

Book-13, 25.13

OFFICE OF COUNTY ENGINEER
RAMSEY CO. MINN.

----- *Plan* ----- Survey

----- COUNTY ROAD "F" -----

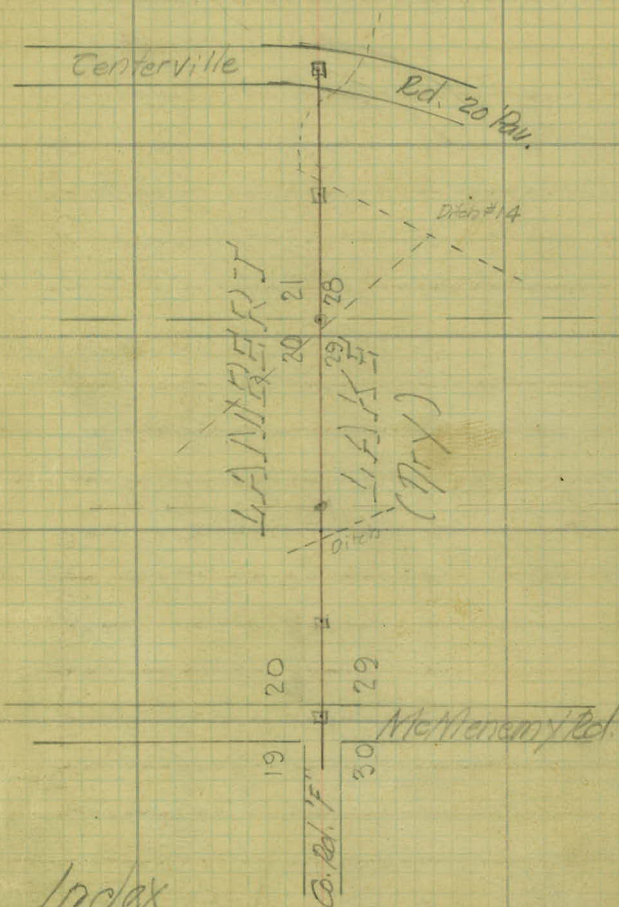
From *McMenemy St* To *Centerville Rd.*

Road Acc't. No. -----

Date Filed *1935* -----

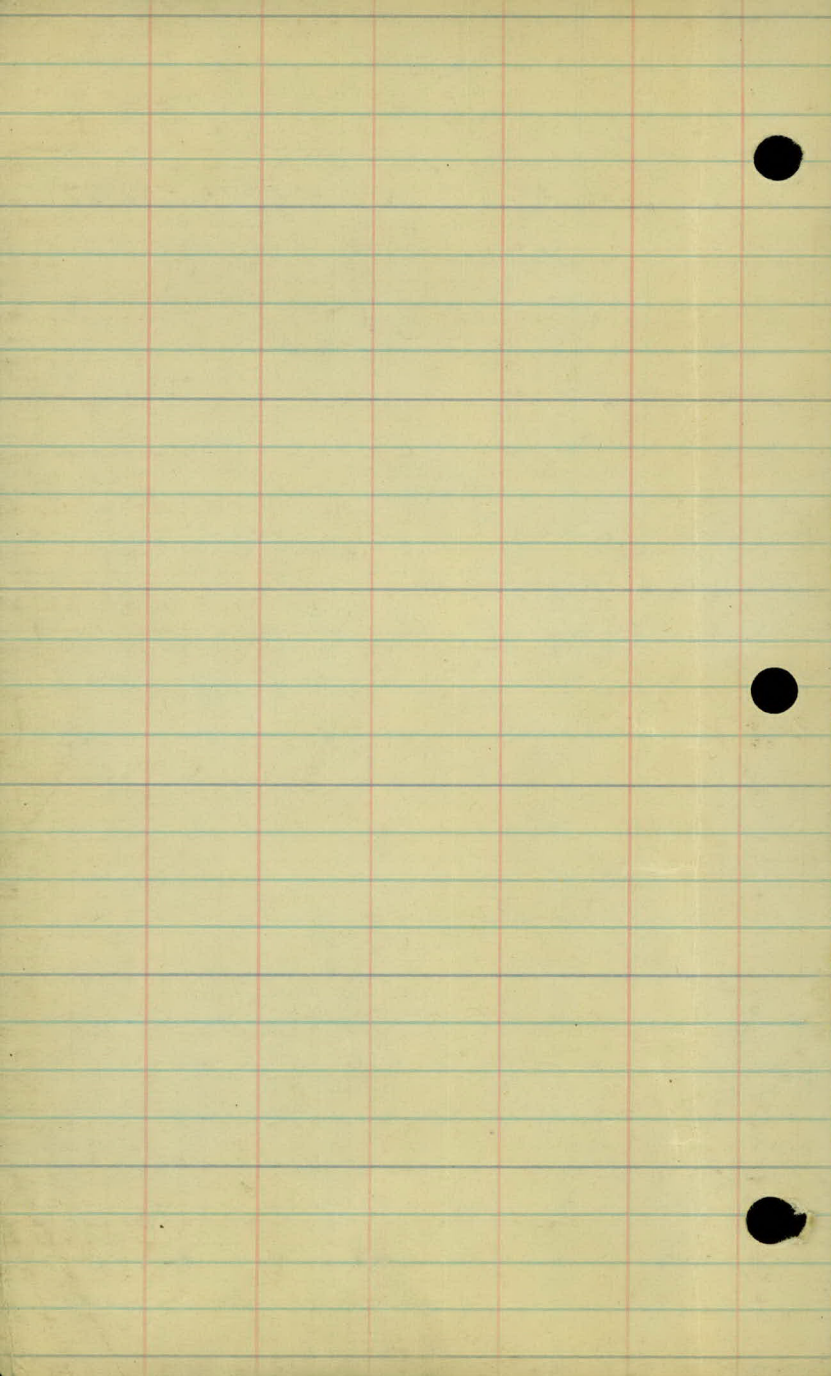
File -----

Plan Survey
County Road "F"
200' West McMenamy to Centerville Rd.



Index	
Alignment	P. 1-3
Topography	P. 4-16
Cross Sections	P. 17-36
Bench Levels	P. 37-40
Recommend.	41

W. H. Carlson
Sept. 10, 1935



1

alignment

Station Point Lt. Δ Rt.

73+48.3

Mon.

$0^{\circ}24'$

71+46.47

68+00

P.O.T.

61+02.95

Rt.
Mon.

$0^{\circ}13'$

57+00

P.O.T.

Mon.

± Rice

0+00 = ± Hodgson Rd.

W.H.C.

2

A.A.W.

8/29/35

K.A.

L.B.H.

Large @ 40.67

□ □ □

□ 33' □ 66' □

20

29

12' Oak

33.2

30.65

2 Ms/Mon cm.

33'

33.45

T.P.

19

30

T.P.

25.19

25.50

T.P.

Stone Mon.

Station Point Lt. Δ Rt.

140+01.49 Mon.

139+68.49 P.O.T. Iron Mon.

139+42.02 P.O.T.

126+81.22

121+81.3 P.O.T.

113+60.18 P.T. 0°14'

97+47.50 P.O.T.

87+31.7 old Stake

Centerville Rd.
20' Conc. Pave.

Stone Mason

2" x 2" Hub

+ Top Large Blue Rock

2" x 2" Hub

3 Nails top Fence Post

24" Elm
Top Edge R.R.
Spike

2" x 2" Hub

2.24
0 R.R.

21

20

29

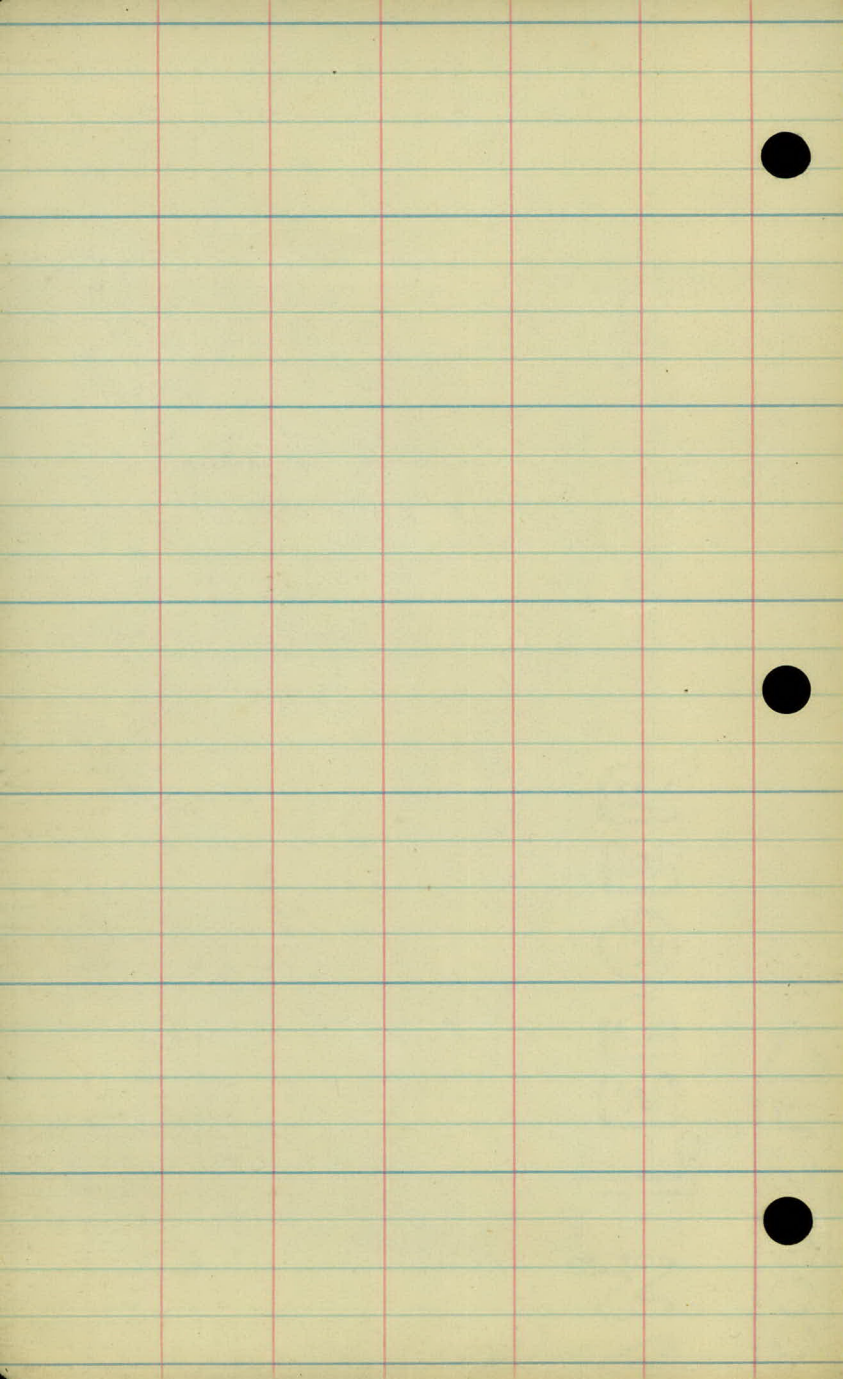
93.21

86.89

53.51

28

65.00



Topography-

13' 8"
Road Bag
at lot.

58

13' 10'

57

14' 10'

56

17' 10'

55

17' 11'

54

W.H.O.
H.A.W.
K.A.
L.B.H.

5

9/5/35

+62-T.P. 20'
+50-Ent. Lt.

+06-T.P. 20'

Cult

20/7

X X X +21- Ferr. 39

+78-T.P. 20'
(B.M.)

X
X

65

64

63

62

61

10295-2 M³ Menemys.

+90- 18" x 44' C.M.
Fair.

+90 21' 17'
+70 = 16' 10'

60

16' 7'

59

13' 8'

Timber Marsh
 68
 110
 +60-12" Will 80'
 +55-12" Will 76'
 +48-8" Will 76'
 +40-Timber 66'

654-Timber
 0

+45-Timber 66'

Timber 87
 Marsh 100

Meadow

Timber 100'
 Marsh

Timber Marsh
 100'

+40-Timber 99

+36-F. Cor.
 +28-20" Oak 17'

+17

+80-1r. Sign 78'

+92

78'

21'

+85-T.P. 29'

+82-1r. Rd. 21'

+52-T.P. 22'

+14-T.P. 21'

72

71

70

69

68

67

66

Cultivated

F-0' Timber 0

Timber

F-1'

+84 Ent.

Timber 2-8" Oak Thick.

F-1

Timber 103

Cultivated.

+99- 6" Oak 2'
+98- 0" Oak - 3'

F-1'

F-0' Timber 60' 108' 100-110-114

F-00

Timber 106

160 Timber 66

79

78

77

76

75

74

73

7 Beg Doplars (Thick)
1" = 3"



Pasture

Pasture.

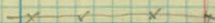
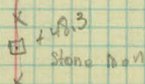
~~117-30 Oak - 31~~



+56-F. Cor. 6'

F. 41
100-70 Oak 58

+49-30 Oak - 37



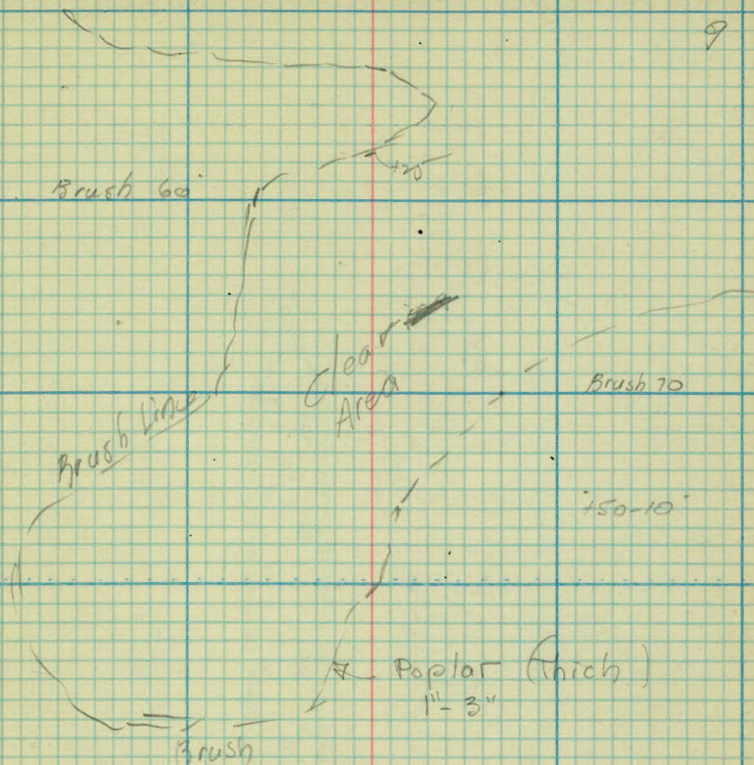
+01-F. Cor. 0'

95

94

93

92



Old Stake. 87431.7

Poplars 1" - 3"
(thick)

100

101

100

99

98

+81- £ Trail

97

96

Weeds.

+48-15' Pop 46

Small Brush

Some Wind Falls

Weeds

+55-6" Oak-10
+48-8" Will. 33'

Tail

+60-24" Elm. 87

98-14-Fea X-2

+76 Fern. 71'

+10-Fea 92'

+51-18" Elm 17'

+47-8" Elm 12'

+32-16" Tw Birch 50'

109

108

107

106

105

104

103

Poplar Brush &

Weeds.

WeedsRed low ground192-14th Wild Sp. 2'Small Brush
Scatt.Weeds.

116

115

114

+60.18 - P.H.

113

112

111

110

Poplar
Brush

Poplar Brush

Weeds

18-Fen X-L

Rock Bar

No Wires

End Swamp Sec
End Brush

Brush Thick

Small Poplars

" Willows

Cat Tails

(Rag Weed thick)

About
450

+600 } Ditch.
+500 }

Ditch

123

122

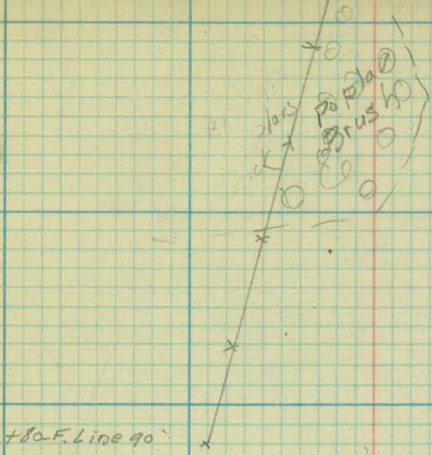
121

120

119

118

117



Sand Borrow
Here

Sand Bar

+75

Pop Brush

120

129

128

127

+81.22 Mon

126

125

124

Pitch 2 26

F-84

14

+50 - E Ditch 25'

F-95'

Weeds.
Cultivated

F-105'

E Ditch 35'

F-89'

(+85 - End of Poplars)
& Willows in Ditch

+36 - Ditch

Ditch full of
Large willows &
Poplars.

+64 - End Row 10'

+81 - F. Cor. 54'
E Ditch 68'

Large
oaks.

Row Oaks 46'

F-33'

Ridge

+90 - Fence

Poplar Brush

138

137

136

135

134

133

132

131

To Centerville Rd.

E-Ditch 65

Top Bank 188

+27 E Ditch 18

+16 Top Bank

E Ditch 95

E Ditch 120

E Ditch.

+22 A Pen. 51

Cult.

Weeds
Cult.

F-73'

141

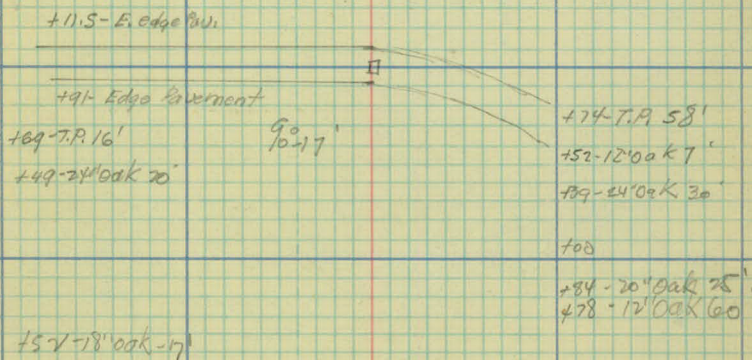
140

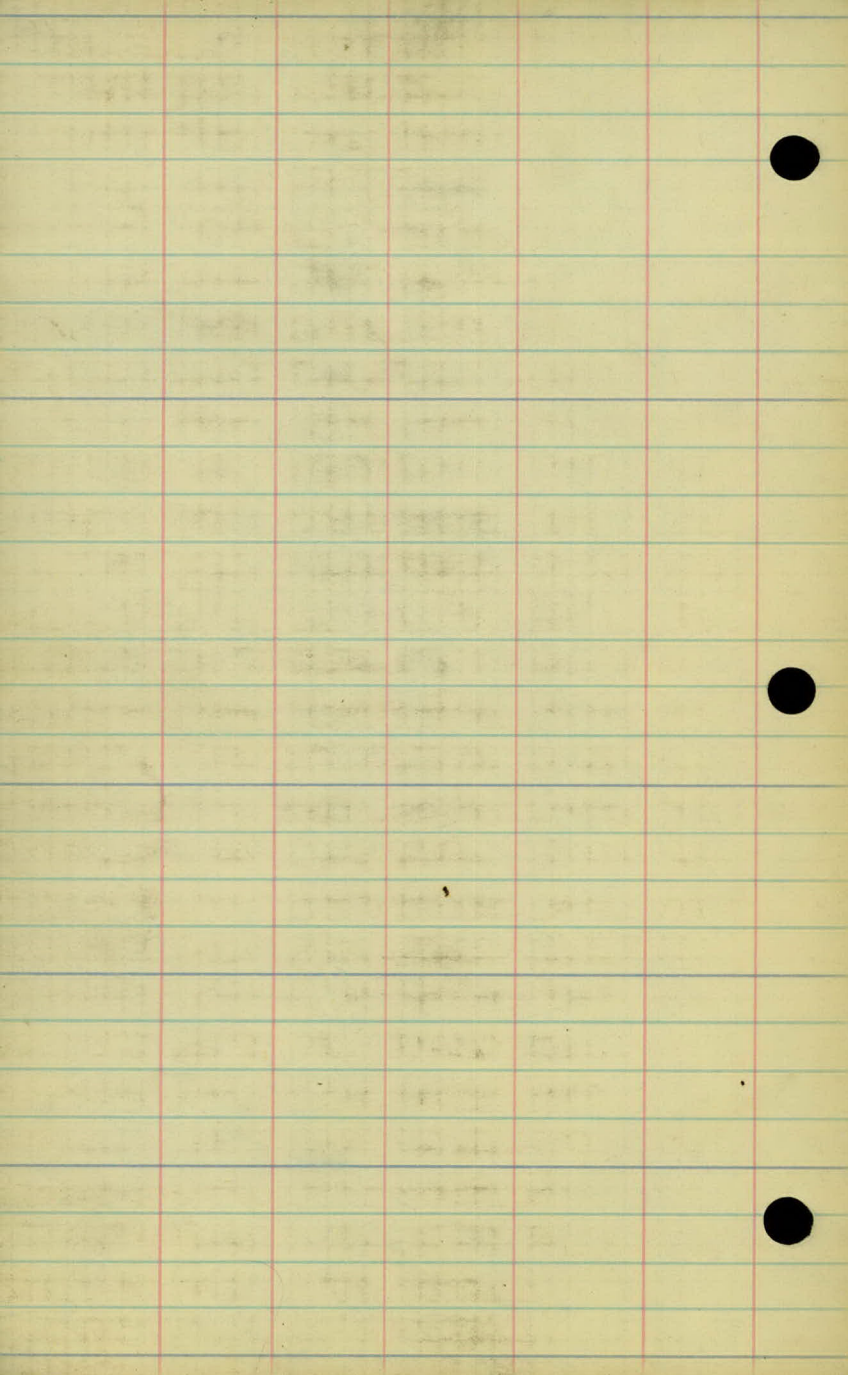
401.49- Stone Mors.

139

138

Notes: See Centerville
Proj. for Curve South





X-Sections.

Sta.	+	π	-	Elev.
B.M.	7.71	948.64		940.93
55 to				941.1
56 to				44.1
57 to				44.0
58 to 55				42.3
58				41.9
+40				40.7
<u>500 Revision 17</u>				
59				38.8
+50				37.2
60				35.6
+60				33.6
T.P.	3.58	938.58	13.64	935.00
60 to 60				33.6
+75				32.8

44.4 Lt. 2 Rt. 7.5/35 18
 Spike in R.P. 20' Lt. Sta. 54178

+3.3 +3.8 2.0 7.6 7.8 7.5
 50 35 32 73 17

8.0 7.0 7.1 1.5 +6.2 +5.0
 10 11 15 25 35 50

49.4

+4.3 2.9 5.2 4.6 4.5
 32 27 19 6

5.0 4.8 1.0 +6.7 +5.5
 9 15 21 31 55

45.0

+1.0 +0.7 4.6 5.0 4.6 4.6
 33 31 22 14 4

5.0 1.7 13.8 +2.5
 11 18 26 60

46.1

2.5 2.6 6.0 6.9 6.4 6.3
 32 22 17 13 6

7.0 6.2 3.1 3.6 3.6
 11 15 18 29 60

45.5

3.1 2.8 7.2 6.7 6.6
 50 22 13

7.3 6.7 4.4 4.8
 11 14 18 60

44.1

4.5 4.5 4.8 8.0 7.9 7.8
 50 23 20 14

8.5 7.6 8.5 10.0 11.0
 10 12 30 50 70

42.8

5.8 5.1 5.8 10.0 10.4 9.9 9.8
 50 33 23 19 14 6

10.2 9.2 10.9 13.2
 9 11 50 80

42.6

6.0 5.5 10.8 11.2 11.9 11.4 11.4
 50 37 28 17 16 5

11.6 10.7 10.7 11.7 16.3
 7 9 29 45 80

42.4

6.0 6.0 8.7 12.5 12.8 13.4 13.0 13.0 12.8
 50 35 29 25 18 17 7

13.3 12.6 12.6 13.8 14.0 5.5
 6 8 26 44 80

42.6

6.0 6.5 4.1

34.1

4.5 5.2
 32 15

6.2 5.3 7.6 9.8 10.9
 9 12 30 50 80

33.9

4.7 4.3

7.0 6.6 5.7 10.7 16.2
 10 14 21 50 80

23.7

27.9 22.4

Sta. + 7 -

938.58

60+88

932.4

61+02.95 = 1 M-Memory/-

31.8

B.M.

7.06

931.52 931.50

61+16

31.1
30.1

B.M. + 7.48 938.98

7.06

931.50

61+28

32.6

61+60

34.7

62

34.7

+50

34.2

63

32.3

+60

31.9

64+00

28.8

T.P.

4.25 932.88

10.35

928.63

65+00

21.2

+50

22.3

66+00

26.3

21.

2

21.

19

33.0

$\frac{5.6}{50}$

$\frac{6.2}{72}$

$\frac{6.2}{72}$

$\frac{8.0}{76}$

28.6
 $\frac{10.0}{50}$

$\frac{14.0}{66}$

26.6
 $\frac{12.0}{80}$

34.4

Drops, $\frac{4.2}{100}$

$\frac{5.4}{50}$

$\frac{6.8}{72}$

$\frac{8.2}{75}$

$\frac{10.4}{66}$

26.6
 $\frac{12.0}{100}$

Top Stone mon. 32.6
M₃ Normans "F"

$\frac{6.0}{50}$

$\frac{6.5}{53}$

7.5

$\frac{10.2}{50}$

$\frac{11.1}{66}$

26.2
 $\frac{12.4}{100}$

38.5

$\frac{0.5}{50}$

$\frac{2.1}{33}$

$\frac{4.1}{15}$

$\frac{6.6}{9}$

$\frac{6.6}{20}$

37.7

$\frac{1.3}{50}$

$\frac{2.0}{33}$

4.3

$\frac{5.9}{1}$

$\frac{6.0}{15}$

35.1

$\frac{3.9}{50}$

$\frac{4.4}{33}$

4.3

$\frac{5.6}{1}$

$\frac{6.5}{14}$

33.6

$\frac{5.4}{50}$

$\frac{5.9}{33}$

$\frac{5.8}{20}$

4.8

$\frac{5.2}{1}$

$\frac{5.5}{15}$

36.5

$\frac{3.5}{50}$

$\frac{5.2}{33}$

$\frac{6.6}{15}$

6.7

$\frac{7.6}{1}$

$\frac{7.8}{15}$

$\frac{11.0}{25}$

35.9

$\frac{3.1}{50}$

$\frac{4.3}{33}$

7.1

$\frac{9.3}{2}$

$\frac{9.7}{12}$

34.3

$\frac{4.7}{50}$

$\frac{6.7}{33}$

$\frac{9.7}{17}$

10.2

$\frac{12.2}{1}$

26.4
 $\frac{12.6}{12}$

28.6

$\frac{4.3}{50}$

$\frac{7.2}{33}$

$\frac{9.7}{17}$

$\frac{10.2}{2}$

11.7

$\frac{13.0}{6}$

$\frac{14.1}{76}$

25.0

$\frac{7.9}{50}$

$\frac{9.0}{33}$

$\frac{9.8}{7}$

10.6

$\frac{12.3}{12}$

29.9

$\frac{3.0}{50}$

$\frac{3.9}{33}$

$\frac{6.4}{15}$

$\frac{6.0}{3}$

6.6

$\frac{8.0}{6}$

$\frac{9.1}{12}$

For Balance of K. Sections see pages 21-22

Sta + π - Elev.

932.88

66+60

26.7

T.P

13.56

945.25

1.19

931.69

67+00

30.1

+60

35.8

68+00

36.8

+65

36.0

69+0

35.1

+65

33.2

70+00

32.4

T.P

5.04

940.39

9.90

935.35

+60

34.2

71+00

32.5

+50

30.7

72+00

27.4

T.P

0.59

927.70

13.28

927.11

+70

21.2

30.6

$$\frac{2.3}{50} \quad \frac{3.2}{33} \quad \frac{4.8}{17} \quad \frac{5.1}{2} \quad 6.2 \quad \frac{8.1}{7} \quad \frac{9.3}{14}$$

35.4

$$\frac{9.9}{50} \quad \frac{12.0}{33} \quad \frac{14.8}{14} \quad 15.2 \quad \frac{17.0}{18}$$

40.5

$$\frac{4.8}{50} \quad \frac{5.9}{33} \quad \frac{7.5}{15} \quad \frac{8.0}{6} \quad 9.5 \quad \frac{12.9}{14}$$

40.1

$$\frac{5.2}{50} \quad \frac{5.9}{33} \quad \frac{6.4}{15} \quad \frac{6.9}{7} \quad 8.5$$

40.5

$$\frac{4.8}{50} \quad \frac{5.5}{33} \quad \frac{6.8}{15} \quad \frac{7.9}{5} \quad 9.3$$

38.8

$$\frac{6.5}{50} \quad \frac{7.0}{33} \quad \frac{8.8}{5} \quad 10.2 \quad \frac{11.7}{18}$$

36.5

$$\frac{8.8}{50} \quad \frac{10.0}{33} \quad \frac{10.8}{15} \quad \frac{11.2}{3} \quad 12.1 \quad \frac{16.1}{25}$$

37.3

$$\frac{8.0}{50} \quad \frac{9.3}{33} \quad \frac{10.7}{15} \quad \frac{11.3}{4} \quad 11.9$$

37.9

$$\frac{2.9}{50} \quad \frac{3.3}{33} \quad \frac{5.3}{5} \quad 6.2 \quad \frac{8.8}{30} \quad \frac{10.7}{42}$$

36.9

$$\frac{3.5}{50} \quad \frac{4.8}{33} \quad \frac{7.1}{4} \quad 7.9 \quad \frac{11.2}{30}$$

36.4

$$\frac{4.0}{50} \quad \frac{5.8}{33} \quad \frac{7.9}{16} \quad \frac{8.5}{5} \quad 9.7 \quad \frac{11.9}{15} \quad \frac{14.4}{30}$$

36.0

$$\frac{5.4}{50} \quad \frac{8.9}{33} \quad \frac{11.9}{15} \quad 13.0 \quad \frac{14.6}{5}$$

25.9

$$\frac{1.8}{50} \quad \frac{4.4}{33} \quad \frac{6.1}{15} \quad 6.5$$

Sta.	+	H.I	-	Elev
		927.70		

73400

18.1

+30

14.3

T.P

914.50

0.06

13.26

914.44

2.55

911.85

911.91

H.

L

Rt.

21

22.9

 $\frac{4.8}{50}$ $\frac{6.4}{33}$ $\frac{8.1}{15}$

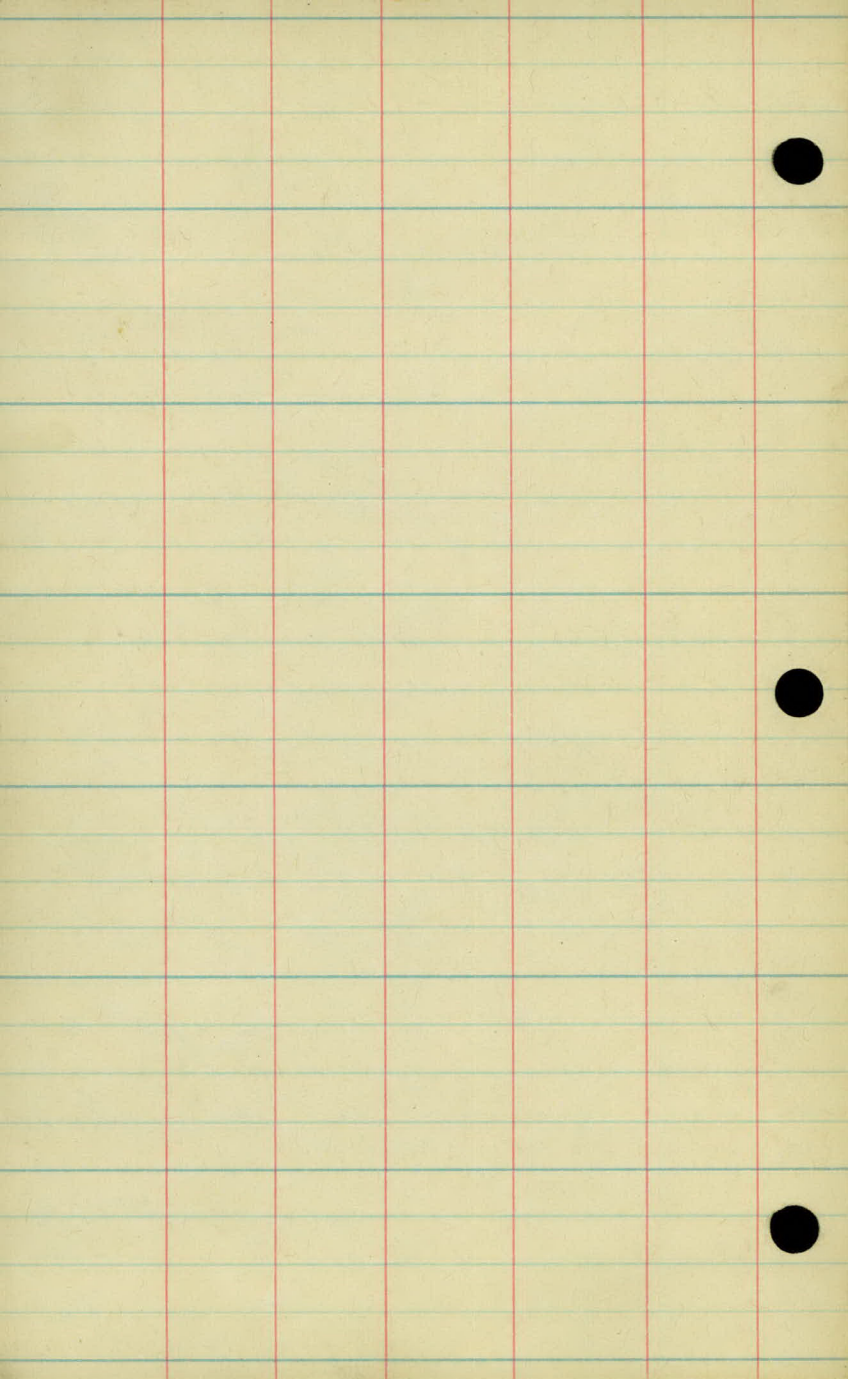
9.6

18.0

 $\frac{9.7}{50}$ $\frac{9.9}{33}$ $\frac{10.8}{22}$

13.4

Top Mon. Sta. 73+48.3



X-Sections

Sta. 61+28 to 73+30

RT only.

Sta.	+	π	-	Elev.
B.M.	1.50	933.00		931.50

61478				
T.P.	5.76	925.97	1229	920.71

61460

6240

450

6340

460

T.P.	0.06	920.03	6.00	919.97
------	------	--------	------	--------

64

65

450

T.P.	7.15	920.59	6.59	913.44
------	------	--------	------	--------

Top Mon. M = Meneniy + F¹

For X sections on Lt. See P. 19, 20, 21

0.4	1.1	11.0	14.0	100.
		66	100.	
x 8.7		7.2	14.4	✓
		66	100.	
x 8.7		7.0	12.4	
		66	100.	
x 8.2		4.7	13.4	
		66	100	13.0
			150	
x 6.3		3.3	13.4	
		66	100	
+ 5.9		7.6	12.3	
		66	100	15.0
			115	
+ 8.8		15.4	12.3	11.6
		4.6	7.7	3.4
		66	90	100
			125	9.0
+ 1.3	64.50	7.8	10.9	10.4
	11.6	66.7	9.1	9.4
	5.4	7.3	100	125
	25	66		
+ 2.3		13.0	10.5	10.5
		7.0	9.5	9.5
		66	100	125

Sta. + T - Elev.

36.7
92059
87

66+00

+60

67

T.P.

6.71

927.16

0.14

92045

+60

68

+65

69

7.50

930.38

4.28

92288

+65

70

+60

71

T.P.

1.03

92496

6.05

923.93

+50

4

E

RT.

24

$$+5.7 \quad \begin{array}{r} 12.3 \\ 83 \\ \hline 66 \end{array} \quad \begin{array}{r} 10.4 \\ 102 \\ \hline 100 \end{array} \quad \begin{array}{r} 10.4 \\ 10.2 \\ \hline 120 \end{array}$$

$$+6.1 \quad \begin{array}{r} 19.1 \\ 1.5 \\ \hline 33 \end{array} \quad \begin{array}{r} 13.1 \\ 7.5 \\ \hline 66 \end{array} \quad \begin{array}{r} 10.6 \\ 10.0 \\ \hline 100 \end{array} \quad \begin{array}{r} 10.1 \\ 10.5 \\ \hline 125 \end{array}$$

$$+9.5 \quad \begin{array}{r} 19.9 \\ 0.7 \\ \hline 51 \end{array} \quad \begin{array}{r} 10.0 \\ 4.6 \\ \hline 66 \end{array} \quad \begin{array}{r} 11.5 \\ 9.1 \\ \hline 88 \end{array} \quad \begin{array}{r} 10.1 \\ 10.5 \\ \hline 125 \end{array}$$

$$+8.6 \quad \begin{array}{r} 20.8 \\ 5.4 \\ \hline 66 \end{array} \quad \begin{array}{r} 13.0 \\ 14.2 \\ \hline 100 \end{array} \quad \begin{array}{r} 12.4 \\ 14.8 \\ \hline 120 \end{array}$$

$$+9.4 \quad \begin{array}{r} 21.9 \\ 5.3 \\ \hline 66 \end{array} \quad \begin{array}{r} 13.2 \\ 14.0 \\ \hline 115 \end{array} \quad \begin{array}{r} 13.0 \\ 14.2 \\ \hline 125 \end{array}$$

$$+8.8 \quad \begin{array}{r} 25.9 \\ 13 \\ \hline 45 \end{array} \quad \begin{array}{r} 23.2 \\ 40 \\ \hline 66 \end{array} \quad \begin{array}{r} 19.1 \\ 8.1 \\ \hline 82 \end{array} \quad \begin{array}{r} 10.0 \\ 17.2 \\ \hline 100 \end{array} \quad \begin{array}{r} 07.5 \\ 19.7 \\ \hline 125 \end{array}$$

$$+7.9 \quad \begin{array}{r} 23.3 \\ 39 \\ \hline 66 \end{array} \quad \begin{array}{r} 14.0 \\ 13.2 \\ \hline 107 \end{array} \quad \begin{array}{r} 07.4 \\ 19.8 \\ \hline 125 \end{array}$$

$$+2.8 \quad \begin{array}{r} 26.9 \\ 3.5 \\ \hline 44 \end{array} \quad \begin{array}{r} 21.7 \\ 8.7 \\ \hline 66 \end{array} \quad \begin{array}{r} 17.9 \\ 12.5 \\ \hline 87 \end{array} \quad \begin{array}{r} 21.4 \\ 9.0 \\ \hline 100 \end{array} \quad \begin{array}{r} 18.5 \\ 11.9 \\ \hline 120 \end{array}$$

$$+3.0 \quad \begin{array}{r} 28.3 \\ 2.1 \\ \hline 33 \end{array} \quad \begin{array}{r} 21.7 \\ 8.7 \\ \hline 66 \end{array} \quad \begin{array}{r} 19.7 \\ 10.7 \\ \hline 85 \end{array} \quad \begin{array}{r} 20.7 \\ 10.2 \\ \hline 100 \end{array} \quad \begin{array}{r} 23.2 \\ 7.2 \\ \hline 120 \end{array}$$

$$+3.8 \quad \begin{array}{r} 26.4 \\ 4.0 \\ \hline 66 \end{array} \quad \begin{array}{r} 24.0 \\ 6.4 \\ \hline 100 \end{array} \quad \begin{array}{r} 23.1 \\ 7.5 \\ \hline 125 \end{array}$$

$$+2.1 \quad \begin{array}{r} 25.8 \\ 4.6 \\ \hline 66 \end{array} \quad \begin{array}{r} 23.7 \\ 6.7 \\ \hline 100 \end{array} \quad \begin{array}{r} 23.0 \\ 7.4 \\ \hline 125 \end{array}$$

$$+5.7 \quad \begin{array}{r} 23.3 \\ 1.7 \\ \hline 66 \end{array} \quad \begin{array}{r} 22.2 \\ 2.8 \\ \hline 100 \end{array} \quad \begin{array}{r} 21.5 \\ 3.5 \\ \hline 125 \end{array}$$

Top Stake 70 - 66 RT.

Sta. + A - Elev.

92496

7240

+70

T.P.

6.36

917.63

13.69

911.27

73

+30

5.70

911.93

4.

1

Rt

28

Dec P. 14-20-21

	22.7	20.6	19.0	17.8
+ 2.4	$\frac{2.3}{33}$	$\frac{4.4}{66}$	$\frac{6.0}{100}$	$\frac{7.2}{125}$
	19.0	17.4	15.5	11.9
- 3.8	$\frac{6.0}{33}$	$\frac{7.6}{66}$	$\frac{9.5}{80}$	$\frac{13.1}{100}$
	14.7	10.3	07.1	06.2
+ 0.5	$\frac{2.9}{33}$	$\frac{7.3}{66}$	$\frac{10.5}{100}$	$\frac{11.4}{125}$
	09.2	06.9	04.4	03.5
- 3.3	$\frac{8.4}{33}$	$\frac{10.7}{66}$	$\frac{13.2}{100}$	$\frac{14.1}{125}$

Top Mon. Sta. 73448.3

Sta.	+	π	-	Elev.
B.M.	1.70	913.61		911.91
74				905.1

+56	Orig Shore Line			901.7
T.P.	2.72	903.25	13.08	900.53

75				99.6
----	--	--	--	------

76				98.4
----	--	--	--	------

77				98.7
----	--	--	--	------

78				98.7
----	--	--	--	------

79				98.6
----	--	--	--	------

80				98.1
----	--	--	--	------

81				97.7
----	--	--	--	------

82				97.4
	3.85	902.07	5.03	898.22

83				97.9
----	--	--	--	------

+50	(Looks Like a Ditch)			97.4
-----	----------------------	--	--	------

84				97.8
----	--	--	--	------

85				97.6
----	--	--	--	------

4.

2

21.

Top Men. Sta. 73-48.3

07.4

01.8

69 06.7
50

8.5

10.2
50

11.8
100

(1/2" steel Rod, 2 Men) 02.2

00.4

98.6

3'-Peat

11.4
50

11.9

13.2
50

15.0
100

00.2

99.1

98.6

7'-Peat

3.1
50

37

4.2

4.7
100

12'-Peat.

49

Assumed 110.

12'-Peat.

46

10'-Peat.

46

10'-Peat.

47

13'-Peat.

52

No Bot @ 14'

56

No Bot @ 14'

59

12'-Peat.

42

11'-Peat.

47

10'-Peat.

43

12'-Peat.

45

Bog Marsh

Sta.

+

T

902.07

86

97.5

87

97.9

88

98.3

T.P.

3.47

902.47

3.07

899.00

89

98.3

90

98.1

91

98.1

92

99.1

93

99.9

T.P.

5.35

906.06

1.76

900.71

94

00.7

95

99.5

+50

99.0

96

Approx. @ 1st Shore

00.2

W. B. H. @ 14'

46

Assumed L.O.

10' Peat.

42

8' Peat.

38

7' Peat.

42

14' Peat.

44

12' Peat.

44

6' Peat.

34

00 Peat.

26

mass by bog

Surface Rock

00 Peat.

00.9

$\frac{5.2}{50}$

54

$\frac{6.2}{42}$

99.8

$\frac{6.3}{70}$

00 Peat

99.9

$\frac{6.2}{50}$ $\frac{5.8}{25}$

66

$\frac{5.6}{40}$

00.7

$\frac{5.4}{70}$

10' Peat.

99.3

$\frac{6.8}{50}$

71

$\frac{7.0}{25}$

99.4

$\frac{6.7}{70}$

6' Peat.

00.3

$\frac{5.8}{50}$

59

$\frac{5.8}{40}$

00.5

$\frac{5.6}{70}$

Sta.	+	π	-	Elev.
		906.06		
96+60		1		01.8
T.P.	9.16	913.73	1.49	904.57
97				03.7
+48		1		09.1
B.M.	1.72	910.73	4.65	909.08 909.01
+70				06.2
98				05.9
+60				04.7
99				04.6
100				03.2
+50				02.4
101				00.6
+50				99.9
102		1		99.9
T.P.	7.24	908.01	9.96	900.77

Lt

E

Rt.

0.0 Peat.

$$\begin{array}{r} 01.4 \\ 47 \\ \hline 50 \end{array}$$

43

$$\begin{array}{r} 4.3 \\ 17 \\ \hline 27 \end{array}$$

$$\begin{array}{r} 03.0 \\ 31 \\ \hline 70 \end{array}$$

03.4

$$\begin{array}{r} 10.3 \\ 50 \\ \hline \end{array}$$

10.0

$$\begin{array}{r} 9.4 \\ 35 \\ \hline \end{array}$$

04.9

$$\begin{array}{r} 8.8 \\ 70 \\ \hline \end{array}$$

08.5

$$\begin{array}{r} 5.2 \\ 50 \\ \hline \end{array}$$

46

$$\begin{array}{r} 4.2 \\ 35 \\ \hline \end{array}$$

09.7

$$\begin{array}{r} 40 \\ 70 \\ \hline \end{array}$$

Spike 24" Elm 87' Lt. Sta. 97+60

$$\begin{array}{r} 4.4 \\ 50 \\ \hline \end{array}$$

$$\begin{array}{r} 4.4 \\ 25 \\ \hline \end{array}$$

45

$$\begin{array}{r} 4.4 \\ 25 \\ \hline \end{array}$$

$$\begin{array}{r} 4.6 \\ 70 \\ \hline \end{array}$$

05.8

$$\begin{array}{r} 4.9 \\ 50 \\ \hline \end{array}$$

$$\begin{array}{r} 5.0 \\ 75 \\ \hline \end{array}$$

$$\begin{array}{r} 4.8 \\ \hline \end{array}$$

$$\begin{array}{r} 5.1 \\ 75 \\ \hline \end{array}$$

05.8

$$\begin{array}{r} 4.9 \\ 70 \\ \hline \end{array}$$

05.4

$$\begin{array}{r} 5.3 \\ 50 \\ \hline \end{array}$$

04.7

60

04.8

$$\begin{array}{r} 5.9 \\ 50 \\ \hline \end{array}$$

04.8

$$\begin{array}{r} 5.9 \\ 50 \\ \hline \end{array}$$

61

04.4

$$\begin{array}{r} 6.3 \\ 50 \\ \hline \end{array}$$

E

75

Peat 1'

83

Peat 7'

10.1

Peat 6'

Assumed

10.8

Level Out

Peat 8'

10.8

Sda. + π - Elev.

908.01

102+50

899.5

103

900.3

+50

00.7

104

01.6

+50

02.8

105

02.4

+50

03.3

B.M.

2.09

✓ 905.92 905.91

106

03.6

+50

04.1

+78

03.³/₄

107.

99.8

+55

97.8

108

97.3

T.D.

5.07

903.21

9.87

898.14

Lt

2

Rt.

29

8' Peat.

85

10

6' Peat.

77

2' Peat.

73

1' Peat.

64

0' Peat (Hon Sand)

52

02.0

6.0

50

46

33

56

6.0

01.4

6.2

50

47

Spike Top Willow stp. 2'-Lt.

105 192

44

39

Sand

47

82

1' Peat

102

2' Peat

107

Sta. + π - E/cv.

903.21

108+50

96.3

109

95.5

+50

95.6

110

95.5

+52

94.6

+58

Bot Ditch. (See TOP.)

93.6

+63

94.2

111.

94.2

+50

93.9

112

94.0

+60

93.9

113

94.6

Lt.

E

Lt.

30

3'-Peat.

6.9

7'-Peat.

7.7

5'-Peat.

7.6

5'-Peat.

7.7

8.6

XSec - Assum L.O.

10'-Peat. - Wet.

9.6

9.0

No Bottom @ 14'

9.0

10'-Peat

9.3

13'-Peat

9.2

No Bottom @ 14'

9.3

8'-Peat

8.6

Sta.	+	-	Elev.
		903.21	
113+40			95.5
+65			97.7
114			98.8
T.B.M.		3.13	900.08
B.M.		2.77	900.44
+45			99.2
115			98.2
+30			97.5
116			97.5
116+50			97.9
117			97.9
118			98.9
119			900.4
T.P.	7.04	908.29	1.96
			906.25

Lt.

Z

Rt.

31

2 -

77

3' - Peat.

96.1

98.4

2' - Peat.

So

$$\begin{array}{r} 7.1 \\ 50 \end{array}$$

55

$$\begin{array}{r} 5.0 \\ 50 \end{array}$$

$$\begin{array}{r} 4.8 \\ 100 \end{array}$$

1.0

98.5

98.4

Sand -
Surface Rock

So

$$\begin{array}{r} 4.7 \\ 50 \end{array}$$

$$\begin{array}{r} 4.4 \\ 50 \end{array}$$

$$\begin{array}{r} 3.7 \\ 50 \end{array}$$

$$\begin{array}{r} 4.8 \\ 100 \end{array}$$

1.0

+ on Blue Rock

$$\begin{array}{r} 98.8 \\ 3.4 \\ 50 \end{array}$$

Rt.

Sta. 113 + 84

98.5

0.0 Peat.

$$\begin{array}{r} 3.4 \\ 50 \end{array}$$

40

$$\begin{array}{r} 4.7 \\ 50 \end{array}$$

2' - Peat

5.0

4' - Peat

5.7

6' - Peat

5.7

2' - Peat

5.3

2' - Peat

5.3

2' - Peat.

4.3

(0.0 Peat + 75)

2.8

— Sands —

Sta.	+	π	-	Elev.	
		908.29			
119				900.5	
150				01.0	
120				901.0	
121				02.2	
122				03.0	
170				04.8	
173				04.8	
T.P.	7.23	¹ 914.08	4.54	¹ 903.75	
124				05.6	
175				05.7	
176				06.4	
180				06.4	
B.M.	2.47	¹ 912.27	1.24	¹ 909.84	909.86

Lt.

2

Rt.

April 6/0
Borlow
22.1.1911.

04.0

99.5

$\frac{43}{100}$	$\frac{6.1}{50}$	7.8	$\frac{2.8}{50}$	$\frac{8.8}{100}$
------------------	------------------	-----	------------------	-------------------

04.9

00.2

$\frac{3.0}{100}$	$\frac{4.1}{65}$	$\frac{5.1}{50}$	$\frac{7.3}{50}$	$\frac{8.0}{50}$	$\frac{8.1}{100}$
-------------------	------------------	------------------	------------------	------------------	-------------------

04.2

99.8

$\frac{4.1}{100}$	$\frac{5.6}{50}$	$\frac{7.3}{50}$	$\frac{8.3}{50}$	$\frac{8.5}{100}$
-------------------	------------------	------------------	------------------	-------------------

05.1

99.9

$\frac{3.2}{100}$	$\frac{4.0}{60}$	$\frac{4.8}{50}$	$\frac{6.1}{50}$	$\frac{7.6}{50}$	$\frac{8.4}{100}$
-------------------	------------------	------------------	------------------	------------------	-------------------

05.1

00.3

F Line = $\frac{3.2}{85}$ $\frac{3.6}{50}$ $\frac{4.3}{15}$ $\frac{5.3}{50}$ $\frac{6.7}{50}$ $\frac{8.0}{100}$

05.8

00.6

F Line = $\frac{2.5}{65}$ $\frac{3.5}{50}$ $\frac{5.2}{23}$ $\frac{6.6}{65}$ $\frac{7.7}{100}$

05.8

01.2

$\frac{2.5}{50}$ $\frac{3.5}{13}$ $\frac{3.1}{76}$ $\frac{5.0}{50}$ $\frac{5.9}{50}$ $\frac{7.1}{100}$

P.O.

55

P.O.

911.2

P.O. $\frac{15.5}{106}$ $\frac{20}{90}$ $\frac{3.9}{15}$ $\frac{5.4}{50}$ $\frac{7.1}{100}$

07.4

$\frac{4.0}{100}$ $\frac{4.2}{63}$ $\frac{4.3}{53}$ $\frac{0.0}{51}$ $\frac{7.6}{37}$ $\frac{4.4}{19}$ $\frac{4.7}{50}$ $\frac{4.7}{33}$ $\frac{7.1}{100}$

05.4

07.5

$\frac{5.7}{65}$ $\frac{2.4}{41}$ $\frac{2.4}{36}$ $\frac{4.3}{22}$ $\frac{4.7}{50}$ $\frac{3.6}{54}$ $\frac{10.1}{68}$ $\frac{3.6}{90}$

R.R. Spike 12" Wh. Oak Ho-Lt. Star. 176+60

Sta. + T - Elev.

912.27

127 . 06.5

+25 05.9

+47 04.7

+55 = 2 Ditch 00.6

+75 07.0

128 04.8

T.P. 4.49 912.46 4.30 907.97

128 04.8

+50 03.9

129 03.7

130 04.3

131 05.1

x 132 05.6

Lt.

L

Rt.

33

04.0

8.3	64	4.1	<u>5.7</u>
70	<u>45</u>	<u>37</u>	<u>18</u>

5.8

6.3

33

Ditch

+

11.9

48

06.0

6.3

68

04.6

<u>77</u>	<u>5.2</u>	<u>5.7</u>
<u>50</u>	<u>40</u>	<u>20</u>

6.4

7.4

12

11.6

25

3.7

42

2.7

75

04.5

<u>7.8</u>	<u>56</u>	<u>5.5</u>
<u>50</u>	<u>37</u>	<u>14</u>

7.6

11.7

11

4.8

28

0.0

75

04.4

<u>79</u>	<u>54</u>	<u>54</u>	<u>7.0</u>
<u>50</u>	<u>37</u>	<u>20</u>	<u>8</u>

11.7

4.8

20

4.8

50

02.9

<u>9.4</u>	<u>6.6</u>	<u>5.0</u>	<u>11.7</u>
<u>50</u>	<u>41</u>	<u>29</u>	<u>16</u>

5.3

4.3

6

5.9

20

5.9

50

05.9

06.6

6.4

16

6.4

50

5.7

90

02.0

00.3

02.6

03.6

<u>10.1</u>	<u>12.2</u>	<u>9.9</u>	<u>8.9</u>
<u>49</u>	<u>41</u>	<u>29</u>	<u>11</u>

-7.7

0.0 Peat

00.1

12'-Peat

<u>12.4</u>	<u>10.4</u>	<u>9.8</u>
<u>78</u>	<u>71</u>	<u>35</u>

8.6

6.8

30

3.9

62

09.5

3.0

80

02.1

<u>10.4</u>	<u>9.8</u>
<u>50</u>	<u>28</u>

8.8

09.6

6.9

50

2.9

100

No Bot @ 14

02.8

Peat 13'

<u>7.7</u>	<u>9.2</u>
<u>50</u>	<u>25</u>

8.2

5.9

50

3.5

90

2.9

75

Fence

03.2

<u>9.3</u>	<u>8.5</u>
<u>50</u>	<u>25</u>

7.2

6.0

30

4.8

55

3.4

80

Fence

04.2

<u>8.3</u>	<u>8.0</u>
<u>50</u>	<u>25</u>

6.9

6.0

30

08.7

3.8

73

Fence

No Bot @ 14

Bernard Franklin

St.	+	π	-	Elev.	
		912.46		06.4 12.4	
133					
134				07.3	
B.M.	5.60	915.83	2.23	06.7 26.4	910.28
135					
136				06.1	
+16				06.3	
+27 - 4 Ditch -				02.1	
+38				05.5	
+50				05.1	
137				05.4	
+35				06.9	
138				08.6	
+28				09.3	
T.P.	12.88	928.35	0.36		915.47

4.

4

RT

30

05.1

06.3

4'-Peat.

$$\begin{array}{r} 7.4 \\ 50 \end{array}$$

6.1

$$\begin{array}{r} 4.5 \\ 30 \end{array}$$

$$\begin{array}{r} 6.2 \\ 63 \end{array}$$

05.5

09.9

4'-Peat.

$$\begin{array}{r} 7.0 \\ 50 \end{array}$$

5.2

$$\begin{array}{r} 4.0 \\ 30 \end{array}$$

$$\begin{array}{r} 7.6 \\ \sqrt{2} \end{array}$$

R.R. Spike Cor. F. Peat. 51'-RT Sta. 134+22

7'-Peat.

$$\begin{array}{r} 11.1 \\ 101 \end{array} \begin{array}{r} 14.8 \\ 95 \end{array} \begin{array}{r} 11.2 \\ 86 \end{array} \begin{array}{r} 11.1 \\ 77 \end{array} \begin{array}{r} 10.4 \\ 50 \end{array}$$

9.2

$$\begin{array}{r} 7.3 \\ 50 \end{array}$$

$$\begin{array}{r} 6.5 \\ 100 \end{array}$$

09.3

04.6

04.8

6'-Peat

$$\begin{array}{r} 11.0 \\ 50 \end{array} \begin{array}{r} 10.2 \\ 36 \end{array} \begin{array}{r} 13.7 \\ 76 \end{array} \begin{array}{r} 10.2 \\ 16 \end{array} \begin{array}{r} 9.7 \\ 77 \end{array}$$

$$\begin{array}{r} 9.3 \\ 33 \end{array}$$

$$\begin{array}{r} 9.2 \\ 70 \end{array}$$

05.2

06.3

$$\begin{array}{r} 10.6 \\ 50 \end{array} \begin{array}{r} 10.0 \\ 29 \end{array} \begin{array}{r} 10.0 \\ 22 \end{array} \begin{array}{r} 13.7 \\ 11 \end{array} \begin{array}{r} 9.5 \\ 75 \end{array}$$

$$\begin{array}{r} 9.6 \\ 33 \end{array}$$

$$\begin{array}{r} 9.5 \\ 70 \end{array}$$

05.3

04.3

6'-Peat

$$\begin{array}{r} 10.5 \\ 50 \end{array} \begin{array}{r} 10.8 \\ 76 \end{array} \begin{array}{r} 9.9 \\ 70 \end{array} \begin{array}{r} 10.0 \\ 12 \end{array} \begin{array}{r} 13.7 \\ 0 \end{array}$$

$$\begin{array}{r} 9.4 \\ 10 \end{array} \begin{array}{r} 10.0 \\ 33 \end{array}$$

$$\begin{array}{r} 9.5 \\ 70 \end{array}$$

05.2

06.0

$$\begin{array}{r} 10.6 \\ 50 \end{array} \begin{array}{r} 10.8 \\ 19 \end{array} \begin{array}{r} 9.8 \\ 12 \end{array} \begin{array}{r} 10.3 \\ 1 \end{array}$$

$$\begin{array}{r} 13.7 \\ 10 \end{array} \begin{array}{r} 9.4 \\ 20 \end{array} \begin{array}{r} 10.0 \\ 33 \end{array}$$

$$\begin{array}{r} 9.8 \\ 70 \end{array}$$

05.1

05.4

$$\begin{array}{r} 10.7 \\ 50 \end{array}$$

$$\begin{array}{r} 10.7 \\ 8 \end{array}$$

$$\begin{array}{r} 10.0 \\ 17 \end{array}$$

$$\begin{array}{r} 10.7 \\ 76 \end{array}$$

$$\begin{array}{r} 13.8 \\ 57 \end{array}$$

$$\begin{array}{r} 10.4 \\ 70 \end{array}$$

$$\begin{array}{r} 10.4 \\ 70 \end{array}$$

05.8

05.2

12'-Peat

$$\begin{array}{r} 10.0 \\ 50 \end{array} \begin{array}{r} 10.1 \\ 70 \end{array} \begin{array}{r} 10.4 \\ 1 \end{array}$$

$$\begin{array}{r} 10.7 \\ 33 \end{array} \begin{array}{r} 11.2 \\ 61 \end{array}$$

$$\begin{array}{r} 13.9 \\ 67 \end{array}$$

$$\begin{array}{r} 10.6 \\ 74 \end{array}$$

07.3

06.2

5'-Peat

$$\begin{array}{r} 8.5 \\ 50 \end{array}$$

8.9

$$\begin{array}{r} 9.1 \\ 22 \end{array}$$

$$\begin{array}{r} 9.6 \\ 50 \end{array}$$

09.0

08.1

4'-Peat

$$\begin{array}{r} 6.8 \\ 50 \end{array}$$

$$\begin{array}{r} 7.4 \\ 75 \end{array}$$

7.2

$$\begin{array}{r} 7.3 \\ 33 \end{array}$$

$$\begin{array}{r} 7.7 \\ 50 \end{array}$$

13.0

08.9

0.0 Peat

$$\begin{array}{r} 3.8 \\ 50 \end{array}$$

$$\begin{array}{r} 5.0 \\ 73 \end{array}$$

6.5

$$\begin{array}{r} 6.8 \\ 33 \end{array}$$

$$\begin{array}{r} 6.9 \\ 50 \end{array}$$

Sto. + 7 - Elev.

928.35

138+60 15.7

139 21.1

144 19.1

+14 22.4

+76 22.6

+57 24.7

+78 17.6

+87 - W. Shoulder. 19.2

+91 W. edge Pav. 18.93

E Pav. 919.44

8.91 928.37 8.91

919.44 919.46

T.P. 2.53 919.01 11.89

916.48

Contd next Page.

L4

R1.

Good Barrow

20.4

19.1

2

14.5

$$\begin{array}{r} 7.8 \\ 80 \end{array}$$

$$\begin{array}{r} 9.3 \\ 50 \end{array}$$

$$\begin{array}{r} 11.3 \\ 18 \end{array}$$

$$\begin{array}{r} 13.7 \\ 17 \end{array}$$

$$\begin{array}{r} 13.9 \\ 17 \end{array}$$

- contd.

24.9

20.8

16.2

$$\begin{array}{r} 31.5 \\ 80 \end{array}$$

$$\begin{array}{r} 5.1 \\ 50 \end{array}$$

$$\begin{array}{r} 7.6 \\ 27 \end{array}$$

$$\begin{array}{r} 7.0 \\ 13 \end{array}$$

$$\begin{array}{r} 7.3 \\ 7.3 \end{array}$$

$$\begin{array}{r} 9.0 \\ 28 \end{array}$$

$$\begin{array}{r} 12.2 \\ 50 \end{array}$$

✓

24.9

23.7

17.2

$$\begin{array}{r} 3.5 \\ 80 \end{array}$$

$$\begin{array}{r} 4.7 \\ 50 \end{array}$$

$$\begin{array}{r} 6.3 \\ 40 \end{array}$$

$$\begin{array}{r} 7.8 \\ 20 \end{array}$$

$$\begin{array}{r} 9.3 \\ 17 \end{array}$$

$$\begin{array}{r} 10.0 \\ 17 \end{array}$$

$$\begin{array}{r} 10.0 \\ 35 \end{array}$$

$$\begin{array}{r} 11.2 \\ 50 \end{array}$$

✓

25.5

24.5

15.9

$$\begin{array}{r} 2.9 \\ 80 \end{array}$$

$$\begin{array}{r} 3.9 \\ 50 \end{array}$$

$$\begin{array}{r} 4.6 \\ 31 \end{array}$$

$$\begin{array}{r} 6.0 \\ 6.0 \end{array}$$

$$\begin{array}{r} 8.3 \\ 15 \end{array}$$

$$\begin{array}{r} 11.5 \\ 38 \end{array}$$

$$\begin{array}{r} 12.5 \\ 50 \end{array}$$

✓

25.5

25.1

19.7

$$\begin{array}{r} 5.9 \\ 80 \end{array}$$

$$\begin{array}{r} 3.3 \\ 50 \end{array}$$

$$\begin{array}{r} 4.3 \\ 20 \end{array}$$

$$\begin{array}{r} 5.8 \\ 17 \end{array}$$

$$\begin{array}{r} 6.3 \\ 28 \end{array}$$

$$\begin{array}{r} 8.7 \\ 50 \end{array}$$

✓

See next Page

25.9

25.4

21.6

$$\begin{array}{r} 3.5 \\ 80 \end{array}$$

$$\begin{array}{r} 3.0 \\ 50 \end{array}$$

$$\begin{array}{r} 3.3 \\ 20 \end{array}$$

$$\begin{array}{r} 3.7 \\ 17 \end{array}$$

$$\begin{array}{r} 4.6 \\ 24 \end{array}$$

$$\begin{array}{r} 6.8 \\ 50 \end{array}$$

✓

19.9

15.9

$$\begin{array}{r} 8.5 \\ 80 \end{array}$$

$$\begin{array}{r} 9.2 \\ 50 \end{array}$$

$$\begin{array}{r} 9.7 \\ 32 \end{array}$$

$$\begin{array}{r} 10.8 \\ 17 \end{array}$$

$$\begin{array}{r} 11.5 \\ 27 \end{array}$$

$$\begin{array}{r} 12.5 \\ 50 \end{array}$$

✓

20.7

17.4

$$\begin{array}{r} 7.7 \\ 50 \end{array}$$

$$\begin{array}{r} 8.4 \\ 29 \end{array}$$

$$\begin{array}{r} 9.2 \\ 17 \end{array}$$

$$\begin{array}{r} 10.5 \\ 32 \end{array}$$

$$\begin{array}{r} 10.8 \\ 45 \end{array}$$

= W. edge B.O.

20.5

Remove Sloping Curb

17.3

$$\begin{array}{r} 7.8 \\ 50 \end{array}$$

$$\begin{array}{r} 9.42 \\ 17 \end{array}$$

$$\begin{array}{r} 11.05 \\ 73 \end{array}$$

= E. P.O.

Red Reading are not top Curb.

20.8

8.91

$$\begin{array}{r} 7.57 \\ 50 \end{array}$$

Sta	+	X	-	Elev.
-----	---	---	---	-------

919.01

138+60

139

+04

114

+76

+57

+78

913.30

T.P.

4.28

913.10

7.99

909.02

Elev. in Ditch 100' E. of Center Rd.

10.8

902.3

- 200' E.

10.9

902.2

L/-

2

RT.

W.H.C.
H.A.W.
K.A.
L.B.H.

Sept 9, 1925

36

- 3.3
Contd from Prec. P.

09.8 08.3
9.2 10.7
60 100
14.4 09.9
46 91
67 100

+ 2.1

13.7 10.5
5.3 8.5
70 100

+ 0.1

14.4 12.2

+ 3.4

46 68
72 100

15.3 12.5

+ 3.6

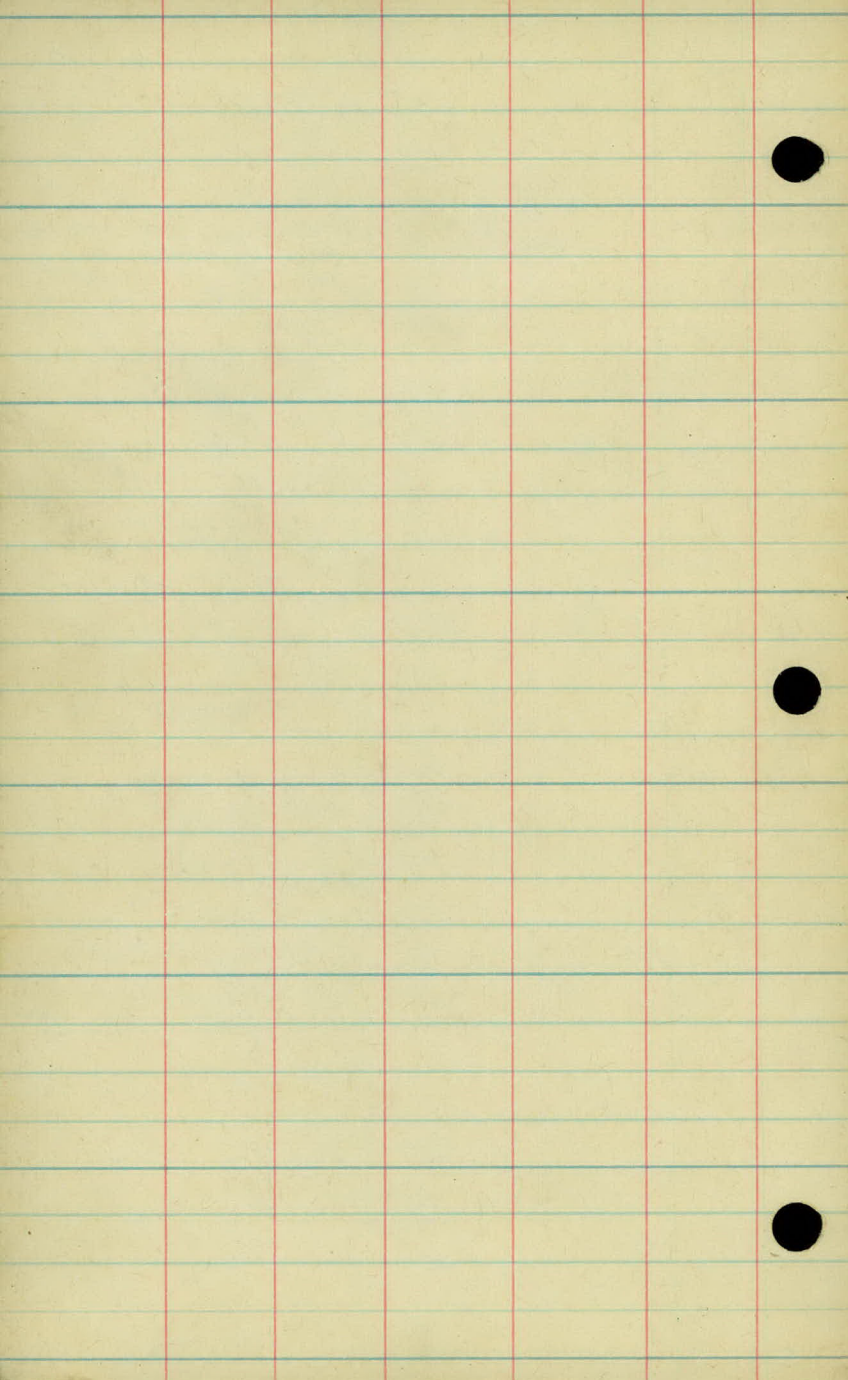
3.7 6.5
85 100

+ 5.7

14.7
43
100

E/- 900.7

18.3 = Flow Line 36" Adv.
thru Centerville
See Centerville Road
for Location



Bench Levels.

$\pm$	π	-	Elev
4.28	928.20		923.92
3.94	926.32	5.82	922.38
5.17	931.37	0.12	926.20
0.16	921.28	10.25	921.12
1.85	909.92	13.21	908.07
2.50	900.46	11.96	897.96
8.12	907.97	0.61	899.85
2.34	909.64	0.67	907.30
13.70	913.73	9.61	900.03
10.46	923.50	0.69	913.04
12.55	935.74	0.31	923.19
9.83	945.49	0.08	935.66
		4.61	940.88

Spike 12" Oak - Cramsie Rd. & Rice

Aug. 31, 1935

H. A. W.

K. A.

Spike in RR. 20' Lt. Sta 54+78

Bench Levels-

	+	-	Elev	
	x5.67	968.45	962.78	
		-6.67	961.78	961.78 Elev.
3.60	968.43	3.62	964.83	
2.07	962.67	7.83	960.60	
1.99	956.68	7.98	954.69	
2.71	952.35	7.04	949.64	
1.20	945.29	8.26	944.09	
2.39	939.86	7.82	937.47	
2.57	936.65	5.78	934.08	
1.43	928.65	9.43	927.22	
		9.19	919.46	B
T.P.	3.77	919.61	12.81	915.84
		9.38	910.23	B.M
5.04	911.79	12.86	902.75	
		1.99	909.80	B.M
8.32	914.02	6.09	905.70	
1.80	904.16	11.66	902.36	
		4.07	900.09	B.M
12.70	908.33	8.53	895.63	
		2.42	905.91	B.M
7.71	908.79	7.25	901.08	
7.19	913.72	2.26	906.53	
		4.71	909.01	B.M
9.80	909.84	13.68	900.04	
8.28	911.25	6.87	902.97	
4.14	910.63	4.76	906.49	

(Elev. 962.78)

15470

Aug. 30, 1935

H.A.W.

Co. Rd "G" & Centerville

K.A.

B.M. High Point on Mont & Parc

12" W. Oak 20' West & 40 ft No. of $\frac{1}{4}$ Cor

High Pt. on Rock So. of Seeline on Fenchlin

Spike Top of Stump. Sta ?

24" Elm Lt Sta. ? on Island ^{87'-Lt. 97+60}

Bench Levels Cont.

+	H.I	-	Elev	
	910.63			
4.77	910.86	4.54	906.09	
4.92	910.93	4.83	906.03	
8.11	914.40	4.66	906.29	
		2.49	911.91	B.M
13.55	927.94	0.01	914.39	
13.53	939.75	1.72	926.22	
4.54	942.69	1.60	938.15	
3.08	939.53	6.24	936.45	
		8.03	931.50	B.M
9.67	949.01	0.19	939.34	
		8.08	940.93	B.M

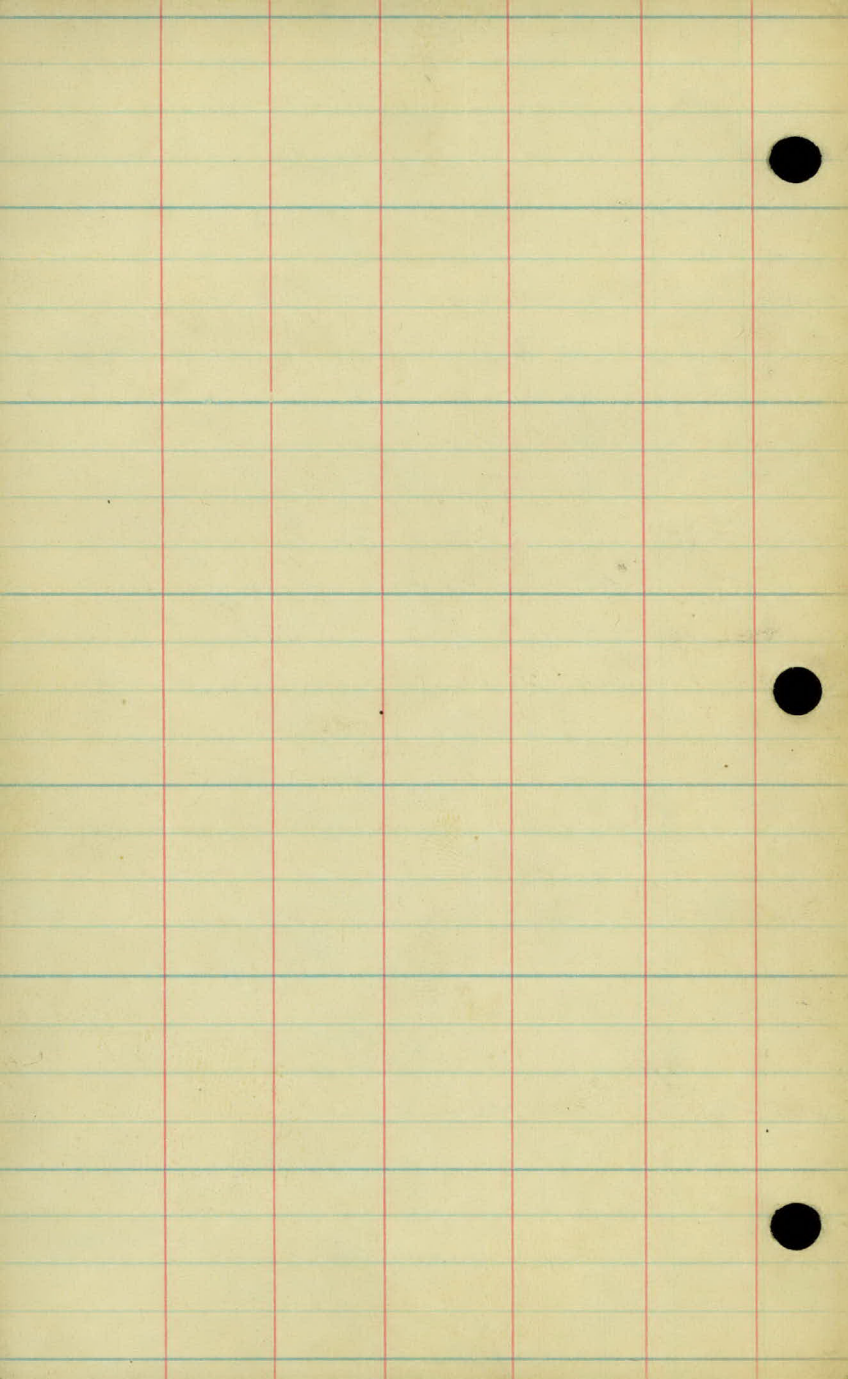
Top of Mean Cor Sta ? =

T.P on Hub on F

Top of Mont. "F & McMenamy."

Spike in (5' T.P.) West on F)
(20' Lt. Sta. 54+78)

38.58
2.06
31.52

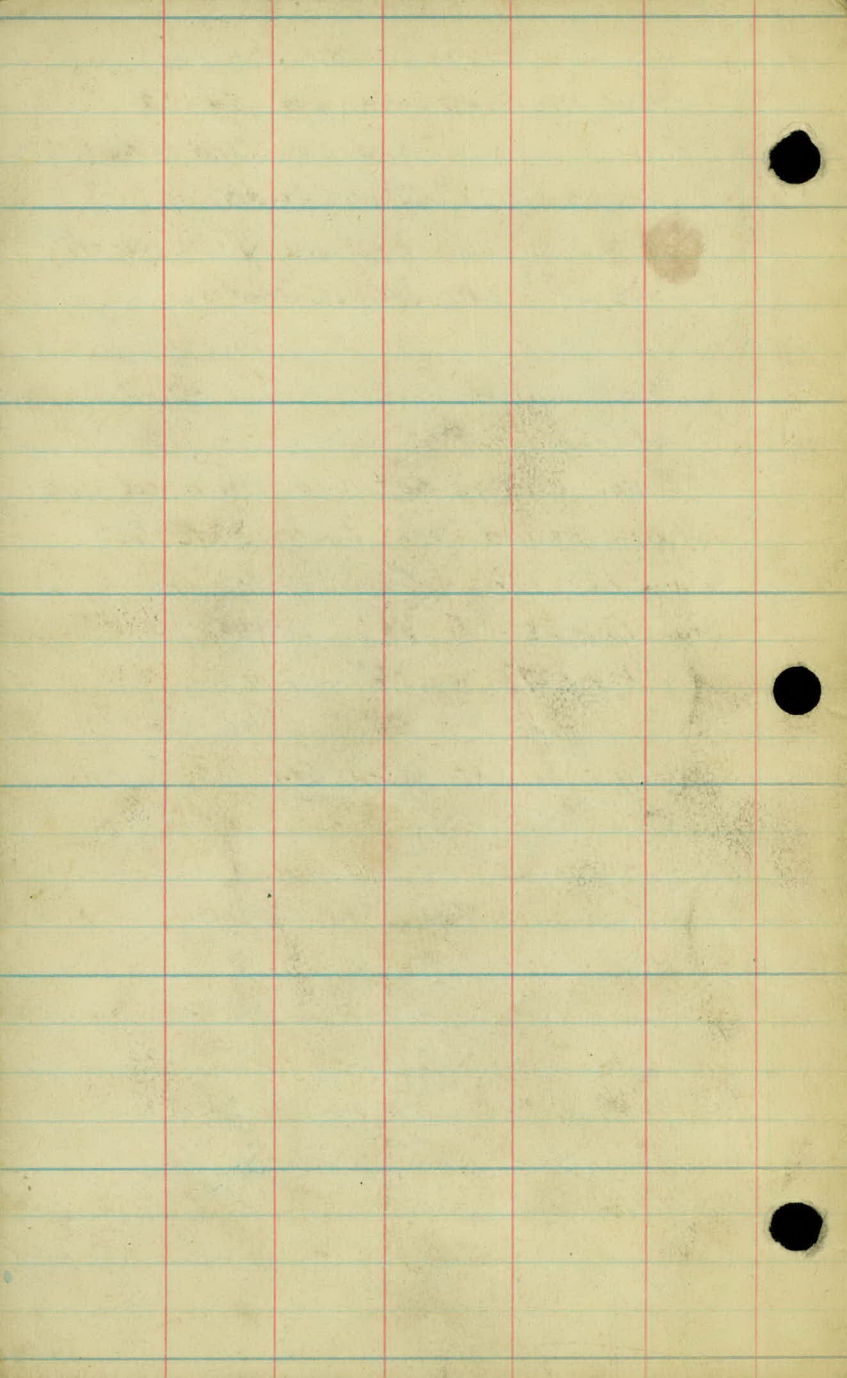


Recommendations

41

- X Borrow on South Side Sta. 54-58
- X Sta. 60+99 Inp. 18"X44' C.M. (Cond Fair) P. 18"
- X " 61+20 P. 18" Drains South.
- X Ditch McMeneny 100' North
- X Sta. 65+ P. 24" Drains South.
- X " 83+50 " 24" " "
- X " 102+00 P. 24" " ?
- X " 110+58 P. 24" " S.E.
- X Channel Change not recommended due to high ground on south side bet. Sta. 127-136
- X Sta. 127+55 P. 36" Drains S.W.
- " 136+27 " 36" " N.W.
- " 139+78 " 24" " South.
- Daylight on Rt. about Sta. 138 to End.

All recommendations are based on placed $\pm$ on Sec. Line



A-Line

Revision

Station Point

$$\begin{cases} 61+70.5 = 50' \text{ Rt of Orig Loc.} \\ 61+75.0 = \text{"A" Line} \end{cases}$$

$$61+75.9 = 10-00$$

$$+50 = 8-02.9$$

$$+75 = 6-40.4$$

$$61+0 = 4-47.9$$

$$60+75.0 = 2-25.4$$

$$60+42.7 = 0-00$$

$$60+78.75 = 9-53\frac{1}{2}'$$

$$60+0 = 7-44.2$$

$$+75 = 5-51.7$$

$$+50 = 3-57.3$$

$$+75 = 2-06.7$$

$$59 = 0-14.2$$

$$58+96.85 = \text{P.C. (Orig Loc.)}$$

$$Eg. = \frac{61 + 70.5}{P.T. 61 + 75.9}$$

$\Delta 13.20$
 $\Delta 20.00$
 $T. 67.55$
 $L.C. 137.13$
 $R. 38.06$
 $Mon. 61 + 70.5$

$50'$
 $EX 5.9'$

Memory

Align

$RC 60 + 42.7$
 $Original Location$

13.82' tangent

$P.T. 60 + 28.25$
 60

$Co. Road 14$
 $Original Location$

$\Delta 19.47$
 $T. 66.80$
 $L.C. 131.9$
 $R. 38.06$

$RC 58 + 96.85$
 59

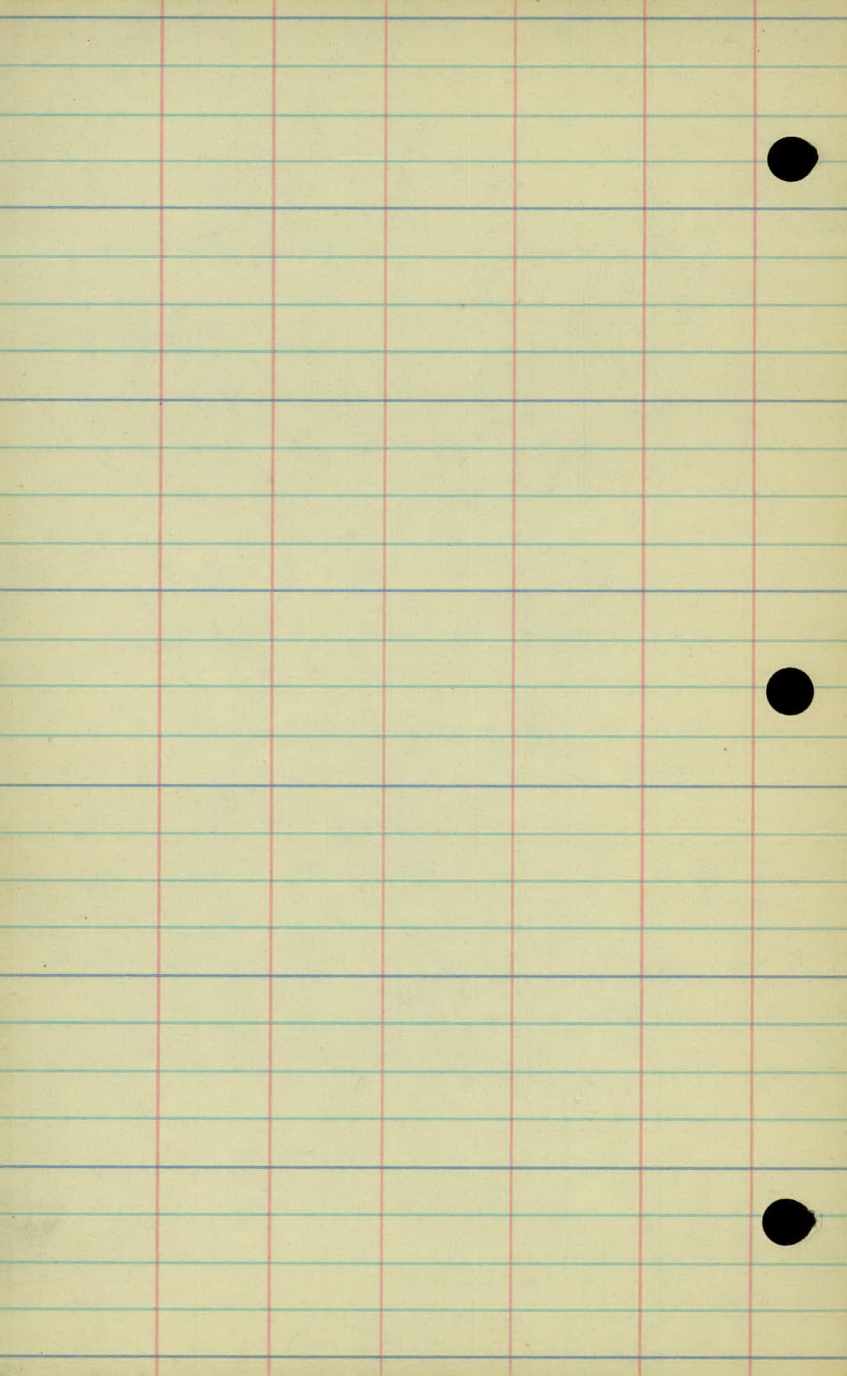
Sta.

Point.

140 ± 0.49 $\square$ Mon. 50' $\rightarrow$

Original location

$\leftarrow$ 50' $\rightarrow$



A-Line
Revision
Cross-sections.
(Sta. 59+0 - 73+62)

Sta.	+	π ✓	-	Elev.
B.M.	8.72	940.22 ✓		931.50
59				38.9 -

+50				37.2 -
-----	--	--	--	--------

60				36.1 -
----	--	--	--	--------

+29 P.T.				34.4 :
----------	--	--	--	--------

+42.5 P.C.				33.1 -
------------	--	--	--	--------

+82				29.9 -
-----	--	--	--	--------

61+0				28.6 -
------	--	--	--	--------

B.M.	1.53	933.03 ✓	8.72	931.50 ✓
------	------	----------	------	----------

+12 = $\frac{1}{2}$ M ^c Menomy.				29.2 -
--	--	--	--	--------

+25				28.5 -
-----	--	--	--	--------

+35				24.7.
-----	--	--	--	-------

+50				22.6 -
-----	--	--	--	--------

T.P.	5.28	927.50 ✓	10.81	922.22 ✓
------	------	----------	-------	----------

Bq, 61+75.9 = 61+70.5

Lk

S

Rt.

46

Top Stone Mon Co. Rd "F" to M^cMerry

$\frac{72.6}{50}$	$\frac{72.5}{23}$	$\frac{1.5}{19}$	$\frac{2.0}{14}$	$\frac{1.3}{1}$	$\frac{1.7}{9}$	$\frac{0.7}{11}$	$\frac{1.2}{28}$	$\frac{2.7}{50}$
-------------------	-------------------	------------------	------------------	-----------------	-----------------	------------------	------------------	------------------

2

$\frac{73.2}{50}$	$\frac{73.4}{31}$	$\frac{2.6}{26}$	$\frac{3.0}{21}$	$\frac{3.7}{21}$	$\frac{3.0}{7}$	$\frac{3.0}{1}$	$\frac{3.1}{4}$	$\frac{2.3}{6}$	$\frac{1.9}{25}$	$\frac{3.9}{50}$
-------------------	-------------------	------------------	------------------	------------------	-----------------	-----------------	-----------------	-----------------	------------------	------------------

4

$\frac{72.2}{60}$	$\frac{72.2}{52}$	$\frac{4.8}{40}$	$\frac{4.8}{34}$	$\frac{5.3}{32}$	$\frac{4.7}{19}$	$\frac{5.0}{8}$	$\frac{4.4}{6}$	$\frac{4.1}{1}$	$\frac{3.9}{15}$	$\frac{5.2}{36}$	$\frac{7.0}{50}$
-------------------	-------------------	------------------	------------------	------------------	------------------	-----------------	-----------------	-----------------	------------------	------------------	------------------

$\frac{5.6}{52}$	$\frac{6.2}{42}$	$\frac{5.8}{30}$	$\frac{6.1}{17}$	$\frac{5.3}{15}$	$\frac{5.8}{1}$	$\frac{7.8}{28}$	$\frac{10.6}{50}$
------------------	------------------	------------------	------------------	------------------	-----------------	------------------	-------------------

$\frac{6.4}{50}$	$\frac{6.1}{33}$	$\frac{6.8}{21}$	$\frac{6.1}{19}$	$\frac{7.1}{1}$	$\frac{9.0}{21}$	$\frac{13.2}{50}$
------------------	------------------	------------------	------------------	-----------------	------------------	-------------------

$\frac{7.5}{50}$	$\frac{7.5}{42}$	$\frac{8.8}{27}$	$\frac{7.2}{22}$	$\frac{10.3}{1}$	$\frac{15.5}{28}$	$\frac{19.0}{50}$
------------------	------------------	------------------	------------------	------------------	-------------------	-------------------

$\frac{8.6}{50}$	$\frac{9.4}{27}$	$\frac{11.6}{1}$	$\frac{13.3}{34}$	$\frac{18.4}{50}$
------------------	------------------	------------------	-------------------	-------------------

$\frac{12.2}{50}$	$\frac{2.7}{30}$	$\frac{3.8}{1}$	$\frac{6.4}{50}$
-------------------	------------------	-----------------	------------------

$\frac{0.4}{50}$	$\frac{0.7}{38}$	$\frac{2.7}{25}$	$\frac{4.5}{1}$	$\frac{6.0}{50} = 2 M^c M.$
------------------	------------------	------------------	-----------------	-----------------------------

$\frac{40.2}{50}$	$\frac{0.4}{39}$	$\frac{5.0}{20}$	$\frac{8.3}{1}$	$\frac{9.5}{15}$	$\frac{7.1}{50} = 5 \frac{1}{2} \text{ in. } M^c$
-------------------	------------------	------------------	-----------------	------------------	---

$\frac{0.2}{50}$	$\frac{0.6}{42}$	$\frac{5.5}{22}$	$\frac{10.4}{1}$	$\frac{14.9}{20}$	$\frac{16.0}{50}$
------------------	------------------	------------------	------------------	-------------------	-------------------

Sta.	+	7	-	Elev.
		927.50		
62 to				22.9
+50				24.7
63				26.3 ✓
T.P.	0.93	924.51 ✓	3.92	923.58 ✓
+60				21.7
64				18.3
T.P.	1.54	917.83 ✓	8.22	916.29 ✓
65				14.5
✓				
+50				14.8
66				15.3
+60				16.1 ✓
T.P.	9.54	926.68 ✓	0.69	917.14 ✓
67				20.1
+60				24.6
68				25.8
+65				25.4

Lt.

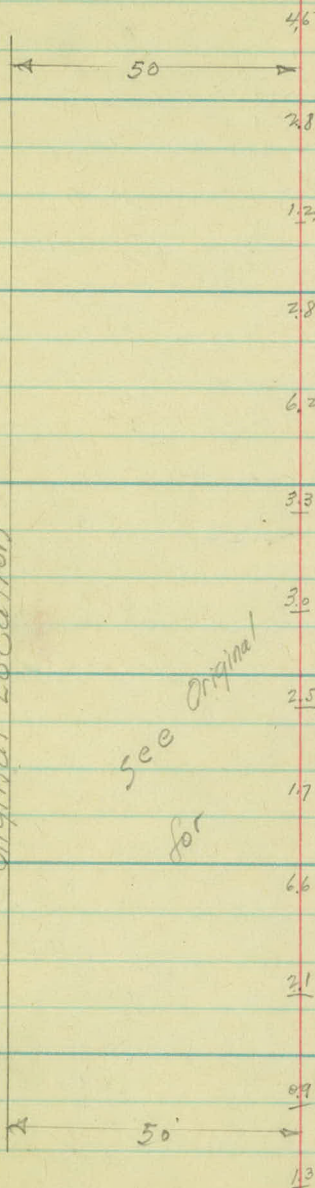
Rt.

47

Original Location

see original
for

Notes
X-sec. Lt. & Rt.



Sta.	+	T ✓	-	Elev.
		926.68		
69+0		✓		26.4
	4.49	928.53	2.64	924.04 ✓
+65				25.2
70				24.0
+60		✓		28.5 ✓
T.P.	1.80	928.20	2.13	926.40
71				27.3
+50				24.4
72				21.6
+50				19.5
73+70				18.5
73+00		✓		13.4
T.P.	1.82	920.72	9.30	918.90 ✓
73+30				08.4
B.M.	3.27	✓	8.80	911.92 ✓
73+62				06.9

0.3

3.34.590
0

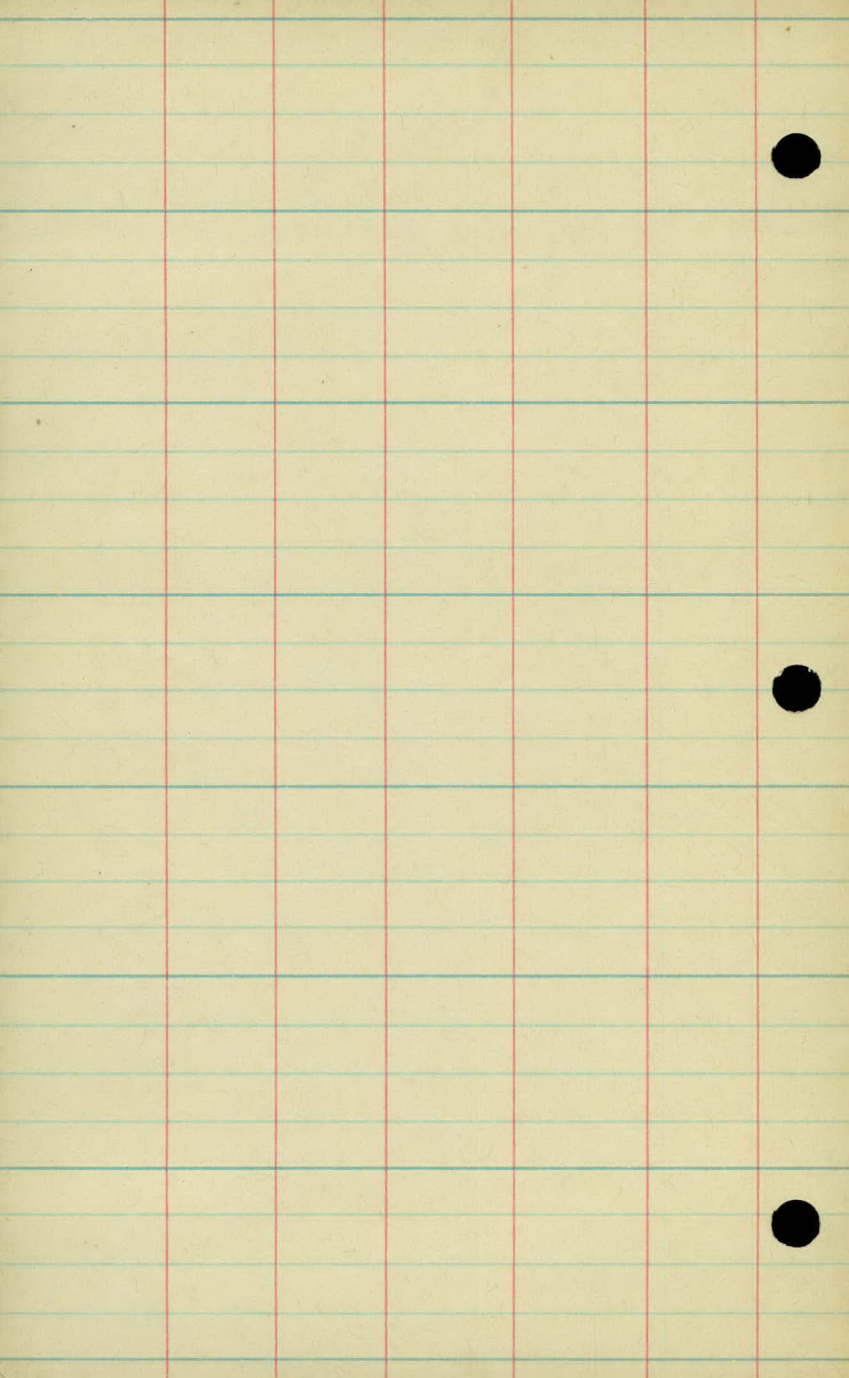
0.9

3.86.65.8
507.4
288.110.5
3012.8
509.714.8

12.3

Top Mon

4.9
506.1
258.39.1
2014.3
3011.2
50



A-Line

Revisions

Cross-Sections

Sta. 97- 97+70

1.

Sta.	+	π	-	Elev.
B.M.	2.86	911.87 ✓		909.01
97+0				04.4

97+35				07.5
-------	--	--	--	------

+48				09.7
-----	--	--	--	------

+60				06.7
-----	--	--	--	------

+70				06.1
-----	--	--	--	------

Lt.

Ct.

Rt.

So

Spike 20" Elm. 137' Lt. 86. 97+60

15

66

97+20-36" 1/2 #37

50

97+35-8" 7/16 #35

50

55443821501850

97+38-12" Elm 1

97+41-12" Elm 5

97+44-10" Birch

-2-2

362150

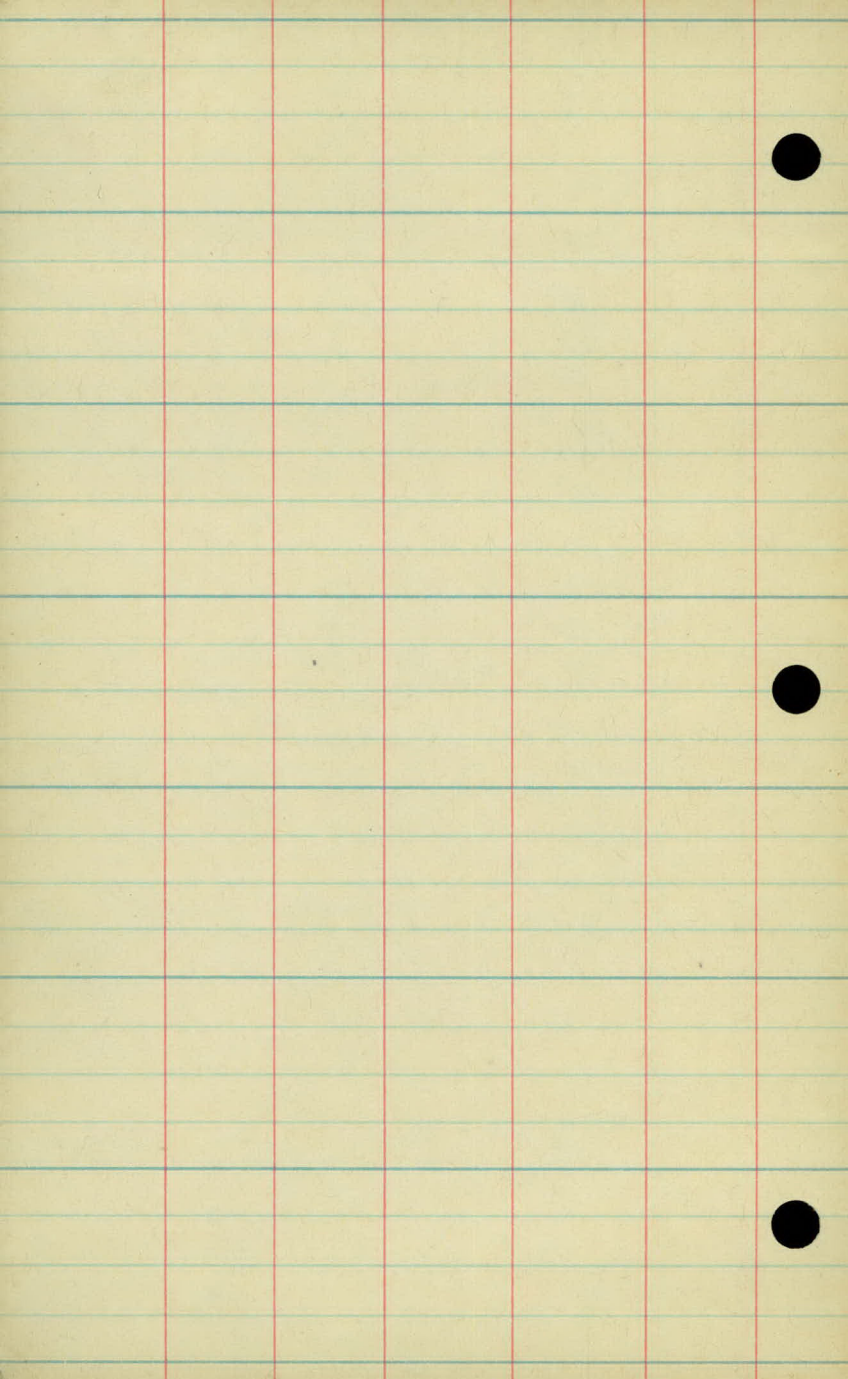
97+56-8" W 111

4852561850

original location

585650

50'



A-Line

Revisions

Cross-Sections.

Sta. 126-138+28

Sta.	+	π	-	Elev.
B.M.	5.11	914.95 ✓		909.84
126				06.0

+50				06.6
-----	--	--	--	------

+80				07.7
-----	--	--	--	------

127				00.4
-----	--	--	--	------

+25				08.7
-----	--	--	--	------

+47				09.7
-----	--	--	--	------

+75				06.4
-----	--	--	--	------

128				05.6
-----	--	--	--	------

+35				09.6
-----	--	--	--	------

+57				06.1
-----	--	--	--	------

129+0				05.5
-------	--	--	--	------

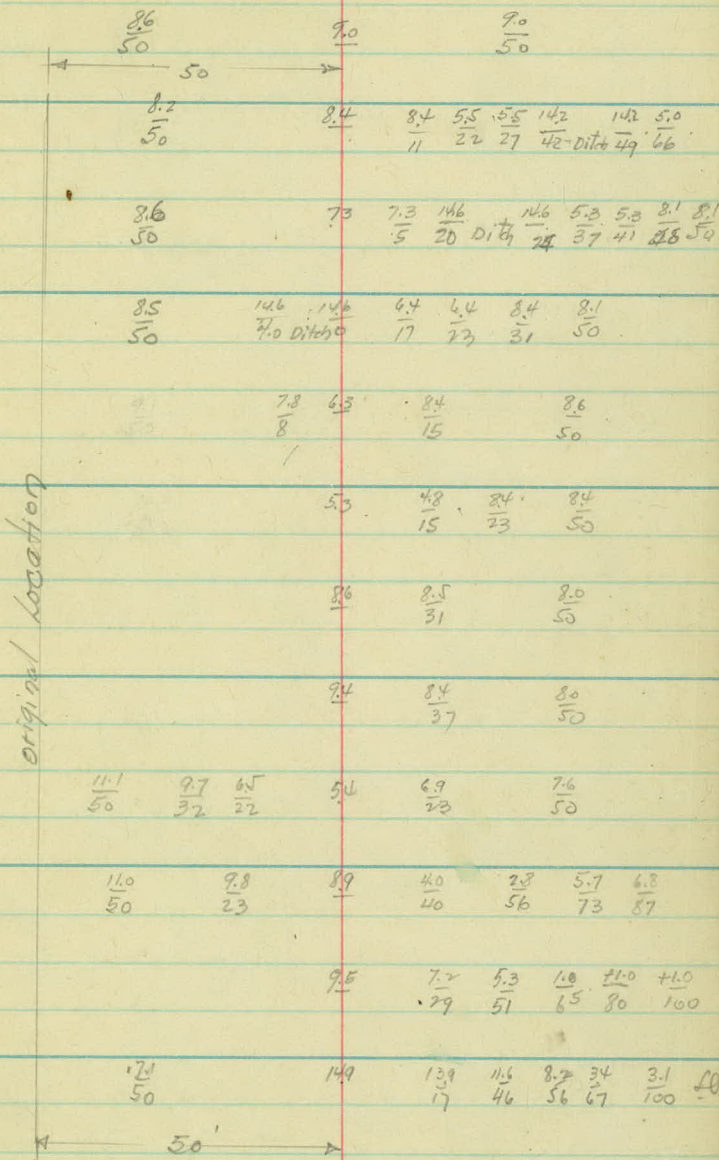
T.P	7.86	921.23 ✓	1.58	913.37 ✓
-----	------	----------	------	----------

129+50				06.3
--------	--	--	--	------

Lt.

Rt.

52



Sta.	+	+	-	Elev.
		921.23		
130				06.6
131				07.3
+50				07.2
132				07.3
+50				08.0
133				08.5
+50				09.1
134				09.9
+40				08.9
135				08.6
B.M.	0.68	910.96	1095	910.28 ✓
136				06.9
+73				05.3

Lt

Z

Rt.

53

$$\begin{array}{r} 146 \\ 0 \end{array}$$

$$\begin{array}{r} 12.7 \\ 38 \end{array} \quad \begin{array}{r} 10.7 \\ 49 \end{array} \quad \begin{array}{r} 5.3 \\ 64 \end{array} \quad \begin{array}{r} 2.6 \\ 68 \end{array} \quad \begin{array}{r} 2.1 \\ 100 \end{array} \quad \begin{array}{r} 2.8 \\ 100 \end{array}$$

$$\begin{array}{r} 139 \\ 34 \end{array}$$

$$\begin{array}{r} 12.1 \\ 34 \end{array} \quad \begin{array}{r} 9.4 \\ 56 \end{array} \quad \begin{array}{r} 4.6 \\ 71 \end{array} \quad \begin{array}{r} 2.9 \\ 100 \end{array} \quad \begin{array}{r} 1.8 \\ 150 \end{array}$$

$$\begin{array}{r} 16.0 \\ 50 \end{array}$$

$$\begin{array}{r} 140 \\ 50 \end{array}$$

$$\begin{array}{r} 12.6 \\ 50 \end{array} \quad \begin{array}{r} 11.5 \\ 50 \end{array} \quad \begin{array}{r} 8.8 \\ 69 \end{array} \quad \begin{array}{r} 7.1 \\ 74 \end{array} \quad \begin{array}{r} 5.2 \\ 100 \end{array} \quad \begin{array}{r} 3.0 \\ 150 \end{array}$$

$$\begin{array}{r} 139 \\ 31 \end{array}$$

$$\begin{array}{r} 12.1 \\ 31 \end{array} \quad \begin{array}{r} 9.0 \\ 60 \end{array} \quad \begin{array}{r} 7.5 \\ 66 \end{array} \quad \begin{array}{r} 6.1 \\ 100 \end{array}$$

$$\begin{array}{r} 15.3 \\ 50 \end{array}$$

$$\begin{array}{r} 132 \\ 21 \end{array}$$

$$\begin{array}{r} 12.1 \\ 21 \end{array} \quad \begin{array}{r} 10.1 \\ 39 \end{array} \quad \begin{array}{r} 6.0 \\ 48 \end{array} \quad \begin{array}{r} 5.0 \\ 100 \end{array} \quad \begin{array}{r} 4.0 \\ 100 \end{array}$$

$$\begin{array}{r} 12.7 \\ 16 \end{array}$$

$$\begin{array}{r} 11.3 \\ 16 \end{array} \quad \begin{array}{r} 9.4 \\ 24 \end{array} \quad \begin{array}{r} 5.7 \\ 30 \end{array} \quad \begin{array}{r} 3.7 \\ 64 \end{array} \quad \begin{array}{r} 3.1 \\ 100 \end{array}$$

$$\begin{array}{r} 14.0 \\ 50 \end{array}$$

$$\begin{array}{r} 13.1 \\ 30 \end{array}$$

$$\begin{array}{r} 12.1 \\ 9 \end{array}$$

$$\begin{array}{r} 10.5 \\ 9 \end{array} \quad \begin{array}{r} 9.7 \\ 14 \end{array} \quad \begin{array}{r} 4.5 \\ 19 \end{array} \quad \begin{array}{r} 4.9 \\ 28 \end{array} \quad \begin{array}{r} 2.4 \\ 58 \end{array} \quad \begin{array}{r} 2.0 \\ 100 \end{array}$$

$$\begin{array}{r} 11.3 \\ 11 \end{array}$$

$$\begin{array}{r} 10.5 \\ 11 \end{array} \quad \begin{array}{r} 6.4 \\ 17 \end{array} \quad \begin{array}{r} 3.5 \\ 59 \end{array} \quad \begin{array}{r} 2.5 \\ 100 \end{array}$$

$$\begin{array}{r} 14.2 \\ 50 \end{array}$$

$$\begin{array}{r} 12.3 \\ 30 \end{array}$$

$$\begin{array}{r} 9.5 \\ 30 \end{array} \quad \begin{array}{r} 7.1 \\ 38 \end{array} \quad \begin{array}{r} 6.6 \\ 64 \end{array} \quad \begin{array}{r} 4.3 \\ 100 \end{array}$$

$$\begin{array}{r} 12.6 \\ 43 \end{array}$$

$$\begin{array}{r} 11.7 \\ 43 \end{array} \quad \begin{array}{r} 10.2 \\ 85 \end{array} \quad \begin{array}{r} 7.0 \\ 96 \end{array} \quad \begin{array}{r} 7.0 \\ 100 \end{array}$$

$$\begin{array}{r} 4.1 \\ 50 \end{array}$$

$$\begin{array}{r} 4.1 \\ 50 \end{array}$$

$$\begin{array}{r} 4.0 \\ 50 \end{array}$$

$$\begin{array}{r} 6.1 \\ 20 \end{array}$$

$$\begin{array}{r} 8.9 \\ 10 \end{array}$$

$$\begin{array}{r} 8.9 \\ 5 \end{array}$$

$$\begin{array}{r} 5.7 \\ 5 \end{array}$$

$$\begin{array}{r} 5.4 \\ 50 \end{array}$$

Sta.	+	*	-	Elev.
------	---	---	---	-------

910.96

+78

02.1

+83

02.1

+92

04.7

137

04.5

+35

06.4

138

08.3

+78

08.8

T.P.

11.75 920.09

76.2

908.34

B.M.

0.61

919.45

L.

Z

R.

54

$$\begin{array}{r} 6.0 \\ 50 \end{array} \quad \begin{array}{r} 6.4 \\ 12 \end{array} \quad \begin{array}{r} 8.9 \\ 5 \end{array} \quad 8.9 \quad \begin{array}{r} 5.5 \\ 5 \end{array} \quad \begin{array}{r} 5.7 \\ 50 \end{array}$$

$$\begin{array}{r} 6.0 \\ 50 \end{array} \quad \begin{array}{r} 6.4 \\ 6 \end{array} \quad \begin{array}{r} 8.9 \\ 0 \end{array} \quad \begin{array}{r} 8.9 \\ 6 \end{array} \quad \begin{array}{r} 5.7 \\ 10 \end{array} \quad \begin{array}{r} 5.7 \\ 50 \end{array}$$

$$6.3 \quad \begin{array}{r} 8.9 \\ 6-12 \end{array} \quad \begin{array}{r} 8.9 \\ 19 \end{array} \quad \begin{array}{r} 5.7 \\ 50 \end{array}$$

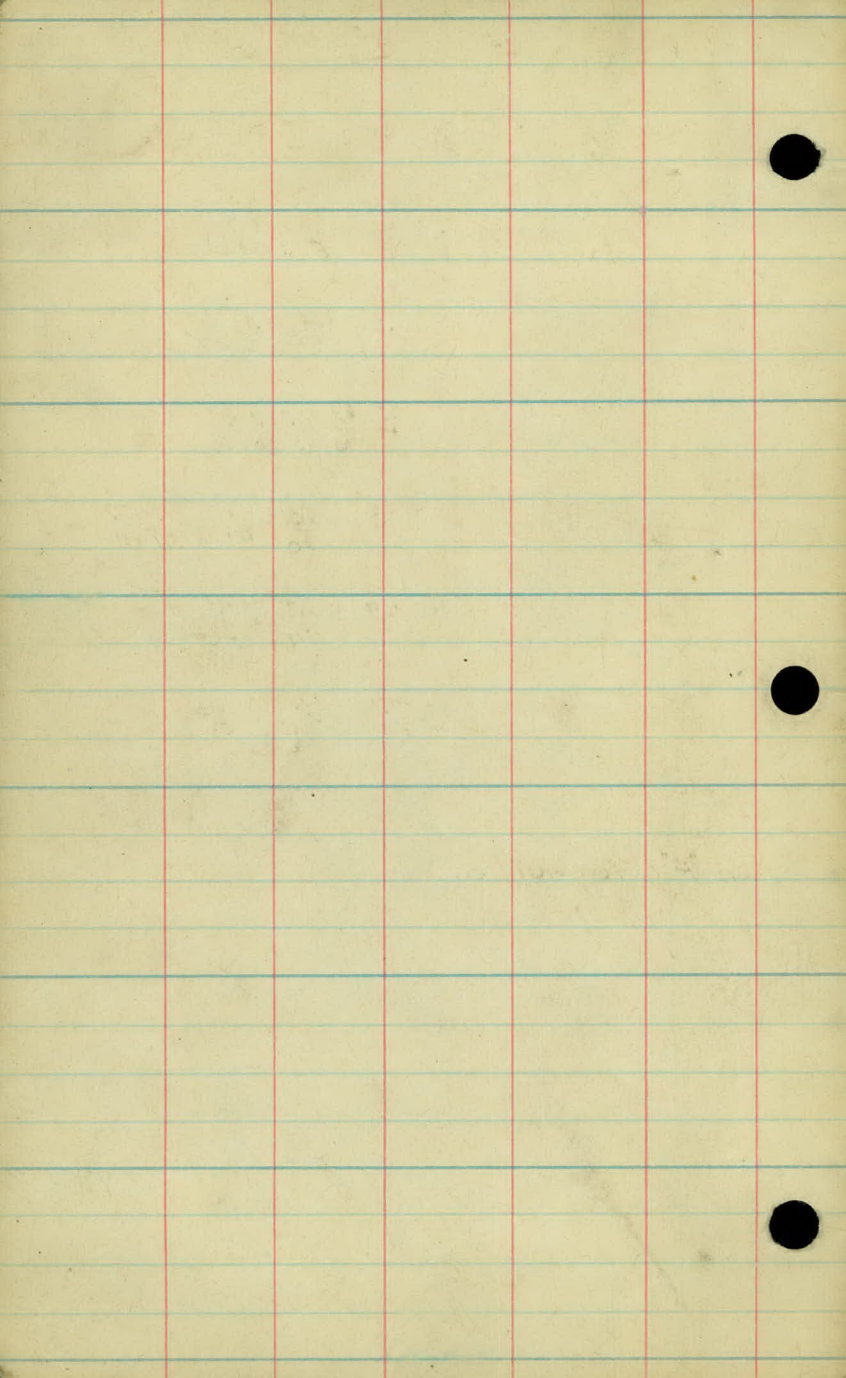
$$\begin{array}{r} 6.5 \\ 10 \end{array} \quad \begin{array}{r} 6.3 \\ 15 \end{array} \quad \begin{array}{r} 8.9 \\ 20 \end{array} \quad \begin{array}{r} 8.9 \\ 26 \end{array} \quad \begin{array}{r} 5.7 \\ 50 \end{array}$$

$$\begin{array}{r} 4.6 \\ 30 \end{array} \quad \begin{array}{r} 5.5 \\ 47 \end{array} \quad \begin{array}{r} 5.7 \\ 54 \end{array} \quad \begin{array}{r} 8.9 \\ 0.1 \end{array}$$

$$2.7 \quad \begin{array}{r} 2.8 \\ 19 \end{array} \quad \begin{array}{r} 4.1 \\ 50 \end{array}$$

$$2.2 \quad \begin{array}{r} 2.6 \\ 34 \end{array} \quad \begin{array}{r} 3.3 \\ 50 \end{array}$$

Mon "F" r Centerville.



Co. Road "F"

Mo Menamy to Centerville Rd.

Sta	+	π	-	Grade
	10.38	941.88		931.50

59				38.5
----	--	--	--	------

+50				36.5
-----	--	--	--	------

60				34.4
----	--	--	--	-----------------

+29				33.1
-----	--	--	--	------

+43				32.3
-----	--	--	--	------

+82				30.4
-----	--	--	--	------

61				29.5
----	--	--	--	------

+12				28.9
-----	--	--	--	------

+25				28.3
-----	--	--	--	------

	1.27	932.77		931.50
--	------	--------	--	--------

+35				27.9
-----	--	--	--	------

			2.25	930.5
--	--	--	------	-------

+50				27.2
-----	--	--	--	------

62				26.7
----	--	--	--	------

Gr. Rod Lt. E. Pt

34 3.1 3.1 / 15 3.1 / 180/31

54 4.7 4.4 / 123/31

6.2 (13) 6.8 / 10.89/31

8.1 9.6 / 12.0 Day 6.7h

(16) 8.9

12.8

12.3

4.9

150 / 48

147 / 93/336

Seiken T.P. J. E. M. & F.

Sta	+	1	-	Grade
-----	---	---	---	-------

932.77

62				25.4
----	--	--	--	------

+50				24.0
-----	--	--	--	------

63				23.0
----	--	--	--	------

+60				22.1
-----	--	--	--	------

T.P	0.81	923.65	2.93	922.84
-----	------	--------	------	--------

64				21.6
----	--	--	--	------

+50				20.9
-----	--	--	--	------

65				20.5
----	--	--	--	------

+50				20.2
-----	--	--	--	------

66				19.9
----	--	--	--	------

+60				19.7
-----	--	--	--	------

67				19.6
----	--	--	--	------

	9.59		2.75	920.90
--	------	--	------	--------

Gr Rod	LT	K	RT
7.4	$\begin{array}{r} +174 \\ 48 \end{array}$	$\begin{array}{r} 106 \overline{) 74} \\ \underline{60} \end{array}$	$\begin{array}{r} 170 \\ -96 \overline{) 342} \end{array}$
8.8	$\begin{array}{r} +100 \\ 48 \end{array}$	$\begin{array}{r} 82 \\ +06 \end{array}$	$\begin{array}{r} 138 \\ -50 \overline{) 250} \end{array}$
9.8	$\begin{array}{r} +84 \\ 48 \end{array}$	$\begin{array}{r} 68 \\ +30 \end{array}$	$\begin{array}{r} 98 \overline{) 142} \\ 90 \overline{) 113} \end{array}$ <i>Doublet</i>
10.7	$\begin{array}{r} +86 \\ 48 \end{array}$	$\begin{array}{r} 21 \overline{) 107} \\ \underline{60} \end{array}$	$\begin{array}{r} 167 \\ -60 \overline{) 270} \end{array}$
2.1	$\begin{array}{r} +54 \\ 48 \end{array}$	$\begin{array}{r} 198 \overline{) 21} \\ \underline{60} \end{array}$	$\begin{array}{r} 106 \\ -85 \overline{) 320} \end{array}$
2.8	$\begin{array}{r} 48 \overline{) 12} \\ \underline{48} \end{array}$	$\begin{array}{r} 32 \overline{) 48} \\ \underline{60} \end{array}$ <i>Doublet</i>	$\begin{array}{r} 122 \\ -94 \overline{) 338} \end{array}$
3.2	$\begin{array}{r} 48 \overline{) 27} \\ \underline{48} \end{array}$	$\begin{array}{r} 37 \overline{) 47} \\ \underline{60} \end{array}$ <i>Doublet</i>	$\begin{array}{r} 124 \\ -92 \overline{) 334} \end{array}$
3.5	$\begin{array}{r} +19 \\ 48 \end{array}$	$\begin{array}{r} 253 \overline{) 50} \\ \underline{60} \end{array}$ <i>Doublet</i>	$\begin{array}{r} 122 \\ -87 \overline{) 324} \end{array}$
3.8	$\begin{array}{r} +57 \\ 48 \end{array}$	$\begin{array}{r} 15 \overline{) 51} \text{ (BTP)} \\ \underline{44} \end{array}$	$\begin{array}{r} 125 \\ -87 \overline{) 324} \end{array}$
4.0	$\begin{array}{r} +73 \\ 48 \end{array}$	$\begin{array}{r} 15 \overline{) 46} \text{ BTP} \\ \underline{30} \end{array}$	$\begin{array}{r} 113 \\ -73 \overline{) 290} \end{array}$
4.1	$\begin{array}{r} +102 \\ 48 \end{array}$	$\begin{array}{r} 36 \\ +06 \end{array}$	$\begin{array}{r} 97 \\ -56 \overline{) 262} \end{array}$

Sta	+	π	-	Grade	
		930.49			
67+60				19.5	
68				19.4	T.P. Blue Top RT
	10.00	928.37	12.18		918.31
+65				19.2	
69				19.1	
+65				18.5	
70				17.9	
	5.99	933.33	1.03		927.34
+60				16.8	
71				15.9	
+50				14.5	
72				13.0	
T.P	1.58	944.30	10.61		922.72
+50				11.5	

Gr. Rod.

L.H.

K.

Kt.

1.0

$$\begin{array}{r} +16.0 \\ 48 \end{array}$$

$$\begin{array}{r} 57 \\ +5.1 \end{array}$$

$$\begin{array}{r} 125 \\ 1000/22.0 \text{ Right.} \end{array}$$

11.1

$$\begin{array}{r} +16.9 \\ 48 \end{array}$$

$$\begin{array}{r} 46 \\ +6.5 \end{array}$$

$$\begin{array}{r} 125 \\ 1000/31.6 \text{ Right} \end{array}$$

Rail 6" out of Sdg. 68-25

9.2

$$\begin{array}{r} 89.0.8 \\ 48/16.3 \end{array}$$

9.3

10.8

$$\begin{array}{r} 54 \\ 48/15.8 \end{array}$$

$$\begin{array}{r} 17 \\ 17.6 \end{array}$$

$$\begin{array}{r} 10.6 \\ 100/41 \end{array}$$

9.9

11.4

$$\begin{array}{r} 76 \\ 48/14.2 \end{array}$$

$$\begin{array}{r} 31 \\ +6.8 \end{array}$$

$$\begin{array}{r} 10.4 \\ 101.0/41 \end{array}$$

10.5

$$\begin{array}{r} 73 \\ 48/15.1 \end{array}$$

$$\begin{array}{r} 37 \\ +6.8 \end{array}$$

$$\begin{array}{r} 8.3 \\ +2.2/41 \end{array}$$

(Stamp.)

16.5

$$\begin{array}{r} 64 \\ 48/17.1 \end{array}$$

$$\begin{array}{r} 45 \\ +12.0 \end{array}$$

$$\begin{array}{r} 7.0 \\ +7.5/41 \end{array}$$

17.4

$$\begin{array}{r} 80 \\ 48/16.4 \end{array}$$

$$\begin{array}{r} 64 \\ +11.0 \end{array}$$

$$\begin{array}{r} 8.9 \\ +8.5/41 \end{array}$$

18.8

$$\begin{array}{r} 91 \\ 48/16.7 \end{array}$$

$$\begin{array}{r} 88 \\ +10.0 \end{array}$$

$$\begin{array}{r} 11.3 \\ +7.5/41 \end{array}$$

20.3

$$\begin{array}{r} 13.3 \\ 48/14.0 \end{array}$$

$$\begin{array}{r} 11.7 \\ +8.6 \end{array}$$

$$\begin{array}{r} 13.8 \\ +6.5/41 \end{array}$$

Top of Sta 7+10

12.8

$$\begin{array}{r} 1.9 \\ 48/10.9 \end{array}$$

$$\begin{array}{r} 48 \\ +8.0 \end{array}$$

$$\begin{array}{r} 7.4 \\ +5.1/41 \end{array}$$

Sta	+	↑	-	Grade
		924.30		
72+70				10.9
73				10.1
	3.30	915.23	1441	911.93
+30				09.2
+62				08.4
B.M.	12			911.93
74				07.5
+56				06.2
75				05.3
+50				04.4
76				03.6
+50				02.9
77				02.3

Gr Rod

Lt.

E

Rt

134

$$\begin{array}{r} 86 \\ + 78 \\ \hline \end{array}$$

$$\begin{array}{r} 11.2 \\ + 2.2 \\ \hline 41 \end{array}$$

$$14.2 \quad \underline{15.7}$$

$$48 \overline{) 64} \\ \underline{48} \\ 17.8$$

$$\begin{array}{r} 15.7 \\ 1000 \overline{) 780} \end{array}$$

6.0

$$48 \overline{) 1.8} \\ \underline{48} \\ 4.2$$

$$\begin{array}{r} 8.1 \\ - 2.1 \\ \hline 19.2 \end{array}$$

6.8

$$48 \overline{) 5.1} \\ \underline{48} \\ 1.7$$

$$\begin{array}{r} 9.0 \\ - 2.2 \\ \hline 19.4 \end{array}$$

top mon. at Sta. 73+48.3

Sta	+	π	-	Grade,
-----	---	-------	---	--------

77+50				01.9
-------	--	--	--	------

78				01.5
----	--	--	--	------

+50				01.2
-----	--	--	--	------

79				01.0
----	--	--	--	------

79+50				01.0
-------	--	--	--	------

80				01.0
----	--	--	--	------

B. Type

81				01.0
----	--	--	--	------

82				01.0
----	--	--	--	------

83				01.0
----	--	--	--	------

84				01.0
----	--	--	--	------

85				01.0
----	--	--	--	------

Gr Rod

Lt

R

Rt,

Sta	+	A	-	Grade
86				01.0
87				01.0
88				01.0
89				01.0
90				01.0
91				01.1
	3.78	912.79		959.01
92				^{0.12} 01.4
93				01.8
94				02.2
				+1.0 +1.80
95				02.6
				+1.6
150				02.8
				+1.4

Gr Rod

Lt

Rt

Rt

11.4

$$13.4 \begin{array}{r} 14.2 \\ - 2.8 \\ \hline \end{array}$$

$$14.7 \\ - 3.3 \\ \hline$$

$$13.1 \begin{array}{r} 26.1 \\ - 3.7 \\ \hline \end{array}$$

11.0

$$13.1 \begin{array}{r} 13.7 \\ - 2.7 \\ \hline \end{array}$$

$$14.1 \\ - 3.1 \\ \hline$$

$$14.7 \begin{array}{r} 26.1 \\ - 3.7 \\ \hline \end{array}$$

10.6

$$21.6 \begin{array}{r} 12.8 \\ - 2.2 \\ \hline \end{array}$$

$$13.0 \\ - 2.4 \\ \hline$$

$$13.3 \begin{array}{r} 23.1 \\ - 2.7 \\ \hline \end{array}$$

10.2

$$21.0 \begin{array}{r} 12.2 \\ - 2.0 \\ \hline \end{array}$$

$$12.1 \\ - 2.2 \\ \hline$$

$$12.2 \begin{array}{r} 21.0 \\ - 2.0 \\ \hline \end{array}$$

10.0

$$21.7 \begin{array}{r} 12.4 \\ - 2.4 \\ \hline \end{array}$$

$$13.6 \\ - 3.6 \\ \hline$$

$$13.5 \begin{array}{r} 25.5 \\ - 3.5 \\ \hline \end{array}$$

Sta	+	π	-	Grade
		912.79		

96				03.0
----	--	--	--	------

1.20

+50				03.2
-----	--	--	--	------

97				03.4
----	--	--	--	------

+35				03.4
-----	--	--	--	------

+48				03.4
-----	--	--	--	------

+60				03.4
-----	--	--	--	------

B.M.				909.01
------	--	--	--	--------

+70				03.5
-----	--	--	--	------

98				03.5
----	--	--	--	------

+50				03.4
-----	--	--	--	------

99				03.4
----	--	--	--	------

+50				03.2
-----	--	--	--	------

B.M.	3.69	912.70		909.01
	4.02	907.92	8.80	903.60

Feb 1937

Gr. Rod

LH

R

RH

9.8

$$23.4 \overline{) 126} \\ \underline{-78} \\ 48$$

$$12.4 \\ \underline{-7.6} \\ 4.8$$

$$12.3 \\ \underline{-7.5} \\ 4.8$$

9.6

11.6

$$41 \overline{) 113} \\ \underline{-82} \\ 31$$

$$10.2 \\ \underline{-9.6} \\ 0.6$$

$$10.1 \\ \underline{-01.5} \\ 41$$

9.5

9.4

$$41 \overline{) 9.0} \\ \underline{-40.4} \\ 49.6$$

$$8.2 \\ \underline{-1.2} \\ 7.0$$

$$8.1 \\ \underline{-2.3} \\ 41$$

9.4

$$41 \overline{) 5.7} \\ \underline{-4.1} \\ 1.6$$

$$4.8 \\ \underline{-4.6} \\ 0.2$$

$$3.2 \\ \underline{-6.2} \\ 41$$

9.4

9.4

$$41 \overline{) 50} \\ \underline{-44} \\ 6$$

$$6.3 \\ \underline{-7.1} \\ 0.8$$

$$6.7 \\ \underline{-2.7} \\ 41$$

Spike 24" Elm 137' Lt. Sda 97+60

9.3

9.3

$$41 \overline{) 7.0} \\ \underline{-12.3} \\ 2.7$$

$$7.0 \\ \underline{-12.3} \\ 2.7$$

$$7.5 \\ \underline{-1.8} \\ 41$$

9.4

$$41 \overline{) 3.7} \\ \underline{-1.7} \\ 2.0$$

$$7.8 \\ \underline{-1.6} \\ 6.2$$

$$8.0 \\ \underline{-1.4} \\ 41$$

9.4

$$41 \overline{) 8.2} \\ \underline{-11.2} \\ 3.0$$

$$8.3 \\ \underline{-1.1} \\ 7.2$$

$$8.5 \\ \underline{-1.7} \\ 41$$

9.6

$$41 \overline{) 8.6} \\ \underline{-11.0} \\ 3.6$$

$$8.7 \\ \underline{-1.9} \\ 6.8$$

$$9.0 \\ \underline{-1.6} \\ 41$$

Sta	+	π	-	Grade	
		907.92			
100				03.0	
+50				02.8	+2
101				02.6	+4
+50				02.4	+5
102				02.2	
+50				02.0	
103				01.8	
+50				01.6	+4
104				01.4	+2
T.P.	8.76	907.96	8.72		899.20
+50				01.2	
105				01.0	

Gr. Rod	wt	$\frac{L}{A}$	RT
4.9 <u>1.2</u>	6.4 41 $\frac{45}{70.4}$	$\frac{48}{+0.1}$	$\frac{4.9}{50.5} / 41$
5.1 <u>1.1</u>	6.6 41 $\frac{57}{80.9}$		
5.3		<u>9.0</u> - Peat Ex.	
5.5		9.4	
5.7		<u>9.9</u>	
5.9		<u>11.2</u>	
6.1			
6.3		10.7	
6.5		9.9	
6.8		8.6	
7.0 BS	11 $\frac{46}{72.4}$	$\frac{6.2}{+0.8}$	$\frac{6.7}{+0.3} / 41$

907.96

Sta	+	-	Grade
105+50			00.7
B.M.		2.04	905.91
106			00.4
+50			00.1
+78			99.9
107			99.8
+55			99.4
108			99.0 ^{+2.5}
+50			98.6 ^{+2.50}
109	1.40	907.32	98.2 ^{+7.5}
+50		2.04	97.8 ^{+1.0}
110			97.4
+58			97.0
111			96.8

Gr. Rod.

Lft.

Rt.

Rt.

7.3

$$\begin{array}{r} 41 \overline{) 4.7} \\ + 1.4 \end{array}$$

$$\begin{array}{r} 53 \\ + 20 \end{array}$$

$$\begin{array}{r} 6.5 \\ + 0.8 \end{array} / 41$$

Spk Top W/10W Sfd. 5.2 Lft. 10.5 + 9.2

7.4

$$\begin{array}{r} 41 \overline{) 4.1} \\ + 3.5 \end{array}$$

$$\begin{array}{r} 41 \\ + 3.5 \end{array}$$

$$\begin{array}{r} 4.8 \\ + 2.9 \end{array} / 41$$

7.9

$$\begin{array}{r} 41 \overline{) 2.9} \\ + 4.0 \end{array}$$

$$\begin{array}{r} 38 \\ + 4.1 \end{array}$$

$$\begin{array}{r} 4.4 \\ + 3.5 \end{array} / 41$$

8.1

$$\begin{array}{r} 41 \overline{) 4.7} \\ + 3.4 \end{array}$$

$$\begin{array}{r} 45 \\ + 3.6 \end{array}$$

$$\begin{array}{r} 5.1 \\ + 3.0 \end{array} / 41$$

8.2

$$\begin{array}{r} 41 \overline{) 8.3} \\ + 11.4 \end{array}$$

$$\begin{array}{r} 20 \\ + 11.2 \end{array}$$

$$\begin{array}{r} 7.5 \\ + 0.7 \end{array} / 41$$

8.6
1.5

10.1

$$\begin{array}{r} 41 \overline{) 9.8} \\ + 10.8 \end{array}$$

10.1 - Perf. Exc.

$$\begin{array}{r} 9.5 \\ + 0.5 \end{array} / 41$$

9.0

10.5

$$\begin{array}{r} 41 \overline{) 10.5} \\ + 10.5 \end{array}$$

11.5 - Perf. Exc.

$$\begin{array}{r} 10.5 \\ + 1.0 \end{array} / 41$$

9.4

12.7 - Perf. Exc.

9.8

$$\begin{array}{r} 14.1 \\ - 4.3 \end{array}$$

6.92 907.32 903.34 10.90 596.42

Sta + 1 - Grade
111+50 96.7

112 96.6

+60 96.6

113 96.8

903.341

+40 97.0

+65 97.1

B.M. 2.90 903.34 2.90 (900.44) ✓

114 97.4

B.M. 3.02 900.32

+45 97.8

115 98.2

+30 98.4

116 99.0

+50 99.4

6.5

$$\frac{8.0}{1000} / 41'$$

6.3

$$41' \overline{) \frac{7.8}{1000}}$$

$$\frac{6.6}{-0.3}$$

$$\frac{5.3}{+1.0} / 41'$$

6.2

$$41' \overline{) \frac{5.4}{+0.8}}$$

$$\frac{5.0}{+1.2}$$

$$\frac{4.4}{+1.8} / 41'$$

+ on Blue Rock 8' Rt. 113+84 Take notes

5.9

$$41' \overline{) \frac{4.3}{+1.6}}$$

$$\frac{3.9}{+2.0}$$

$$\frac{4.9}{+1.0} / 41'$$

Top Blue Rock 53' Rt. 113+75

5.5

$$41' \overline{) \frac{3.9}{+1.6}}$$

$$\frac{3.1}{+0.4}$$

$$\frac{7.0}{1000} / 41'$$

5.1

$$41' \overline{) \frac{5.3}{101.3}}$$

4.9

$$41' \overline{) \frac{6.0}{100.4}}$$

4.3 5.8

$$41' \overline{) \frac{5.8}{100.0}}$$

9.3 Batten

3.9 5.4

7.9 Batten

516	+	X	-	Grade
		903.34		

117				99.8
	6.08	905.41	4.01	899.33

118				00.6
-----	--	--	--	------

119				01.4
-----	--	--	--	------

120				01.2
-----	--	--	--	------

121				03.0
-----	--	--	--	------

122				03.8
-----	--	--	--	------

123				04.6
-----	--	--	--	------

T.P.	7.17	910.86	1.72	903.69
------	------	--------	------	--------

124				05.4
-----	--	--	--	------

+50				05.8
-----	--	--	--	------

125				06.2
-----	--	--	--	------

126				06.8
-----	--	--	--	------

B.M.	1.09		1.09	909.80
------	------	--	------	--------

+50				07.0
-----	--	--	--	------

	4.63	914.43		909.80
--	------	--------	--	--------

3.5

81 extra
4.64.8 03
~~4.7~~7.2
-2.4

4.0

41' 53
20.35.9
-7.9

5.9/20.7

3.6 01
1.8

3.2

41' 43 20.7 5.1
20.0 -1.95.4
-7.2

5.3/21.3

2.4 89
1.5

41' 36 20.3

4.8
-2.4

5.4/24.0

1.6 31

41' 27 20.4

3.8
-2.2

4.8/24.6

0.8

41' 02 20.6

2.9
-2.1

3.6/23.4

5.5

41' 58 20.1 ✓

6.5
-7.0

2.9/22.2

5.1

41' 55 20.1

6.2
-7.1

3.4/18.9

4.7 61 ✓

41' 53 20.09

5.8
-7.1

5.9/20.3/41'

4.1

41' 46 20.0

4.8
-0.7

4.2/20.2/41'

12" W-0.0 70' Lt. 1/2 120x60

3.9 10.4 900.5 43' 4.0
20.6

0.2

900.5 - 20 - Cult. - 900.8
20

Sta. + K - Grade.

914.43

127

07.2

+25

07.2

+47

07.3

+75

07.4

128

07.4

+35

07.5

+57

07.5

129

07.6

+50

07.7

130

07.8

07.9

131

08.0

+50

08.1

13.58

921.80

6.21

908.22

$$\begin{array}{r} 3.7 \text{ dit} \\ 7.2 \quad 900.6 \\ 13.9 \end{array}$$

$$\begin{array}{r} 42 \overline{) 7.5} \\ 126.4 \end{array}$$

$$\begin{array}{r} 11.2 \\ -4.0 \end{array}$$

$$\begin{array}{r} 7.7 \\ 101.0 / 41 \end{array}$$

$$7.2 \quad 13.9$$

$$\begin{array}{r} 43 \overline{) 2.8} \\ 185.1 \end{array}$$

$$\begin{array}{r} 5.2 \\ +7.0 \end{array}$$

$$7.1 \quad 8.6$$

$$\begin{array}{r} 14. \text{ dit} \\ 30.7 \overline{) 8.6} \\ 120.0 \end{array}$$

$$\begin{array}{r} 5.4 \\ +7.7 \end{array}$$

$$\begin{array}{r} 7.8 \\ 120.8 / 41 \end{array}$$

$$7.0$$

$$\begin{array}{r} 8.1 \\ -1.1 \end{array}$$

$$7.0$$

$$\begin{array}{r} 14. \text{ dit} \\ 36.8 \overline{) 8.5} \\ 120.0 \end{array}$$

$$\begin{array}{r} 9.0 \\ -2.0 \end{array}$$

$$\begin{array}{r} 7.3 \\ 121.2 / 41 \end{array}$$

$$6.9$$

$$8.4$$

$$\begin{array}{r} 7.5 \\ 120.9 / 98 \end{array}$$

$$6.8$$

$$\begin{array}{r} 10.8 \text{ Real} \\ -4.0 \text{ exc.} \end{array}$$

$$\begin{array}{r} 9.2 \\ 14.2 \end{array}$$

$$\begin{array}{r} 4.9 \\ +9.3 \end{array} \quad \begin{array}{r} 78 \\ 150 \end{array} \quad \begin{array}{r} +20 \\ 150 \end{array}$$

$$6.7$$

$$\begin{array}{r} 11.2 \text{ Return} \\ - \end{array}$$

$$12.1$$

$$\begin{array}{r} 3.7 \\ +10.4 \end{array} \quad \begin{array}{r} 78 \\ 150 \end{array} \quad \begin{array}{r} +11.6 \\ 150 \end{array}$$

$$6.6$$

$$\begin{array}{r} 9.9 \text{ Return} \\ - \end{array}$$

$$14.0$$

$$\begin{array}{r} 3.3 \\ +10.7 \end{array} \quad \begin{array}{r} 78 \\ 150 \end{array} \quad \begin{array}{r} +11.4 \\ 150 \end{array}$$

$$6.5$$

$$12.9$$

$$\begin{array}{r} 2.8 \\ +11.1 \end{array} \quad \begin{array}{r} 78 \\ 150 \end{array} \quad \begin{array}{r} +12.2 \\ 150 \end{array}$$

$$6.4$$

$$13.8$$

$$\begin{array}{r} 2.7 \\ +9.1 \end{array} \quad \begin{array}{r} 78 \\ 150 \end{array} \quad \begin{array}{r} +11.8 \\ 150 \end{array}$$

$$6.3$$

$$13.7$$

$$\begin{array}{r} 7.7 \\ +6.0 \end{array} \quad \begin{array}{r} 78 \\ 150 \end{array} \quad \begin{array}{r} +10.4 \\ 150 \end{array}$$

Sta.	+	-	Grade.
		921.80	
132			08.2
+50			08.3
133			08.4
+50			08.5
134			08.6
B.M.		11.52	910.23
+40			08.7
135			08.8
+50	1.80	912.03	910.23
			09.4
136			10.0
+50			11.2
+78			11.9
137			13.0
+35			14.3
+80			14.8
138			16.0
	13.27	915.16	911.99
		0.04	

$$13.6 \quad 20.4 \overline{) 154} \quad \begin{array}{r} 145 \\ -29 \\ \hline \end{array} \quad \begin{array}{r} 7.8 / 78' \\ +5.8 / 78' \\ \hline \end{array} \quad \begin{array}{r} +9.1 \\ 150' \end{array}$$

$$13.5 \quad \begin{array}{r} \text{Day} \\ \text{Lk} \end{array} 19.3 \overline{) 150} \quad \begin{array}{r} 138 \\ -03 \\ \hline \end{array} \quad \begin{array}{r} 6.2 / 78' \\ +7.2 / 78' \\ \hline \end{array} \quad \begin{array}{r} +9.0 \\ 150' \end{array}$$

$$13.4 \quad \begin{array}{r} \text{Day} \\ \text{Lk} \end{array} 34.0 \overline{) 149} \quad \begin{array}{r} 13.1 \\ +03 \\ \hline \end{array} \quad \begin{array}{r} 3.8 / 78' \\ +9.6 / 78' \\ \hline \end{array} \quad \begin{array}{r} +10.1 \\ 150' \end{array}$$

$$13.3 \quad 41 \overline{) 142} \quad \begin{array}{r} 122 \\ +10 \\ \hline \end{array} \quad \begin{array}{r} 78 / 78' \\ +10.5 / 78' \\ \hline \end{array} \quad \begin{array}{r} +11.3 \\ 150' \end{array}$$

$$13.2 \quad 41 \overline{) 143} \quad \begin{array}{r} 11.8 \\ +14 \\ \hline \end{array} \quad \begin{array}{r} 36 / 78' \\ +9.6 / 78' \\ \hline \end{array} \quad \begin{array}{r} +11.2 \\ 150' \end{array}$$

1-10th Sta. 134+22 30th in cor. F.D.

$$13.1 \quad 41 \overline{) 146} \quad \begin{array}{r} 12.8 \\ +03 \\ \hline \end{array} \quad \begin{array}{r} 61 / 78' \\ +7.0 / 78' \\ \hline \end{array} \quad \begin{array}{r} +11.1 \\ 150' \end{array}$$

$$13.0 \quad 18.6 \overline{) 143} \quad \begin{array}{r} 13.2 \\ -02 \\ \hline \end{array} \quad \begin{array}{r} 11.2 / 78' \\ +1.8 / 78' \\ \hline \end{array} \quad \begin{array}{r} +7.6 \\ 150' \end{array}$$

$$2.6 \quad 21.3 \overline{) 147} \quad \begin{array}{r} 40 \\ -14 \\ \hline \end{array} \quad \begin{array}{r} 11 / 41' \\ 200 / 41' \\ \hline \end{array} \quad \begin{array}{r} 100 \\ 150' \end{array}$$

$$2.0 \quad \begin{array}{r} 53 \\ -3.3 \\ \hline \end{array}$$

$$\begin{array}{r} -7.5 \\ 37.5 \end{array}$$

$$-7.7$$

$$\begin{array}{r} -9.0 \\ 142.0 \end{array}$$

Sta.	+	π	-	Grade
138+28				16.5
		925.26		
+60				16.5
139				17.0
+57				17.0
B.M			5.85	919.46

L

E

RT.

$$\begin{array}{r} -7.3 \\ 26.9 \end{array}$$

$$\begin{array}{r} -88 \\ 414 \end{array}$$

8.5

8.5

$$41 \overline{) \frac{10.5}{200.3}} \quad 249 \overline{) \frac{11.8}{-3.3}}$$

$$\begin{array}{r} 14.7 \\ -6.2 \end{array}$$

$$\begin{array}{r} -2.2 \\ 28 \\ -83 \end{array} / 29.9$$

8.3

$$41 \overline{) \frac{4.5}{+2.8}}$$

$$\begin{array}{r} 83 \\ 80 \end{array}$$

$$\begin{array}{r} 13.0 \\ -4.7 \end{array} / 29.1$$

8.3

$$41 \overline{) \frac{0.8}{+7.5}}$$

$$\begin{array}{r} 41 \\ +4.7 \end{array}$$

$$\begin{array}{r} 9.8 \\ 20.20 \end{array} / 48$$

High point on mont.

X-Sections for Borrow Pit.

Sta	+	-	Elev. Grade.
	771	927.11	919.40

70+60

71+0

71+50

72+0

72+50

T.P.

0.25

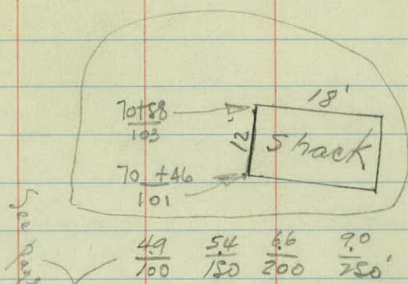
804

919.07

Lt.

±

Rt.



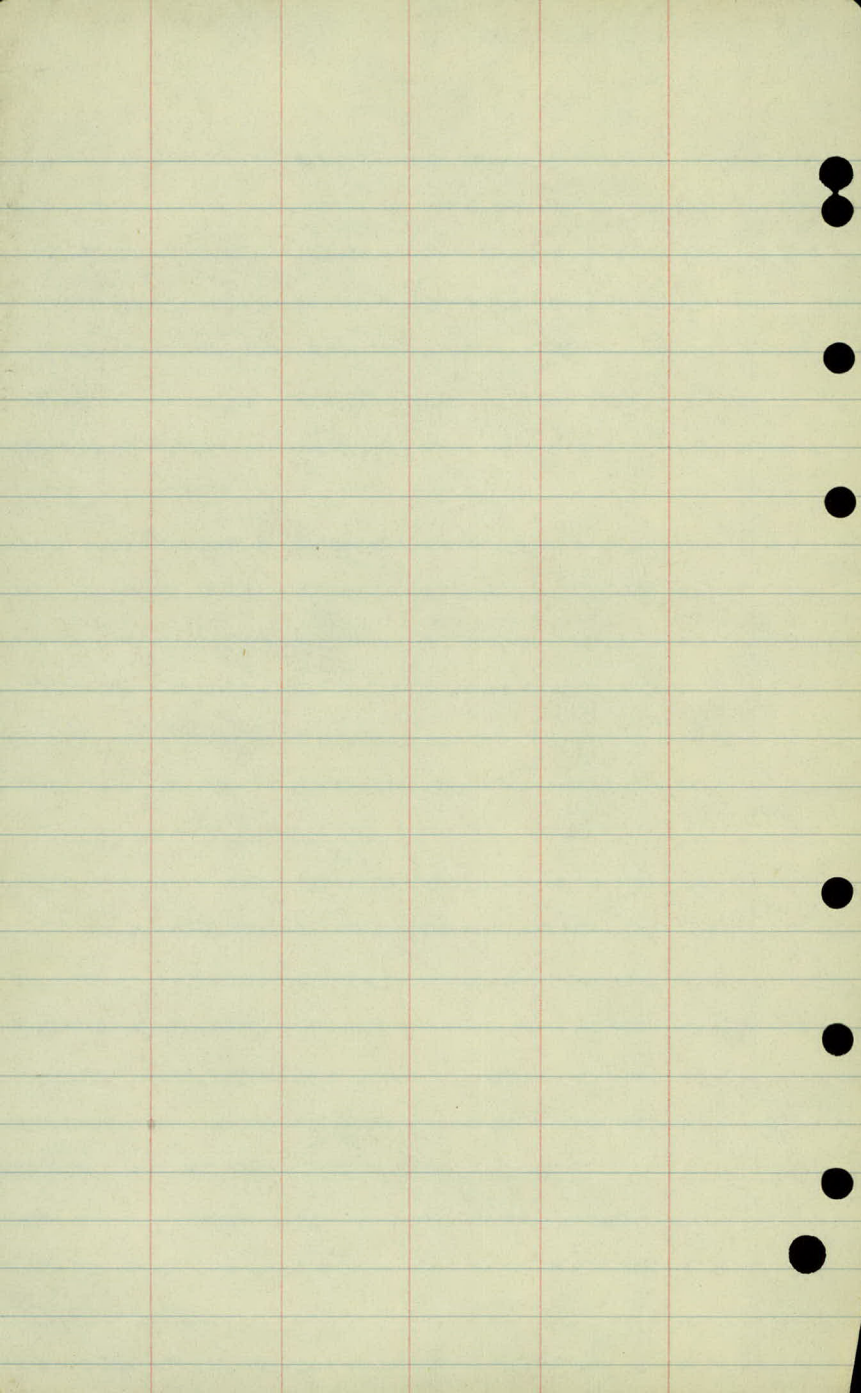
(Make 10:1 or 90:1 ft.)

$$\frac{52}{100} \quad \frac{64}{150} \quad \frac{91}{200} \quad \frac{148}{250}$$

$$\frac{67}{100} \quad \frac{77}{128} \quad \frac{101}{150} \quad \frac{187}{200} =$$

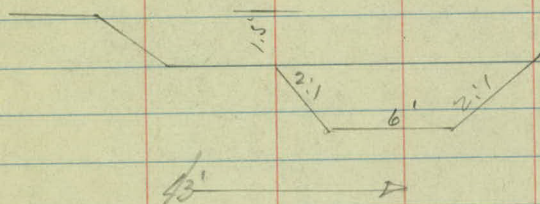
$$\frac{101}{100} \quad \frac{162}{178} \quad \frac{138}{158} =$$

$$\frac{132}{57} \quad \frac{138}{80} \quad \frac{198}{100} =$$



Slope Stakes
for Channel Change
Sta. 126+50 to 137+35

2 Ditch 43' Right.



Sta.	+	-	±	Grade	Ditch grade
B.M.	2.72	912.52			909.80
126+50				07.0	899.9
127+0				07.2	99.92
+50				07.3	99.95
128				907.4	999.97
+50				07.5	900.00
129				07.6	900.02
+50				07.7	900.05
130				07.8	900.07
	5.46	913.98 910.48	4.50	908.02	
+50				07.9	900.10
131				08.0	900.12
+50				08.1	900.15

June 22, 1937

87

43 ——— 2 Ditch

Ditch

12.6

150 / $\frac{60}{106.0}$

$\frac{58}{106.8} / 14.6$

12.55

144 / $\frac{69}{105.7}$

$\frac{61}{106.5} / 16.0$

12.55

140 / $\frac{68}{105.7}$

$\frac{59}{106.0} / 16.2$

142 / $\frac{69}{105.6}$

$\frac{55}{107.0} / 17.0$

12.5

158 / $\frac{60}{106.4}$

$\frac{3.2}{10.92} / 2.4$

12.4

186 / $\frac{60}{106.3}$

12.45

152 / $\frac{64}{106.1}$

*Barrow
not exc
@ this time*

12.40

160 / $\frac{59}{106.5}$

12.38

166 / $\frac{66}{106.8}$

12.36

166 / $\frac{66}{106.8}$

$\frac{60}{107.4} / 17.8$

12.33

168 / $\frac{65}{106.9}$

$\frac{64}{107.0} / 17.0$

Grade Ditch
grade

913.48

132 08.2 900.17

+80 08.3 900.20

133 08.4 00.23

+50 08.5 900.25

134 08.6 00.27

+50 08.7 900.30

135 08.8 00.32

+50 08.9 900.35

136 10.0 00.37

+80 11.2 900.40

137 13.0 00.42

+80 900.48

499

920.96

0.51

2.53

911.97

$$13.30 \quad 17.4 \begin{array}{r} 5.1 \\ \hline 107.2 \end{array}$$

$$10.68 \begin{array}{r} 6.5 \\ \hline 16.6 \end{array}$$

$$13.28 \quad 19.4 \begin{array}{r} 5.1 \\ \hline 108.2 \end{array}$$

$$10.85 \begin{array}{r} 4.8 \\ \hline 20.0 \end{array}$$

$$13.25 \quad 20.4 \begin{array}{r} 4.6 \\ \hline 108.7 \end{array}$$

$$10.90 \begin{array}{r} 4.3 \\ \hline 21.0 \end{array}$$

$$13.23 \quad 21.2 \begin{array}{r} 4.1 \\ \hline 109.1 \end{array}$$

$$10.91 \begin{array}{r} 4.1 \\ \hline 21.2 \end{array}$$

$$13.20 \quad 21.2 \begin{array}{r} 4.1 \\ \hline 109.1 \end{array}$$

$$10.94 \begin{array}{r} 3.8 \\ \hline 21.8 \end{array}$$

$$13.18 \quad 20.0 \begin{array}{r} 4.7 \\ \hline 108.5 \end{array}$$

$$10.93 \begin{array}{r} 3.9 \\ \hline 21.6 \end{array}$$

$$13.15 \quad 19.0 \begin{array}{r} 5.2 \\ \hline 108.0 \end{array}$$

$$10.84 \begin{array}{r} 4.8 \\ \hline 19.8 \end{array}$$

$$13.13 \quad 20.2 \begin{array}{r} 4.5 \\ \hline 108.6 \end{array}$$

$$10.70 \begin{array}{r} 6.1 \\ \hline 17.0 \end{array}$$

$$13.1 \quad 19.2 \begin{array}{r} 5.0 \\ \hline 108.1 \end{array}$$

$$10.63 \begin{array}{r} 6.8 \\ \hline 18.6 \end{array}$$

$$13.08 \quad 21.8 \begin{array}{r} 3.7 \\ \hline 109.4 \end{array}$$

$$10.54 \begin{array}{r} 7.7 \\ \hline 18.8 \end{array}$$

$$13.05 \quad 20.4 \begin{array}{r} 4.7 \\ \hline 108.9 \end{array}$$

$$10.48 \begin{array}{r} 8.2 \\ \hline 17.6 \end{array}$$

$$13.0 \quad m$$

$$10.40 \begin{array}{r} 8.4 \\ \hline 17.1 \end{array}$$

	+	+	-	Elev.
	2.78	912.58		909.80
N. end 36" Culv.			11.88	900.70
So. " 36"			12.16	900.42
F/Line Ditch Sta 120+50			12.7	899.9
43'-Rt.				
	0.15	919.61		919.46
	3.18	913.34	9.45	910.16
F/Line 36" Culv			12.82	900.52
thru Cent. Road				

67175 L 15" X 36" CM

67175 L 12" X 20" CM

107150 L Pl. 24" X 50" CM,

107150 L Pl. 24" X 44"

11310 L Pl. 36" X 44" Fill 2' E

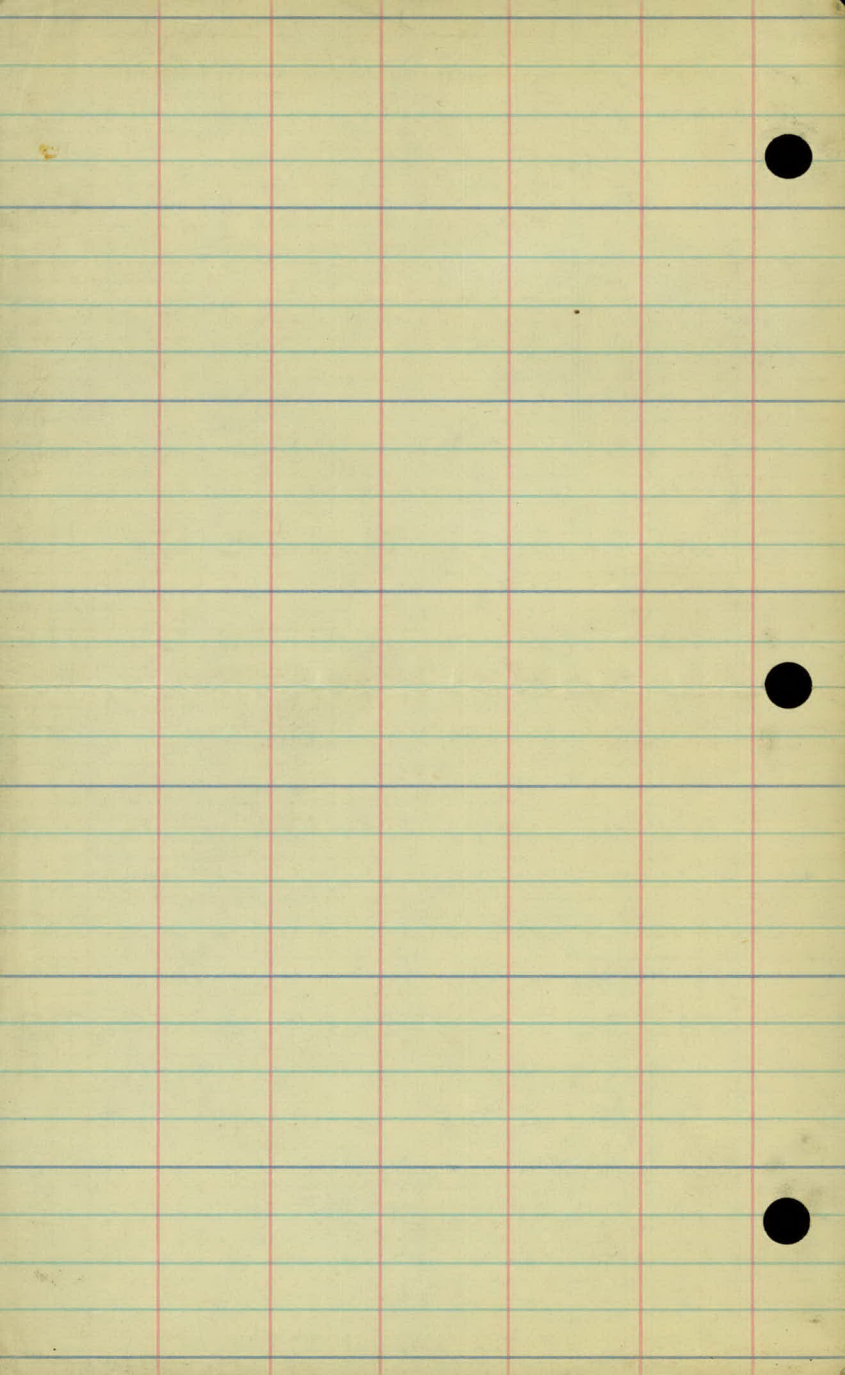
11810 L Pl. 24" X 44" Fill 1.7' E
Ditch from 11710

176150 L 42" X 88" CM.
36"

52
80
122

80
132

22
28
30



	24"	12"	Bands
18'	22'	(20')	3-24"
18'	22'		1-15"
36	26'		1-36"
	24'		(2-36") in place
	22'		
	22'		

40.6
1.8
m.

138

36"

30'
22'
22'
28'
30' } In place

50
44
44
138 ✓

10 to

Gutter Stakes

Co. Rd. E of Centerville Rd.

N. Side of Ditch

East half

Top
Plank

Gutter
Gr. Rod.

0	+00	5.90	6.40 ✓
	+25		6.45 ✓
	+50	6.02	6.50 ✓
	+75		6.55 ✓
1		6.12	6.60 ✓
	+25		6.65 ✓
	+50	6.15	6.70 ✓
	+75		6.75 ✓
2		6.19	6.80 ✓
	+25		6.85 ✓
	+50	6.45	6.90 ✓
	+75		6.95 ✓
3		6.48	7.00 ✓
	+25		7.05 ✓
	+50	6.61	7.10 ✓
	+75		7.15 ✓
4		6.70	7.20 ✓
	+25		7.25 ✓
	+50	6.89	7.30 ✓
	+75		7.35 ✓
5		6.90	7.40 ✓
	+25		7.45 ✓
	+46	7.0	7.50 ✓

= Top End Plank.

Top End Plank at Spillway

West half.

Top
Plank.

Gutter
Gr. Rod.

0 +00 6.21 6.60 ✓

+50 6.70 ✓

1 6.24 6.80 ✓

+50 6.90 ✓

2 6.46 7.00 ✓

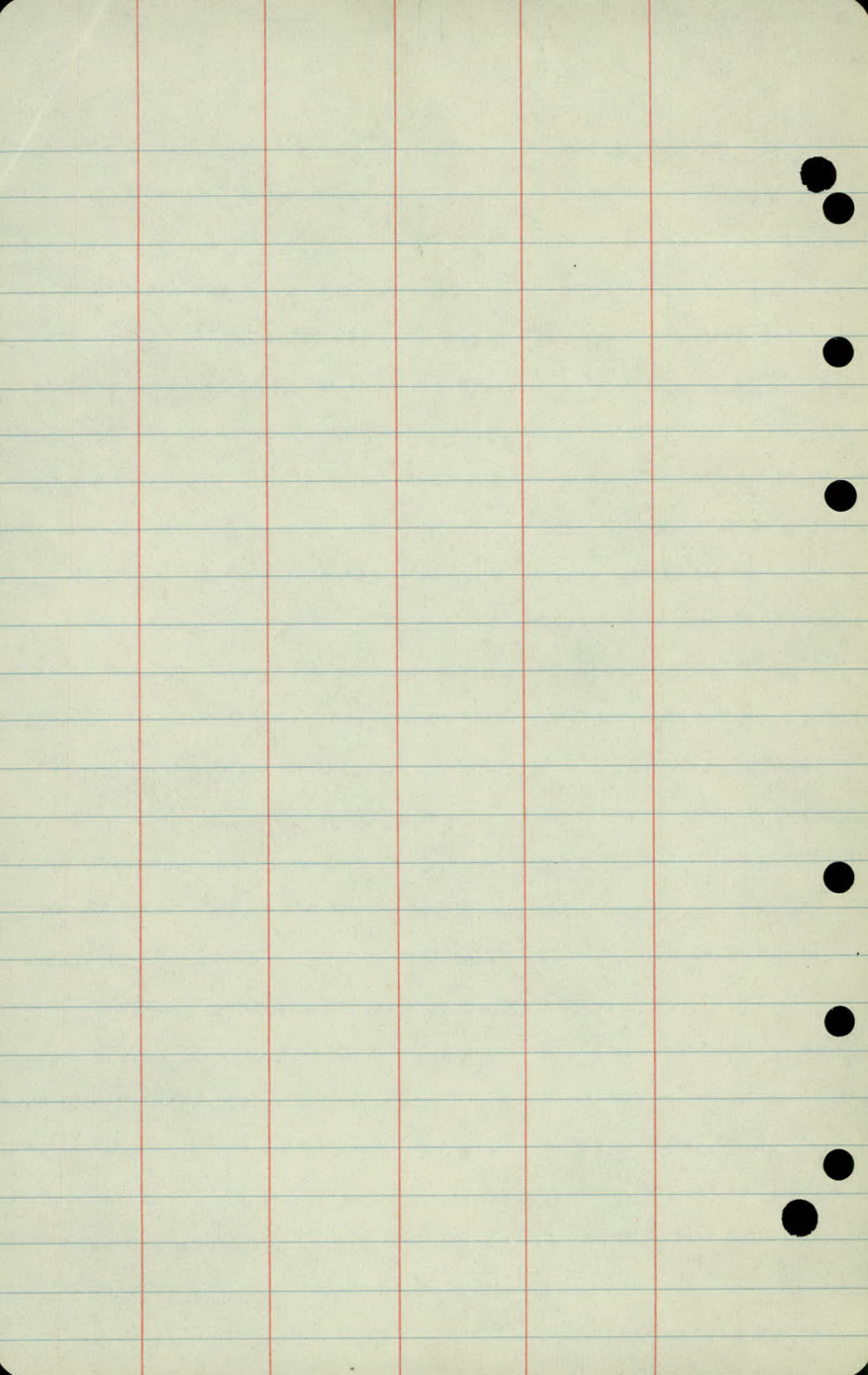
+48 6.59 7.1 ✓

+75 7.15 ✓

3 7.2 ✓

+25 7.30

Top Plank.



Co. Rd "F"

Curb & Spillway Grades.

So. Side Pitch

Sta.	+	π	-	Elev.
------	---	-------	---	-------

Sta 00 = E. End Curb.

+25

+50

+75

+87 Spillway

1
+25

+50

+75

+92 $\frac{1}{2}$

2

+25

Top Curb	Ground		
3.93	4.4	4.4	✓
4.03	4.7	4.6	✓
4.10	4.7	4.77	✓
4.07	5.0	4.94	✓
4.02 4.02	4.8	5.02	✓
3.99	4.7	5.05	✓
4.12	4.7	5.1	✓
4.08	4.7	5.15	✓
4.15	4.9	5.2	✓
4.17	5.1	5.24	✓
4.17	5.0	5.25	✓
4.28	5.0	5.3	✓

2+50

+75

+97 Spillway

3+25

+50

+75

+85 $\frac{1}{2}$

4

+25

+50

+72 Spillway

5

+25

+50

+57

5 +95

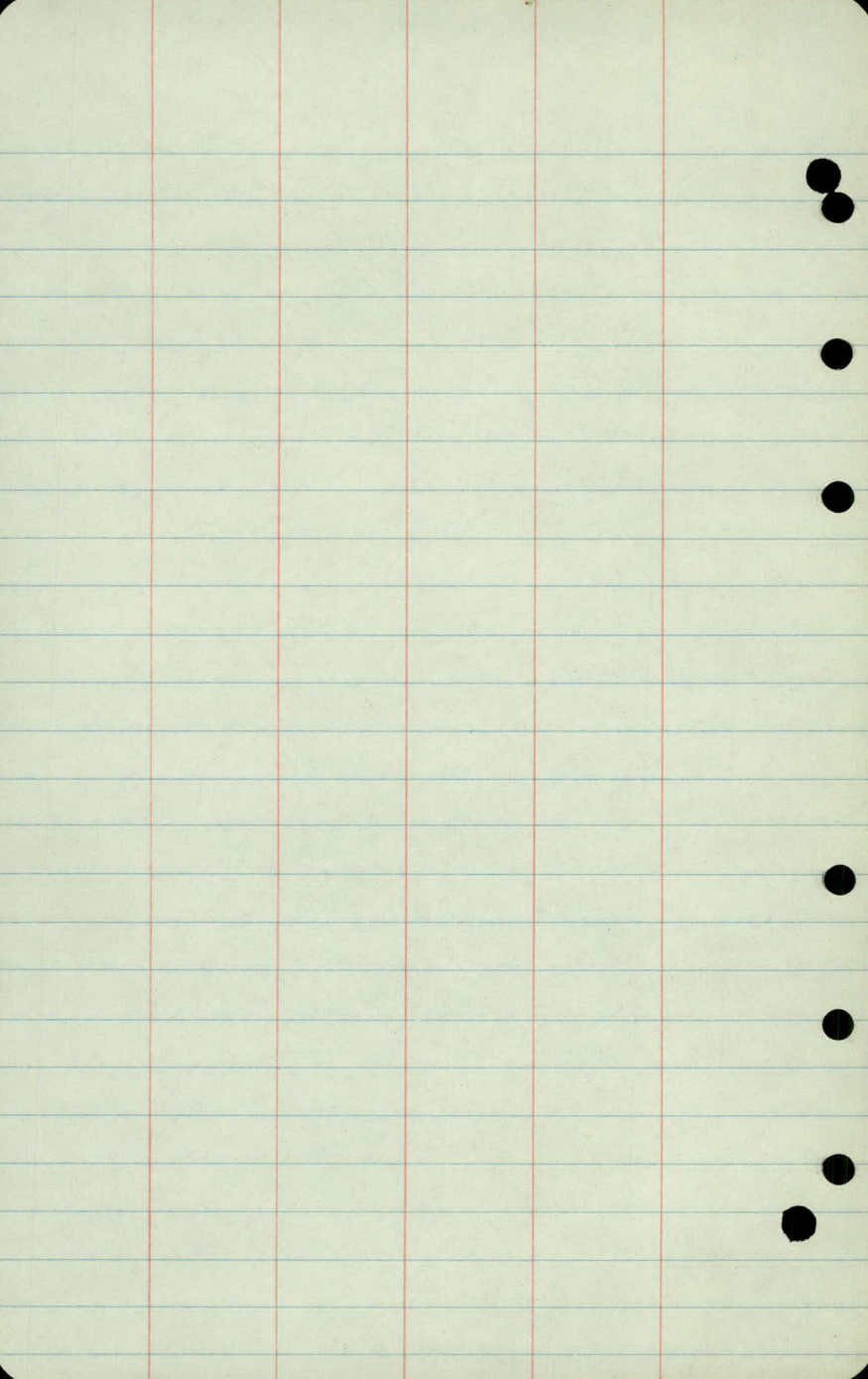
6 +21 Spillway

+50

+75

Top Curb	Ground	
4.26	5.1	5.35 ✓
4.30	5.2	5.4 ✓
4.83		
4.63	5.1	5.45 ✓
4.57	5.1	5.5 ✓
4.64	5.1	5.55 ✓
4.59	5.3	5.6 ✓
4.71	5.3	5.62 ✓
4.72	5.4	5.65 ✓
4.64	5.3	5.7 ✓
4.71	5.4	5.75 ✓
4.98		
4.87	5.3	5.8 ✓
4.85	5.3	5.7 ✓
4.93	5.2	5.55 ✓
4.87	5.1	5.4 ✓
4.82	5.3	5.3

4.76	4.9	4.9 ✓
5.08		
5.20	5.2	5.6 ✓
4.97	5.0	5.4 ✓
5.02	5.2	5.2 ✓
4.77	4.5	4.5



Ditch stakes

Co RIF" at Centerville Rd

Sta	+	-	Grade
B.M.	2.13	911.93	909.80

126 +50

900.2

127

00.3

+50

00.4

128

00.5

+50

00.6

E/cv Present Gr. = 00.21

129 +04

~~00.71~~

T.P.

2.45

911.55

2.83

909.10

+44

00.30

130

00.31

+50

00.32

131

00.33

+50

00.34

Gr. Rod

Spl. in 12" W.O. 90' Lt 126100

12.23 ✓

~~11.79~~ ✓

12.13

~~11.43~~ ✓

12.03 10:53 ✓

~~11.53~~

11.93 ✓

~~11.43~~

11.83

~~11.33~~

11.72

~~11.22~~ = W. End Culv.

11.25 E. End Culv.

11.24 ✓

11.23 ✓

11.22 ✓

11.21 ✓

Sta	+	π	-	Grade
		911.55		

132				00.35
-----	--	--	--	-------

	+50			00.35
T.P.	4.99	912.19	4.35	907.20

133				00.36
-----	--	--	--	-------

	+50			
--	-----	--	--	--

134

	+50			
--	-----	--	--	--

135	+06			
-----	-----	--	--	--

900.39

Gr. Rod.

11.20 ✓

11.20 ✓

11.83

11.82 ✓

11.81 ✓

11.81 ✓

11.80

W. End Culk

$$\begin{array}{r}
 912.19 \\
 11.80 \\
 \hline
 910.39
 \end{array}$$

