

Bk 23- Dr. 12

OFFICE OF COUNTY ENGINEER
RAMSEY CO. MINN.

_____ Plan _____ Survey _____

_____ COUNTY ROAD "D" _____

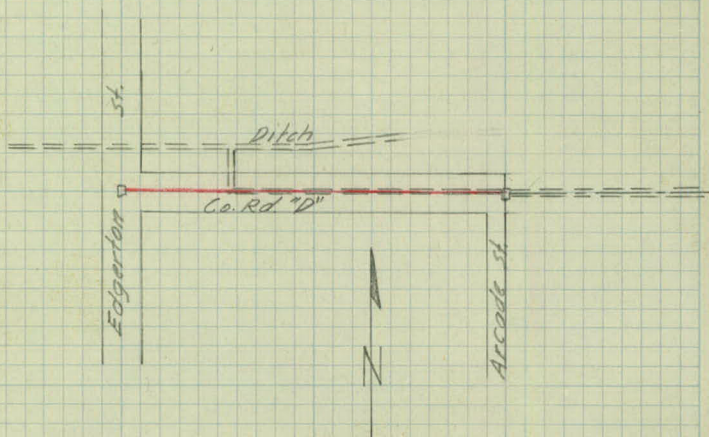
From Edgerton St. To Arcade St _____

Road Acc't. No. _____

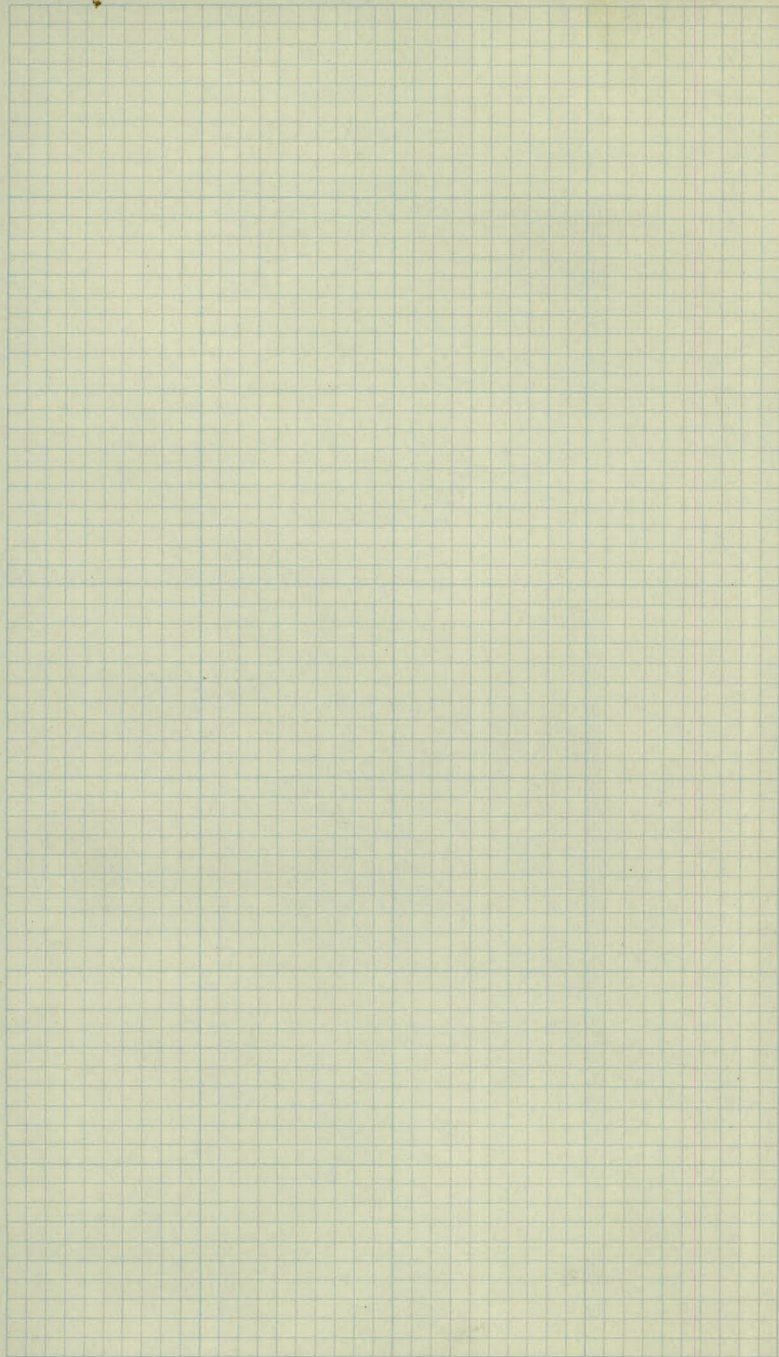
Date Filed 10-26-35 _____

File _____

PLAN SURVEY
CO. RD. "D"
Edgerton St. to Arcade St.



INDEX	
Align	- 1-2
Topog	- 3-7
X Sections	- 8-14



1

Alignment

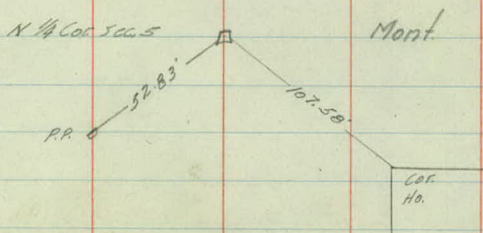
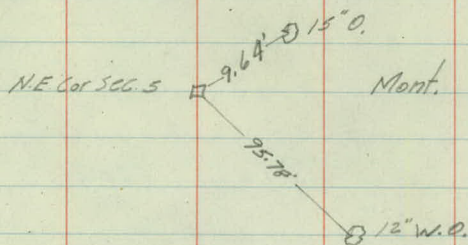
Sta	Point	ΔLt	ΔRt
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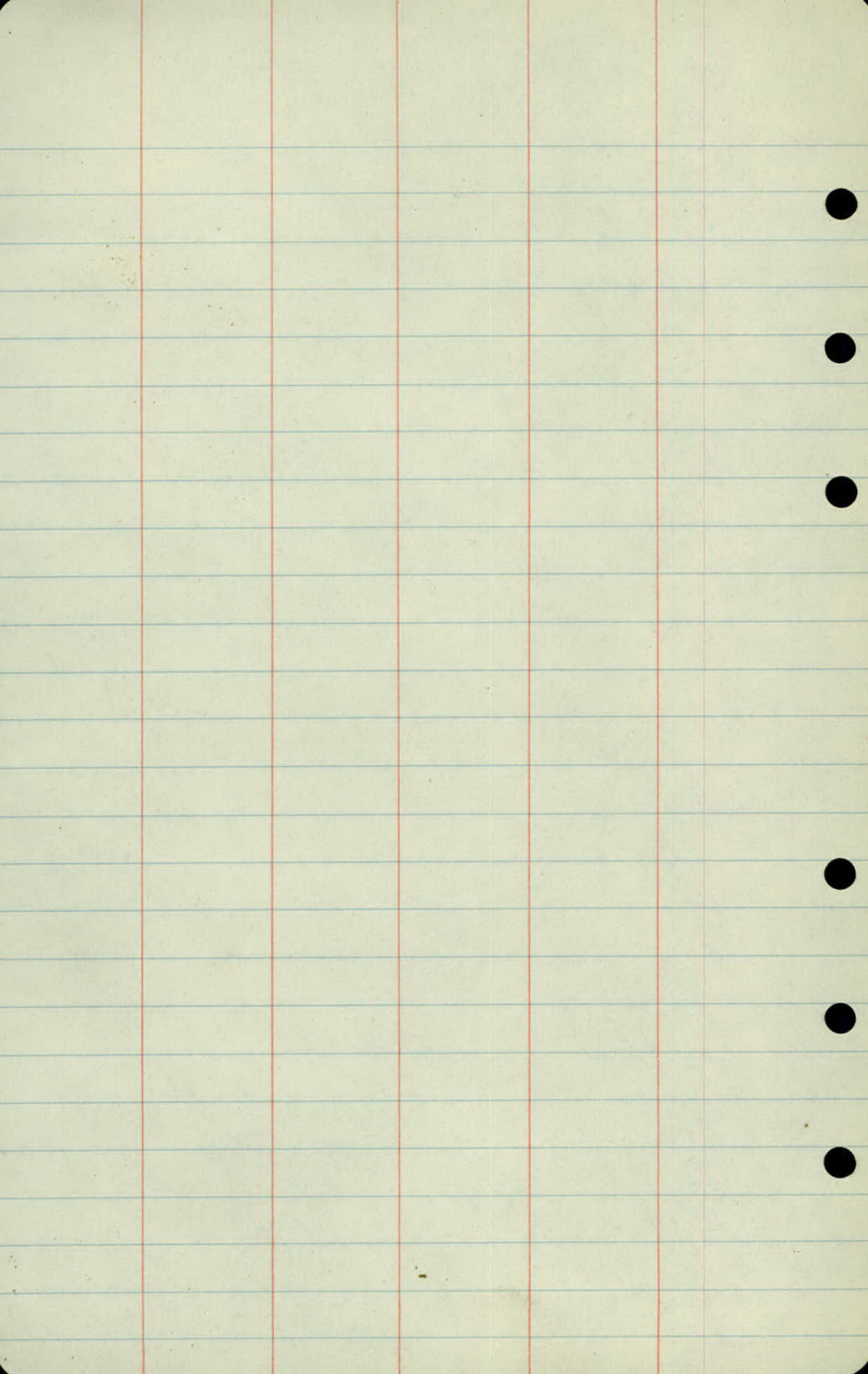
26	+32.18 = E Arcade St		
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0	+100 = E Edgerton St		
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9/5/39
K.A.
L.G.
M.B.

2





Topography

93-18" Poplar-1'

150-15" Poplar-1'

151-12" Poplar-2'

5 113-18" Tree Willow-2'
FC-3'

116-Dim Ditch-3'
117-Brush-15'

118-Beg. Brush & Trees
156-End

149-1st of Ditches-128'

4 3' Bottom
107-Dim Ditch-4'
FC-0.0 103-16" Elm-39'
180-Beg. Brush

3 Pitch-126' FC-1'

163-End Brush

112-3" Elm-3'

2 FC-0.0

170-Beg. Brush

1 120-8" Elm-1'

FC 0.0

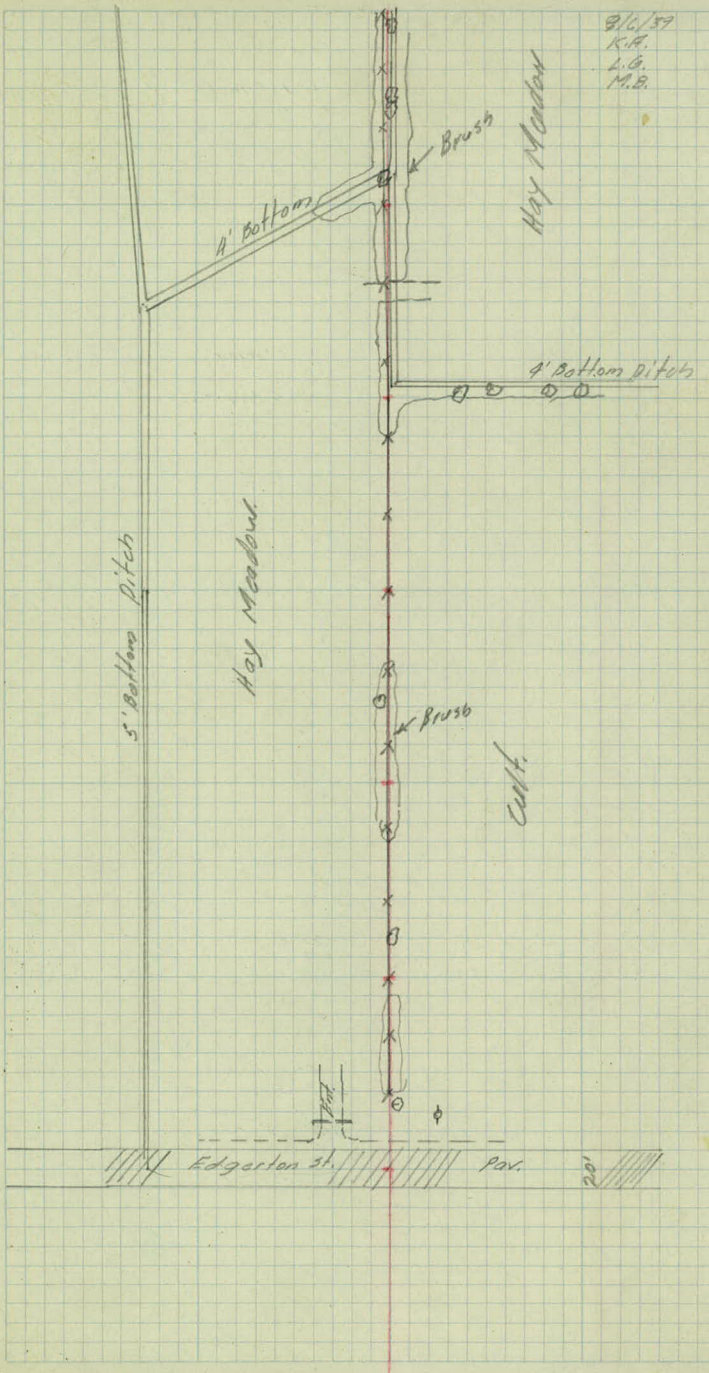
190-End Brush

Beg. Brush
138-Beg. FC-0.0
133-18" Oak-3'
128-P.P.-26'

124-15" 19-40'-20'

0100 Pitch-125'

8/10/59
K.R.
L.G.
M.B.



Beg. Lt. 20'

+64-8" Triple Willow - 3'
+58-12" Willow - 20'

12 Fc - 2'

Ditch - 3'

+74-8" Willow - 3'

+25-30" Poplar - 3'

11

Ditch - 3'

+43 Fc Cor - 3'

+64-12" Willow - 3'

10

Ditch - 3'

9

+07 Fc Cor - 2' ✓

Ditch - 3'

+75-Δ in Ditch - 230'

+97-30" Poplar - 3'

+10 Fc Cor - 2'

+59-24" Pop - 3'
~~+64-12" Willow - 3'~~ Emb. 2nd 3.5.0

8 Fc - 2' Δ in Ditch - 158'

+09-12" Elm - 20'
+05-6" Poplar - 6'
+02-07-12" Ditch 2' Bottom?
Ditch - 6'

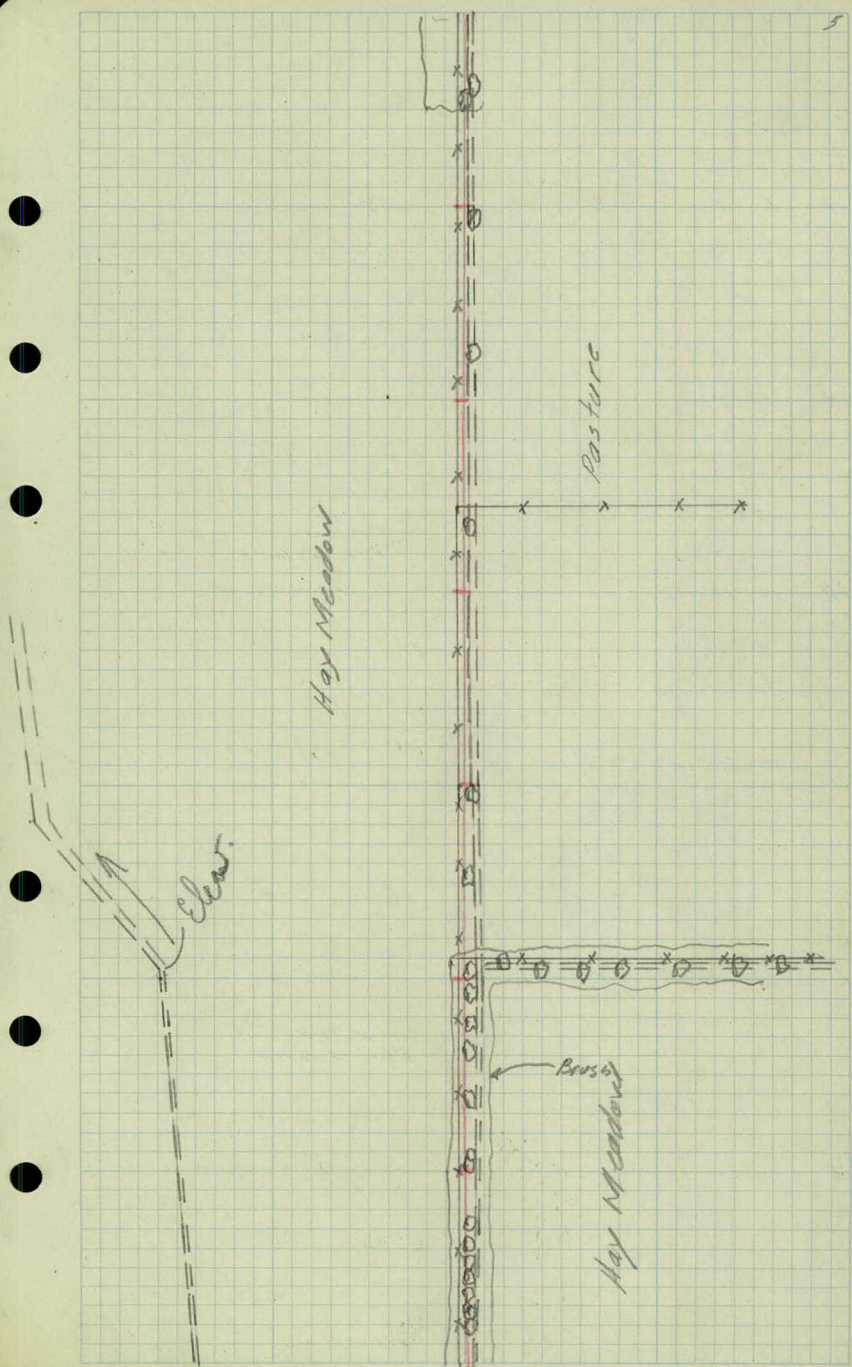
7

+92-18" Poplar - 4'
+76-18" Poplar - 4'
+65-8" Poplar - 3'
+62-15" Poplar - 4'
+39-10" Willow - 4'
+08-15" Poplar - 3'
+02-12" Poplar - 3'

Ditch - 4'
+77-6" Poplar - 2'
+74-30" Poplar - 4'
+62-18" Poplar - 2'
+49-8" Poplar - 2'
+46-15" Poplar - 2'
+36-12" Poplar - 2'
+34-6" Willow - 3'
+25-8" Willow - 5'
+20-6" Poplar - 3'
Ditch - 3'

6

Fc - 3'



19 Fc - 3'

Ditch - 1'

+60-End Brush - 20'

+52-20" Poplar - 1'
+45-20" Poplar - 6'
+37-8" Poplar - 2'

18 Fc - 3'

Ditch - 3'

+42-6" Elm - 1'

+55-10" Willow - 2'

17 Fc - 1'

+28-15" Tw Elm - 4'

Ditch - 3'

+79-15" Poplar - 4'

+53-4" Poplar - 13'

16 +18-Fc Cor - 2' Trees

+18-15" Triple Elm - 25'

Ditch - 3'

15 Brush - 23' Fc - 2'

Ditch - 4'

+50-30" Poplar - 5'
+35-15" Poplar - 3'

14 Fc - 1' Brush - 23'

Ditch - 2'

13 Fc - 02'

+12-15" Willow - 2'
Ditch - 0.5'

Hay Meadow

Brush

Cult



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+100-Ditch - 0.0

+132-Pitch - 6'

26

Pitch - 00

+129-End G.B. - 2'

+104-Beg. G.B. - 3'

+110-Edge Turn around
+104-End Fc + Woods - 8'

25

Pitch - 90

Fc + Woods - 7'

24

Pitch - 90

Fc + Woods - 8'

23 Woods - 28'

+121-Dio Fc - 3'

+100-Dio Fc - 11'

22 Fc - 5' Woods - 27'

Pitch - 2'

21 Woods - 25'

+192-Beg. Woods -

+150-Beg. Woods - 20'

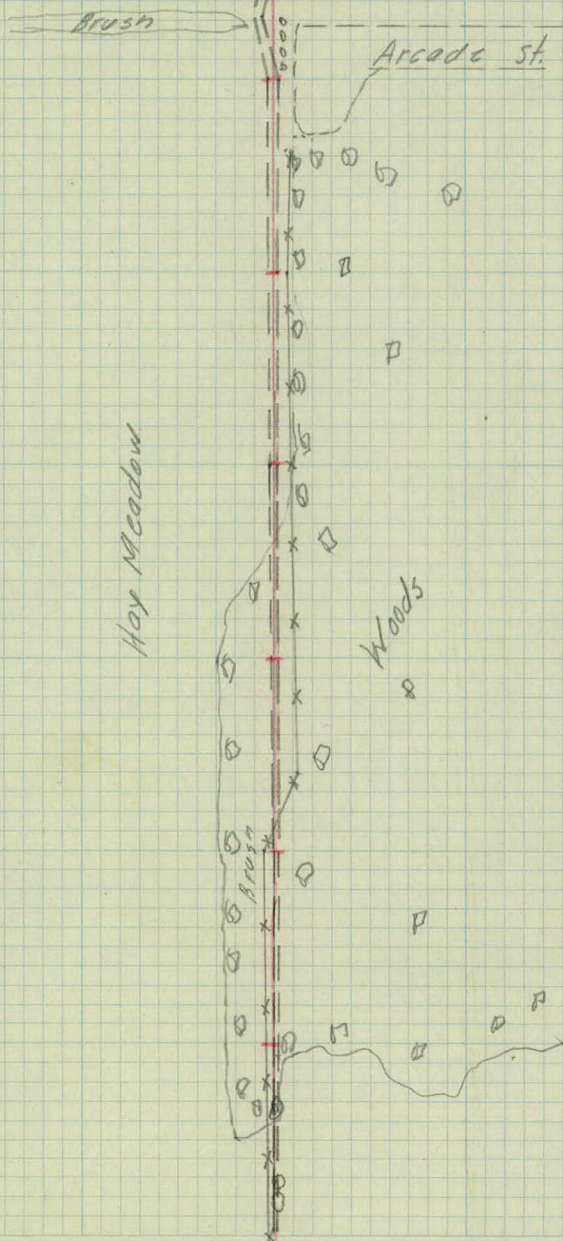
+107-29" Poplar - 1'

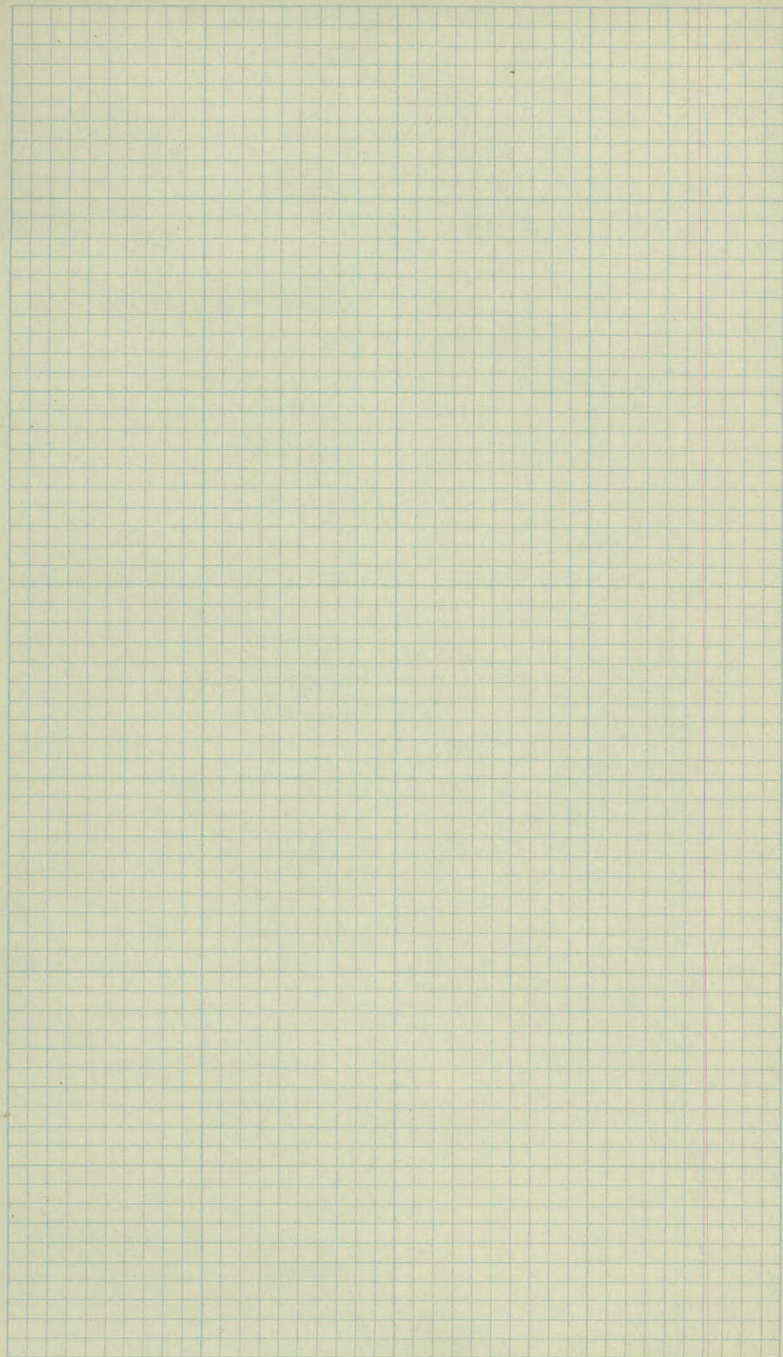
20 Fc - 4

+129-8" Poplar - 1'

+119-18" Poplar - 1'

Pitch - 2'





xsections

Sta	+	-	Elev
B.M.	2.69	711.64	908.95

0	+00		08.95
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	+10		08.85
--	-----	--	-------

	+14		08.1
--	-----	--	------

	+24	to 4' Bottom Ditch	04.3
--	-----	--------------------	------

	+33		07.5
--	-----	--	------

1			07.3
---	--	--	------

	+50		07.4
--	-----	--	------

2			07.6
---	--	--	------

	+50		06.9
--	-----	--	------

I.P.	4.85	712.44	707.59
------	------	--------	--------

3			07.4
---	--	--	------

	+50		07.6
--	-----	--	------

Lt

E

Rt

Top stone Mant. & Edgerton *Calc. D°

269

292
50

219

279
50

36
50

35

34
50

101.74

Calc Under Edgerton	9.9 125	73 50	74 41	40 37	43 24	74 20	73	1.3 30	7.2 50
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<u>50</u> 50	<u>45</u> 22	<u>41</u>	<u>42</u> 25	<u>4.2</u> 50
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<u>50</u> 50	<u>49</u> 28	<u>46</u> 3	<u>43</u>	<u>4.0</u> 4	<u>46</u> 6	<u>46</u> 32	<u>46</u> 50
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<u>49</u> 50	<u>46</u> 28	<u>46</u> 5	<u>4.2</u> 4	<u>37</u> 6	<u>4.2</u> 6	<u>46</u> 19	<u>4.6</u> 50
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<u>49</u> 50	<u>48</u> 29	<u>48</u> 4	<u>40</u> 4	<u>38</u> 7	<u>45</u> 7	<u>45</u> 25	<u>41</u> 50
-----------------	-----------------	----------------	----------------	----------------	----------------	-----------------	-----------------

<u>49</u> 50	<u>48</u> 30	<u>48</u> 3	<u>47</u> 5	<u>47</u> 5	<u>52</u> 9	<u>52</u> 31	<u>50</u> 50
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<u>56</u> 50	<u>54</u> 30	<u>52</u> 3	<u>50</u> 5	<u>50</u> 5	<u>54</u> 6	<u>5.5</u> 50
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<u>54</u> 50	<u>51</u> 30	<u>51</u> 3	<u>48</u> 5	<u>47</u> 5	<u>51</u> 7	<u>53</u> 28	<u>57</u> 50
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Sta	+	π	-	Elev
		912.44		
4				07.4
+07	L. & Bottom Ditch			07.5
+13				07.7
T.P.	3.47	911.99	3.92	908.52
+50				07.3
5	Lt. side Parallel to Ditch			07.6
HL	L. Ditch Ht.			04.0
+18				04.1
6				05.1
7.				07.0
T.P.	5.53	912.97	4.55	907.44
8				07.2
+06	L. Off take ditch rt.			

Lt.

K

Rt.

$$\frac{60}{50} \frac{51}{24}$$

$$\frac{52}{2}$$

$$\frac{50}{2}$$

$$\frac{51}{27}$$

$$\frac{51}{30}$$

$$\frac{60}{50}$$

$$\frac{57}{25}$$

$$\frac{52}{10}$$

$$\frac{49}{1}$$

$$\frac{49}{4}$$

$$\frac{7.2}{30}$$

$$\frac{6.5}{100}$$

$$\frac{6.6}{150}$$

$$\frac{6.1}{50}$$

$$\frac{62}{50}$$

$$\frac{58}{26}$$

$$\frac{51}{10}$$

$$\frac{47}{1}$$

$$\frac{47}{3}$$

$$\frac{67}{6}$$

$$\frac{6.7}{8}$$

$$\frac{51}{21}$$

$$\frac{52}{50}$$

$$\frac{49}{50}$$

$$\frac{58}{50}$$

$$\frac{55}{30}$$

$$\frac{53}{10}$$

$$\frac{47}{3}$$

$$\frac{62}{5}$$

$$\frac{62}{9}$$

$$\frac{48}{50}$$

$$\frac{49}{50}$$

$$\frac{57}{50}$$

$$\frac{53}{35}$$

$$\frac{49}{16}$$

$$\frac{44}{4}$$

$$\frac{68}{6}$$

$$\frac{68}{9}$$

$$\frac{52}{21}$$

$$\frac{48}{50}$$

$$\frac{48}{50}$$

Int of Ditches

$$\frac{80}{100}$$

$$\frac{80}{50}$$

$$\frac{80}{50}$$

$$\frac{54}{50}$$

$$\frac{54}{31}$$

$$\frac{49}{6}$$

$$\frac{19}{3}$$

$$\frac{46}{10}$$

$$\frac{48}{20}$$

$$\frac{48}{50}$$

$$\frac{48}{50}$$

$$\frac{50}{22}$$

$$\frac{37}{10}$$

$$\frac{47}{9}$$

$$\frac{69}{2}$$

$$\frac{19}{4}$$

$$\frac{7.9}{7}$$

$$\frac{54}{11}$$

$$\frac{42}{20}$$

$$\frac{45}{50}$$

$$\frac{46}{50}$$

$$\frac{54}{50}$$

$$\frac{52}{22}$$

$$\frac{44}{19}$$

$$\frac{37}{5}$$

$$\frac{50}{4}$$

$$\frac{7.5}{6}$$

$$\frac{7.5}{10}$$

$$\frac{51}{18}$$

$$\frac{44}{50}$$

$$\frac{47}{50}$$

$$\frac{53}{50}$$

$$\frac{53}{17}$$

$$\frac{43}{10}$$

$$\frac{43}{5}$$

$$\frac{58}{5}$$

$$\frac{8.2}{8}$$

$$\frac{8.2}{18}$$

$$\frac{39}{34}$$

$$\frac{45}{50}$$

$$\frac{47}{50}$$

$$\frac{04.77}{6} \frac{04.77}{50} \frac{05.17}{100}$$

Sta	+	π	-	Elev
		912.97		
8	+50			07.5
9				06.9
	+50			06.7
10				06.6
	+50			06.4
11				06.7
T.P.	400	912.56	4.91	908.56
	+50			07.1
12				07.0
	+50			07.0
13				07.0
	+50			07.9

Lt.

A

Pt.

$$\frac{50}{50} \frac{50}{20} \frac{46}{15} \frac{43}{3} \frac{55}{4} \frac{69}{6} \frac{69}{9} \frac{50}{12} \frac{41}{17} \frac{50}{30} \frac{51}{30}$$

$$\frac{50}{50} \frac{53}{26} \frac{44}{17} \frac{47}{4} \quad \frac{61}{3} \frac{70}{6} \frac{70}{12} \frac{47}{28} \frac{52}{50} \frac{52}{50}$$

$$\frac{51}{50} \frac{57}{25} \frac{48}{18} \frac{52}{10} \frac{52}{3} \frac{63}{3} \frac{74}{5} \frac{74}{10} \frac{57}{24} \frac{54}{50} \frac{58}{50}$$

$$\frac{52}{50} \frac{56}{25} \frac{44}{14} \frac{51}{10} \frac{54}{3} \frac{64}{2} \frac{73}{5} \frac{73}{9} \frac{52}{23} \frac{53}{50} \frac{55}{50}$$

$$\frac{52}{50} \frac{58}{25} \frac{48}{20} \frac{54}{10} \frac{53}{4} \frac{66}{2} \frac{68}{4} \frac{68}{9} \frac{58}{21} \frac{51}{50} \frac{52}{50}$$

$$\frac{51}{50} \frac{55}{24} \frac{49}{20} \quad \frac{51}{4} \quad \frac{63}{9} \frac{65}{7} \frac{55}{26} \frac{51}{50} \frac{53}{50}$$

$$\frac{48}{50} \frac{51}{25} \frac{40}{17} \frac{45}{4} \quad \frac{55}{2} \frac{57}{4} \frac{57}{21} \frac{46}{50} \frac{48}{50}$$

$$\frac{48}{50} \frac{49}{26} \frac{38}{19} \frac{45}{4} \frac{56}{3} \frac{56}{10} \frac{47}{26} \frac{47}{50} \frac{47}{50}$$

$$\frac{52}{50} \frac{48}{21} \frac{42}{15} \quad \frac{46}{3} \quad \frac{56}{3} \frac{56}{8} \frac{50}{26} \frac{49}{50} \frac{49}{50}$$

$$\frac{46}{50} \frac{48}{23} \frac{44}{16} \frac{51}{2} \frac{56}{4} \frac{56}{7} \frac{49}{50} \frac{46}{50}$$

$$\frac{44}{50} \frac{44}{22} \frac{36}{19} \frac{44}{10} \frac{42}{2} \frac{47}{2} \frac{54}{4} \frac{54}{6} \frac{47}{24} \frac{47}{50} \frac{44}{50}$$

Sta.	+	π	-	Elev
		912.56		
T.P.	5.33	914.46	3.43	909.13
14				07.4
	+50			07.8
15				08.1
	+50			08.3
16				08.5
	+50			09.1
17				09.4
	+50			09.7
18				10.1
T.P.	6.85	917.36	3.95	910.51
	+50			10.4
19				10.4

LH

L

RH

$$\frac{6.0}{50} \frac{5.9}{22} \frac{5.1}{19} \quad \frac{5.0}{10} \frac{6.2}{3} \quad \frac{7.1}{2} \frac{7.7}{5} \quad \frac{5.8}{8} \frac{5.8}{36} \frac{5.9}{50}$$

$$\frac{5.8}{50} \frac{5.7}{22} \frac{5.1}{12}$$

$$\frac{5.9}{2} \frac{6.7}{1} \frac{6.9}{5} \frac{6.9}{5} \quad \frac{5.9}{11} \frac{5.8}{28} \frac{6.0}{50}$$

$$\frac{5.7}{50} \frac{5.6}{23} \frac{5.0}{14} \frac{5.5}{4} \quad \frac{6.4}{3} \frac{6.9}{5} \frac{6.9}{5} \quad \frac{6.0}{7} \frac{5.7}{27} \frac{5.8}{50}$$

$$\frac{5.5}{50} \frac{5.2}{20} \frac{5.3}{9}$$

$$\frac{5.5}{2}$$

$$\frac{6.2}{2} \frac{6.6}{5} \frac{6.6}{5}$$

$$\frac{5.1}{9} \frac{5.6}{50}$$

$$\frac{5.2}{50} \frac{5.8}{24} \frac{4.1}{16} \quad \frac{5.0}{11} \quad \frac{5.1}{3} \quad \frac{6.0}{1} \frac{6.1}{4} \frac{6.1}{7} \quad \frac{5.2}{29} \frac{5.3}{50} \frac{5.1}{50}$$

$$\frac{5.0}{50} \frac{4.7}{20} \frac{4.1}{17} \quad \frac{4.8}{6} \quad \frac{4.9}{2} \quad \frac{5.4}{4} \frac{5.6}{22} \frac{5.6}{28} \quad \frac{4.9}{28} \frac{4.8}{50}$$

$$\frac{4.7}{50} \frac{4.5}{20} \frac{3.7}{15} \quad \frac{4.6}{2} \quad \frac{5.1}{2} \frac{5.4}{4} \frac{5.4}{4} \quad \frac{4.7}{9} \frac{4.3}{25} \frac{4.5}{50}$$

$$\frac{4.6}{50} \frac{4.5}{18} \quad \frac{4.3}{2}$$

$$\frac{4.8}{4} \frac{4.9}{7} \frac{4.9}{19} \quad \frac{3.9}{19} \frac{4.3}{50}$$

$$\frac{4.4}{18} \frac{4.2}{18} \quad \frac{4.0}{9} \quad \frac{4.4}{2} \frac{4.8}{4} \frac{4.8}{4} \quad \frac{4.2}{7} \frac{3.8}{21} \frac{3.6}{50}$$

sta-18

$$\frac{6.9}{50} \frac{6.4}{20} \quad \frac{6.5}{6}$$

$$\frac{7.0}{3} \frac{7.2}{6} \frac{6.6}{19} \quad \frac{6.4}{19} \frac{6.7}{50}$$

$$\frac{6.5}{50} \frac{6.5}{22} \frac{5.9}{18} \frac{6.4}{14}$$

$$\frac{6.4}{4} \frac{7.0}{1} \quad \frac{7.0}{3} \frac{7.0}{9} \quad \frac{6.3}{9} \quad \frac{5.9}{50}$$

Sta	+	π	-	Elev.
		917.36		
19	+50			10.6
20				11.8
	+50			11.7
21				12.7
	+50			12.6
22				13.0
	+50			12.9
23				13.2
I.P.	8.55	923.69	2.22	915.14
	+50			14.1
24				15.0
	+75			15.8

Lt

K

Rt

$$\frac{6.0}{50} \quad \frac{6.0}{22} \quad \frac{5.5}{18} \quad \frac{6.2}{1} \quad \frac{6.8}{1} \quad \frac{6.9}{3} \quad \frac{6.9}{4} \quad \frac{6.0}{18} \quad \frac{5.5}{50} \quad \frac{5.7}{50}$$

$$\frac{5.6}{50} \quad \frac{5.5}{26} \quad \frac{5.2}{18} \quad \frac{5.0}{10} \quad \frac{5.6}{1} \quad \frac{5.8}{1} \quad \frac{6.4}{2} \quad \frac{6.4}{5} \quad \frac{5.5}{35} \quad \frac{5.2}{50} \quad \frac{5.2}{50}$$

$$\frac{5.0}{50} \quad \frac{5.1}{22} \quad \frac{4.6}{19} \quad \frac{5.0}{14} \quad \frac{5.1}{2} \quad \frac{5.7}{1} \quad \frac{6.2}{3} \quad \frac{6.2}{6} \quad \frac{5.1}{20} \quad \frac{4.9}{20} \quad \frac{4.9}{50}$$

$$\frac{4.8}{50} \quad \frac{4.7}{26}$$

$$\frac{4.7}{2} \quad \frac{5.3}{3} \quad \frac{5.3}{7} \quad \frac{4.6}{18} \quad \frac{4.5}{18} \quad \frac{4.4}{50}$$

$$\frac{4.5}{50} \quad \frac{4.4}{28} \quad \frac{4.9}{25} \quad \frac{4.1}{20} \quad \frac{4.2}{14} \quad \frac{4.5}{2} \quad \frac{5.0}{4} \quad \frac{5.1}{4} \quad \frac{4.2}{7} \quad \frac{4.2}{26} \quad \frac{4.1}{50}$$

$$\frac{4.1}{50} \quad \frac{3.9}{22} \quad \frac{4.2}{20} \quad \frac{3.6}{18}$$

$$\frac{3.7}{2}$$

$$\frac{4.4}{2} \quad \frac{4.6}{5} \quad \frac{3.6}{14} \quad \frac{3.4}{14} \quad \frac{3.4}{50}$$

$$\frac{3.4}{50} \quad \frac{3.3}{25} \quad \frac{3.0}{22} \quad \frac{2.9}{2}$$

$$\frac{4.5}{7} \quad \frac{4.5}{5} \quad \frac{2.3}{9} \quad \frac{3.1}{9} \quad \frac{2.7}{50}$$

$$\frac{2.8}{50}$$

$$\frac{3.0}{2}$$

$$\frac{4.2}{3} \quad \frac{4.2}{5} \quad \frac{1.6}{10} \quad \frac{2.5}{10} \quad \frac{2.6}{50}$$

$$\frac{8.6}{50}$$

$$\frac{8.3}{4}$$

$$\frac{9.6}{1} \quad \frac{9.7}{4} \quad \frac{1.5}{11} \quad \frac{8.2}{11} \quad \frac{7.8}{50}$$

$$\frac{7.6}{50} \quad \frac{7.0}{25} \quad \frac{7.1}{6}$$

$$\frac{8.7}{2} \quad \frac{8.7}{1} \quad \frac{8.7}{3} \quad \frac{7.0}{11} \quad \frac{7.0}{11} \quad \frac{6.3}{50}$$

$$\frac{5.1}{50} \quad \frac{4.7}{24}$$

$$\frac{4.8}{6}$$

$$\frac{7.9}{1} \quad \frac{7.9}{1} \quad \frac{3.9}{5} \quad \frac{4.7}{13} \quad \frac{5.0}{32} \quad \frac{4.9}{50}$$

Sta	+	π	-	Elev
		923.69		

25				15.6
----	--	--	--	------

+58				16.1
-----	--	--	--	------

26				16.6
----	--	--	--	------

+23				18.8
-----	--	--	--	------

+28				17.0
-----	--	--	--	------

+32.18				18.1
--------	--	--	--	------

B.M.	5.30	918.39		918.42
------	------	--------	--	--------

Lt.

C.

Rt.

$$\frac{51}{50} \quad \frac{48}{22} \quad \frac{46}{6}$$

$$\frac{81}{1} \quad \frac{81}{5} \quad \frac{35}{5} \quad \frac{49}{13} \quad \frac{51}{38} \quad \frac{52}{50}$$

$$\frac{51}{50} \quad \frac{51}{1} \quad \frac{51}{6}$$

$$\frac{76}{1} \quad \frac{76}{4} \quad \frac{50}{9} \quad \frac{52}{16} \quad \frac{59}{50} \quad \frac{57}{50}$$

$$\frac{59}{50} \quad \frac{60}{31} \quad \frac{68}{12} \quad \frac{53}{4} \quad \frac{71}{1} \quad \frac{71}{1} \quad \frac{50}{5} \quad \frac{46}{17} \quad \frac{45}{50}$$

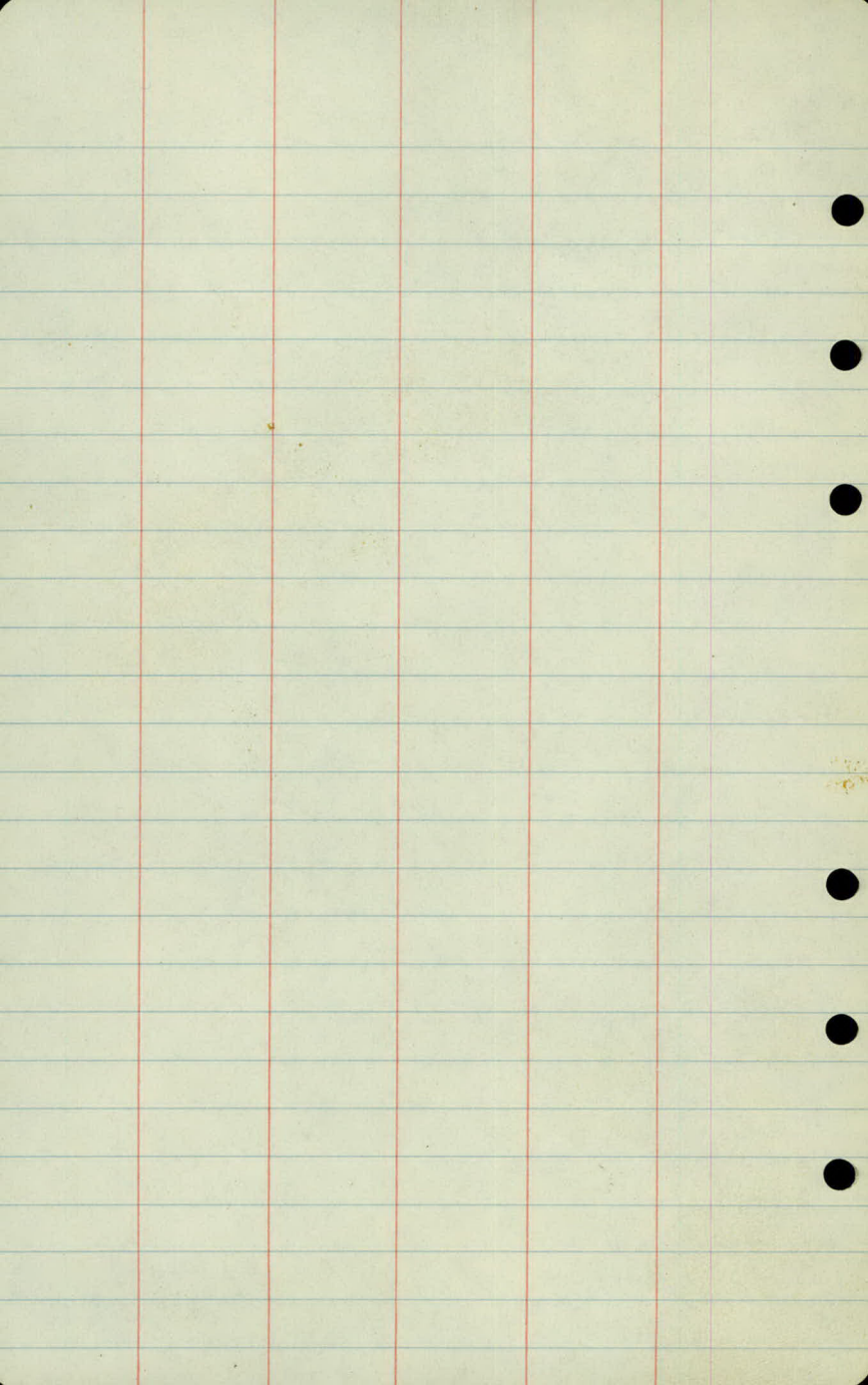
$$\frac{51}{50} \quad \frac{56}{20} \quad \frac{52}{10} \quad \frac{78}{7} \quad \frac{70}{5} \quad \frac{51}{3} \quad \frac{49}{27} \quad \frac{49}{27} \quad \frac{51}{50}$$

$$\frac{50}{50} \quad \frac{54}{25} \quad \frac{54}{9} \quad \frac{73}{7} \quad \frac{73}{5} \quad \frac{68}{4} \quad \frac{67}{1} \quad \frac{62}{3} \quad \frac{62}{27} \quad \frac{61}{50}$$

$$\text{Ditch Lt.} \quad \frac{62}{50} \quad \frac{63}{29} \quad \frac{73}{5} \quad \frac{56}{1} \quad \frac{52}{24} \quad \frac{57}{50}$$

Top Mont Arcade St + Co. Rd "D"

Ditch along & drains East



Ditch Levels

1584 ft. of Sta. 8+00 East

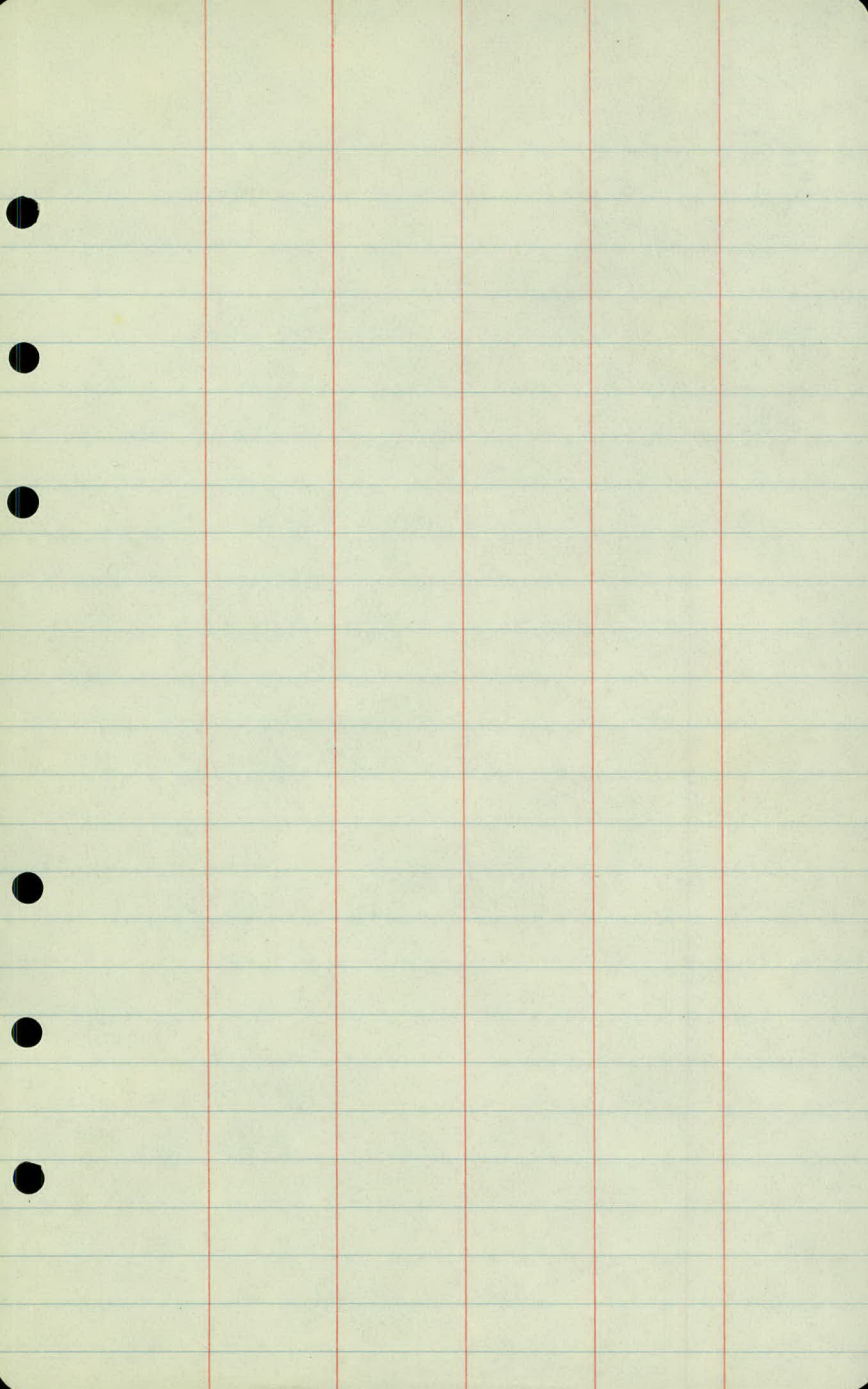
Sta.	+	Σ	-	Elev.
B.M.	2.63	911.58		(908.95)
I.P.	4.05	912.63	3.00	908.58
$8+00 = 158' 24.3''$				
0+00			8.8	03.83

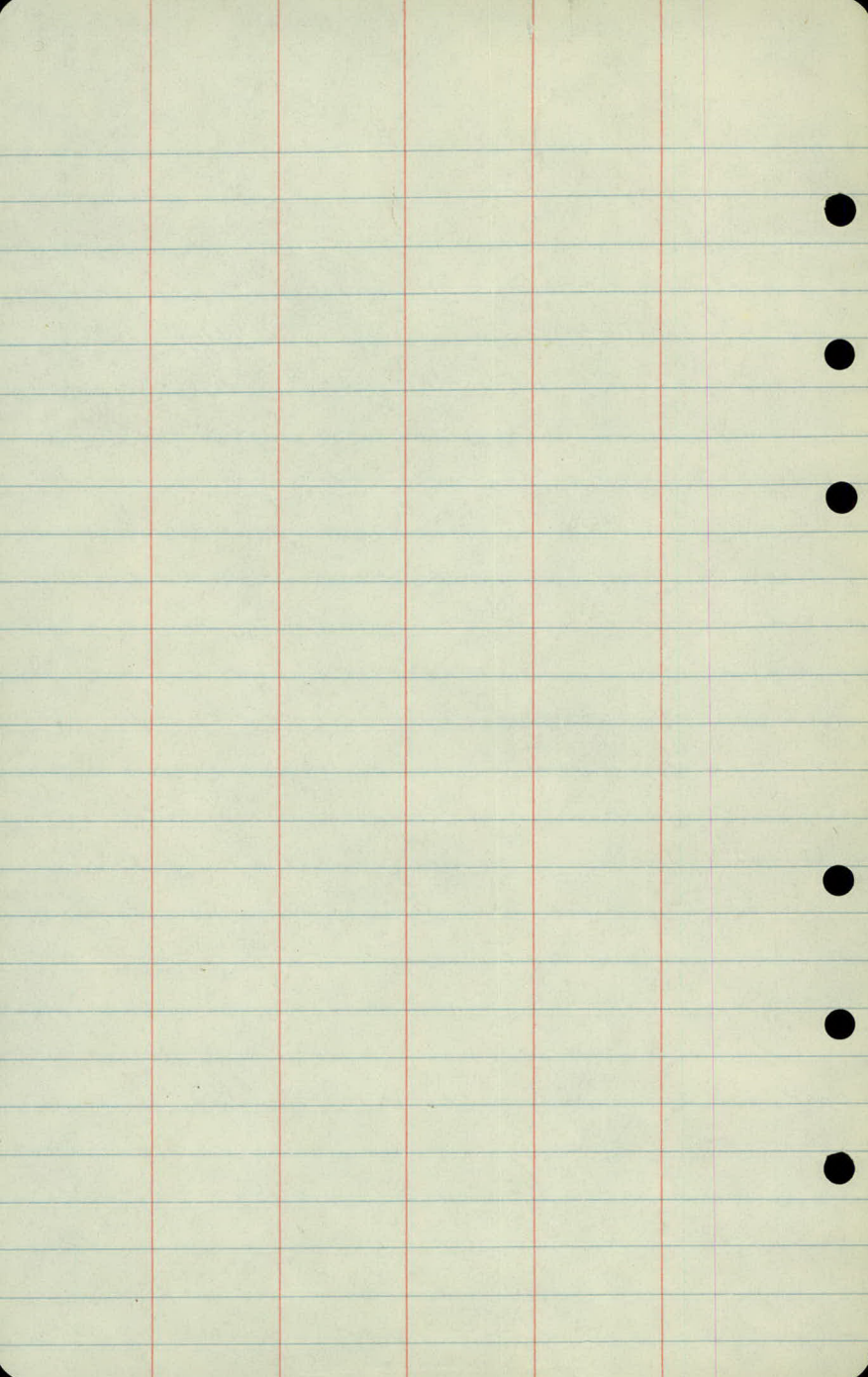
1			8.7	03.93
---	--	--	-----	-------

2			8.6	04.03
---	--	--	-----	-------

3			8.3	04.33
---	--	--	-----	-------

4			8.3	04.33
---	--	--	-----	-------





Slope Stakes

Co. Rd. "D"

Edgerton St. to Arcade.

Sta	+	π	-	Grade.	Gr. Rod.	pitch Gr. Lt.
B.M.	3.07	912.02			(908.95)	
0	+00					
	+29					02.0
	+39			08.6	10.0	02.0
1				08.5	9.9	02.1
	+50			08.3	9.8	02.2
2				08.2	9.7	02.3
	+50			08.1	9.6	02.4
3				08.0	9.5	02.5
T.P.	5.71	913.18	4.55	907.47		
	+50			07.9	10.6	02.6
4				07.7	10.5	02.7
	+13			07.7	10.5	02.7

11/9/37
K. F.
L.G.
M.B.
M.A.G.

Ditch
Gr.
St.

Gr. Rod.

Lt.

Gr.

St.

Gr. Rod.

Top Mont. Edgerton & Card "D"

908.7

086

3.4

$$41.0' / \frac{52}{R48}$$

$$\frac{45}{-11}$$

$$\frac{43}{R01/24.4'}$$

3.5

$$40.6' / \frac{55}{R44}$$

$$\frac{47}{-12}$$

$$\frac{51}{R04/24.0'}$$

3.7

$$40.4' / \frac{52}{R46}$$

$$\frac{44}{-07}$$

$$\frac{43}{R08/24.6'}$$

3.8

$$39.6' / \frac{53}{R44}$$

$$\frac{47}{-09}$$

$$\frac{49}{R09/24.8'}$$

3.9

$$39.0' / \frac{53}{R43}$$

$$\frac{46}{-07}$$

$$\frac{49}{R10/25.0'}$$

4.0

$$38.8' / \frac{51}{R44}$$

$$\frac{47}{-07}$$

$$\frac{52}{R08/24.6'}$$

S.S. Stake L.L. 5400

5.3

$$38.6' / \frac{61}{R45}$$

$$\frac{55}{-02}$$

$$\frac{62}{R11/25.2'}$$

5.5

$$37.0' / \frac{65}{R40}$$

$$\frac{57}{-02}$$

$$\frac{56}{R19/26.8'}$$

087

7.5

5.5

056

Sta.	+	π	-	Grade.	Gr. Red	Ditch Gr. Lt.
		713.18				
4	+50			07.7	10.4	02.8
5				07.6	10.3	02.9
	+18			07.6	10.2	03.0
	+60			07.7	10.1	03.1
6				07.7	10.1	03.1
	+50			07.7	10.0	03.2
7				07.8	9.9	03.3
T.P.	527	912.63	5.82	907.36		
	+50			07.7	9.2	03.4
	culv. 20' Lt.		culv. 20' Lt.	08.0	9.1	03.5
	+50			08.1	8.6	04.0
9				08.1	8.1	04.5

Gr. Rod.	Lt	R	Rt	Ditch Gr. Rt.	Gr. Rod.
5.5	$35.8 / \frac{6.9}{R35}$	$\frac{5.9}{-0.4}$	$\frac{5.8}{R219/27.2}$	05.5	7.7
5.6	$37.0 / \frac{6.0}{R43}$	$\frac{5.7}{-0.1}$	$\frac{6.1}{R217/26.8}$	05.4	7.8
5.6	$35.4 / \frac{6.6}{R36}$			05.3	
5.5	$36.6 / \frac{5.9}{R42}$	$\frac{8.7}{-3.2}$	$\frac{5.8}{R22/28.4}$	05.2	8.0
5.5	$36.6 / \frac{5.9}{R42}$	$\frac{8.5}{-3.0}$	$\frac{5.7}{R24/28.0}$	05.1	8.1
5.5	$36.0 / \frac{6.0}{R40}$	$\frac{7.6}{-2.1}$	$\frac{5.6}{R26/29.6}$	05.0	8.2
5.4	$35.0 / \frac{6.4}{R35}$	$\frac{7.1}{-1.7}$	$\frac{5.6}{R28/30.6}$	04.8	8.4
4.7	$35.2 / \frac{5.6}{R36}$	$\frac{6.0}{-1.3}$	$\frac{5.5}{R24/30.2}$	04.7	7.9
4.6	$36.0 / \frac{5.1}{R40}$	$\frac{5.4}{-1.2}$	$\frac{4.6}{R35/32.0}$	04.5	8.1
4.5	$35.2 / \frac{4.6}{R40}$	$\frac{5.1}{-0.9}$	$\frac{5.7}{R26/25.8}$	05.3	7.3
4.5	$33.2 / \frac{4.6}{R35}$	$\frac{5.8}{-1.3}$	$\frac{4.8}{R17/26.4}$		

sta	+	π	-	Grade	Ditch	
					Gr. Rod.	Gr. Lt.
		912.63				
9	+50			08.2	7.6	05.0
10				08.3	7.1	05.5
	+50			08.4	6.6	06.0
11				08.5		
T.P.	5.31	913.29	4.65	707.98		
	+50			08.5		
12				08.6		
	+50			08.7		
13				08.8		
	+50			08.9		
14				09.0		
	+50			09.1		

Gr. Rod

Lt

R

Rt

4.4

$$30.8' / \frac{49}{R2.7}$$

$$\frac{6.1}{-1.7}$$

$$\frac{53}{R1.1} / 25.2'$$

4.3

$$28.8' / \frac{50}{R2.1}$$

$$\frac{6.1}{-1.8}$$

$$\frac{50}{R1.3} / 25.6'$$

4.2

$$26.6' / \frac{52}{R1.4}$$

$$\frac{6.3}{-2.1}$$

$$\frac{48}{R1.4} / 25.8'$$

4.1

$$24.8' / \frac{52}{R2.0.9}$$

$$\frac{5.9}{-1.8}$$

$$\frac{4.9}{R1.2} / 25.4'$$

4.8

$$25.0' / \frac{58}{R1.0}$$

$$\frac{6.3}{-1.5}$$

$$\frac{56}{R1.2} / 25.4'$$

4.7

$$25.2' / \frac{56}{R1.1}$$

$$\frac{6.3}{-1.7}$$

$$\frac{54}{R1.2} / 25.4'$$

4.6

$$25.0' / \frac{56}{R1.0}$$

$$\frac{6.4}{-1.8}$$

$$\frac{55}{R1.1} / 25.2'$$

4.5

$$24.8' / \frac{56}{R2.9}$$

$$\frac{6.3}{-1.8}$$

$$\frac{53}{R1.2} / 25.4'$$

4.4

$$25.4' / \frac{52}{R1.2}$$

$$\frac{5.8}{-1.4}$$

$$\frac{5.1}{R1.3} / 25.6'$$

4.3

$$25.8' / \frac{4.9}{R1.4}$$

$$\frac{5.6}{-1.3}$$

$$\frac{4.9}{R1.4} / 25.6'$$

4.2

$$26.2' / \frac{4.6}{R1.6}$$

$$\frac{5.3}{-1.1}$$

$$\frac{4.5}{R1.7} / 26.4'$$

sta	+	π	-	Grade	
		913.29			
15				09.3	
	1.50			09.5	
16				09.8	
B.M.	4.27	915.50	2.06	911.23	911.25
	1.50			10.0	
17				10.3	
	1.50			10.5	
18				10.8	
	1.50			11.1	
19				11.4	
	1.50			11.8	
20				12.3	

Cor. Rod.

L.F.

R

R.F.

4.0

$$26.2' \frac{44}{R16}$$

$$\frac{5.2}{-1.2}$$

$$\frac{46}{R14/25.8'}$$

3.8

$$25.8' \frac{44}{R14}$$

$$\frac{5.1}{-1.3}$$

$$\frac{42}{R16/26.2'}$$

3.5

$$26.9' \frac{40}{R15}$$

$$\frac{4.6}{-1.1}$$

$$\frac{4.0}{R15/26.0'}$$

Spk. in 16" Elm 38' R.F. 16 + 19

5.5

$$26.4' \frac{58}{R17}$$

$$\frac{4.6}{-1.1}$$

$$\frac{6.1}{R14/25.8'}$$

5.2

$$26.2' \frac{56}{R16}$$

$$\frac{6.1}{-0.9}$$

$$\frac{5.2}{R20/27.0'}$$

5.0

$$26.2' \frac{54}{R16}$$

$$\frac{-0.9}{-0.9}$$

$$\frac{5.5}{R15/26.0'}$$

4.7

$$25.6' \frac{52}{R13}$$

$$\frac{5.3}{-0.6}$$

$$\frac{5.0}{R17/26.4'}$$

4.4

$$26.0' \frac{49}{R13}$$

$$\frac{5.1}{-0.7}$$

$$\frac{4.5}{R19/26.8'}$$

4.1

$$25.8' \frac{47}{R14}$$

$$\frac{5.3}{-1.2}$$

$$\frac{4.3}{R18/26.6'}$$

3.7

$$26.2' \frac{41}{R16}$$

$$\frac{4.9}{-0.6}$$

$$\frac{3.9}{R19/26.6'}$$

3.2

$$26.0' \frac{37}{R15}$$

$$\frac{4.0}{-0.8}$$

$$\frac{3.4}{R18/26.6'}$$

Sta	+	π	-	Grade
		915.60		
20	+50			12.8
I.P.	5.99	918.81	2.68	912.82
21				13.4
	+50			13.9
22				14.4
	+50			14.9
23				15.4
	+50			16.0
T.P.	6.00	921.88	2.93	915.88
24				16.5
	+40			17.0
	+75			17.3
25				17.5

Gr. Rod.

L1

9.

21

2.7

$$26.0' / \frac{3.2}{R1.5}$$

$$\frac{3.8}{-1.1}$$

$$\frac{3.0}{R1.7/26.4'}$$

5.4

$$25.4' / \frac{6.2}{R1.2}$$

$$\frac{6.0}{-0.6}$$

$$\frac{5.9}{R1.5/26.0'}$$

4.7

$$24.6' / \frac{6.1}{R0.8}$$

$$\frac{6.4}{-1.5}$$

$$\frac{5.6}{R1.3/25.6'}$$

4.4

$$24.0' / \frac{5.5}{R0.9}$$

$$\frac{5.7}{-1.3}$$

$$\frac{4.9}{R1.5/26.0'}$$

3.9

$$25.2' / \frac{4.8}{R1.1}$$

$$\frac{5.6}{-1.7}$$

$$\frac{4.3}{R1.6/26.2'}$$

3.4

$$25.6' / \frac{4.1}{R1.3}$$

$$\frac{5.2}{-1.8}$$

$$\frac{3.7}{R1.7/26.4'}$$

2.8

$$25.8' / \frac{3.4}{R0.4}$$

$$\frac{4.7}{-1.9}$$

$$\frac{3.2}{R1.8/26.6'}$$

5.4

$$27.4' / \frac{5.2}{+0.2}$$

$$\frac{7.1}{-1.7}$$

$$\frac{4.9}{+0.5/28.0'}$$

4.9

$$28.6' / \frac{4.1}{+0.8}$$

$$\frac{6.6}{-1.9}$$

$$\frac{3.8}{+1.7/29.2'}$$

4.6

$$30.0' / \frac{3.1}{+1.5}$$

$$\frac{6.1}{-1.5}$$

$$\frac{3.3}{+1.3/29.6'}$$

4.4

$$29.4' / \frac{3.2}{+1.2}$$

$$\frac{6.2}{-1.8}$$

$$\frac{3.4}{+1.0/29.0'}$$

Sta + π - Grade

921.88

25 +50

18.0

26

18.6

+32.18

18.8

B.M.

5.37

923.79

3.51

918.37

(918.42)

B.M.

4.64

919.15

Ditch Change Lt.

24 +75

17.3

8.5

25

17.5

8.4

+50

18.0

8.3

26

18.6

8.1

+32.18

18.8

8.0

Gr. Rod.

Lt.

G.

Rt.

3.9

$$\frac{274'137}{102}$$

$$\frac{91}{R18/256}$$

3.3

$$\frac{254'41}{R12}$$

$$\frac{53}{-20}$$

$$\frac{29}{10.9/27.8}$$

3.1

$$\frac{262'35}{R16}$$

Top Mont. Arcade + Co. Rd. "D"

Spk. in 15" O 10'S.E. of Mont.

6.5

$$\frac{30.0'50}{41.6}$$

6.3

232

$$\frac{30.0'50}{R34}$$

5.8

240

$$\frac{294'56}{R27}$$

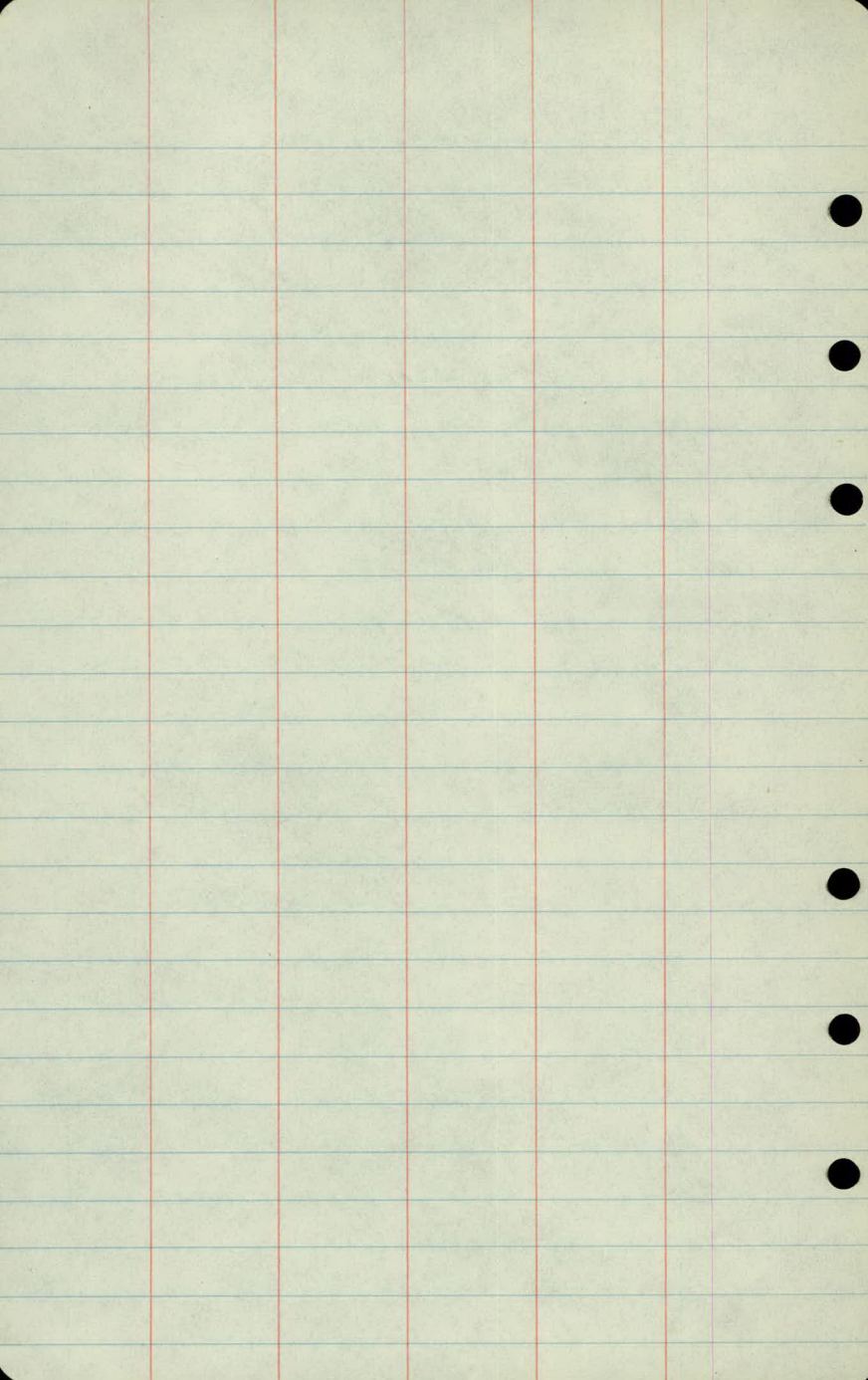
5.2

248

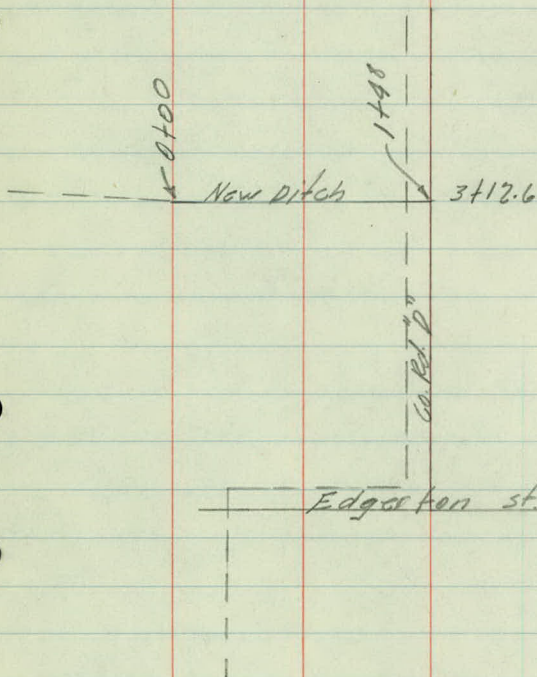
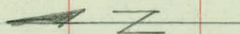
$$\frac{290'60}{R21}$$

5.0

$$\frac{304'53}{R27}$$



ditch at 3+12.6



Sta	+	π	-	Grade
B.M.	3.83	911.83		908.00

0 +00

+50

+85

1 +09

+48 = Sta. 3+12.6 Cor. Rd. 1D"

Lt

K

Rt

Top Blue Top sta. 3100

7.0

7.1

$$4.4 / \begin{array}{r} 5.4 \\ 1.9 \end{array}$$

$$\begin{array}{r} 5.4 \\ 1.7 \end{array} / 4.4$$

7.2

$$5.8 / \begin{array}{r} 4.8 \\ 12.9 \end{array}$$

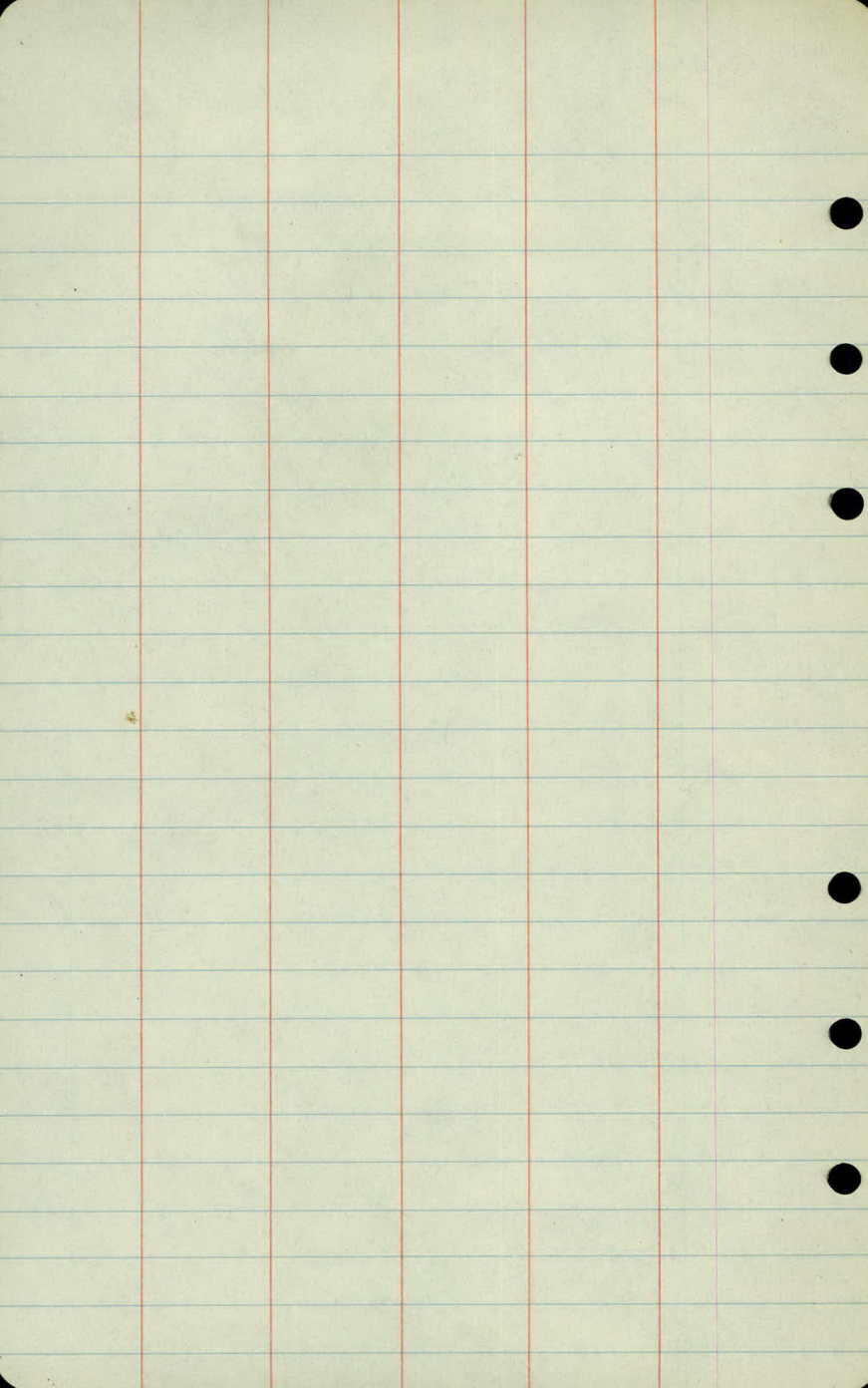
$$\begin{array}{r} 4.8 \\ \hline \end{array}$$

$$\begin{array}{r} 4.8 \\ 12.4 \end{array} / 5.8$$

7.3

$$6.0 / \begin{array}{r} 4.8 \\ 12.5 \end{array}$$

$$\begin{array}{r} 4.8 \\ 12.5 \end{array} / 6.0$$



Staking Notes
Channel Change
90° Lt 8+00

Sta	+	π	-	Grade
		712.63		

0	+00			03.5
---	-----	--	--	------

	+21			03.5
--	-----	--	--	------

	+50			03.6
--	-----	--	--	------

1				03.7
---	--	--	--	------

	+25			03.8
--	-----	--	--	------

Gr Rod.

Lt

R

Rt

H. 1. from slope stakes 60.00' D"

9.13

$$\frac{87.1}{+19.0}$$

9.1

$$10.0' / \frac{51}{+14.0}$$

$$\frac{49}{+12} / 10.4'$$

9.0

$$9.8' / \frac{51}{+13.9}$$

$$\frac{50}{+10.0} / 10.0'$$

8.9

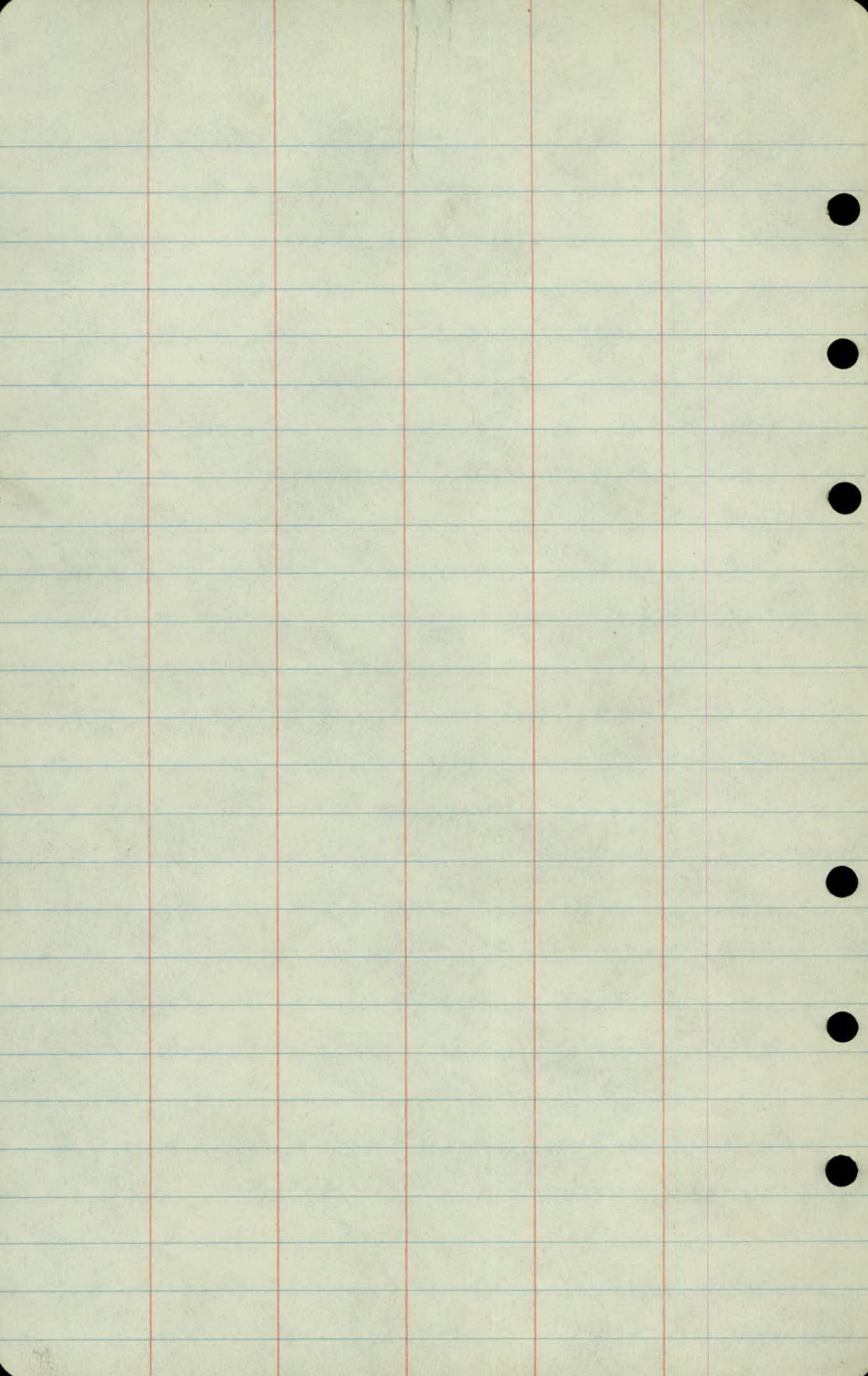
$$8.4' / \frac{51}{+13.2}$$

$$\frac{56}{+13} / 8.6'$$

8.8

$$8.0' / \frac{58}{+13.0}$$

$$\frac{63}{+25} / 7.0'$$



Co. Rd. 'D'

Slope stakes.

ditch change at

0100 to sta-

Sta	+	-	Grade	Ditch Grade
B.M.	4.01	912.96		(908.95)
0	+33		908.6	
	+50		08.6	
TP	335	911.96	4.35	908.61
1				08.5
	+50		08.3	
2			08.2	
	+50		08.1	
3			08.0	
	+50		07.9	
4			07.7	
	+07		07.7	05.2 6.76
	+50		07.7	5.3 6.7

Gr. Rod.

Q.

Rt.

Top Mast Edgerton & Co. Rd. "D"

4.36 ✓

4.46

$\frac{59}{16.05} / 240'$

3.46 ✓

3.66 ✓

3.76 ✓

$\frac{1.4}{1.4} / 4.8$
2.5

3.86 ✓

3.96 ✓

4.06 ✓

4.26

6.23 = FL. Cal'n.

4.27

4.26

2.4 pccp
23.8

$\frac{45}{12.2} / 282'$

Sta	+	π	-	Grade	Ditch Gr Bt.
		911.96			
5				07.6	6.6 5.4
+50				07.6	6.5 5.5
6				07.7	6.36 5.6
+50				07.7	05.7
T.P.	4.56	912.74	278	908.18	
7				07.8	05.8
+50				07.9	
7+95				08.0	
8 +12				08.0	
+50				08.1	
9				08.1	
+50				08.2	
10				08.3	

4

ct.

✓ 4.36 2.2 PCOP
23.4

$\frac{48}{21.8} / 27.0'$

✓ 4.36 2.1 PCOP
23.2

$\frac{45}{22.0} / 27.2'$

✓ 4.26 2.1 PCOP
23.2

$\frac{44}{22.0} / 27.2'$

4.26

$\frac{42}{20.1} / 27.2'$

✓ 4.94

$\frac{51}{21.8} / 26.4'$

✓ 4.84

$\frac{53}{20.5} / 26.0'$

4.7

$\frac{48}{21.9} / 26.8'$

4.7

$\frac{25.8}{21.4} / \frac{5.3}{5.2}$

$\frac{4.3}{20.9} / 27.8'$

4.6

$\frac{25.8}{21.4} / \frac{5.2}{5.1}$

$\frac{47}{21.9} / 26.8'$

4.6

$\frac{26.0}{21.5} / \frac{5.1}{5.4}$

$\frac{49}{20.7} / 26.4'$

4.5

$\frac{25.2}{21.1} / \frac{5.4}{5.1}$

4.4

$\frac{25.2}{21.1} / \frac{5.3}{5.1}$

Sto	+	π	-	Grade
		712.79		

10	+50			08.4
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11				08.5
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Gr. Rod.

4

Rt

4.3

246/55
R08

4.2

