

B-16-D-12

Dr. 12 - Bk. 16

OFFICE OF COUNTY ENGINEER
RAMSEY CO. MINN.

PLAN Survey

MISSISSIPPI ST.

From Edgerton St. To Labore Road.

Road Acc't. No. W-41

Date Filed 12-28-38

File

26' Top

2:1 Fill Cont

21' to Back Slope

Mississippi St.

Slope stakes Edgerton
St. to Labore Road.

Sta.	+	x	-	Rev. Grade.
B.M.	5.34	914.59		909.27
5+00			09.8	10.05 Revised Grades
+50			09.9	9.8
+70			09.9	9.8
6			09.9	9.7
+50			09.9	9.7
7			10.0	9.8
+50			10.0	9.8
8			10.1	9.8

Lt.

E

Rt.

21

Spike in Cottonwood 200' Rt. 10+50

4.8
6.8DC
1.8
24.6~~4.8~~
DC ~~1.8~~
24.04.6
60.0~~5.1~~
DC ~~1.5~~
24.44.7
6.7DC 1.8
24.6~~5.0~~
DC ~~1.7~~
24.45.4
F0.7~~5.7~~
DC ~~1.0~~
23.0DC 1.1
23.24.7
6.7

X

4.7
6.7~~5.0~~
DC ~~1.7~~
24.4DC 1.9
24.85.6
F0.9
0.7~~5.3~~
DC ~~1.4~~
23.8DC 1.6
24.24.7
6.72.1
DC 1.9
24.45.3
F1.0
0.85.3
DC 1.4
23.81.6
24.24.6
6.65.2
DC 1.4
23.81.6
24.25.8
F1.0
1.05.1
DC 1.1
23.21.3
23.64.6
6.65.4
DC 1.2
23.41.4
23.85.8
F1.0
1.05.4
DC 1.2
23.41.4
23.84.5
6.55.3
DC 1.2
23.41.5
24.05.8
F1.3
F1.05.2
DC 1.2
23.41.6
24.2

Sta	+	π	-	Grade	Revised Grade
		714.59			
8+50				10.1	9.8
9				10.2	9.9
+50				10.2	9.9
10				10.3	10.0
+50 +35				10.3	10.0
11				10.4	10.0
T.P.	5.34	915.20	4.73	909.86	
+50				10.4	10.0
12				10.5	10.1

4

8

21

$$\begin{array}{r} 4.5 \\ 6.5 \end{array}$$

$$\begin{array}{r} 5.7 \\ \cancel{DCD} \times 1.1 \\ \hline 22.6 \end{array}$$

$$\begin{array}{r} 5.8 \\ \cancel{F.3} \\ \hline 1.0 \end{array}$$

$$\begin{array}{r} 5.2 \\ \cancel{DCD} \times 1.6 \\ \hline 23.6 \end{array}$$

$$\begin{array}{r} 4.4 \\ 6.4 \end{array}$$

$$\begin{array}{r} 5.7 \\ \cancel{DCD} \times 1.0 \\ \hline 22.4 \end{array}$$

$$\begin{array}{r} 5.9 \\ \cancel{F.1} \\ \hline 1.7 \end{array}$$

$$\begin{array}{r} 5.7 \\ \cancel{DCD} \times 1.0 \\ \hline 22.4 \end{array}$$

$$\begin{array}{r} 4.4 \\ 6.4 \end{array}$$

$$\begin{array}{r} 5.7 \\ \cancel{DCD} \times 1.0 \\ \hline 22.4 \end{array}$$

$$\begin{array}{r} 6.0 \\ \cancel{F.1} \\ \hline 1.3 \end{array}$$

$$\begin{array}{r} 6.0 \\ \cancel{DCD} \times 0.7 \\ \hline 21.8 \end{array}$$

$$\begin{array}{r} 4.3 \\ 6.3 \end{array}$$

$$\begin{array}{r} 5.3 \\ \cancel{DCD} \times 1.3 \\ \hline 22.0 \end{array}$$

$$\begin{array}{r} 5.8 \\ \cancel{F.1} \\ \hline 1.7 \end{array}$$

$$\begin{array}{r} 5.8 \\ \cancel{DCD} \times 0.8 \\ \hline 22.0 \end{array}$$

$$\begin{array}{r} 4.3 \\ 6.3 \end{array}$$

$$\begin{array}{r} 5.5 \\ \cancel{DCD} \times 1.1 \\ \hline 22.6 \end{array}$$

$$\begin{array}{r} 5.9 \\ \cancel{F.1} \\ \hline 1.3 \end{array}$$

$$\begin{array}{r} 5.9 \\ \cancel{DCD} \times 0.7 \\ \hline 21.8 \end{array}$$

$$\begin{array}{r} 4.2 \\ 6.2 \end{array}$$

$$\begin{array}{r} 5.3 \\ \cancel{DCD} \times 1.3 \\ \hline 22.8 \end{array}$$

$$\begin{array}{r} 6.2 \\ \cancel{F.2} \\ \hline 1.6 \end{array}$$

$$\begin{array}{r} 5.4 \\ \cancel{DCD} \times 1.2 \\ \hline 22.4 \end{array}$$

$$\begin{array}{r} 4.8 \\ 6.8 \end{array}$$

$$\begin{array}{r} 6.6 \\ \cancel{DCD} \times 0.6 \\ \hline 21.1 \end{array}$$

$$\begin{array}{r} 7.1 \\ \cancel{F.3} \\ \hline 1.9 \end{array}$$

$$\begin{array}{r} 5.5 \\ \cancel{DCD} \times 0.7 \\ \hline 21.1 \end{array}$$

$$\begin{array}{r} 4.7 \\ 6.7 \end{array}$$

$$\begin{array}{r} 6.5 \\ \cancel{DCD} \times 0.4 \\ \hline 21.1 \end{array}$$

$$\begin{array}{r} 7.3 \\ \cancel{F.2} \\ \hline 2.7 \end{array}$$

$$\begin{array}{r} 7.0 \\ \cancel{F.2} \\ \hline 17 \end{array}$$

Sta.	+	π	-	Grade	Revised Grades
		911.70			
12+50				10.5	10.1
13				10.6	10.2
+50				10.6	10.2
14				10.7	10.3
+50				10.7	10.3
15				10.8	10.3
+50				10.8	10.3
16				10.9	10.4

LT.

ET

ET

4.7
6.7
7.1

$\frac{6.7}{DC.08}$ $\frac{0.5}{22.0}$
 ~~$\frac{F.2.8}{21.0}$~~

$\frac{7.0}{2.3}$
F.F.1.9

$\frac{6.8}{2.1}$ $\frac{0.3}{21.6}$
 ~~$\frac{F.2.1}{17.2}$~~

4.6
6.6
7.0

$\frac{6.5}{DC.08}$ $\frac{0.5}{22.0}$
 ~~$\frac{F.2.8}{21.0}$~~

$\frac{6.9}{2.3}$
F.F.1.9

$\frac{6.5}{DC.08}$ $\frac{0.5}{22.0}$
 ~~$\frac{F.2.1}{21.0}$~~

4.6
6.6
7.0

$\frac{6.0}{DC.08}$ $\frac{1.0}{23.0}$
 ~~$\frac{F.2.4}{21.0}$~~

$\frac{6.6}{2.0}$
F.F.1.6

$\frac{6.1}{DC.08}$ $\frac{0.9}{22.0}$
 ~~$\frac{F.2.0}{21.0}$~~

4.5
6.5

$\frac{5.7}{DC.08}$ $\frac{1.2}{23.4}$
 ~~$\frac{F.2.6}{21.0}$~~

$\frac{5.6}{2.1}$
F.F.1.7

$\frac{5.3}{DC.08}$ $\frac{1.6}{24.0}$
 ~~$\frac{F.2.4}{21.0}$~~

4.5
6.5

$\frac{5.7}{DC.08}$ $\frac{1.2}{23.4}$
 ~~$\frac{F.2.6}{21.0}$~~

$\frac{5.1}{2.0}$
F.F.0.2

$\frac{5.3}{DC.08}$ $\frac{1.6}{24.0}$
 ~~$\frac{F.2.4}{21.0}$~~

4.4
6.4

$\frac{5.0}{DC.08}$ $\frac{1.9}{24.8}$
 ~~$\frac{F.2.8}{21.0}$~~

$\frac{4.8}{2.0}$
F.F.0.1

$\frac{4.8}{DC.08}$ $\frac{2.1}{25.0}$
 ~~$\frac{F.2.4}{21.0}$~~

4.4
6.4

$\frac{4.9}{DC.08}$ $\frac{2.0}{25.0}$
 ~~$\frac{F.2.8}{21.0}$~~

$\frac{4.9}{2.0}$
F.F.0.0

$\frac{4.5}{DC.08}$ $\frac{2.4}{25.8}$
 ~~$\frac{F.2.4}{21.0}$~~

4.3
6.3

$\frac{5.1}{DC.08}$ $\frac{1.7}{24.4}$
 ~~$\frac{F.2.4}{21.0}$~~

$\frac{5.1}{2.0}$
F.F.0.3

$\frac{4.8}{DC.08}$ $\frac{2.0}{25.0}$
 ~~$\frac{F.2.4}{21.0}$~~

Sta	+	K	-	Grade	Revised Grades
		915.70			
16 +50				10.9	10.4
T.P.	4.22	915.70	4.22	910.98	
17				11.0	10.5
+50				11.0	10.5
18				11.1	10.5
+50				11.1	10.5
19				11.2	10.6
+50				11.3	10.6
20				11.3	10.7

$$\begin{array}{r} 4.3 \\ 6.3 \end{array}$$

$$\begin{array}{r} 5.1 \\ \text{PC} \cancel{17} \\ 23.4 \end{array} \quad \begin{array}{r} 17 \\ 24.4 \end{array}$$

$$\begin{array}{r} 5.2 \\ \text{PC} \cancel{9} \\ \text{F.O.} 4 \end{array}$$

$$\begin{array}{r} 4.8 \\ \text{PC} \cancel{17} \\ 24.0 \end{array} \quad \begin{array}{r} 2.0 \\ 21 \end{array}$$

$$\begin{array}{r} 4.2 \\ 6.2 \end{array}$$

$$\begin{array}{r} 5.4 \\ \text{PC} \cancel{17} \\ 26.6 \end{array} \quad \begin{array}{r} 13 \\ 23.6 \end{array}$$

$$\begin{array}{r} 5.2 \\ \text{PC} \cancel{9} \\ \text{F.O.} 1 \end{array}$$

$$\begin{array}{r} 5.0 \\ \text{PC} \cancel{17} \\ 23.4 \end{array} \quad \begin{array}{r} 1.7 \\ 24.4 \end{array}$$

$$\begin{array}{r} 4.2 \\ 6.2 \end{array}$$

$$\begin{array}{r} 5.7 \\ \text{PC} \cancel{17} \\ 22.0 \end{array} \quad \begin{array}{r} 1.0 \\ 23.0 \end{array}$$

$$\begin{array}{r} 4.8 \\ \text{PC} \cancel{9} \\ \text{F.O.} 1 \end{array}$$

$$\begin{array}{r} 5.0 \\ \text{PC} \cancel{17} \\ 23.4 \end{array} \quad \begin{array}{r} 1.7 \\ 24.4 \end{array}$$

$$\begin{array}{r} 4.1 \\ 6.1 \end{array}$$

$$\begin{array}{r} 5.1 \\ \text{PC} \cancel{17} \\ 24.4 \end{array} \quad \begin{array}{r} 1.6 \\ 24.4 \end{array}$$

$$\begin{array}{r} 4.9 \\ \text{PC} \cancel{9} \\ \text{F.O.} 2 \end{array}$$

$$\begin{array}{r} 5.0 \\ \text{PC} \cancel{17} \\ 22.0 \end{array} \quad \begin{array}{r} 1.7 \\ 24.4 \end{array}$$

$$\begin{array}{r} 4.1 \\ 6.1 \end{array}$$

$$\begin{array}{r} 1.6 \\ \text{PC} \cancel{17} \\ 20.0 \end{array} \quad \begin{array}{r} 1.1 \\ 23.1 \end{array}$$

$$\begin{array}{r} 5.1 \\ \text{PC} \cancel{9} \\ \text{F.O.} 4 \end{array}$$

$$\begin{array}{r} 5.2 \\ \text{PC} \cancel{17} \\ 22.0 \end{array} \quad \begin{array}{r} 1.5 \\ 24.0 \end{array}$$

$$\begin{array}{r} 4.0 \\ 6.0 \end{array}$$

$$\begin{array}{r} 5.9 \\ \text{PC} \cancel{17} \\ 21.4 \end{array} \quad \begin{array}{r} 0.7 \\ 22.4 \end{array}$$

$$\begin{array}{r} 5.4 \\ \text{PC} \cancel{9} \\ \text{F.O.} 1 \end{array}$$

$$\begin{array}{r} 5.8 \\ \text{PC} \cancel{17} \\ 21.4 \end{array} \quad \begin{array}{r} 0.8 \\ 22.6 \end{array}$$

$$\begin{array}{r} 3.9 \\ 5.9 \\ 6.6 \end{array}$$

$$\begin{array}{r} 5.8 \\ \text{PC} \cancel{17} \\ 21.4 \end{array} \quad \begin{array}{r} 0.8 \\ 22.6 \end{array}$$

$$\begin{array}{r} 5.7 \\ \text{PC} \cancel{9} \\ 1.1 \end{array}$$

$$\begin{array}{r} 6.3 \\ \text{PC} \cancel{17} \\ 11.0 \end{array} \quad \begin{array}{r} \text{PC} 0.4 \\ 21.8 \end{array}$$

$$\begin{array}{r} 3.9 \\ 5.9 \\ 6.1 \end{array}$$

$$\begin{array}{r} 5.7 \\ \text{PC} \cancel{17} \\ 21.4 \end{array} \quad \begin{array}{r} 0.8 \\ 22.6 \end{array}$$

$$\begin{array}{r} 5.1 \\ \text{PC} \cancel{9} \\ 1.0 \end{array}$$

$$\begin{array}{r} 6.2 \\ \text{PC} \cancel{17} \\ 11.0 \end{array} \quad \begin{array}{r} 0.3 \\ 21.6 \end{array}$$

Stn	+	K	-	Grade	Revised Grades
20+50		915.70		11.4	10.7
21				11.4	10.7
T.P.	4.65	915.75	4.60	910.60	
+50				11.5	10.8
22				11.5	10.8
+50				11.6	10.8
23				11.6	10.9
+50				11.7	11.0
24				11.7	11.0

LX

E

EX

6

$$\begin{array}{r} 3.8 \\ 1.8 \\ \hline 6.5 \end{array}$$

$$\begin{array}{r} 6.3 \\ 1.2 \\ \hline 1.0 \\ 21.4 \end{array}$$

$$\begin{array}{r} 6.0 \\ 1.1 \\ \hline 1.1 \end{array}$$

$$\begin{array}{r} 5.9 \\ 1.2 \\ \hline 0.7 \\ 22.4 \end{array}$$

$$\begin{array}{r} 3.8 \\ 1.8 \\ \hline \end{array}$$

$$\begin{array}{r} 5.6 \\ 0.6 \\ \hline 21.4 \\ 22.8 \end{array}$$

$$\begin{array}{r} 5.1 \\ 1.3 \\ \hline 0.6 \end{array}$$

$$\begin{array}{r} 5.1 \\ 0.7 \\ \hline 1.4 \\ 23.8 \end{array}$$

$$\begin{array}{r} 3.8 \\ 1.8 \\ \hline \end{array}$$

$$\begin{array}{r} 5.3 \\ 0.6 \\ \hline 22.0 \\ 23.4 \end{array}$$

$$\begin{array}{r} 4.8 \\ 1.0 \\ \hline 0.3 \end{array}$$

$$\begin{array}{r} 5.1 \\ 0.7 \\ \hline 1.4 \\ 23.8 \end{array}$$

$$\begin{array}{r} 3.8 \\ 1.8 \\ \hline \end{array}$$

$$\begin{array}{r} 5.2 \\ 0.6 \\ \hline 22.2 \\ 23.6 \end{array}$$

$$\begin{array}{r} 4.8 \\ 1.0 \\ \hline 0.3 \end{array}$$

$$\begin{array}{r} 5.0 \\ 0.8 \\ \hline 1.5 \\ 22.6 \\ 24.0 \end{array}$$

$$\begin{array}{r} 3.7 \\ 1.7 \\ \hline \end{array}$$

$$\begin{array}{r} 5.4 \\ 0.6 \\ \hline 21.6 \\ 23.4 \end{array}$$

$$\begin{array}{r} 5.4 \\ 1.7 \\ \hline 0.9 \end{array}$$

$$\begin{array}{r} 5.4 \\ 0.3 \\ \hline 1.1 \\ 23.4 \end{array}$$

$$\begin{array}{r} 3.7 \\ 1.7 \\ \hline 6.4 \end{array}$$

$$\begin{array}{r} 5.5 \\ 0.6 \\ \hline 21.4 \\ 23.8 \end{array}$$

$$\begin{array}{r} 6.1 \\ 1.7 \\ \hline 1.7 \end{array}$$

$$\begin{array}{r} 5.2 \\ 1.2 \\ \hline 0.3 \\ 21.6 \end{array}$$

$$\begin{array}{r} 3.6 \\ 1.6 \\ \hline 6.2 \end{array}$$

$$\begin{array}{r} 5.2 \\ 0.6 \\ \hline 21.8 \\ 23.4 \end{array}$$

$$\begin{array}{r} 5.1 \\ 1.5 \\ \hline 0.8 \end{array}$$

$$\begin{array}{r} 5.1 \\ 1.2 \\ \hline 0.7 \\ 22.4 \end{array}$$

$$\begin{array}{r} 3.6 \\ 1.6 \\ \hline \end{array}$$

$$\begin{array}{r} 4.8 \\ 0.6 \\ \hline 22.6 \\ 24.0 \end{array}$$

$$\begin{array}{r} 4.6 \\ 1.0 \\ \hline 0.3 \end{array}$$

$$\begin{array}{r} 5.4 \\ 0.6 \\ \hline 0.9 \\ 21.8 \end{array}$$

0.1476

Sta.	+	π	-	Grade	Rev. Grades
		915.75			

24+50				11.8	11.0
-------	--	--	--	------	------

25				11.8	11.0
----	--	--	--	------	------

+50				11.9	11.1
-----	--	--	--	------	------

26				11.9	11.1
----	--	--	--	------	------

+50				12.0	11.4
+65					

27				12.0	11.4
----	--	--	--	------	------

+50				12.1	11.4
-----	--	--	--	------	------

B.M.	8.68	921.43	2.50	918.75	912.75
------	------	--------	------	--------	--------

28				12.2	11.4
----	--	--	--	------	------

Lt.

E

Rt.

7

$$\begin{array}{r} 3.5 \\ 5.1 \\ \hline \end{array}$$

$$\begin{array}{r} 5.1 \\ \cancel{DC 0.4} \\ 21.8 \end{array} \quad \begin{array}{r} 1.2 \\ 23.4 \end{array}$$

$$\begin{array}{r} 4.7 \\ \cancel{F.18} \\ 0.4 \end{array}$$

$$\begin{array}{r} 5.2 \\ \cancel{DC 0.7} \\ 21.6 \end{array} \quad \begin{array}{r} 1.1 \\ 23.2 \end{array}$$

$$\begin{array}{r} 3.5 \\ 5.1 \\ \hline 6.3 \end{array}$$

$$\begin{array}{r} 5.1 \\ \cancel{F.18} \\ 10.6 \end{array} \quad \begin{array}{r} DC 0.5 \\ 22.0 \end{array}$$

$$\begin{array}{r} 5.3 \\ \cancel{F.18} \\ 1.0 \end{array}$$

$$\begin{array}{r} 5.1 \\ \cancel{F.18} \\ 10.0 \end{array} \quad \begin{array}{r} DC 0.8 \\ 22.6 \end{array}$$

$$\begin{array}{r} 3.4 \\ 5.4 \\ \hline 6.2 \end{array}$$

$$\begin{array}{r} 5.4 \\ \cancel{F.18} \\ 10.0 \end{array} \quad \begin{array}{r} DC 0.8 \\ 22.6 \end{array}$$

$$\begin{array}{r} 5.2 \\ \cancel{F.18} \\ 1.0 \end{array}$$

$$\begin{array}{r} 5.4 \\ \cancel{F.18} \\ 10.0 \end{array} \quad \begin{array}{r} DC 0.8 \\ 22.6 \end{array}$$

$$\begin{array}{r} 3.4 \\ 5.4 \\ \hline 6.2 \end{array}$$

$$\begin{array}{r} 5.2 \\ \cancel{DC 0.4} \\ 21.4 \end{array} \quad \begin{array}{r} 1.0 \\ 23.0 \end{array}$$

$$\begin{array}{r} 5.4 \\ \cancel{F.18} \\ 1.2 \end{array}$$

$$\begin{array}{r} 5.7 \\ \cancel{F.18} \\ 11.6 \end{array} \quad \begin{array}{r} DC 0.5 \\ 22.0 \end{array}$$

$$\begin{array}{r} 3.3 \\ 5.3 \\ \hline \end{array}$$

$$\begin{array}{r} 4.6 \\ \cancel{DC 0.8} \\ 20.4 \end{array} \quad \begin{array}{r} 1.5 \\ 24.0 \end{array}$$

$$\begin{array}{r} 4.4 \\ \cancel{F.18} \\ 0.2 \end{array}$$

$$\begin{array}{r} 4.7 \\ \cancel{DC 0.6} \\ 21.2 \end{array} \quad \begin{array}{r} 1.4 \\ 23.8 \end{array}$$

$$\begin{array}{r} 3.3 \\ 5.3 \\ \hline \end{array}$$

$$\begin{array}{r} 4.0 \\ \cancel{DC 0.3} \\ 20.5 \end{array} \quad \begin{array}{r} 2.1 \\ 25.2 \end{array}$$

$$\begin{array}{r} 4.0 \\ \cancel{F.18} \\ 6.0 \end{array}$$

$$\begin{array}{r} 4.1 \\ \cancel{DC 0.7} \\ 23.4 \end{array} \quad \begin{array}{r} 2.0 \\ 25.0 \end{array}$$

$$\begin{array}{r} 3.2 \\ 5.2 \\ \hline \end{array}$$

$$\begin{array}{r} 3.8 \\ \cancel{DC 0.8} \\ 20.8 \end{array} \quad \begin{array}{r} 2.3 \\ 21.6 \end{array}$$

$$\begin{array}{r} 3.8 \\ \cancel{F.18} \\ 0.3 \end{array}$$

$$\begin{array}{r} 4.0 \\ \cancel{DC 0.4} \\ 21.2 \end{array} \quad \begin{array}{r} 2.1 \\ 25.2 \end{array}$$

Top of Elec. Conduit N.W. Cor. of No. 80' Rt 27+80

$$\begin{array}{r} 9.2 \\ 11.2 \\ \hline \end{array}$$

$$\begin{array}{r} 9.8 \\ \cancel{DC 1.8} \\ 20.8 \end{array} \quad \begin{array}{r} 2.2 \\ 25.2 \end{array}$$

$$\begin{array}{r} 9.3 \\ \cancel{F.18} \\ 6.0 \end{array}$$

$$\begin{array}{r} 10.1 \\ \cancel{DC 1.1} \\ 20.1 \end{array} \quad \begin{array}{r} 1.9 \\ 24.8 \end{array}$$

Sta.	+	X	-	Grade	Rev. Grades
		921.43			
28+50				12.5	11.8
29				12.8	12.8
+50				13.3	12.7
30				13.9	13.3
+50				14.7	14.1
31				15.5	14.9
+50				16.3	15.8
32				17.2	16.7

4

E

B

8

8.9
10.9
$$\begin{array}{r} 96 \\ \cancel{26.1} \times 2.0 \\ \hline 21.0 \end{array}$$

$$\begin{array}{r} 92 \\ \cancel{20.3} \times 6.04 \\ \hline \end{array}$$

$$\begin{array}{r} 98 \\ \cancel{20.1} \times 18 \\ \hline 24.6 \end{array}$$
8.6
10.6
$$\begin{array}{r} 93 \\ \cancel{26.1} \times 19 \\ \hline 24.8 \end{array}$$

$$\begin{array}{r} 87 \\ \cancel{20.3} \times 6.05 \\ \hline \end{array}$$

$$\begin{array}{r} 95 \\ \cancel{20.1} \times 17 \\ \hline 24.4 \end{array}$$
8.1
10.1
$$\begin{array}{r} 90 \\ \cancel{26.1} \times 17 \\ \hline 24.4 \end{array}$$

$$\begin{array}{r} 86 \\ \cancel{20.3} \times 6.01 \\ \hline \end{array}$$

$$\begin{array}{r} 93 \\ \cancel{20.8} \times 1.4 \\ \hline 23.8 \end{array}$$
7.5
9.5
$$\begin{array}{r} 86 \\ \cancel{20.8} \times 15 \\ \hline 24.0 \end{array}$$

$$\begin{array}{r} 81 \\ \cancel{20.3} \times 6.00 \\ \hline \end{array}$$

$$\begin{array}{r} 88 \\ \cancel{20.4} \times 13 \\ \hline 23.6 \end{array}$$
6.7
8.7
$$\begin{array}{r} 80 \\ \cancel{26.1} \times 13 \\ \hline 23.6 \end{array}$$

$$\begin{array}{r} 74 \\ \cancel{20.3} \times 6.01 \\ \hline \end{array}$$

$$\begin{array}{r} 73 \\ \cancel{20.1} \times 18 \\ \hline 24.6 \end{array}$$
5.9
7.9
$$\begin{array}{r} 78 \\ \cancel{26.1} \times 6.7 \\ \hline 22.4 \end{array}$$

$$\begin{array}{r} 65 \\ \cancel{20.3} \times 6.00 \\ \hline \end{array}$$

$$\begin{array}{r} 67 \\ \cancel{20.1} \times 16 \\ \hline 24.2 \end{array}$$
5.1
7.1
$$\begin{array}{r} 67 \\ \cancel{26.1} \times 11 \\ \hline 23.2 \end{array}$$

$$\begin{array}{r} 55 \\ \cancel{20.3} \times 6.01 \\ \hline \end{array}$$

$$\begin{array}{r} 57 \\ \cancel{20.1} \times 17 \\ \hline 24.4 \end{array}$$
4.2
6.2
$$\begin{array}{r} 58 \\ \cancel{26.1} \times 5 \\ \hline 22.0 \end{array}$$

$$\begin{array}{r} 43 \\ \cancel{20.3} \times 6.04 \\ \hline \end{array}$$

$$\begin{array}{r} 47 \\ \cancel{20.1} \times 21 \\ \hline 25.2 \end{array}$$

Sta.	+	π	-	Grade	Per. Grades
		921.43			
32+50				18.0	17.6
33				18.8	18.5
+50				19.6	19.3
34				20.4	20.2
T.P.	6.67	927.10	0.60	990.83	
+50				21.0	20.8
35				21.6	21.5
+50				21.9	21.9
36				22.2	22.2

LH.

E

RH.

9

$$\begin{array}{r} 34 \\ 1.4 \end{array}$$

$$\begin{array}{r} 41 \\ \cancel{DC 18} \\ 24.6 \end{array} \quad \begin{array}{r} 17 \\ 24.4 \end{array}$$

$$\begin{array}{r} 34 \\ \cancel{100} \\ 60.4 \end{array}$$

$$\begin{array}{r} 36 \\ \cancel{DC 18} \\ 24.6 \end{array} \quad \begin{array}{r} 22 \\ 25.4 \end{array}$$

$$\begin{array}{r} 2.6 \\ 4.6 \end{array}$$

$$\begin{array}{r} 32 \\ \cancel{DC 18} \\ 24.6 \end{array} \quad \begin{array}{r} 17 \\ 24.4 \end{array}$$

$$\begin{array}{r} 26 \\ \cancel{100} \\ 60.3 \end{array}$$

$$\begin{array}{r} 30 \\ \cancel{DC 18} \\ 24.2 \end{array} \quad \begin{array}{r} 19 \\ 24.8 \end{array}$$

$$\begin{array}{r} 1.8 \\ 3.8 \end{array}$$

$$\begin{array}{r} 28 \\ \cancel{DC 18} \\ 24.6 \end{array} \quad \begin{array}{r} 13 \\ 23.6 \end{array}$$

$$\begin{array}{r} 22 \\ \cancel{100} \\ 60.1 \end{array}$$

$$\begin{array}{r} 24 \\ \cancel{DC 18} \\ 24.8 \end{array} \quad \begin{array}{r} 17 \\ 24.4 \end{array}$$

$$\begin{array}{r} 1.0 \\ 3.0 \end{array}$$

$$\begin{array}{r} 11 \\ \cancel{DC 18} \\ 24.6 \end{array} \quad \begin{array}{r} 17 \\ 24.4 \end{array}$$

$$\begin{array}{r} 12 \\ \cancel{100} \\ 60.0 \end{array}$$

$$\begin{array}{r} 14 \\ \cancel{DC 18} \\ 24.2 \end{array} \quad \begin{array}{r} 18 \\ 24.6 \end{array}$$

$$\begin{array}{r} 6.5 \\ 8.5 \end{array}$$

$$\begin{array}{r} 67 \\ \cancel{DC 18} \\ 24.6 \end{array} \quad \begin{array}{r} 20 \\ 25.0 \end{array}$$

$$\begin{array}{r} 61 \\ \cancel{100} \\ 60.9 \end{array}$$

$$\begin{array}{r} 63 \\ \cancel{DC 18} \\ 24.4 \end{array} \quad \begin{array}{r} 24 \\ 25.8 \end{array}$$

$$\begin{array}{r} 5.9 \\ 7.9 \end{array}$$

$$\begin{array}{r} 61 \\ \cancel{DC 18} \\ 24.6 \end{array} \quad \begin{array}{r} 17 \\ 24.8 \end{array}$$

$$\begin{array}{r} 54 \\ \cancel{100} \\ 60.6 \end{array}$$

$$\begin{array}{r} 62 \\ \cancel{DC 18} \\ 24.4 \end{array} \quad \begin{array}{r} 18 \\ 24.6 \end{array}$$

$$\begin{array}{r} 5.6 \\ 7.6 \end{array}$$

$$\begin{array}{r} 18 \\ \cancel{DC 18} \\ 24.6 \end{array}$$

$$\begin{array}{r} 49 \\ \cancel{100} \\ 60.7 \end{array}$$

$$\begin{array}{r} 55 \\ \cancel{DC 21} \\ 25.2 \end{array}$$

$$\begin{array}{r} 5.3 \\ 7.3 \end{array}$$

$$\begin{array}{r} 15 \\ \cancel{DC 18} \\ 24.6 \end{array}$$

$$\begin{array}{r} 48 \\ \cancel{100} \\ 60.5 \end{array}$$

$$\begin{array}{r} 16 \\ \cancel{DC 17} \\ 24.4 \end{array}$$

Sta.	+	π	-	Grade
		927.50		

36+50				22.4
-------	--	--	--	------

37				22.5
----	--	--	--	------

+50				22.6
-----	--	--	--	------

38				22.7
----	--	--	--	------

+50				22.8
-----	--	--	--	------

T.P.	643	928.44	5.49	927.01
------	-----	--------	------	--------

39				22.9
----	--	--	--	------

+50				23.0
-----	--	--	--	------

40				23.1
----	--	--	--	------

Lt.

E

Rt.

10

$$\begin{array}{r} 5.1 \\ 7.1 \end{array}$$

$$\begin{array}{r} 5.7 \\ 0.614 \\ \hline 23.8 \end{array}$$

$$\begin{array}{r} 4.9 \\ 60.2 \end{array}$$

$$\begin{array}{r} 5.6 \\ 0.615 \\ \hline 24.0 \end{array}$$

$$\begin{array}{r} 5.0 \\ 7.0 \end{array}$$

$$\begin{array}{r} 5.9 \\ 0.611 \\ \hline 23.2 \end{array}$$

$$\begin{array}{r} 5.1 \\ 60.1 \end{array}$$

$$\begin{array}{r} 5.6 \\ 0.614 \\ \hline 23.8 \end{array}$$

$$\begin{array}{r} 4.9 \\ 6.9 \end{array}$$

$$\begin{array}{r} 5.9 \\ 0.610 \\ \hline 23.0 \end{array}$$

$$\begin{array}{r} 5.3 \\ 60.4 \end{array}$$

$$\begin{array}{r} 6.1 \\ 0.608 \\ \hline 22.6 \end{array}$$

$$\begin{array}{r} 4.8 \\ 6.8 \end{array}$$

$$\begin{array}{r} 6.2 \\ 0.606 \\ \hline 22.2 \end{array}$$

$$\begin{array}{r} 5.5 \\ 60.7 \end{array}$$

$$\begin{array}{r} 5.9 \\ 0.609 \\ \hline 22.8 \end{array}$$

$$\begin{array}{r} 4.7 \\ 6.7 \end{array}$$

$$\begin{array}{r} 5.9 \\ 0.608 \\ \hline 22.6 \end{array}$$

$$\begin{array}{r} 5.4 \\ 60.7 \end{array}$$

$$\begin{array}{r} 5.9 \\ 0.608 \\ \hline 22.6 \end{array}$$

$$\begin{array}{r} 5.5 \\ 7.5 \end{array}$$

$$\begin{array}{r} 7.1 \\ 0.604 \\ \hline 21.8 \end{array}$$

$$\begin{array}{r} 6.5 \\ 61.0 \end{array}$$

$$\begin{array}{r} 7.0 \\ 0.605 \\ \hline 22.0 \end{array}$$

$$\begin{array}{r} 5.4 \\ 7.4 \end{array}$$

$$\begin{array}{r} 7.2 \\ 0.602 \\ \hline 21.4 \end{array}$$

$$\begin{array}{r} 6.3 \\ 60.9 \end{array}$$

$$\begin{array}{r} 6.5 \\ 0.609 \\ \hline 22.8 \end{array}$$

$$\begin{array}{r} 5.3 \\ 7.3 \end{array}$$

$$\begin{array}{r} 7.1 \\ 0.602 \\ \hline 21.4 \end{array}$$

$$\begin{array}{r} 6.3 \\ 61.0 \end{array}$$

$$\begin{array}{r} 6.6 \\ 0.607 \\ \hline 22.4 \end{array}$$

Sta. + π - Grade

978.44

40+50

23.2

41

23.3

+50

23.4

42

23.5

+50

23.6

43

23.7

+50

23.8

44

23.9

4.

E

Et.

11

5.2
7.2
$$\begin{array}{r} 20 \\ DC0.2 \\ \hline 21.4 \end{array}$$

$$\begin{array}{r} 61 \\ \hline F.O.9 \end{array}$$

$$\begin{array}{r} 6.3 \\ DC0.9 \\ \hline 22.8 \end{array}$$
5.1
7.1
$$\begin{array}{r} 68 \\ DC0.3 \\ \hline 21.4 \end{array}$$

$$\begin{array}{r} 59 \\ \hline F.O.8 \end{array}$$

$$\begin{array}{r} 6.3 \\ DC0.8 \\ \hline 22.6 \end{array}$$
5.0
7.0
$$\begin{array}{r} 67 \\ DC0.3 \\ \hline 21.6 \end{array}$$

$$\begin{array}{r} 56 \\ \hline F.O.6 \end{array}$$

$$\begin{array}{r} 58 \\ DC1.2 \\ \hline 23.4 \end{array}$$
4.9
6.9
$$\begin{array}{r} 65 \\ DC0.4 \\ \hline 21.8 \end{array}$$

$$\begin{array}{r} 52 \\ \hline F.O.3 \end{array}$$

$$\begin{array}{r} 56 \\ DC1.3 \\ \hline 23.6 \end{array}$$
4.8
6.8
$$\begin{array}{r} 58 \\ DC1.8 \\ \hline 22.0 \end{array}$$

$$\begin{array}{r} 49 \\ \hline F.O.1 \end{array}$$

$$\begin{array}{r} 56 \\ DC1.2 \\ \hline 22.4 \end{array}$$
4.7
6.7
$$\begin{array}{r} 53 \\ DC1.4 \\ \hline 22.8 \end{array}$$

$$\begin{array}{r} 51 \\ \hline F.O.4 \end{array}$$

$$\begin{array}{r} 56 \\ DC1.1 \\ \hline 22.2 \end{array}$$
4.6
6.6
$$\begin{array}{r} 57 \\ DC0.4 \\ \hline 22.2 \end{array}$$

$$\begin{array}{r} 52 \\ \hline F.O.6 \end{array}$$

$$\begin{array}{r} 60 \\ DC0.6 \\ \hline 22.2 \end{array}$$
4.5
6.5
$$\begin{array}{r} 64 \\ DC0.1 \\ \hline 21.2 \end{array}$$

$$\begin{array}{r} 54 \\ \hline F.O.9 \end{array}$$

$$\begin{array}{r} 60 \\ DC0.5 \\ \hline 22.0 \end{array}$$

Sta.	+	K	-	Grade
		928.44		

44+50				24.0
-------	--	--	--	------

T.P.	5.44	928.20	5.16	923.98
------	------	--------	------	--------

45				24.1
----	--	--	--	------

+50				24.2
-----	--	--	--	------

46				24.3
----	--	--	--	------

+50				24.4
-----	--	--	--	------

B.M.			6.69	922.01	922.01
------	--	--	------	--------	--------

B.M.	4.49	928.81	8.1	924.32	
------	------	--------	-----	--------	--

47				24.5
----	--	--	--	------

+50				24.5
-----	--	--	--	------

48				24.5
----	--	--	--	------

+50				24.5
-----	--	--	--	------

4.

5

6.

4.3
6.3

$\frac{38}{DC.21}$
26.0

$\frac{39}{CO.4}$

$\frac{28}{DC.35}$
28.0

4.3
6.3

$\frac{35}{DC.28}$
26.6

$\frac{36}{CO.7}$

$\frac{28}{DC.35}$
28.0

4.3
6.3

$\frac{37}{DC.26}$
26.2

$\frac{42}{CO.1}$

$\frac{39}{DC.24}$
25.8

4.3
6.3

$\frac{48}{DC.15}$
24.0

$\frac{51}{CO.8}$

$\frac{47}{DC.16}$
24.2

Sta.	+	π	-	Elev.
------	---	-------	---	-------

1		578.81		
---	--	--------	--	--

49				24.5
----	--	--	--	------

+50				24.5
-----	--	--	--	------

50				24.4
----	--	--	--	------

+50				24.4
-----	--	--	--	------

51				24.3
----	--	--	--	------

+50				24.2
-----	--	--	--	------

+92 ⁸⁸				24.1
-------------------	--	--	--	------

Lt.

L

Lt.

4.3
6.3

$$\begin{array}{r} 5.0 \\ DC1.3 \\ \hline 23.6 \end{array}$$

$$\begin{array}{r} 5.5 \\ F1.7 \\ \hline \end{array}$$

$$\begin{array}{r} 5.3 \\ DC1.0 \\ \hline 23.0 \end{array}$$

4.3
6.3

$$\begin{array}{r} 5.2 \\ DC1.1 \\ \hline 23.2 \end{array}$$

$$\begin{array}{r} 5.4 \\ F1.1 \\ \hline \end{array}$$

$$\begin{array}{r} 5.5 \\ DC0.8 \\ \hline 22.6 \end{array}$$

4.4
6.4

$$\begin{array}{r} 5.1 \\ DC1.3 \\ \hline 23.6 \end{array}$$

$$\begin{array}{r} 4.9 \\ F0.5 \\ \hline \end{array}$$

$$\begin{array}{r} 5.5 \\ DC0.9 \\ \hline 22.8 \end{array}$$

4.4
6.4

$$\begin{array}{r} 5.4 \\ DC1.0 \\ \hline 23.0 \end{array}$$

$$\begin{array}{r} 5.2 \\ F0.8 \\ \hline \end{array}$$

$$\begin{array}{r} 5.5 \\ DC0.9 \\ \hline 22.8 \end{array}$$

4.5
6.5

$$\begin{array}{r} 5.1 \\ DC1.4 \\ \hline 23.8 \end{array}$$

$$\begin{array}{r} 4.9 \\ F0.4 \\ \hline \end{array}$$

$$\begin{array}{r} 5.2 \\ DC1.3 \\ \hline 23.6 \end{array}$$

4.6
6.6

$$\begin{array}{r} 4.8 \\ DC1.8 \\ \hline 24.6 \end{array}$$

$$\begin{array}{r} 4.6 \\ F0.0 \\ \hline \end{array}$$

$$\begin{array}{r} 4.9 \\ DC1.7 \\ \hline 24.4 \end{array}$$

4.7
6.7

Sta.

+

⌞

-

Elev.

4.

8

8+

12

4.4
6.4

55
DC09
22.8

51
F.O.7

56
DC08
22.6

4.6
6.6

61
DC0.5
22.0

54
F.O.8

58
DC08
22.6

4.5
6.5

56
DC0.9
22.8

51
F.O.6

56
DC0.9
22.8

4.4
6.4

46
DC18
24.6

47
F.O.3

47
DC1.7
24.4

4.3
6.3

38
DC2.5
26.0

40
F.O.3

31
DC2.5
27.4

Spike in P.P. 90' 6139+80

Sta.	+	-	Grade
B.M.	12.71	915.35	902.64
0+00			
0+21			03.0
0+50			04.3
0+80			05.8
1			06.8
+16			07.6
+37.6			08.4
+40			08.5
+56			09.1

McClamp Tox sends us out to
 test stakes as desired
 by property owner.

✓

4.

8

13

13

$$\frac{DC.12.1}{57.3}$$

$$\frac{14.3}{14.3}$$

$$\frac{12.3}{600}$$

$$\frac{1.4}{DC.12.9} \quad \frac{DC.12.4}{58.2}$$

$$\frac{11.0}{13.0}$$

$$\frac{9.5}{C.1.5}$$

$$\frac{DC.11.6}{55.8} \quad \frac{1.7}{DC.11.5} \quad \frac{58.0}{58.0}$$

$$\frac{9.5}{11.5} \quad \text{2 to 1} \quad \frac{8.2}{DC.3.3} \quad \frac{27.6}{27.6}$$

$$\frac{6.7}{C.2.8}$$

$$\frac{DC.10.7}{52.7} \quad \frac{1.7}{DC.10.8} \quad \frac{51.7}{51.7}$$

14 to 1
plan

$$\frac{8.5}{10.5} \quad \frac{1.4}{1.4} \quad \frac{4.0}{DC.6.5} \quad \frac{30.7}{30.7}$$

$$\frac{5.2}{C.3.3}$$

$$\frac{1.7}{DC.10.8} \quad \frac{34.2}{34.2} \quad \frac{DC.9.1.4}{48.3}$$

$$\frac{7.7}{9.7} \quad \text{By Crampton, 1, 1} \quad \frac{DC.8.6}{27.7} \quad \frac{27.7}{27.7}$$

$$\frac{4.4}{C.3.3}$$

$$\frac{2.7}{DC.7.0} \quad \frac{31.5}{31.5}$$

$$\frac{7.0}{9.0}$$

$$\frac{1.9}{DC.7.1} \quad \frac{35.2}{35.2}$$

OK by Harbor

$$\frac{2.0}{DC.7.0} = \text{2 to 1 By Crampton} \quad \frac{35}{35}$$

x

$$\frac{6.3}{8.3}$$

$$\frac{2.0}{P.L. 6.3} \quad \frac{33.7}{33.7}$$

$$\frac{2.0}{C.4.3}$$

$$\frac{1.4}{DC.6.9} \quad \text{2 to 1 By Crampton} \quad \frac{34.8}{34.8}$$

Sta	+	π	-	Elev
-----	---	-------	---	------

		915.35		
--	--	--------	--	--

+62				09.3
-----	--	--	--	------

2				10.4
---	--	--	--	------

T.P.	4.51	919.17	0.69	914.66
------	------	--------	------	--------

+50				11.0
-----	--	--	--	------

3				11.2
---	--	--	--	------

+50				10.9
-----	--	--	--	------

4				10.6
---	--	--	--	------

+50				10.3
-----	--	--	--	------

5x00				10.0
------	--	--	--	------

27.

2

27.

14

6.1
8.1

X

5.0
7.0

1.7
DC 5.3
31.6

1.3
3.7

1.2 2 to 1
DC 5.8
32.6

8.2
10.2

5.5
DC 4.7
30.4

5.2
C.3.0

5.6
DC 4.6
30.2

8.0
10.0

5.2
DC 4.8
30.6

5.0
C.3.0

6.0
DC 4.0
29.0

8.3
10.3

5.7
DC 4.6
30.2

6.1
C.2.2

7.3
DC 3.0
27.0

8.6
10.6

7.0
DC 6.3
28.2

7.7
C.0.9

8.1
DC 2.5
26.0

8.9
10.9

8.7
DC 2.2
25.4

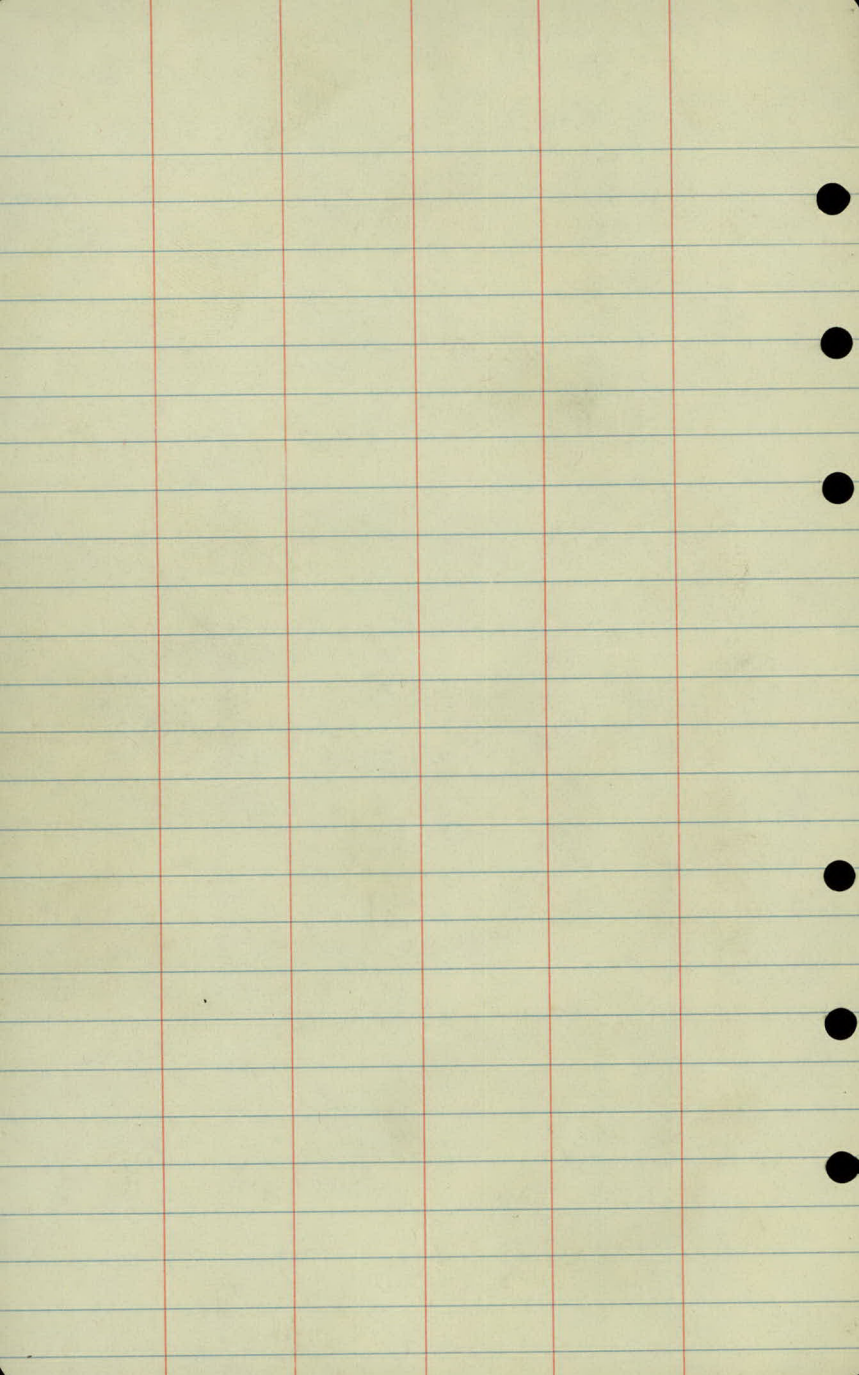
8.5
C.0.4

8.9
DC 2.0
25.0

9.2

9.2
C.0.0 10K

See Fig 5



Angle

Defl.

15

Sta. Point Lt. Rt.

1+64.37

P.T.

27°36'

Correction
95

+60

25°47'

0.83°36'

T. 39.41

+50

21°36'

L. 66.03

+40

17°25'

1+37.55

P.I.

55°14'

+30

13°14'

+20

9°04'

+10

4°33'

1

0°42'

0+88.34

P.C.

Grade
off
Parcment

0-34

18.9

14.9

5.0

9.9

48.5

0-84

10.7

12.7

5.0

D.C. 7.7

48.5

0-139

8.5

10.5

5.4

D.C. 5.1

48.5

0-188

7.2

9.2

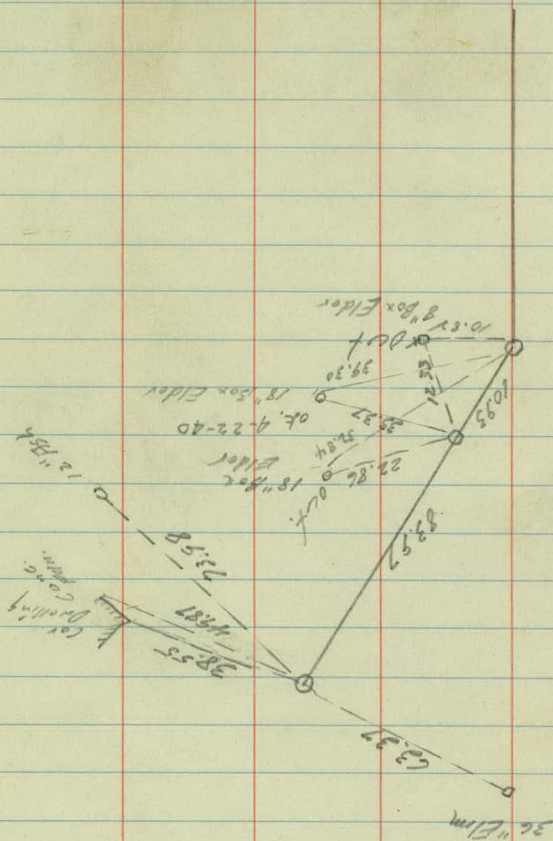
5.9

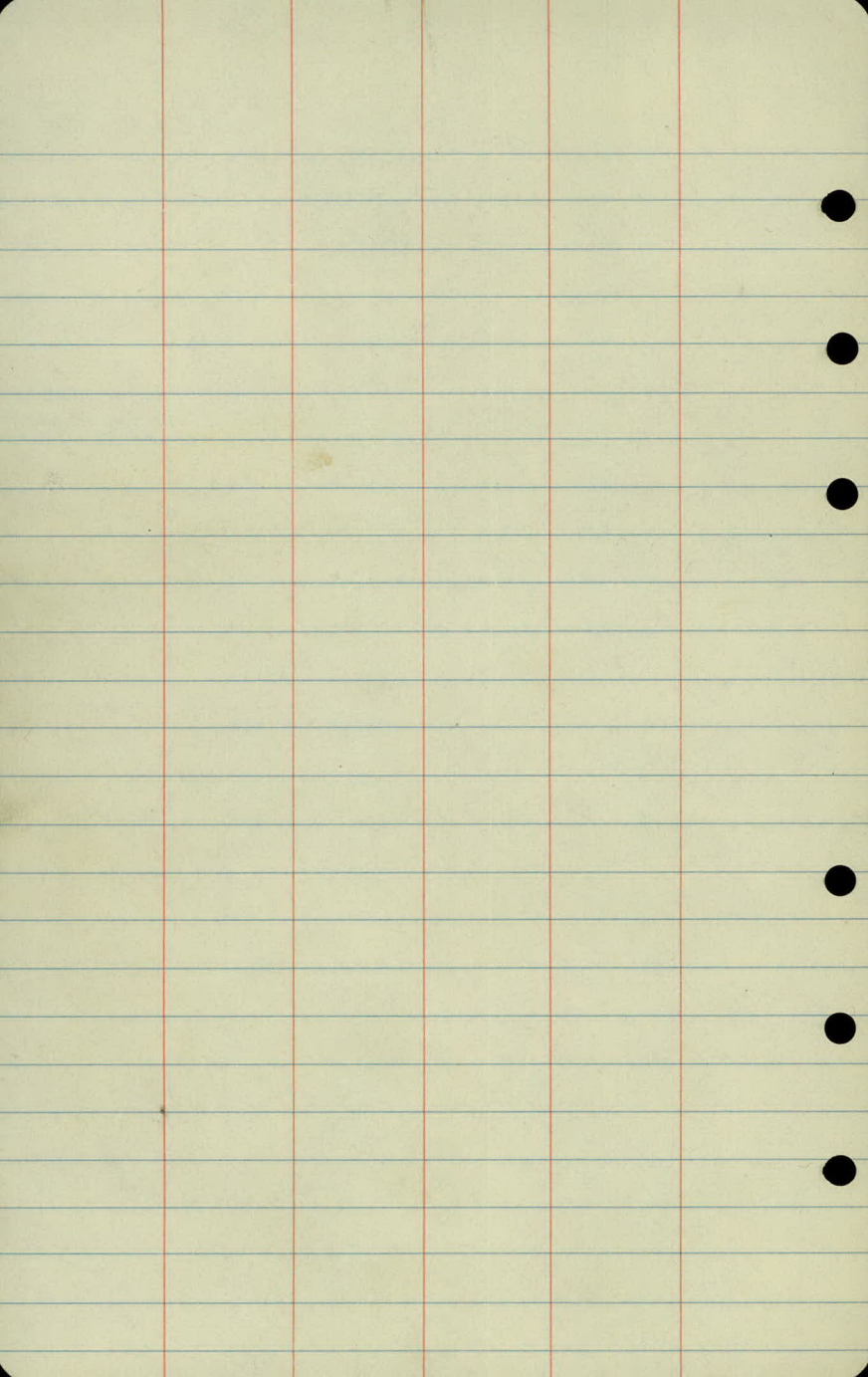
D.C. 3.3

48.5

Edgerton St. Home P. 1. South.
Mr. Compton sent us out to set
these stakes as decided by
property owner.

16





Grade $D = 83^{\circ}36'$ $\Delta = 55^{\circ}12'$

1+44.37 P.T.

06.6

 $T = 39.21$ $L = 66.03$

+40

+30

1+20

05.5

1+17.55 P.I.

+10

+00

04.7

0+90

0+80

0+78.34 P.C.

03.8

North

Lot Iron

78.14 x Elm

54.53

Line to Irons
Munn's Property

67.98 x Hub

Lot Iron

58.30

x Hub

Mississippi St.
Grade Plugs.

Sta.	+	K	-	Elev.
B.M.	11.01	913.65		902.64

0+21				03.0
------	--	--	--	------

+50				04.3
-----	--	--	--	------

+80				05.8
-----	--	--	--	------

1				06.8
---	--	--	--	------

+16				07.6
-----	--	--	--	------

+37.6				08.4
-------	--	--	--	------

+56				09.1
-----	--	--	--	------

2				10.4
---	--	--	--	------

+50				11.0
-----	--	--	--	------

3				11.2
---	--	--	--	------

Lt.

E

Rt.

10.7

✓

$$\begin{array}{r} B.T. \\ 9.9 \\ \hline C.1.7 \end{array}$$

9.4

✓

7.9

✓

6.9

✓

$$\begin{array}{r} B.T. \\ 5.4 \\ \hline C.1.5 \end{array}$$

6.1

✓

5.3

✓

$$\begin{array}{r} B.T. \\ 3.6 \\ \hline C.1.7 \end{array}$$

4.6

✓

$$\begin{array}{r} B.T. \\ 4.0 \\ \hline C.0.6 \end{array}$$

3.3

✓

2.7

✓

2.5

Sta.

+

π

-

Elev.

Lt.

£

Rt.

20

Mississippi St.

Clean ditch from culvert
at Sta. 5450 North to Main ditch
at Sta. 7422

Grade
Rod.

Sta.

+

K

-

0+00

7.0

+50

7.26

1

7.52

+50

7.79

2

8.05

+50

8.31

3

8.57

+50

8.83

3+84

9.0

3+98

9.1

4

9.1

+50

9.36

5

9.61

+50

9.87

6

10.12

+50

10.38

7

10.63

+50

10.89

+72

11.0

Rod.
Reading Cut
from
Blue Top.

F.L. Rd Culvert Miss. St.

7.0 00

6.12 C 1.14

6.47 C 1.05

6.37 C 1.42

6.31 C 1.94

6.40 C 1.91

6.86 C 1.71

6.38 C 2.45

Al. Line Culvert

9.0

Al. Line Culvert

9.1

7.04 C 2.06

7.50 C 1.86

7.70 C 1.91

8.16 C 1.71

8.57 C 1.55

8.55 C 1.83

8.30 C 2.33

9.40 C 1.49

11.0 C 0.0

Sta.

+

π

-

Elev.

W. B. Twp

Mississippi St.

Plan survey from
Edgerton St. to Labor Road.

9/38

White Bear Township.

Angle

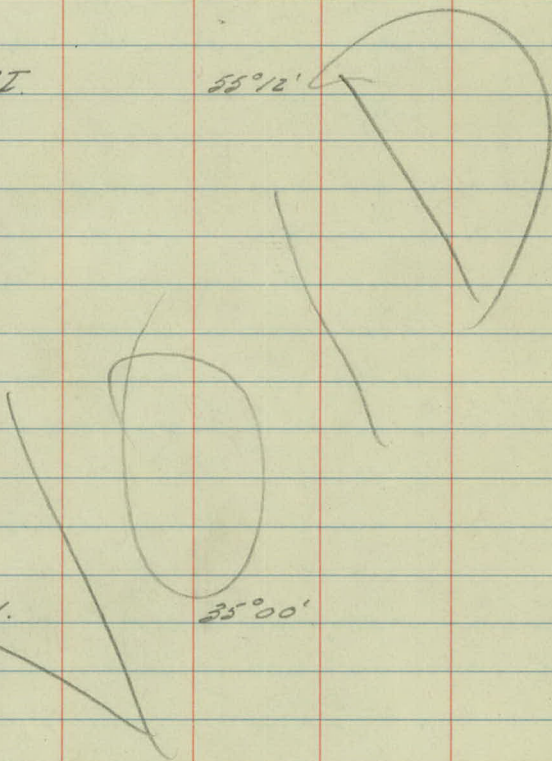
Sta.	Point	Lt.	Rt.
------	-------	-----	-----

1+17.55	P.I.		
---------	------	--	--

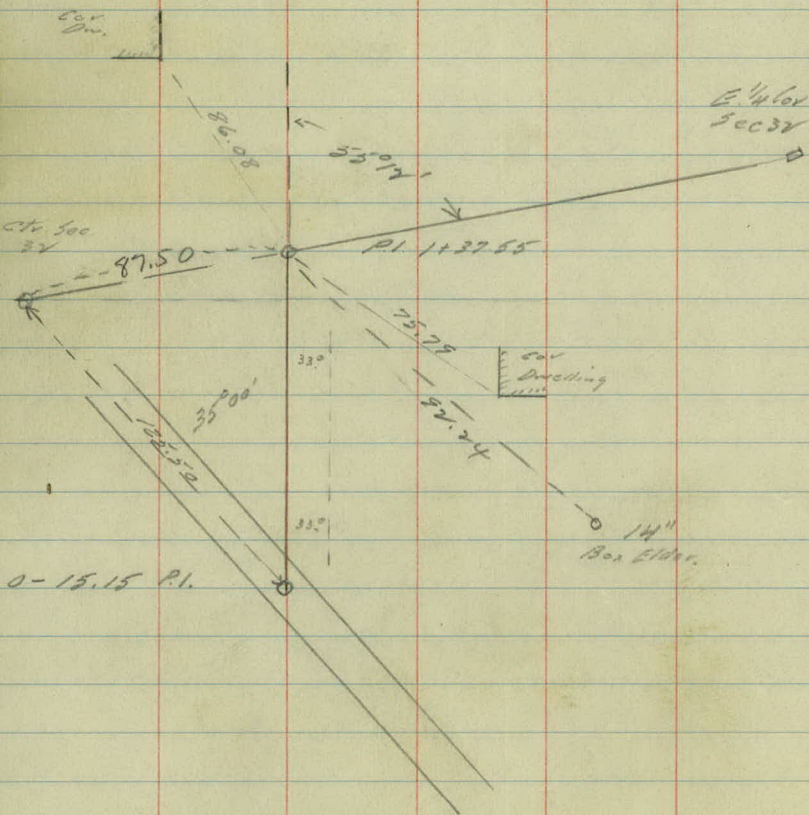
55°12'

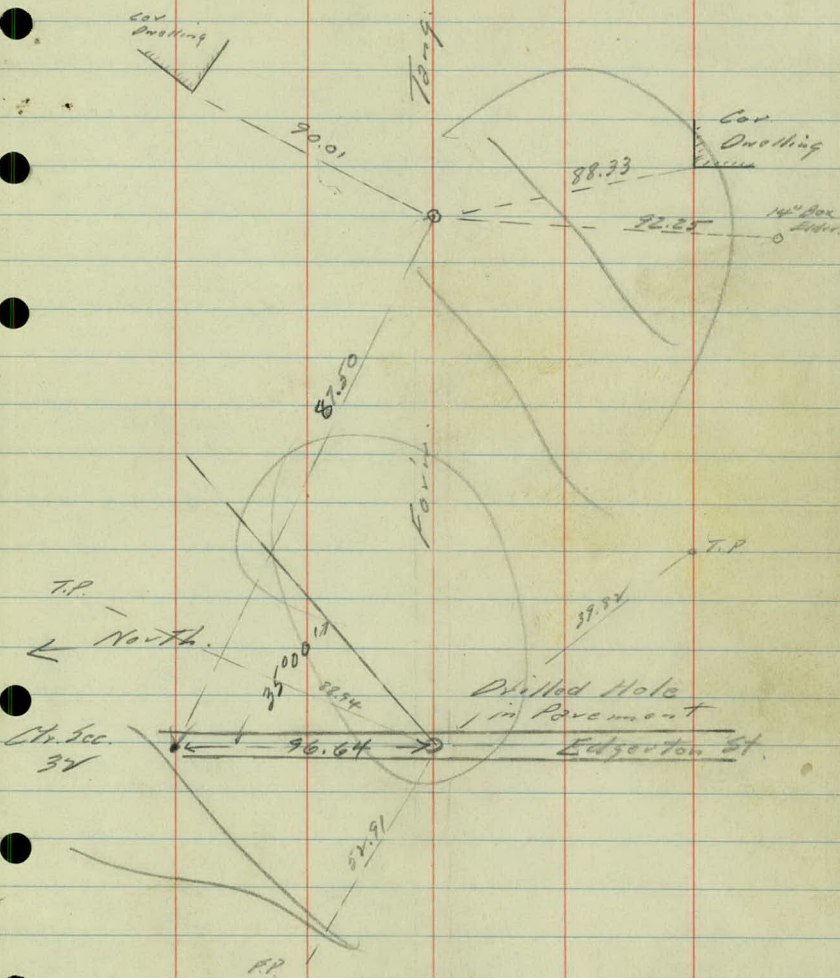
0+00	P.I.		
------	------	--	--

35°00'



Mississippi St.





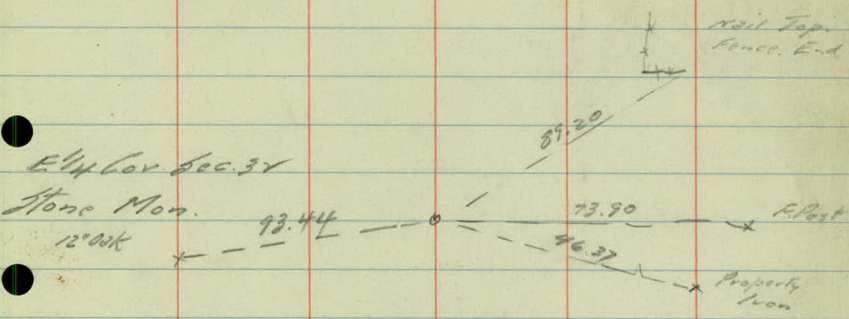
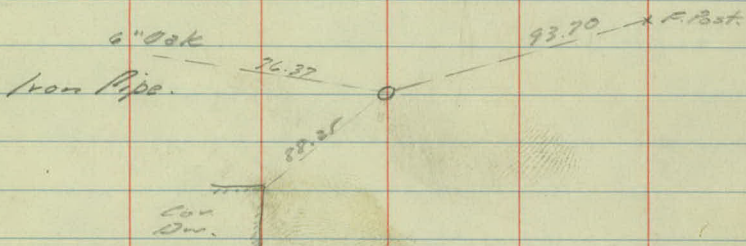
Angle

Sta	Point	Lt.	Rt.
-----	-------	-----	-----

46+68.50	P.O.T.		
----------	--------	--	--

26+62.70			
----------	--	--	--

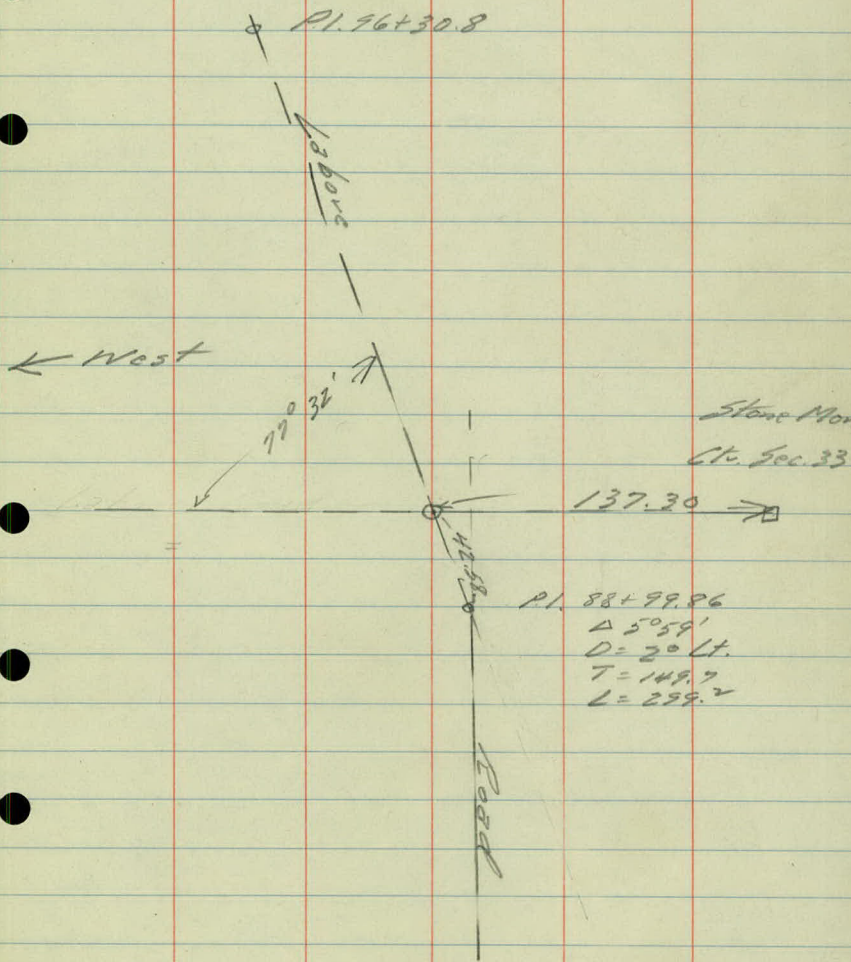
		0° 8' 30"	
--	--	-----------	--

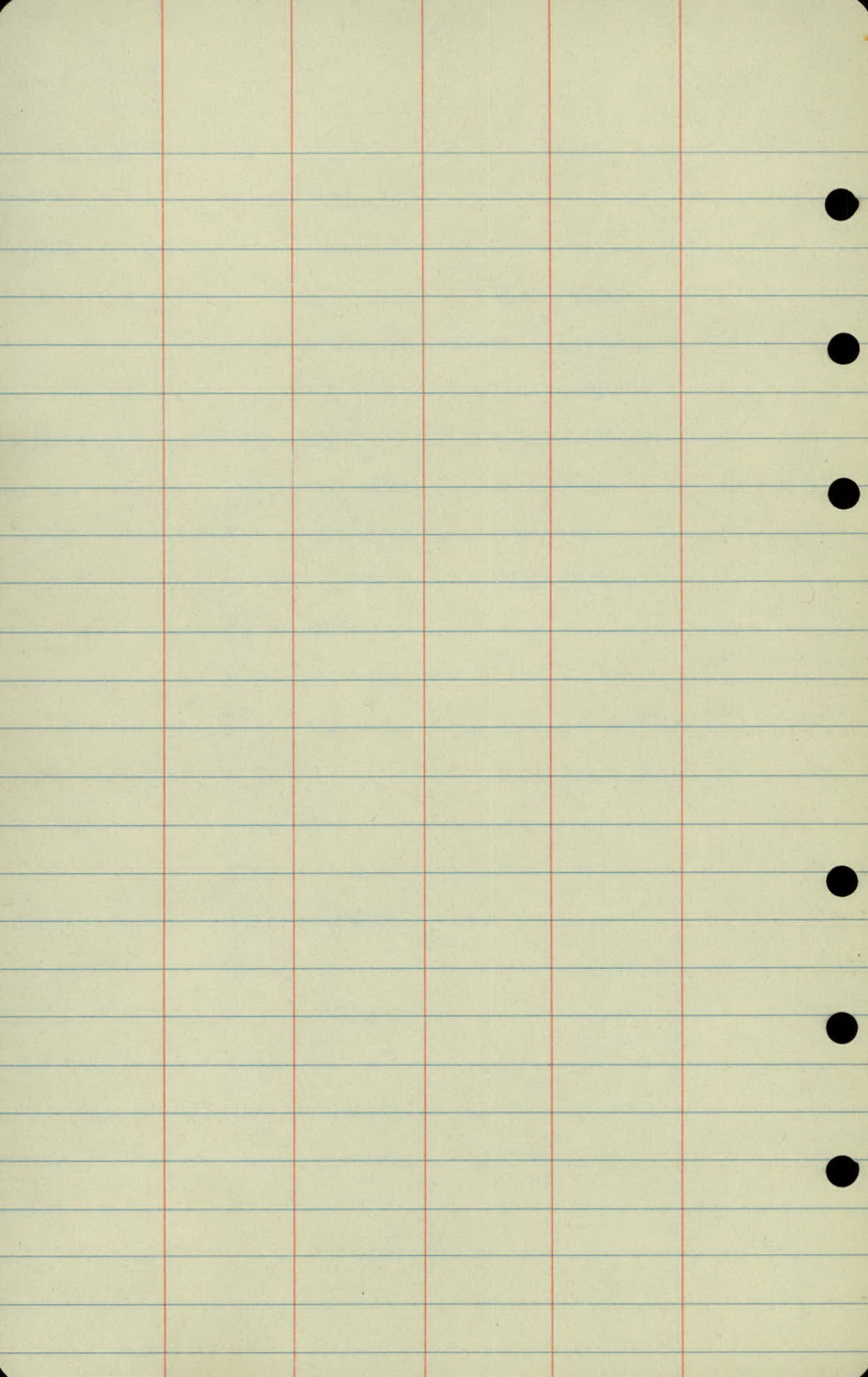


Angle.

[illegible]

51 + 9288 P.I.





Topography 9/38

2+00

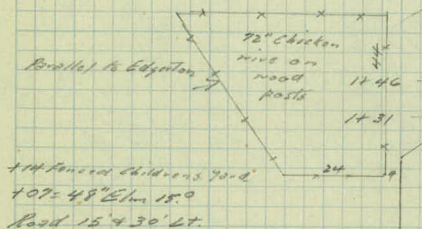
1+00

0+00

Farm yard

+86 = 30" Stump on E
+80 = 36" Stump on E

Orchard
40' Lt.



Farm yard
to yard

30°

O+82 = 12" x 24" C.M.

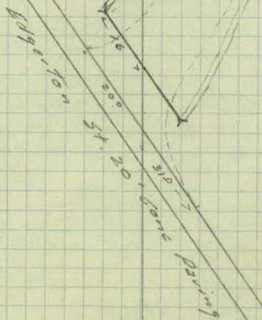
+56 T.P. 29

+63 End Bubble Gutter 9' Lt.
{ 4' Top
3' Bottom
O+50 Road 8' x 26' Lt.

+50 End Bubble Gutter 28°
{ 2' Top
2' Bottom

O+26 = 15" x 47' V.T.P.

+35 P.P. 40°



7

6

5

4

3

2

FC 33.0

7

Cultivated

Fish

Cultivated

5470 - Shallow Ditch

5454

FC 33.0

FC 33.0

+20 = 4" Apple Tree 26°
+400 = 6" Apple Tree 26°

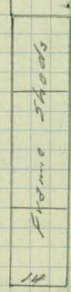
Wagon

35

3480

+81 = 4" Apple Tree 22°

Orchard 40' - 1



30

5419

Back

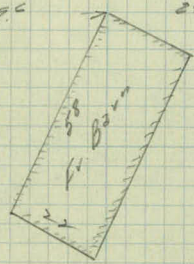
+75 Reg. FC 000

496

2484

2433 Bover

21.4



14

13

12

11

10

9

8

7

33.0 1414 8

170 = 30" Stump. on E

12405 Shallow

Cultivated

Ditch

E Rt.

Post-6

33.0

Timber

33.0

101202

33.0

14504

Cultivated

33.0

Cultivated

33.0

21

20

19

18

17

16

15

14

+85= 36" Stamp on E

+60= 48" Stamp on E

+52= 30" Stamp on E

Calibrated

Trail

Wagon

Calibrated

+20= 48" Stamp on E

29

²
Gravelled Road.
8 9

28

Begin Gravelled Road

27

26

25

24

23

22

061. Ent. 34' Dist

42' dist

+88 = 12" x 42' C.M.

16

← To yards

+128 F. 2 30°

10' Dist Ent.

18°

28 + 17 = 12" x 16' C.M.

+38 RP 25°

12' Dist Ent.

28 + 10 = 12" x 16' C.M.

16.0

+44.509 yards

26 + 62.702

Cultivated

Trail

Wagon

Cultivated

36

Gravel Road.
6 5

35

6 5

34

7 7

33

8 8

32

6 6

31

7 7

30

5 8

29

61255

+27 P.P. 22.5

Cultivated

Cultivated

+31 End yard

+23 P.P. 25

10' Dist Entr.

33+03 = 12" x 24' C.M.

10' Dist Entr.

33+00 = 12" x 22' C.M.

yard

yard

+38 = 12" Oak 20

+20 Bog yd.

+18

+16 = 8" Tr. Oak 20

+01 = 18" Oak 20

+80 = 20" Oak 21

+58 P.P. 25.0

Cultivated

Cultivated

8' Dist Entr.

+29 = 12" x 22' C.M.



30+00 P.P. 26.0

End yard +65

yards

yards



10' Dist Entr.

+65 = 12" x 16' C.M.

43

Gravelled Road.

7 7

42

7 7

41

7 6

40

7 7

39

7 7

38

7 6

37

9 6

36

$90 - 15 =$
 8' Dist. Entr.
 $+53 = 12" \times 16' C.M.$

+50 Bog Fe. 24

$90 - 15 =$
 8' Dist. Entr.
 $+47 = 12" \times 16' C.M.$

8' Dist. Entr.
 $+47 = 12" \times 16' C.M.$

$90 - 15 =$
 8' Dist. Entr.
 $+16 = 12" \times 16' C.M.$

12' C.P. 55

12' Dist. Entr.
 $36 + 39 = 12" \times 24' C.M.$

+77 P.P. 25

+61 P.P. 25

+43 P.P. 25

50

Gravelled Road.
£6-20

49

5-18

48

4-18

47

2-18

46

1 14

45

5 11

44

8 9

43

7 7

Travelled Road.

2

57

51

} 7-20

50

Labore 5149288

①

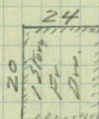
Road 18' Bl. Top.

27 x x x 51469 J x

27

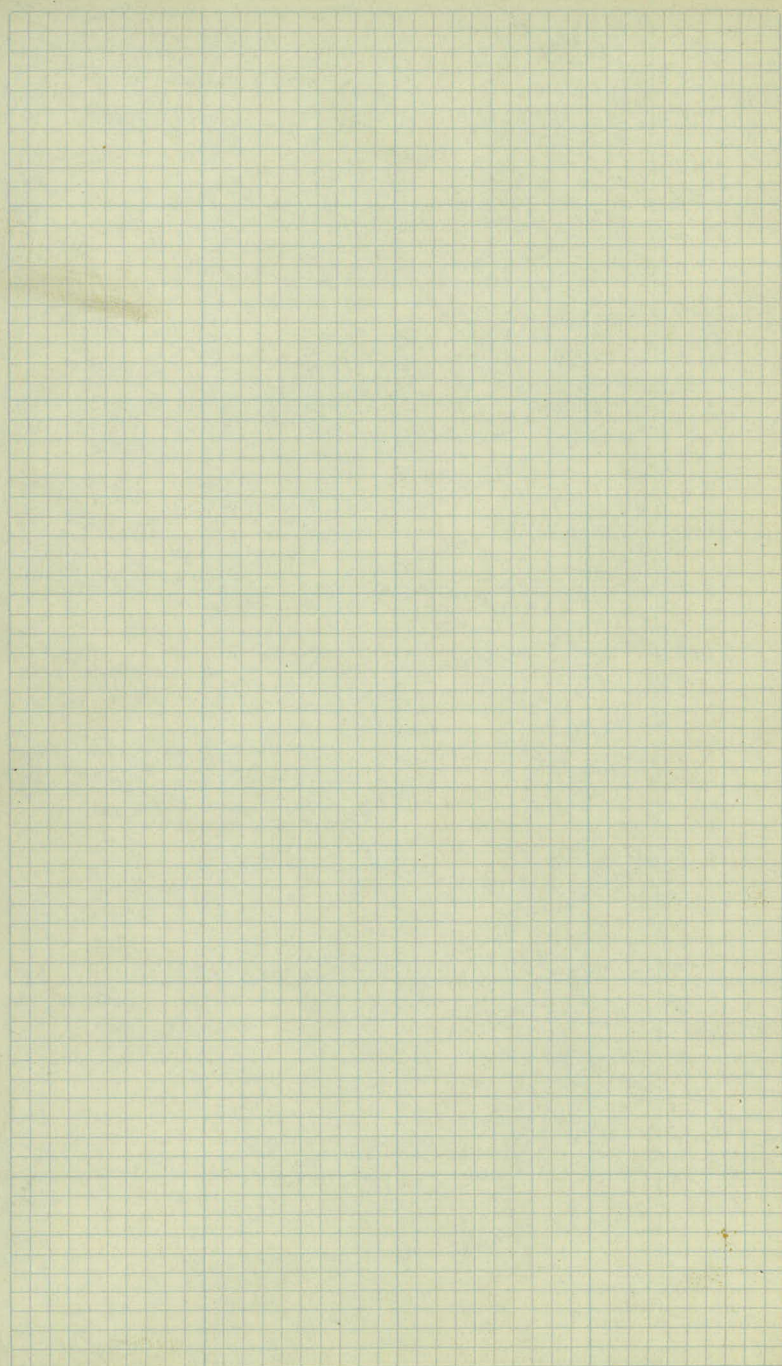
Pasture

116 P.P. 25



10' →
← 50' →
Cutting

+36



Bench Levels.

	+	π	-	Elev.
B.M.	13.79	912.27		898.48
B.M	9.63	912.27	9.63	902.64
	7.77	919.06	0.98	911.29
	4.03	914.12	8.97	910.09
B.M	4.85	914.12	4.85	909.27
	4.24	915.15	3.21	910.91
	3.33	914.94	3.54	911.61
B.M	7.60	920.35	2.19	912.75
	7.42	927.27	0.50	919.85
B.M.	6.35	928.36	5.26	922.01
	3.31	928.81	2.86	925.50
B.M			4.49	924.32

Description

Spike in 24" Elm @ Edgerton St. and
Vadnais Blvd. (Vadnais Survey of 1938)

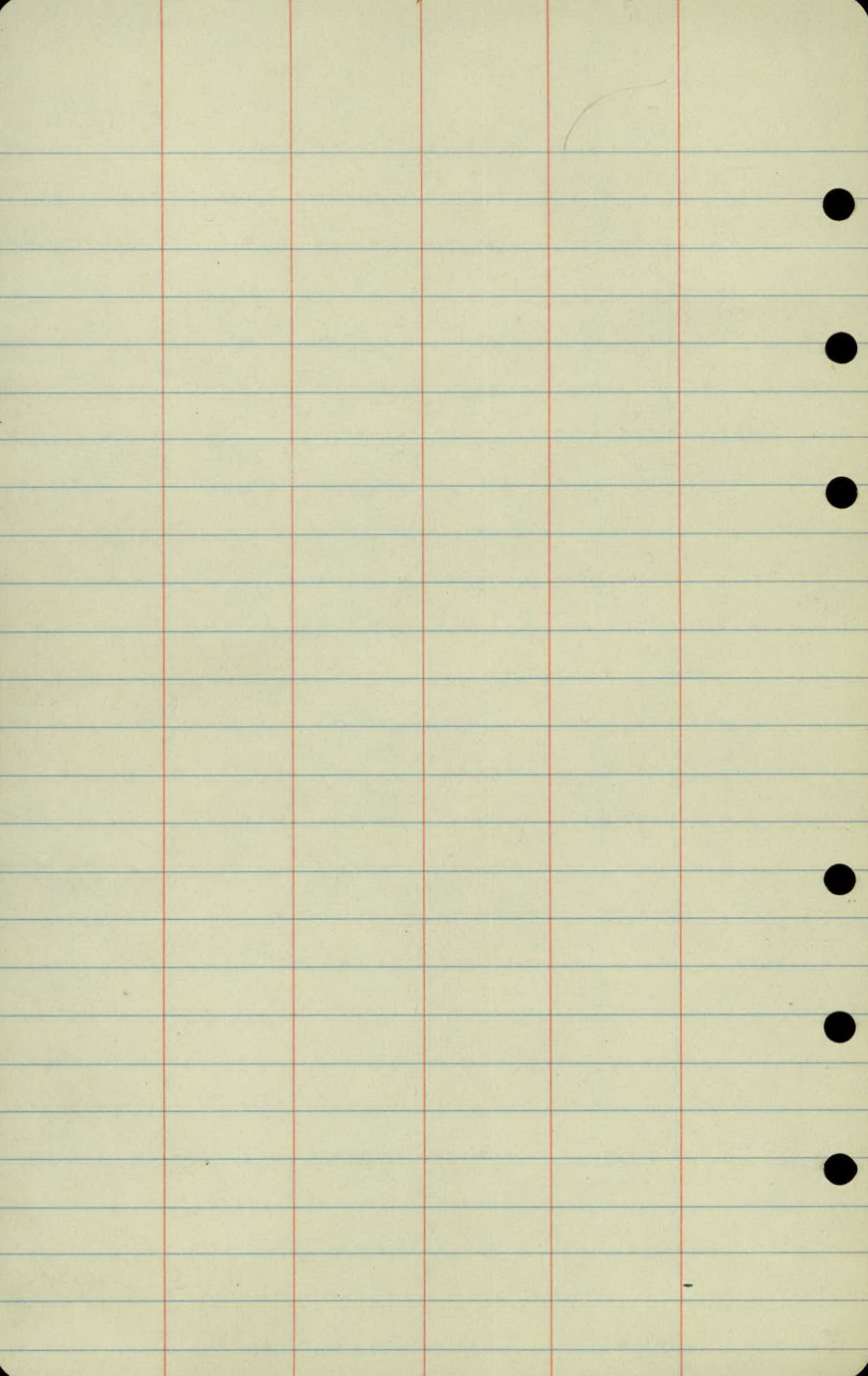
Drill hole @ Edgerton + 2+00

Spk in 36" Cottonwood 200' Rt Sta 10+50

Top of Electrical Conduit at Northwest Cor House 80' Rt Sta
27+80

Spk in P.P. 90" Lt Sta 39+80 ✓

Top of Beat Spk Sta 51+92.86



Mississippi St.
Cross Sections

Sta.	+	K	-	Elev.
B.M.	10.64	913.46		902.64

0-15 E Edgerton St. (Parallel) 04.02

0+00 03.4

+21 03.6

+50 03.9

+80 08.6

1+00 10.1

T.P. 8.58 919.11 2.73 910.53

1+16 (Elm 31' out on Lt.) 10.9

1+37.55 off Back Tangent 12.0

1+37.55 off Fore Tang. 12.0

2+00 5.4 913.9 (914.0)

Lt.

E

Rt.

Drill hole Edgerton St.

$\frac{14.3}{100}$	$\frac{11.7}{50}$	$\frac{9.24}{50}$	$\frac{6.7}{50}$	$\frac{4.2}{100}$
--------------------	-------------------	-------------------	------------------	-------------------

Edgerton

 $\frac{10.12}{10}$

$\frac{9.9}{8}$	$\frac{9.8}{10}$	$\frac{10.4}{10}$	$\frac{9.0}{17}$	$\frac{4.1}{27}$	$\frac{+0.7}{34}$	$\frac{+0.7}{50}$
-----------------	------------------	-------------------	------------------	------------------	-------------------	-------------------

Edgerton

4

$\frac{11.5}{26}$	$\frac{11.4}{14}$	$\frac{10.0}{6}$	$\frac{9.7}{5}$	$\frac{9.4}{7}$	$\frac{9.9}{9}$	$\frac{9.9}{14}$	$\frac{8.0}{19}$	$\frac{3.3}{21}$	$\frac{+0.3}{29}$	$\frac{+0.3}{29}$	$\frac{+1.5}{36}$
-------------------	-------------------	------------------	-----------------	-----------------	-----------------	------------------	------------------	------------------	-------------------	-------------------	-------------------

Edgerton

2

$\frac{13.7}{54}$	$\frac{13.4}{39}$	$\frac{11.0}{26}$	$\frac{10.4}{18}$	$\frac{2.6}{11}$	$\frac{7.4}{9}$	$\frac{7.3}{10}$	$\frac{7.9}{11}$	$\frac{7.9}{21}$	$\frac{0.0}{50}$	$\frac{+0.9}{50}$
-------------------	-------------------	-------------------	-------------------	------------------	-----------------	------------------	------------------	------------------	------------------	-------------------

$\frac{12.7}{54}$	$\frac{3.4}{25}$	$\frac{10.2}{21}$	$\frac{0.1}{15}$	$\frac{5.3}{7}$	$\frac{5.0}{6}$	$\frac{4.7}{11}$	$\frac{4.7}{11}$	$\frac{5.5}{13}$	$\frac{5.5}{13}$	$\frac{0.5}{23}$	$\frac{+0.7}{34}$	$\frac{+1.0}{50}$
-------------------	------------------	-------------------	------------------	-----------------	-----------------	------------------	------------------	------------------	------------------	------------------	-------------------	-------------------

$\frac{11.6}{50}$	$\frac{2.7}{35}$	$\frac{7.10}{33}$	$\frac{0.0}{16}$	$\frac{4.1}{7}$	$\frac{4.1}{5}$	$\frac{3.1}{4}$	$\frac{3.2}{3}$	$\frac{2.2}{19}$	$\frac{0.0}{31}$	$\frac{+1.0}{50}$
-------------------	------------------	-------------------	------------------	-----------------	-----------------	-----------------	-----------------	------------------	------------------	-------------------

$\frac{13.4}{50}$	$\frac{11.6}{46}$	$\frac{5.6}{44}$	$\frac{0.5}{18}$	$\frac{5.1}{8}$	$\frac{2.1}{6}$	$\frac{8.4}{4}$	$\frac{8.2}{8}$	$\frac{8.3}{19}$	$\frac{7.2}{22}$	$\frac{5.5}{50}$
-------------------	-------------------	------------------	------------------	-----------------	-----------------	-----------------	-----------------	------------------	------------------	------------------

$\frac{5.9}{50}$	$\frac{5.5}{18}$	$\frac{8.2}{11}$	$\frac{8.2}{8}$	$\frac{7.3}{6}$	$\frac{7.1}{7}$	$\frac{7.6}{13}$	$\frac{8.5}{14}$	$\frac{8.5}{16}$	$\frac{0.6}{23}$	$\frac{5.0}{50}$
------------------	------------------	------------------	-----------------	-----------------	-----------------	------------------	------------------	------------------	------------------	------------------

$\frac{5.6}{50}$	$\frac{5.8}{27}$	$\frac{6.7}{23}$	$\frac{6.7}{20}$	$\frac{7.0}{10}$	$\frac{7.1}{7}$	$\frac{8.3}{26}$	$\frac{7.4}{43}$	$\frac{6.1}{50}$
------------------	------------------	------------------	------------------	------------------	-----------------	------------------	------------------	------------------

Check on ground

No. + π - Grade

Cross sections.

T.P. 4.02

Sta.	+	π	-	Elev.
B.M.	6.28	908.91		902.64

0+00 Along & Edgerton St. 02.64

0+00 02.6

0+37 02.9

0+64 08.3

T.P. 11.02 918.87 1.07 907.85

0+75 13.4

1 13.6

+12.55 Back Tangent 13.0

+12.55 Fore Tangent 13.0

+40 12.1

+56 10.9

+62 13.4

Lt.

E

Rt.

18

Drill hole in Brement & Edgerton

$\frac{11.3}{100}$ $\frac{5.8}{50}$ $\frac{6.78}{50}$ $\frac{3.8}{50}$ $\frac{1.4}{100}$

$\frac{6.3}{17}$ $\frac{5.8}{17}$ $\frac{5.9}{22}$ $\frac{6.5}{25}$ $\frac{4.9}{34}$ $\frac{20}{44}$ $\frac{+50}{50}$ $\frac{+100}{60}$

E Edgerton

$\frac{8.9}{30}$ $\frac{8.4}{16}$ $\frac{6.0}{6}$ $\frac{5.2}{15}$ $\frac{3.8}{24}$ $\frac{3.3}{28}$ $\frac{3.9}{33}$ $\frac{20}{38}$ $\frac{+45}{50}$

E Edgerton

$\frac{106}{50}$ $\frac{102}{36}$ $\frac{83}{25}$ $\frac{50}{19}$ $\frac{15}{5}$ $\frac{0.6}{5}$ $\frac{10}{8}$ $\frac{20}{7}$ $\frac{20}{9}$ $\frac{14}{11}$ $\frac{11}{24}$ $\frac{16}{27}$ $\frac{18}{30}$ $\frac{20}{33}$ $\frac{+40}{44}$ $\frac{12}{50}$

E Edgerton

$\frac{208}{23}$ $\frac{206}{41}$ $\frac{158}{34}$ $\frac{140}{21}$ $\frac{88}{8}$ $\frac{54}{6}$ $\frac{55}{5}$ $\frac{57}{2}$ $\frac{74}{4}$ $\frac{106}{11}$ $\frac{102}{16}$ $\frac{103}{27}$ $\frac{111}{29}$ $\frac{111}{30}$ $\frac{69}{38}$ $\frac{53}{49}$ $\frac{52}{20}$

E Edgerton

$\frac{226}{77}$ $\frac{224}{63}$ $\frac{154}{41}$ $\frac{130}{34}$ $\frac{114}{29}$ $\frac{52}{27}$ $\frac{53}{5}$ $\frac{26}{10}$ $\frac{85}{11}$ $\frac{81}{15}$ $\frac{82}{28}$ $\frac{77}{37}$ $\frac{51}{20}$

$\frac{240}{71}$ $\frac{236}{76}$ $\frac{214}{63}$ $\frac{127}{45}$ $\frac{86}{36}$ $\frac{57}{33}$ $\frac{59}{5}$ $\frac{85}{7}$ $\frac{85}{9}$ $\frac{77}{14}$ $\frac{77}{29}$ $\frac{84}{31}$ $\frac{84}{33}$ $\frac{20}{36}$ $\frac{59}{50}$

$\frac{86}{50}$ $\frac{54}{27}$ $\frac{53}{7}$ $\frac{59}{5}$ $\frac{53}{6}$ $\frac{89}{14}$ $\frac{84}{20}$ $\frac{88}{37}$ $\frac{55}{10}$ $\frac{108}{51}$ $\frac{108}{53}$ $\frac{66}{68}$ $\frac{51}{96}$

$\frac{5.3}{50}$ $\frac{5.6}{30}$ $\frac{7.4}{26}$ $\frac{7.4}{23}$ $\frac{6.8}{21}$ $\frac{6.2}{11}$ $\frac{6.8}{6.8}$ $\frac{7.8}{17}$ $\frac{8.5}{15}$ $\frac{8.5}{22}$ $\frac{7.5}{25}$ $\frac{6.9}{32}$ $\frac{5.7}{50}$

$\frac{6.0}{50}$ $\frac{6.6}{47}$ $\frac{6.6}{45}$ $\frac{5.8}{40}$ $\frac{6.2}{10}$ $\frac{4.8}{3}$ $\frac{8.0}{8.0}$ $\frac{7.7}{2}$ $\frac{5.6}{10}$ $\frac{4.8}{26}$ $\frac{6.0}{32}$ $\frac{5.1}{50}$

$\frac{6.3}{50}$ $\frac{6.1}{16}$ $\frac{7.5}{10}$ $\frac{7.5}{6}$ $\frac{5.5}{3}$ $\frac{5.5}{5.5}$ $\frac{4.8}{32}$ $\frac{5.0}{50}$

Sta. + π - Elev.

918.87

2+00 14.0

+50 14.0

3+00 14.2

4+00 11.4

4+00 14.4

T.P 3.09 914.52 7.44 911.43

5+00 10.0

+50 09.2

+70 Ditch LEFT 08.8

2+00 09.0

7+00 08.7

8+00 08.8

9+00 08.6

10+00 08.7

B.M 426 913.53 5.25 909.27

Lt.

E

Rt.

19

$$\frac{5.1}{50} \frac{5.9}{45} \frac{4.9}{43} 4.9 \quad \frac{4.9}{35} \frac{5.4}{50}$$

$$\frac{5.0}{50} 4.9 \quad \frac{5.0}{28} \frac{5.0}{50}$$

$$\frac{4.7}{50} 4.7 \quad \frac{5.1}{11} \frac{5.5}{12} \frac{5.7}{35} \frac{5.7}{50}$$

$$\frac{6.2}{50} \frac{6.7}{40} \quad 7.5 \quad \frac{7.0}{20} \frac{7.6}{29} \frac{7.7}{40} \frac{7.7}{50}$$

$$\frac{4.4}{50} \frac{5.0}{8} 4.5 \quad \frac{4.8}{16} \frac{5.0}{38} \frac{4.6}{50}$$

$$\frac{4.6}{50} \frac{4.9}{12} \frac{4.4}{2} 5.3 \quad \frac{5.6}{15} \frac{5.8}{37} \frac{5.2}{50}$$

$$\frac{7.2}{350} \frac{7.0}{300} \frac{6.1}{250} \frac{6.7}{200} \frac{6.9}{150} \frac{6.7}{100} \frac{6.6}{50} 5.7 \quad \frac{6.0}{50} \frac{6.0}{100} \frac{5.9}{150} \frac{6.4}{200} \frac{6.2}{250} \frac{6.3}{300}$$

$$\frac{4.8}{50} \frac{4.9}{9} \frac{6.0}{4} \frac{5.6}{3} 5.5 \quad \frac{5.6}{11} \frac{5.1}{14} \frac{5.4}{30} \frac{5.2}{50}$$

$$\frac{5.0}{50} \frac{5.4}{9} 5.8 \quad \frac{6.0}{8} \frac{5.5}{13} \frac{5.5}{28} \frac{5.2}{30} \frac{5.2}{50}$$

$$\frac{5.3}{50} \frac{5.7}{4} 5.7 \quad \frac{5.8}{8} \frac{5.3}{12} \frac{5.3}{28} \frac{5.0}{31} \frac{4.9}{36} \frac{4.9}{50}$$

$$\frac{5.6}{50} \frac{5.6}{17} \frac{6.0}{4} 5.9 \quad \frac{6.0}{7} \frac{5.5}{11} \frac{5.9}{28} \frac{5.5}{30} \frac{5.4}{35} \frac{5.4}{50}$$

$$\frac{5.5}{50} \frac{5.3}{15} \frac{5.4}{3} 5.8 \quad \frac{6.0}{8} \frac{5.6}{11} \frac{6.0}{28} \frac{5.7}{50}$$

5pK in Cottonwood 200 Rt Sta 10+50

5/2.	+	π	-	Elev.
		913.53		
10+35				08.5
11+00				08.3
12+00				07.9
12+00		Ditch Rt		07.9
13+00				08.5
14+00				09.5
15+00				10.1
T.P.	5.08	915.11	3.50	910.03
16+00				10.1
17+00				10.0
18+00				10.3
19+00				10.0
+50				09.5

Lt.

E

Rt.

20

$$\frac{4.7}{50} \quad \frac{4.5}{11} \quad 5.0 \quad \frac{5.1}{8} \quad \frac{4.8}{10} \quad \frac{4.8}{28} \quad \frac{4.2}{30} \quad \frac{4.6}{50}$$

$$\frac{3.8}{50} \quad \frac{4.2}{13} \quad \frac{4.5}{2} \quad 5.2 \quad 3 \quad \frac{4.0}{14} \quad \frac{4.4}{23} \quad \frac{4.8}{28} \quad \frac{4.7}{50}$$

$$\frac{4.5}{50} \quad \frac{4.8}{20} \quad \frac{5.1}{2} \quad 5.6 \quad 3 \quad \frac{4.6}{28} \quad \frac{5.4}{30} \quad \frac{4.9}{50}$$

$$5.6 \quad \frac{5.6}{30} \quad \frac{5.6}{80} \quad \frac{5.7}{130} \quad \frac{5.3}{180} \quad \frac{5.9}{230} \quad \frac{5.9}{280} \quad \frac{6.0}{330}$$

$$\frac{4.6}{50} \quad \frac{4.7}{24} \quad \frac{5.2}{5} \quad \frac{4.6}{4} \quad \frac{4.4}{2} \quad 5.0 \quad \frac{5.2}{2} \quad \frac{4.7}{3} \quad \frac{4.9}{19} \quad \frac{4.8}{30} \quad \frac{5.0}{50}$$

$$\frac{3.9}{50} \quad \frac{4.1}{23} \quad \frac{3.5}{3} \quad 4.0 \quad \frac{3.4}{6} \quad \frac{3.7}{50}$$

$$\frac{3.8}{50} \quad \frac{3.4}{38} \quad \frac{3.8}{7} \quad \frac{2.6}{1} \quad 3.4 \quad \frac{3.9}{2} \quad \frac{3.5}{4} \quad \frac{3.0}{22} \quad \frac{3.0}{50}$$

$$\frac{5.0}{50} \quad \frac{5.0}{35} \quad \frac{5.1}{8} \quad \frac{4.5}{2} \quad 5.0 \quad \frac{5.4}{2} \quad \frac{5.2}{5} \quad \frac{5.4}{7} \quad \frac{4.6}{31} \quad \frac{4.4}{15}$$

$$\frac{5.1}{50} \quad \frac{5.2}{33} \quad \frac{5.1}{7} \quad \frac{4.3}{2} \quad 5.1 \quad \frac{5.7}{2} \quad \frac{5.2}{5} \quad \frac{4.8}{20} \quad \frac{4.6}{50}$$

$$\frac{5.0}{50} \quad \frac{5.1}{34} \quad \frac{4.8}{3} \quad 4.8 \quad \frac{5.6}{7} \quad \frac{4.5}{32} \quad \frac{4.6}{50}$$

$$\frac{6.0}{50} \quad 5.1 \quad \frac{5.5}{7} \quad \frac{6.0}{8} \quad \frac{5.5}{50}$$

$$\frac{5.4}{50} \quad \frac{5.7}{22} \quad \frac{6.0}{3} \quad \frac{5.6}{2} \quad 5.6 \quad \frac{6.5}{10} \quad \frac{5.9}{24} \quad \frac{5.8}{50}$$

Sta	+	T	-	Elev
		915.11		
20+00				09.7
21+00				10.1
22+00				10.5
23+00				09.2
T.P.	6.76	916.41	5.46	909.65
24+00				10.6
25+00				09.9
250				10.4
26+00				09.9
+63				11.3
27				11.3
+50				11.4
B.M	3.66	916.41	3.66	912.75

H.

A

H

$$\frac{5.6}{50}$$

$$\frac{5.9}{3}$$

$$5.4$$

$$\frac{5.7}{8}$$

$$\frac{6.1}{14}$$

$$\frac{5.7}{32}$$

$$\frac{5.9}{50}$$

$$\frac{6.0}{50}$$

$$\frac{5.3}{22}$$

$$\frac{5.7}{4}$$

$$5.0$$

$$\frac{5.3}{8}$$

$$\frac{5.0}{22}$$

$$\frac{5.2}{50}$$

$$\frac{5.1}{50}$$

$$\frac{4.9}{13}$$

$$\frac{5.4}{4}$$

$$4.6$$

$$\frac{5.1}{6}$$

$$\frac{4.8}{24}$$

$$\frac{4.2}{50}$$

$$\frac{4.7}{50}$$

$$\frac{4.9}{25}$$

$$5.9$$

$$\frac{6.2}{15}$$

$$\frac{5.8}{24}$$

$$\frac{5.4}{50}$$

$$\frac{5.5}{50}$$

$$\frac{6.6}{4}$$

$$\frac{5.9}{3}$$

$$5.8$$

$$\frac{6.0}{6}$$

$$\frac{6.6}{17}$$

$$\frac{6.5}{26}$$

$$\frac{6.9}{50}$$

$$\frac{7.8}{50}$$

$$\frac{7.2}{25}$$

$$\frac{6.8}{5}$$

$$\frac{6.1}{15}$$

$$\frac{6.9}{5}$$

$$\frac{6.5}{34}$$

$$\frac{6.4}{50}$$

$$\frac{6.6}{50}$$

$$\frac{6.5}{32}$$

$$\frac{6.7}{4}$$

$$\frac{6.1}{3}$$

$$6.0$$

$$\frac{6.4}{3}$$

$$\frac{6.7}{4}$$

$$\frac{6.3}{38}$$

$$\frac{6.2}{50}$$

$$\frac{6.0}{50}$$

$$\frac{6.2}{25}$$

$$\frac{6.4}{4}$$

$$6.5$$

$$\frac{7.0}{4}$$

$$\frac{6.5}{33}$$

$$\frac{6.1}{50}$$

$$\frac{4.8}{50}$$

$$\frac{4.9}{26}$$

$$5.1$$

$$\frac{5.2}{9}$$

$$\frac{5.8}{12}$$

$$\frac{5.2}{14}$$

$$\frac{5.2}{50}$$

$$\frac{5.3}{50}$$

$$\frac{5.2}{17}$$

$$\frac{5.9}{16}$$

$$\frac{5.9}{14}$$

$$\frac{5.4}{14}$$

$$5.1$$

$$\frac{5.1}{16}$$

$$\frac{5.7}{17}$$

$$\frac{5.7}{19}$$

$$\frac{5.1}{21}$$

$$\frac{5.4}{50}$$

$$\frac{4.8}{50}$$

$$\frac{5.0}{12}$$

$$\frac{5.7}{15}$$

$$\frac{5.0}{9}$$

$$5.0$$

$$\frac{5.0}{11}$$

$$\frac{5.8}{18}$$

$$\frac{5.1}{20}$$

$$\frac{5.4}{50}$$

Sta.	+	K	-	Elev.
28		916.41		12.2

29				12.8
----	--	--	--	------

30				13.4
----	--	--	--	------

31				15.0
----	--	--	--	------

T.P.	11.89	927.34	0.96	915.45
------	-------	--------	------	--------

32				17.2
----	--	--	--	------

33				18.7
----	--	--	--	------

34				20.2
----	--	--	--	------

35				22.1
----	--	--	--	------

36				22.7
----	--	--	--	------

37				22.4
----	--	--	--	------

38				22.0
----	--	--	--	------

39				21.9
----	--	--	--	------

40				22.1
----	--	--	--	------

2

4+

4+

$$\frac{45}{50} \quad \frac{47}{17} \quad \frac{55}{16} \quad \frac{49}{10} \quad \frac{42}{9} \quad \frac{46}{9} \quad \frac{57}{18} \quad \frac{50}{20} \quad \frac{53}{50}$$

$$\frac{41}{50} \quad \frac{42}{19} \quad \frac{50}{15} \quad \frac{36}{9} \quad \frac{43}{10} \quad \frac{51}{18} \quad \frac{42}{20} \quad \frac{46}{50}$$

$$\frac{25}{50} \quad \frac{36}{16} \quad \frac{44}{14} \quad \frac{37}{9} \quad \frac{30}{9} \quad \frac{37}{9} \quad \frac{43}{18} \quad \frac{38}{21} \quad \frac{41}{50}$$

$$\frac{20}{50} \quad \frac{23}{28} \quad \frac{28}{26} \quad \frac{24}{15} \quad \frac{31}{13} \quad \frac{11}{14} \quad \frac{19}{8} \quad \frac{29}{17} \quad \frac{20}{17} \quad \frac{16}{21} \quad \frac{23}{30} \quad \frac{20}{50}$$

$$\frac{108}{50} \quad \frac{110}{47} \quad \frac{115}{16} \quad \frac{119}{14} \quad \frac{101}{14} \quad \frac{74}{14} \quad \frac{105}{16} \quad \frac{106}{50}$$

$$\frac{86}{50} \quad \frac{92}{16} \quad \frac{106}{14} \quad \frac{106}{14} \quad \frac{93}{8} \quad \frac{86}{13} \quad \frac{100}{13} \quad \frac{91}{16} \quad \frac{84}{50}$$

$$\frac{71}{50} \quad \frac{24}{16} \quad \frac{80}{13} \quad \frac{80}{14} \quad \frac{25}{10} \quad \frac{71}{10} \quad \frac{78}{10} \quad \frac{75}{50}$$

$$\frac{61}{50} \quad \frac{57}{16} \quad \frac{62}{15} \quad \frac{62}{14} \quad \frac{53}{14} \quad \frac{52}{9} \quad \frac{59}{9} \quad \frac{63}{50}$$

$$\frac{54}{50} \quad \frac{51}{16} \quad \frac{59}{14} \quad \frac{59}{13} \quad \frac{49}{9} \quad \frac{46}{9} \quad \frac{50}{8} \quad \frac{60}{8} \quad \frac{60}{10} \quad \frac{51}{14} \quad \frac{53}{50}$$

$$\frac{57}{50} \quad \frac{56}{16} \quad \frac{60}{14} \quad \frac{60}{14} \quad \frac{52}{9} \quad \frac{49}{6} \quad \frac{53}{6} \quad \frac{61}{9} \quad \frac{61}{11} \quad \frac{52}{14} \quad \frac{56}{50}$$

$$\frac{60}{50} \quad \frac{59}{16} \quad \frac{65}{15} \quad \frac{65}{14} \quad \frac{56}{10} \quad \frac{53}{6} \quad \frac{55}{6} \quad \frac{63}{9} \quad \frac{63}{11} \quad \frac{56}{14} \quad \frac{56}{50}$$

$$\frac{59}{50} \quad \frac{58}{16} \quad \frac{65}{14} \quad \frac{57}{9} \quad \frac{54}{6} \quad \frac{59}{6} \quad \frac{63}{9} \quad \frac{56}{14} \quad \frac{59}{22} \quad \frac{59}{50}$$

$$\frac{58}{50} \quad \frac{58}{16} \quad \frac{63}{14} \quad \frac{57}{10} \quad \frac{54}{6} \quad \frac{57}{6} \quad \frac{64}{9} \quad \frac{55}{50}$$

Sta.	+	π	-	Elev.	
		927.34			
B.M.	6.17	928.18	5.33	922.01	922.01
41				22.5	
42				23.2	
43				23.4	
44				23.1	
45				23.3	
+50				23.6	
46				24.0	
+50				24.7	
T.P.	3.37	928.63	2.92	925.26	
47				24.8	
+50				25.2	
48				24.6	

Lt.

Q

Rt.

Spike in P.P. 90' Lt. 5 1/2. 39+80

$$\frac{63}{50} \quad \frac{65}{16} \quad \frac{69}{14} \quad \frac{69}{13} \quad \frac{61}{9} \quad \cancel{57} \quad \frac{61}{7} \quad \frac{66}{9} \quad \frac{66}{10} \quad \frac{61}{12} \quad \frac{62}{50}$$

$$\frac{63}{50} \quad \frac{61}{16} \quad \frac{65}{14} \quad \frac{65}{9} \quad \cancel{50} \quad \frac{64}{7} \quad \frac{68}{9} \quad \frac{64}{12} \quad \frac{63}{50}$$

$$\frac{50}{50} \quad \frac{51}{17} \quad \frac{66}{18} \quad \frac{51}{12} \quad \cancel{48} \quad \frac{52}{7} \quad \frac{58}{10} \quad \frac{55}{16} \quad \frac{56}{50}$$

$$\frac{58}{50} \quad \frac{61}{16} \quad \frac{65}{18} \quad \frac{65}{14} \quad \frac{58}{11} \quad \cancel{51} \quad \frac{57}{9} \quad \frac{68}{12} \quad \frac{68}{14} \quad \frac{59}{16} \quad \frac{59}{50}$$

$$\frac{52}{50} \quad \frac{55}{18} \quad \frac{62}{14} \quad \frac{52}{6} \quad \cancel{49} \quad \frac{50}{5} \quad \frac{57}{11} \quad \frac{62}{13} \quad \frac{56}{15} \quad \frac{61}{28} \quad \frac{55}{50}$$

$$\frac{54}{50} \quad \frac{54}{26} \quad \frac{51}{13} \quad \frac{60}{12} \quad \frac{51}{4} \quad \cancel{46} \quad \frac{48}{7} \quad \frac{54}{13} \quad \frac{59}{14} \quad \frac{59}{15} \quad \frac{55}{17} \quad \frac{49}{27} \quad \frac{49}{50}$$

$$\frac{40}{50} \quad \frac{42}{10} \quad \frac{52}{8} \quad \frac{44}{2} \quad \cancel{42} \quad \frac{38}{7} \quad \frac{46}{14} \quad \frac{51}{16} \quad \frac{51}{18} \quad \frac{44}{19} \quad \frac{43}{30} \quad \frac{40}{50}$$

$$\frac{32}{50} \quad \frac{32}{32} \quad \cancel{35} \quad \frac{30}{8} \quad \frac{40}{19} \quad \frac{29}{26} \quad \frac{34}{50}$$

$$\frac{37}{50} \quad \cancel{38} \quad \frac{35}{3} \quad \frac{32}{9} \quad \frac{38}{19} \quad \frac{30}{21} \quad \frac{36}{50}$$

$$\frac{37}{50} \quad \cancel{34} \quad \frac{30}{10} \quad \frac{36}{20} \quad \frac{27}{24} \quad \frac{29}{50}$$

$$\frac{36}{50} \quad \cancel{40} \quad \frac{34}{11} \quad \frac{43}{20} \quad \frac{35}{22} \quad \frac{31}{50}$$

5/2 + K - Elev

928.63

49 23.5

50 23.9

51 23.9

+50 24.1

51+97.88 Labore Road 24.3

B.M. 4.29 924.34 924.32

Lt.

Z

Rt.

24

$$\frac{5.2}{50}$$

$$\frac{5.1}{50}$$

$$\frac{5.2}{4}$$

$$\frac{4.4}{12}$$

$$\frac{5.1}{19}$$

$$\frac{5.5}{21}$$

$$\frac{5.0}{24}$$

$$\frac{5.0}{50}$$

$$\frac{4.8}{50}$$

$$\frac{4.7}{50}$$

$$\frac{4.8}{6}$$

$$\frac{4.3}{13}$$

$$\frac{5.1}{20}$$

$$\frac{5.4}{22}$$

$$\frac{4.9}{26}$$

$$\frac{5.0}{50}$$

$$\frac{5.2}{50}$$

$$\frac{4.7}{50}$$

$$\frac{4.7}{6}$$

$$\frac{4.1}{14}$$

$$\frac{4.8}{21}$$

$$\frac{5.1}{22}$$

$$\frac{4.5}{26}$$

$$\frac{4.5}{50}$$

$$\frac{5.1}{50}$$

$$\frac{4.5}{50}$$

$$\frac{4.8}{3}$$

$$\frac{4.3}{12}$$

$$\frac{4.7}{21}$$

$$\frac{4.9}{23}$$

$$\frac{4.1}{27}$$

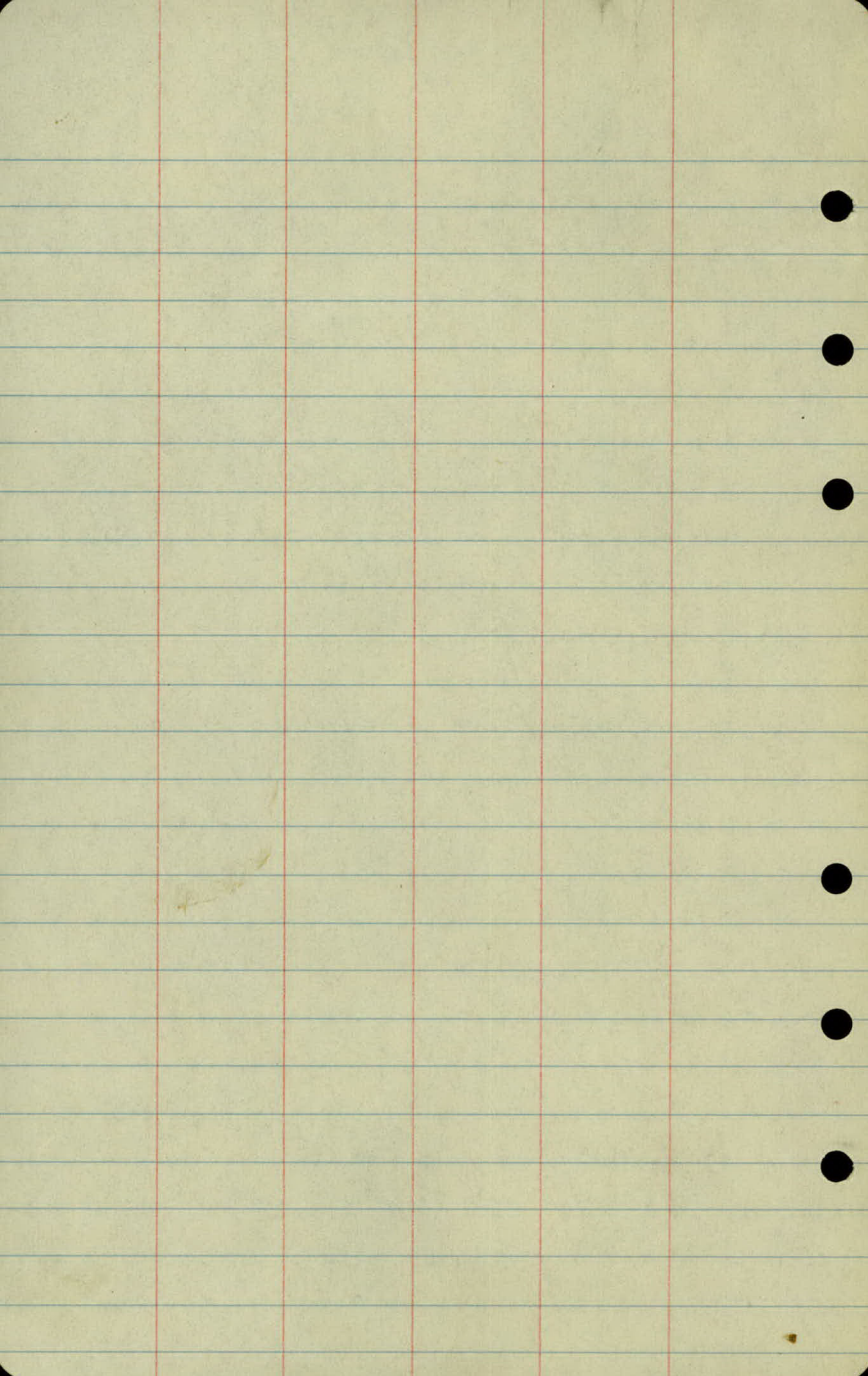
$$\frac{4.1}{50}$$

$$\frac{4.5}{50}$$

$$\frac{4.3}{50}$$

$$\frac{4.2}{50}$$

Top of Best Spike & Labore Road.



Plan Survey

MISSISSIPPI ST.

700' East from EDGERTON ST.

EDGERTON

350' No of MISSISSIPPI

6/20/40

Party

R.P.

A.M.

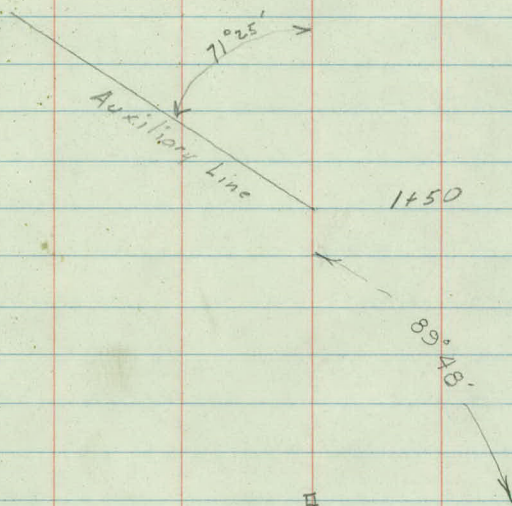
C.F.

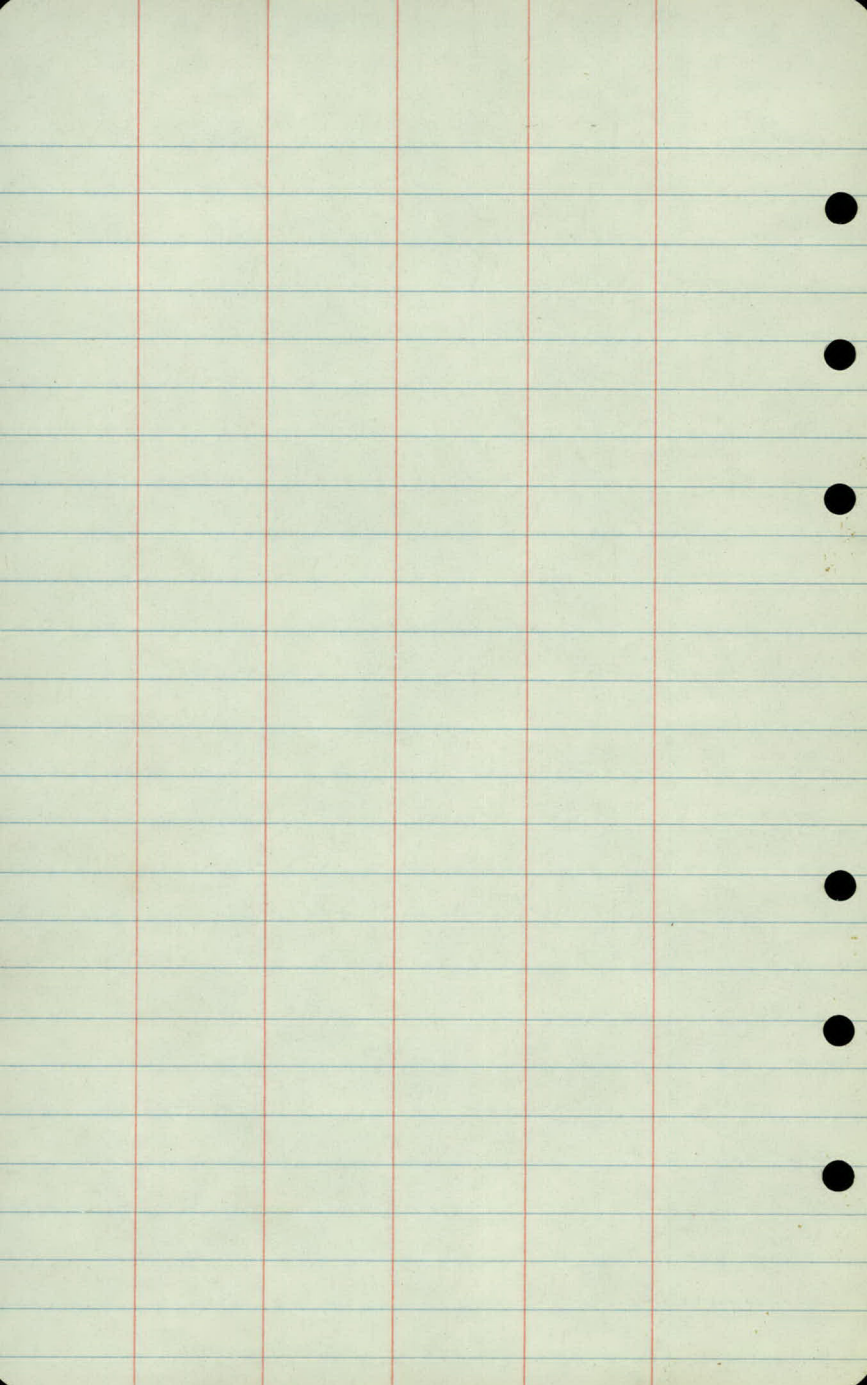
7100

0+50.05

Cfr. Sec. 32-W.B.T.

Spike





Topography

MISSISSIPPI ST.

from Edgerton 700' East

+50

+34 Cor. Barn 86

+19 Cor Sheds 36

+06 Cor. Crib - 43

13

+95 Cor Crib 40
+86 Cor. Barn 86
+82 Cor. Shed - 50

3

14

+50

15

13

+47 Cor. Shed 31
+37 Cor. Shed 32

2

15

12

+13 Cor. Ho. 84

+71 Cor. Ho. 114

+60 Ent

+51 End Gutter 11

+50 Shldr 6

+48 Cor. Ho. 85

+75 Cor. Ho. 64

+62 Cor. Ho. 82

no. 20
Rd Shldr

+30 Cor. Ho. - 96

+39 Shldr x 3 E

1

+00 - 2nd Elm 01

+00 Shldr - 27- 70
+00 RP 99

+63.5 E Rock Paved Gutter
+60 Edge Pave. Xs E

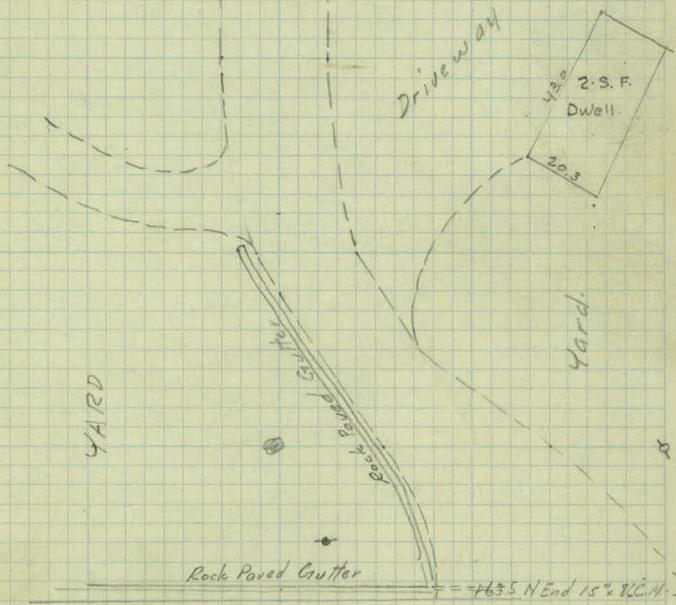
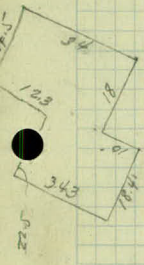
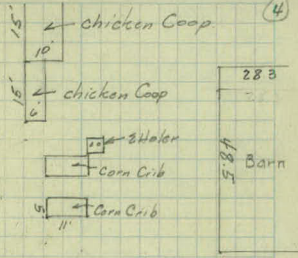
+75 T.P. 10.5

+50

0

+31 Apple 490
+10 Apple 490
+73 Apple 490
+43 Apple 460
+33 P.P. 100
+30 G.P. 104

Apple Orchard.



EDGERTON
20' Pavement

7

13

13

+50

6

13

13

16

+58 - 18" x 30" Conc.

14

+50

5

12

14

4+50

4

12

12 Fe.

35

+93 Cor. Shcd 36

3+50

CULTIVATED

CULTIVATED

125 Ent
12" x 16" C. 14. 19'

+ 82 Ditch - 24

+ 68 Rge. Fir Ditch

+ 41 Apple 71

+ 27 Apple 92

+ 19 Apple - 27

+ 00 Apple 27

+ 82 Apple - 78

+ 08 Apple 95

+ 52 Apple 500

+ 46 Apple 93

+ 33 Apple - 490

+ 13 Apple 500

+ 08 Apple 94

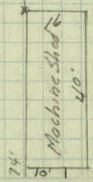
+ 62 G' Elm 490

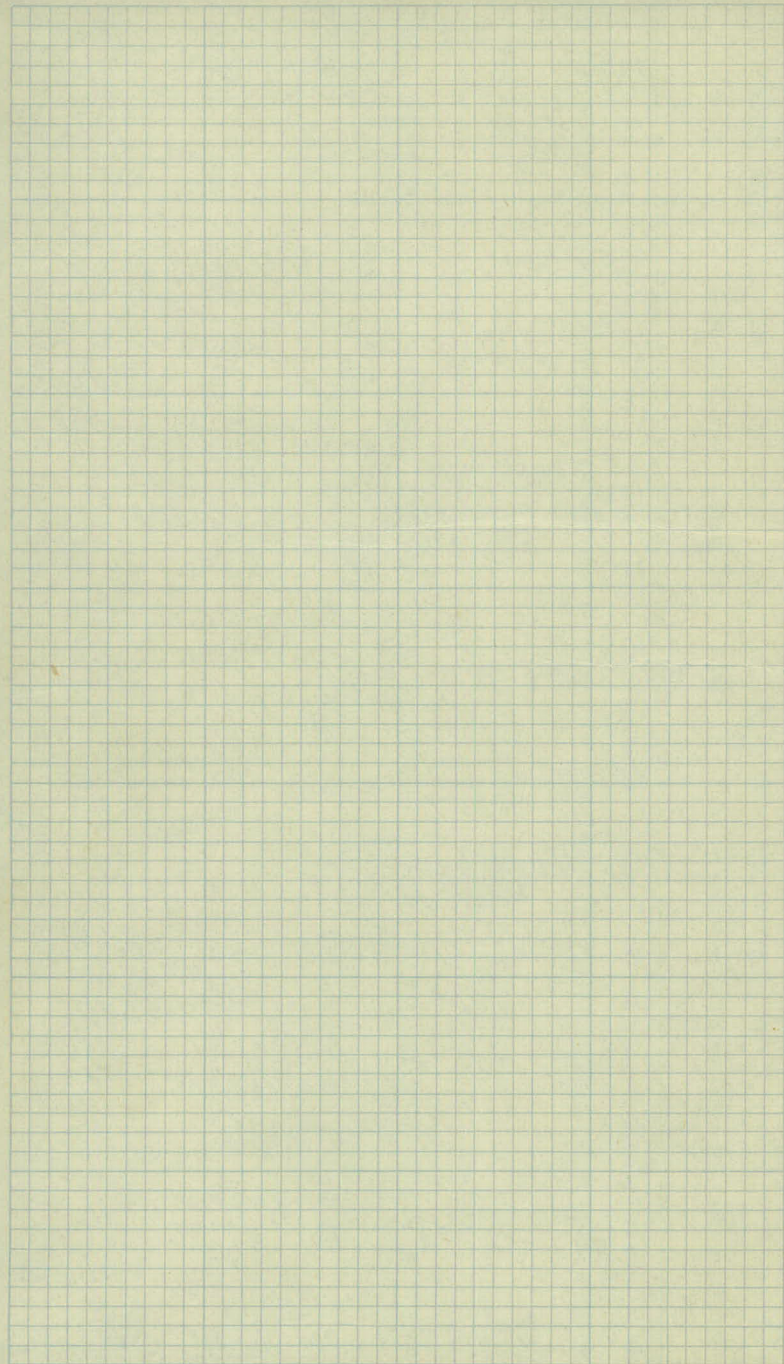
+ 51 Apple 490

APPLE ORCHARD

+ 00 Fe. Log 33

Born Yard





1437.55
 $\Delta 55^{\circ} 12'$

87.5 P.I

75' Rad.

55.12

29 82

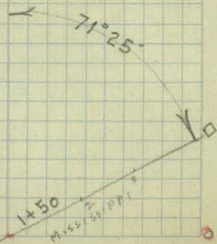
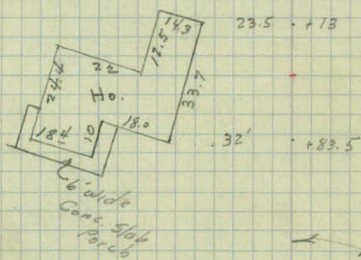
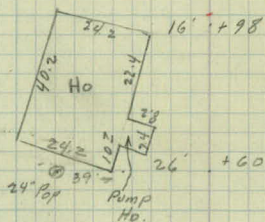
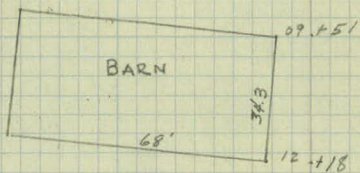
T.

39.20

-540.15-

(5)
Additional Topog.

Taken from Auxiliary Line
Beginning at 1450 - Mississippi St. Notes
To Tie in Bldgs.



Cross Sections

MISSISSIPPI ST.
from Edgerton 700' East

Sta.	+	Σ	-	Elev.
B.M.	4.02	906.66		902.64
0+50			8.88	97.78
+60			8.99	97.67
+64			9.9	96.8
+68			7.4	99.3
T.P.	10.34	913.98	3.02	903.64
T.P.	10.63	919.21	5.40	908.58
+85			11.0	08.2
+89			5.5	13.7
T.P.	1.71	916.40	4.52	914.69
1			1.8	14.6
+06			2.1	14.3
+32			8.1	08.3
+36			8.9	07.5
+41			7.8	08.6
+57			7.1	09.3

Drill Hole in Pave 96.64 S Gtr. Sec.

$\frac{13.87}{100}$ $\frac{11.11}{45}$ $\frac{6.85}{40}$ $\frac{3.88}{100}$

8.88

$\frac{13.95}{100}$ $\frac{11.81}{57}$ $\frac{6.98}{57}$ $\frac{3.97}{100}$

8.99

$\frac{14.5}{100}$ $\frac{12.5}{56}$ $\frac{8.5}{28}$ $\frac{8.1}{38}$ $\frac{7.05}{39}$ $\frac{6.6}{40}$ $\frac{4.6}{69}$ $\frac{3.5}{100}$ $\frac{4.79}{100}$

9.9

$\frac{12.1}{100}$ $\frac{9.6}{35}$ $\frac{5.7}{36}$ $\frac{6.7}{39}$ $\frac{5.6}{40}$ $\frac{4.4}{69}$ $\frac{3.4}{100}$

7.4

$\frac{10.8}{100}$ $\frac{12.7}{71}$ $\frac{14.3}{45}$ $\frac{13.3}{14}$ $\frac{9.3}{15}$ $\frac{9.9}{21}$ $\frac{15.3}{33}$ $\frac{16.4}{34}$ $\frac{15.3}{36}$ $\frac{14.8}{60}$ $\frac{14.9}{86}$ $\frac{16.0}{90.75}$

11.0

$\frac{7.2}{50}$ $\frac{6.6}{50}$ $\frac{6.0}{20}$ $\frac{5.6}{5.5}$ $\frac{6.6}{13}$ $\frac{14.8}{15}$ $\frac{15.9}{30}$ $\frac{15.0}{32}$ $\frac{14.2}{34}$ $\frac{14.5}{57}$ $\frac{15.8}{78}$ $\frac{16.0}{82.88}$

13

Top Steps

$\frac{3.5}{83}$ $\frac{3.2}{69}$ $\frac{3.0}{34}$ $\frac{2.1}{1.8}$ $\frac{10.3}{5}$ $\frac{11.3}{22}$ $\frac{10.8}{26}$ $\frac{10.3}{42}$ $\frac{10.7}{57}$ $\frac{12.0}{63.28}$ $\frac{11.0}{74}$

1.8

$\frac{2.8}{90}$ $\frac{2.9}{51}$ $\frac{2.7}{16}$ $\frac{9.9}{16}$ $\frac{10.9}{19}$ $\frac{10.1}{24}$ $\frac{9.6}{36}$ $\frac{10.0}{50}$ $\frac{11.5}{54.61}$ $\frac{10.0}{66}$

2.1

$\frac{2.7}{91}$ $\frac{2.8}{47}$ $\frac{3.0}{22}$ $\frac{9.1}{8.1}$ $\frac{8.2}{2}$ $\frac{7.9}{5}$ $\frac{7.6}{24}$ $\frac{8.8}{40}$ $\frac{2.2}{45.48}$ $\frac{1.9}{72}$ $\frac{1.9}{100}$

8.1

$\frac{2.8}{100}$ $\frac{2.9}{64}$ $\frac{4.0}{23}$ $\frac{8.0}{3}$ $\frac{9.0}{1}$ $\frac{8.9}{8.9}$ $\frac{8.1}{2}$ $\frac{7.8}{18}$ $\frac{7.2}{41}$ $\frac{7.5}{45.43}$ $\frac{2.3}{64}$ $\frac{1.9}{85}$

8.9

$\frac{2.8}{100}$ $\frac{2.8}{83}$ $\frac{3.2}{54}$ $\frac{3.0}{29}$ $\frac{7.6}{5}$ $\frac{8.8}{3}$ $\frac{7.5}{7.8}$ $\frac{6.8}{17}$ $\frac{5.6}{40}$ $\frac{2.5}{48}$ $\frac{1.8}{58}$ $\frac{1.8}{80}$

7.8

$\frac{3.0}{100}$ $\frac{3.0}{85}$ $\frac{3.5}{61}$ $\frac{4.3}{35}$ $\frac{6.8}{19}$ $\frac{7.3}{9}$ $\frac{7.0}{18}$ $\frac{5.9}{44}$ $\frac{4.7}{50}$ $\frac{2.0}{58}$ $\frac{1.8}{74}$

7.1

Sta	+	π	-	Elev.
		916.40		
1 + 74			6.5	09.9
+ 84			6.3	10.1
2			6.0	10.4
+ 30			5.5	10.9
T.P.	7.57	918.61	5.36	911.04
+ 50			7.4	11.2
3			7.1	11.5
+ 50			7.3	11.3
T.P.	4.21	915.00	7.82	910.79
4			3.8	11.2
+ 50			4.2	10.8
5			4.4	10.6
+ 50			4.5	10.5
+ 58	18" x 30" Conc.		4.5	10.5
Profile Ditch Lt.				

(Profile Drive on left)

$\frac{3.0}{100}$ $\frac{3.0}{70}$ $\frac{3.5}{50}$ $\frac{6.0}{26}$ $\frac{6.9}{11}$ $\frac{6.7}{6.5}$ $\frac{5.8}{16}$ $\frac{4.0}{29}$ $\frac{2.2}{55}$ $\frac{2.2}{61}$

$\frac{2.5}{100}$ $\frac{2.5}{60}$ $\frac{3.3}{42}$ $\frac{3.2}{37}$ $\frac{5.6}{29}$ $\frac{6.6}{12}$ $\frac{6.5}{6.3}$ $\frac{4.6}{11}$ $\frac{3.6}{37}$ $\frac{2.7}{58}$ $\frac{2.3}{63}$

$\frac{2.4}{100}$ $\frac{3.6}{65}$ $\frac{3.2}{49}$ $\frac{2.7}{32}$ $\frac{6.2}{24}$ $\frac{6.3}{17}$ $\frac{6.1}{6.0}$ $\frac{4.7}{12}$ $\frac{3.6}{33}$ $\frac{2.5}{47}$ $\frac{2.3}{72}$

$\frac{2.8}{100}$ $\frac{2.7}{59}$ $\frac{2.8}{43}$ $\frac{3.6}{32}$ $\frac{6.7}{22.18}$ $\frac{6.1}{15}$ $\frac{5.8}{19}$ $\frac{4.2}{31}$ $\frac{2.9}{47}$ $\frac{2.7}{67}$ $\frac{2.3}{100}$

$\frac{4.5}{100}$ $\frac{4.7}{55}$ $\frac{5.2}{34}$ $\frac{6.5}{28}$ $\frac{9.1}{22.18}$ $\frac{8.0}{15}$ $\frac{7.8}{7.4}$ $\frac{9.0}{13}$ $\frac{5.0}{17.21}$ $\frac{4.2}{29}$ $\frac{4.2}{86}$

$\frac{4.2}{100}$ $\frac{4.6}{73}$ $\frac{4.4}{50}$ $\frac{5.1}{47}$ $\frac{5.1}{28}$ $\frac{9.2}{22.18}$ $\frac{7.6}{14}$ $\frac{7.7}{9.1}$ $\frac{9.3}{13}$ $\frac{5.5}{17.21}$ $\frac{5.6}{30}$ $\frac{5.1}{40}$ $\frac{5.7}{60}$ $\frac{6.4}{86}$ $\frac{6.4}{100}$

$\frac{4.9}{100}$ $\frac{5.6}{67}$ $\frac{5.2}{45}$ $\frac{5.3}{30}$ $\frac{9.6}{22.18}$ $\frac{7.9}{13}$ $\frac{7.9}{7.3}$ $\frac{9.6}{12}$ $\frac{6.9}{17.21}$ $\frac{6.9}{26}$ $\frac{6.9}{35}$ $\frac{7.0}{86}$ $\frac{7.5}{100}$

$\frac{2.6}{100}$ $\frac{2.8}{50}$ $\frac{3.2}{28}$ $\frac{6.0}{21.17}$ $\frac{4.3}{13}$ $\frac{4.0}{3.8}$ $\frac{6.1}{12}$ $\frac{4.1}{17.21}$ $\frac{4.0}{26}$ $\frac{4.0}{33}$ $\frac{4.5}{50}$ $\frac{4.5}{100}$

$\frac{3.2}{100}$ $\frac{3.2}{85}$ $\frac{3.9}{66}$ $\frac{4.2}{48}$ $\frac{4.5}{26}$ $\frac{6.6}{22.18}$ $\frac{4.8}{13}$ $\frac{4.7}{4.2}$ $\frac{6.7}{12}$ $\frac{4.7}{18.22.25}$ $\frac{4.7}{32}$ $\frac{5.0}{35}$ $\frac{5.1}{52}$ $\frac{4.7}{100}$

$\frac{5.1}{100}$ $\frac{5.0}{67}$ $\frac{5.2}{37}$ $\frac{5.0}{26}$ $\frac{6.7}{21.17}$ $\frac{5.1}{13}$ $\frac{5.0}{4.4}$ $\frac{6.8}{13}$ $\frac{5.0}{17.21}$ $\frac{5.0}{20}$ $\frac{5.1}{34}$ $\frac{5.1}{47}$ $\frac{5.7}{60}$ $\frac{5.7}{100}$

$\frac{5.0}{100}$ $\frac{5.0}{58}$ $\frac{6.1}{41}$ $\frac{6.3}{24}$ $\frac{7.0}{21.18}$ $\frac{5.1}{13}$ $\frac{5.1}{4.5}$ $\frac{7.1}{13}$ $\frac{6.0}{16.20}$ $\frac{6.2}{23}$ $\frac{5.6}{30}$ $\frac{5.4}{60}$ $\frac{5.4}{100}$

$\frac{5.1}{100}$ $\frac{5.0}{66}$ $\frac{5.0}{52}$ $\frac{5.8}{47}$ $\frac{6.0}{27}$ $\frac{7.2}{22}$ $\frac{7.1}{16}$ $\frac{7.20}{16}$ $\frac{5.2}{14}$ $\frac{5.0}{4.5}$ $\frac{7.40}{13}$ $\frac{7.1}{16}$ $\frac{6.9}{20}$ $\frac{6.0}{24}$ $\frac{5.3}{33}$ $\frac{5.8}{36}$ $\frac{5.7}{63}$ $\frac{5.5}{100}$

$\frac{7.5}{200}$ $\frac{7.5}{141}$ $\frac{7.4}{100}$ $\frac{7.1}{73}$ $\frac{7.3}{46}$ $\frac{7.2}{20}$

Sta.	+	π	-	Elev.
------	---	-------	---	-------

915.00

6			4.5	10.5
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+50

			4.6	10.4
--	--	--	-----	------

7			4.6	10.4
---	--	--	-----	------

T.R.	2.31	912.60	4.71	910.29
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B.M.			9.92	902.68
------	--	--	------	--------

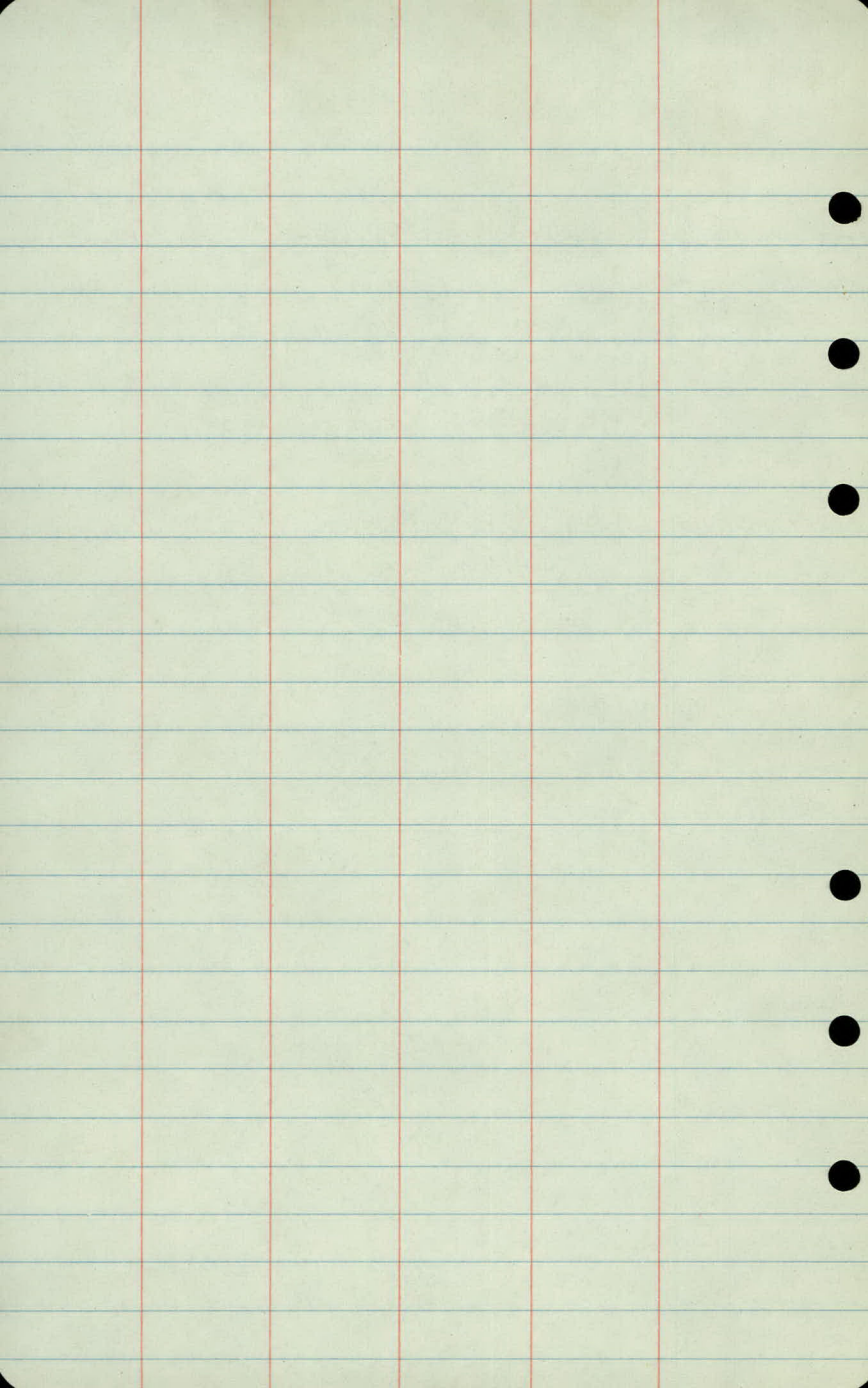
902.64

$\frac{5.2}{100}$	$\frac{5.1}{61}$	$\frac{4.9}{26}$	$\frac{7.0}{22-18}$	$\frac{5.0}{13}$	$\frac{5.0}{4.5}$	$\frac{5.0}{13}$	$\frac{7.1}{18-21}$	$\frac{5.7}{24}$	$\frac{5.5}{35}$	$\frac{5.3}{46}$	$\frac{5.4}{64}$	$\frac{5.4}{100}$
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$\frac{4.7}{100}$	$\frac{5.0}{55}$	$\frac{5.2}{25}$	$\frac{7.1}{21-17}$	$\frac{5.0}{13}$	$\frac{5.2}{4.6}$	$\frac{7.2}{13}$	$\frac{5.7}{17-21}$	$\frac{5.2}{24}$	$\frac{5.0}{34}$	$\frac{5.1}{60}$	$\frac{5.1}{100}$
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$\frac{5.3}{100}$	$\frac{5.5}{61}$	$\frac{5.6}{24}$	$\frac{7.2}{21-17}$	$\frac{5.2}{13}$	$\frac{5.2}{4.6}$	$\frac{7.1}{13}$	$\frac{5.7}{17-22}$	$\frac{5.1}{24}$	$\frac{5.0}{45}$	$\frac{5.0}{60}$	$\frac{5.0}{100}$
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Drill Hole Edgerton



11
TOPOGRAPHY

EDGERTON

From Ctn. Sec. 32 No. to Soo Line Bridge

+50

3

Ctr. Track 63.5

+83 End Ctr. Island

+50

+55 Ctr. Face Pier

+36 Ctr. Face Pier

111 T.P. 24

2 Ctr. Track - 46.5

+04 Beg. Ctr. Island 11.3

+87 Rye Tie Fe.

+50

+56 Clump Ltee 50
+54 Fe Cor 44

1

?

+20 Cor. Ho	31.5
+09 T.P.	24
+05 B.E.	42
+00 Ash	38

+95 Cor. Ho	60
+88 Ash	43

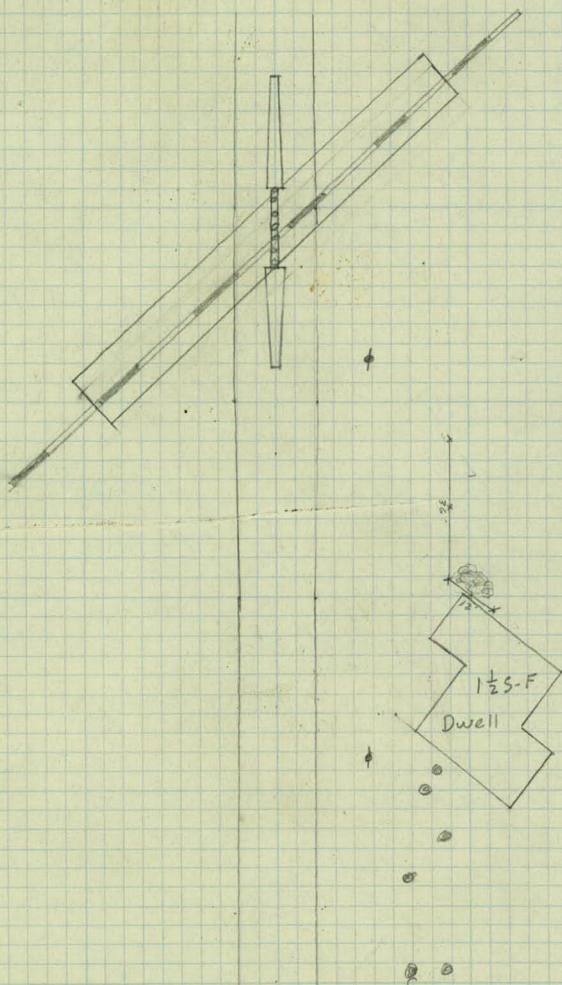
+77 Ash	34
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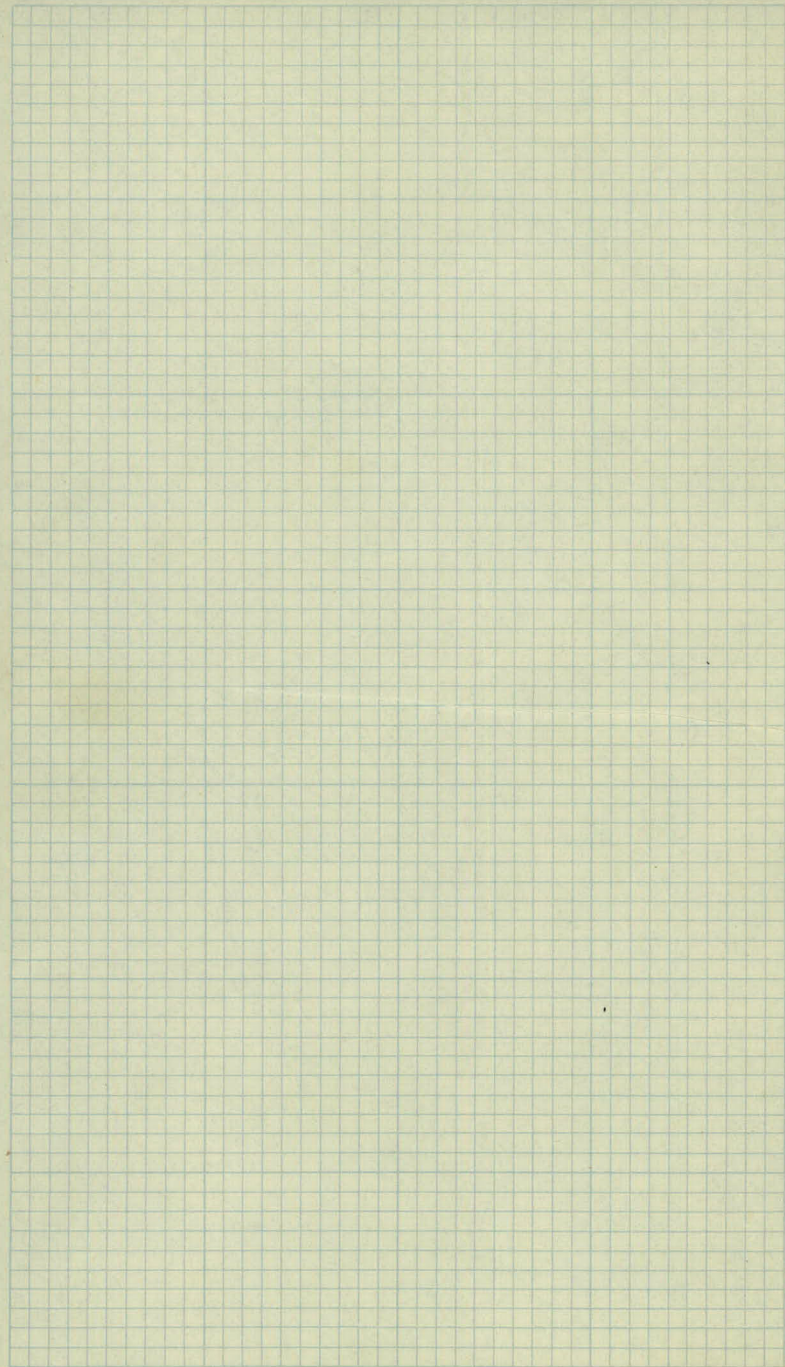
+50

+54 2E lms - 34 - 44

0+00

24 Elm 50





Cross Sections

EDGERTON

from Mississippi No

Sta	+	π	-	E/cv.
B.M.	0.48	903.12		902.64
0+00 = 0+50.05 Mississippi			5.36	97.76
+50			7.84	95.28
1			10.34	92.78
+50			12.78	90.34
T.P.	0.87	891.48	12.51	890.61
2			3.30	88.18
+50			4.3	87.18
3			5.82	85.66
+50			6.32	85.16
T.P.	12.72	903.72	0.48	891.00
B.M.	10.38	913.02	1.12	902.60 (902.64)
T.P.	5.87	917.14	1.75	911.27
0+00				97.76
+50				95.28
1				92.78

$$\begin{array}{r} 5.44 \quad 5.86.3 \quad 4.3 \quad 1.9 \\ 5.36 \quad 10 \quad 13 \quad 14 \quad 17 \quad 22 \end{array}$$

$$\begin{array}{r} 7.92 \quad 8.2 \quad 8.7 \quad 6.8.2.6 \\ 7.84 \quad 10 \quad 12 \quad 14 \quad 17 \quad 25 \end{array}$$

$$\begin{array}{r} 10.45 \quad 10.5 \quad 11.0 \quad 9.2 \quad 3.8 \\ 10.34 \quad 10 \quad 12 \quad 14 \quad 17 \quad 26 \end{array}$$

$$\begin{array}{r} 12.95 \quad 13.1 \quad 13.7 \quad 11.3 \quad 5.9 \\ 12.78 \quad 10 \quad 12 \quad 14 \quad 18 \quad 26 \end{array}$$

$$\begin{array}{r} 3.36 \quad 3.51 \quad 3.3 \quad 2.5 \\ 3.30 \quad 11 \quad 12 \quad 17 \quad 18 \end{array}$$

$$\begin{array}{r} 4.55 \quad 5.05 \quad 5.08 \quad 5.22 \quad 4.75 \quad 2.1 \\ 4.3 \quad 2 \quad 2 \quad 13 \quad 15 \quad 15 \quad 22 \end{array}$$

$$\begin{array}{r} 6.06 \quad 5.9 \quad 6.0 \quad 6.4 \quad 4.1 \quad 1.3 \\ 5.82 \quad 11 \quad 12 \quad 15 \quad 16.18 \quad 21 \quad 26 \end{array}$$

$$\begin{array}{r} 6.70 \quad 6.6 \quad 6.4 \quad 7.0 \quad 4.7 \\ 6.32 \quad 12 \quad 13 \quad 16 \quad 20.25 \quad 27 \end{array}$$

-19.38

-21.86

-24.36

10.5	16.1	16.6	12.9	10.2	9.5	10.8	11.3
8.9	3.3	2.8	6.5	9.2	9.9	8.8	8.1
36	39	55	65	77	80	85	100
14.3	17.3	18.2	17.9	17.5			
7.6	4.6	3.7	4.0	4.4			
38	40	72	94	100			
15.5	18.1	19.6	20.7	20.8			
8.9	6.3	4.8	3.7	3.6			
37	40	56	88	100			

Sta. + π - Elev.

917.14

1+50

90.34

2

88.18

T.P.

1.19

909.47

8.86

908.28

+50

87.18

3

85.66

+50

85.16

-26.80

18.1	19.4	20.7	22.2	22.4
8.7	7.4	6.1	4.6	4.4
38	51	81	92	100

-28.96

16.5	20.1	21.2	21.7
12.5	8.9	7.8	7.3
38	63	84	100

-22.29

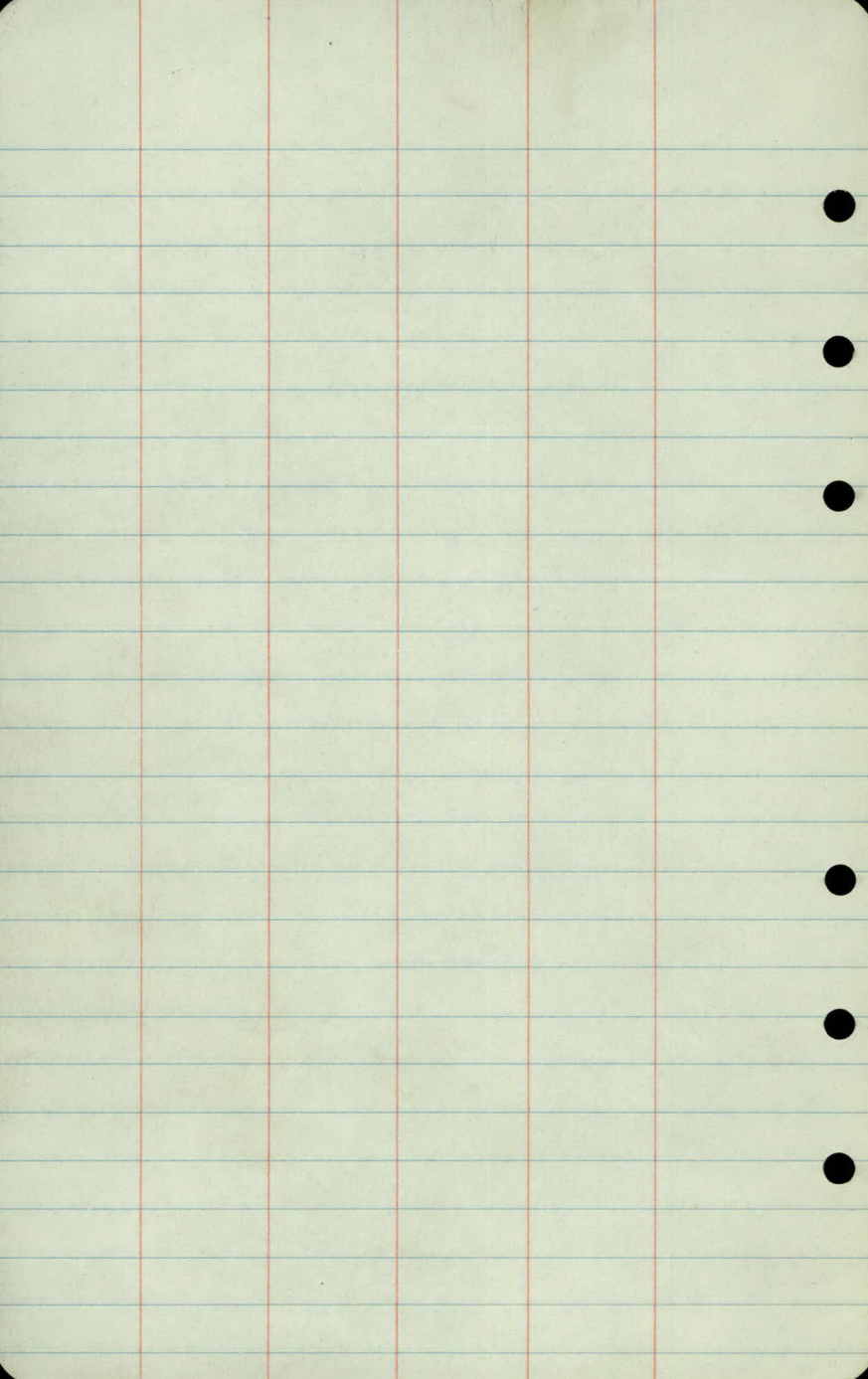
11.6	11.5	13.3	18.8	20.0
10.7	10.8	9.0	3.5	2.3
36	47	66	80	86

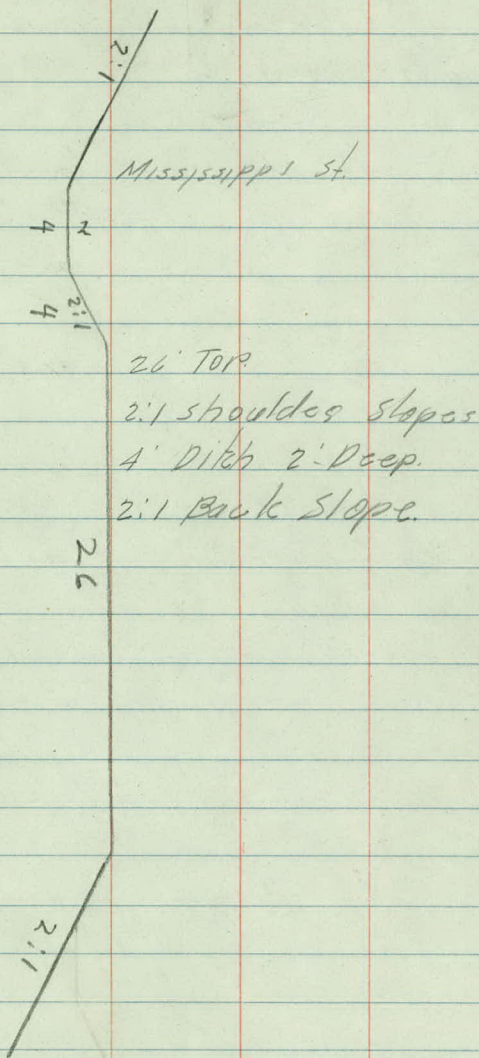
-23.81

17.9	18.3	19.19	19.2	18.3	17.2	15.9	15.7	17.8
5.9	5.5	4.62	4.60	5.5	6.6	7.9	8.1	6.6
45	55	57	64	68	75	81	89	100

-24.31

12.8	12.8	14.6	16.9	18.3
11.5	11.5	9.7	7.4	6.0
40	50	74	85	100





Sta	+	π	-	Grade
B.M.	15.67	918.31		(902.64)

0 +50.5 = 4 Edgerton St.

+64	97.5
-----	------

+68	97.5
-----	------

+85	98.3
-----	------

+89	98.6
-----	------

1	99.9
---	------

+66	99.9
-----	------

+32	01.9
-----	------

+36	02.2
-----	------

+41	02.6
-----	------

+57	03.8
-----	------

7-2-40

Gr. Rod

Lt

R

Rt.

Drill hole in Pav. of 60

19.7

530/5.7
41.9.0

46
41.5.1

18.9

16.4

480/4.9
41.5

100
44.4

sta	+	π	-	Grade
-----	---	-------	---	-------

918.31

1	+74			051
---	-----	--	--	-----

	+84			059
--	-----	--	--	-----

2				070
---	--	--	--	-----

	+30			086
--	-----	--	--	-----

	+50			095
--	-----	--	--	-----

TP	363	915.15	679	911.52
----	-----	--------	-----	--------

3				10.3
---	--	--	--	------

	+50			10.50
--	-----	--	--	-------

4				10.7
				10.3

	+50			10.9
				10.1

5				099
---	--	--	--	-----

	+50			09.8
--	-----	--	--	------

Gr. Rod

Lt

R

Rt

13.2

$$390' / \frac{6.2}{17.0}$$

$$\frac{83}{14.9}$$

11.3

$$386' / \frac{45}{16.8}$$

$$\frac{79}{13.4}$$

9.7

$$33.0' / \frac{57}{14.0}$$

$$\frac{73}{12.6}$$

8.8

$$32.6' / \frac{50}{12.8}$$

$$\frac{70}{11.8}$$

4.9

$$30.8' / \frac{20}{12.9}$$

$$\frac{36}{11.3}$$

$$\frac{19}{130/31.0'}$$

4.6

$$30.2' / \frac{1.8}{12.6}$$

$$\frac{38}{10.8}$$

$$\frac{24}{11.2/27.4'}$$

4.9

$$28.4' / \frac{13.2}{11.7}$$

$$\frac{39}{11.0}$$

$$\frac{39}{11.0/27.0'}$$

5.1

$$25.8' / \frac{11.7}{10.4}$$

$$\frac{43}{10.8}$$

$$\frac{48}{10.3/25.6'}$$

5.3

$$25.2' / \frac{5.2}{10.1}$$

$$\frac{46}{10.7}$$

$$\frac{55}{10.8/24.6'}$$

5.4

$$22.8' / \frac{6.5}{10.9}$$

$$\frac{47}{10.7}$$

$$\frac{60}{10.9/22.8'}$$

Sta.	+	π 915/15	-	Grade	
6	+58			09.8	
6				09.7	
	+50			09.7	
7		913 .09		09.8	
T.P.	4.04	913.13	6.06	909.09	
B.M.	14.88	917.52	10.45	902.68	902.64
B.M.			4.21	908.88	.88

Grade Change

4	+00			10.7	
	+50			10.9	

Gr. Rod

Lt

R

Rt

5.4

$$\frac{250}{100} \frac{54}{100}$$

$$\frac{46}{108}$$

$$\frac{58}{1016} / 24.2$$

5.5

$$\frac{46}{109}$$

5.5

$$\frac{254}{101} \frac{54}{101}$$

$$\frac{47}{108}$$

$$\frac{58}{1017} / 24.4$$

5.4

$$\frac{242}{1016} \frac{58}{1016}$$

$$\frac{48}{106}$$

$$\frac{59}{1014} / 24.2$$

Drill Hole in Pav.

Top Stone End Rubble Gutter

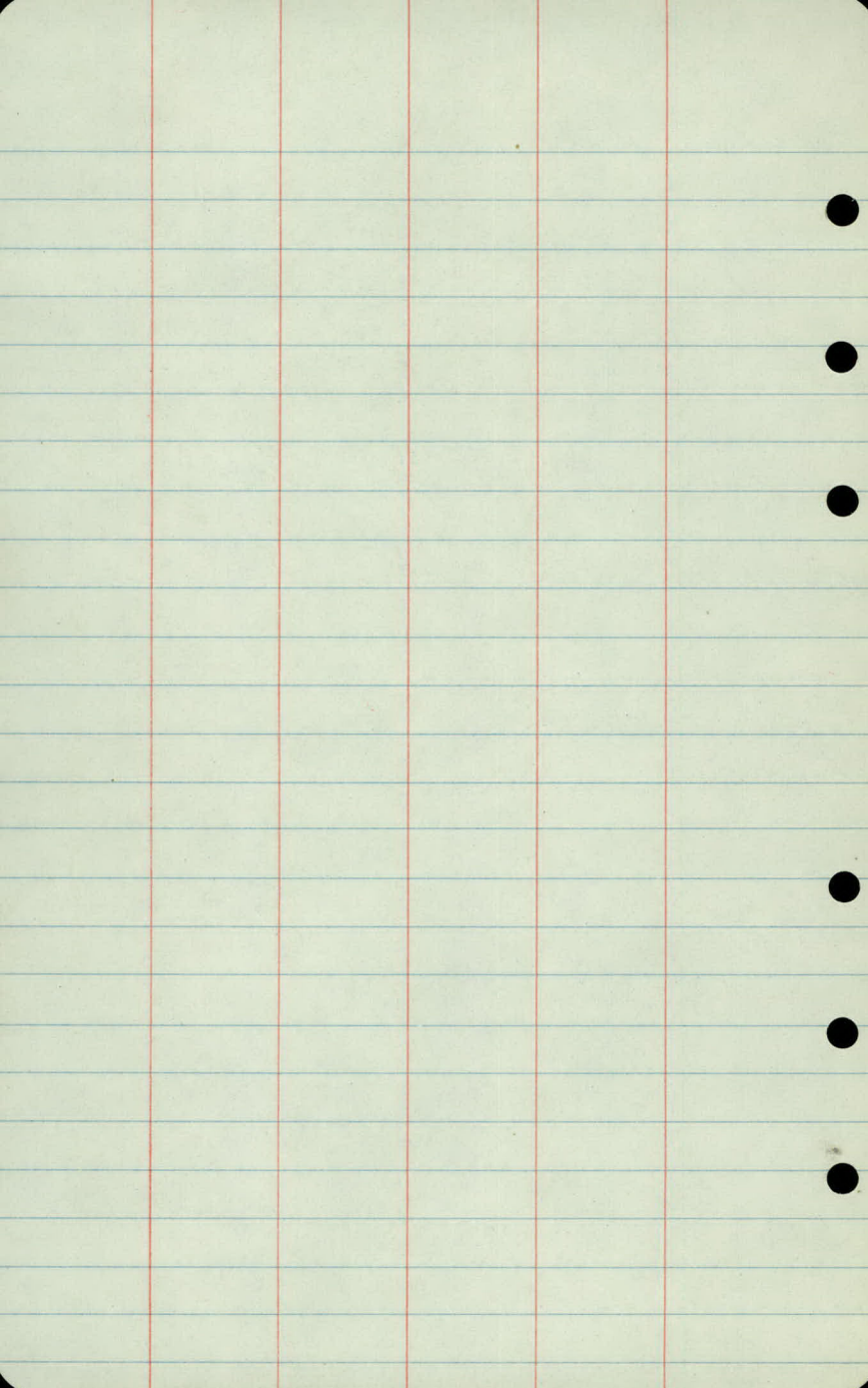
6.8

$$\frac{272}{111} \frac{51}{111}$$

$$\frac{63}{105}$$

$$\frac{64}{107} / 25.8$$

6.6



Gutter Levels

Edgerton St.

pt. side

Sta	+	π	-	Elev	Cutter Dist
B.M.	2.65	905.29			902.64

2
+00 = Edgertown
Mississippiist.

+55			11.1	94.2	14.2
-----	--	--	------	------	------

			13.2	92.1	14.0
--	--	--	------	------	------

T.P.	2.65	895.08	12.86	892.43	
------	------	--------	-------	--------	--

+50			5.7	89.4	14.2
-----	--	--	-----	------	------

2			7.4	87.7	15.0
---	--	--	-----	------	------

+45			8.7	86.4	17.0
-----	--	--	-----	------	------

T.P.	12.14	905.51	1.71	893.37	
------	-------	--------	------	--------	--

B.M.			2.87	902.64	
------	--	--	------	--------	--

7-2-40

lt.

ft.

pt.

Top drill hole in pav.

Slope stakes

Sta	+	π	-	Ditch Grade R/L
B.M.	10.04	918.92		(908.88)
0	+55			94.2
T.P.	5.00	915.97	7.95	910.91
1	+20			91.0
	+50			89.4
2				87.7
	+20			87.0
	+45			86.4
T.P.	5.30	917.51	3.76	912.21
B.M.			14.88	902.63 (902.64)

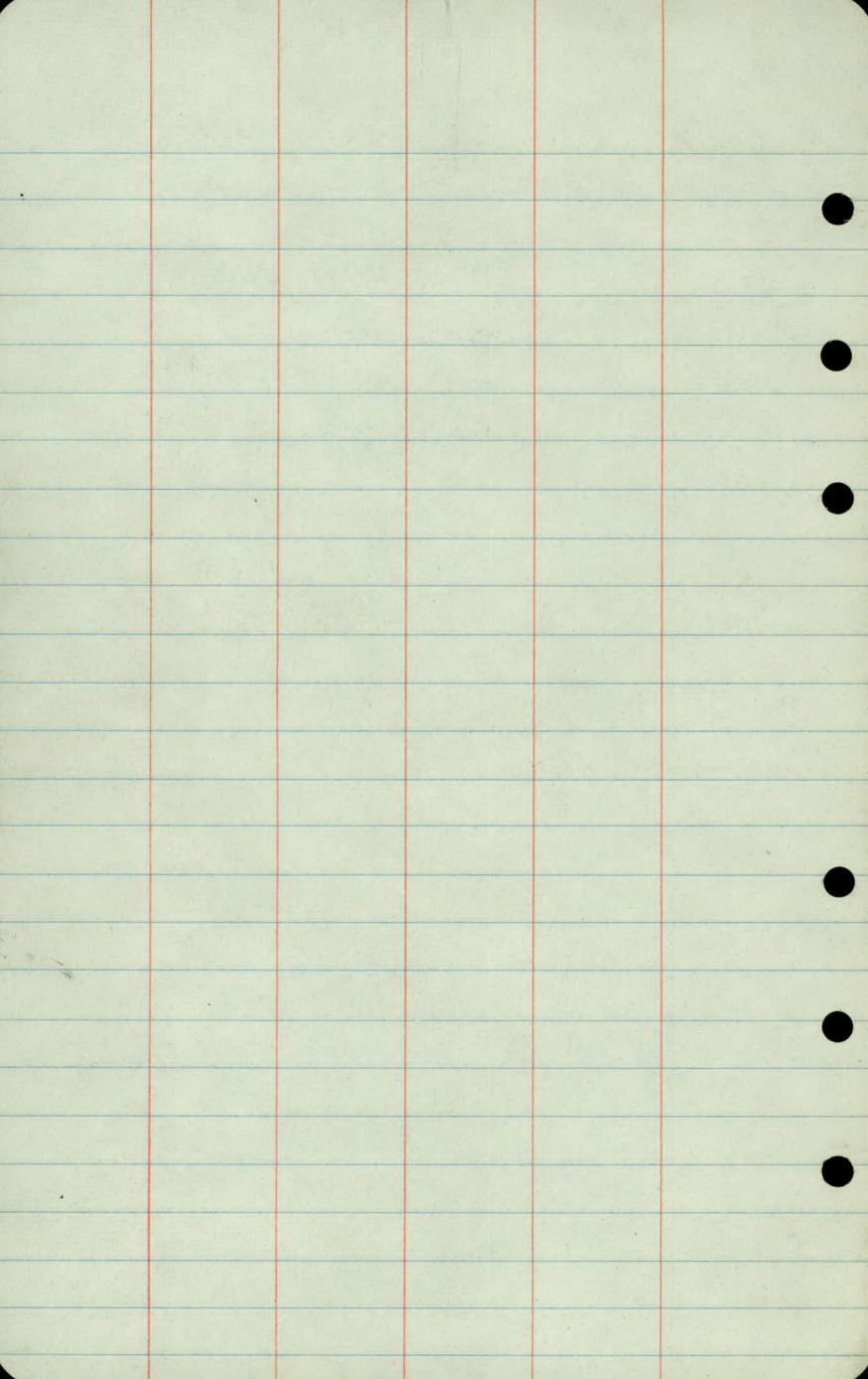
7-5-90

Grade Rod Ditch 0.0
 & Dist 2:1 3:1

Top End Stone Gutter. From Mississippi slope stakes.

24.7	14.0	$\frac{59}{+188/81.6}$	$\frac{56}{+191/71.3}$	$\frac{24.7}{50}$ 18.8
25.0	14.0	$\frac{45}{+20.5/55.0}$	$\frac{31}{+21.9/49.7}$	
26.6	14.0	$\frac{6.0}{+20.6/55.2}$	$\frac{3.0}{+21.6/}$	
28.3	15.0	$\frac{8.1}{+20.2/55.4}$	$\frac{7.0}{+21.3/78.9}$	
29.0	16.0	$\frac{12.2}{+20.3/49.6}$	$\frac{8.2}{+20.8/78.4}$	
29.6	17.0			

Top Drill hole in Pav 0+00



X sections

Mississippi St.
North Side

Sta 0700 to Sta 10400

7/17/42

HAW

AM

L.C

Sta	+	Δ	-	Elev
B.M	9.97	912.61		902.64
0+00				03.3
+50				04.2
+64				04.8
+83				05.9
1+00				07.0
+30				09.2
+50				09.5
+64.37	P.C			10.0
T.P.	4.70	915.32	1.99	910.12
1+30				6.1
+50				
+64				
2+00				10.6

L4.

£

Top Drill/hole £ Edgerton Str 40100

$$\frac{102}{28} \quad \frac{96}{13} \quad 9.3$$

$$\frac{128}{41} \quad \frac{118}{31} \quad \frac{123}{31} \quad \frac{121}{27} \quad \frac{111}{26} \quad \frac{92}{11} \quad 8.4$$

$$\frac{135}{50} \quad \frac{143}{44} \quad \frac{110}{35} \quad \frac{119}{21} \quad \frac{110}{14} \quad \frac{90}{14} \quad 9.8$$

$$\frac{111}{50} \quad \frac{87}{44} \quad \frac{41}{34} \quad \frac{44}{31} \quad \frac{65}{26} \quad \frac{110}{25} \quad \frac{104}{13} \quad \frac{91}{8} \quad 6.7$$

$$\frac{20}{50} \quad \frac{120}{42} \quad \frac{120}{31} \quad \frac{00}{28} \quad \frac{46}{20} \quad \frac{98}{18} \quad \frac{103}{12} \quad \frac{53}{7} \quad 5.6$$

$$\frac{1.6}{23} \quad \frac{91}{19} \quad \frac{87}{10} \quad \frac{3.9}{3} \quad 3.4$$

$$\frac{81}{29} \quad \frac{83}{18} \quad \frac{31}{13} \quad 3.1$$

$$\frac{7.9}{32} \quad \frac{7.8}{23} \quad \frac{24}{17} \quad 2.6$$

$$\frac{1.9}{50} \quad \frac{1.9}{37} \quad (6.1)$$

$$\frac{2.4}{50} \quad \frac{2.4}{40} \quad \frac{31}{33} \quad (5.8)$$

$$\frac{2.4}{50} \quad \frac{3.0}{34} \quad (5.3)$$

$$\frac{1.8}{50} \quad \frac{2.0}{35}$$

$$\frac{9.7}{33} \quad \frac{9.2}{25} \quad \frac{4.9}{18} \quad 4.7$$

Sta	+	π	-	Elev
		915.32		
2+50				11.4
3				11.4
+50				11.2
4				11.1
+50				10.7
5				10.4
+47		18" X 31 Conc		10.5
6				10.4
+50				10.3
7				10.3
+16	21"	Side Drain		07.72
+36	21"	Side Drain		07.62

41.

#

$$\frac{1.6}{50} \quad \frac{2.4}{32}$$

$$\frac{8.7}{30} \quad \frac{7.8}{22} \quad \frac{4.0}{16} \quad 3.9$$

$$\frac{1.5}{50} \quad \frac{1.9}{36} \quad \frac{8.2}{32} \quad \frac{7.5}{24} \quad \frac{3.8}{19} \quad \frac{3.2}{16} \quad \frac{4.3}{13} \quad 3.9$$

$$\frac{2.2}{50} \quad \frac{2.2}{47} \quad \frac{2.3}{31} \quad \frac{7.3}{28} \quad \frac{6.6}{22} \quad \frac{4.0}{18} \quad \frac{3.8}{14} \quad \frac{4.6}{13} \quad 4.1$$

$$\frac{3.4}{50} \quad \frac{3.8}{34} \quad \frac{4.4}{27} \quad \frac{8.2}{22} \quad \frac{8.2}{18} \quad \frac{4.9}{14} \quad 4.2$$

$$\frac{4.6}{50} \quad \frac{5.0}{26} \quad \frac{7.7}{22} \quad \frac{7.7}{18} \quad \frac{5.2}{13} \quad 4.6$$

$$\frac{4.8}{50} \quad \frac{5.5}{25} \quad \frac{7.5}{21-18} \quad \frac{5.3}{13} \quad 4.9$$

$$\frac{5.1}{50} \quad \frac{6.3}{26} \quad \frac{7.4}{21} \quad \frac{7.54}{INV} \quad \frac{5.4}{13} \quad 4.8$$

907.56

776
INV

$$\frac{5.5}{50} \quad \frac{5.4}{26} \quad \frac{7.4}{21} \quad \frac{7.3}{17} \quad \frac{5.4}{13} \quad 4.9$$

$$\frac{5.5}{50} \quad \frac{5.8}{24} \quad \frac{7.7}{22-} \quad \frac{7.7}{18} \quad \frac{5.3}{13} \quad 5.0$$

$$\frac{4.9}{50} \quad \frac{6.1}{28} \quad \frac{6.3}{27} \quad \frac{7.3}{18} \quad \frac{5.5}{14} \quad 5.0$$

$$\frac{7.60}{INV}$$

$$\frac{7.70}{INV}$$

Sta	+	X	-	Elev
-----	---	---	---	------

		915.32		
--	--	--------	--	--

7+50				10.3
------	--	--	--	------

8				10.4
---	--	--	--	------

+15		15" Side Drain		
-----	--	----------------	--	--

+36		15" Side Drain		
-----	--	----------------	--	--

+50				10.4
-----	--	--	--	------

9				10.3
---	--	--	--	------

+50				10.3
-----	--	--	--	------

10				10.3
----	--	--	--	------

T.P.	1.39	912.06	4.65	910.67
------	------	--------	------	--------

B.M.			7.41	902.65 902.64
------	--	--	------	---------------

Kt.

£

$$\frac{5.9}{50} \quad \frac{5.8}{24} \quad \frac{7.4}{22} \quad \frac{7.3}{17} \quad \frac{5.6}{14} \quad 5.0$$

$$\frac{6.2}{50} \quad \frac{6.1}{25} \quad \frac{7.6}{21} \quad \frac{7.3}{17} \quad \frac{5.5}{14} \quad 4.9$$

$$907.57$$

$$\frac{7.75}{Inv.}$$

$$907.57$$

$$\frac{7.75}{Inv.}$$

$$\frac{5.8}{50} \quad \frac{6.6}{23} \quad \frac{7.3}{21} \quad \frac{7.5}{17} \quad \frac{5.3}{13} \quad 4.9$$

$$\frac{6.5}{50} \quad \frac{6.2}{23} \quad \frac{7.3}{21} \quad \frac{7.3}{18} \quad \frac{5.6}{13} \quad 5.0$$

$$\frac{6.3}{50} \quad \frac{6.4}{23} \quad \frac{7.3}{21-18} \quad \frac{5.7}{14} \quad 5.0$$

$$\frac{6.6}{50} \quad \frac{6.2}{23} \quad \frac{7.0}{21-18} \quad \frac{5.6}{14} \quad 5.0$$

Top Drill hole Edgerton Str.

