

Book 25 Dr 12

OFFICE OF COUNTY ENGINEER
RAMSEY CO. MINN.

PLAN

Survey

Edgerton & Stockdale Rds.
From Kahler Rd To Clover Str

Road Acc't. No. W-74177

Date Filed. 1-30-43

File

Align

Edgerton Str

From Kohler Rd to Stockdale Rd

10/8/41

N.A.W

A.M.

L.L.

C.N.

10/15/41

drawn up

Sta	Pl	Alt	Art
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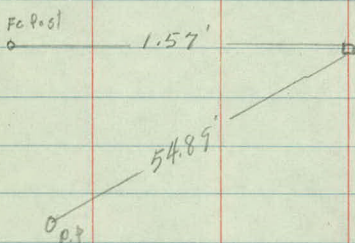
13+18.95	P.1		
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		89°40'	
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7+37 ⁰⁰	P.O.T.		
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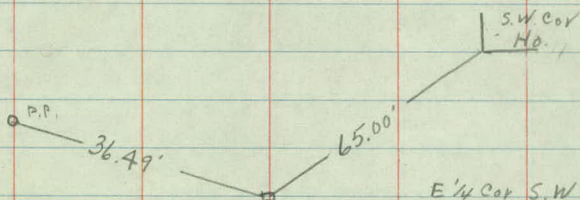
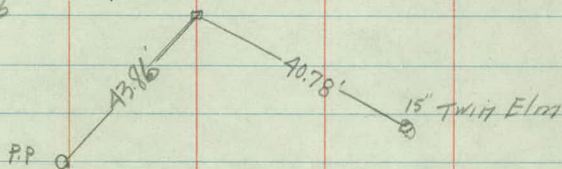
0+00	P.O.T.		
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Description

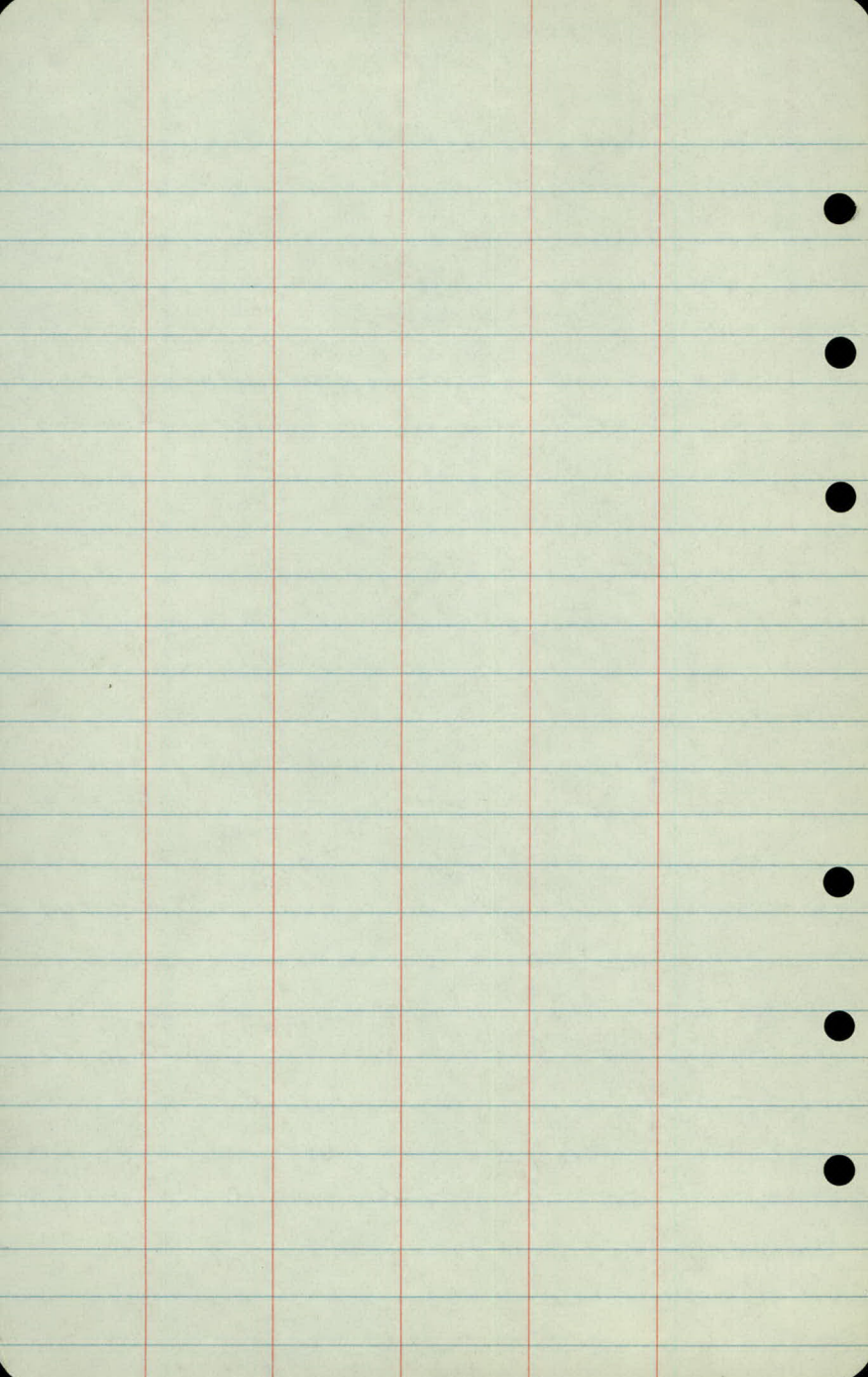


Stone Mark
C: Sec - 29 - 30 - 22

2"x2" Hub



E 1/4 Cor S.W. 1/4 Sec
29 - 30 - 22



Revised
Align

Stockdole Rd

10/2/41

N/4W

HM

ON

L.L

5+9

$\Delta L + \Delta R$

417202

20°04'

0+316

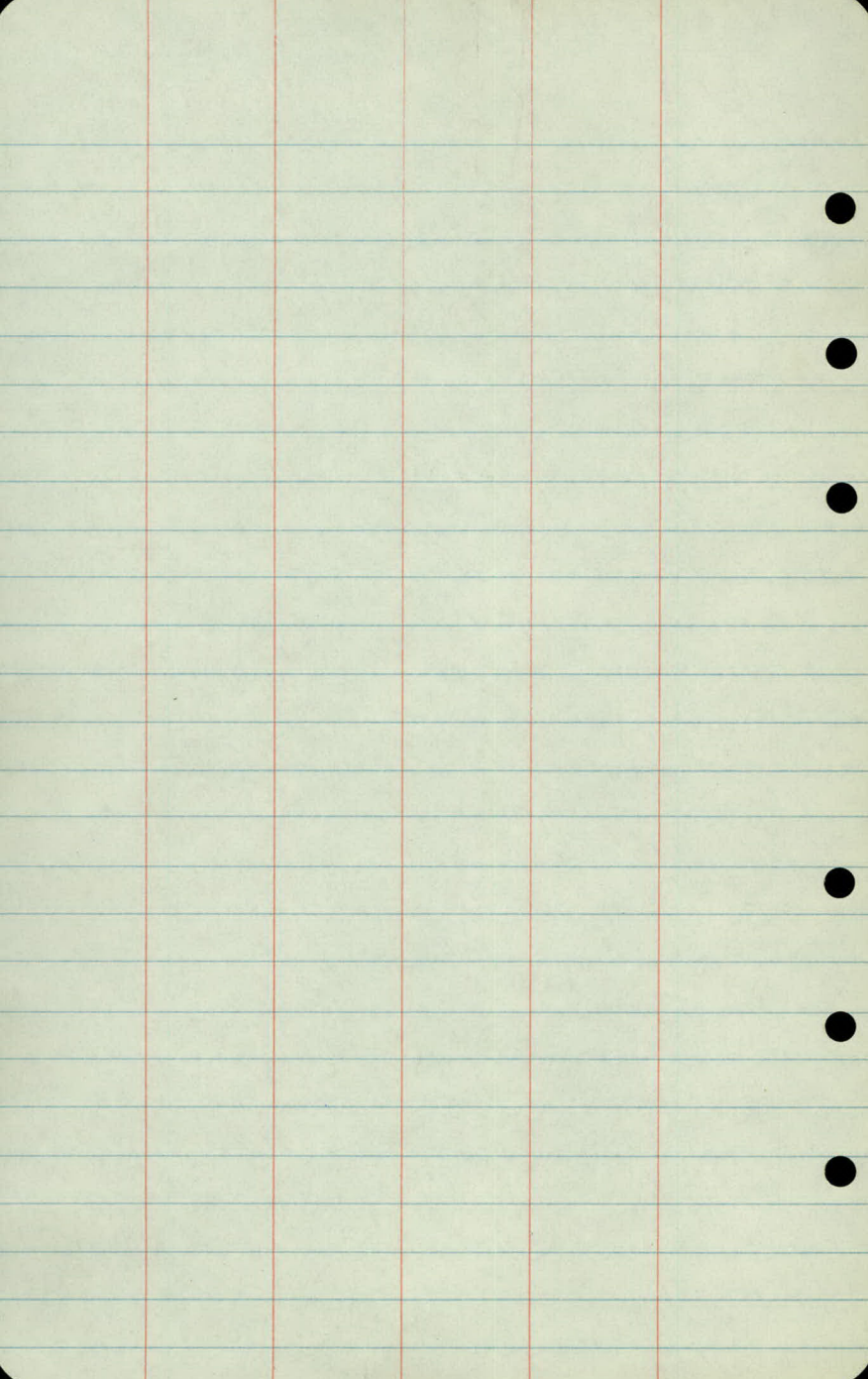
8°15'

0+00

Nail

Iron

Mon



Align

Stockdale Rd

From Edgerton To Hobler Rd

Sta

Pt.

$\Delta L + API$

4+72.02 P.1

19°16'

0+1.36 P.1

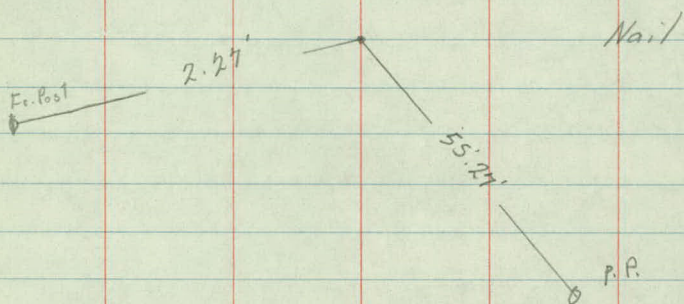
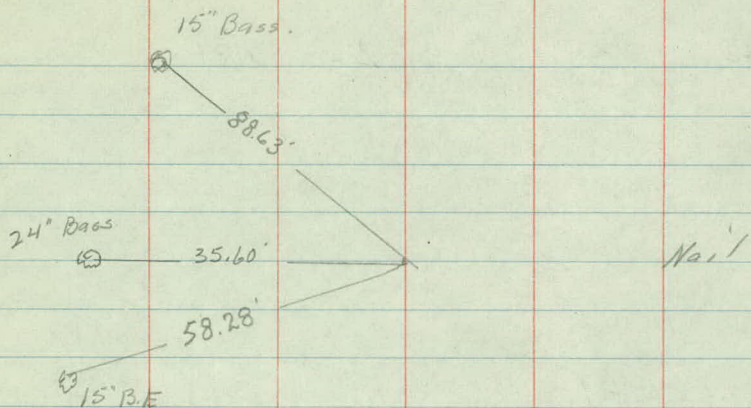
7°45'

SEE REVISED

0+00 =

13+18.95

Edgerton Str



Mon

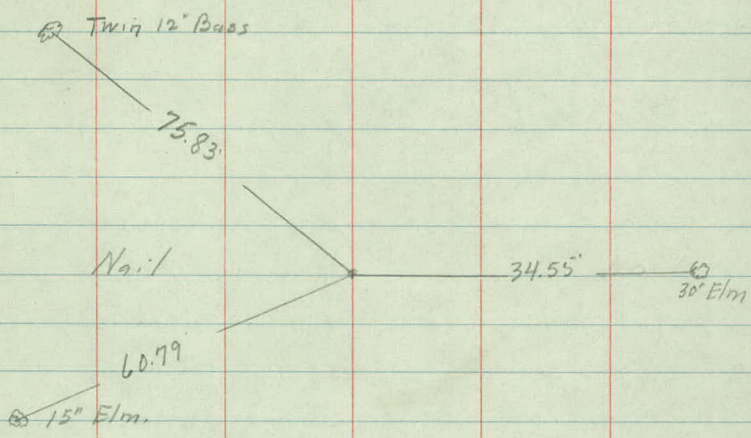
Sta	Pt	ΔL	ΔR
-----	----	------------	------------

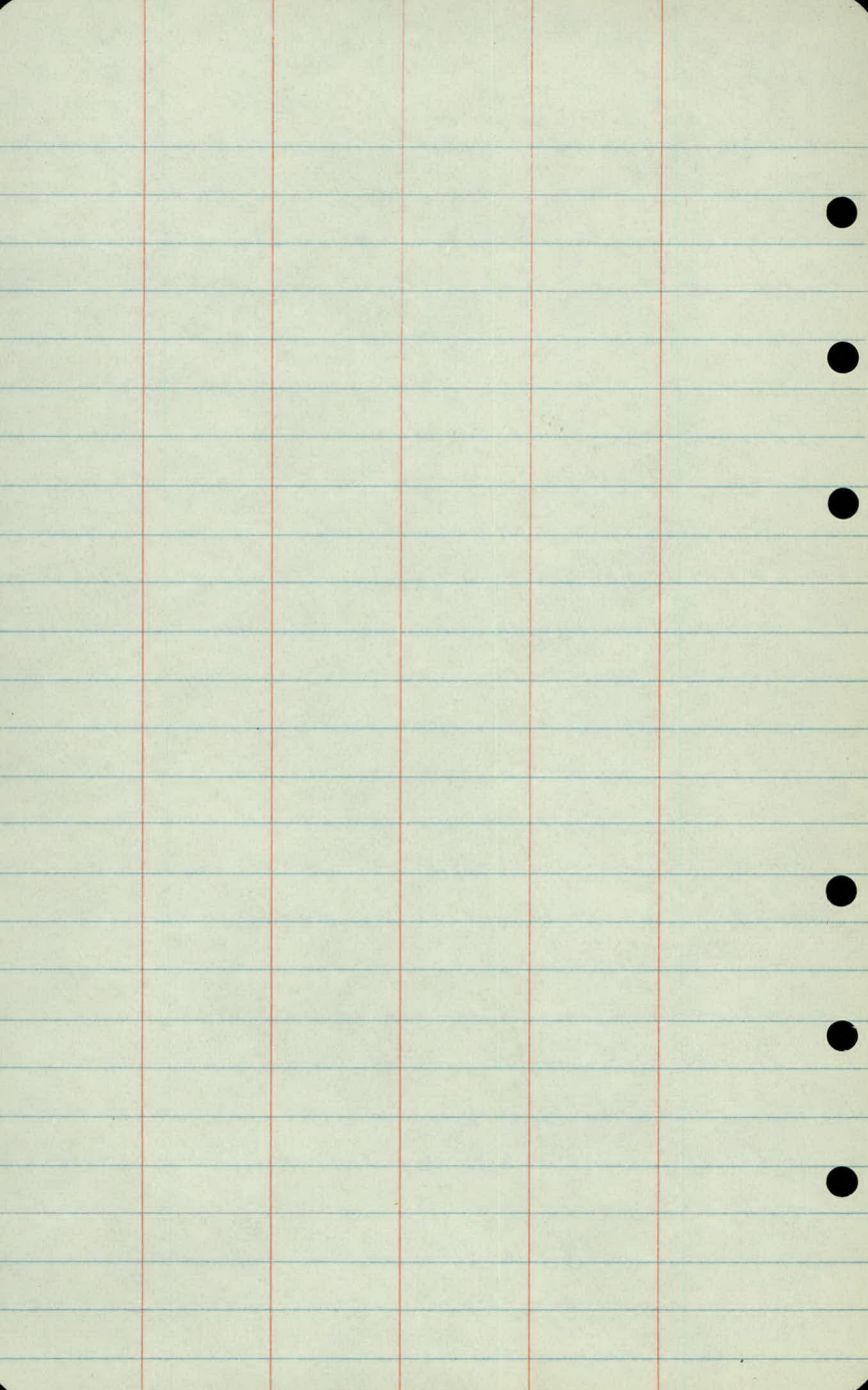
9+08.5 ⁻³	P.I.		
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		5°23'	
--	--	-------	--

7+14.5	P.O.T		
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		±	Clover Ave
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Bench levels

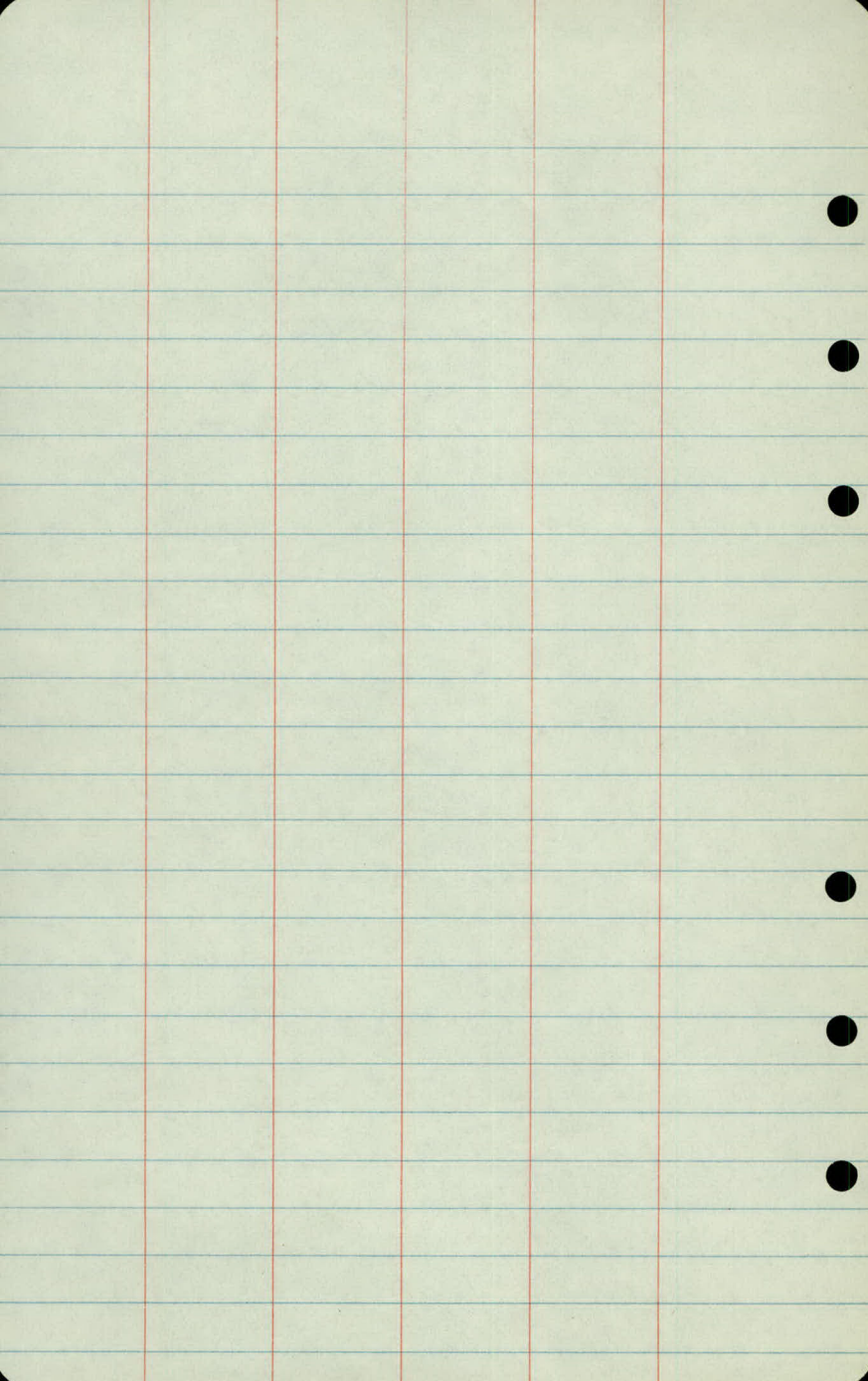
Sta	+	Δ	-	Elev
B.M.	6.22	922.28		916.06
	3.20	916.65	8.83	913.45
	3.27	912.17	7.75	908.90
B.M.	8.80	912.17	8.80	903.37
	7.67	916.69	3.15	909.02
			3.77	912.92

Description

Top Mon Edgerton + Hobbs Rd

SpK in P.P. 33' Lt. Sta 12+75 Edgerton St.

SpK P.P. N.E. Cor. Stockdale Rd + Clover Sts.



Profile Levels

Edgerton Str

Sta	+	π	-	Elev.
B.M	5.69	921.75		916.06
-1+00				14.0
-0+50				14.6
0+00				16.1
+50				17.5
1				17.4
+50				16.4
+68				15.4
2				12.8
+25				10.3
+50				09.7
3				10.2
+25				11.2

Lt.

L

Rt

9

Top Mon. Edgerton + Kohler Rels

7.8

7.2

5.7

5

4.3

6.7
Gro. at Ho.

4.4

 $\frac{+1.0}{\text{Gro at Ho}}$

5.4

6.4

 $\frac{4.4}{33}$

9.0

 $\frac{12.0}{33}$ $\frac{14.8}{\text{Ent to Ho}}$ $\frac{6.5}{33}$ 11.5 $\frac{11.8}{6}$ $\frac{9.3}{12}$ $\frac{9.8}{20}$ $\frac{12.2}{33}$

12.1

 $\frac{8.5}{33}$

11.5

10.6

Sta	+	Δ	-	Elev
		921.75		

3+50				11.6
------	--	--	--	------

4				12.1
---	--	--	--	------

T.P	3.98	916.66	907	912.68
-----	------	--------	-----	--------

+50				12.8
-----	--	--	--	------

5				13.2
---	--	--	--	------

+50				11.1
-----	--	--	--	------

6				11.0
---	--	--	--	------

+50				10.4
-----	--	--	--	------

7				11.4
---	--	--	--	------

+59				10.2
-----	--	--	--	------

+68				08.4
-----	--	--	--	------

8				08.2
---	--	--	--	------

+30				08.3
		Approx. $\pm$		Back Arc

Lt

L

Rt

10

10.2

$$\frac{9.7}{33}$$

9.7

$$\frac{12.3}{33}$$

$$\frac{14.3}{\text{Ent. Elev}}$$

$$\frac{4.7}{\text{Elev old Trail}}$$

3.9

$$\frac{5.3}{\text{Rd}}$$

$$\frac{3.1}{33}$$

3.5

5.6

$$\frac{6.7}{33 \text{ Rd}}$$

5.7

6.3

$$\frac{7.1}{33}$$

5.3

$$\frac{8.7}{33}$$

4.5

8.3

8.5

$$\frac{7.4}{50}$$

8.4

8.4

Sta	+	Σ	-	Elev
		91666		

8+50				07.6
------	--	--	--	------

9				06.6
---	--	--	--	------

T.P	6.77	91436	9.07	907.59
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+50				05.3
-----	--	--	--	------

10				04.2
----	--	--	--	------

+50				03.1
-----	--	--	--	------

11				02.5
----	--	--	--	------

+50				01.2
-----	--	--	--	------

12				02.2
----	--	--	--	------

+50				02.9
-----	--	--	--	------

13				02.8
----	--	--	--	------

+18.75				99.7
--------	--	--	--	------

+50				00.3
-----	--	--	--	------

B.M.			11.02	903.34 903.37
------	--	--	-------	---------------

Lt

L

Rt

9.1

10.1

 $\frac{10.0}{Rd}$

9.1

10.2

 $\frac{9.3}{Rd}$

11.3

11.9

 $\frac{10.6}{Rd}$

13.2

12.2

 $\frac{10.5}{Rd}$

11.5

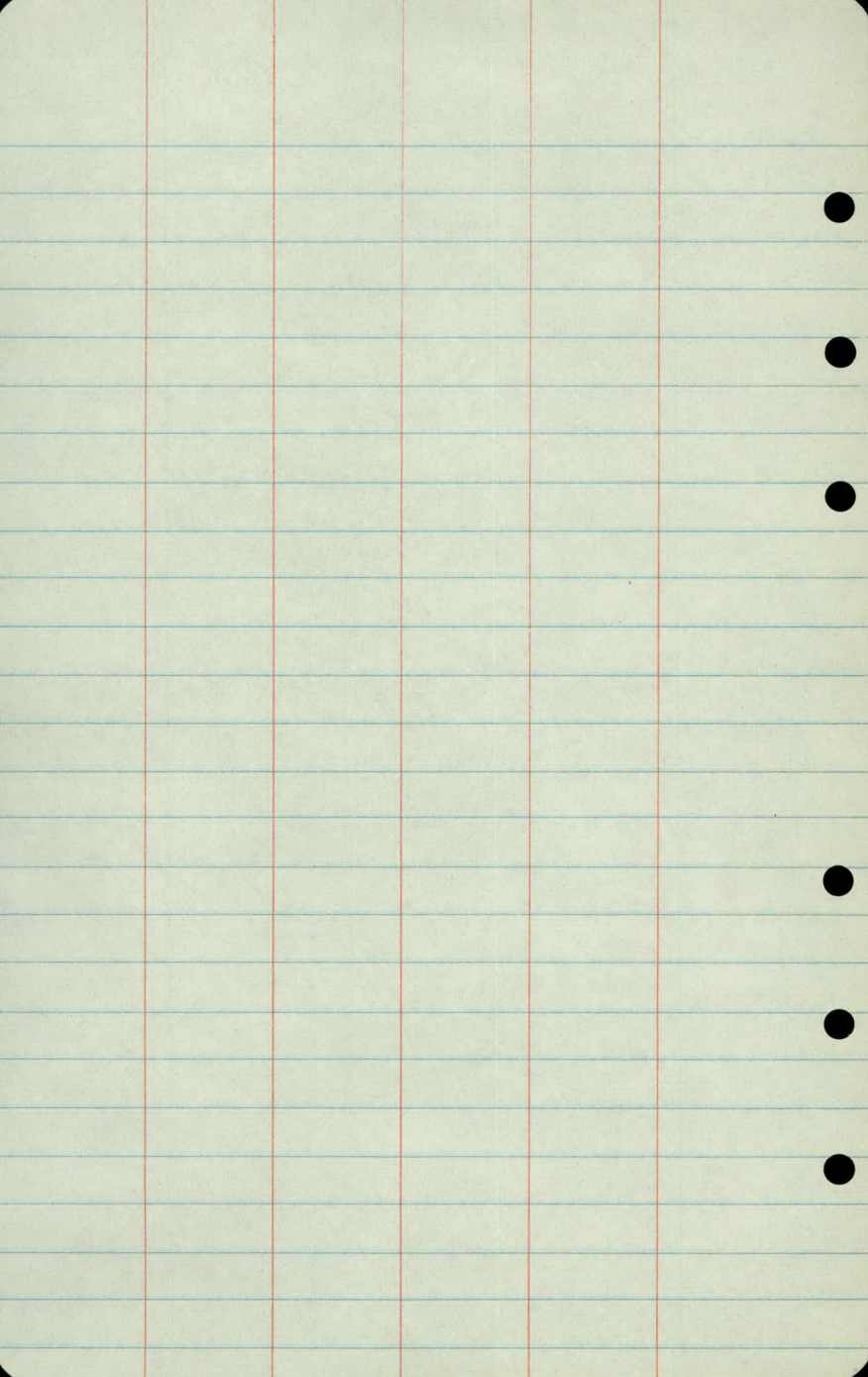
 $\frac{141}{33}$ $\frac{13.6}{6}$

11.6

14.7

14.1

Spk in P.P. 33' Lt 12+75



Profile Levels

Stockdale Rd

Sta	+	π	-	Elev
B.M	11.02	914.39.		903.37
0+00				99.7.

+50				02.9.
-----	--	--	--	-------

1				05.3.
---	--	--	--	-------

+50				08.3.
-----	--	--	--	-------

+72				13.3.
-----	--	--	--	-------

2				12.5.
---	--	--	--	-------

+15				10.1.
-----	--	--	--	-------

+50				08.4.
-----	--	--	--	-------

3				06.8.
---	--	--	--	-------

+50				06.8.
-----	--	--	--	-------

4				08.4.
---	--	--	--	-------

T.P	6.52	917.26.	3.65	910.74.
-----	------	---------	------	---------

+50				11.3.
-----	--	--	--	-------

Lt.

L

Rt

$$\frac{14.1}{33}$$

14.7

$$\frac{10.1}{33}$$

11.5

$$\frac{9.4}{Rd}$$

9.1

$$\frac{5.4}{Rd}$$

6.1

1.1

1.9

4.3

6.0

$$\frac{5.3}{Rd}$$

7.6

$$\frac{6.8}{Rd}$$

7.6

6.0

6.0

Sta	+	π	-	Elev
-----	---	-------	---	------

917.26

4+72				11.8.
------	--	--	--	-------

5				12.5.
---	--	--	--	-------

+23				12.6.
-----	--	--	--	-------

+61				10.4.
-----	--	--	--	-------

+77				11.3.
-----	--	--	--	-------

6				10.8.
---	--	--	--	-------

+25				11.0.
-----	--	--	--	-------

+50				10.0.
-----	--	--	--	-------

+75				09.1.
-----	--	--	--	-------

7				09.3.
---	--	--	--	-------

+15				09.6.
-----	--	--	--	-------

B.M

4.35 912.91 912.92

Lt

L

Rt

5.5

4.8

4.7

6.9

6.0

6.5

$$\frac{8.3}{Rd}$$

6.3

7.3

8.2

8.0

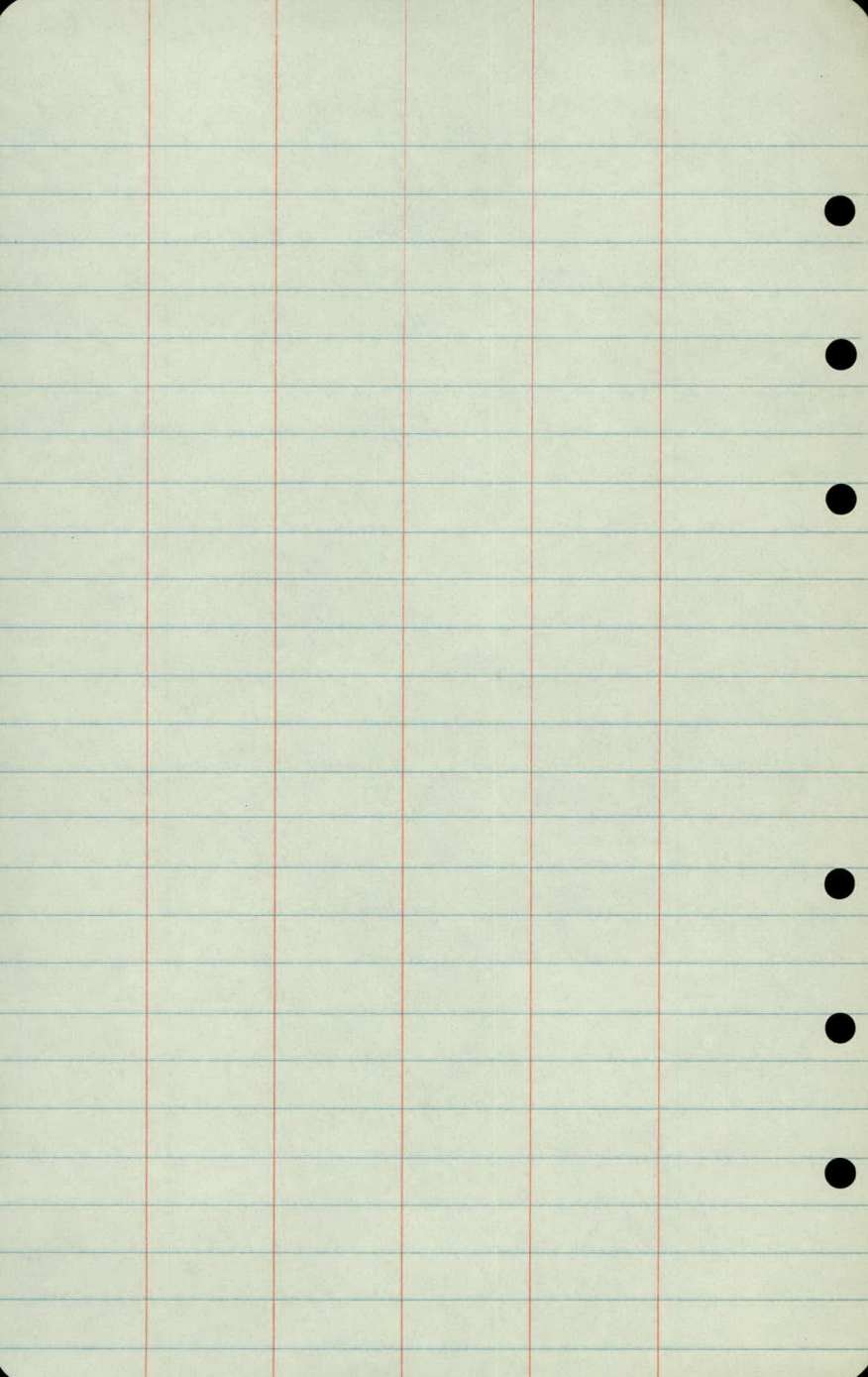
$$\frac{8.8}{Rd}$$

$$\frac{5.1}{5.0}$$

7.7

$$\frac{8.8}{Rd}$$

Sp K. in P.P. N.E Cor Stockdale Rd & Clover St



Clearing & Grubbing

Stockdale Rd

LA

L

R+

Stg

Trees

0+00

1

1

32

2

3

1

2

3

2

4

4

2

5

6

18

7

Lt.

2

Rt

16

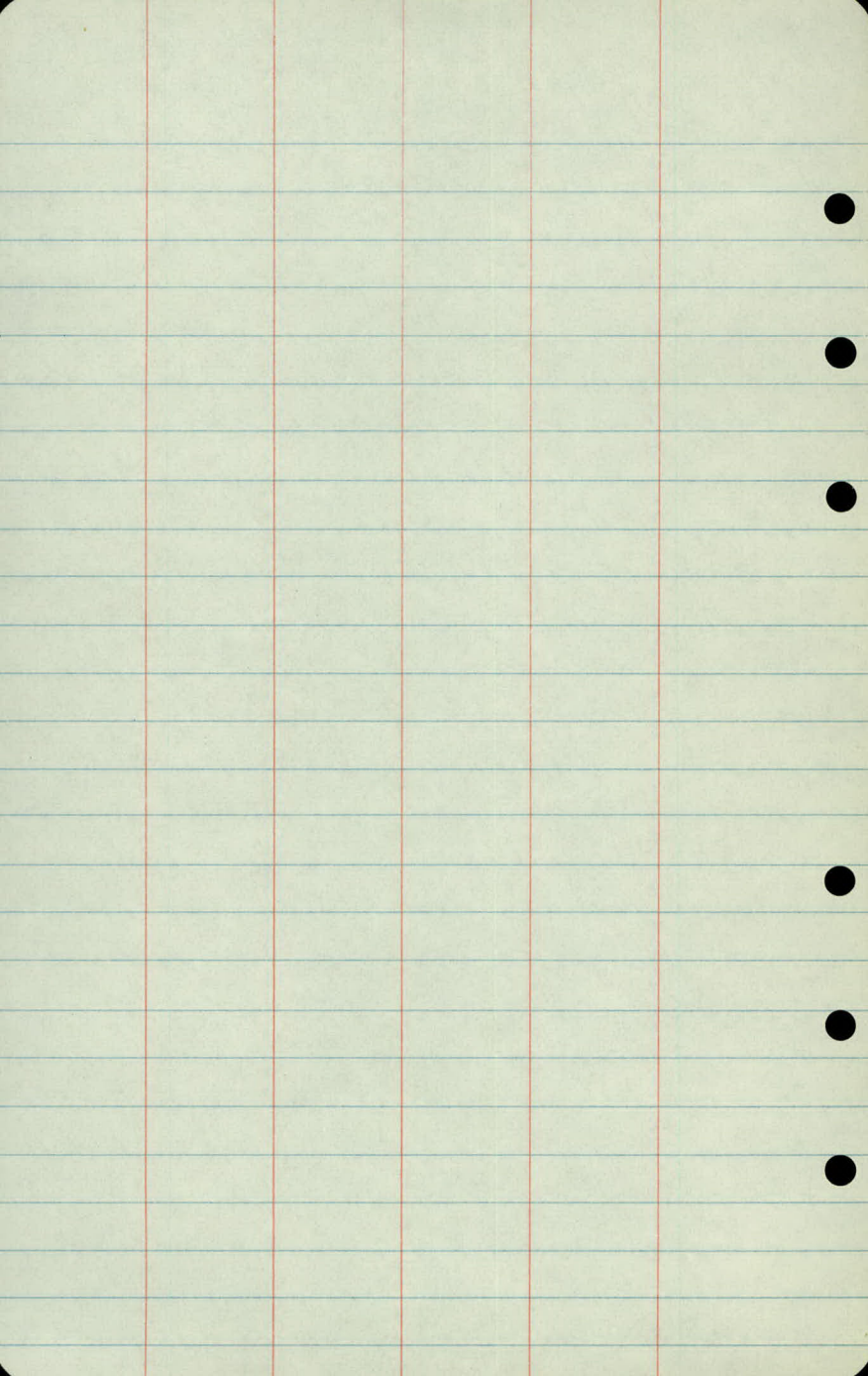
Stumps

/

/

/

/



Clearing + Grubbing

Edgerton Str.

Lt

L

Rt

Sta

Trees

0

2

1

2

2

2

3

1

4

5

4

6

4

7

3

8

Lt

£

Rt

stumps

1

2

2

1

1

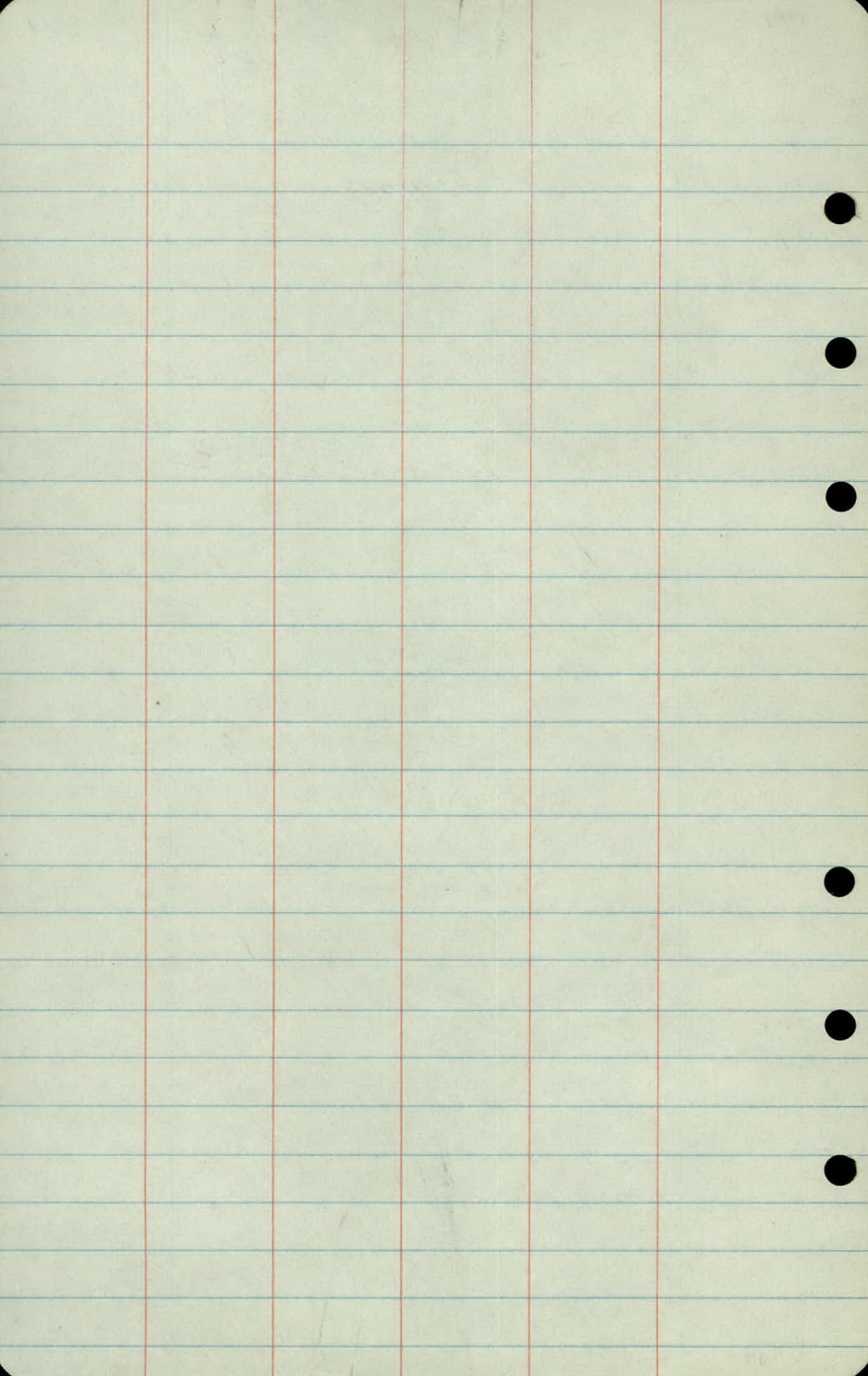
1

9

8

7

1



Edgerton Str.

Slope Stakes

Sta	+	π	-	Elev	
B.M	6.97	923.03		916.06	
-1+00				14.0	13.5
-0+50				14.4	13.9
0+00				14.6	14.1
+50				14.7	14.2
1				14.6	14.1
+50				14.3	13.8
+68				14.1	13.6
2				13.9	13.4
+25				13.7	13.2
+50				13.5	13.0
3				13.1	12.6
+25				12.9	12.4

L +

X

R +

Gr Rod Ditch

Top Man Edgerton + Kohler Rd

9.0 9.5

3.5

$$8.6 \quad 9.1 \quad \begin{array}{r} 8.8 \\ 0.3 \\ \hline 15.6 \end{array}$$

$$7.8 \\ 0.8$$

$$\begin{array}{r} 8.6 \\ 0.5 \\ \hline 16.0 \end{array}$$

$$8.4 \quad 8.9 \quad \begin{array}{r} 7.1 \\ 1.8 \\ \hline 18.6 \end{array}$$

$$\begin{array}{r} 7.2 \\ 1.2 \\ \hline \end{array}$$

$$\begin{array}{r} 8.1 \\ 0.8 \\ \hline 16.6 \end{array}$$

$$8.3 \quad 8.8 \quad \begin{array}{r} 6.2 \\ 2.6 \\ \hline 20.2 \end{array}$$

$$\begin{array}{r} 5.8 \\ 2.6 \\ \hline \end{array}$$

$$\begin{array}{r} 6.9 \\ 1.9 \\ \hline 18.8 \end{array}$$

$$8.4 \quad 8.9 \quad \begin{array}{r} 4.6 \\ 4.3 \\ \hline 23.6 \end{array}$$

$$\begin{array}{r} 5.7 \\ 0.3 \\ \hline \end{array}$$

$$\begin{array}{r} 7.1 \\ 1.8 \\ \hline 18.6 \end{array}$$

$$8.7 \quad 9.2 \quad \begin{array}{r} 5.1 \\ 4.1 \\ \hline 23.2 \end{array}$$

$$\begin{array}{r} 6.9 \\ 1.8 \\ \hline \end{array}$$

$$\begin{array}{r} 7.9 \\ 1.3 \\ \hline 17.6 \end{array}$$

$$8.9 \quad 9.4 \quad \begin{array}{r} 6.1 \\ 3.3 \\ \hline 21.6 \end{array}$$

$$\begin{array}{r} 7.7 \\ 1.2 \\ \hline \end{array}$$

$$\begin{array}{r} 8.5 \\ 0.9 \\ \hline 16.8 \end{array}$$

$$9.1 \quad 9.6 \quad \begin{array}{r} 8.5 \\ 1.1 \\ \hline 17.2 \end{array}$$

$$\begin{array}{r} 10.2 \\ 1.1 \\ \hline \end{array}$$

$$\begin{array}{r} 16.6 \\ 1.0 \\ \hline 17.0 \end{array}$$

$$9.3 \quad 9.8 \quad \begin{array}{r} 10.4 \\ 0.6 \\ \hline 16.2 \end{array}$$

$$\begin{array}{r} 12.7 \\ 3.4 \\ \hline \end{array}$$

$$\begin{array}{r} 10.7 \\ 0.9 \\ \hline 16.8 \end{array}$$

$$9.5 \quad 10.0 \quad \begin{array}{r} 12.3 \\ 2.3 \\ \hline 19.6 \end{array}$$

$$\begin{array}{r} 13.5 \\ 4.0 \\ \hline \end{array}$$

$$\begin{array}{r} 11.7 \\ 1.7 \\ \hline 18.4 \end{array}$$

$$9.9 \quad 10.4 \quad \begin{array}{r} 12.2 \\ 1.8 \\ \hline 18.6 \end{array}$$

$$\begin{array}{r} 12.9 \\ 3.0 \\ \hline \end{array}$$

$$\begin{array}{r} 11.7 \\ 1.3 \\ \hline 17.6 \end{array}$$

$$10.1 \quad 10.6 \quad \begin{array}{r} 11.1 \\ 0.5 \\ \hline 16.0 \end{array}$$

$$\begin{array}{r} 11.9 \\ 1.8 \\ \hline \end{array}$$

$$\begin{array}{r} 11.4 \\ 0.8 \\ \hline 16.6 \end{array}$$

Sta	+	·	-	Elev
		923.03		
3+50				12.7 12.2

4				12.3 11.8
T.P.	465	917.35	10.33	912.70
+50				11.9 11.4

5				11.5 11.0
+50				11.0 10.5

6				10.4 09.9
+50				09.9 09.4

7				09.3 08.8
T.P.	432	914.06	7.61	909.74
+59				08.5 08.0

+68				08.4 7.9
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8				08.1 7.6
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+30				07.7
T.P.	5.24	911.16	8.14	905.92

L+

R

R+

Gr Rd Ditch Gr.

10.3 10.8
 $\frac{10.8}{C0.0/15.0}$

11.4
 F1.1

11.4
 $\frac{F0.6}{16.2}$

10.7 11.2
 $\frac{11.2}{C0.0/15.0}$

11.0
 F0.3

10.3
 $\frac{C0.9}{16.8}$

5.5 6.0
 $\frac{4.5}{C1.5/18.0}$

4.5
 C1.0

4.6
 $\frac{C1.4}{17.8}$

5.9 6.4
 $\frac{3.9}{C2.5/20.0}$

4.1
 C1.8

5.1
 $\frac{C1.3}{17.6}$

6.4 6.9
 $\frac{5.0}{C1.9/18.8}$

6.3
 C0.1

6.3
 $\frac{C0.4}{16.2}$

7.0 7.5
 $\frac{6.3}{C1.2/17.4}$

6.4
 C0.6

5.9
 $\frac{C1.6}{18.2}$

7.5 8.0
 $\frac{7.7}{C0.3/15.6}$

6.9
 $\frac{C1.1}{17.2}$

8.1 8.6
 $\frac{7.8}{C0.8/16.4}$

6.0
 C2.1

8.4
 $\frac{C0.7}{15.4}$

5.6 6.1
 $\frac{4.4}{C2.2/20.0}$

4.6
 C2.0

5.7
 $\frac{C1.4}{17.8}$

6.7 7.2

No stakes

7.0 7.5
 $\frac{2.7}{C4.8/24.4}$

1
 C0.1

6.1
 $\frac{C1.4}{17.8}$

7.4 7.9

No stakes

Sta + π - Elev

911.16

8+50

07.5

07.0

9

06.9

06.4

+50

06.3

05.8

T.P.

711.16

05.92

10

05.7

05.2

+50

05.1

04.6

11

04.5

04.0

+50

03.9

03.4

12

03.3

02.8

+50

02.7

02.2

B.M.

786

903.30

903.37

13

02.1

01.6

+18.75

01.8

01.3

+50

01.5

01.0

Lt.

Z

Rt

4.7 52

$$\begin{array}{r} 2.8 \\ C 2.4 \\ \hline 19.8 \end{array}$$

$$\begin{array}{r} 3.5 \\ C 1.1 \\ \hline \end{array}$$

$$\begin{array}{r} 3.9 \\ C 1.3 \\ \hline 17.2 \end{array}$$

53 58

$$\begin{array}{r} 4.6 \\ C 1.2 \\ \hline 17.4 \end{array}$$

$$\begin{array}{r} 4.5 \\ C 0.7 \\ \hline \end{array}$$

$$\begin{array}{r} 4.4 \\ C 1.4 \\ \hline 17.8 \end{array}$$

59 64

$$\begin{array}{r} 5.9 \\ C 0.5 \\ \hline 16.0 \end{array}$$

$$\begin{array}{r} 5.9 \\ C 0.0 \\ \hline \end{array}$$

$$\begin{array}{r} 5.3 \\ C 1.1 \\ \hline 17.2 \end{array}$$

5.5 60

$$\begin{array}{r} 6.8 \\ F 0.8 \\ \hline 16.6 \end{array}$$

$$\begin{array}{r} 7.0 \\ F 1.5 \\ \hline \end{array}$$

$$\begin{array}{r} 6.1 \\ F 0.1 \\ \hline 15.2 \end{array}$$

6.1 66

$$\begin{array}{r} 7.6 \\ F 1.0 \\ \hline 17.0 \end{array}$$

$$\begin{array}{r} 8.2 \\ F 2.1 \\ \hline \end{array}$$

$$\begin{array}{r} 6.8 \\ F 0.2 \\ \hline 15.4 \end{array}$$

6.7 72

$$\begin{array}{r} 8.6 \\ F 1.4 \\ \hline 17.8 \end{array}$$

$$\begin{array}{r} 8.7 \\ F 2.0 \\ \hline \end{array}$$

$$\begin{array}{r} 7.5 \\ F 0.3 \\ \hline 15.6 \end{array}$$

7.3 78

$$\begin{array}{r} 9.8 \\ F 2.0 \\ \hline 19.0 \end{array}$$

$$\begin{array}{r} 10.1 \\ F 2.8 \\ \hline \end{array}$$

$$\begin{array}{r} 7.7 \\ C 0.1 \\ \hline 15.2 \end{array}$$

7.9 84

$$\begin{array}{r} 10.2 \\ F 1.8 \\ \hline 18.6 \end{array}$$

$$\begin{array}{r} 9.1 \\ F 1.2 \\ \hline \end{array}$$

$$\begin{array}{r} 7.9 \\ C 0.5 \\ \hline 16.0 \end{array}$$

8.5 90

$$\begin{array}{r} 10.4 \\ F 1.4 \\ \hline 17.8 \end{array}$$

$$\begin{array}{r} 7.9 \\ C 0.2 \\ \hline \end{array}$$

$$\begin{array}{r} 8.2 \\ C 0.8 \\ \hline 16.6 \end{array}$$

9.1 96

$$\begin{array}{r} 11.2 \\ F 1.4 \\ \hline 18.2 \end{array}$$

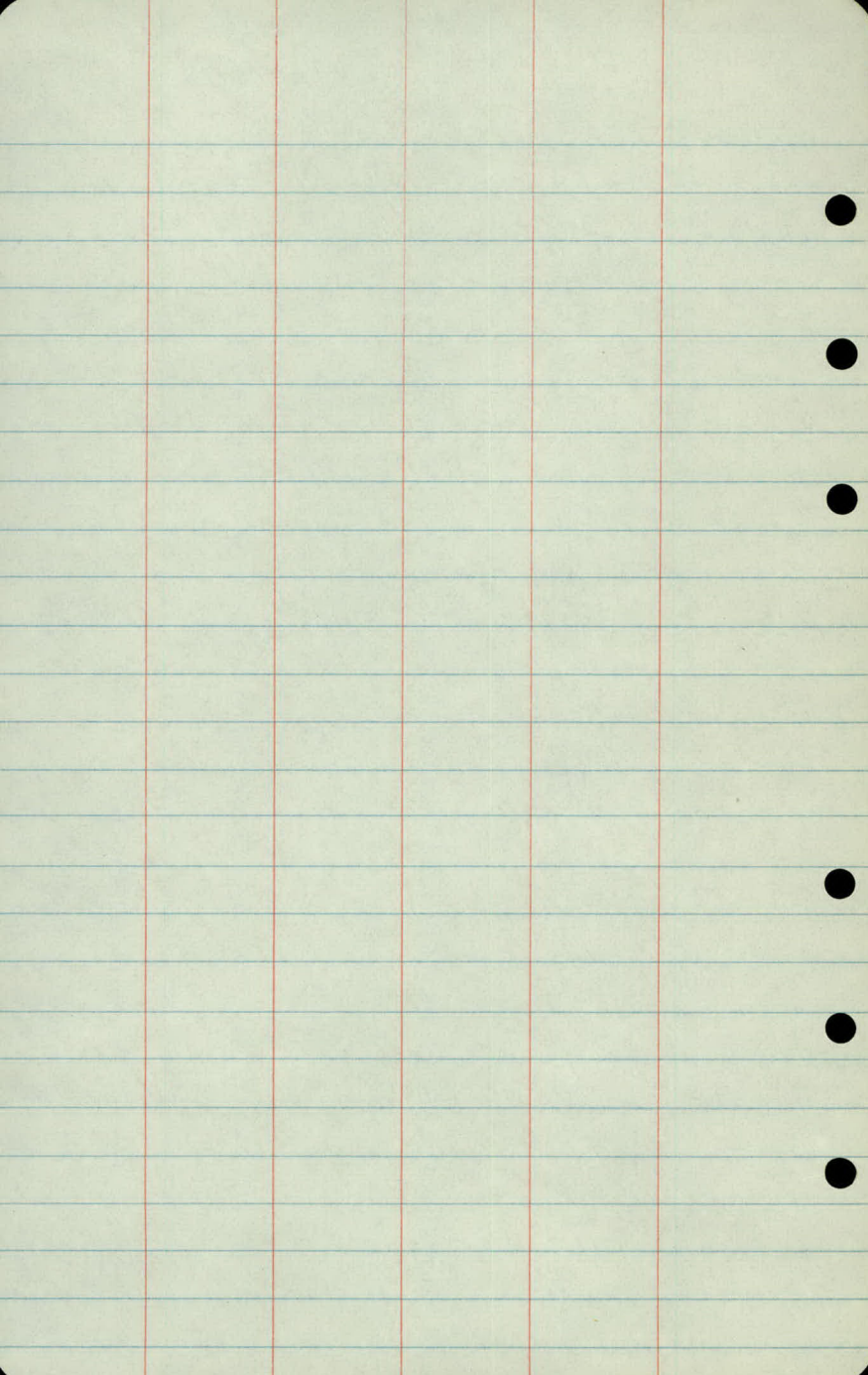
$$\begin{array}{r} 8.5 \\ C 0.2 \\ \hline \end{array}$$

$$\begin{array}{r} 7.3 \\ C 2.3 \\ \hline 19.6 \end{array}$$

9.7 10.2

$$\begin{array}{r} 11.6 \\ F 1.4 \\ \hline 17.8 \end{array}$$

$$\begin{array}{r} 11.2 \\ F 1.5 \\ \hline \end{array}$$



Stockdale Rd

Slope Stakes

Sta	+	Δ	-	Elev	
B.M	7.85	911.22		903.37	
0+00				01.8	01.3

+50			02.9	03.1	02.6
-----	--	--	------	------	------

1			05.3	04.4	03.9
---	--	--	------	------	------

+50				05.7	05.2
-----	--	--	--	------	------

T.P	4.79	915.11	0.85	910.37	
-----	------	--------	------	--------	--

+72				06.2	
-----	--	--	--	------	--

2			12.5	06.8	06.3
---	--	--	------	------	------

+50				07.8	7.3
-----	--	--	--	------	-----

3			06.8	08.7	08.2
---	--	--	------	------	------

+50				09.6	09.1
-----	--	--	--	------	------

4			08.4	10.4	09.9
---	--	--	------	------	------

+50				11.4	10.9
-----	--	--	--	------	------

T.P	7.86	918.72	3.30	911.86	
-----	------	--------	------	--------	--

Lt

±

Rt

Spk in P.P. 33 Lt Sta 12+75

9.4 99

8.1 86
8.6
C0.08.5
F046.2
C2.4
19.86.8 7.3
6.6
C0.7/16.45.9
C0.94.5
C2.8
20.65.5 6.0
3.4
C2.6
20.22.9
C2.62.0
C4.0
23.0

No Sta Kcs

8.4 8.9
3.1
C5.8
26.62.9
C5.53.0
C5.9
26.87.4 7.9
6.9
C1.0
17.06.8
C0.66.2
C1.7
18.46.5 7.0
7.1
F2.1
19.28.3
F1.87.9
F0.9
16.85.6 6.1
8.9
F2.8
20.68.4
F2.88.0
F1.9
18.84.8 5.3
7.4
F2.1
19.26.8
F2.06.9
F1.6
18.23.8 4.3
4.3
C0.0
15.04.0
F0.23.6
C0.7
16.4

Sta	+	Δ	-	Elev
		91872		
4+72				11.3 108
5			12.5	115 110
+25				115 110
+61				114 109
+77				11.3 108
6			0.3	11.1 106
+25				10.9 10.4
+50				10.6 10.1
+75				10.4 09.9
7				10.1 09.6
+25				10.0 09.5
B.M			5.80	912.92

LH

Z

RH

7.4 79 $\frac{6.8}{C1.1/17.2}$ 6.9
C0.5 $\frac{6.3}{C1.5/18.2}$ 7.2 77 $\frac{6.1}{C1.4/18.2}$ 6.2
C1.0 $\frac{6.0}{C1.7/18.4}$ 7.2 77 $\frac{4.8}{C2.6/10.8}$ 6.2
C1.0 $\frac{7.1}{C0.6/16.2}$ 7.3 78 $\frac{5.7}{C2.1/19.2}$ 7.7
F0.4 $\frac{10.2}{F2.5/20.0}$

7.4 79

No Stock

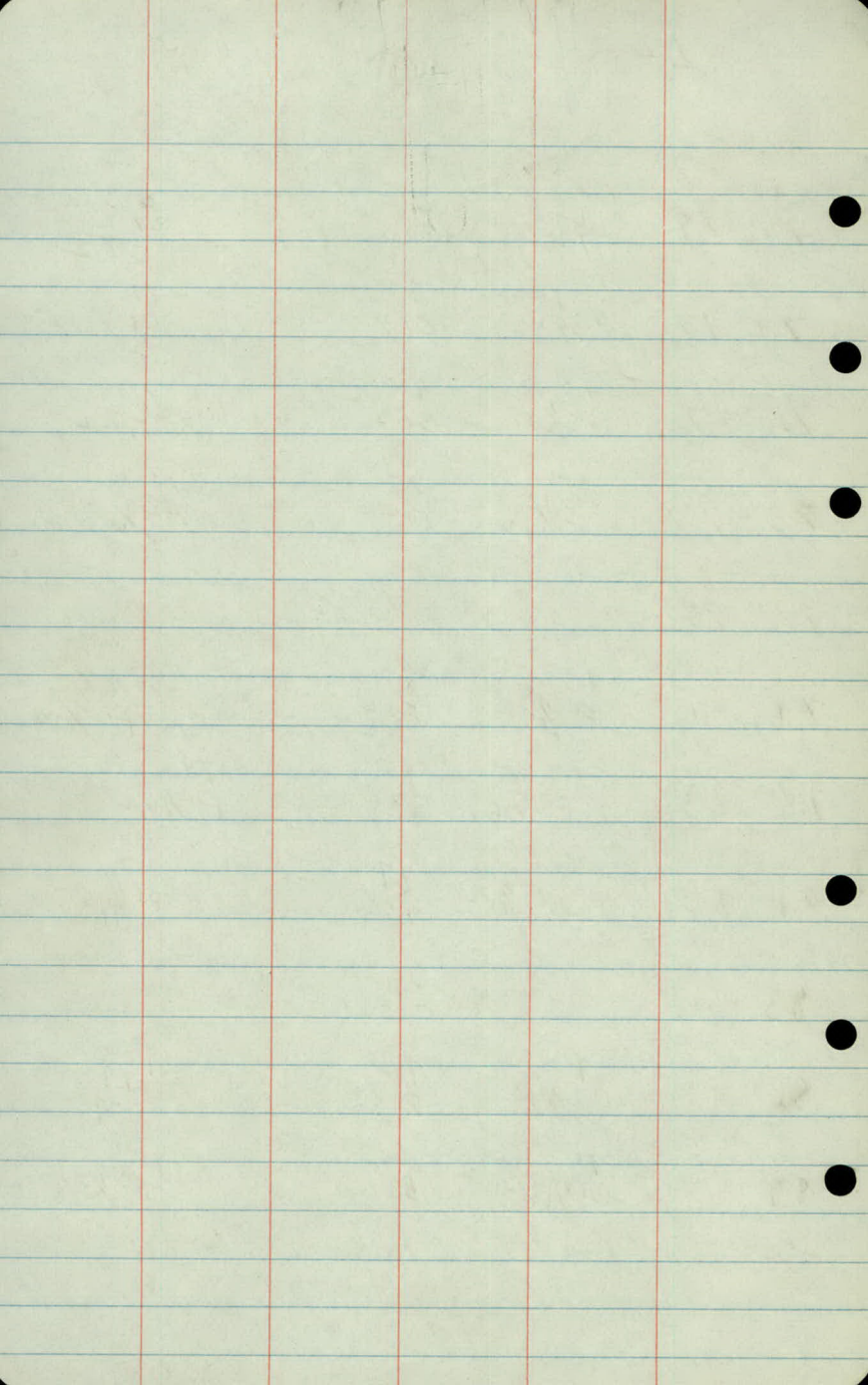
7.6 81 $\frac{8.3}{F0.2/15.4}$ 8.0
F0.4 $\frac{9.9}{F1.8/18.2}$ 7.8 83 $\frac{8.7}{F0.4/15.8}$ 7.8
F0.0 $\frac{9.9}{F1.2/18.2}$ 8.1 86 $\frac{8.4}{C0.2/15.4}$ 8.7
F0.6 $\frac{10.0}{F1.4/17.8}$

8.3 88

No Stock

8.6 9.1 $\frac{9.8}{C1.3/17.8}$ 9.6
F1.0 $\frac{10.2}{F1.1/17.2}$ 8.7 9.2 $\frac{9.4}{C1.8/18.4}$ 9.5
F0.8 $\frac{10.1}{F0.9/18.8}$

SpH. P.P N.E. Cor Stockdale Clover





97.79
1 45
—
.34

92.79
4.25
—
88 54

Wright

Barnes

1840

Deary

504

18 or 19

17-401 - *Chrysophanes*

15416 ?

330

660

217,800

586E

Blue Type

Stockdale Rd

Sta	+	π	-	Elev	
BM	9.39	912.76		903.37	
0+00				01.8	01.3
+50				03.1	02.1
1				04.4	03.9
+50				05.7	05.2
+72				06.2	05.7
2				06.8	06.3
+15					
+50				07.8	07.3
3				08.7	09.2
+50				09.5	09.1
4				10.4	09.9
+50				11.4	10.9
T.R	5.24	916.13	1.87	910.89	

Lt

±

Rt

Spk in P.P 33' Lt Sta 12+75

9.7

10.2

Br.

C/O

8.9 9.9

M1

C/O

7.6 6.6

C.O.C.O.
BT

7.1 6.1

C.O.
B.TC.O.
B.T

6.5

C.O.
BTC.O.
B.T

5.5 5.0

Grade

4.6

Grade

3.7

Grade

2.9

Grade

1.9

Sta	r	π	-	Elev
		916.13		
4+72				11.3 10.8
5				11.5 11.0
+25				11.5 11.0
+61				11.4 10.9
+77				11.3 10.8
6				11.1 10.6
+25				10.9 10.4
+50				10.6 10.1
+75				10.4 09.9
7				10.1 09.6
+25				10.0 09.5
BM		3.21		912.92

2+

L

R+

5.3

5.1

5.1

5.2

5.3

5.5

5.7

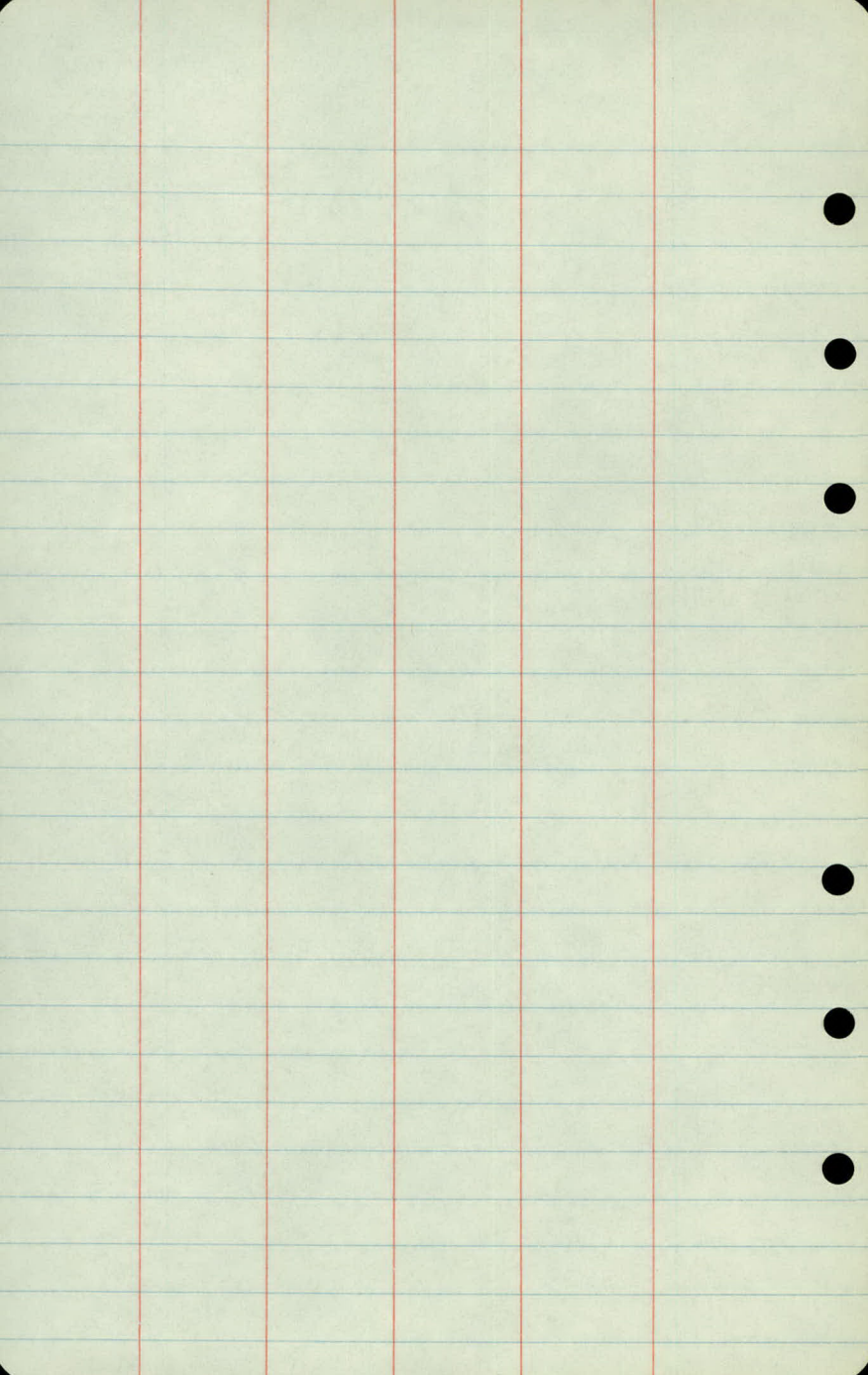
6.0

6.2

6.5

6.6

Spk in P.P.



Blue Tops

Edgerton Str

10/4/1

Sta	+	π	-	Elev	
				90337	
-0+50				14.4	13.9
0+00				14.6	14.1
+50				14.7	14.2
1				14.6	14.1
+50				14.3	13.8
	6.36	919.77	332	913.41	
2				13.9	13.4
+50				13.5	13.0
3				13.1	12.6
+50				12.7	12.2
4				12.3	11.8

5.7

$\frac{3.7}{C2.0}$

$\frac{4.7}{C1.4}$

5.6

$\frac{3.6}{C1.4}$

$\frac{3.6}{C2.0/BT}$

5.7

$\frac{3.7}{C2.0/BT}$

$\frac{4.7}{C1.0/BT}$

1.0

BT

BT

3.3

BT

BT

3.7

BT

BT

4.1

BT

BT

4.5

$\frac{B.T}{g}$

$\frac{4.5}{B.T/g}$

4.9

$\frac{B.T}{g}$

$\frac{4.9}{B.T}$

4+50

11.9

11.4

5

11.5

11.0

+50

11.0

10.5

6

10.4

9.9

+50

09.9

6.99 9/16.73

909.74

B.M

2.52 9/12.26

909.74

16+50

09.9

09.4

7

09.3

08.8

+50

08.5

08.0

8

08.1

07.6

+50

07.5

07.0

9

06.9

06.4

5.3

$$\begin{array}{r} 4.3 \\ B.T \\ \hline C1.0 \end{array}$$

G./BT

5.7

$$\begin{array}{r} 4.7 \\ C1.0 \\ \hline B.T \end{array}$$

B.T

6.2

$$\begin{array}{r} 5.2 \\ C1.0 \\ \hline B.T \end{array}$$

BT

6.8

$$\begin{array}{r} 5.8 \\ C1.0 \\ \hline B.T \end{array}$$

$$\begin{array}{r} C1.0 \\ B.T \end{array}$$

7.9

$$\begin{array}{r} 1.9 \\ B.T \\ \hline C1.0 \end{array}$$

$$\begin{array}{r} 2.9 \\ B.T \end{array}$$

3.5

$$\begin{array}{r} 2.5 \\ C1.0 \\ \hline B.T \end{array}$$

$$\begin{array}{r} 3.5 \\ B.T \end{array}$$

4.3

$$\begin{array}{r} 4.3 \\ B.T \end{array}$$

$$\begin{array}{r} 4.3 \\ B.T \end{array}$$

4.7

C2.0

$$\begin{array}{r} 4.7 \\ B.T \end{array}$$

5.3

$$\begin{array}{r} 4.3 \\ C1.0 \end{array}$$

$$\begin{array}{r} 5.3 \\ B.T \end{array}$$

5.9

$$\begin{array}{r} 4.9 \\ C1.0 \end{array}$$

$$\begin{array}{r} 4.9 \\ C1.0 \end{array}$$

Sta	+	π	-	Elev	
		912.26			
9+50				06.3	05.8
10				05.7	05.2
	3.20	908.37	7.09	904.17	
+50				05.1	04.6
11				04.5	04.0
+50				03.9	03.4
12				03.3	02.8
+50				02.7	02.2
13				02.1	01.6
+50				01.5	01.0
		5.03		903.37	

27

2

R1

6.5

6.5
B.T6.5
B.T

7.1

7.1
B.T13.7
7.1

3.8

3.8
B.T3.8
B.T

4.4

4.4
B.T4.4
B.T

5.0

5.0
B.T5.0
B.T

5.6

5.6
B.T4.6
C.T. 0

6.2

