

399 X-9-D, Dr. 11-A

OFFICE OF COUNTY ENGINEER
RAMSEY CO. MINN.

FINAL X-SECTION Survey

NO. COUNTY LINE

From..... To.....

Road Acc't. No.

Date Filed.....

File.....

1-10
6/21/35

Puntell
Bell
Skog
Goldberg

Final X-Sections
and Farm Ent + Culvert Measurements

No. County Line

Sta	+	π	-	Elev.
B.M.	5.24	884.39		879.15
①	6.75	889.81	1.33	883.06
59				81.0
+50				82.0
60				83.0
+50				83.6
61				84.4
+50				84.9
62				85.4
+50				85.6
63				85.3
+50				84.6

SpK. in 20" Oak 120' Lt Sta. 55+84

$$\begin{array}{r} 11.6 \\ 33 \end{array} \quad \begin{array}{r} 10.4 \\ 18 \end{array} \quad \begin{array}{r} 9.0 \\ 13 \end{array} \quad \begin{array}{r} 8.8 \\ 6 \end{array} \quad \begin{array}{r} 9.1 \\ 12 \end{array} \quad \begin{array}{r} 10.4 \\ 17-21 \end{array} \quad \begin{array}{r} 9.7 \\ 22 \end{array} \quad \begin{array}{r} 9.7 \\ 33 \end{array}$$

$$\begin{array}{r} 10.0 \\ 33-18 \end{array} \quad \begin{array}{r} 8.0 \\ 13 \end{array} \quad \begin{array}{r} 7.8 \\ 6 \end{array} \quad \begin{array}{r} 8.1 \\ 13 \end{array} \quad \begin{array}{r} 9.4 \\ 17 \end{array} \quad \begin{array}{r} 9.6 \\ 21 \end{array} \quad \begin{array}{r} 9.2 \\ 22 \end{array} \quad \begin{array}{r} 9.0 \\ 33 \end{array}$$

$$\begin{array}{r} 9.1 \\ 33 \end{array} \quad \begin{array}{r} 8.7 \\ 17 \end{array} \quad \begin{array}{r} 7.0 \\ 13 \end{array} \quad \begin{array}{r} 6.8 \\ 13 \end{array} \quad \begin{array}{r} 7.0 \\ 17 \end{array} \quad \begin{array}{r} 8.2 \\ 22 \end{array} \quad \begin{array}{r} 8.7 \\ 23 \end{array} \quad \begin{array}{r} 7.6 \\ 33 \end{array}$$

$$\begin{array}{r} 7.6 \\ 33 \end{array} \quad \begin{array}{r} 7.3 \\ 22 \end{array} \quad \begin{array}{r} 7.8 \\ 21-17 \end{array} \quad \begin{array}{r} 6.1 \\ 13 \end{array} \quad \begin{array}{r} 6.2 \\ 13 \end{array} \quad \begin{array}{r} 6.4 \\ 17 \end{array} \quad \begin{array}{r} 7.4 \\ 22 \end{array} \quad \begin{array}{r} 7.3 \\ 24 \end{array} \quad \begin{array}{r} 6.4 \\ 33 \end{array}$$

$$\begin{array}{r} 6.2 \\ 33 \end{array} \quad \begin{array}{r} 6.0 \\ 23 \end{array} \quad \begin{array}{r} 7.1 \\ 22 \end{array} \quad \begin{array}{r} 7.0 \\ 17 \end{array} \quad \begin{array}{r} 5.6 \\ 13 \end{array} \quad \begin{array}{r} 5.4 \\ 13 \end{array} \quad \begin{array}{r} 5.4 \\ 16 \end{array} \quad \begin{array}{r} 6.7 \\ 22 \end{array} \quad \begin{array}{r} 6.8 \\ 24 \end{array} \quad \begin{array}{r} 5.2 \\ 33 \end{array}$$

$$\begin{array}{r} 4.8 \\ 33 \end{array} \quad \begin{array}{r} 4.6 \\ 26 \end{array} \quad \begin{array}{r} 6.6 \\ 20-17 \end{array} \quad \begin{array}{r} 4.9 \\ 13 \end{array} \quad \begin{array}{r} 4.9 \\ 13 \end{array} \quad \begin{array}{r} 6.6 \\ 19-22 \end{array} \quad \begin{array}{r} 3.1 \\ 30 \end{array} \quad \begin{array}{r} 3.0 \\ 33 \end{array}$$

$$\begin{array}{r} 2.3 \\ 40 \end{array} \quad \begin{array}{r} 2.4 \\ 31 \end{array} \quad \begin{array}{r} 6.1 \\ 11-17 \end{array} \quad \begin{array}{r} 4.5 \\ 13 \end{array} \quad \begin{array}{r} 4.4 \\ 13 \end{array} \quad \begin{array}{r} 4.5 \\ 13 \end{array} \quad \begin{array}{r} 6.6 \\ 19 \end{array} \quad \begin{array}{r} 6.5 \\ 23 \end{array} \quad \begin{array}{r} 1.6 \\ 33 \end{array} \quad \begin{array}{r} 1.4 \\ 40 \end{array}$$

$$\begin{array}{r} 1.7 \\ 40 \end{array} \quad \begin{array}{r} 1.8 \\ 33 \end{array} \quad \begin{array}{r} 6.0 \\ 23-17 \end{array} \quad \begin{array}{r} 4.4 \\ 13 \end{array} \quad \begin{array}{r} 4.2 \\ 13 \end{array} \quad \begin{array}{r} 4.3 \\ 19 \end{array} \quad \begin{array}{r} 6.5 \\ 24 \end{array} \quad \begin{array}{r} 6.3 \\ 33 \end{array} \quad \begin{array}{r} 2.0 \\ 40 \end{array}$$

$$\begin{array}{r} 2.5 \\ 40 \end{array} \quad \begin{array}{r} 2.4 \\ 33 \end{array} \quad \begin{array}{r} 6.1 \\ 23-18 \end{array} \quad \begin{array}{r} 4.5 \\ 13 \end{array} \quad \begin{array}{r} 4.5 \\ 13 \end{array} \quad \begin{array}{r} 6.1 \\ 19-23 \end{array} \quad \begin{array}{r} 3.5 \\ 33 \end{array} \quad \begin{array}{r} 3.7 \\ 40 \end{array}$$

$$\begin{array}{r} 4.0 \\ 40 \end{array} \quad \begin{array}{r} 4.0 \\ 33 \end{array} \quad \begin{array}{r} 6.8 \\ 23-19 \end{array} \quad \begin{array}{r} 5.2 \\ 13 \end{array} \quad \begin{array}{r} 5.2 \\ 13 \end{array} \quad \begin{array}{r} 7.0 \\ 19 \end{array} \quad \begin{array}{r} 6.8 \\ 23 \end{array} \quad \begin{array}{r} 5.0 \\ 31 \end{array} \quad \begin{array}{r} 5.0 \\ 40 \end{array}$$

Sta	+	π	-	Elev.
		889.81		
64				83.8
	+50			83.0
65				81.5
	+50			80.0
66				78.6
①	3.11	881.69	11.23	878.58
	+50			77.0
67				75.3
	+50			73.5
68	+68			72.5
68				71.7
	+20			71.3
①	2.75	873.37	11.07	870.62

7.2 6.8 7.5 7.5 6.1 4.1
40 31 26 19 13 6.0 4.0 7.7 7.7 5.7 5.7
13 19 23 32 40

8.2 7.5 8.5 8.6 6.7 5.0
40 31 24 19 13 6.8 6.8 8.4 6.0 6.0
13 19-23 33 40

8.6 8.4 9.8 8.1 7.0
40 31 23-19 13 8.3 8.2 10.0 10.0 8.0 8.2
13 19 24 31 40

9.8 11.2 11.3 9.7 9.4
40 31 24 19 13 9.8 9.7 11.2 10.2 10.4
13 19-26 31 40

9.3 9.5 12.8 11.3 10.9
40 33 23-19 13 11.2 11.2 12.7 13.0 11.6 11.7
13 19 26 32 40

Top Lt Blue top Sta 66+00

1.2 1.5 6.4 4.7 4.2
40 33 22-18 13 4.7 4.7 6.2 4.0 4.1
13 19-24 33 40

3.0 2.3 7.6 7.7 6.4 6.4
40 33 22 18 13 6.4 6.4 7.7 7.8 6.6
13 19 26 31-40

4.9 5.4 9.4 8.2 8.6
40 33 22-18 13 8.2 8.1 9.6 9.9
13 19-27 33

6.8 7.4 10.5 9.1 9.7
40 33 24-19 13 9.2 9.2 10.7 11.4
13 19 33

8.1 8.6 11.2 9.8 11.0
40 32 24-19 13 10.0 9.8 13.7 14.6
13 29 40

9.4 9.7 11.8 11.7 10.4 11.7
40 31 25 18 13 10.4 10.4 14.6 14.7
13 31 40

Top Lt Blue top Sta 68+50

Sta + π - Elev

87337

68+50

70.7

69

69.7

+50

69.0

70

68.5

+50

68.5

71

68.7

+50

68.6

72

68.8

+50

69.1

+60

69.2

+80

69.1

+85

69.0

$$\frac{3.6}{2.3} \quad \frac{4.0}{2.7} \quad \frac{4.8}{2.3} \quad \frac{4.7}{1.9} \quad \frac{4.2}{1.8} \quad \frac{2.7}{1.3} \quad 2.7 \quad \frac{2.7}{1.3} \quad \frac{6.4}{2.7} \quad \frac{6.2}{4.0}$$

$$\begin{array}{r} 6.2 \\ 33 \end{array} \quad \begin{array}{r} 6.4 \\ 21 \end{array} \quad \begin{array}{r} 3.8 \\ 13 \end{array} \quad \begin{array}{r} 5.6 \\ 3.7 \\ 13 \end{array} \quad \begin{array}{r} 6.7 \\ 24 \end{array} \quad \begin{array}{r} 6.7 \\ 33 \end{array}$$

$$\begin{array}{r} 6.0 \\ 4.4 \overline{) 6.6} \\ \underline{4.4} \\ 2.2 \\ \underline{2.2} \\ 0.0 \end{array} \quad \begin{array}{r} 4.5 \\ 13 \overline{) 4.5} \\ \underline{13} \\ 0.0 \end{array} \quad \begin{array}{r} 6.7 \\ 21 \overline{) 6.7} \\ \underline{42} \\ 25 \\ \underline{21} \\ 4 \end{array} \quad \begin{array}{r} 6.8 \\ 33 \overline{) 6.8} \\ \underline{33} \\ 35 \\ \underline{33} \\ 2 \end{array}$$

$$\begin{array}{r} 73 \\ 33 \end{array} \quad \begin{array}{r} 75 \\ 23 \end{array} \quad \begin{array}{r} 49 \\ 13 \end{array} \quad \begin{array}{r} 66 \\ 49 \end{array} \quad \begin{array}{r} 50 \\ 13 \end{array} \quad \begin{array}{r} 77 \\ 23 \end{array} \quad \begin{array}{r} 76 \\ 33 \end{array}$$

$$\frac{6.8}{33} \quad \frac{7.0}{20} \quad \frac{5.0}{13} \quad \frac{6.4}{4.9} \quad \frac{5.0}{13} \quad \frac{6.7}{20} \quad \frac{6.7}{33}$$

$$\begin{array}{r} 6.8 \\ 33 \end{array} \quad \begin{array}{r} 6.8 \\ 20 \end{array} \quad \begin{array}{r} 5.0 \\ 13 \end{array} \quad \begin{array}{r} 6.7 \\ 4.7 \end{array} \quad \begin{array}{r} 4.9 \\ 13 \end{array} \quad \begin{array}{r} 6.6 \\ 20 \end{array} \quad \begin{array}{r} 6.0 \\ 33 \end{array}$$

$$33 \cdot \frac{68}{20} \quad \frac{50}{13} \quad 61 \quad 4.8 \quad \frac{50}{13} \quad \frac{616}{21} \quad \frac{65}{33}$$

$$\begin{array}{r} 6.8 \\ 33 \overline{) 2244} \\ \underline{198} \\ 264 \\ \underline{231} \\ 33 \end{array}$$

$$\begin{array}{r} 6.9 \\ \underline{33} \end{array} \quad \begin{array}{r} 6.8 \\ \underline{22} \end{array} \quad \begin{array}{r} 4.6 \\ \underline{13} \end{array} \quad \begin{array}{r} 6.3 \\ 4.3 \end{array} \quad \begin{array}{r} 4.5 \\ \underline{13} \end{array} \quad \begin{array}{r} 6.7 \\ \underline{22-34} \end{array}$$

$$33 - \frac{6.6}{2} \quad \frac{4.7}{13} \quad \frac{6.4}{4.2} \quad \frac{4.6}{13} \quad \frac{9.7}{27} \quad \frac{9.0}{33}$$

$$\begin{array}{r} 11.6 \\ 20 \end{array} \quad \begin{array}{r} 10.4 \\ 25 \end{array} \quad \begin{array}{r} 4.5 \\ 13 \end{array} \quad 4.3 \quad \begin{array}{r} 4.5 \\ 13 \end{array} \quad \begin{array}{r} 9.6 \\ 26 \end{array} \quad \begin{array}{r} 10.1 \\ 33 \end{array}$$

F.L.ne. — 12.00 C.M.

$$\begin{array}{r} 11.8 \\ \underline{31} \end{array} \quad \begin{array}{r} 10.0 \\ \underline{25} \end{array} \quad \begin{array}{r} 4.5 \\ \underline{13} \end{array} \quad 44 \quad \begin{array}{r} 4.6 \\ \underline{13} \end{array} \quad \begin{array}{r} 9.3 \\ \underline{26} \end{array} \quad \begin{array}{r} 9.3 \\ \underline{33} \end{array}$$

Sta	+	π	-	Elev.
		873.37		
72+95				69.0
73	+50			69.2
	+50			69.8
74	+50			70.6
	+50			71.2
75				71.9
	+40			72.7
	+50			73.0
①	10.73	883.44	0.66	872.71
76				73.6
	+50			74.4
	+76			74.8
77				75.2

FLine 11.45

$$\frac{6.8}{33} \frac{7.3}{24} \frac{4.4}{13} 4.4 \frac{4.5}{13} \frac{9.1}{23} \frac{8.0}{33}$$

$$\frac{6.4}{33} \frac{7.3}{24} \frac{4.3}{13} 4.2 \frac{4.4}{13} 11.2 \frac{26-33}{26-33}$$

$$\frac{6.6}{33} \frac{6.5}{24} \frac{3.8}{13} 3.6 \frac{3.7}{13} \frac{6.9}{26-33}$$

$$\frac{5.8}{33} \frac{5.0}{22} \frac{3.0}{13} 5.4 \frac{3.0}{13} \frac{5.0}{22} \frac{5.2}{33}$$

$$\frac{5.5}{33} \frac{4.8}{23} \frac{2.4}{13} 2.6 \frac{2.3}{13} \frac{3.8}{20-27} \frac{3.0}{32-40}$$

$$\frac{3.5}{40} \frac{3.0}{33} \frac{3.1}{30} \frac{3.0}{21} \frac{1.5}{13} 1.8 \frac{1.4}{13} \frac{3.1}{20-26} \frac{1.6}{31} \frac{1.8}{40}$$

$$\frac{2.8}{40} \frac{2.0}{30} \frac{2.5}{27-19} \frac{0.9}{13} 1.4 \frac{1.0}{13} \frac{2.6}{21-28} \frac{1.2}{33} \frac{1.1}{40}$$

$$\frac{2.4}{40} \frac{1.9}{31} \frac{2.5}{19} \frac{2.3}{20} \frac{0.7}{13} 1.3 \frac{0.7}{13} \frac{2.4}{20} \frac{2.5}{27} \frac{1.3}{32} \frac{0.7}{40}$$

$$\frac{13.1}{33} \frac{13.2}{26} \frac{10.0}{13} 12.1 \frac{10.0}{13} \frac{12.4}{24} \frac{12.2}{33}$$

$$\frac{13.0}{33-29} \frac{9.2}{13} 11.7 \frac{9.0}{13} \frac{11.8}{25-33}$$

$$\frac{11.2}{33} \frac{11.0}{27} \frac{8.6}{13} 10.7 \frac{8.6}{13} \frac{10.4}{22-33}$$

$$\frac{8.2}{40} \frac{8.4}{31} \frac{9.8}{25-20} \frac{8.1}{13} 9.3 \frac{8.1}{13} \frac{9.8}{19-28} \frac{8.8}{31-40}$$

Sta	+	π	-	Elev
		883.44		
77+50				76.1
78				77.0
+50				77.7
79				78.8
+50				79.7
80				80.5
+50				81.0
81				81.7
+50				82.4
82				82.9
①	2.78	885.55	0.67	882.77
+50				83.0
83				82.9

$$\begin{array}{r} 6-10 \\ 83.77 \\ 2.78 \\ \hline 86.55 \end{array}$$

$$\begin{array}{r} 6.3 \quad 6.4 \quad 9.1 \quad 9.0 \quad 7.4 \quad 7.4 \\ 40 \quad 33 \quad 24 \quad 19 \quad 13 \quad 13 \end{array} \quad \begin{array}{r} 7.4 \\ 7.3 \end{array} \quad \begin{array}{r} 7.4 \quad 8.8 \\ 13 \quad 20-24 \end{array} \quad \begin{array}{r} 6.5 \\ 33-40 \end{array}$$

$$\begin{array}{r} 4.2 \quad 4.4 \quad 8.2 \quad 6.4 \quad 5.6 \\ 35 \quad 38 \quad 23-19 \quad 13 \quad 6.4 \end{array} \quad \begin{array}{r} 6.4 \quad 7.8 \\ 13 \quad 20-24 \end{array} \quad \begin{array}{r} 5.6 \quad 6.1 \\ 33 \quad 40 \end{array}$$

$$\begin{array}{r} 4.4 \quad 4.8 \quad 7.5 \quad 5.1 \quad 7.1 \\ 40 \quad 33 \quad 24-19 \quad 13 \quad 5.1 \end{array} \quad \begin{array}{r} 5.1 \quad 7.3 \\ 13 \quad 20-25 \end{array} \quad \begin{array}{r} 6.0 \\ 31-40 \end{array}$$

$$\begin{array}{r} 5.0 \quad 5.3 \quad 6.5 \quad 4.7 \quad 4.1 \\ 40 \quad 31 \quad 16-20 \quad 13 \quad 4.6 \end{array} \quad \begin{array}{r} 4.6 \quad 6.4 \quad 6.1 \\ 13 \quad 20 \quad 33 \end{array}$$

$$\begin{array}{r} 6.2 \quad 5.5 \quad 6.0 \quad 5.8 \quad 3.9 \quad 4.1 \\ 33 \quad 26 \quad 25 \quad 19 \quad 13 \quad 3.7 \end{array} \quad \begin{array}{r} 4.0 \quad 6.2 \quad 6.3 \\ 13 \quad 21 \quad 33 \end{array}$$

$$\begin{array}{r} 5.5 \quad 4.5 \quad 3.1 \quad 3.6 \\ 33 \quad 19 \quad 13 \quad 2.9 \end{array} \quad \begin{array}{r} 2.9 \quad 5.7 \quad 6.0 \\ 13 \quad 24 \quad 33 \end{array}$$

$$\begin{array}{r} 4.6 \quad 4.0 \quad 2.4 \quad 2.1 \\ 40 \quad 19-20 \quad 13 \quad 2.4 \end{array} \quad \begin{array}{r} 2.5 \quad 4.8 \quad 5.3 \\ 13 \quad 25 \quad 33 \end{array}$$

$$\begin{array}{r} 2.8 \quad 2.3 \quad 3.4 \quad 1.7 \quad 1.4 \\ 40 \quad 31 \quad 16-20 \quad 13 \quad 1.7 \end{array} \quad \begin{array}{r} 1.8 \quad 3.7 \quad 4.0 \\ 13 \quad 23 \quad 33 \end{array}$$

$$\begin{array}{r} 1.4 \quad 0.6 \quad 0.8 \quad 1.8 \quad 2.8 \quad 1.1 \quad 0.7 \\ 40 \quad 33 \quad 32 \quad 31 \quad 24-18 \quad 13 \quad 1.0 \end{array} \quad \begin{array}{r} 1.1 \quad 2.6 \quad 2.6 \quad 2.3 \quad 2.6 \\ 13 \quad 19 \quad 22 \quad 23 \quad 33 \end{array}$$

$$\begin{array}{r} 0.8 \quad 0.2 \quad 0.5 \quad 0.6 \quad 2.5 \quad 0.7 \quad 0.1 \\ 40 \quad 33 \quad 32 \quad 31 \quad 19-24 \quad 13 \quad 0.5 \end{array} \quad \begin{array}{r} 0.8 \quad 2.3 \quad 1.3 \quad 1.8 \\ 13 \quad 18-21 \quad 23 \quad 33 \end{array}$$

Top Lt Blue top Sta 82+00

$$\begin{array}{r} 2.6 \quad 1.9 \quad 2.5 \quad 2.8 \quad 4.2 \quad 2.6 \\ 40 \quad 32 \quad 32 \quad 30 \quad 24-19 \quad 13 \end{array} \quad \begin{array}{r} 2.6 \quad 4.2 \quad 4.0 \quad 1.5 \quad 1.4 \\ 13 \quad 18 \quad 22 \quad 26 \quad 33 \end{array}$$

$$\begin{array}{r} 2.6 \quad 2.0 \quad 2.4 \quad 2.5 \quad 4.1 \quad 2.6 \\ 40 \quad 33 \quad 32 \quad 30 \quad 24-19 \quad 13 \end{array} \quad \begin{array}{r} 2.7 \quad 2.8 \quad 4.3 \quad 4.4 \quad 1.2 \quad 1.6 \\ 13 \quad 13 \quad 17 \quad 21 \quad 26 \quad 33 \end{array}$$

Sta	+	π	-	Elev
		885.55		
83+50				82.9
84				82.8
+50				82.5
B.M.		0.95	884.60	884.51
85				82.2
+50				81.7
86				81.4
+50				80.9
87				80.9
+50				80.7
88	6.15	886.82	4.88	880.67
+50				80.9
				80.9
89				81.1
+50				81.3

7-10
60 88553
84.57

3.1 2.5 2.9 4.5 4.4 2.7 2.1 2.6 4.1 4.0 1.2 1.0
40 33 31 27 19 13 2.7 13 18 22 26 33

4.0 3.5 4.7 4.5 2.9 2.9 2.6 4.3 4.0 2.0 1.9
40 33 26 20 13 2.8 13 18 22 25 31

5.3 4.7 4.5 3.0 3.1 3.0 4.6 2.0 1.4
40 30 19 13 3.1 13 18-22 27 33

Spk in 20" Pop Rt. Sta 84+75

5.8 4.8 5.0 4.9 3.5 2.7 3.6 5.0 4.8 2.5 2.1
33 27 25 19 13 3.4 13 18 22 26 33

6.0 5.3 5.5 5.4 3.9 4.1 3.9 5.4 5.2 2.6 2.8
40 31 28 19 13 3.9 13 18 21 26 33

6.8 6.1 6.4 6.1 4.3 5.0 4.3 6.2 5.8
40 32 30 19 13 4.2 13 18-23 25-33

8.7 8.3 7.6 4.7 6.5 4.7 4.7 8.4 8.7
33 28 24 13 4.7 13 28 40

7.8 7.5 4.8 6.9 4.8 8.0 8.5 9.0
33 28 23 13 4.7 13 25 29 40

6.0 6.2 6.6 4.9 6.4 5.0 7.3 7.8 8.0
40 30 26 21 13 4.7 13 23 29 40

Lt Blue Top 87+50 7.0

6.7 8.0 7.9 6.3 5.9 6.4 8.0 8.5 8.8
40-33 26 20 13 5.9 13 21 27 40
6.2 5.1 6.0 7.8 6.2 5.9 6.3 7.5 7.9 8.4
40 34 31 25 20 13 5.9 13 20 24-30 40

5.2 4.8 5.3 7.7 7.6 6.0 5.7 6.0 7.5 7.1
45 38 34 26 21 13 5.7 13 20-28 32-40

4.7 4.5 4.8 7.2 5.8 4.4 5.7 7.3 6.5
40 37 33 25-20 13 5.5 13 20-27 31-40

Sta	+	π	-	Elev
		886.82		81.6
90				81.6
	+50			81.7
91				81.9
	+50			82.0
92				82.3
	+50			82.2
93				82.3
	+50			82.0
94				81.7
	+50			81.7
95				81.6
①	7.59	889.25	5.16	881.66
	+50			81.9
	+70			82.1
	+86			82.3

$$40-37 \frac{4.0}{37} \frac{4.4}{33} \frac{6.8}{25} \frac{6.9}{19} \frac{5.5}{13} \overset{4.5}{5.2} \frac{5.6}{13} \frac{7.0}{21} \frac{7.0}{27} \frac{6.5}{31-40}$$

$$\frac{3.8}{40} \frac{4.1}{31} \frac{4.5}{33} \frac{6.7}{25} \frac{6.8}{19} \frac{5.4}{13} \overset{5.3}{5.1} \frac{5.3}{13} \frac{6.7}{20} \frac{6.8}{27} \frac{6.3}{31-40}$$

$$\frac{5.5}{38} \frac{5.5}{33} \frac{6.7}{26} \frac{6.6}{20} \frac{5.2}{13} \overset{5.1}{4.9} \frac{5.2}{13} \frac{6.9}{21} \frac{7.1}{28} \frac{6.9}{32} \frac{6.8}{40}$$

$$\frac{5.1}{40} \frac{5.3}{34} \frac{5.6}{31} \frac{6.5}{26} \frac{6.6}{20} \frac{5.0}{13} \overset{5.5}{4.8} \frac{5.0}{13} \frac{6.4}{21} \frac{6.6}{25} \frac{6.4}{31} \frac{6.1}{40}$$

$$40-36 \frac{4.7}{36} \frac{4.9}{31} \frac{6.5}{25} \frac{6.4}{20} \frac{4.9}{13} \overset{4.6}{4.5} \frac{4.9}{13} \frac{6.3}{21} \frac{6.4}{28} \frac{6.0}{31} \frac{5.7}{40}$$

$$40-34 \frac{4.6}{34} \frac{4.9}{30} \frac{6.4}{24} \frac{4.9}{20} \frac{4.9}{13} \overset{5.3}{4.6} \frac{4.9}{13} \frac{6.2}{21} \frac{6.3}{25-37}$$

$$40-35 \frac{5.4}{35} \frac{5.6}{31} \frac{6.5}{27-20} \frac{5.0}{13} \overset{6.0}{4.5} \frac{5.0}{13} \frac{6.7}{20} \frac{7.2}{24} \frac{7.3}{33}$$

$$40-31 \frac{6.0}{31} \frac{6.7}{27-20} \frac{5.1}{13} \overset{6.3}{4.8} \frac{5.1}{13} \frac{7.1}{20} \frac{7.5}{24}$$

$$40-31 \frac{6.0}{31} \frac{6.8}{26} \frac{6.7}{19} \frac{5.2}{13} \overset{6.3}{5.1} \frac{5.2}{13} \frac{7.2}{19} \frac{7.5}{23} \frac{8.0}{33}$$

$$\frac{5.8}{40} \frac{5.9}{31} \frac{6.6}{26-20} \frac{5.1}{13} \overset{6.0}{5.1} \frac{5.2}{13} \frac{7.0}{19} \frac{7.3}{23} \frac{7.7}{33}$$

$$\frac{5.1}{40} \frac{5.0}{31} \frac{6.5}{25-20} \frac{5.2}{13} \overset{5.9}{5.2} \frac{5.2}{13} \frac{6.7}{18} \frac{7.1}{22} \frac{7.3}{33}$$

FL242M
12.03

$$\begin{array}{r} 7.6 \\ 31 \\ 12.0 \\ 33-27 \\ 7.5 \\ 40 \end{array} \begin{array}{r} 1 \\ 26 \\ 9.0 \\ 27 \\ 7.7 \\ 33 \end{array} \begin{array}{r} 8.7 \\ 20 \\ 8.5 \\ 18 \\ 8.8 \\ 20 \end{array} \begin{array}{r} 7.4 \\ 13 \\ 7.3 \\ 13 \\ 7.2 \\ 13 \end{array} \begin{array}{r} 7.4 \\ 13 \\ 7.2 \\ 13 \\ 7.0 \end{array} \begin{array}{r} 9.0 \\ 20 \\ 8.5 \\ 19 \\ 8.4 \\ 20 \end{array} \begin{array}{r} 9.4 \\ 23 \\ 8.8 \\ 23-33 \\ 8.6 \\ 22 \end{array} \begin{array}{r} 9.6 \\ 33 \\ 8.8 \\ 33 \\ 8.5 \\ 33 \end{array}$$

FL242M
12.09

Sta	+	-	Elev
		889.25	
96			82.3
	+50		82.8
97			83.2
	+50		84.0
98			84.5
	+47		84.8
	+52		85.0
	+58		85.0
	+65	Shoulder	85.2
	+79.05	Hodgson Rd	85.3
BM.		477	884.48

477

4.3
 $\frac{7.5}{40} \frac{7.8}{31} \frac{8.5}{27} \frac{8.6}{20} \frac{7.1}{13} \frac{7.0}{13} \frac{7.2}{13} \frac{8.5}{21} \frac{12.0}{27-30}$

1.5
 $\frac{6.2}{40} \frac{6.3}{31} \frac{7.6}{26} \frac{8.2}{22} \frac{8.0}{19} \frac{6.6}{13} \frac{6.5}{13} \frac{6.6}{13} \frac{7.7}{19} \frac{8.0}{23-31} \frac{8.3}{40}$

6.9
 $\frac{4.6}{40} \frac{4.9}{34} \frac{7.5}{25} \frac{7.6}{22} \frac{7.3}{18} \frac{6.1}{13} \frac{6.1}{13} \frac{7.3}{18} \frac{7.7}{22} \frac{7.3}{25} \frac{6.1}{31-40}$

5.9
 $\frac{3.2}{40} \frac{3.6}{36} \frac{6.5}{26} \frac{6.9}{23} \frac{6.6}{19} \frac{5.6}{13} \frac{5.3}{13} \frac{5.6}{13} \frac{6.8}{18} \frac{7.0}{21} \frac{6.8}{25} \frac{5.7}{31-40}$

5.2
 $\frac{2.3}{45} \frac{2.5}{38} \frac{5.8}{24} \frac{6.2}{21} \frac{5.9}{18} \frac{4.9}{13} \frac{4.8}{13} \frac{4.9}{13} \frac{6.1}{19} \frac{6.4}{22} \frac{6.1}{25} \frac{4.9}{31-40}$

4.9
 $\frac{2.1}{45} \frac{2.3}{37} \frac{5.3}{26} \frac{5.8}{22} \frac{5.6}{19} \frac{4.4}{13} \frac{4.5}{13} \frac{4.5}{13} \frac{5.5}{18} \frac{5.9}{22} \frac{5.5}{25} \frac{3.7}{33} \frac{3.4}{40}$

4.7
 $\frac{4.9}{46} \frac{4.4}{36} \frac{5.5}{21} \frac{5.4}{22} \frac{4.5}{15} \frac{4.3}{16} \frac{4.6}{16} \frac{5.5}{21-28} \frac{5.4}{40}$

4.5
 $\frac{5.8}{50} \frac{5.5}{30} \frac{4.6}{22} \frac{4.3}{15} \frac{4.5}{15} \frac{4.6}{26} \frac{5.6}{35} \frac{6.2}{50}$

$\frac{4.8}{50} \frac{4.4}{27} \frac{4.1}{22} \frac{4.5}{22} \frac{4.8}{50}$

$\frac{4.3}{50} 4.0 \frac{4.3}{50}$

SprK. in TP. SE Cor Hodgson & No Co. Line

64+41 Field Ent Rt

72+40 Field Ent Rt

72+95 $\pm$ Culvert Inp

83+97 Farm Ent Rt

84+85 Farm Ent Rt

95+87 $\pm$ Culvert Inp

12" X 20' C.M. - 23' Rt. Ent = 18' X 12' X 1.5 Deep

24' long X 15 Top - 1' Deep - No Culvert

24" X 56' C.M. Culv.

15" X 20' C.M. - 19' Rt.

Ent = 18' X 6' X 2' Deep

15" X 20' C.M. 19' Rt.

Ent = 18' X 6' X 2' Deep

24" X 60' C.M. Culv.

