

B-19-DIV

Dr 12 - Bk. 19

OFFICE OF COUNTY ENGINEER
RAMSEY CO. MINN.

PLAN Survey

ORCHARD LANE

From Willow Ave. To White Bear Ave.

Road Acc't. No. W-6

Date Filed 12-28-38 File

W.B.Twp.

1

ORCHARD LANE

Plan survey from
West 1/4 Cor. Sec. 35 to White
Bear Ave. the ctr. of Sec. 35
White Bear Township.

10/
38

Bratger }
Wilke }
Goldberg }
Moeschter }

Angle.

Sta. Point Lt. Rt.

26+40¹² P.O.T.

14+96⁵⁰ P.O.T.

4+00.5 P.O.T.

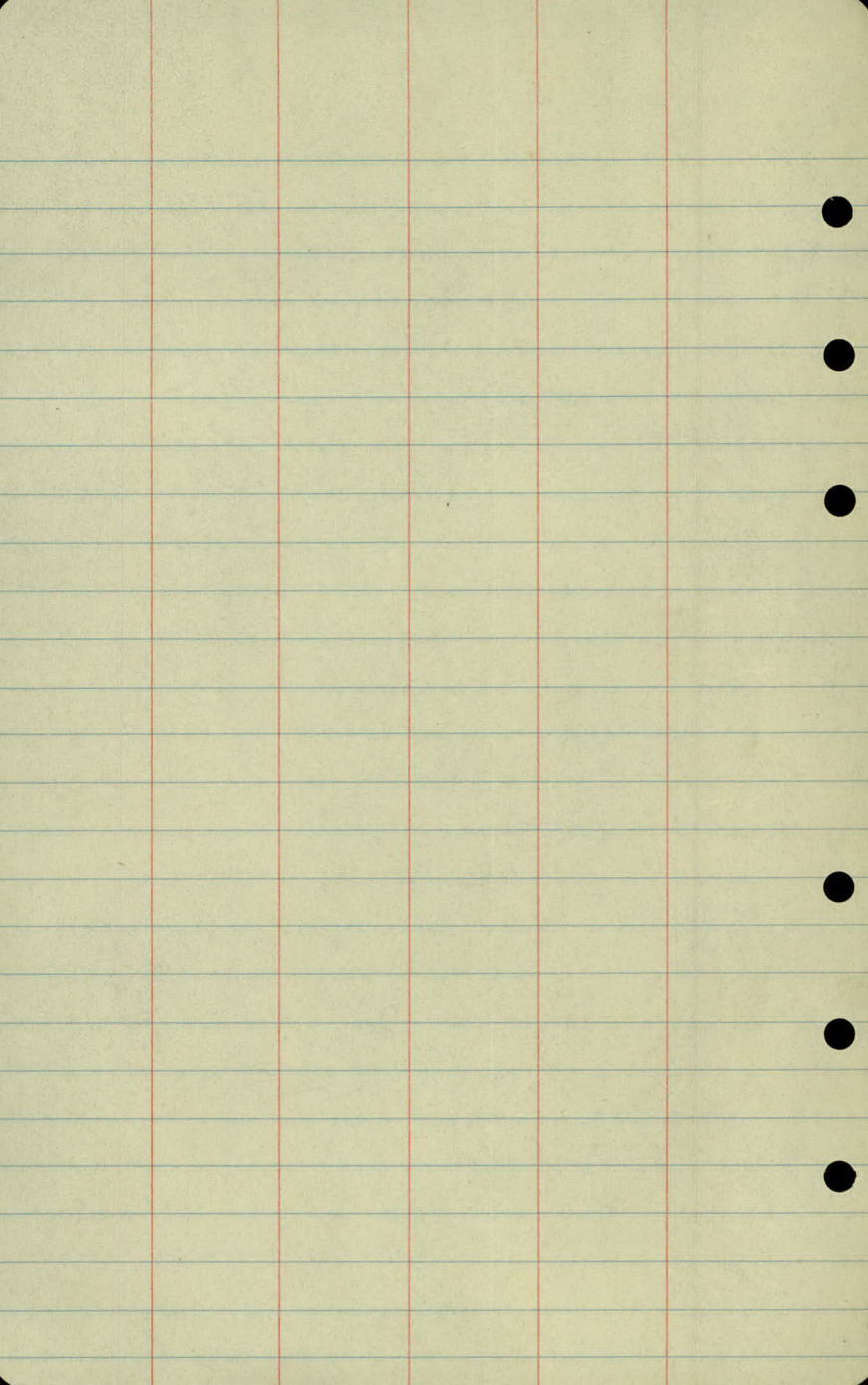
0+00 P.O.T.

Iron Plug in Cement White Bear Ave

2" Hub.

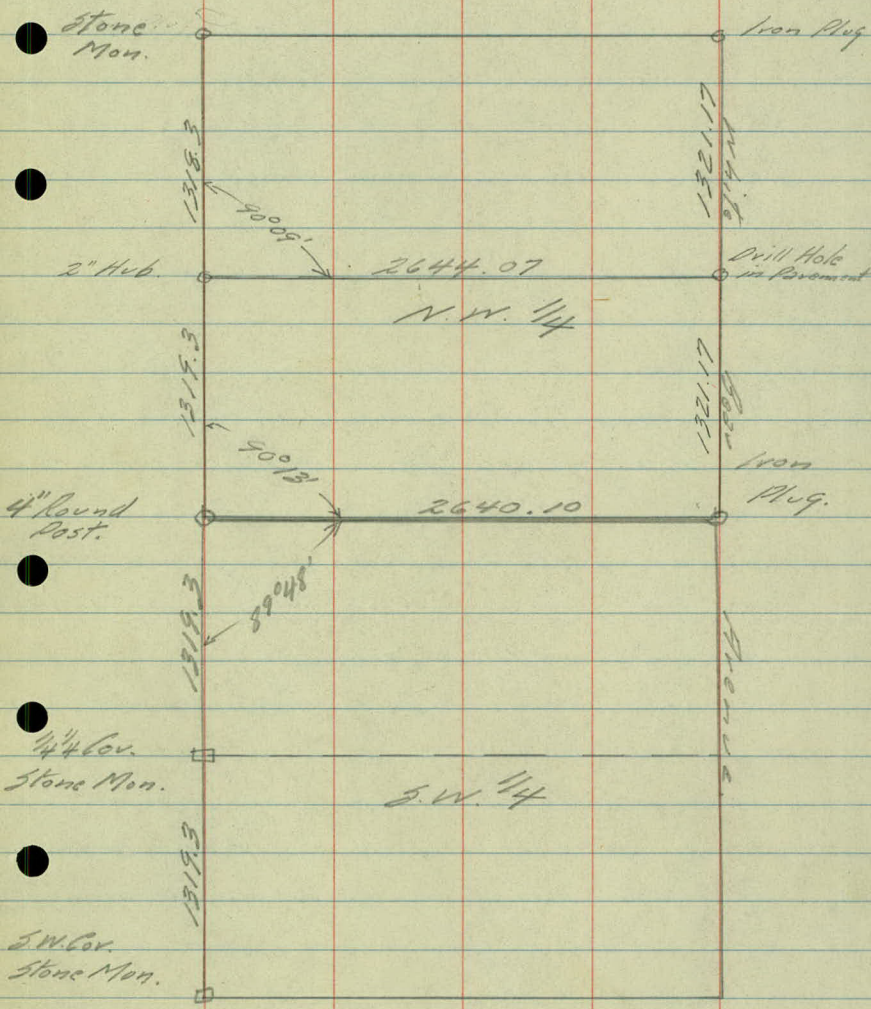
2" Hub.

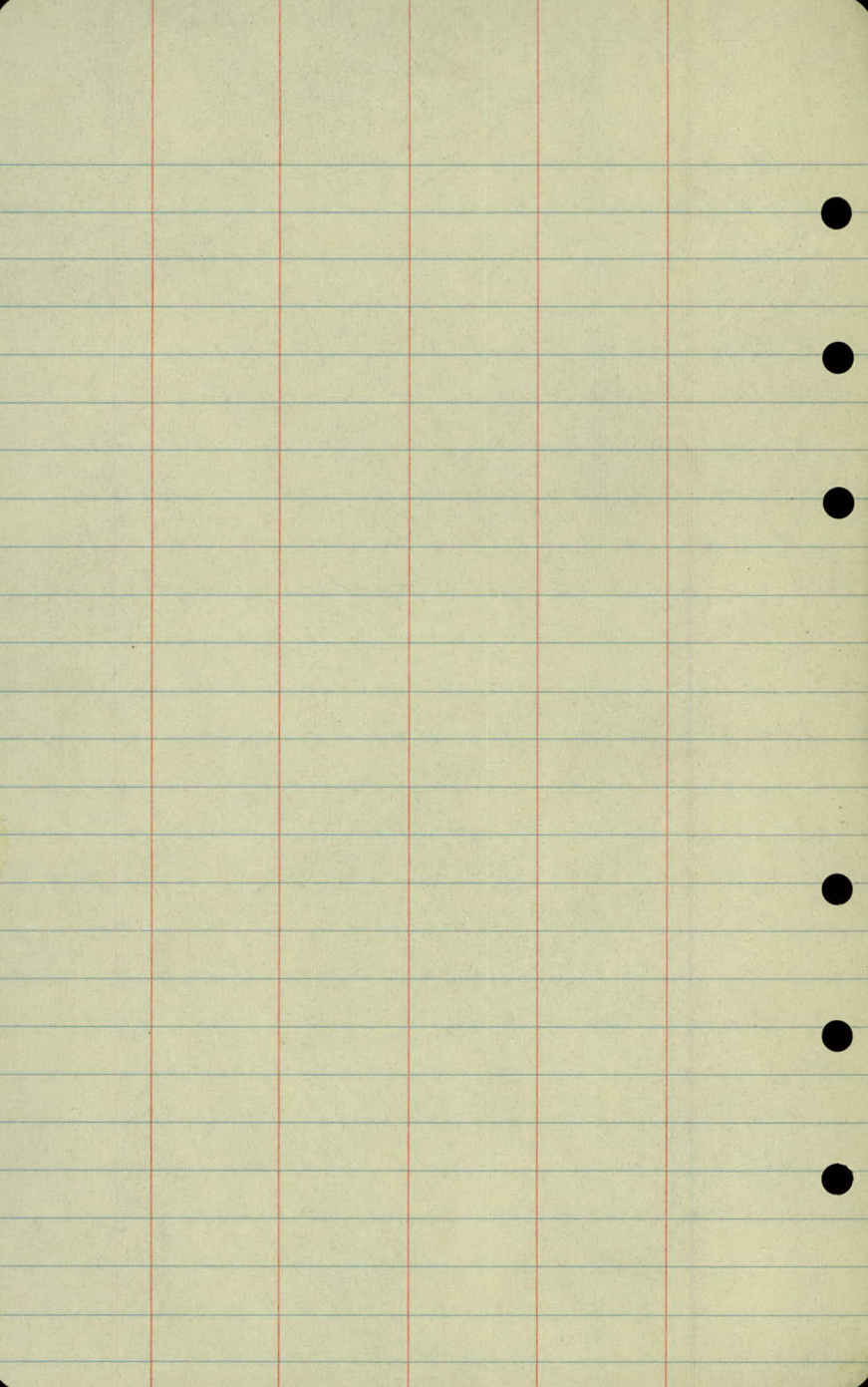
3" Round Hub.



North →

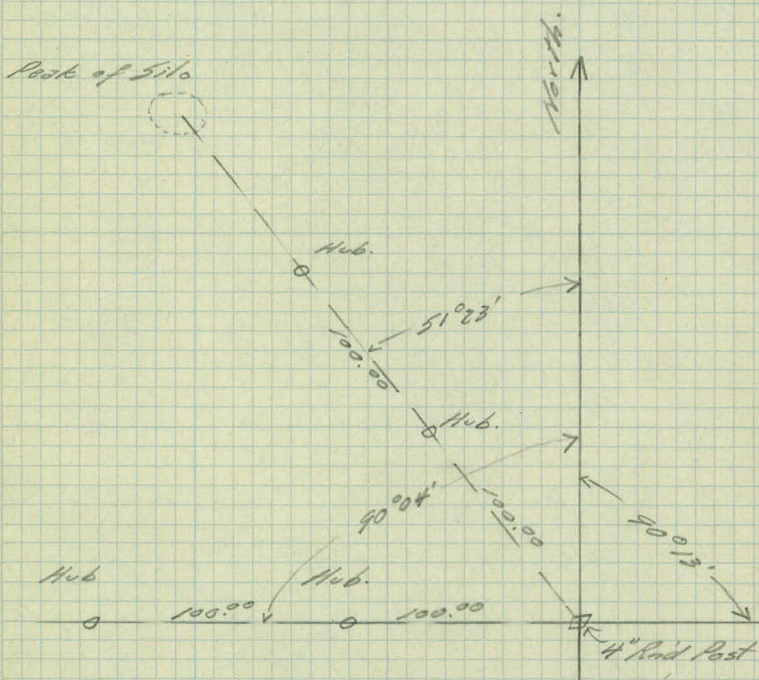
Section 35 White Bear Township.

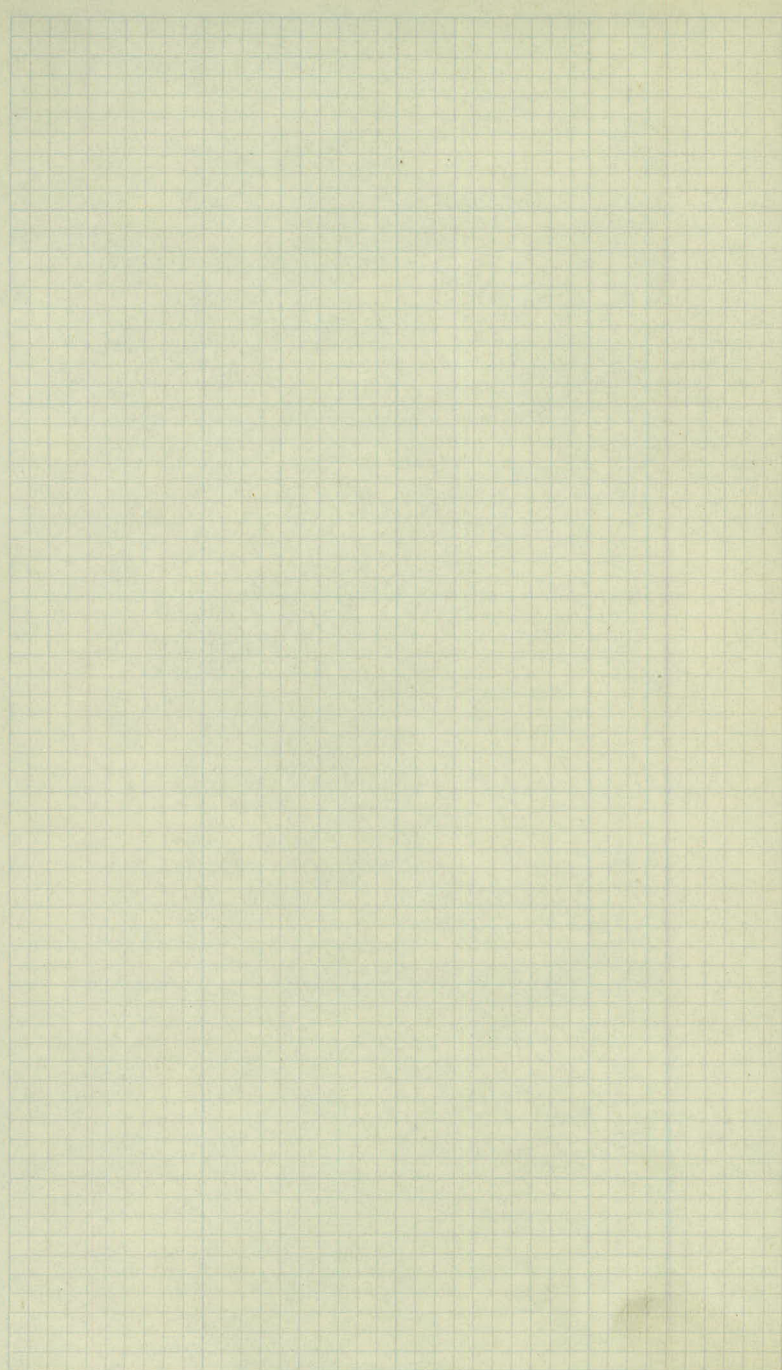




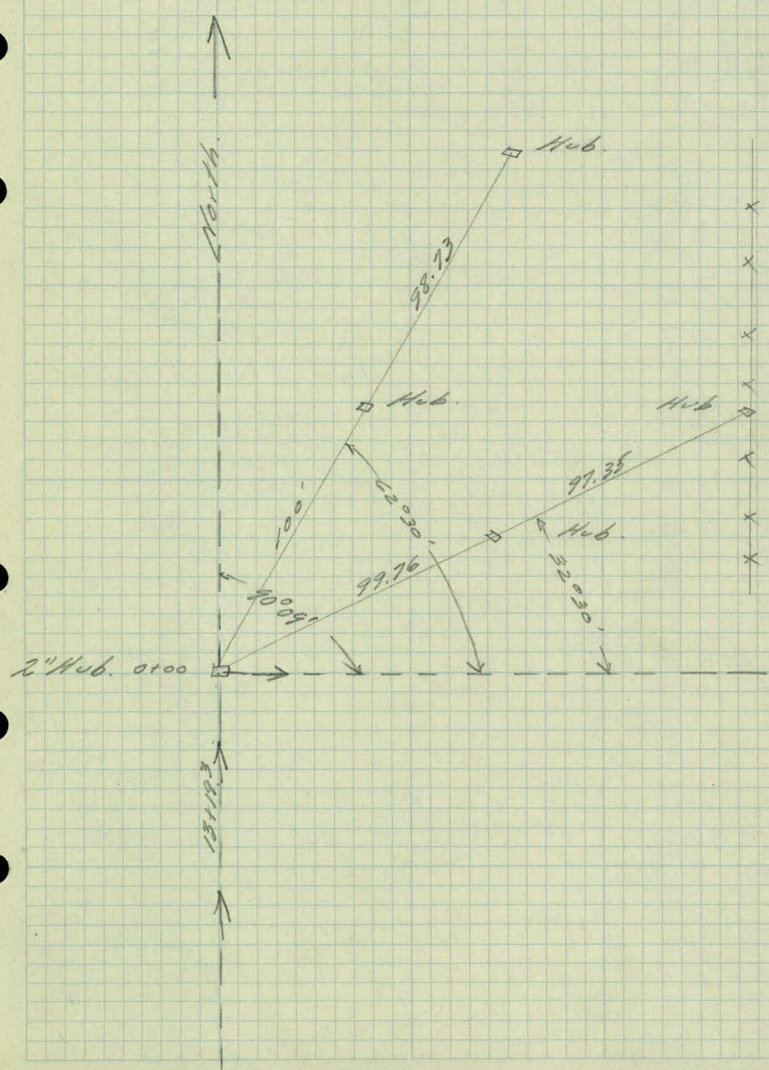
4
West 1/4 Cor. Sec. 35

White Bear Township.

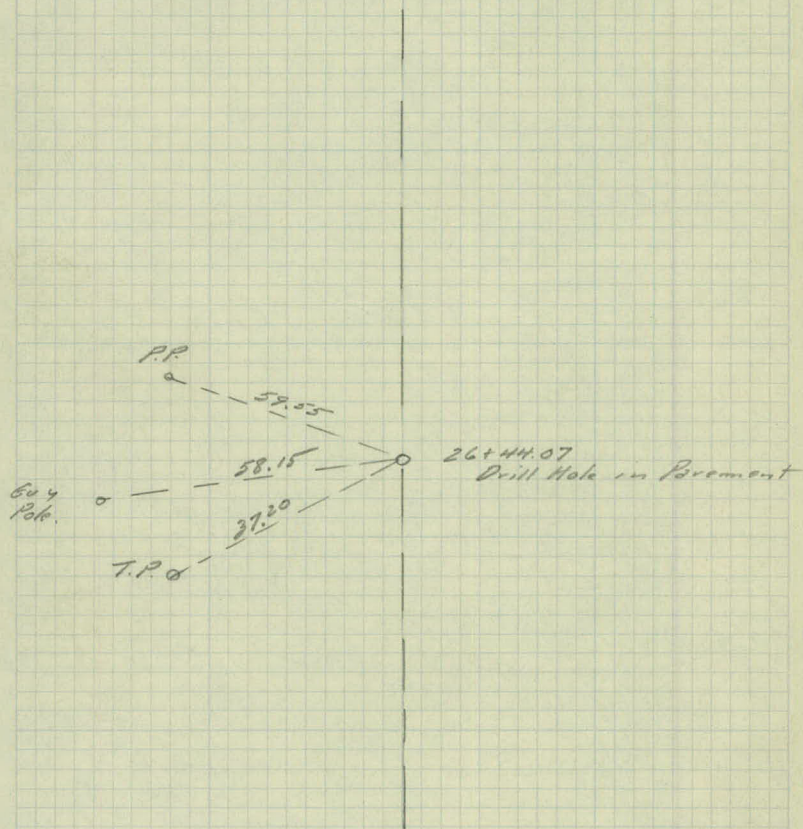


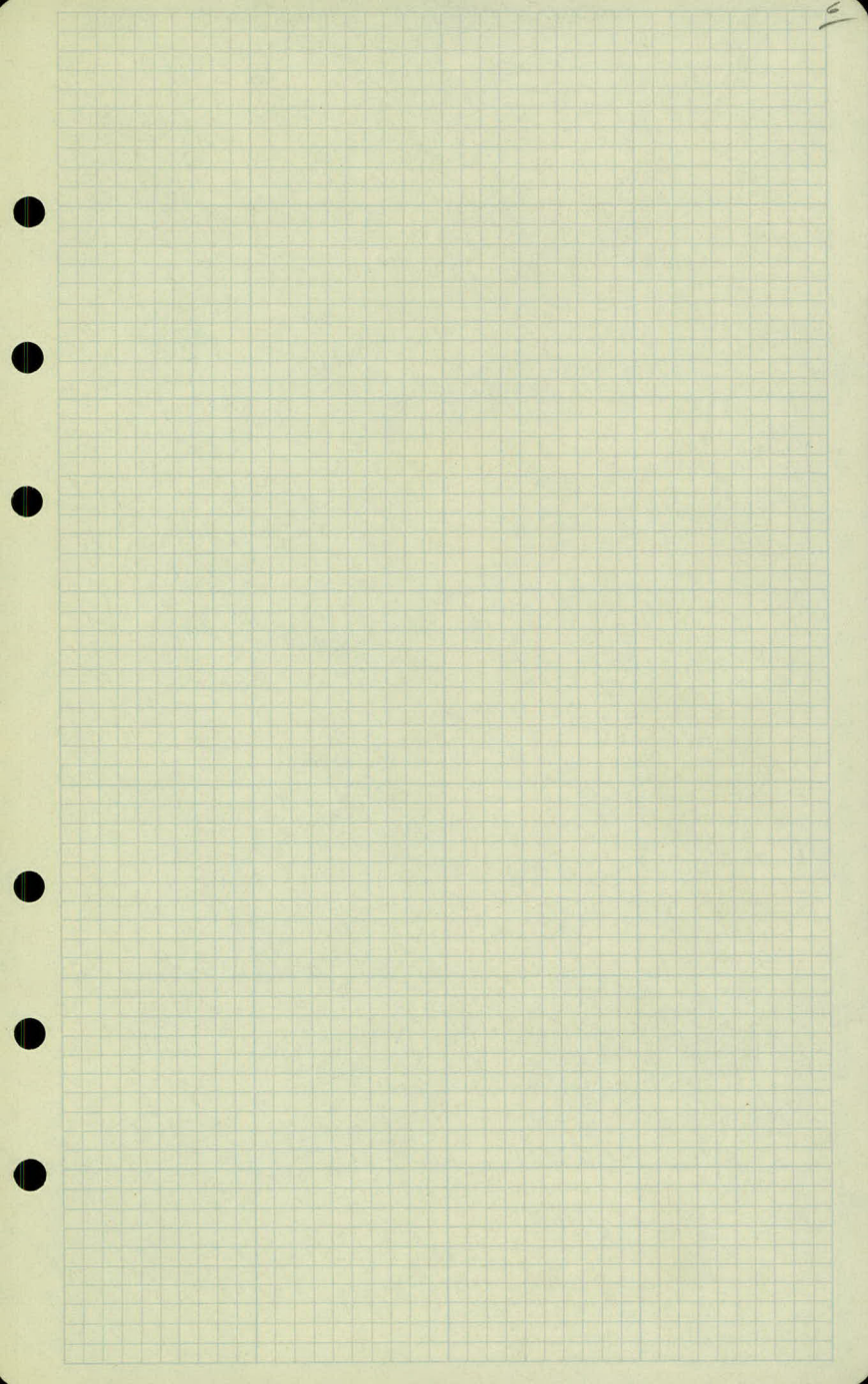


West $\frac{1}{4}$ Cor. of the N.W. $\frac{1}{4}$ of $\text{Sec } 35$



East $\frac{1}{4}$ Cor. of the N.W. $\frac{1}{4}$ Sec. 35





6

11-19 wagon
Trail
E

5

13-21

4

16-24

3

16-24

2

7-15

1

0

Cultivated

5' Wagon Trail

Cultivated

185' 8' Wagon Trail

1428 End of Post & Brush.

Brush & Post Bag



13

10-25 2

12

8-22

11

8-16

10

7-15

9

8-16

8

10-18

7

8-16

6

Cultivated

+64 = 4" Elm 33'

+64

Yard.

+80 = 2" Tree 34'

+67 = 8" Dirt Entrance

+50 Beg. Graveled Road

Cultivated

Oregon Trail

1345 20" Dirt Entrance. Price 8
+04
12+99 = 12" x 20' C.M. 6' L.T. 2

53'

12+64 End
Tree Row

Cultivated

145" Fruit
Trees spaced
20' Ctrs.

58' 10+10

Cultivated

20
8424 Engraved
Road.

19 10-22

18 9423

17 8423

16

15 10+24 Lt.

14

13

27

⁸
62.464
Road.

26

64.20

25

74.20

24

23

84.22

22

21

84.24 Lt.

20

+40.10 White Bear Ave. 20' long, Porement

+16 = 12" x 24" C.M.

+13 T.P. 25.0

3' L + E

+21 Rd Syn 7.0

+78 P.P. 26.0

Cultivated

Cultivated

+136 P.P. 26.5

+93 P.P. 27.5

Cultivated

+52 P.P. 28.0

Cultivated

+54 = 4" Elm 39.0

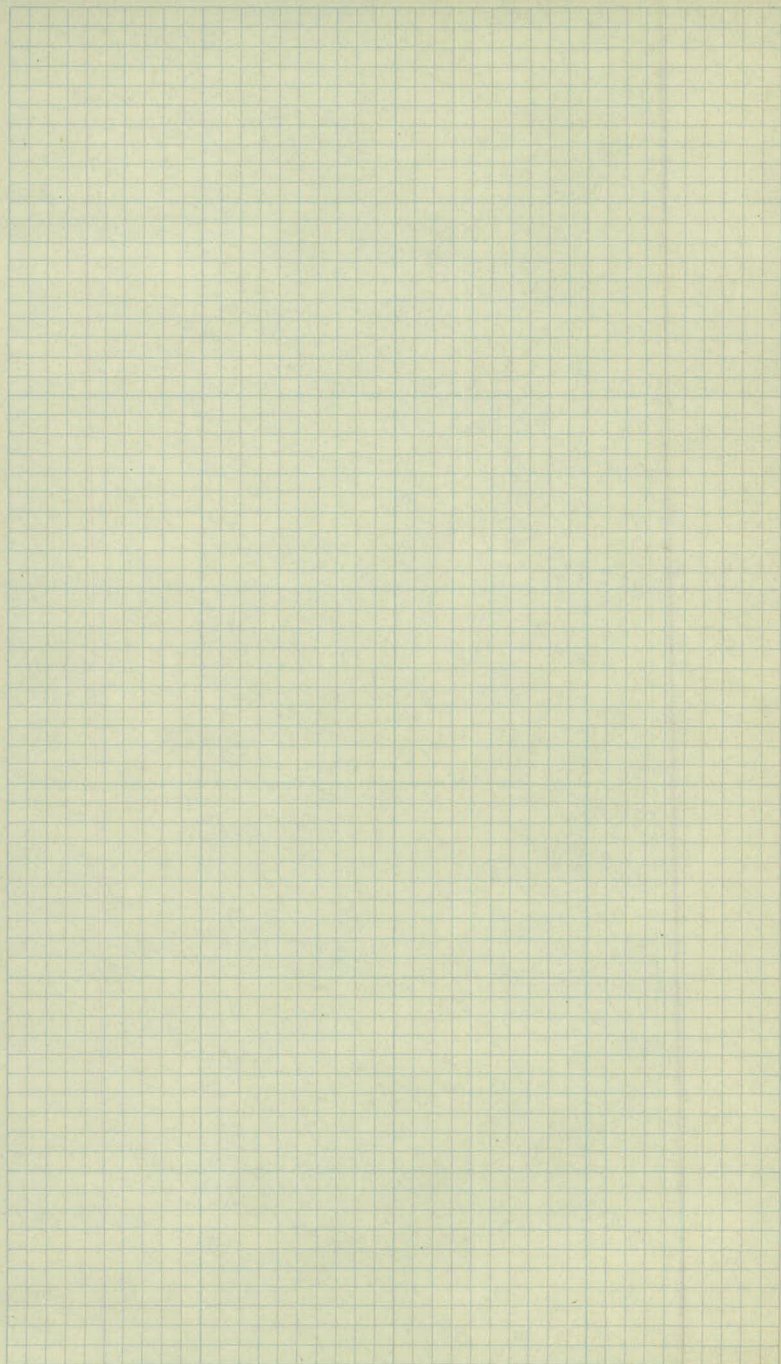
+67 = 2" Elm 36.0

+19 = 8' Dirt Entry

+06 P.P. 29.0

yard





Orchard Lane

10/38

Sta	+	K	-	Elev.
T.P.	12.75	922.14		909.39
B.M.	13.26	922.14	13.26	908.88

0-50				08.1.
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0+00				08.1.
------	--	--	--	-------

+50				08.8.
-----	--	--	--	-------

1				08.4.
---	--	--	--	-------

+17				08.3.
-----	--	--	--	-------

+60				13.6.
-----	--	--	--	-------

2				18.0.
---	--	--	--	-------

T.P.	11.70	933.26	0.58	921.56.
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+50				22.7.
-----	--	--	--	-------

3				28.2.
---	--	--	--	-------

T.P.	8.35	940.13	1.48	931.98.
------	------	--------	------	---------

+50				31.9.
-----	--	--	--	-------

4				33.8.
---	--	--	--	-------

Lt.

E

Rt.

Top of Eagle Iron at W¹/₄ Cor. Sec. 35
Spike in Fence Post Sta. 0 - 100

$$\frac{140}{50}$$

$$\frac{140}{50}$$

$$\frac{140}{50}$$

$$\frac{140}{50}$$

$$\frac{140}{50}$$

$$\frac{140}{50}$$

$$\frac{133}{50}$$

$$\frac{133}{50}$$

$$\frac{133}{50}$$

$$\frac{124}{50}$$

$$\frac{137}{50}$$

$$\frac{137}{50}$$

$$\frac{110}{50}$$

$$\frac{111}{38}$$

$$\frac{116}{23}$$

$$\frac{128}{50}$$

$$\frac{132}{50}$$

$$\frac{71}{50}$$

$$\frac{78}{39}$$

$$\frac{80}{14}$$

$$\frac{85}{50}$$

$$\frac{82}{14}$$

$$\frac{98}{22}$$

$$\frac{108}{44}$$

$$\frac{116}{50}$$

$$\frac{20}{50}$$

$$\frac{38}{5}$$

$$\frac{41}{50}$$

$$\frac{65}{50}$$

$$\frac{78}{50}$$

$$\frac{89}{30}$$

$$\frac{86}{23}$$

$$\frac{92}{14}$$

$$\frac{106}{50}$$

$$\frac{150}{50}$$

$$\frac{24}{50}$$

$$\frac{35}{24}$$

$$\frac{35}{13}$$

$$\frac{51}{50}$$

$$\frac{115}{28}$$

$$\frac{102}{50}$$

$$\frac{56}{50}$$

$$\frac{61}{36}$$

$$\frac{66}{14}$$

$$\frac{82}{50}$$

$$\frac{118}{31}$$

$$\frac{145}{50}$$

$$\frac{39}{50}$$

$$\frac{46}{33}$$

$$\frac{49}{15}$$

$$\frac{63}{50}$$

$$\frac{89}{27}$$

$$\frac{123}{50}$$

212 + π - Elev.

940.13

4450 33.8.

5 32.5.

+50 33.5.

6 33.2.

T.P. 1.40 934.08 7.45 932.68.

+50 29.9.

7 25.8.

+65 23.7.

8 23.8.

+50 24.7.

9 27.6.

+50 30.4.

T.P. 11.23 944.81 0.50 933.58.

10 33.9.

Lt.

E

Rt.

$$\frac{56}{50} \quad \frac{54}{13} \quad \frac{63}{\cancel{13}} \quad \frac{84}{30} \quad \frac{111}{50}$$

$$\frac{60}{50} \quad \frac{64}{12} \quad \frac{76}{\cancel{12}} \quad \frac{93}{26} \quad \frac{121}{50}$$

$$\frac{54}{50} \quad \frac{58}{9} \quad \frac{66}{\cancel{9}} \quad \frac{83}{30} \quad \frac{105}{50}$$

$$\frac{72}{50} \quad \frac{66}{9} \quad \frac{69}{\cancel{9}} \quad \frac{74}{30} \quad \frac{88}{50}$$

$$\frac{42}{50} \quad \frac{43}{26} \quad \frac{42}{9} \quad \frac{42}{\cancel{9}} \quad \frac{41}{33} \quad \frac{47}{50}$$

$$\frac{26}{50} \quad \frac{28}{33} \quad \frac{28}{8} \quad \frac{83}{\cancel{8}} \quad \frac{82}{19} \quad \frac{88}{50}$$

$$\frac{105}{50} \quad \frac{101}{19} \quad \frac{104}{\cancel{19}} \quad \frac{104}{50}$$

$$\frac{104}{50} \quad \frac{102}{20} \quad \frac{103}{\cancel{20}} \quad \frac{97}{50}$$

$$\frac{54}{50} \quad \frac{52}{24} \quad \frac{54}{8} \quad \frac{54}{\cancel{8}} \quad \frac{50}{50}$$

$$\frac{68}{50} \quad \frac{66}{23} \quad \frac{65}{\cancel{23}} \quad \frac{64}{50}$$

$$\frac{28}{50} \quad \frac{32}{17} \quad \frac{37}{\cancel{17}} \quad \frac{32}{50}$$

$$\frac{97}{50} \quad \frac{107}{21} \quad \frac{109}{\cancel{21}} \quad \frac{122}{21} \quad \frac{122}{50}$$

Sta	+	π	-	Elev.	
		944.81.			
10+50				34.5.	
11				38.4.	
+50				41.8.	
12				40.4.	
+50				38.8.	
13				39.1.	
B.M.	4.60	944.81	4.60	940.21.	
+60				38.31.	
14				38.6.	
14					
+50				41.2.	41.4
+85				42.7.	
15				42.3.	
+50				39.2.	

Lt. £ Rt

$$\frac{93}{50} \quad \frac{93}{20} \quad \frac{95}{8} \quad \frac{103}{\cancel{20}} \quad \frac{108}{20} \quad \frac{109}{50}$$

$$\frac{60}{50} \quad \frac{64}{22} \quad \frac{64}{\cancel{20}} \quad \frac{68}{21} \quad \frac{67}{50}$$

$$\frac{33}{50} \quad \frac{35}{25} \quad \frac{44}{22} \quad \frac{39}{13} \quad \frac{40}{6} \quad \frac{30}{3} \quad \frac{30}{\cancel{20}} \quad \frac{34}{20} \quad \frac{30}{50}$$

$$\frac{42}{50} \quad \frac{45}{24} \quad \frac{42}{14} \quad \frac{48}{6} \quad \frac{44}{\cancel{20}} \quad \frac{47}{30} \quad \frac{47}{50}$$

$$\frac{57}{50} \quad \frac{62}{26} \quad \frac{56}{22} \quad \frac{51}{16} \quad \frac{54}{9} \quad \frac{66}{4} \quad \frac{60}{\cancel{20}} \quad \frac{63}{18} \quad \frac{52}{50}$$

$$\frac{57}{50} \quad \frac{63}{27} \quad \frac{54}{23} \quad \frac{50}{16} \quad \frac{54}{10} \quad \frac{61}{8} \quad \frac{57}{\cancel{20}} \quad \frac{58}{21} \quad \frac{62}{50}$$

Spike in RP 100' Rt. 515. 13120

$$\frac{45}{50} \quad \frac{53}{29} \quad \frac{60}{26} \quad \frac{63}{24} \quad \frac{50}{16} \quad \frac{54}{10} \quad \frac{62}{5} \quad \frac{65}{\cancel{20}} \quad \frac{71}{18} \quad \frac{70}{50}$$

$$\frac{54}{50} \quad \frac{58}{29} \quad \frac{64}{27} \quad \frac{56}{25} \quad \frac{52}{17} \quad \frac{58}{7} \quad \frac{63}{5} \quad \frac{62}{\cancel{20}} \quad \frac{60}{35} \quad \frac{58}{50}$$

$$\frac{53}{50} \quad \frac{51}{30} \quad \frac{54}{27} \quad \frac{47}{16} \quad \frac{51}{10} \quad \frac{54}{6} \quad \frac{36}{3} \quad \frac{34}{\cancel{20}} \quad \frac{36}{50}$$

$$\frac{47}{50} \quad \frac{44}{31} \quad \frac{51}{26} \quad \frac{43}{17} \quad \frac{45}{13} \quad \frac{50}{6} \quad \frac{23}{2} \quad \frac{21}{\cancel{20}} \quad \frac{24}{32} \quad \frac{21}{50}$$

$$\frac{55}{50} \quad \frac{53}{26} \quad \frac{48}{24} \quad \frac{44}{17} \quad \frac{53}{15} \quad \frac{25}{12} \quad \frac{25}{\cancel{20}} \quad \frac{24}{23} \quad \frac{36}{50}$$

$$\frac{71}{50} \quad \frac{60}{26} \quad \frac{51}{17} \quad \frac{54}{18} \quad \frac{60}{6} \quad \frac{56}{\cancel{20}} \quad \frac{55}{50}$$

Sta.	+	π	-	Elev.
		944.81		

16				39.7.
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T.P.	7.5V	946.73	5.60	939.21
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+80				39.6.
-----	--	--	--	-------

+80				36.9.
-----	--	--	--	-------

17				35.0.
----	--	--	--	-------

+37				32.8.
-----	--	--	--	-------

+67				32.8.
-----	--	--	--	-------

C.M. Culvert

18				38.8.
----	--	--	--	-------

+80				40.2.
-----	--	--	--	-------

19				42.5.
----	--	--	--	-------

+30				43.0.
-----	--	--	--	-------

20				40.3.
----	--	--	--	-------

B.M.	14.18	946.73	14.18	934.55
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Lt.

E

Rt.

$$\frac{68}{20} \quad \frac{61}{25} \quad \frac{54}{15} \quad \frac{60}{8} \quad \frac{65}{4} \quad \frac{51}{5} \quad \frac{64}{20}$$

$$\frac{76}{50} \quad \frac{71}{31} \quad \frac{87}{27} \quad \frac{86}{24} \quad \frac{81}{15} \quad \frac{83}{11} \quad \frac{88}{7} \quad \frac{90}{4} \quad \frac{71}{9} \quad \frac{88}{9} \quad \frac{92}{27} \quad \frac{108}{50}$$

$$\frac{76}{50} \quad \frac{85}{37} \quad \frac{51}{31} \quad \frac{94}{24} \quad \frac{90}{15} \quad \frac{101}{5} \quad \frac{98}{10} \quad \frac{114}{25} \quad \frac{118}{25} \quad \frac{131}{20}$$

$$\frac{78}{50} \quad \frac{51}{34} \quad \frac{97}{26} \quad \frac{94}{16} \quad \frac{98}{8} \quad \frac{102}{5} \quad \frac{117}{10} \quad \frac{130}{23} \quad \frac{134}{23} \quad \frac{153}{50}$$

$$\frac{104}{50} \quad \frac{116}{34} \quad \frac{107}{27} \quad \frac{100}{15} \quad \frac{105}{7} \quad \frac{138}{10} \quad \frac{150}{10} \quad \frac{163}{50}$$

$$\frac{126}{50} \quad \frac{127}{43} \quad \frac{118}{30} \quad \frac{108}{25} \quad \frac{101}{13} \quad \frac{110}{5} \quad \frac{138}{26} \quad \frac{150}{26} \quad \frac{162}{50}$$

$$\frac{132}{141} \quad 33.5 \quad \frac{141}{141} \quad 32.6$$

$$\frac{121}{50} \quad \frac{118}{35} \quad \frac{106}{26} \quad \frac{98}{17} \quad \frac{103}{8} \quad \frac{114}{3} \quad \frac{79}{16} \quad \frac{126}{16} \quad \frac{118}{50}$$

$$\frac{106}{50} \quad \frac{98}{27} \quad \frac{80}{16} \quad \frac{98}{1} \quad \frac{65}{6} \quad \frac{73}{27} \quad \frac{22}{27} \quad \frac{64}{50}$$

$$\frac{97}{50} \quad \frac{84}{27} \quad \frac{80}{16} \quad \frac{83}{6} \quad \frac{42}{1} \quad \frac{28}{5} \quad \frac{25}{5} \quad \frac{40}{50}$$

$$\frac{81}{50} \quad \frac{75}{46} \quad \frac{78}{27} \quad \frac{74}{17} \quad \frac{71}{6} \quad \frac{60}{14} \quad \frac{37}{2} \quad \frac{21}{5} \quad \frac{28}{5} \quad \frac{44}{10}$$

$$\frac{88}{10} \quad \frac{79}{27} \quad \frac{84}{25} \quad \frac{78}{11} \quad \frac{86}{11} \quad \frac{64}{14} \quad \frac{69}{14} \quad \frac{66}{10}$$

Top of Conc. Wall N.E. Cor. 150' Lt. Sta 18135

Sta.	+	T	-	Elev.
		946.73		
20+50				37.4.
21				35.7.
+50				35.4.
22				36.1.
T.P.	10.98	947.71	10.00	936.73
+50				35.6.
23				35.8.
+50				37.0.
24				39.6.
+50				41.4.
25				41.9.
+50				44.3.

Lt.

E

Rt.

16

$$\frac{10^2}{50} \quad \frac{10^0}{31} \quad \frac{9^2}{17} \quad \frac{9^6}{9} \quad \frac{10^1}{4} \quad \frac{9^3}{14} \quad \frac{9^7}{14} \quad \frac{8^0}{50}$$

$$\frac{13^3}{50} \quad \frac{12^5}{33} \quad \frac{10^7}{26} \quad \frac{10^3}{15} \quad \frac{10^6}{8} \quad \frac{11^6}{3} \quad \frac{11^0}{110} \quad \frac{10^2}{31} \quad \frac{9^0}{50}$$

$$\frac{12^8}{50} \quad \frac{12^1}{32} \quad \frac{11^0}{26} \quad \frac{10^6}{15} \quad \frac{10^8}{7} \quad \frac{12^1}{2} \quad \frac{11^3}{113} \quad \frac{10^5}{31} \quad \frac{9^4}{50}$$

$$\frac{11^7}{50} \quad \frac{11^6}{37} \quad \frac{11^3}{25} \quad \frac{10^5}{15} \quad \frac{10^7}{8} \quad \frac{11^6}{3} \quad \frac{10^6}{106} \quad \frac{10^2}{38} \quad \frac{9^6}{50}$$

$$\frac{12^1}{50} \quad \frac{12^1}{35} \quad \frac{12^2}{26} \quad \frac{11^1}{15} \quad \frac{11^6}{9} \quad \frac{12^3}{3} \quad \frac{12^3}{2} \quad \frac{12^1}{121} \quad \frac{11^6}{22} \quad \frac{10^0}{50}$$

$$\frac{11^1}{50} \quad \frac{12^4}{28} \quad \frac{11^8}{24} \quad \frac{10^8}{14} \quad \frac{11^3}{8} \quad \frac{12^5}{3} \quad \frac{12^1}{2} \quad \frac{11^9}{119} \quad \frac{11^0}{28} \quad \frac{9^0}{50}$$

$$\frac{11^4}{50} \quad \frac{11^6}{39} \quad \frac{11^1}{24} \quad \frac{10^3}{15} \quad \frac{10^6}{8} \quad \frac{11^5}{3} \quad \frac{11^0}{2} \quad \frac{10^7}{107} \quad \frac{10^4}{21} \quad \frac{8^0}{50}$$

$$\frac{10^0}{50} \quad \frac{10^1}{40} \quad \frac{9^2}{26} \quad \frac{9^8}{23} \quad \frac{9^0}{14} \quad \frac{8^4}{8} \quad \frac{5^8}{3} \quad \frac{8^1}{1} \quad \frac{8^1}{81} \quad \frac{2^6}{24} \quad \frac{5^1}{50}$$

$$\frac{2^6}{50} \quad \frac{2^4}{26} \quad \frac{8^1}{24} \quad \frac{2^2}{14} \quad \frac{2^1}{7} \quad \frac{8^0}{3} \quad \frac{6^5}{1} \quad \frac{6^3}{63} \quad \frac{5^3}{23} \quad \frac{2^8}{50}$$

$$\frac{6^4}{50} \quad \frac{6^3}{38} \quad \frac{5^2}{26} \quad \frac{6^2}{24} \quad \frac{5^3}{13} \quad \frac{5^7}{7} \quad \frac{6^1}{3} \quad \frac{5^8}{51} \quad \frac{6^3}{51} \quad \frac{6^4}{25} \quad \frac{4^1}{50}$$

$$\frac{5^0}{50} \quad \frac{4^7}{40} \quad \frac{5^0}{26} \quad \frac{3^9}{21} \quad \frac{4^8}{23} \quad \frac{4^2}{15} \quad \frac{5^0}{3} \quad \frac{4^7}{1} \quad \frac{3^4}{31} \quad \frac{4^4}{51} \quad \frac{5^4}{25} \quad \frac{4^3}{50}$$

Sta.	+	π	-	Elev.
		947.71		
26				44.3
+17				43.2
+15				41.8
+22				43.4
+26				44.0
+40.10				44.2
B.M.			3.55	944.16

Lt.

E

Rt.

17

$$\frac{38}{50} \quad \frac{38}{31} \quad \frac{32}{24} \quad \frac{38}{23} \quad \frac{34}{12} \quad \frac{40}{2} \quad \frac{34}{1} \quad \frac{32}{1} \quad \frac{42}{13} \quad \frac{44}{50}$$

$$\frac{40}{50} \quad \frac{37}{23} \quad \frac{34}{13} \quad \frac{38}{5} \quad \frac{42}{2} \quad \frac{45}{1} \quad \frac{47}{50}$$

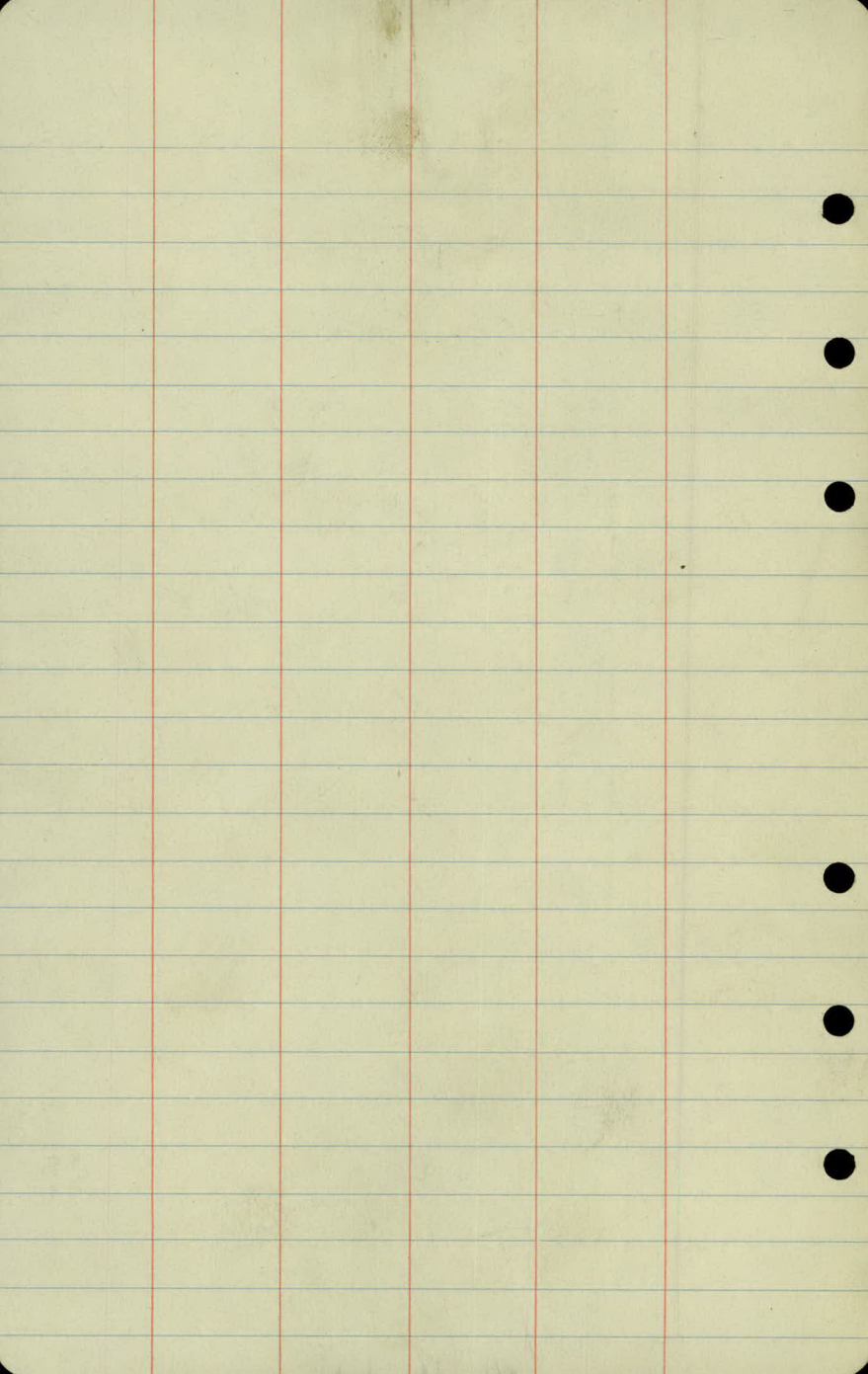
$$\frac{57}{50} \quad \frac{60}{29} \quad \frac{38}{26} \quad \frac{34}{14} \quad \frac{44}{4} \quad \frac{57}{3} \quad \frac{59}{1} \quad \frac{69}{50}$$

$$\frac{54}{50} \quad \frac{54}{36} \quad \frac{37}{28} \quad \frac{33}{15} \quad \frac{38}{6} \quad \frac{43}{1} \quad \frac{58}{10} \quad \frac{69}{50}$$

$$\frac{33}{50} \quad \frac{33}{23} \quad \frac{33}{12} \quad \frac{37}{1} \quad \frac{39}{20}$$

$$\frac{32}{50} \quad \frac{35}{1} \quad \frac{39}{50}$$

Top of Iron Plug Ch. Sec. 35



Orchard Lane

0+00 - \$10.00 9.0 12.0

25R 50Rt

+50 \$7.0 20Rt 20Lft.
7.0 6.0

1+00 \$4.0 20Rt 20Lft.
4.0 3.0

1+25 \$2.0 20Rt
2.0

+50 \$2.0 20Rt.
2.0

PUSH SOUNDINGS

north off orch Lane

1+00 \$6.0

1+50 \$5.0

Push sounding of feet

~~Monday~~

~~Paul~~

~~Call Mr Buckman~~

~~Sept 3~~

Orchard Lane.

Slope Stakes.

$\frac{12}{38}$

26' Crown

2:1 Slopes

21' to Backslope @ ditch

Sta.	+	X	-	Elev.
B.M.	10.84	919.70		908.88
0+48				16.7

+48				16.7
-----	--	--	--	------

1				16.9
---	--	--	--	------

+17				16.9
-----	--	--	--	------

+60				17.8
-----	--	--	--	------

T.P.	8.52	927.28	0.94	918.76
------	------	--------	------	--------

2				18.6
---	--	--	--	------

+50				19.6
-----	--	--	--	------

T.P.	13.73	937.20	3.81	923.47
------	-------	--------	------	--------

3				20.7
---	--	--	--	------

+50				21.7
-----	--	--	--	------

24.

E

24.

3.0

10.7
F.7.7

11.4
F.8.4
29.8

3.0

10.9
F.7.9
28.8

11
F.8.1
29.2

2.8

10.2
F.7.4
27.8

11.2
F.8.4

10.8
F.8.0
29.0

2.8

1.9

5.3
F.3.4
19.8

6.0
F.4.1

6.3
F.4.4
21.8

8.7
10.7

8.7
D.C.2.5
26.0

9.4
F.0.7

10.4
D.C.0.3
21.6

7.7
9.7

3.0
D.C.6.7
34.4

4.6
C.3.1

6.5
D.C.3.2
27.4

Top & slope 2450

16.5
18.5

6.1
D.C.12.4
45.8

9.0
C.7.5

12.3
D.C.6.2
37.4

15.5
17.5

2.5
D.C.15.0
57.0

5.2
C.10.3

9.8
D.C.7.7
36.4

Sta. + π - Grade

937.20

4

22.8

+50

23.8

5

24.9

+50

25.9

6

27.0

1.47 935.20 3.47 933.73

+50

28.0

7

29.1

+65

30.5

Lt.

E

Rt.

$$\begin{array}{r} 144 \\ 164 \end{array}$$

$$\begin{array}{r} 09 \\ DC15.5 \\ \hline 52.0 \end{array}$$

$$\begin{array}{r} 3.3 \\ C11.1 \end{array}$$

$$\begin{array}{r} 77 \\ DC8.7 \\ \hline 38.4 \end{array}$$

$$\begin{array}{r} 134 \\ 154 \end{array}$$

$$\begin{array}{r} 26 \\ DC12.8 \\ \hline 46.6 \end{array}$$

$$\begin{array}{r} 33 \\ C10.1 \end{array}$$

$$\begin{array}{r} 67 \\ DC8.7 \\ \hline 38.4 \end{array}$$

$$\begin{array}{r} 123 \\ 143 \end{array}$$

$$\begin{array}{r} 33 \\ DC11.0 \\ \hline 43.0 \end{array}$$

$$\begin{array}{r} 46 \\ C77 \end{array}$$

$$\begin{array}{r} 73 \\ DC7.0 \\ \hline 35.0 \end{array}$$

$$\begin{array}{r} 113 \\ 133 \end{array}$$

$$\begin{array}{r} 25 \\ DC10.8 \\ \hline 42.6 \end{array}$$

$$\begin{array}{r} 36 \\ C77 \end{array}$$

$$\begin{array}{r} 60 \\ DC7.3 \\ \hline 35.0 \end{array}$$

$$\begin{array}{r} 102 \\ 122 \end{array}$$

$$\begin{array}{r} 45 \\ DC7.7 \\ \hline 36.4 \end{array}$$

$$\begin{array}{r} 40 \\ C62 \end{array}$$

$$\begin{array}{r} 47 \\ DC7.5 \\ \hline 36.0 \end{array}$$

$$\begin{array}{r} 7.2 \\ 9.2 \end{array}$$

$$\begin{array}{r} 5.8 \\ DC3.4 \\ \hline 27.8 \end{array}$$

$$\begin{array}{r} 5.4 \\ C1.8 \end{array}$$

$$\begin{array}{r} 5.2 \\ DC4.0 \\ \hline 29.0 \end{array}$$

6.1

$$\begin{array}{r} 19 \\ 9.0 \\ F2.9 \\ \hline 18.8 \end{array}$$

$$\begin{array}{r} 9.3 \\ F3.2 \end{array}$$

$$\begin{array}{r} 19.5 \\ 9.5 \\ F3.4 \\ \hline 19.8 \end{array}$$

4.7

$$\begin{array}{r} 11.4 \\ F6.7 \\ \hline 26.4 \end{array}$$

$$\begin{array}{r} 11.5 \\ F6.8 \end{array}$$

$$\begin{array}{r} 11.5 \\ F6.8 \\ \hline 26.8 \end{array}$$

5 1/2 + π - Grade

935.20

8 31.2

+50 32.2

9 33.3

T.P. 13.54 941.81 693 928.27

+50 34.3

10 35.4

+50 36.5

11 37.5

T.P. 663 945.82 263 939.19

+50 38.4

L+

E

R+

4.0

$$\begin{array}{r} 11.4 \\ F7.4 \\ \hline 27.8 \end{array}$$

$$\begin{array}{r} 11.4 \\ F7.4 \end{array}$$

$$\begin{array}{r} 10.8 \\ F6.8 \\ \hline 26.6 \end{array}$$

3.0

$$\begin{array}{r} 10.4 \\ F7.4 \\ \hline 27.8 \end{array}$$

$$\begin{array}{r} 10.5 \\ F7.5 \end{array}$$

$$\begin{array}{r} 9.9 \\ F6.9 \\ \hline 26.8 \end{array}$$

1.9

$$\begin{array}{r} 8.2 \\ F6.3 \\ \hline 23.6 \end{array}$$

$$\begin{array}{r} 7.4 \\ F5.7 \end{array}$$

$$\begin{array}{r} 7.5 \\ F5.6 \\ \hline 24.2 \end{array}$$

7.5

$$\begin{array}{r} 11.0 \\ F3.5 \\ \hline 20.0 \end{array}$$

$$\begin{array}{r} 11.3 \\ F3.8 \end{array}$$

$$\begin{array}{r} 11.2 \\ F3.7 \\ \hline 20.4 \end{array}$$

6.4
8.4

$$\begin{array}{r} 7.8 \\ DC0.6 \\ \hline 22.2 \end{array}$$

$$\begin{array}{r} 7.9 \\ F1.5 \end{array}$$

$$\begin{array}{r} 8.7 \\ F2.3 \\ \hline 19.6 \end{array}$$

5.3
7.3

$$\begin{array}{r} 6.4 \\ DC0.9 \\ \hline 22.9 \end{array}$$

$$\begin{array}{r} 7.3 \\ F2.0 \end{array}$$

$$\begin{array}{r} 7.9 \\ F2.6 \\ \hline 18.2 \end{array}$$

4.3
6.3

$$\begin{array}{r} 3.9 \\ DC2.4 \\ \hline 25.9 \end{array}$$

$$\begin{array}{r} 3.6 \\ DC0.9 \end{array}$$

$$\begin{array}{r} 3.6 \\ DC2.7 \\ \hline 26.4 \end{array}$$

7.4
9.4

$$\begin{array}{r} 4.6 \\ DC4.8 \\ \hline 30.4 \end{array}$$

$$\begin{array}{r} 4.0 \\ DC3.4 \end{array}$$

$$\begin{array}{r} 4.1 \\ DC0.3 \\ \hline 31.6 \end{array}$$

Sto. + K - Grade

945.82

12

39.1

150

39.6

13

39.8

B.M.

5.61

940.21

940.21

4.

5

6

6.7
8.7

5.5
DC3.2
27.4

5.3
C1.4

5.5
DC3.2
27.4

6.2
8.2

6.7
DC1.2
240

7.0
F0.8

6.5
DC1.2
244

6.0
8.0

6.5
DC1.3
240

6.7
F0.7

6.8
DC1.2
23.4

