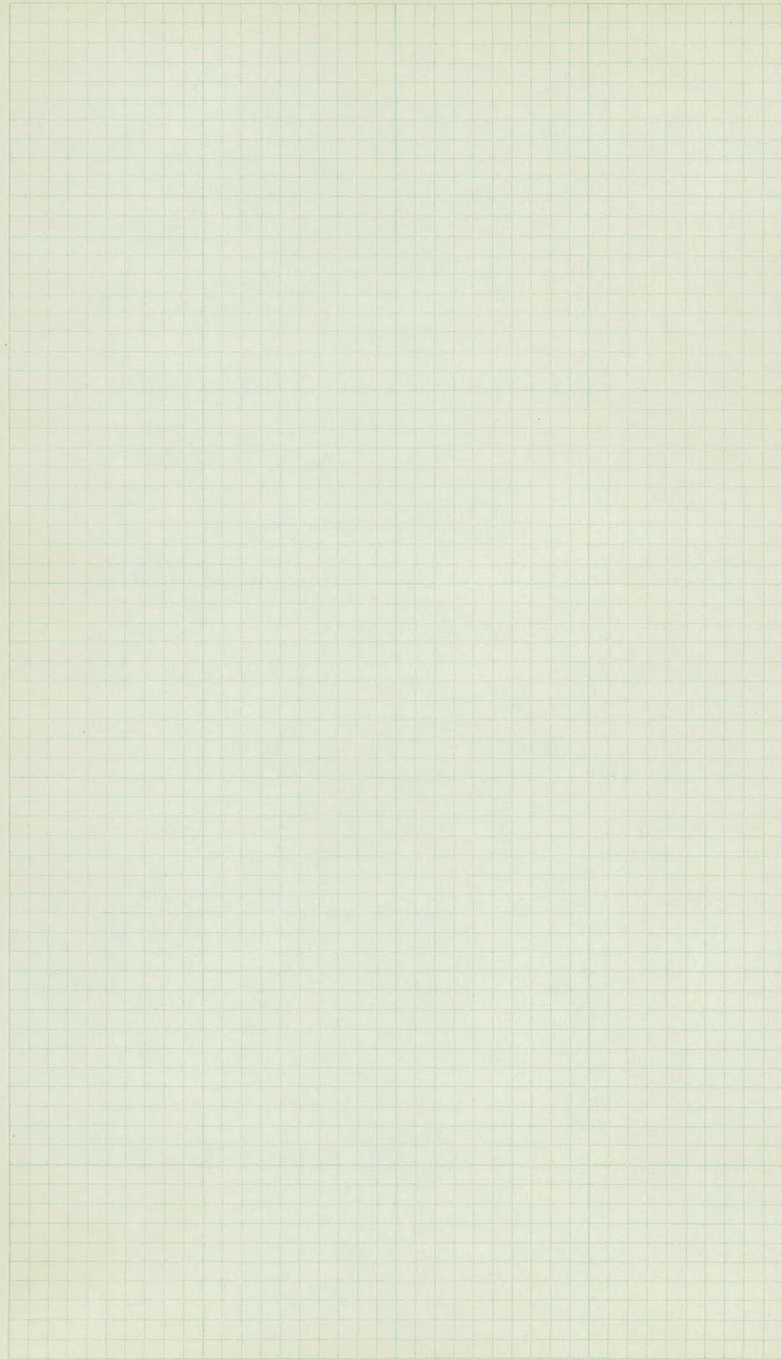
M. 12' 12' Cone. Pit

Barrel

8' Trail

Extra 5' 10' 8'





B. Line Topaz

5

+24 End Curb Rad 20'
+15 Beg Curb Rad 30'
4 Parc 3'

+87 End Curve Pave Edge 5.5'
+79 End Rad 39'
+60 Beg Curb Rad 36'
+16 End Barricade 16'
+09 Curb 65.8
+09 Beg Curve in Pave 383'
3

+97 Beg Barricade 24'
+88 15" B.E 44
+62 30" C.H 21'
+57 6" B.E 18'
+57 12" B.E 34'
+38 6" B.E 47'
+20 24" E/m 59'

2 Curb Line 146' +10 End Rad 110'
+97 Water Tap 44'
+90 12" B.E 53' +95 Beg Gutter Rad 114'
+75 15" E/m 37'
+75 T.P 85' 4 Beg Blacktop Rad 104
+73 10" B.E 65'
+35 End Rad 0'
+31 Beg Rad 45'

+100 Rd 0'-33'

+76 Edge Rd 0'
+65 18" Elm 18'
+59 Edge Walk 0'
+54 24" Elm 41'
+24 30" Oak 18'

LK 60

+79 12" Elm 24'
+63 12" Elm 26'
+52 PP 10
+50 LK 63'
+50 6" B.E 27'

Trail 37'

+10 Island 25'
+00 Island 0-40'
+98 20" Oak 30'
+80 Island 30'

+03 1/2 Trail

+37 6" B.E 20'
+36 Water Valve 18'
+32 End Wall 31'
+29 Beg 12" Ret Wall 29'
+22 Con 10" Dia Circ. Pu Ho 32'
+22 End Pump Ho 22'
+17 End Wall 22
+14 1/4 Wall 24'
+08 Beg 12" Ret Wall 36
LK 63'

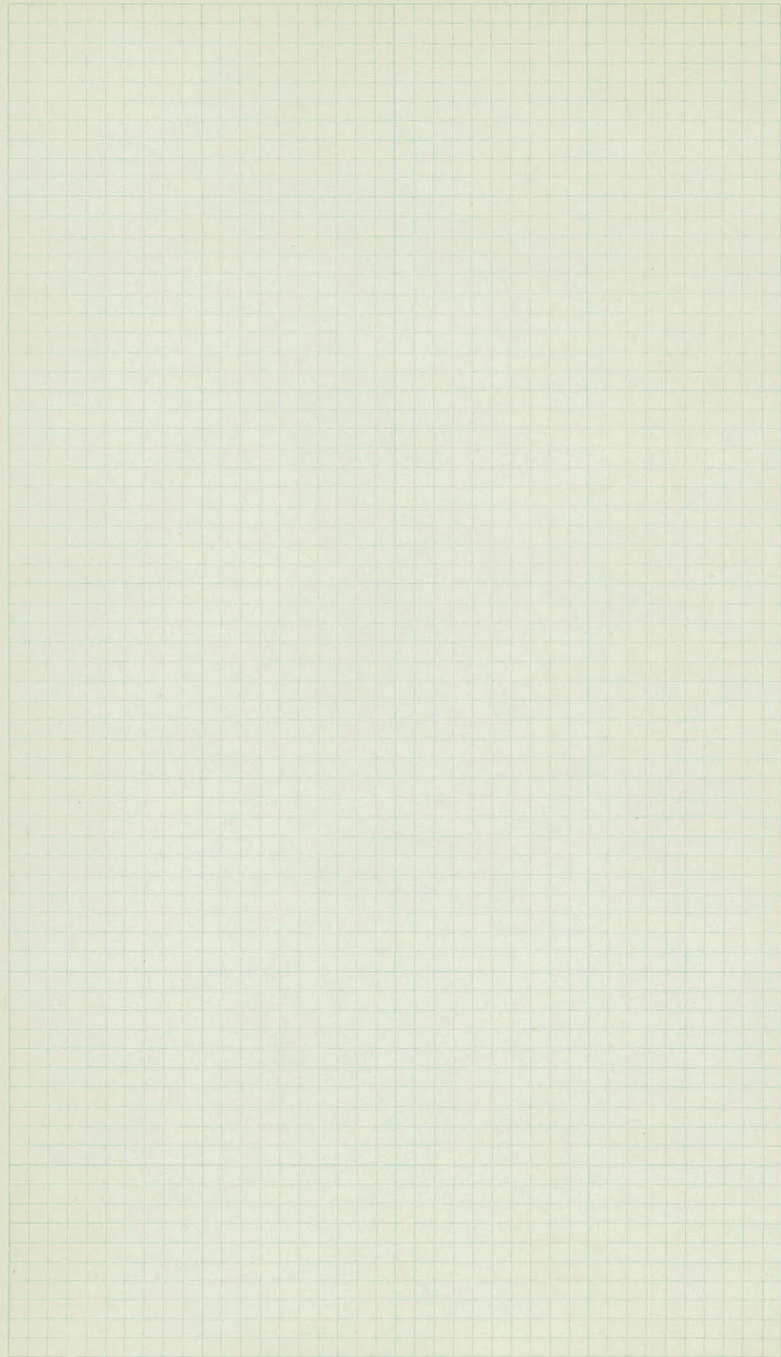
+96 18" E/m 34'
+75 LK 68'

+42 End Trail 19'
+42 PP 63'
+37 30" Elm 49'
+26 10" Pop 77' LK
+02 18" Oak 42
LK 86'

+75 8' Trail 41
+73 5" H 14'
+63 18" Oak 10'

+21 PP 98'
LK 124'
+97 T.P 19
+94 24" Oak 71'
+70 LK 132'
+52 24" Oak 27'



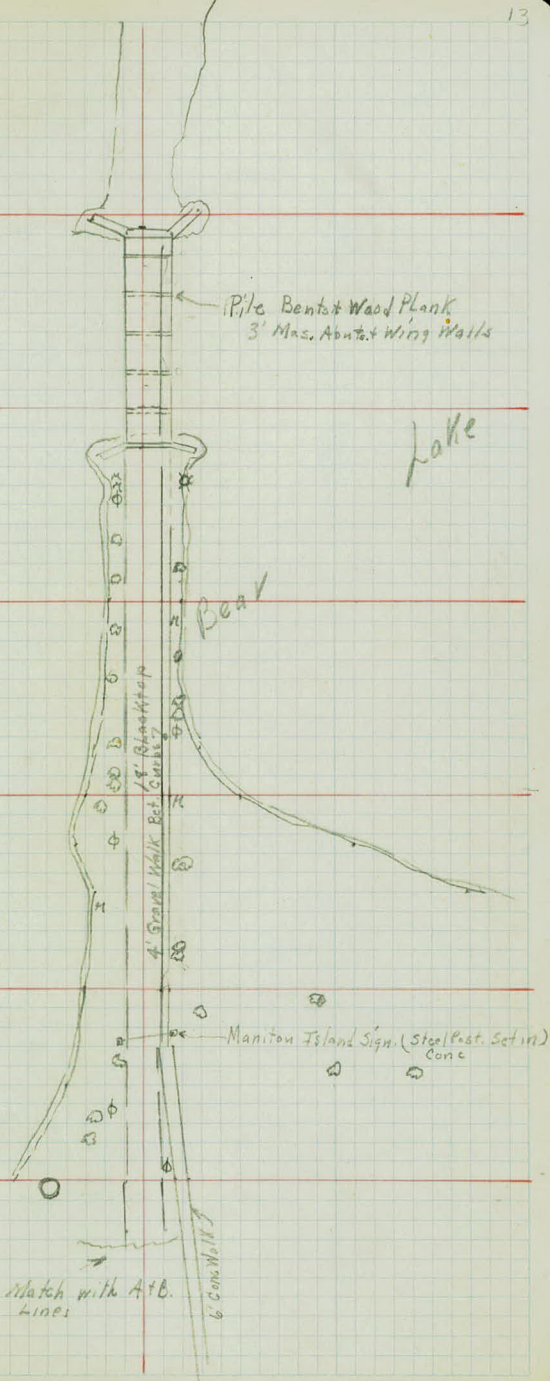


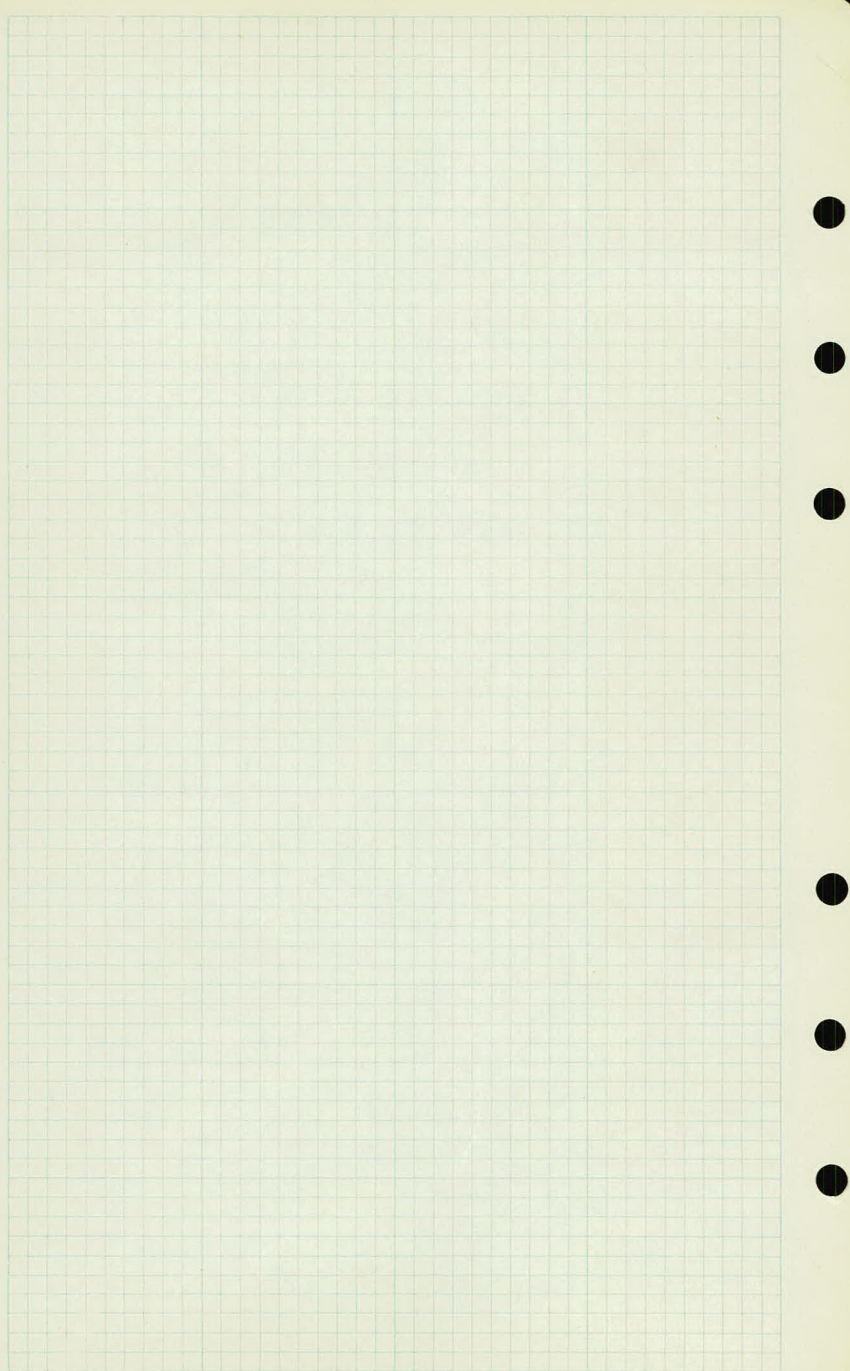
C Line

Topog

6 LK Rd LK
 14' L 9 30
 +85 10" Elm 10'
 +74 15" Elm 11' +75 LK 14
 +21 T.P. 11'
 5 17' LK 21'
 +97 End Wing Wall 27'
 +94 End G.R. 9'
 +91 Cen 3' Mas Wing Wall 9'
 +99 10" W. 11' 17'
 +97 Tw 10" W. 11' 17'
 +80 12" CoH 21'
 +65 12" W. 11' 17'
 +59 12" W. 11' 22'
 +48 24" W. 11' 16'
 +13 PP 14'
 +02 End Wing Wall 27'
 +94 End G.R. 13'
 +91 Cen 3' Mas Wing Wall 13'
 +89 End Wheel G. 9'
 4
 +83 Cen 3' Mas Wing Wall 8'
 +75 Cen 3' Mas Wing Wall 22'
 +64 Stu 12'
 +58 Stu 13'
 +51 T.P. 14' 781 GR 9
 +31 15" W. 11' 16'
 +12 10" W. 11' 14'
 3 17' 9' 9 LK 19'
 +89 30" CoH 15'
 +61 Tw 10" W. 11' 18'
 +50 LK 21'
 +29 Tw. Wall 19'
 +25 LK 28'
 +10 12" CoH 18'
 +08 12" CoH 15'
 2 LK 30' 10' 9 LK 50'
 +95 30" CoH 21'
 +78 T.P. 17'
 +75 LK 34'
 +50 LK 25'
 +44 Stu 21'
 1 100 LK 29' 7 98
 +72 Sign Standard 12'
 +66 24" Elm 12'
 +50 LK 40'
 +39 T.P. 18'
 +34 24" Oak 23'
 +23 30" Oak 22'
 0 67' 9' 9'
 0-04 Cen 10" Dia Cir Pul Ho 50
 0-25 8' 11'
 +83 Cen 3' Mas Wing Wall 13'
 +75 Cen 3' Mas Wing Wall 25'
 +70 End Curb 9'
 +64 Arc L.P. 14' + LK
 +37 End Curb 13'
 +19 18" W. 11' 16'
 Curb 9'
 +71 Stu 15'
 +73 10" W. 11' 16'
 +70 15" W. 11' 18'
 +48 6" W. 11' 18'
 +41 15" W. 11' 18'
 +36 PP 14'
 Curb 9-13.7'
 +78 Stu 18'
 +65 15" Elm 17'
 +38 10" B.E. 19'
 +36 12" B.E. 18'
 +13 T.P. 14'
 Curb 8.8-13.5'
 +96 10" CoH 90'
 +89 24" CoH 30'
 +76 Sign Standard 15'
 +66 Beg Curb 8.4-13.4'
 +66 End Wall 8.4-14.4'
 +59 6" Pop 150'
 +57 15" Pop 141'
 +07 PP 12'
 Wall 16'-22'
 19.5'-24.5'

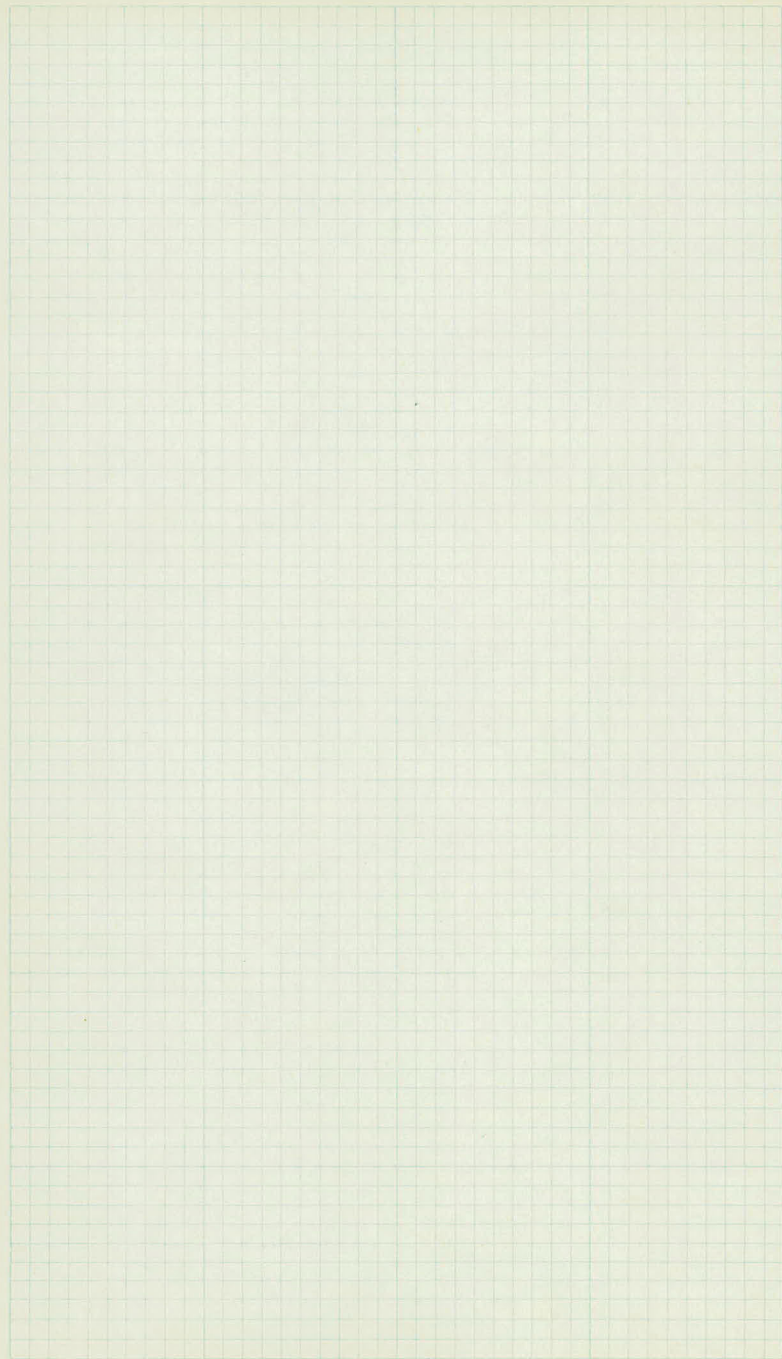
White





+40 LK 15'

+40 LK 66-166



X Sections

Matoska Park

Sta	+	Δ	-	Elev.
B.M	4.16	932.70		928.74
	6.86	937.84	1.92	930.98
0+00				34.2 ✓
+20				34.2 ✓
+36				34.1 ✓
+39				34.0 ✓
+43				34.0 ✓
+60				33.8 ✓
+80				33.7 ✓
+100				33.6 ✓
+106				33.5 ✓

27

2

Rt

Top. S.E. Cor Headwall Co Pump #1 (L.I.B.)

[illegible]

34.41	33.94	34.21	34.04	33.91	34.3	33.0	29.9	29.1	27.1	26.7	27.4	25.9	24.9
<u>3.43</u>	<u>3.90</u>	<u>3.63</u>	<u>3.80</u>	<u>3.93</u>	<u>3.6</u>	<u>4.8</u>	<u>7.9</u>	<u>8.7</u>	<u>10.7</u>	<u>11.1</u>	<u>10.4</u>	<u>11.9</u>	<u>12.9</u>
22	22	11	2	1	373	10	21	22	26	30	33-34	36	40

34.42	33.85	34.17	34.01	33.88	33.9	31.4	31.91	29.7	27.2	27.1	26.6	27.4	26.0	25.6	25.2
<u>3.42</u>	<u>3.99</u>	<u>3.67</u>	<u>3.83</u>	<u>3.96</u>	<u>3.96</u>	<u>5.73</u>	<u>8.1</u>	<u>10.6</u>	<u>10.7</u>	<u>11.2</u>	<u>10.4</u>	<u>11.8</u>	<u>12.1</u>	<u>12.1</u>	<u>12.1</u>
22	22	11	2	1	12	21	21-22	22	23	25	32	36	37	43	45

$\frac{346}{22}$	$\frac{346}{22}$	$\frac{346}{11}$	$\frac{346}{2}$	$\frac{399}{1}$	382	$\frac{38}{10}$	$\frac{49}{16}$	$\frac{7.5}{21}$	$\frac{91}{23}$	$\frac{10.5}{25}$	$\frac{11.7}{39}$	$\frac{121}{49}$	$\frac{112}{54}$	$\frac{118}{71}$	$\frac{121}{100}$	$\frac{128}{101}$
34.8	33.0	34.20	33.78	33.85		340	32.9	30.3	28.7	27.3	26.1	25.7	26.6	26.0	26.6	25.3

✓	34.08.	34.04.	33.83.	33.69.	33.7.	31.5.	28.2.	27.0.	26.8.	26.6.	28.5.	26.7.	25.5.
	$\frac{3.70}{22}$	$\frac{3.80}{11}$	$\frac{4.01}{2}$	$\frac{4.15}{1}$	$3.98 \frac{41}{12}$	$\frac{6.3}{19} \frac{9.6}{26}$	$\frac{10.8}{40}$	$\frac{11.0}{67} \frac{11.2}{121}$	$\frac{9.3}{123}$	$\frac{11.1}{126}$	$\frac{12.3}{127}$		

9.	✓	344.9	33.70	33.54	33.6	32.3	28.1	27.2	27.0	26.7	25.7	24.8	✓
		$\frac{3.75}{22}$	$\frac{389}{11}$	$\frac{414}{2}$	$\frac{4.30}{1}$	$\frac{42}{8}$	$\frac{5.5}{16}$	$\frac{9.7}{27}$	$\frac{10.6}{57}$	$\frac{10.8}{100}$	$\frac{11}{126}$	$\frac{12}{131}$	$\frac{130}{144}$

[illegible]

✓	$\frac{437}{22}$	$\frac{410}{11}$	$\frac{429}{2}$	$\frac{448}{1}$	429	$\frac{48}{15}$	$\frac{54}{20}$	$\frac{84}{22}$	$\frac{93}{30}$	$\frac{109}{31}$	$\frac{120}{61}$	$\frac{120}{77}$	$\frac{125}{101}$	$\frac{125}{115}$	$\frac{111}{125}$	$\frac{113}{125}$
													$\frac{130}{144}$	$\frac{121}{130}$		✓
													248	257		

Sta	+	π	-	Elev
		937.84		
1+13				33.5 . ✓
+13				
+40				33.3 . ✓
+49				33.3 . ✓
+51				33.3 . ✓
+56				33.2 . ✓
+80				33.1 . ✓
2				33.1 . ✓
+20				32.9 . ✓
+40				32.8 . ✓

Sta	+	π	-	Elev
		93784		
2+60				32.6 . ✓
+80				32.5 . ✓
3.				32.5 . ✓
+20				32.3 . ✓
+40				32.2 . ✓
+60				32.1 . ✓
+80				32.0 . ✓
4				32.1 . ✓

Lt

R

Rt

✓	32.58	32.84	32.58	32.47	32.8	32.3	30.0	28.8	27.7	25.7	25.3	✓
✓	526 22	500 11	526 2	537 1	516 6	5378 20	90 46	101 100	121 129	125 133	125 136	✓
✓	32.45	32.70	32.50	32.37	32.6	31.2	30.1	28.9	27.4	26.1	25.6	✓
✓	539 22	514 11	534 2	547 1	528 7	66 24	77 43	89 97	104 130	117 132	122 135	✓
✓	32.35	32.60	32.38	32.26	32.6	31.1	29.9	28.7	27.4	25.8	24.9	✓
✓	549 22	524 11	546 2	558 1	534 7	67 26	79 50	91 100	104 130	120 137	129 140	✓
✓	32.22	32.48	32.28	32.15	32.5	31.4	30.2	28.4	27.3	26.7	25.6	✓
✓	562 22	536 11	556 2	569 1	551 6	64 19	76 40	94 100	105 129	117 132	122 134	✓
✓	32.12	32.37	32.17	32.08	31.9	29.8	29.6	27.3	28.1	26.1	25.6	✓
✓	572 22	547 11	567 2	576 1	558 9	80 41	82 82	105 129	97 131	117 135	122 139	✓
✓	32.06	32.27	32.09	31.97	32.1	30.4	29.6	28.7	27.1	28.5	25.9	✓
✓	578 22	562 11	575 2	587 1	566 7	74 24	82 43	91 92	107 125	93 131	119 133	✓
✓	32.01	32.19	32.01	31.89	32.1	30.4	28.9	28.7	27.0	25.0	25.3	✓
✓	583 23	565 12	583 3	595 2	571 1	74 17	89 41	91 91	108 128	128 129	125 131	✓
✓	31.95	32.19	31.98	31.80	32.03	31.9	30.7	29.5	29.1	28.6	27.2	✓
✓	589 24	565 13	586 4	604 3	581 2	71 8	83 26	87 47	92 93	101 125	98 129	✓
✓	31.95	32.19	31.98	31.80	32.03	31.9	30.7	29.5	29.1	28.6	27.2	✓
✓	589 24	565 13	586 4	604 3	581 2	71 8	83 26	87 47	92 93	101 125	98 129	✓

Sta + π - Elev

937.84

4+20

31.8 . ↓

T.P.

484

935.82

6.86

930.98

+26

12" C.M. Drain to Lake

31.7 . ↓

+31

31.6 . ↓

+60

30.5 . ↓

+80

30.1 . ↓

5

29.7 . ↓

+20

29.4 . ↓

+40

29.3 . ↓

19

LT

24

RT

✓ 25.3

3162.	3208	3190.	3177.	3196.	3117.	306.	297.	303.	297.	289.	274.	279.	125
602	576	594	607	588	61	72	81	75	81	89	104	79	121
26	16	6	5	4	60	1	5	25	41	76	123	125	128

[illegible]

$\frac{402}{28}$	$\frac{372}{17}$	$\frac{393}{8}$	$\frac{408}{7}$	$\frac{386}{6}$	$\frac{40}{3}$	$\frac{495}{5}$	$\frac{56}{12}$	$\frac{59}{20}$	$\frac{61}{23}$	$\frac{63}{42}$	$\frac{68}{88}$	$\frac{74}{123}$	$\frac{92}{127}$	$\frac{102}{131}$	$\frac{106}{133}$	25
3180.	3210.	3189.	3174.	3196.	3182.	309.	302.	299.	297.	295.	290.	284.	266.			

31.82	32.08	31.96	31.81	32.0	31.52	30.1	29.1	28.3	28.5	27.6	28.9	25.6
$\frac{400}{33}$	$\frac{374}{22}$	$\frac{386}{13}$	$\frac{401}{12}$	$\frac{382}{11}$	$\frac{43}{7}$	$\frac{5.7}{7}$	$\frac{67}{19}$	$\frac{75}{55}$	$\frac{73}{83}$	$\frac{8.2}{120}$	$\frac{6.9}{122-125}$	$\frac{10.2}{127}$

✓	$\frac{4.01}{37}$	$\frac{3.74}{26}$	$\frac{3.74}{17}$	$\frac{4.02}{16}$	$\frac{3.88}{15}$	$\frac{3.9}{11}$	$\frac{5.6}{4}$	$\frac{5.7}{18}$	$\frac{6.3}{18}$	$\frac{7.1}{35}$	$\frac{7.8}{67}$	$\frac{7.6}{90}$	$\frac{8.2}{119}$	$\frac{8.2}{123-125}$	$\frac{10.2}{129}$	✓
	31.81	32.08	31.88	31.80	31.94	31.92	30.22	29.5	28.7	28.0	28.2	27.6	28.8	25.6		

390	366	390	403	394	37	57	66	42	18	77	82	89	81	102	105
43	33	23	22	21	15	6	61	10	25	53	87	102	120	122-126	129
3192	3216	3192	3179	3208	3212	3012	292	286	280	281	276	269	277	25	105

3202	3225	3197	3184	3216	3224	3032	2992	2900	2780	2740	2660	2710	2570	2540
$\frac{380}{50}$	$\frac{359}{40}$	$\frac{385}{29}$	$\frac{398}{28}$	$\frac{366}{27}$	$\frac{3655}{21}$	$\frac{59}{13}$	$\frac{64}{6}$	$\frac{68}{13}$	$\frac{80}{39}$	$\frac{84}{88}$	$\frac{92}{117}$	$\frac{87}{119-124}$	$\frac{101}{127}$	$\frac{104}{130}$

32.108.	32.34.	32.10.	31.97.	32.17.	32.132.	30.42.	30.12.	28.7.	27.6.	27.4.	27.6.	27.5.	25.6.	25.3.
$\frac{374}{57}$	$\frac{348}{46}$	$\frac{372}{36}$	$\frac{385}{35}$	$\frac{365}{34}$	$\frac{35}{29}$	$\frac{54}{21}$	$\frac{57}{13}$	$\frac{71}{18}$	$\frac{82}{52}$	$\frac{84}{86}$	$\frac{82}{110}$	$\frac{83}{123}$	$\frac{102}{128}$	$\frac{105}{130}$

Sta	+	Σ	-	Elev
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935.82 ✓

5+60

29.1 . ✓

+80

28.8 . ↓

6

28.7 . ↓

+20

28.5 . ↓

+40

28.0 . ↓

+60

27.7 . ↓

+80

27.8 . ↓

7

27.6 . ↓

ht.

h

RT

32.24	32.44	32.03	32.07	32.30	32.32	31.12	30.02	28.0	27.6	27.0	28.3	25.6	25.2
358 333	379 376	352	35	47	47	47	5.8	7.8 8.2	8.8	7.5	10.2	10.2	10.2
68 58	47 46	44	41	34	18	6.7	30	63	121	124 126	128	133	
32.33	32.40	32.32	32.27	32.36	31.22	30.32	28.6	27.7	27.1	27.4	26.9	28.5	25.6
349 342	350	355	346	46	55	5.8	7.2	8.1	8.7	8.4	8.7	7.3	10.2
77 66	56	55	54	46	37	22	20	73	96	111	126	131	133
32.47	32.64	32.41	32.26	32.45	32.32	30.42	28.5	27.5	27.5	26.9	27.9	26.1	25.6
335 318	341 352	337	35	54	54	5.4	7.3	8.3	8.3	8.9	9.9	9.7	10.2
83 72	61 60	59	56	47	42	25	22	51	81	125	129	135	139
32.60	32.76	32.50	32.38	32.56	32.12	30.52	28.2	27.5	27.2	27.4	29.4	26.4	25.6
322 306	332	344	326	37	53	70	76	8.3	8.6	8.4	6.4	6.4	9.4
96 85	73	71	70	63	56	70	23	60	100	132	136 140	141	147 151
32.73	32.93	32.66	32.52	32.71	32.62	30.82	27.9	27.8	27.3	27.1	27.8	26.1	25.6
309 289	316	330	311	32	5.0	7.2	7.9	8.0	8.5	8.7	8.0	9.7	10.2 10.5
112 99	88	87	86	81	69	24	25	73	100	139	141	146	149 151
33.10	33.04	32.78	32.62	32.79	32.72	30.82	27.9	27.7	27.9	27.4	27.7	27.3	26.7
272 278	304	320	303	31	5.0	6.5	7.9	8.1	7.9	8.4	8.1	8.5	9.1
125 112	101	100	99	95	80	50	14	19	24	49	98	114	142
33.73	33.52	33.01	32.86	32.98	32.82	29.62	27.7	27.4	27.5	27.8	27.7	27.3	26.7
209 230	281	296	284	30	40	6.2	8.1	8.4	8.3	8.0	8.6	8.1	8.1
142 132	120	118	116	111	104	18	12	17	25	27	48	60	80
33.68	33.71	33.18	33.02	33.21	32.92	31.12	27.8	27.5	27.0	28.2	27.2	26.8	26.2
214 211	264	280	261	2.9	47	6.3	8.0	8.3	8.8	7.6	8.6	9.0	9.2
157 144	133	131	129	120	100	66	10	38	55	70	100	135	157
33.68	33.71	33.18	33.02	33.21	32.92	31.12	27.8	27.5	27.0	28.2	27.2	26.8	26.2
214 211	264	280	261	2.9	47	6.3	8.0	8.3	8.8	7.6	8.6	9.0	9.2
157 144	133	131	129	120	100	66	10	38	55	70	100	135	157

Sta	+	π	-	Elev
		935.82		

7+20				27.7
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+40				27.8
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+60				27.8
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T.P	8.81	937.63	7.00	928.82
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+80				28.1
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8				28.1
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T.P	9.00	937.82	8.81	928.82
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+20				28.3
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+40				28.4
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+60				28.4
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$\checkmark$
 34.71
 111
 502

34.82
 4.15
 3.0
 19

	LT	♀	RT
33.39.	33.60.	33.53.	33.91.
2.45	5.29	191	2.07
146	33.62	171	33.75.
33.60	33.62	30.92	
22	30.22	30.22	
142	29.42	28.62	
139	7.2	28.72	
116	8.0	27.82	
110	8.1	27.7	
100	8.2	27.6	
61	8.6	27.2	
50	8.2	27.6	
36	8.2	28.2	
20	8.2	28.2	
8.1	8.1	27.7	
18	8.2	27.6	
30	8.6	27.2	
44	8.2	27.6	
54	8.2	28.2	
70	8.2	28.2	
89	8.1	27.7	
100	8.1	27.1	
115	8.1	26.9	
137	8.1	26.5	
153	8.1	26.5	
176	8.1	26.5	
199	8.1	26.5	
21	8.1	26.5	
33.94	33.60	33.53	33.91
2.45	5.29	191	2.07
146	33.62	171	33.75.
33.60	33.62	30.92	
22	30.22	30.22	
142	29.42	28.62	
139	7.2	28.72	
116	8.0	27.82	
110	8.1	27.7	
100	8.2	27.6	
61	8.6	27.2	
50	8.2	27.6	
36	8.2	28.2	
20	8.2	28.2	
8.1	8.1	27.7	
18	8.2	27.6	
30	8.6	27.2	
44	8.2	27.6	
54	8.2	28.2	
70	8.2	28.2	
89	8.1	27.7	
100	8.1	27.1	
115	8.1	26.9	
137	8.1	26.5	
153	8.1	26.5	
176	8.1	26.5	
199	8.1	26.5	
21	8.1	26.5	
33.94	33.60	33.53	33.91
2.45	5.29	191	2.07
146	33.62	171	33.75.
33.60	33.62	30.92	
22	30.22	30.22	
142	29.42	28.62	
139	7.2	28.72	
116	8.0	27.82	
110	8.1	27.7	
100	8.2	27.6	
61	8.6	27.2	
50	8.2	27.6	
36	8.2	28.2	
20	8.2	28.2	
8.1	8.1	27.7	
18	8.2	27.6	
30	8.6	27.2	
44	8.2	27.6	
54	8.2	28.2	
70	8.2	28.2	
89	8.1	27.7	
100	8.1	27.1	
115	8.1	26.9	
137	8.1	26.5	
153	8.1	26.5	
176	8.1	26.5	
199	8.1	26.5	
21	8.1	26.5	
33.94	33.60	33.53	33.91
2.45	5.29	191	2.07
146	33.62	171	33.75.
33.60	33.62	30.92	
22	30.22	30.22	
142	29.42	28.62	
139	7.2	28.72	
116	8.0	27.82	
110	8.1	27.7	
100	8.2	27.6	
61	8.6	27.2	
50	8.2	27.6	
36	8.2	28.2	
20	8.2	28.2	
8.1	8.1		

Sta	+	π	-	Elev	
		937.82			
8+80				28.5 .	✓
9				28.9 .	✓
0+10		"B" Line		29.0 .	✓
+50				29.1 .	✓
+58				30.3 .	✓
+68				30.5 .	✓
+76				30.1 .	✓
1+00				30.7 .	✓

L+

K

R+

28.6
9.2 9.7 10.4 11.2 11.8 12.3
93 24 54 95 136 181 212

29.4
8.4 8.3 9.1 8.9 9.8 11.3 11.5 11.6 12.3
8.9 4 12 23 46 71 116 140 175 216

28.4
9.4
45 22 88 9 25 49 63

28.8
9.0 8.9 9.2
58 36 14 8.7 30.2 30.20 30.0 29.5 29.7 29.4 28.6 28.2 26.6 25.6
92 96 112 122 94 109 128 134

29.2
8.5 8.7 8.7
60 26 9 75 30.3 29.7 29.7 28.6 28.4 27.2 26.2 25.5
11 20 45 60 93 124 127 133

29.4 29.2 29.5 30.7 30.66 30.0 29.9 28.8 29.1 27.3 26.0 25.6
8.4 8.1 8.3 7.1 7.16 7.8 7.9 9.0 8.7 10.5 11.8 12.2
63 30 17 12 7 7.3 9 33 52 75 123 126 133

29.5 29.5 30.9 30.8 29.6 28.9 29.1 27.5 26.1 25.6
8.3 8.3 6.9 7.0 8.2 8.9 9.1 10.3 11.7 12.2
65 31 21 11 31 40 74 115 126 129

32.3 32.6 32.2 31.2 31.1 30.9 29.1 29.2 28.4 27.3 26.2 25.6
5.5 5.2 5.6 6.6 6.7 7.8 8.7 8.6 9.4 10.5 11.6 12.2
73 13 48 37 12 7.1 21 36 53 95 119 123 128

Sta + Δ - Elev

937.82

+25

30.1 . ✓

+50

30.9 . ✓

+75

31.8 . ✓

2

32.7 . ✓

T.P 6.12 942.18 1.76

936.06

+12

32.9 . ✓

+20

32.5 . ✓

+30

33.1 . ✓

+40

34.1 . ✓

+60

34.4 . ✓

Lt

R

Rt

✓	$\frac{42}{86}$	$\frac{44}{74}$	$\frac{56}{63}$	$\frac{62}{32}$	$\frac{72}{16}$	77	$\frac{82}{17}$	$\frac{85}{42}$	$\frac{86}{75}$	$\frac{95}{95}$	$\frac{105}{106}$	$\frac{121}{113}$
	33.6	33.4	32.2	31.6	30.6		29.6	29.3	29.2	28.3	27.3	25.7

✓	$\frac{42}{98}$	$\frac{49}{63}$	$\frac{62}{24}$	69	$\frac{76}{21}$	$\frac{83}{48}$	$\frac{95}{86}$	$\frac{105}{97}$	$\frac{121}{106}$			
	33.6	32.9	31.6		30.2	29.5	28.3	27.3	25.7			

✓	$\frac{28}{111}$	$\frac{30}{95}$	$\frac{31}{77}$	$\frac{42}{46}$	$\frac{60}{16}$	60	$\frac{66}{72}$	$\frac{80}{38}$	$\frac{90}{67}$	$\frac{103}{82}$	$\frac{117}{89}$	$\frac{122}{97}$
	35.0	34.8	34.7	33.6	31.8		31.2	29.8	28.8	27.5	26.1	25.6

✓	$\frac{19}{134}$	$\frac{19}{114}$	$\frac{1.1}{108}$	$\frac{1.2}{100}$	$\frac{1.7}{66}$	$\frac{29}{43}$	$\frac{48}{20}$	5.1	$\frac{61}{10}$	$\frac{66}{19}$	$\frac{64}{22}$	$\frac{75}{34}$	$\frac{8.9}{57}$	$\frac{103}{75}$	$\frac{117}{82}$	$\frac{12.2}{86}$
	35.9	35.9	36.7	36.6	36.1	34.9	33.0		31.7	31.2	31.4	30.3	28.9	27.5	26.1	25.6

✓	$\frac{60}{130}$	$\frac{60}{115}$	$\frac{49}{104}$	$\frac{52}{74}$	$\frac{63}{51}$	$\frac{84}{27}$	$\frac{86}{74}$	93	$\frac{10.4}{18}$	$\frac{11.5}{28}$	$\frac{118}{41}$	$\frac{13.0}{55}$	$\frac{150}{75}$	$\frac{165}{81}$		
	36.2	36.2	37.3	37.0	35.9	33.8	33.6		31.8	30.7	30.4	29.2	27.2	25.7		

✓	$\frac{58}{122}$	$\frac{59}{109}$	$\frac{58}{108}$	$\frac{47}{98}$	$\frac{51}{56}$	$\frac{82}{25}$	$\frac{90}{7}$	97	$\frac{99}{76}$	$\frac{114}{26}$	$\frac{120}{44}$	$\frac{137}{60}$	$\frac{164}{80}$			
	36.4	36.3	36.4	37.5	37.1	34.0	33.2		32.3	30.8	30.2	28.5	25.8			

✓	$\frac{56}{115}$	$\frac{56}{101}$	$\frac{45}{93}$	$\frac{42}{67}$	$\frac{54}{51}$	$\frac{79}{28}$	$\frac{82}{8}$	$\frac{89}{4}$	9.1	$\frac{94}{13}$	$\frac{113}{35}$	$\frac{123}{43}$	$\frac{139}{59}$	$\frac{147}{67}$	$\frac{156}{69}$	$\frac{166}{76}$
	36.6	36.6	37.7	37.5	36.8	34.3	34.0	33.3		32.8	30.9	29.9	28.3	27.5	26.6	25.6

✓	$\frac{54}{107}$	$\frac{54}{93}$	$\frac{43}{83}$	$\frac{46}{61}$	$\frac{37.9}{38}$	$\frac{37.6}{46}$	$\frac{35.6}{66}$	$\frac{34.4}{22}$	$\frac{34.7}{10}$	81	$\frac{34.1}{6}$	$\frac{33.2}{10}$	$\frac{32.2}{19}$	$\frac{30.4}{36}$	$\frac{30.0}{45}$	$\frac{27.6}{62}$	$\frac{26.5}{67}$	$\frac{25.7}{73}$
	36.8	36.8	37.9	37.9	37.6	35.6	34.4	34.7		34.1	33.2	32.2	30.4	30.0	27.6	26.5	25.7	

✓	$\frac{5.0}{92}$	$\frac{5.1}{81}$	$\frac{4.9}{78}$	$\frac{3.6}{67}$	$\frac{5.4}{43}$	$\frac{6.1}{26}$	$\frac{7.4}{12}$	$\frac{7.2}{6}$	$\frac{7.7}{3}$	7.8	$\frac{8.1}{5}$	$\frac{8.0}{10}$	$\frac{9.2}{18}$	$\frac{10.7}{29}$	$\frac{12.1}{39}$	$\frac{15.0}{49}$	$\frac{16.2}{69}$	$\frac{16.6}{72}$
	37.2	37.1	37.3	38.6	36.8	36.1	34.8	35.0	34.5		34.1	34.2	33.0	31.5	30.1	27.2	26.0	25.6

Sta + Δ - Elev

942.18

2+85

36.4

+96

38.3

3

38.5

+15

39.0

+30

39.3

+60

39.6

+80

40.1

4

39.4

+15

39.1

B.M

13.41

928.77

L+

K

R+

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 37.8 \\
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 \end{array}
 \quad
 \begin{array}{r}
 37.6 \\
 \hline
 4.6 \\
 12
 \end{array}
 \quad
 \begin{array}{r}
 35.7 \\
 \hline
 6.5 \\
 16
 \end{array}
 \quad
 \begin{array}{r}
 32.7 \\
 \hline
 9.5 \\
 25
 \end{array}
 \quad
 \begin{array}{r}
 30.0 \\
 \hline
 12.2 \\
 31
 \end{array}
 \quad
 \begin{array}{r}
 29.0 \\
 \hline
 13.2 \\
 33
 \end{array}
 \quad
 \begin{array}{r}
 27.1 \\
 \hline
 15.1 \\
 40
 \end{array}
 \quad
 \begin{array}{r}
 25.6 \\
 \hline
 16.6 \\
 61
 \end{array}$$

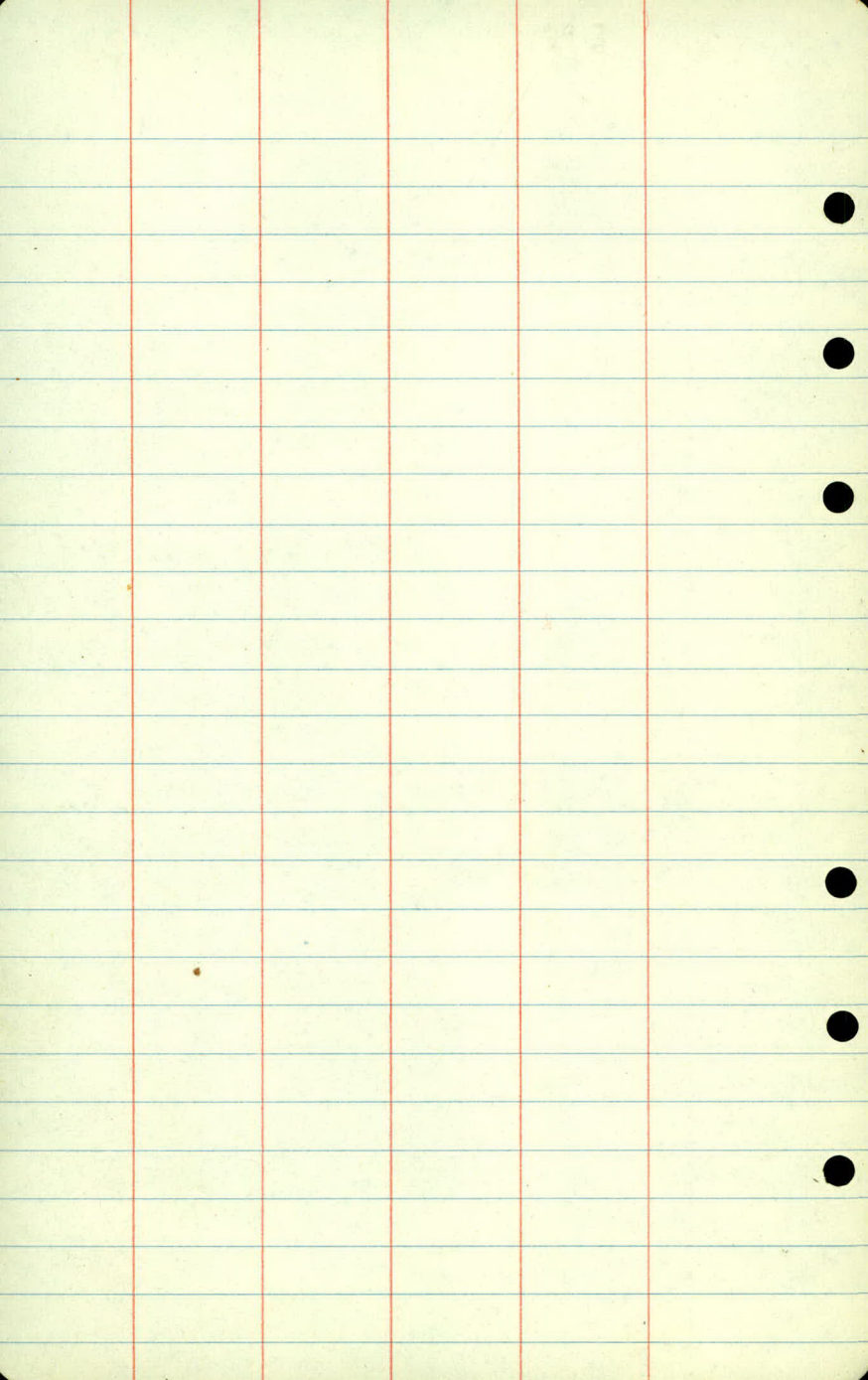
$$\begin{array}{r}
 39.0 \\
 \hline
 3.2 \\
 25
 \end{array}
 \quad
 \begin{array}{r}
 38.8 \\
 \hline
 3.4 \\
 12
 \end{array}
 \quad
 \begin{array}{r}
 39.7 \\
 \hline
 2.5 \\
 8
 \end{array}
 \quad
 2.5
 \quad
 \begin{array}{r}
 39.0 \\
 \hline
 3.2 \\
 11
 \end{array}
 \quad
 \begin{array}{r}
 30.5 \\
 \hline
 11.7 \\
 31
 \end{array}
 \quad
 \begin{array}{r}
 27.6 \\
 \hline
 14.5 \\
 42
 \end{array}
 \quad
 \begin{array}{r}
 25.6 \\
 \hline
 16.6 \\
 64
 \end{array}$$

$$\begin{array}{r}
 39.2 \\
 \hline
 3.0 \\
 17
 \end{array}
 \quad
 \begin{array}{r}
 39.1 \\
 \hline
 3.1 \\
 6
 \end{array}
 \quad
 2.1
 \quad
 \begin{array}{r}
 38.8 \\
 \hline
 3.4 \\
 13
 \end{array}
 \quad
 \begin{array}{r}
 37.3 \\
 \hline
 4.9 \\
 19
 \end{array}
 \quad
 \begin{array}{r}
 30.3 \\
 \hline
 11.9 \\
 29
 \end{array}
 \quad
 \begin{array}{r}
 30.3 \\
 \hline
 11.9 \\
 39
 \end{array}
 \quad
 \begin{array}{r}
 26.3 \\
 \hline
 15.9 \\
 50
 \end{array}
 \quad
 \begin{array}{r}
 25.6 \\
 \hline
 16.6 \\
 68
 \end{array}$$

$$\begin{array}{r}
 39.4 \\
 \hline
 2.8 \\
 14
 \end{array}
 \quad
 \begin{array}{r}
 39.1 \\
 \hline
 3.1 \\
 3
 \end{array}
 \quad
 2.8
 \quad
 \begin{array}{r}
 39.9 \\
 \hline
 2.3 \\
 9
 \end{array}
 \quad
 \begin{array}{r}
 37.3 \\
 \hline
 4.9 \\
 21
 \end{array}
 \quad
 \begin{array}{r}
 30.9 \\
 \hline
 11.3 \\
 34
 \end{array}
 \quad
 \begin{array}{r}
 26.4 \\
 \hline
 15.8 \\
 50
 \end{array}
 \quad
 \begin{array}{r}
 25.6 \\
 \hline
 16.6 \\
 69
 \end{array}$$

$$\begin{array}{r}
 3.1 \\
 7
 \end{array}
 \quad
 \begin{array}{r}
 2.3 \\
 14
 \end{array}
 \quad
 \begin{array}{r}
 6.6 \\
 26
 \end{array}
 \quad
 \begin{array}{r}
 11.9 \\
 37
 \end{array}
 \quad
 \begin{array}{r}
 11.9 \\
 66
 \end{array}
 \quad
 \begin{array}{r}
 16.6 \\
 69
 \end{array}$$

Top S.E. Cor. Hd. W. Pump. #1



C Line

Sta	+	π	-	Elev
B.M.	5.18	953.92		948.74
0+00		933.92		29.1.

+20

28.7.

+40

28.7.

+60

28.6.

+80

28.6.

28.6.

+20

28.5.

+40

28.4.

✓ 25.6. 26.1. 26.6. 27.3. 28.4. 28.9. 28.9. 29.1. 29.12. 29.0. 28.3. 28.6. 28.9.

Top S.E. Cor Abyt Pump Ho #1

Gen. Wall

$\frac{83}{70}$ $\frac{78}{66}$ $\frac{73}{64}$ $\frac{66}{46}$ $\frac{55}{23}$ $\frac{50}{9}$ $\frac{50}{10}$ $\frac{48}{11}$ $\frac{480}{18}$ $\frac{49}{24}$ $\frac{5.6}{29}$ $\frac{5.3}{50}$ $\frac{5.0}{80}$

✓ 25.6. 26.2. 27.1. 27.1. 27.6. 28.7. 28.8. 28.7. 28.8. 28.4. 27.9. 27.9. 27.9.

$\frac{83}{57}$ $\frac{7.7}{51}$ $\frac{68}{46}$ $\frac{68}{40}$ $\frac{6.3}{38}$ $\frac{5.2}{27}$ $\frac{5.1}{9}$ $\frac{5.2}{8}$ $\frac{5.1}{21}$ $\frac{5.5}{24}$ $\frac{6.0}{46}$ $\frac{6.0}{92}$ $\frac{6.0}{100}$

✓ 25.6. 26.6. 28.2. 27.7. 28.0. 28.7. 28.7. 28.8. 28.2. 28.1. 27.3. 27.1. 27.4.

$\frac{83}{45}$ $\frac{73}{28}$ $\frac{5.7}{17}$ $\frac{6.2}{14}$ $\frac{5.9}{10}$ $\frac{5.2}{9}$ $\frac{5.2}{8}$ $\frac{5.1}{19}$ $\frac{5.7}{22}$ $\frac{5.8}{41}$ $\frac{6.6}{59}$ $\frac{6.8}{82}$ $\frac{6.5}{107}$

✓ 25.6. 25.6. 25.6. 25.8. 28.5. 28.4. 28.4. 28.6. 28.0. 27.7. 27.0. 26.4.

$\frac{83}{37}$ $\frac{7.1}{20}$ $\frac{5.4}{9}$ $\frac{5.3}{8}$ $\frac{5.5}{12}$ $\frac{5.3}{18}$ $\frac{5.9}{22}$ $\frac{6.2}{41}$ $\frac{6.9}{63}$ $\frac{7.5}{123}$

✓ 25.6. 26.8. 28.5. 28.2. 28.4. 28.1. 28.1. 27.5. 27.5. 26.9. 26.9. 26.9.

$\frac{83}{33}$ $\frac{7.1}{16}$ $\frac{5.4}{9}$ $\frac{5.3}{9}$ $\frac{5.5}{9}$ $\frac{5.9}{18}$ $\frac{6.4}{30}$ $\frac{6.4}{46}$ $\frac{7.0}{71}$ $\frac{7.0}{129}$

✓ 25.6. 26.0. 26.4. 27.8. 28.5. 28.1. 28.32. 28.0. 26.9. 26.8. 26.4.

$\frac{83}{30}$ $\frac{7.9}{29}$ $\frac{7.5}{19}$ $\frac{6.1}{15}$ $\frac{5.4}{9}$ $\frac{5.8}{9}$ $\frac{5.60}{9}$ $\frac{5.9}{15}$ $\frac{7.0}{23}$ $\frac{7.1}{61}$ $\frac{7.5}{121}$

✓ 25.6. 25.8. 26.5. 27.9. 28.5. 28.1. 28.29. 28.2. 27.1. 26.3. 26.5. 26.0. 25.7.

$\frac{83}{28}$ $\frac{8.1}{23}$ $\frac{7.4}{22}$ $\frac{6.0}{17}$ $\frac{5.4}{9}$ $\frac{5.8}{9}$ $\frac{5.63}{9}$ $\frac{5.7}{14}$ $\frac{6.8}{18}$ $\frac{7.6}{48}$ $\frac{7.4}{58}$ $\frac{7.9}{143}$ $\frac{8.2}{200}$

✓ 25.6. 26.4. 27.8. 28.3. 28.1. 28.25. 28.0. 27.0. 26.3. 26.2. 26.2. 25.6.

$\frac{83}{26}$ $\frac{7.5}{23}$ $\frac{6.1}{15}$ $\frac{5.6}{10}$ $\frac{5.8}{9}$ $\frac{5.61}{9}$ $\frac{5.9}{14}$ $\frac{6.9}{18}$ $\frac{7.6}{23}$ $\frac{7.7}{57}$ $\frac{7.7}{113}$ $\frac{8.3}{174}$

Sta + Δ - Elev

+60

953.92
923.92

28.5. $\searrow$

+80

28.4. $\searrow$

2

28.4. $\searrow$

+25

28.5. $\searrow$

+50

28.4. $\searrow$

3

28.2. $\searrow$

+50

28.1. $\searrow$

+80.65

West End Bridge

28.0. $\searrow$

✓	25.6.	26.4.	26.7.	27.8.	28.3.	281.	282.2.	28.2.	26.3.	25.9.	25.6.	
	$\frac{8.3}{28}$	$\frac{7.5}{27}$	$\frac{7.2}{20}$	$\frac{6.1}{15}$	$\frac{5.6}{11}$	54	$\frac{5.8}{9}$	$\frac{5.70}{9}$	$\frac{5.7}{13}$	$\frac{7.6}{22}$	$\frac{8.0}{85}$	$\frac{8.3}{164}$
✓	25.6.	26.7.	26.8.	27.2.	28.2.	27.9.	28.16.	27.9.	25.8.	25.4.	25.7.	
	$\frac{8.3}{39}$	$\frac{7.2}{36}$	$\frac{7.1}{22}$	$\frac{6.7}{17}$	$\frac{5.7}{11}$	5.5	$\frac{6.0}{9}$	$\frac{5.76}{9}$	$\frac{6.0}{14}$	$\frac{8.1}{24}$	$\frac{8.5}{42}$	$\frac{8.2}{78}$
25.4.	WS	25.4.	26.8.	27.2.	28.3.	27.9.	28.15.	27.9.	26.1.	25.7.	25.6.	
	$\frac{8.18}{31}$	$\frac{8.3}{31}$	$\frac{7.1}{27}$	$\frac{6.7}{18}$	$\frac{5.6}{11}$	5.5	$\frac{6.0}{9}$	$\frac{5.77}{9}$	$\frac{6.0}{14}$	$\frac{7.9}{20}$	$\frac{8.2}{31}$	$\frac{8.3}{45}$
✓	25.6.	27.0.	27.3.	28.3.	28.3.	27.8.	28.16.	27.8.	25.9.	25.6.		
	$\frac{8.3}{30}$	$\frac{6.9}{26}$	$\frac{6.6}{19}$	$\frac{5.6}{11}$	5.4	$\frac{6.1}{9}$	$\frac{5.76}{9}$	$\frac{6.1}{14}$	$\frac{8.0}{22}$	$\frac{8.3}{28}$		
✓	25.6.	26.8.	27.8.	28.2.	27.9.	28.12.	27.5.	25.6.				
	$\frac{8.3}{22}$	$\frac{7.1}{18}$	$\frac{6.1}{12}$	$\frac{5.7}{10}$	5.5	$\frac{6.0}{9}$	$\frac{5.80}{9}$	$\frac{6.4}{14}$	$\frac{8.3}{29}$			
✓	25.7.	27.7.	28.3.	27.6.	28.7.	27.0.	26.0.	25.6.				
	$\frac{8.2}{15}$	$\frac{6.2}{14}$	$\frac{5.5}{9}$	5.7	$\frac{6.3}{9}$	$\frac{5.85}{9}$	$\frac{6.9}{12}$	$\frac{7.9}{16}$	$\frac{8.3}{19}$			
✓	25.6.	26.2.	27.3.	27.9.	27.7.	28.0.	25.6.					
	$\frac{8.3}{13}$	$\frac{7.7}{12}$	$\frac{6.6}{11}$	$\frac{6.0}{8}$	5.8	$\frac{6.2}{9}$	$\frac{5.85}{9}$	$\frac{5.9}{12}$	$\frac{8.3}{15}$			
✓	25.6.	28.9.	28.9.	28.9.	28.9.	25.6.						
	$\frac{8.3}{14}$	$\frac{5.0}{9}$	49	$\frac{5.7}{14}$	$\frac{8.3}{17}$							

