

Book 10, Dr. 12

OFFICE OF COUNTY ENGINEER
RAMSEY CO. MINN.

PLAN. Survey

KADNAIS BLVD.

From Rice St. To Kadnais Blvd

Road Acc't. No. 33-W32
34-W32

L.

fil

12-10-31

Notes Used for
Plans

Proj. 33-W32

Transit Notes
Vodnoie Cut-off

513.30

+27⁸⁶ P.T. ✓

1031

8255

Aug 21 02 Lt

4+58.75 P.L.

+50

445

4

0555

3+87.64 P.C. ✓

218.64

1+69° P.T. .05

1030

9045

5195

+50

2 ↑

1+00 P.L.

Aug 21 Pt

+50

1345

0+29 P.C.

0+00

FAST

5.69° 00 E

x N 89° 58 E

Misty and Cloudy.

12-8-31 Weber
Shooglen
Wilke
Bell
Stemmer

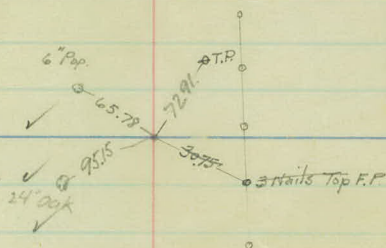
$\Delta 21^{\circ}02'$

$D=150$

$T=71.1$

$L=140.22$

$R=383.07$



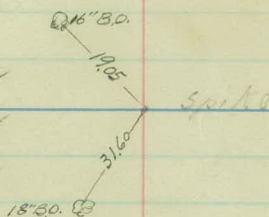
$\Delta 21^{\circ}$

$D=150$

$T=71.0$

$L=140.0$

$R=383.07$



2

2

Rec 190.0
C. W. 1/4 Cor. Sec. 31 - T3p R22'

NOWASSO
Blvd.

Sta. Point Anglt AngPt.

21+90⁵⁵ P.O.T.

✓
N 89° 54' E.

+36⁹⁷ P.T. ✓

7° 41'

15.

5° 50'

14+60⁷⁰ P.I.

15° 22' RIGHT

+50

3° 20'

14

0° 50'

13+83³ P.C. ✓

✓
N 74° 32' E.

11+95⁴⁹ P.T. ✓

7° 43'

+50

5° 26' 5"

11+18⁹ P.I.

15° 26' 44"

11

2° 56' 5"

+50

0° 26' 5"

10+41¹⁰ P.C. ✓

✓
N 89° 58' E.

Spt

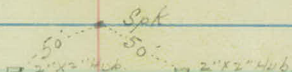
$\Delta 1522$ RT

D 10°

T = 77.40 ✓

L = 153.67 ✓

R = 573.686 ✓



$\Delta 1526$ LT

D 10°

T = 77.74 ✓

L = 154.33 ✓

R = 573.686 ✓

74.13
OT.P.

23.20 - OT.P.
Spt.

OT.P.

+1250 P.T. ✓ Anyht Anyht

✓
S 54° 12' E

P.T.

5824' Height

X

✓
1400'
1200'
1130'
1010'
900'
740'
630'
5190'
400'
300'
13030'
01730'

✓
N 46° 24' E

+9057 P.T. ✓

1145'
929'
659'
2330' Height
429'
159' _{at 450}

P.T.

2330' Height

N 89° 54' E

P.C.

70 24
 11.5 min 3 PM.
 3985.0 F.S.

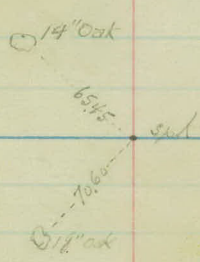
$\Delta - 59^{\circ} - 24'$
 $D - 5^{\circ} - 00' RT$
 $T - 653.83$
 $L - 1188.00$
 $R - 1146.28$

15" HO. ② - 54.0



15.7
 7.18
 3.14
 1.18
 4.29
 1.10
 5.44
 1.12
 6.59
 1.11
 8.14
 1.10
 8.35
 1.12
 5.44

$\Delta 2330'$
 $D 5^{\circ}$
 $T = 238.43 \checkmark$
 $L = 470.0 \checkmark$
 $R = 1146.28 \checkmark$



STATION POINT

Δ LT Δ RT

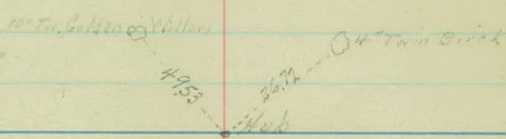
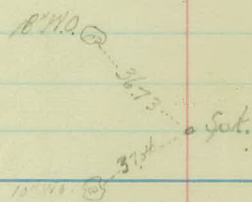
+32 ³³	P.T. ✓	34°10'
57		31°35'
+50		27°35'
56		23°35'
+50		19°35'
55+49 ¹³	P.I.	
55		15°35'
+50		11°35'
54		7°35'
+50		3°35'
53+05 ²⁵	T.C. ✓	

N 57° 28' E.

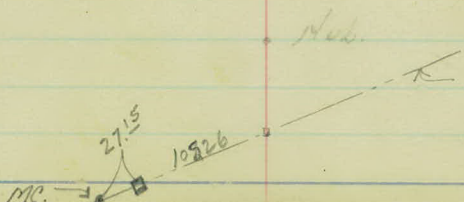
x

S 54° 12' E.

52+84⁰⁷ Hub int W. line Sec
31-30-22



$\Delta 6820'$
 $D 16^\circ L$
 $T = 243.85 \checkmark$
 $L = 427.09 \checkmark$
 $R = 359.265 \checkmark$





Topography

Proj. 33-W-32

5

4

3

2

1

0+00

Low Land.

Low Land

+26-P.P. 26'

+00-F. 31'

+20-Beg. Low Land Lt. & Rt.

+50-F. 38'

+50-E Rd. 6'

+00-E Rd. 20'

+68-Stu. 10'

+51-Tr. 9'

+21-Tr. 17'

+04-Tr. 18'

+50-E Rd. 39'

+19-Tr. 9'

+94-Tr. 20'

+64-Tr. 28'

+21-Tr. 40'

+17-Tr. 28'

+00-Stu. 9'



+44-Cor. Pig Pen 6'

+03-Cor. Pig Pen 17'

+44-Tr. 8'

+20-Stu. 20'

+20-Tr. 7'

+08-Tr. 24'



+85-Tr. 31'

+78-Tr. 35'

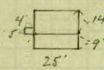
+72-Tr. 23'

+62-Tr. 28'

+35-Stump. 1'

+23-P.P. 38'

+19-18 M. Boas &



+41-Tr. 9'

+31-Tr. 16'

+03-Tr. 11'

+79 Cor. Ho. 60.5' 1-5-F

+97-Ice Ho. 16'

+92-Tr. 8'

+58-Tr. 15'

+23-T.P. 12'

+11.3 Edge Pavement

E Rice St

Donaso Blvd

12

11

10

9

8

7

6

14

+73-End. Low Land L+Rt. ---
+67-5+4. 2

+75-Rd. 40'

12"x21" Vit.

+31-No. End. X-Brain 20

+00-Rd. 23'

+50-Rd. 11'

+25-P.P. 32'

+00-Q Rd. 4'

Low Land.

Low Land

+82-P.P. 26'

+30-P.P. 26'

+76-P.P. 26'

+30-End F.

19

18

17

16

15

14

13

16

+44-Beg. Cult.
+44-End Orchard 15'

+80-Orchard 12'

+10-Beg. Orchard 34'
+00-Rd. 7'

+85-E. Dr.

+00-Rd. 5'

+50-Rd. 11'
+40-Beg. Cult.

+00-Rd. 17'

+76-Rd. 59.7'

Cult.

Orchard

Cult.

Pasture

Hay Field

Yard

+88-Stu. 22'

+57-Ev. gr. Tr. E
+30-Ev. gr. Tr. E
+15-Ev. gr. Tr. E

+84-Tr. E
+83-10"X16" C.N. X-Drain
+78-Tr. E
+69-Tr. E
+59-Tr.
+42-F. Cor. 18'

+98-Ev. gr. Tr. E

+63-Ev. gr. Tr. E
+08-Ev. gr. Tr. E
+06-F. E
+00-Rd. 7'

+85-E. Dr.

+43-Ho. 57'

+31-Hedge 4'

+43-Rd. E

+00-Rd. 36'

1-5 F.
30'

26

25

24

23

22

21

20

18

+00-End of Trail

+92-Tr. 35'

+29-Ev. 9r. 6'
+18-Ev. 9r. Tr. 5'
+12-Ev. 9r. Tr. 4'
+00-F. 2.5'

+96-Ev. 9r. Tr. 3'
+83-Ev. 9r. Tr. 2'

+44-Tr. 30'

Pasture

+25-F. Int.

Cult.

Cult.

Trail
Trail

+79-Ev. 9r. Tr. 16'
+77-F. Cor. 16'

Pasture

+41-Stu. 24'

33

32

31

30

29

28

27

27

+60-F. 58'

+34-Stu. 17'
+13-Tr. 3'
+00-Stu. 16'
+82-Stu. 22'
+68-Tr. 28'
+65-Tr. 7'
+51-Stu. 30'
+45-Tr. 14'
+39-Tr. 9'
+37-Stu. 16'
+27-Stu. 26'
+19-Stu. 34'
+08-Stu. 14'

+79-Tr. 10'
+75-Tr. 3'
+54-Tr. 28'
+49-Tr. 1'
+43-Tr. 3'
+40-Tr. 37'
+33-Tr. 36'
+06-Stump 31'
+95-Tr. 28'
+87-Tr. 31'
+69-Tr. 35'
+61-House 54'
+60-Tr. 25'

+37-House 61.5
+25-Tr. 38'
+14-Tr. 32'

+95-Stu. 23' & 19'
+89-Tr. 29'
+83-Tr. 1'

24'
125'
13.8'

Pasture

End Low Land

Pasture

Ditch 2

Low Land

Begin Low Land

+00-Ditch 50'

+50-Ditch 4

+18-F. 4
+11-F. 4

+46-Stu. 25'
+40-Tr. 24'
+39-Stu. 37'
+36-Stu. 28'
+27-Stu. 5'
+16-Tr. 4'
+10-Tr. 22'
+06-Stu. 2'
+05-Stu. 21'
+98-Stu. 18' & 34'
+90-Stu. 24'
+77-Stu. 39'
+61-Tr. 24'
+53-Stu. 10'
+30-Stu. 4
+22-Stu. 20'
+21-Stu. 3'
+14-Tr. 12'
+02-Tr. 4'

+84-Stu. 7'

+55-Stu. 2'

+00-F. 35'
+90-Ev. gr. Tr. 33'
+85-" " " 31'
+76-" " " 30'
+67-" " " 28'
+23-Ev. gr. Tr. 19'
+16-Ev. gr. Tr. 18'
+12-Ev. gr. Tr. 17'
+04-F. Int. 15'
+00-E. Trail 22'
+00-F. 12'

Cult.

40

39

38

37

36

35

34

22

11-29-32

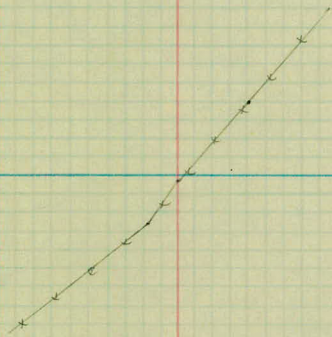
Reforested

Reforested

+74- F. Δ 18'
+50- F. 48'

+40- F. 42'

+97- F. Δ



Pasture

Pasture

47

46

45

44

43

42

41

21

Lake 43'

F. 40'

+00-Stu. 23'

+82-Stu. 32'

+78-Tr. 34'

+73-Tr. 31'

+62-End F. 26'

+50-Lake 54'

Lake

Small Trees & Brush

Wooded

+00-F. 37'

+40-End of Reforest

+00-F. 28'

+00-F. 24'

+50-F. 39'

+50-F. 12'

+00-F. 51'

+00-E Rd. 26'

Wooded

Vadnais

Bvd.

+00-F. 4'

+00-F. 36'

Reforested

Reforested

54

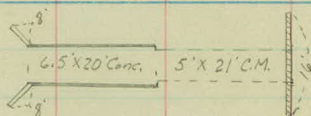
53

52

51

50

+ 93



Invert Elev. 880.6

49

48

55

56

57

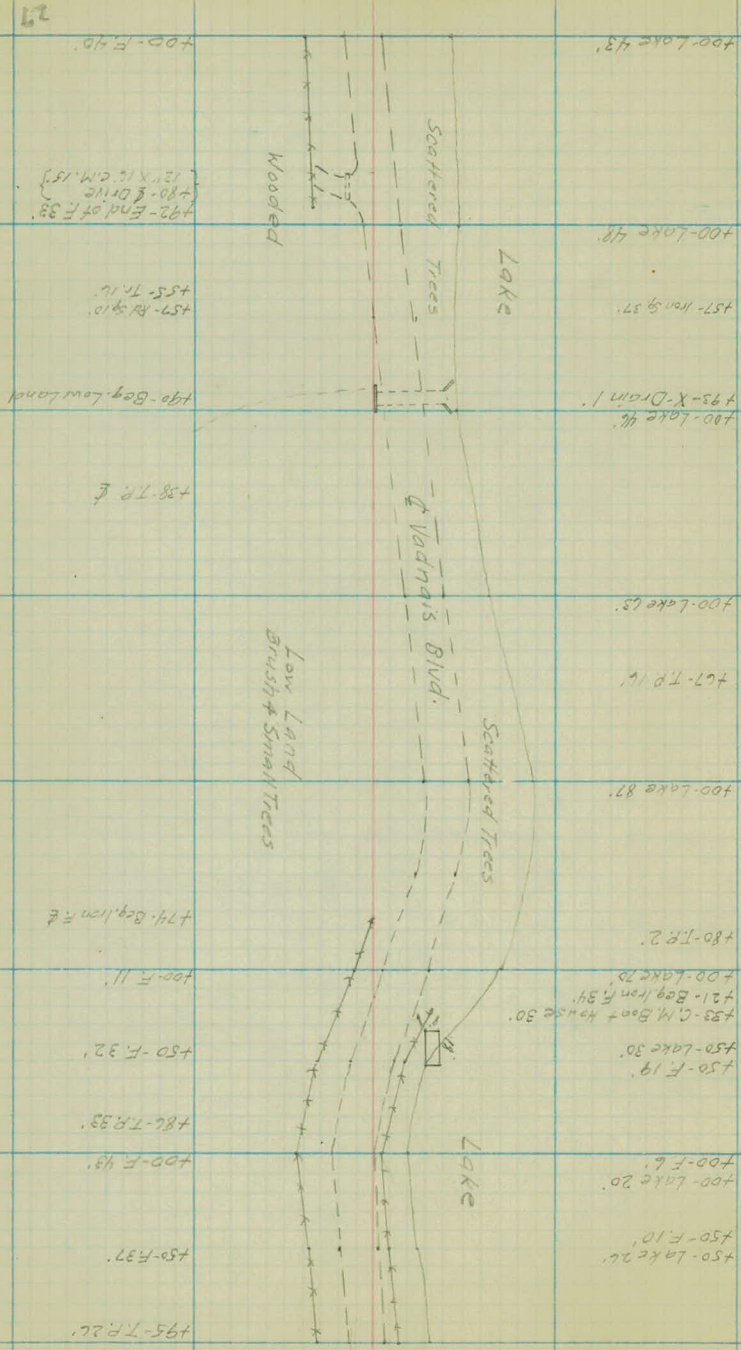
58

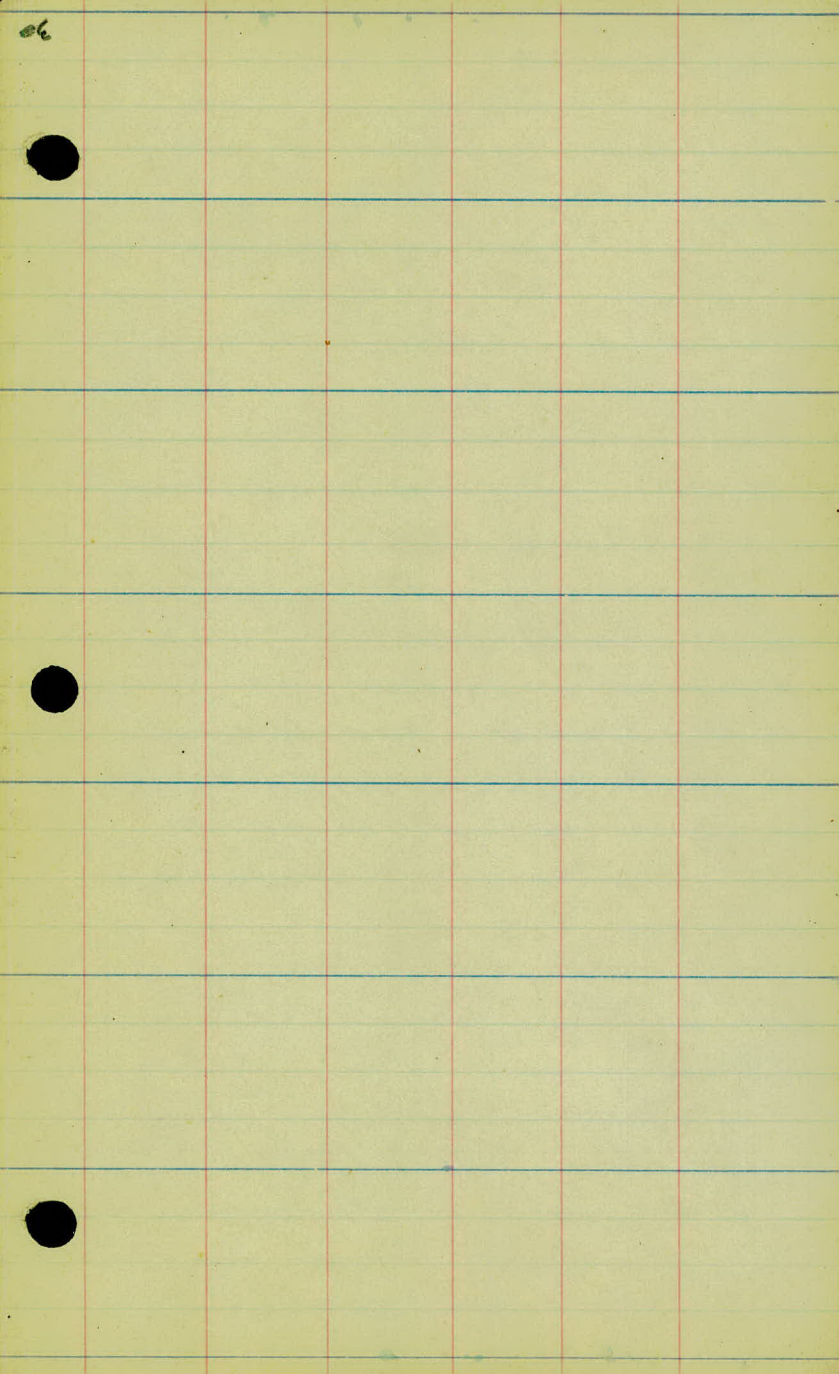
59

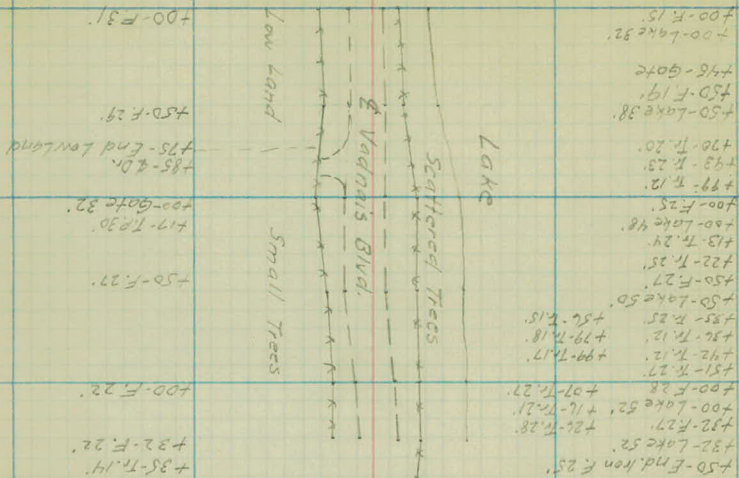
60

61

28







X-Sections
Proj. 33-W-32

STA 7 H.I. -

B.M. 0.05 925.18 925.13

FLY

0400

4 Rice St.

23.5

+19

23.2

+22

22.3

+50

20.8

1

18.6

+50

15.2

+73

13.4

T.P.

0.69

914.15

11.72

913.46

2

10.4

+50

03.3

T.P.

0.27

901.12

13.30

900.85

3

97.0

+50

90.7

T.P.

2.48

892.39

11.21

889.91

4

85.2

923.68 23.6 ✓ 23.7 ✓ 23.6 ✓ 23.5 ✓ 23.1 ✓ 22.7 ✓ 22.5 ✓ 22.0 ✓ 21.4 ✓ 19.5 ✓ 20.5 ✓ 22.3 ✓ 19.6 ✓ 7.54 920.16 (42)	Elev -		14.1 927.70	4.02 927.70	B.M. 23+00 +50 24+00 +50 25 +50 26 +50 27 +30 +50 28 +50 T.P.	0.17 920.33
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34 W 32

FLY

-

H.I.

+

STH

23

25.2

24

24.7

+50

24.2

25

22.4

B.M.

6.96

923.68

923.68

+50

18.9

T.P.

3.64

924.78

9.50

921.14

+89

17.7

26

17.9

+40

21.0

+70

21.9

27

21.3

+30

19.6

+70

21.7

28

22.3

40

$$\begin{array}{r} 2.3 \\ 2.9 \\ \hline 5.2 \end{array} \quad \begin{array}{r} 30 \\ 18 \\ \hline 48 \end{array} \quad \begin{array}{r} 5.0 \\ 4.5 \\ \hline 9.5 \end{array}$$

$$\begin{array}{r} 6.5 \\ 7.7 \\ \hline 14.2 \end{array} \quad \begin{array}{r} 5.0 \\ 2.7 \\ \hline 7.7 \end{array} \quad \begin{array}{r} 5.0 \\ 2.7 \\ \hline 7.7 \end{array}$$

$$\begin{array}{r} 4.8 \\ 5.9 \\ \hline 10.7 \end{array} \quad \begin{array}{r} 3.0 \\ 6.5 \\ \hline 9.5 \end{array} \quad \begin{array}{r} 5.0 \\ 4.9 \\ \hline 9.9 \end{array}$$

$$\begin{array}{r} 7.6 \\ 8.5 \\ \hline 16.1 \end{array} \quad \begin{array}{r} 5.0 \\ 2.8 \\ \hline 7.8 \end{array} \quad \begin{array}{r} 5.0 \\ 2.8 \\ \hline 7.8 \end{array}$$

$$\begin{array}{r} 8.3 \\ 8.9 \\ \hline 17.2 \end{array} \quad \begin{array}{r} 5.0 \\ 3.0 \\ \hline 8.0 \end{array} \quad \begin{array}{r} 5.0 \\ 3.0 \\ \hline 8.0 \end{array}$$

$$\begin{array}{r} 5.6 \\ 5.3 \\ \hline 10.9 \end{array} \quad \begin{array}{r} 5.4 \\ 1.8 \\ \hline 7.2 \end{array} \quad \begin{array}{r} 5.4 \\ 1.8 \\ \hline 7.2 \end{array}$$

$$\begin{array}{r} 14.5 \\ 13.8 \\ \hline 28.3 \end{array} \quad \begin{array}{r} 5.0 \\ 3.5 \\ \hline 8.5 \end{array} \quad \begin{array}{r} 5.0 \\ 3.5 \\ \hline 8.5 \end{array}$$

$$\begin{array}{r} 11.0 \\ 10.1 \\ \hline 21.1 \end{array} \quad \begin{array}{r} 5.0 \\ 3.2 \\ \hline 8.2 \end{array} \quad \begin{array}{r} 5.0 \\ 3.2 \\ \hline 8.2 \end{array}$$

$$\begin{array}{r} 14.7 \\ 13.5 \\ \hline 28.2 \end{array} \quad \begin{array}{r} 5.0 \\ 3.0 \\ \hline 8.0 \end{array} \quad \begin{array}{r} 5.0 \\ 3.0 \\ \hline 8.0 \end{array}$$

$$\begin{array}{r} 12.5 \\ 10.8 \\ \hline 23.3 \end{array} \quad \begin{array}{r} 5.0 \\ 2.2 \\ \hline 7.2 \end{array} \quad \begin{array}{r} 5.0 \\ 2.2 \\ \hline 7.2 \end{array}$$

$$\begin{array}{r} 14.3 \\ 12.1 \\ \hline 26.4 \end{array} \quad \begin{array}{r} 5.0 \\ 3.2 \\ \hline 8.2 \end{array} \quad \begin{array}{r} 5.0 \\ 3.2 \\ \hline 8.2 \end{array}$$

Spk in 10" Oak 45' R# 54.21+00

$$\begin{array}{r} 8.7 \\ 7.1 \\ \hline 15.8 \end{array} \quad \begin{array}{r} 5.0 \\ 3.0 \\ \hline 8.0 \end{array} \quad \begin{array}{r} 5.0 \\ 3.0 \\ \hline 8.0 \end{array}$$

$$\begin{array}{r} 5.1 \\ 5.1 \\ \hline 10.2 \end{array} \quad \begin{array}{r} 5.0 \\ 2.7 \\ \hline 7.7 \end{array} \quad \begin{array}{r} 5.0 \\ 2.7 \\ \hline 7.7 \end{array}$$

ELEV

-

910.56



16

06.1

+50

02.2

T.P

5.94

904.53

11.97

898.59



17

97.6

+50

95.5

18

95.3

+50

99.1

T.P

11.89

916.18

0.24

904.29



19

03.9

+50

08.9

T.P

10.26

925.65

0.79

915.39



20

14.3

+50

17.9

T.P

6.64

930.64

1.65

924.00



21

22.7

B.M.

3.71

926.93



+50

25.4

22

25.7

2.0 2.7 2.2 3.8 5.0
 4.1 4.6 4.7 6.7 8.0
 6.7 1.5 6.7 1.7 1.7

4.8 1.9 1.6 1.2 1.8 3.8 5.0
 4.3 1.8 4.3 1.8 1.8 3.8 5.0

1.7 0.9 1.3 2.8 5.0
 5.7 4.3 1.5 5 1.3

Spk. in 15" Willow 35' L. 12+55

0.7 0.9 1.4 1.3 1.4 0.8 5.0
 4.5 1.2 2.4 3.8 5.0

Spk. in P.P. 100' R. 13+85

12.3 12.2 11.7 12.0 21 8.0
 12.4 12.8 12.0 21 8.0

11.7 12.3 11.7 11.4 4 11.5 21 5.0
 12.4 11.6 8.5 8.2 11.4 4 11.5 21 5.0

10.3 10.7 3.4 9.3 6 16 5.0
 10.6 6.2 5.8 8 23 8 3.0

10.8 8.2 5.1 4.3 5.2 2 4.9 3 2.0 5.0
 10.8 8.2 5.1 4.3 5.2 2 4.9 3 2.0 5.0

6.6 2.6 2.6 4.1 3.7 4 4.3 2 11 2.7 5.0
 6.6 2.6 2.6 4.1 3.7 4 4.3 2 11 2.7 5.0

2.9 2.9 2.6 2.3 3.0 2 4 1.5 3.3 5.0
 2.9 2.9 2.6 2.3 3.0 2 4 1.5 3.3 5.0

9.5 9.4 8.9 8.8 9.6 8.3 2.9 5.3
 9.5 9.4 8.9 8.8 9.6 8.3 2.9 5.3

2.1 2.0 2.3 5.0 5.2 5.4 2.0 1.7 1.3
 3.5 1.6 1.1 5.2 6 9 14 2.7 5.0

0.9 1.5 3.2 1.8 1.5 3.7 4.1 2.3 2.4 2.0
 0.9 1.5 3.2 1.8 1.5 3.7 4.1 2.3 2.4 2.0

STA + H.I. - Elev

886.38

12+50

79.7

+73

82.1

+79

85.1

B.M.

4.49

881.89

881.87

13

85.2

B.M.

12.65

897.79

1.24

885.14

+45

& Water Works Rd.

85.8

14

86.3

+20

88.5

+31

92.9

+38

93.5

+50

94.8

T.P.

13.35

908.93

2.21

895.58

15

99.0

T.P.

4.84

910.56

3.21

905.72

+50

95.4

+70

96.9

%

6.6 6.6 5.0
12 12 6.1
6.4 4.1 4.0 3.7 5.0

6.5 6.6 7.2 6.8 3
5.3 4.4 5.1 2.2 2.6 2.9 3.0 5.0
6.5 6.5 6.5 6.5 6.5 6.5 6.5 6.5

5.0 6.6 6.9 8 3 5.3 8
4.8 5.4 6.5 7.4 7.4 7.4 7.5 6.6
5.0 6.6 6.6 6.6 6.6 6.6 6.6 6.6

5.0 6.6 6.7 13 12 6 3 5.3 11
6.6 6.6 6.6 6.6 6.6 6.6 6.6 6.6

5.0 6.6 6.5 16 15 9 6 5.6 7
7.0 7.4 7.0 5.9 5.8 7.1 7.4 6.9 7.0

5.0 6.6 6.7 16 15 10 7 5.7 8
6.6 7.4 7.0 5.8 5.8 6.9 7.3 6.6 6.9

5.0 6.6 6.5 27 17 15 11 9 5.6 7
6.5 6.6 6.6 6.6 6.6 6.6 6.6 6.6 6.6

Spr. in 12" Birch 4.2 7.1 8.4 4.3

5.0 6.6 12.1 12.1 12.8 12.9 12.4 11.4 11.1 7
12.1 12.1 12.1 12.1 12.1 12.1 12.1 12.1 12.1

5.0 6.6 11.7 11.5 12.3 12.4 11.8 10.7 10.3 7
11.7 11.7 11.7 11.7 11.7 11.7 11.7 11.7 11.7

5.0 6.6 10.7 10.9 11.6 11.6 10.8 8.9 7 8.9 7
10.7 10.7 10.7 10.7 10.7 10.7 10.7 10.7 10.7

5.0 6.6 10.5 10.5 10.9 7.1 6.5 5 12 14 16 8.0
10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5

5.0 6.6 10.6 10.6 8.7 4.4 4.5 12 22 26 5.0
10.6 10.6 10.6 10.6 10.6 10.6 10.6 10.6 10.6

Spr. in 24" Oak 7.5 7.4 5.4 3.5 5.5

5.0 6.6 9.5 9.5 9.2 8.4 10 2.0 1.9 8.6 9.5
9.5 9.5 9.5 9.5 9.5 9.5 9.5 9.5 9.5

STA. + H.I. - ELEV.

872.94

4+12

B.M.

3.97

888.42

840.

879.

+50

859.

5

83.5

6

82.1

7

81.3

8

N.G.

B.M.

4.22

886.38

10.23

882.16

80.8

9

80.7

10

80.8

+50

81.1

11

81.1

+25

99.6

+50

79.8

12

Spt. in P.R. NW. Cor. Rice & Owasso Blvd No.

1.4
50
1.7
50

2.1 1.7 50
2.3 2.4 2.0 2.5 50

2.4 2.3 3.0 3.2 2.5 2.8
50 30 1.6 2.9 2.0 3.0 50

3.8 4.2 4.1 4.4 4.7 4.3 4.2
50 40 2.1 4.4 2.5 3.5 4.0 50

7.0 7.0 6.8 6.3 6.4 6.2
50 33 1.4 6.6 1.2 2.8 50

11.2 10.6 9.4 9.3 8.8
50 13 10.0 10 3.3 50

13.6 12.4 12.0 11.4 10.2
50 13 6 11.8 19 50

5.0 4.6 4.1 3.3 2.2 1.9
50 30 12 3.8 1.6 3.4 50

18.0 12.6 11.5 9.8 9.2 8.5 9.8
50 37 12 10.9 1.8 3.2 4.7 50

5.8 4.6 4.1 3.7 3.1 2.0 1.2
50 15 4.1 1.8 3.2 4.3 50

11.6 10.7 9.8 6.4 5.7 5.7 7.3
50 25 10.4 2.6 3.2 4.0 4.6 50

8.5 8.0 7.2 7.2 1.1 1.0 1.0 2.1 1.2
50 16 7.2 2.5 1.4 2.0 2.6 3.7 50

LEFT & RIGHT

Mont Ctr. Sec. 34-30-22

$\frac{2.5}{50}$	$\frac{2.4}{27}$	$\frac{6.2}{21}$	$\frac{6.2}{17}$	$\frac{4.2}{13}$	41	$\frac{4.2}{13}$	$\frac{6.0}{17}$	$\frac{6.1}{22}$	$\frac{2.6}{27}$	$\frac{2.6}{50}$
------------------	------------------	------------------	------------------	------------------	----	------------------	------------------	------------------	------------------	------------------

$\frac{3.0}{50}$	$\frac{3.0}{26}$	$\frac{6.0}{22}$	$\frac{6.0}{16}$	$\frac{4.3}{13}$	40	$\frac{4.2}{13}$	$\frac{6.0}{16}$	$\frac{6.2}{22}$	$\frac{3.0}{27}$	$\frac{2.7}{50}$
------------------	------------------	------------------	------------------	------------------	----	------------------	------------------	------------------	------------------	------------------

$\frac{3.4}{50}$	$\frac{3.3}{26}$	$\frac{5.8}{21}$	$\frac{6.1}{17}$	$\frac{4.4}{13}$	41	$\frac{4.4}{13}$	$\frac{6.0}{16}$	$\frac{6.0}{22}$	$\frac{3.0}{27}$	$\frac{3.0}{50}$
------------------	------------------	------------------	------------------	------------------	----	------------------	------------------	------------------	------------------	------------------

$\frac{4.4}{50}$	$\frac{4.5}{26}$	$\frac{6.7}{22}$	$\frac{6.7}{17}$	$\frac{4.7}{13}$	42	$\frac{4.7}{13}$	$\frac{6.5}{17}$	$\frac{6.5}{21}$	$\frac{3.6}{26}$	$\frac{3.4}{50}$
------------------	------------------	------------------	------------------	------------------	----	------------------	------------------	------------------	------------------	------------------

$\frac{6.2}{50}$	$\frac{6.6}{22}$	$\frac{7.0}{21}$	$\frac{6.8}{16}$	$\frac{5.1}{13}$	46	$\frac{5.0}{13}$	$\frac{7.0}{17}$	$\frac{7.0}{22}$	$\frac{4.8}{27}$	$\frac{4.2}{50}$
------------------	------------------	------------------	------------------	------------------	----	------------------	------------------	------------------	------------------	------------------

$\frac{12.6}{50}$	$\frac{10.1}{21}$	$\frac{5.3}{13}$	50	$\frac{5.3}{14}$	$\frac{7.6}{19}$	$\frac{6.2}{50}$
-------------------	-------------------	------------------	----	------------------	------------------	------------------

$\frac{16.5}{50}$	$\frac{12.6}{23}$	$\frac{5.7}{11}$	5.2	$\frac{5.8}{16}$	$\frac{7.7}{21}$	$\frac{7.7}{26}$	$\frac{7.0}{28}$	$\frac{5.0}{50}$
-------------------	-------------------	------------------	-----	------------------	------------------	------------------	------------------	------------------

$\frac{9.1}{50}$	$\frac{6.8}{17}$	$\frac{7.8}{15}$	$\frac{7.7}{10}$	$\frac{5.8}{6}$	5.1	$\frac{5.7}{22}$	$\frac{7.2}{25}$	$\frac{7.2}{30}$	$\frac{5.8}{33}$	$\frac{5.3}{50}$
------------------	------------------	------------------	------------------	-----------------	-----	------------------	------------------	------------------	------------------	------------------

$\frac{6.6}{50}$	$\frac{6.5}{10}$	$\frac{8.0}{8}$	$\frac{7.8}{2}$	6.3	$\frac{6.3}{28}$	$\frac{8.0}{33}$	$\frac{8.2}{37}$	$\frac{7.5}{38}$	$\frac{7.6}{50}$
------------------	------------------	-----------------	-----------------	-----	------------------	------------------	------------------	------------------	------------------

$\frac{9.0}{50}$	$\frac{9.5}{30}$	$\frac{8.8}{9}$	8.2	$\frac{8.1}{3}$	$\frac{6.6}{7}$	$\frac{6.2}{33}$	$\frac{6.8}{36}$	$\frac{6.2}{42}$	$\frac{6.2}{50}$
------------------	------------------	-----------------	-----	-----------------	-----------------	------------------	------------------	------------------	------------------

$\frac{9.3}{50}$	$\frac{9.2}{34}$	$\frac{8.1}{10}$	7.2	$\frac{6.5}{5}$	$\frac{5.8}{36}$	$\frac{5.5}{38}$	$\frac{5.3}{50}$
------------------	------------------	------------------	-----	-----------------	------------------	------------------	------------------

$\frac{10.8}{50}$	$\frac{6.6}{21}$	5.4	$\frac{3.8}{30}$	$\frac{3.2}{50}$
-------------------	------------------	-----	------------------	------------------

—	$\frac{14.0}{27}$	8.1	$\frac{6.4}{25}$	$\frac{5.5}{50}$
---	-------------------	-----	------------------	------------------

+ H.I. - Elev

920.33

28+50

19.6 ✓

29

13.1 ✓

+50

03.5 ✓

T.P. 0.85 908.02 13.16 907.17

29

13.1 ✓

+50

03.5 ✓

+90⁵¹ F.T.

885.1 ✓

T.P. 0.56 895.60 12.98 895.04

29+50

03.5 ✓

+90⁵¹

85.1

T.P. 1.54 884.14 13.00 882.60

B.M.

1.33 882.81 882.80

Left & Right.

$$\frac{13.0}{50}$$

$$\textcircled{0.7}$$

$$\frac{13.0}{23} \quad 72 \quad \frac{3.0}{24} \quad \frac{0.4}{41} \quad \frac{0.2}{50}$$

$$\textcircled{16.8} \quad \frac{13.2}{19} \quad \frac{7.4}{50}$$

$$\frac{8.7}{50} \quad \textcircled{+5.1}$$

$$\frac{10.5}{25} \quad 45$$

$$12.9 \quad \frac{6.7}{25} \quad \frac{2.7}{50}$$

Top Spt 29 + 90.57

$$\frac{4.0}{50} \quad \textcircled{+7.9}$$

$$\frac{14.8}{50} \quad \frac{7.5}{25} \quad \textcircled{10.5}$$

Spt in 18" Q. 140' Rt Sta 32 + 00

$$\begin{array}{r} 5.7 \\ 50 \end{array} \quad \begin{array}{r} 5.5 \\ 26 \end{array} \quad \begin{array}{r} 5.4 \\ 12 \end{array} \quad \begin{array}{r} 5.7 \\ 5.4 \end{array} \quad \begin{array}{r} 5.5 \\ 17 \end{array} \quad \begin{array}{r} 5.5 \\ 50 \end{array}$$

$$\begin{array}{r} 6.4 \\ 50 \end{array} \quad \begin{array}{r} 6.8 \\ 33 \end{array} \quad \begin{array}{r} 5.7 \\ 11 \end{array} \quad \begin{array}{r} 6.2 \\ 5.9 \end{array} \quad \begin{array}{r} 6.1 \\ 20 \end{array} \quad \begin{array}{r} 6.1 \\ 50 \end{array}$$

$$\begin{array}{r} 7.3 \\ 50 \end{array} \quad \begin{array}{r} 6.9 \\ 20 \end{array} \quad \begin{array}{r} 6.5 \\ 6.4 \end{array} \quad \begin{array}{r} 6.5 \\ 21 \end{array} \quad \begin{array}{r} 6.4 \\ 50 \end{array}$$

$$\begin{array}{r} 11.1 \\ 50 \end{array} \quad \begin{array}{r} 10.3 \\ 32 \end{array} \quad \begin{array}{r} 8.8 \\ 12 \end{array} \quad \begin{array}{r} 8.2 \\ 8.2 \end{array} \quad \begin{array}{r} 7.7 \\ 12 \end{array} \quad \begin{array}{r} 7.1 \\ 30 \end{array} \quad \begin{array}{r} 7.1 \\ 50 \end{array}$$

Mont. Cent. Sec. 31

$$\begin{array}{r} 16.2 \\ 50 \end{array} \quad \begin{array}{r} 14.0 \\ 30 \end{array} \quad \begin{array}{r} 12.8 \\ 15 \end{array} \quad \begin{array}{r} 12.1 \\ 12 \end{array} \quad \begin{array}{r} 12.4 \\ 4 \end{array} \quad \begin{array}{r} 10.8 \\ 11.7 \end{array} \quad \begin{array}{r} 10.7 \\ 5 \end{array} \quad \begin{array}{r} 9.0 \\ 19 \end{array} \quad \begin{array}{r} 9.0 \\ 50 \end{array}$$

$$\begin{array}{r} 14.0 \\ 50 \end{array} \quad \begin{array}{r} 11.3 \\ 35 \end{array} \quad \begin{array}{r} 9.1 \\ 17 \end{array} \quad \begin{array}{r} 8.0 \\ 13 \end{array} \quad \begin{array}{r} 7.1 \\ 7.1 \end{array} \quad \begin{array}{r} 5.9 \\ 4 \end{array} \quad \begin{array}{r} 5.3 \\ 22 \end{array} \quad \begin{array}{r} 2.9 \\ 50 \end{array}$$

$$\begin{array}{r} 13.4 \\ 50 \end{array} \quad \begin{array}{r} 10.4 \\ 32 \end{array} \quad \begin{array}{r} 8.8 \\ 18 \end{array} \quad \begin{array}{r} 7.6 \\ 13 \end{array} \quad \begin{array}{r} 6.9 \\ 6.9 \end{array} \quad \begin{array}{r} 5.9 \\ 3 \end{array} \quad \begin{array}{r} 4.7 \\ 25 \end{array} \quad \begin{array}{r} 2.6 \\ 50 \end{array}$$

$$\begin{array}{r} 6.1 \\ 50 \end{array} \quad \begin{array}{r} 5.1 \\ 31 \end{array} \quad \begin{array}{r} 4.1 \\ 16 \end{array} \quad \begin{array}{r} 3.5 \\ 12 \end{array} \quad \begin{array}{r} 3.8 \\ 3.8 \end{array} \quad \begin{array}{r} 3.1 \\ 7 \end{array} \quad \begin{array}{r} 2.9 \\ 20 \end{array} \quad \begin{array}{r} 2.1 \\ 50 \end{array}$$

$$\begin{array}{r} 4.0 \\ 50 \end{array} \quad \begin{array}{r} 3.2 \\ 22 \end{array} \quad \begin{array}{r} 3.0 \\ 12 \end{array} \quad \begin{array}{r} 2.4 \\ 9 \end{array} \quad \begin{array}{r} 2.9 \\ 5 \end{array} \quad \begin{array}{r} 2.9 \\ 2.9 \end{array} \quad \begin{array}{r} 2.5 \\ 10 \end{array} \quad \begin{array}{r} 2.7 \\ 28 \end{array} \quad \begin{array}{r} 2.8 \\ 50 \end{array}$$

$$\begin{array}{r} 3.9 \\ 50 \end{array} \quad \begin{array}{r} 3.5 \\ 33 \end{array} \quad \begin{array}{r} 3.6 \\ 10 \end{array} \quad \begin{array}{r} 3.2 \\ 4 \end{array} \quad \begin{array}{r} 3.5 \\ 3.5 \end{array} \quad \begin{array}{r} 3.5 \\ 13 \end{array} \quad \begin{array}{r} 3.8 \\ 28 \end{array} \quad \begin{array}{r} 4.8 \\ 50 \end{array}$$

$$\begin{array}{r} 6.1 \\ 50 \end{array} \quad \begin{array}{r} 6.6 \\ 27 \end{array} \quad \begin{array}{r} 6.1 \\ 12 \end{array} \quad \begin{array}{r} 5.2 \\ 5.2 \end{array} \quad \begin{array}{r} 4.7 \\ 2 \end{array} \quad \begin{array}{r} 4.6 \\ 12 \end{array} \quad \begin{array}{r} 3.4 \\ 35 \end{array} \quad \begin{array}{r} 3.4 \\ 50 \end{array}$$

$$\begin{array}{r} 5.9 \\ 50 \end{array} \quad \begin{array}{r} 4.7 \\ 34 \end{array} \quad \begin{array}{r} 4.1 \\ 20 \end{array} \quad \begin{array}{r} 3.1 \\ 3.1 \end{array} \quad \begin{array}{r} 2.3 \\ 12 \end{array} \quad \begin{array}{r} 2.4 \\ 26 \end{array} \quad \begin{array}{r} 1.3 \\ 50 \end{array}$$

$$\begin{array}{r} 8.3 \\ 50 \end{array} \quad \begin{array}{r} 6.4 \\ 38 \end{array} \quad \begin{array}{r} 4.5 \\ 27 \end{array} \quad \begin{array}{r} 3.3 \\ 14 \end{array} \quad \begin{array}{r} 2.5 \\ 2.5 \end{array} \quad \begin{array}{r} 1.6 \\ 11 \end{array} \quad \begin{array}{r} 0.8 \\ 27 \end{array} \quad \begin{array}{r} 0.4 \\ 38 \end{array} \quad \begin{array}{r} 0.5 \\ 50 \end{array}$$

STA 7 H.I. - ELEV

924.78

923.95

2.86

921.92

T.P.

2.03

28+25

21.1.

+50

19.7.

+75

17.1.

29

13.1.

+50

T.P.

0.49

910.78

13.66

910.29

28+75

29

+50

03.8.

+80

97.6.

30

T.P.

0.21

897.79

13.20

897.58

29+50

+80

$$\begin{array}{r} 11.6 \\ 50 \end{array} \quad \begin{array}{r} 9.2 \\ 40 \end{array} \quad \begin{array}{r} 6.5 \\ 30 \end{array} \quad \begin{array}{r} 4.5 \\ 16 \end{array} \quad 2.9 \quad \begin{array}{r} 2.0 \\ 15 \end{array} \quad \begin{array}{r} 1.2 \\ 30 \end{array} \quad \begin{array}{r} 0.0 \\ 50 \end{array}$$

$$\begin{array}{r} 17.5 \\ 50 \end{array} \quad \begin{array}{r} 14.5 \\ 40 \end{array} \quad \begin{array}{r} 11.2 \\ 30 \end{array} \quad \begin{array}{r} 6.7 \\ 11 \end{array} \quad 4.3 \quad \begin{array}{r} 3.4 \\ 16 \end{array} \quad \begin{array}{r} 2.3 \\ 34 \end{array} \quad \begin{array}{r} 1.2 \\ 50 \end{array}$$

$$\begin{array}{r} 12.0 \\ 19 \end{array} \quad \begin{array}{r} 8.1 \\ 6 \end{array} \quad 6.9 \quad \begin{array}{r} 5.5 \\ 8 \end{array} \quad \begin{array}{r} 4.2 \\ 22 \end{array} \quad \begin{array}{r} 2.6 \\ 50 \end{array}$$

$$\begin{array}{r} 13.8 \\ 13 \end{array} \quad 10.9 \quad \begin{array}{r} 8.0 \\ 14 \end{array} \quad \begin{array}{r} 6.4 \\ 24 \end{array} \quad \begin{array}{r} 4.5 \\ 37 \end{array} \quad \begin{array}{r} 3.7 \\ 50 \end{array}$$

$$\textcircled{20.2} \quad \begin{array}{r} 13.7 \\ 30 \end{array} \quad \begin{array}{r} 10.8 \\ 50 \end{array}$$

$$\begin{array}{r} 9.0 \\ 50 \end{array} \quad \begin{array}{r} 2.7 \\ 30 \end{array} \quad \times 6.3$$

$$\begin{array}{r} 12.3 \\ 50 \end{array} \quad \begin{array}{r} 6.5 \\ 30 \end{array} \quad \times 2.3$$

$$\begin{array}{r} 10.6 \\ 15 \end{array} \quad 7.0 \quad \begin{array}{r} 4.1 \\ 15 \end{array}$$

$$13.2 \quad \begin{array}{r} 9.1 \\ 16 \end{array} \quad \begin{array}{r} 5.1 \\ 35 \end{array} \quad \begin{array}{r} 2.9 \\ 50 \end{array}$$

$$18.4 \quad \begin{array}{r} 14.0 \\ 15 \end{array} \quad \begin{array}{r} 10.3 \\ 30 \end{array} \quad \begin{array}{r} 6.0 \\ 50 \end{array}$$

$$\begin{array}{r} 7.3 \\ 50 \end{array} \quad \begin{array}{r} 4.0 \\ 40 \end{array} \quad \begin{array}{r} 1.5 \\ 30 \end{array} \quad \times 6.0$$

$$\begin{array}{r} 12.0 \\ 40 \end{array} \quad \begin{array}{r} 8.7 \\ 30 \end{array} \quad \begin{array}{r} 4.9 \\ 15 \end{array} \quad 0.2$$

STA

7

H.I. ✓

FLEV

897.79

30

92.0.

+32

T.P. 0.87 885.65 ✓ 13.01 884.78 ✓

29+80

B.M. 2.80 882.85 ✓ 882.80

30

92.0

+32

80.6.

+50

79.5.

31

77.5

+50

77.0.

32

77.3.

+45

77.2.

+50 £ Ditch

33

77.6.

T.P. 11.06 889.12 ✓ 7.59 878.06 ✓

+40

78.7.

+65

81.0.

$$\begin{array}{r} 10.2 \\ 74 \end{array} 5.8$$

172

$$\begin{array}{r} 10.4 \quad 5.3 \quad 1.7 \\ 20 \quad 37 \quad 50 \end{array}$$

$$\begin{array}{r} 3.9 \\ 50 \end{array}$$

$$+11.9$$

Spk. in 18" Oak 140 Rt. 32+00

$$\begin{array}{r} 5.9 \quad 5.3 \quad 3.4 \\ 50 \quad 37 \quad 30 \end{array}$$

$$+6.3$$

$$\begin{array}{r} 7.9 \quad 6.9 \quad 6.1 \quad 5.4 \quad 2.1 \\ 50 \quad 30 \quad 25 \quad 15 \quad 10 \end{array}$$

$$\begin{array}{r} 8.2 \quad 7.5 \quad 7.1 \quad 6.5 \quad 5.2 \quad 3.5 \quad 1.6 \quad 0.0 \quad +3.5 \\ 50 \quad 30 \quad 18 \quad 10 \quad 6.2 \quad 19 \quad 26 \quad 37 \quad 40 \quad 50 \end{array}$$

$$\begin{array}{r} 9.5 \quad 8.8 \quad 7.8 \quad 7.1 \\ 50 \quad 22 \quad 22 \quad 50 \end{array}$$

$$\begin{array}{r} 9.5 \quad 9.1 \quad 8.2 \quad 7.8 \\ 50 \quad 25 \quad 25 \quad 50 \end{array}$$

$$\begin{array}{r} 9.7 \quad 10.0 \quad 9.1 \quad 8.9 \quad 8.7 \quad 8.0 \quad 7.5 \\ 50 \quad 43 \quad 37 \quad 26 \quad 10 \quad 24 \quad 50 \end{array}$$

$$\begin{array}{r} 9.6 \quad 8.5 \quad 7.6 \quad 8.3 \quad 7.2 \\ 50 \quad 14 \quad 13 \quad 25 \quad 50 \end{array}$$

Editch

$$\begin{array}{r} 9.1 \quad 9.0 \quad 7.5 \quad 5.8 \quad 5.6 \quad 8.5 \quad 4.8 \quad 4.8 \\ 50 \quad 25 \quad 13 \quad 26 \quad 41 \quad 50 \quad 63 \quad 65 \end{array}$$

$$\begin{array}{r} 12.3 \quad 12.0 \quad 11.6 \quad 9.9 \quad 8.4 \quad 8.6 \quad 8.4 \\ 50 \quad 32 \quad 17 \quad 10.4 \quad 7 \quad 16 \quad 32 \quad 50 \end{array}$$

$$\begin{array}{r} 11.2 \quad 10.7 \quad 9.9 \quad 9.2 \quad 8.2 \quad 8.7 \quad 8.0 \quad 7.9 \\ 50 \quad 27 \quad 23 \quad 9 \quad 3 \quad 17 \quad 35 \quad 50 \end{array}$$

STA

7

H.I. ✓ -

ELEV

889.12

33+82

81.1.

34

83.8.

+25

87.5.

T.P.

11.89

899.62 ✓

1.39

887.73 ✓

34+25

+55

91.3.

+80

93.2.

35

94.8.

+20

94.8.

+60

97.2.

36

99.0.

T.P.

11.64

911.08 ✓

0.18

899.44 ✓

+50

02.7.

37

08.8.

T.P.

4.56

915.12 ✓

0.52

910.56 ✓

+50

12.3.

$$\begin{array}{r} 9.9 \\ 50 \end{array} \quad \begin{array}{r} 9.1 \\ 30 \end{array} \quad \begin{array}{r} 7.8 \\ 20 \end{array} \quad \begin{array}{r} 7.3 \\ 10 \end{array} \quad 8.0 \quad \begin{array}{r} 7.0 \\ 13 \end{array} \quad \begin{array}{r} 6.3 \\ 24 \end{array} \quad \begin{array}{r} 6.0 \\ 42 \end{array} \quad \begin{array}{r} 5.8 \\ 50 \end{array}$$

$$\begin{array}{r} 9.1 \\ 50 \end{array} \quad \begin{array}{r} 7.2 \\ 38 \end{array} \quad \begin{array}{r} 6.5 \\ 28 \end{array} \quad \begin{array}{r} 6.1 \\ 9 \end{array} \quad 5.3 \quad \begin{array}{r} 3.9 \\ 12 \end{array} \quad \begin{array}{r} 3.1 \\ 24 \end{array} \quad \begin{array}{r} 3.1 \\ 50 \end{array}$$

$$\begin{array}{r} 5.8 \\ 50 \end{array} \quad \begin{array}{r} 5.5 \\ 40 \end{array} \quad \begin{array}{r} 4.0 \\ 18 \end{array} \quad 1.6$$

12.1

$$\begin{array}{r} 10.2 \\ 17 \end{array} \quad \begin{array}{r} 9.0 \\ 32 \end{array} \quad \begin{array}{r} 8.3 \\ 50 \end{array}$$

$$\begin{array}{r} 13.0 \\ 50 \end{array} \quad \begin{array}{r} 11.7 \\ 33 \end{array} \quad \begin{array}{r} 9.9 \\ 14 \end{array} \quad 8.3 \quad \begin{array}{r} 6.5 \\ 18 \end{array} \quad \begin{array}{r} 4.9 \\ 33 \end{array} \quad \begin{array}{r} 4.0 \\ 50 \end{array}$$

$$\begin{array}{r} 10.2 \\ 50 \end{array} \quad \begin{array}{r} 8.4 \\ 35 \end{array} \quad \begin{array}{r} 7.6 \\ 20 \end{array} \quad 6.4 \quad \begin{array}{r} 4.4 \\ 19 \end{array} \quad \begin{array}{r} 2.5 \\ 38 \end{array} \quad \begin{array}{r} 1.8 \\ 50 \end{array}$$

$$\begin{array}{r} 8.8 \\ 50 \end{array} \quad \begin{array}{r} 7.9 \\ 33 \end{array} \quad \begin{array}{r} 6.0 \\ 16 \end{array} \quad 4.8 \quad \begin{array}{r} 3.7 \\ 16 \end{array} \quad \begin{array}{r} 2.5 \\ 34 \end{array} \quad \begin{array}{r} 2.0 \\ 50 \end{array}$$

$$\begin{array}{r} 6.4 \\ 50 \end{array} \quad \begin{array}{r} 5.6 \\ 35 \end{array} \quad \begin{array}{r} 5.2 \\ 18 \end{array} \quad 4.8 \quad \begin{array}{r} 3.8 \\ 17 \end{array} \quad \begin{array}{r} 2.5 \\ 33 \end{array} \quad \begin{array}{r} 2.1 \\ 50 \end{array}$$

$$\begin{array}{r} 3.1 \\ 50 \end{array} \quad \begin{array}{r} 2.9 \\ 38 \end{array} \quad \begin{array}{r} 2.4 \\ 18 \end{array} \quad 2.4 \quad \begin{array}{r} 2.3 \\ 12 \end{array} \quad \begin{array}{r} 2.3 \\ 28 \end{array} \quad \begin{array}{r} 3.1 \\ 50 \end{array}$$

$$\begin{array}{r} 1.3 \\ 50 \end{array} \quad \begin{array}{r} 1.4 \\ 31 \end{array} \quad \begin{array}{r} 0.7 \\ 18 \end{array} \quad 0.6 \quad \begin{array}{r} 0.1 \\ 12 \end{array} \quad \begin{array}{r} 0.1 \\ 28 \end{array} \quad \begin{array}{r} 0.7 \\ 50 \end{array}$$

$$\begin{array}{r} 8.1 \\ 50 \end{array} \quad \begin{array}{r} 8.5 \\ 43 \end{array} \quad \begin{array}{r} 8.4 \\ 24 \end{array} \quad 8.4 \quad \begin{array}{r} 6.3 \\ 18 \end{array} \quad \begin{array}{r} 8.7 \\ 37 \end{array} \quad \begin{array}{r} 9.5 \\ 46 \end{array} \quad \begin{array}{r} 9.3 \\ 50 \end{array}$$

$$\begin{array}{r} 2.0 \\ 50 \end{array} \quad \begin{array}{r} 2.0 \\ 35 \end{array} \quad \begin{array}{r} 2.2 \\ 16 \end{array} \quad 2.3 \quad \begin{array}{r} 3.9 \\ 17 \end{array} \quad \begin{array}{r} 5.4 \\ 37 \end{array} \quad \begin{array}{r} 6.7 \\ 50 \end{array}$$

$$\begin{array}{r} 2.4 \\ 50 \end{array} \quad \begin{array}{r} 1.9 \\ 31 \end{array} \quad \begin{array}{r} 2.0 \\ 10 \end{array} \quad 2.8 \quad \begin{array}{r} 3.7 \\ 24 \end{array} \quad \begin{array}{r} 5.0 \\ 44 \end{array} \quad \begin{array}{r} 5.7 \\ 50 \end{array}$$

STN.

H.I.

ELE

915.12

38

12.2.

+50

09.3.

B.M.

6.94

915.05

6.94

908.18

908.11

39

09.8.

+50

05.0.

T.P.

2.08

904.18

12.95

902.10

40

99.6.

+50

00.1.

41

98.6.

+50

93.6.

+85

91.1.

42

92.6.

+50

00.6.

T.P.

11.52

914.95

0.75

903.43

43

10.1.
10.1.

+30

12.1.

$\frac{6.6}{50}$	$\frac{5.2}{41}$	$\frac{4.2}{22}$	2.9	$\frac{4.1}{22}$	$\frac{4.6}{41}$	$\frac{5.0}{50}$
------------------	------------------	------------------	-----	------------------	------------------	------------------

$\frac{8.2}{50}$	$\frac{6.8}{39}$	$\frac{5.8}{22}$	5.8	$\frac{6.8}{17}$	$\frac{7.5}{36}$	$\frac{8.2}{50}$
------------------	------------------	------------------	-----	------------------	------------------	------------------

Spt. in 14" Oak. 45' Rt. 38+70

$\frac{8.5}{50}$	$\frac{7.2}{41}$	$\frac{6.9}{24}$	7.3	$\frac{7.8}{21}$	$\frac{9.3}{33}$	$\frac{10.9}{50}$
------------------	------------------	------------------	-----	------------------	------------------	-------------------

$\frac{12.1}{50}$	$\frac{11.1}{38}$	$\frac{10.3}{25}$	10.1	$\frac{11.5}{23}$	$\frac{13.5}{50}$
-------------------	-------------------	-------------------	------	-------------------	-------------------

$\frac{4.3}{50}$	$\frac{4.6}{36}$	$\frac{5.0}{20}$	4.6	$\frac{4.3}{17}$	$\frac{4.3}{37}$	$\frac{4.7}{50}$
------------------	------------------	------------------	-----	------------------	------------------	------------------

$\frac{3.1}{50}$	$\frac{3.8}{20}$	4.1	$\frac{5.0}{12}$	$\frac{5.5}{30}$	$\frac{5.9}{50}$
------------------	------------------	-----	------------------	------------------	------------------

$\frac{4.4}{50}$	$\frac{5.2}{23}$	5.6	$\frac{6.2}{20}$	$\frac{6.6}{35}$	$\frac{6.9}{50}$
------------------	------------------	-----	------------------	------------------	------------------

$\frac{8.2}{50}$	$\frac{9.4}{32}$	$\frac{10.3}{16}$	10.6	$\frac{11.1}{20}$	$\frac{10.9}{35}$	$\frac{10.8}{50}$
------------------	------------------	-------------------	------	-------------------	-------------------	-------------------

$\frac{9.1}{50}$	$\frac{10.7}{32}$	$\frac{12.4}{14}$	13.1	$\frac{14.3}{21}$	$\frac{14.3}{50}$
------------------	-------------------	-------------------	------	-------------------	-------------------

$\frac{7.9}{50}$	$\frac{9.6}{32}$	$\frac{10.8}{15}$	11.6	$\frac{12.1}{15}$	$\frac{12.7}{33}$	$\frac{13.6}{50}$
------------------	------------------	-------------------	------	-------------------	-------------------	-------------------

$\frac{1.5}{50}$	$\frac{2.3}{30}$	$\frac{2.8}{13}$	3.6	$\frac{4.5}{15}$	$\frac{5.4}{35}$	$\frac{6.1}{50}$
------------------	------------------	------------------	-----	------------------	------------------	------------------

$\frac{6.2}{50}$	$\frac{5.4}{41}$	$\frac{4.6}{25}$	4.9	$\frac{5.4}{21}$	$\frac{6.2}{37}$	$\frac{6.7}{50}$
------------------	------------------	------------------	-----	------------------	------------------	------------------

$\frac{6.7}{50}$	$\frac{5.1}{35}$	$\frac{3.7}{18}$	2.9	$\frac{3.0}{20}$	$\frac{3.2}{50}$
------------------	------------------	------------------	-----	------------------	------------------

STA

7

HI ✓

-

ELEV

914.95

43+50

11.5.

44

06.6.

+50

02.1.

T.P.

1.28

903.36 ✓

12.87

902.08 ✓

44+50

02.1

45

99.0.

+50

97.7.

B.M.

4.25

906.60 ✓

1.02

902.34 ✓

902.35

46

97.9.

+50

97.5.

47

96.9.

+25

96.5.

+59

95.9.

+71

95.6.

+90

95.2.

<u>8.1</u>	<u>6.1</u>	<u>4.4</u>		<u>2.8</u>	<u>2.8</u>	<u>2.1</u>
50	27	14	3.5	18	38	50

<u>15.1</u>	<u>15.4</u>	<u>12.3</u>	<u>11.0</u>	<u>9.5</u>		<u>7.0</u>	<u>4.2</u>
56	51	46	33	15	8.4	22	50

	<u>12.3</u>	<u>9.8</u>	<u>9.1</u>
12.9	15	38	50

$\frac{38}{45}$ $\frac{46}{27}$ $\frac{2.5}{23}$ 1.3

$\frac{6.8}{50}$ $\frac{5.1}{43}$ $\frac{4.6}{27}$ $\frac{5.3}{11}$ $\frac{4.4}{16}$ $\frac{4.0}{33}$ $\frac{2.5}{50}$

$\frac{9.0}{50}$ $\frac{6.9}{35}$ $\frac{5.4}{30}$ $\frac{5.0}{14}$ $\frac{5.7}{57}$ $\frac{6.1}{3}$ $\frac{5.6}{18}$ $\frac{4.8}{42}$ $\frac{4.3}{50}$

S.E. Cor. Mont 22' Lt. 46+91 - M.C.

<u>12.9</u>	<u>10.1</u>	<u>9.1</u>	<u>8.7</u>		<u>9.2</u>	<u>9.1</u>	<u>8.6</u>	<u>7.9</u>
50	25	18	4	8.7	10	21	32	50

Lake	<u>14.3</u>	<u>10.9</u>	<u>9.4</u>	<u>9.3</u>	<u>8.2</u>	<u>9.6</u>		<u>9.4</u>	<u>9.0</u>	<u>7.7</u>	<u>6.4</u>	<u>6.3</u>
55	47	37	29	25	16	13	9.1	16	19	24	31	50

<u>2.4</u>	<u>2.8</u>	<u>3.5</u>	<u>3.2</u>	<u>9.3</u>	<u>10.0</u>		<u>9.4</u>	<u>10.0</u>	<u>3.9</u>	<u>4.3</u>
41	28	21	16	7	5	9.7	9	25	35	50

<u>4.6</u>	<u>7.9</u>	<u>1.9</u>	<u>1.5</u>	<u>9.6</u>	<u>10.3</u>		<u>9.7</u>	<u>10.4</u>	<u>3.2</u>	<u>3.7</u>
38	26	20	17	5	2	10.1	11	28	37	50

<u>4.6</u>	<u>10.7</u>	<u>2.8</u>	<u>2.6</u>	<u>10.7</u>	<u>11.0</u>		<u>10.3</u>	<u>10.7</u>	<u>10.0</u>	<u>2.1</u>	<u>3.2</u>
39	27	23	19	6	3	10.7	10	22	29	41	50

<u>4.6</u>	<u>10.1</u>	<u>3.9</u>	<u>3.1</u>	<u>10.6</u>	<u>11.3</u>		<u>10.6</u>	<u>10.9</u>	<u>10.7</u>	<u>4.9</u>	<u>4.2</u>	<u>2.5</u>	<u>4.4</u>
39	25	25	19	8	4	11.0	10	20	28	42	46	48	56

<u>4.6</u>	<u>11.2</u>	<u>7.1</u>	<u>5.3</u>	<u>5.0</u>	<u>11.7</u>		<u>11.1</u>	<u>11.6</u>	<u>12.0</u>	<u>11.9</u>	<u>13.3</u>	<u>14.6</u>
42	28	28	25	19	8	11.4	9	19	29	38	41	50

Lake Elev. 882.2

STA. 7 H.I. ✓ ELEV

906.60

48 94.9.

+22 94.0.

T.P. 3.34 897.18 ✓ 12.46 ✓ 894.14

+60 92.3.

+70 91.9.

+88 91.0.

49 90.4.

+50 88.0.

T.P. 0.50 889.00 ✓ 8.98 ✓ 888.50

+73 86.7.

+86 84.6.

+93 80.8.

50 82.5.

+50 79.4.

51 78.4.

LK 8.1 5.8 5.5 10.5 12.1 11.5 11.9 13.0 15.0
42 29 24 20 12 8 11.7 8 22 39 50

LK 12.4 8.2 7.1 6.9 12.1 13.1 12.5 12.8 13.2 12.8 15.5
44 35 30 27 22 14 10 12.6 6 20 28 39 50

LK 6.0 0.9 0.3 2.1 3.2 5.4 5.9 5.6 6.2 4.9 4.8 7.4 9.0
47 43 34 32 28 22 18 13 5.2 15 17 22 32 39 50

LK 10.0 5.6 2.5 1.5 2.9 3.9 5.6 6.4 5.9 6.7 6.6 7.9 9.1
47 44 44 39 35 29 22 19 14 5.6 10 15 19 35 50

LK 11.2 7.0 4.6 5.4 7.1 6.6 6.8 7.4 7.1 7.6 6.5 6.7 5.0 3.9
48 43 43 39 22 17 9 6.5 11 14 15 24 28 34 36 50

LK 8.3 6.1 6.3 7.4 7.7 7.1 7.4 8.2 8.3 6.5 6.0 5.5 4.5
48 40 39 23 20 17 6 7.1 9 12 22 24 27 42 50

LK 10.7 9.5 9.9 9.2 9.5 10.9 9.7 10.1 10.8 14.5 14.2
57 50 29 23 9 9.5 3 9 17 25 32 41 50

LK 6.8 3.3 2.1 2.4 1.8 2.1 4.5 6.3 7.4 8.0
52 46 31 26 15 1 23 6 22 35 50

LK 6.8 3.9 2.5 2.9 2.4 2.9 5.6 6.6 8.8
44 42 32 28 16 2 4.4 6 23 50

LK 6.8 3.7 2.5 3.1 2.6 3.0 8.2 9.1 8.4 9.5
43 40 32 28 16 1 1 8.2 20 23 50

LK 6.8 3.1 2.6 3.4 2.9 3.1 6.5 8.7 9.6 9.7 9.0 9.4
46 42 33 28 18 1 1 6.5 4 18 28 33 50

LK 6.8 3.5 3.3 4.4 4.0 4.5 10.3 11.4 11.4
54 48 38 36 24 10 9.6 4 27 50

3.2 3.4 4.6 4.9 4.6 5.1 9.2 10.3 10.5 10.5
50 47 43 40 30 17 9 4 10.6 24 50

57A

7

H.I

-

ELEV

889.00 ✓

51+50

79.0.

B.M.

3.28

885.72 ✓

885.73

52

79.0.

+30

77.9.

+55

77.9.

+84

78.4.

53

80.4.

—

+12

83.7.

+50

82.5.

T.P.

7.04

889.51 ✓

6.53

882.47 ✓

54

83.0.

+50

84.1.

55

84.7.

+50

84.6.

+73

84.6.

4 Rd.
 $\frac{6.3}{50} \frac{5.3}{48} \frac{4.9}{38} \frac{5.2}{25} \frac{9.5}{15} \frac{10.0}{11} \frac{10.1}{10.0} \frac{10.6}{19} \frac{10.6}{50}$

Spk. in 24" Pop. 40 Lt. 51+15

$\frac{5.1}{50} \frac{4.8}{43} \frac{5.9}{29} \frac{8.0}{23} \frac{9.7}{10} \frac{10.0}{10.0} \frac{9.7}{25} \frac{10.4}{50}$

4 Rd.
 $\frac{4.8}{50} \frac{4.8}{41} \frac{6.1}{27} \frac{9.1}{21} \frac{10.2}{17} \frac{11.1}{11.1} \frac{11.4}{29} \frac{10.9}{50}$

4 Rd.
 $\frac{5.1}{50} \frac{4.9}{36} \frac{6.0}{21} \frac{10.1}{13} \frac{11.2}{11.1} \frac{10.7}{24} \frac{10.8}{28} \frac{10.8}{50}$

4 Rd.
 $\frac{4.3}{50} \frac{6.7}{44} \frac{5.1}{38} \frac{5.0}{28} \frac{6.0}{13} \frac{9.5}{5} \frac{10.6}{10.6} \frac{11.5}{5} \frac{12.1}{19} \frac{11.3}{26} \frac{11.1}{50}$

4 Rd.
 $\frac{4.1}{50} \frac{4.6}{41} \frac{6.1}{37} \frac{5.3}{33} \frac{5.1}{22} \frac{6.0}{6} \frac{8.6}{8.6} \frac{10.9}{5} \frac{11.7}{10} \frac{11.6}{16} \frac{10.5}{29} \frac{10.5}{50}$

4 Rd.
 $\frac{3.8}{50} \frac{4.5}{36} \frac{6.1}{33} \frac{5.4}{28} \frac{5.2}{17} \frac{5.8}{5.8} \frac{10.0}{8} \frac{10.8}{12} \frac{10.4}{17} \frac{10.1}{30} \frac{10.4}{50}$

Lk. $\frac{6.8}{36} \frac{4.2}{31} \frac{4.2}{18} \frac{5.3}{16} \frac{6.0}{12} \frac{5.3}{5.3} \frac{5.2}{14} \frac{6.2}{20} \frac{9.5}{24} \frac{10.1}{32} \frac{10.1}{50}$

Lk. $\frac{7.3}{20} \frac{4.8}{16} \frac{4.4}{4} \frac{6.3}{2} \frac{6.5}{6.5} \frac{5.4}{14} \frac{6.4}{31} \frac{10.0}{37} \frac{10.0}{43} \frac{10.4}{50}$

Lk. $\frac{7.3}{25} \frac{4.6}{23} \frac{3.7}{9} \frac{5.3}{6} \frac{5.4}{5.4} \frac{4.9}{11} \frac{5.4}{25} \frac{9.2}{35} \frac{9.3}{39} \frac{9.4}{50}$

Lk. $\frac{7.3}{31} \frac{3.5}{28} \frac{3.8}{15} \frac{5.6}{11} \frac{5.1}{8} \frac{4.8}{4.8} \frac{5.4}{17} \frac{8.6}{24} \frac{9.6}{29} \frac{9.4}{33} \frac{10.0}{50}$

Lk. $\frac{7.3}{38} \frac{3.7}{35} \frac{3.3}{18} \frac{5.2}{14} \frac{5.5}{10} \frac{4.9}{4.9} \frac{4.9}{16} \frac{8.3}{22} \frac{8.9}{28} \frac{8.8}{35} \frac{9.0}{50}$

Lk. $\frac{7.3}{41} \frac{3.7}{39} \frac{3.4}{21} \frac{6.0}{14} \frac{6.2}{11} \frac{5.7}{9} \frac{4.9}{4.9} \frac{4.6}{6} \frac{4.7}{18} \frac{7.3}{24} \frac{7.7}{30} \frac{7.4}{34} \frac{5.4}{43} \frac{5.8}{50}$

5717

7

17.1

-

ELEY.

889.51

55+83

84.7.

56

84.8.

+50

B.M.

5.21

894.38

0.35

889.16

889.17

85.9.

57

87.5.

+32.33 End

88.4.

+50

89.0.

58

90.4.

+50

B.M.

5.21

889.17

92.0.

Lk $\frac{7.3}{42}$ $\frac{3.7}{37}$ $\frac{3.5}{23}$ $\frac{6.3}{15}$ $\frac{6.3}{12}$ $\frac{5.7}{10}$ 4.8 $\frac{4.5}{6}$ $\frac{4.6}{20}$ $\frac{5.1}{24}$ $\frac{5.1}{30}$ $\frac{5.6}{41}$ $\frac{4.9}{50}$

Lk $\frac{7.3}{45}$ $\frac{3.6}{39}$ $\frac{3.4}{24}$ $\frac{6.6}{16}$ $\frac{6.7}{11}$ $\frac{5.6}{9}$ 4.7 $\frac{4.3}{7}$ $\frac{4.2}{21}$ $\frac{4.6}{32}$ $\frac{3.7}{39}$ $\frac{2.7}{50}$

Lk $\frac{7.3}{46}$ $\frac{3.1}{40}$ $\frac{3.0}{26}$ $\frac{5.3}{21}$ $\frac{6.3}{17}$ $\frac{5.6}{12}$ $\frac{4.4}{10}$ 3.6 $\frac{3.3}{7}$ $\frac{3.2}{18}$ $\frac{4.1}{25}$ $\frac{3.3}{28}$ $\frac{3.1}{35}$ $\frac{0.0}{46}$

Spk. in 14" Pop. 14 Rt 57+35

Lk $\frac{12.2}{50}$ $\frac{8.2}{40}$ $\frac{8.1}{28}$ $\frac{9.2}{24}$ $\frac{8.9}{18}$ $\frac{7.9}{15}$ 6.9 $\frac{7.1}{11}$ $\frac{6.9}{14}$ $\frac{7.4}{19}$ $\frac{6.4}{22}$ $\frac{5.9}{27}$ $\frac{3.3}{34}$ $\frac{0.6}{47}$

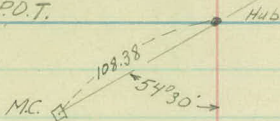
Lk $\frac{12.2}{48}$ $\frac{8.1}{39}$ $\frac{8.0}{27}$ $\frac{7.7}{17}$ $\frac{6.9}{15}$ 6.0 $\frac{6.2}{10}$ $\frac{5.6}{13}$ $\frac{6.0}{17}$ $\frac{4.7}{22}$ $\frac{4.3}{27}$ $\frac{0.4}{41}$

5.4

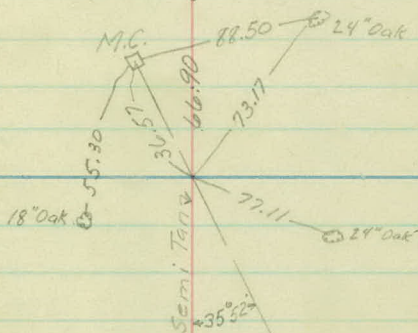
4.0

2.4

52+84.03 P.O.T.



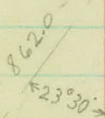
P.T. 47+25.0



P.I. 41+90.83

Cent. Sec. 31

P.O.T. 33+28.85



Cent. Sec. 31

Gen. Sec. 31 $\square$ $\swarrow$ 90° 32' $\searrow$ 89° 29' $\swarrow$ 24+23.37
 --- 230.03 ---

$\square$ So. 1/4 Cor. Sec. 31

LINE REVISION

FOR

ALTERNATE

B.M. 4.37 ✓ 928.05 923.68

25+50 19.1

+89 18.0

26 18.7

+40 21.5

+70 22.3

27 21.8

+30 20.8

+70 22.4

28 21.4

+50 23.3

29 ✓ 21.6

B.M. 4.37 ✓ 923.68

Mont. Cen. Sec. 31

$$\frac{13.9}{50} \quad \frac{11.5}{30} \quad \frac{9.7}{14} \quad 9.0 \quad \frac{8.2}{4} \quad \frac{7.4}{30} \quad \frac{6.1}{50}$$

$$\frac{10.9}{50} \quad \frac{13.9}{32} \quad \frac{11.3}{14} \quad 10.1 \quad \frac{9.0}{2} \quad \frac{8.2}{22} \quad \frac{6.2}{50}$$

$$\frac{15.3}{50} \quad \frac{12.5}{32} \quad \frac{10.4}{15} \quad \frac{9.9}{2} \quad 9.4 \quad \frac{8.8}{5} \quad \frac{7.5}{27} \quad \frac{5.8}{50}$$

$$\frac{8.3}{50} \quad \frac{6.5}{17} \quad 6.6 \quad \frac{6.3}{11} \quad \frac{5.8}{28} \quad \frac{5.1}{50}$$

$$\frac{6.6}{50} \quad \frac{6.2}{24} \quad 5.7 \quad \frac{5.8}{8} \quad \frac{5.8}{24} \quad \frac{5.4}{50}$$

$$\frac{26}{50} \quad \frac{7.3}{37} \quad \frac{6.3}{17} \quad 6.3 \quad \frac{6.6}{23} \quad \frac{7.7}{50}$$

$$\frac{9.7}{50} \quad \frac{9.5}{16} \quad \frac{8.0}{19} \quad 7.3 \quad \frac{6.8}{14} \quad \frac{7.3}{33} \quad \frac{7.3}{50}$$

$$\frac{7.1}{50} \quad \frac{6.7}{40} \quad \frac{5.7}{15} \quad 5.7 \quad \frac{5.3}{26} \quad \frac{4.8}{50}$$

$$\frac{6.5}{50} \quad \frac{5.1}{36} \quad 3.7 \quad \frac{4.1}{7} \quad \frac{3.6}{21} \quad \frac{3.8}{50}$$

$$\frac{9.4}{50} \quad \frac{6.2}{18} \quad 4.8 \quad \frac{10}{25} \quad \frac{3.5}{50}$$

$$\frac{12.5}{50} \quad \frac{8.0}{25} \quad 6.5 \quad \frac{4.8}{25} \quad \frac{3.6}{50}$$

29

28

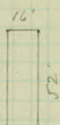
27

26

25

+25- Tr. 4

+75- Sta. 11



+07-84r. 17'
+00-54r. 24'

Yard

+90- Tr. 11'
+75- Tr. 5'
+61- Sta. 16'
+60- Tr. 1'
+47- Sta. 7'
+21- Sta. 5'
+21- F. Int.
+17- Ev. 9r. Tr. 20-25-30'

Orchard

+95- Ev. 9r. Tr. 1'
+89- " " " 1'
+82- Apple Tr. 33'
+82- Ev. 9r. Tr. 1'
+72- " " " 1'
+59- Apple Tr. 5'
+26- Ev. 9r. Tr. 1'
+19- " " " 1'
+14- " " " 1'
+07- F. Int.

Berry Patch

Pasture

Cultivated

+44- Ev. 9r. Tr. 1'
+19- " " " 1'
+12- " " " 1'

+45- Ev. 9r. Tr. 1'
+82- " " " 1'



Plants in hand. 12/21/32
Proj. 33-432
Vait
Carley
Croise

- X 0+50 Rt. pl. 15" X 24" C.M.
- X 0+50 to 3+50 Cl. 15 Gr. 16
- X 3+50 Rt - Pl. 24" X 36" P3
- X 12+ V.P. in pl. Reint.
- X 12+40 Pl. 30" X 42" P3
- X 12+00 to 13+00 Cl. 3+1-
- X 15+85 Rt. & Lt. - Pl. 2 - 15" X 20" C.Ms
- X 16+50 to 18+50 Cl. 10 +1- Gr. 1
- X 17+83 Reint. culv. Pl. 24" P3 X 60'
- X 19+50 to 22+00 Cl. 1 Gr. 7
- X 21+75 Lt - Pl. 15" X 20" C.M.
- X 23+00 - Rt. & Lt. No. culv. req
- X 26+00 to 27+50 Cl. & Gr. 7
- X 27+50 to 30+00 Cl. 22 Gr. 40
- X 26+00 Lt. No. culv. req.
- X 26+00 Rt. Pl. 15" X 20" C.M.
- X 32+45 Pl. 36" X 72 P3
- X 35+50 Pl 2. 15" X 20" C.Ms R & L
- X 40+00 - 40+50 - Cl. 1
- X 37+00 to 41+25 - Gr. A. 0.61
- X 42+25 to 45+00 - Gr. A. 0.41
- X 41+85 - Pl. 24" P3 X 54'
- X 43+00 to 45+00 Cl. 4
- X 45+00 Lt Pl. 18" P3 X 32'

- X 45+50 to 46+00 Cl. & Gr. 1
- X 47+00 to 49 - Cl. & Gr. 24 tr
- X 48+92 Rt. R. 122. PA 15' x 20.0, M
- X 49+50 - 50+00 Cl. & Gr. 1
- X 50+00 - 53+25 Cl. Acro. ^{0.2} Rt. side
- X 49+93 Ext. Rt. 60" x 20' CM,
- X 53+50 - 57+25 Cl. & Gr. 34 tr.

34W32
Alignment
Line Change

57+03.56 P.T. $35^{\circ}39'$

57 $35^{\circ}20'$

+50 $30^{\circ}50'$

56 $26^{\circ}20'$

+50 $21^{\circ}50'$

$\Delta-71^{\circ}18'$

$D-18^{\circ}L$

55+36.7 P.I.

$T-229.25$

$L-396.11$

55 $17^{\circ}20'$

$R-319.63$

+50 $12^{\circ}50'$

54 $8^{\circ}20'$

183

+50 $3^{\circ}50'$

113

53+07.45 P.C. $0^{\circ}00'$

49+49.98 P.T.

$1^{\circ}30'$

$\Delta-3^{\circ}00'$

$D-3^{\circ}R$

49+00 P.I.

$0^{\circ}45'$

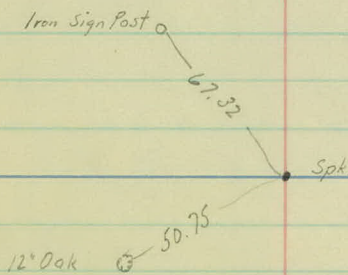
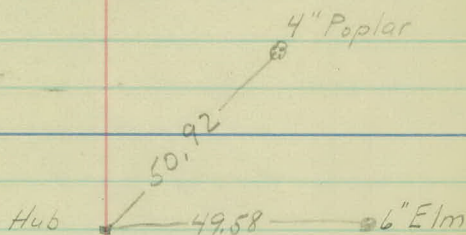
$T-50.02$

$L-100.0$

48+49.98 P.C.

$0^{\circ}00'$

$R-1910.08$



57+32.33 old P.T.

57+53.71=

18" Oak



36.73

10" Oak



37.04

Spk.



34W 32
X-Sections
Line Change

B.M. 8.94 894.67 ✓ 885.73
90.5

49+00

+50

87.9

T.P. 4.57 890.48 ✓ 8.76 885.91 ✓

+85

83.9

+95

80.3

50

80.3

+06

81.5

+30

79.2

B.M. 3.40 889.13 ✓ 4.75 885.73 ✓

51

78.3

+50

78.6

T.P. 4.30 888.24 ✓ 5.19 883.94 ✓

52

79.0

+50

77.7

53

77.4

T.P. 5.46 889.14 ✓ 4.56 883.68 ✓

26

Spt in 24" Poplar Lt. 51+15

 $\frac{12.0}{50}$ $\frac{3.3}{39}$ $\frac{3.6}{24}$ $\frac{5.0}{18}$ 4.2 $\frac{4.7}{10}$ $\frac{5.3}{21}$ $\frac{3.7}{25}$ $\frac{2.0}{50}$
 $\frac{7.2}{50}$ $\frac{6.5}{30}$ $\frac{7.0}{26}$ $\frac{6.3}{13}$ 6.8 $\frac{8.2}{5}$ $\frac{7.2}{11}$ $\frac{7.0}{16}$ $\frac{9.4}{31}$ $\frac{11.4}{36}$ $\frac{11.7}{50}$
 $\frac{8.2}{50}$ $\frac{5.3}{46}$ $\frac{3.9}{35}$ $\frac{4.4}{31}$ $\frac{4.0}{20}$ $\frac{4.2}{7}$ 6.6 $\frac{9.1}{23}$ $\frac{11.0}{50}$
 $\frac{8.1}{50}$ $\frac{5.4}{46}$ $\frac{4.0}{36}$ $\frac{4.6}{33}$ $\frac{4.2}{21}$ $\frac{4.5}{6}$ $\frac{9.6}{6}$ 10.2 $\frac{11.0}{11}$ $\frac{11.2}{50}$
 $\frac{8.1}{50}$ $\frac{5.4}{46}$ $\frac{4.0}{36}$ $\frac{4.6}{33}$ $\frac{4.2}{21}$ $\frac{5.0}{9}$ 10.2 $\frac{11.0}{11}$ $\frac{11.2}{50}$
 $\frac{6.3}{50}$ $\frac{4.4}{47}$ $\frac{4.2}{38}$ $\frac{5.2}{35}$ $\frac{4.5}{24}$ $\frac{4.8}{11}$ 9.0 $\frac{11.0}{11}$ $\frac{11.2}{50}$
 $\frac{4.8}{50}$ $\frac{4.5}{42}$ $\frac{5.5}{39}$ $\frac{5.1}{27}$ $\frac{5.6}{13}$ $\frac{10.8}{5}$ 11.3 $\frac{11.3}{50}$
 $\frac{5.1}{50}$ $\frac{4.8}{42}$ $\frac{5.2}{28}$ $\frac{10.5}{17}$ 10.8 $\frac{10.8}{50}$
 $\frac{5.1}{50}$ $\frac{5.6}{37}$ $\frac{9.7}{29}$ 10.5 $\frac{10.4}{50}$
 $\frac{4.7}{50}$ $\frac{5.1}{45}$ $\frac{8.5}{32}$ 9.2 $\frac{9.8}{34}$ $\frac{9.8}{50}$
 $\frac{4.5}{50}$ $\frac{5.0}{41}$ $\frac{8.7}{34}$ $\frac{10.0}{23}$ 10.5 $\frac{10.2}{50}$
 $\frac{4.6}{50}$ $\frac{5.2}{26}$ $\frac{10.2}{15}$ 10.8 $\frac{10.8}{20}$ $\frac{10.5}{50}$

889.14

53+45

79.1

+73

83.1

54

83.7

+50

84.3

55

82.8

+50

81.7

T.P. 5.71 890.11 - 4.74 884.40 ✓

+78

84.6

56

84.9

+50

85.9

57+03.56 P.T.

87.1

B.M.

0.95 889.16 ✓ 889.17

$$\frac{4.2}{50} \quad \frac{4.2}{42} \quad \frac{5.8}{39} \quad \frac{5.4}{14} \quad \frac{6.2}{8} \quad 10.0 \quad \frac{10.4}{50}$$

$$\frac{3.8}{40} \quad \frac{3.8}{34} \quad \frac{6.3}{29} \quad \frac{5.3}{6} \quad 60 \quad \frac{10.1}{7} \quad \frac{10.4}{50}$$

$$\frac{4.0}{40} \quad \frac{4.0}{29} \quad \frac{6.2}{20} \quad \frac{5.4}{14} \quad 5.4 \quad \frac{5.6}{4} \quad \frac{9.8}{12} \quad \frac{10.1}{19} \quad \frac{10.4}{50}$$

$$\frac{3.3}{40} \quad \frac{3.3}{32} \quad \frac{5.4}{25} \quad \frac{4.7}{13} \quad 4.8 \quad \frac{5.2}{4} \quad \frac{9.2}{11} \quad \frac{9.6}{15} \quad \frac{10.0}{50}$$

$$\frac{3.5}{45} \quad \frac{3.5}{37} \quad \frac{5.0}{33} \quad \frac{4.4}{16} \quad \frac{4.8}{4} \quad 6.3 \quad \frac{8.5}{5} \quad \frac{9.0}{10} \quad \frac{9.5}{50}$$

$$\frac{3.0}{45} \quad \frac{3.0}{38} \quad \frac{5.1}{31} \quad \frac{4.5}{19} \quad \frac{4.5}{6} \quad 7.4 \quad \frac{8.6}{9} \quad \frac{9.0}{50}$$

$$\frac{3.7}{45} \quad \frac{3.7}{37} \quad \frac{6.3}{31} \quad \frac{5.3}{14} \quad 5.5 \quad \frac{8.8}{7} \quad \frac{8.8}{27} \quad \frac{7.4}{50}$$

$$\frac{4.0}{45} \quad \frac{4.0}{38} \quad \frac{6.8}{28} \quad \frac{5.4}{15} \quad 5.2 \quad \frac{5.8}{18} \quad \frac{6.7}{33} \quad \frac{3.3}{50}$$

$$\frac{3.8}{40} \quad \frac{3.8}{37} \quad \frac{7.2}{28} \quad \frac{5.6}{20} \quad 4.2 \quad \frac{4.1}{11} \quad \frac{5.2}{17} \quad \frac{4.0}{28} \quad \frac{2.7}{36}$$

$$\frac{3.6}{40} \quad \frac{3.6}{32} \quad \frac{5.2}{20} \quad \frac{4.0}{16} \quad 3.0 \quad \frac{3.0}{12} \quad \frac{3.4}{17} \quad \frac{2.7}{25} \quad \frac{4.3}{33}$$

Spk. in 14" Poplar 14' Rt. 57+35

34W/32
Topog.
Line Change

55

54

53

52

51

50

49

F.39'

+50-F.38'

F.37'

+50-F.33'

F.31'

+50-F.42'

+26-F.4'

+17-Beg. F.57'

+20-T.P.22'

+74-Beg. F.19'

+64-T.P.30'

+37-T.P.6'

+93-X Drain 5.5'

F.15'

+85-End Low Land

+50-F.9'

+08-T.P.5'
F.10'

+50-F.16'

F.19'

+94-T.P.9'

+50-F.7.5'

58

57

(94)

56

+03.56 F. 32'

+50 - F. 37'

X			X
X			X
X			X
X			X
X			X

+03.56 F. 20'

+50 - F. 20'

+35 - T. P. 19'
+18 - Gate 19'
+03 - E. Dr.

SS 4.2

10 Rod. # 34-W 32
V1920N1915

Lake

Elev. 8694

+65-1069.40'
+65-2084.245'
+49-100'

+00-54'

+45-4

77.2

Inlet
76.4

Inlet
76.6

77.8

K-Drain

35' Peat

75.8

71.6
Quartz

34

33 -

32

97

