

Book-9-C, Bk 11-A

Dr 11A-BK 9C

18E
FIELD BOOK
360A

35-M20

35-M20

KEUFFEL & ESSER CO.

DRAWING MATERIALS AND SURVEYING INSTRUMENTS. NEW YORK.

CHICAGO. ST. LOUIS. SAN FRANCISCO. MONTREAL.

TABLES FOR EXCAVATIONS AND EMBANKMENTS.

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.

ROADWAY 18 FEET WIDE. SIDE SLOPES 1 TO 1.

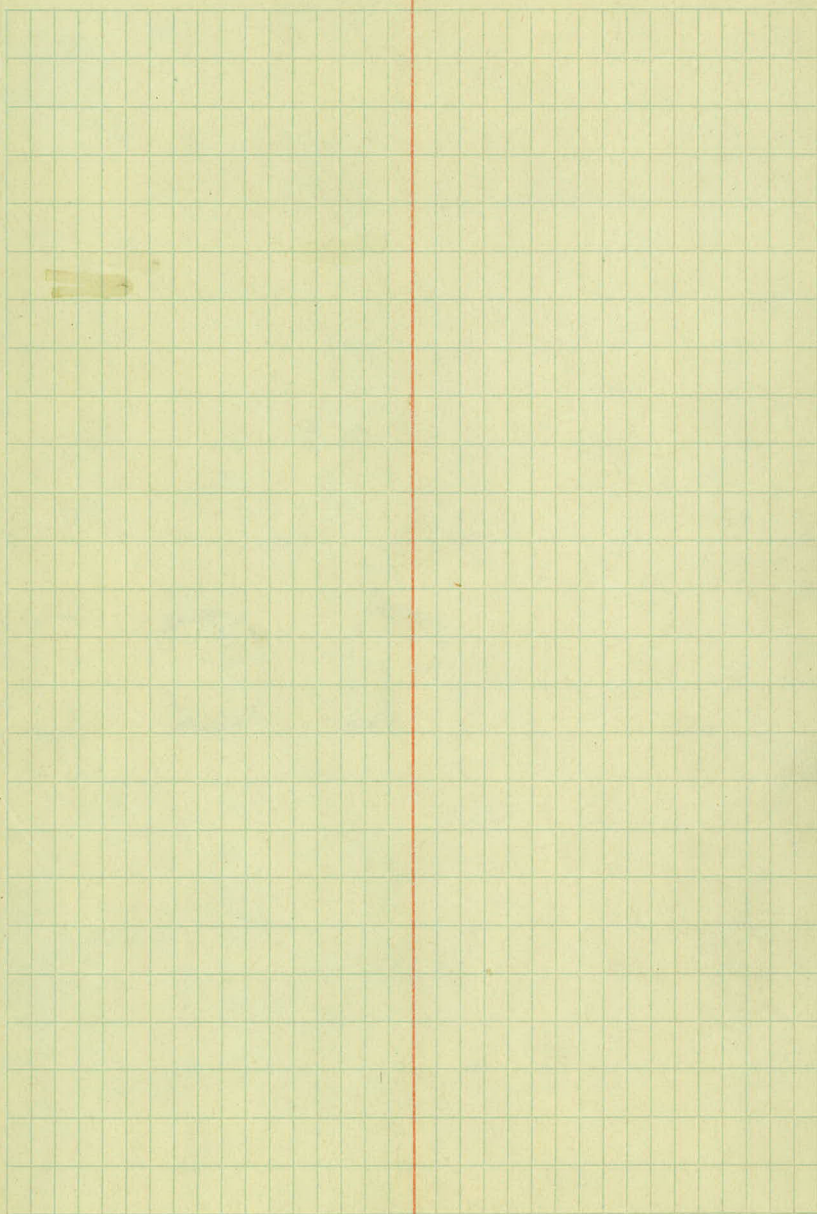
FOR SINGLE TRACK EXCAVATION.

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	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	0
1	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	1
2	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	2
3	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	3
4	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	4
5	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	5
6	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	6
7	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	7
8	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	8
9	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	9
10	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	10
11	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	11
12	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	12
13	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	13
14	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	14
15	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	15
16	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	16
17	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	17
18	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	18
19	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	19
20	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	20
21	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	21
22	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	22
23	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	23
24	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	24
25	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	25
26	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	26
27	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	27
28	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	28
29	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	29
30	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	30
31	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	31
32	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	32
33	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	33
34	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	34
35	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	35
36	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	36

Calculated by Julien A. Hall, M. Am. Soc. C. E.

For Kelth's Railroad Curve Tables see end of book.



Sta	+	π	- Elev	Ground	Grade	Dt. Grade
B.M.	5.73	884.88				
①	7.16	891.88	0.16 - 884.72			
62						
+50					85.5	
63				86.3	84.5	83.0
+50	C-32		C-31	86.1	84.9	83.4
64	C-31		C-29	85.1	84.2	82.7
+50	C-31		C-31.5	84.8	83.2	81.7
65				82.8	82.0	80.5
+50				80.4	80.4	78.9

Gr.
Road

SpK in 20" Oak 120' Lt Sta 55+64 Elev. 879.15

To be Revised

Page 23

$$\frac{4.5}{33} \quad \frac{C4.5}{4.4} \quad \frac{4.1}{15} \quad \frac{4.8}{8} \quad \frac{C2.7}{4.7} \quad \frac{4.7}{7} \quad \frac{5.2}{17} \quad \frac{C3.4}{5.5} \quad \frac{5.6}{33}$$

7.4
8.9

$$\frac{6.2}{40} \quad \frac{C2.3}{6.2} \quad \frac{6.3}{25} \quad \frac{5.3}{13} \quad \frac{C1.1}{5.9} \quad \frac{6.5}{9} \quad \frac{DC1.4}{7.1} \quad \frac{7.0}{33}$$

7.0
8.5

$$\frac{7.3}{40} \quad \frac{DC0.7}{8.5} \quad \frac{6.7}{7} \quad \frac{C1.1}{6.6} \quad \frac{7.3}{13} \quad \frac{C1.6}{7.6} \quad \frac{7.6}{29.4}$$

7.7
9.2

$$\frac{10.0}{40} \quad \frac{DC0.6}{9.6} \quad \frac{9.1}{24} \quad \frac{6.5}{7} \quad \frac{C1.3}{7.4} \quad \frac{8.0}{8} \quad \frac{C2.1}{8.1} \quad \frac{8.1}{40}$$

8.7
10.2

$$\frac{10.7}{40} \quad \frac{DC0.9}{11.5} \quad \frac{9.1}{8} \quad \frac{8.4}{7} \quad \frac{9.1}{3} \quad \frac{9.3}{0} \quad \frac{C0.6}{10.1} \quad \frac{DC1.0}{10.4} \quad \frac{10.6}{40}$$

9.9
11.4

$$\frac{11.9}{40} \quad \frac{DC1.3}{11.7} \quad \frac{11.6}{13} \quad \frac{10.7}{7} \quad \frac{F0.1}{11.6} \quad \frac{12.1}{19} \quad \frac{DC0.7}{12.3} \quad \frac{12.6}{40}$$

11.5
13.0

Sta	+	Σ	-	Ground	Grade	Dt. Grade
0	3.00	882.33	12.55	879.33		
66				79.0	78.7	77.2
+50				77.5	77.0	75.5
67				75.5	75.3	73.8
+50				73.0	73.6	72.1
68				72.1	73.0	71.5
0	3.10	874.04	11.39	870.94		
68				70.9	72.0	70.5
+20				70.2	71.4	69.9

x = Stake not set

DG.

Red

Gr
Red

all 31.0' except Sta. 67 which is 32'

$$\begin{array}{r} \text{X} \\ 63.2 \\ 1.7 \quad \frac{1.9}{4} \quad \frac{2.0}{12} \quad \frac{2.7}{5} \quad \frac{3.4}{4} \quad \text{C.O.1} \quad \frac{3.9}{27} \quad \text{D.C.} \quad \frac{4.2}{40} \\ \hline 35.8 \quad \hline 0 \quad \hline 31 \end{array}$$

3.6
5.1

$$\begin{array}{r} \text{X} \\ 6.50 \\ 1.5 \quad \frac{1.8}{50} \quad \frac{2.0}{35} \quad \frac{1.1}{12} \quad \frac{3.7}{8} \quad \frac{4.9}{4} \quad \text{C.O.3} \quad \frac{5.0}{0} \quad \frac{4.3}{16} \quad \text{C.19} \quad \frac{5.0}{40} \\ \hline 43.0 \quad \hline 0 \quad \hline 31 \end{array}$$

5.3
6.8

$$\begin{array}{r} \text{X} \\ 66.2 \\ 2.2 \quad \frac{2.3}{50} \quad \frac{3.3}{29} \quad \frac{3.5}{12} \quad \frac{7.1}{3} \quad \text{F.O.3} \quad \frac{7.2}{7} \quad \frac{7.2}{19} \quad \text{D.C.O.9} \quad \frac{7.6}{40} \\ \hline 47.8 \quad \hline 0 \quad \hline 31 \end{array}$$

7.0
8.5

$$\begin{array}{r} \text{X} \\ 64.0 \\ 5.5 \quad \frac{6.2}{50} \quad \frac{6.8}{21} \quad \frac{6.6}{11} \quad \frac{9.1}{4} \quad \text{F.1.1} \quad \frac{10.3}{18} \quad \text{F.1.6} \quad \frac{10.7}{33} \\ \hline 39.0 \quad \hline 0 \quad \hline 31 \end{array}$$

8.7
10.2

$$\begin{array}{r} 6.5 \quad 7.7 \quad 8.1 \quad 8.2 \quad 9.8 \quad 10.5 \quad 10.4 \quad 11.6 \\ \hline 50 \quad 30 \quad 16 \quad 9 \quad 4 \quad 0 \quad 11 \quad 40 \end{array}$$

9.3

$$\begin{array}{r} \text{X} \\ 62.9 \\ 0.3 \quad \frac{0.6}{40} \quad \frac{1.6}{19} \quad \frac{1.6}{9} \quad \frac{3.2}{4} \quad \text{F.1.6} \quad \frac{3.2}{7} \quad \frac{4.8}{16} \quad \text{F.4.1} \quad \frac{6.9}{40} \\ \hline 34.6 \quad \hline 0 \quad \hline 31 \end{array}$$

2.0
3.5

$$\begin{array}{r} 1.5 \quad 2.7 \quad 4.3 \quad 4.0 \quad 4.0 \quad 5.4 \quad 7.1 \quad 6.9 \\ \hline 40 \quad 17 \quad 5 \quad 4 \quad 6 \quad 12 \quad 25 \quad 40 \end{array}$$

Sta	+	Σ 874.04	-	Ground	Grade	Dt. Grade
68+50				69.1	70.6	69.1
69				68.3	69.6	68.1
+50				67.7	68.8	67.3
70				66.9	68.4	66.9
+50				67.3	68.2	66.7
	487	871.65 4.39		67.4	68.3	66.8
71				67.4	68.3	66.8
+50				67.3	68.3	66.8
B.M.	487	871.65		866.78		
72				66.9	68.5	67.0

$\frac{4.1}{36}$	DC 0.5	$\frac{4.7}{22}$	$\frac{4.1}{14}$	$\frac{6.1}{6}$	$\frac{5.3}{4}$	$\frac{5.3}{7}$	$\frac{6.8}{13}$	$\frac{7.5}{17}$	$\frac{6.8}{19}$	$\frac{F3.4}{26.6}$	$\frac{6.8}{40}$	Gr.B
	$\frac{4.4}{31.0}$											3.4
												4.9

BM Ctr Mon EI 866.78

$\frac{4.8}{40}$	$\frac{D.C.0.1}{4.8}$	$\frac{4.7}{20}$	$\frac{4.6}{13}$	$\frac{4.5}{8}$	$\frac{4.7}{17}$	$\frac{6.0}{18}$	$\frac{4.8}{20}$	$\frac{D.C.0.3}{4.6}$	$\frac{4.6}{31.0}$	$\frac{4.6}{40}$	3.4
	$\frac{31.0}{4.8}$										4.9

$\frac{5.2}{40}$	$\frac{F1.8}{5.2}$	$\frac{5.0}{7}$	$\frac{F1.2}{4.6}$	$\frac{4.9}{9}$	$\frac{4.9}{17}$	$\frac{6.0}{18}$	$\frac{4.8}{21}$	$\frac{D.C.0.1}{4.8}$	$\frac{4.8}{31.0}$	$\frac{4.8}{40}$	3.4
	$\frac{20.2}{5.2}$		$\frac{0}{4.6}$								4.9

Ctr. Mon Sta 72+38

$\frac{5.2}{40}$	$\frac{F2.0}{5.2}$	$\frac{5.2}{7}$	$\frac{F1.6}{4.6}$	$\frac{5.2}{15}$	$\frac{6.8}{21}$	$\frac{6.8}{25}$	$\frac{F3.0}{6.2}$	$\frac{5.2}{25.0}$	$\frac{5.2}{28.4}$	3.2
	$\frac{21.0}{5.2}$		$\frac{0}{4.6}$							4.1

Sta	+	π	-	Ground	Grade	Dt. Grade
		871.65				
+250				67.1	68.7	
+60					68.7	
+80					68.9	
+85					69.0	
+95					69.1	
73				66.6	69.1	
+50				66.9	69.7	

Gr.
Rod.

$\frac{5.2}{40}$	$\frac{F2.2}{5.2}$ $\frac{21.8}{5}$	$\frac{4.6}{5}$	$\frac{F1.8}{4.8}$ $\frac{0}{5}$	$\frac{4.6}{5}$	$\frac{5.1}{9}$	$\frac{F1.9}{4.9}$ $\frac{20.6}{40}$	$\frac{5.0}{40}$	$\frac{3.0}{45}$
------------------	--	-----------------	-------------------------------------	-----------------	-----------------	---	------------------	------------------

3.0
45

$\frac{5.2}{40}$	$\frac{F2.7}{5.3}$ $\frac{23.8}{10}$	$\frac{5.3}{10}$	$\frac{4.9}{6}$	$\frac{5.2}{5}$	$\frac{F2.5}{5.1}$ $\frac{0}{5}$	$\frac{5.4}{5}$	$\frac{9.4}{9}$	$\frac{9.4}{29}$	$\frac{F4.9}{7.5}$ $\frac{32.6}{40}$	$\frac{5.9}{40}$	$\frac{2.6}{35}$
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$\frac{F2.7}{4.7}$ $\frac{23.8}{8}$	$\frac{4.7}{8}$	$\frac{4.9}{7}$	$\frac{F2.8}{4.8}$ $\frac{0}{9}$	$\frac{4.8}{9}$	$\frac{F3.2}{5.2}$ $\frac{25.8}{33}$	$\frac{5.1}{33}$	$\frac{2.0}{35}$
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Sta	+	π	-	Ground	Grade	Dt. Grade
BM	9.22	876.0		866.78		
74				68.0	70.3	
+50				69.8	71.0	
75				71.6	71.9	
+40				72.0		
+50				72.1	72.7	
76				71.3	73.6	
+50				71.7	74.4	

$$\begin{array}{r} 866.78 \\ 922 \\ \hline 876.00 \end{array}$$

6

Gr. Rod

Chr Mon Sta 72+38

$$\frac{8.8}{40}$$

$$\frac{F2.3}{8.0} \frac{7.4}{13}$$

$$\frac{7.4}{9}$$

$$\frac{7.8}{8}$$

$$\frac{7.7}{2}$$

$$\frac{F2.3}{8.0}$$

$$\frac{7.6}{6}$$

$$\frac{F2.0}{7.7}$$

$$\frac{8.0}{40}$$

$$\frac{5.7}{72}$$

$$\frac{8.4}{40}$$

$$\frac{F2.4}{7.4} \frac{6.4}{8}$$

$$\frac{6.9}{3}$$

$$\frac{6.6}{1}$$

$$\frac{F1.2}{6.2}$$

$$\frac{5.8}{4}$$

$$\frac{6.4}{7}$$

$$\frac{5.5}{18}$$

$$\frac{DC.0.9}{5.6}$$

$$\frac{5.7}{40}$$

$$\frac{5.0}{65}$$

$$\frac{6.2}{40}$$

$$\frac{DC.0.0}{5.6} \frac{4.1}{16-8}$$

$$\frac{5.1}{6-1}$$

$$\frac{F0.3}{4.4}$$

$$\frac{3.6}{4}$$

$$\frac{4.3}{9}$$

$$\frac{DC.1.3}{4.3}$$

$$\frac{4.3}{40}$$

$$\frac{4.1}{5.6}$$

$$\frac{5.7}{42}$$

$$\frac{3.0}{8}$$

$$\frac{3.7}{5}$$

$$4.0$$

$$\frac{3.3}{2}$$

$$\frac{4.0}{7}$$

$$\frac{4.0}{52}$$

$$4.0$$

$$\frac{5.4}{40}$$

$$\frac{DC.0.4}{4.4} \frac{3.1}{8}$$

$$\frac{3.8}{5}$$

$$\frac{4.1}{40}$$

$$\frac{F0.6}{3.9}$$

$$\frac{3.4}{3}$$

$$\frac{4.0}{9}$$

$$\frac{DC.1.0}{3.8}$$

$$\frac{4.1}{40}$$

$$\frac{3.3}{48}$$

$$\frac{5.7}{40}$$

$$\frac{F3.4}{5.8} \frac{5.8}{12}$$

$$\frac{4.6}{5}$$

$$\frac{F2.3}{4.7}$$

$$\frac{4.7}{4}$$

$$\frac{F2.5}{4.9}$$

$$\frac{4.5}{40}$$

$$\frac{2.4}{39}$$

$$\frac{5.5}{40}$$

$$\frac{F3.9}{5.5} \frac{5.5}{11}$$

$$\frac{4.2}{8}$$

$$\frac{3.9}{3}$$

$$\frac{F2.7}{4.3}$$

$$\frac{4.3}{3}$$

$$\frac{4.7}{6}$$

$$\frac{F2.9}{4.5}$$

$$\frac{4.3}{40}$$

$$1.5$$

Sta	+	π	-	Ground	Grade	Dt. Grad
-----	---	-------	---	--------	-------	----------

		876.00 883.482				
76+76				65.2	74.7	
0	8.92	883.48	1.44	74.56		

77				74.1	75.3	
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+50				76.0	76.1	
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78 ✓				77.8	77.0	23 148 575
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+50				77.3	77.8	
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79				78.7	78.7	
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+50				78.7	79.5	
-----	--	--	--	------	------	--

Gr Rod

$$\frac{11.3}{40} \quad \frac{11.2}{17} \quad \frac{10.4}{11} \quad 10.8 \quad \frac{10.3}{2} \quad \frac{10.4}{9} \quad \frac{10.4}{23} \quad \frac{10.3}{40}$$

$$\frac{8.4}{40} \quad \text{DC. 1.4} \quad \frac{8.4}{23} \quad \frac{7.8}{16} \quad \frac{8.5}{10} \quad \frac{9.5}{8} \quad \text{F. 1.2} \quad \frac{8.9}{2} \quad \frac{8.7}{7} \quad \frac{9.0}{20} \quad \text{DC. 0.9} \quad \frac{8.8}{40} \quad \frac{8.2}{9.7}$$

$$\frac{6.3}{40} \quad \text{DC. 2.6} \quad \frac{6.3}{33.4} \quad \frac{6.1}{22} \quad \frac{6.1}{11} \quad \frac{7.1}{6-3} \quad \text{F. 0.1} \quad \frac{7.5}{6} \quad \frac{6.5}{3} \quad \frac{7.0}{7} \quad \frac{6.7}{23} \quad \text{DC. 2.4} \quad \frac{6.5}{32.6} \quad \frac{6.5}{40} \quad \frac{7.4}{8.9}$$

$$\frac{4.3}{50} \quad \text{DC. 3.7} \quad \frac{4.3}{37.8} \quad \frac{4.0}{23} \quad \frac{3.8}{12} \quad \frac{5.5}{7} \quad \frac{6.08}{5.7} \quad \frac{4.8}{3} \quad \frac{5.7}{8} \quad \frac{5.7}{23} \quad \text{DC. 2.3} \quad \frac{5.7}{32.2} \quad \frac{5.9}{40} \quad \frac{6.5}{8.0}$$

$$\frac{4.6}{40} \quad \text{DC. 2.6} \quad \frac{4.6}{33.4} \quad \frac{4.3}{21} \quad \frac{3.9}{12} \quad \frac{4.7}{8} \quad \frac{4.8}{2} \quad \frac{4.2}{6} \quad \frac{4.2}{3} \quad \frac{5.3}{7} \quad \frac{5.7}{23} \quad \text{DC. 1.3} \quad \frac{5.9}{31.0} \quad \frac{6.2}{40} \quad \frac{5.7}{7.2}$$

$$\frac{5.3}{40} \quad \text{DC. 1.3} \quad \frac{5.3}{31.0} \quad \frac{5.0}{22} \quad \frac{4.0}{12} \quad \frac{5.0}{8} \quad \frac{5.2}{2} \quad \frac{0.8}{4.8} \quad \frac{6.2}{9} \quad \frac{6.6}{23} \quad \text{F. 1.7} \quad \frac{6.5}{19.8} \quad \frac{6.8}{40} \quad \frac{4.8}{6.3}$$

$$\frac{6.2}{40} \quad \frac{6.1}{32} \quad \text{DC. 0.6} \quad \frac{5.5}{17} \quad \frac{4.8}{14} \quad \frac{4.7}{10} \quad \frac{5.0}{9} \quad \text{F. 0.8} \quad \frac{5.5}{5} \quad \frac{5.9}{11} \quad \text{F. 2.0} \quad \frac{6.0}{21.0} \quad \frac{6.2}{40} \quad \frac{4.0}{5.5}$$

Sta	+	Δ	-	Ground	Grade	Dt Grade
BM	2.95	887.52		884.57		
80				79.8	80.4	
+50				80.7	81.0	
81				82.0	81.8	
+50				82.7	82.3	
82				83.5	82.7	
+50				84.3	82.9	
83				84.3	83.0	

884.52
2.95
887.52

8

5/14/35

Perfell
Stoughton
Bath
Galloway

SpK in 20 Pop Rt. Sta 84 175

112	101	9.1	$\frac{F1.5}{8.6}$	8.5	8.5	8.1	$\frac{F0.8}{7.9}$	8.5	9.3	$\frac{F2.7}{9.8}$	$\frac{10.3}{40}$	7.1
45	36	28	$\frac{19.0}{19.0}$	12	7	4	$\frac{1.9}{0}$	5	12	$\frac{23.8}{23.8}$	40	8.6

8.7	$\frac{0026.}{8.0}$	6.7	7.2	6.7	$\frac{F0.3}{6.8}$	8.0	8.6	$\frac{F2.7}{9.2}$	9.6	6.5
40	$\frac{29.7}{29.7}$	11	7	4	$\frac{0}{0}$	4	12	$\frac{23.8}{23.8}$	40	8.0

7.0	$\frac{C.07}{6.5}$	5.2	6.0	5.8	5.4	$\frac{C.01}{5.6}$	6.8	7.5	$\frac{F2.2}{7.9}$	8.4	5.7
40	$\frac{31.0}{31.0}$	16-11	11	8	4	$\frac{0}{0}$	5	15	$\frac{21.8}{21.8}$	40	7.2

5.2	$\frac{DC.17}{5.0}$	4.4	3.8	5.1	5.1	4.7	$\frac{C.03}{4.9}$	6.1	$\frac{DC.02}{6.5}$	7.0	5.2
40	$\frac{31.0}{31.0}$	20	15	9	7	3	$\frac{0}{0}$	6	$\frac{22.3}{22.3}$	40	6.7

4.7	$\frac{DC.17}{4.6}$	4.4	3.6	3.8	4.4	4.3	4.1	$\frac{C.0.6}{4.2}$	4.7	5.5	$\frac{DL.07}{5.6}$	6.0	4.8
40	$\frac{31.0}{31.0}$	24	16	11	10	7	3	$\frac{0}{0}$	3	15	$\frac{22.5}{22.5}$	40	6.3

4.5	$\frac{DC.10}{4.1}$	3.8	2.8	2.9	3.6	3.1	$\frac{C1.3}{3.3}$	3.5	$\frac{DC.1}{2.6}$	3.9	4.6
40	$\frac{31.0}{31.0}$	22	17	12	7-11	3	$\frac{0}{0}$	16	$\frac{3.5}{3.5}$	40	6.1

4.5	$\frac{C1.8}{4.2}$	3.6	3.6	3.2	$\frac{C1.2}{3.3}$	3.0	$\frac{DC.1}{3.0}$	3.6	4.5
40	$\frac{31.0}{31.0}$	19	9	4	$\frac{0}{0}$	17	$\frac{3.0}{3.0}$	40	6.0

Sta	+	Σ	-	Ground	Grade
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887.52

Σ
886.31

83+50

82.6

83.6

83.0

84

82.1

82.9

82.8

3.5

+50

82.1

82.1

82.5

3.8

B.M. 2.02

886.59

85

81.9

81.9

82.1

4.2

+50

81.5

81.5

81.6

4.7

86

80.6

80.6

81.3

5.0

+50

79.1

79.1

81.0

5.3

GrR

$$\begin{array}{r} 5.0 \\ \hline 40 \end{array} \quad \begin{array}{r} C.12 \\ 4.8 \\ \hline 31.0 \end{array} \quad \begin{array}{r} 4.7 \\ 27 \end{array} \quad \begin{array}{r} 4.2 \\ 14 \end{array} \quad \begin{array}{r} 4.4 \\ 9 \end{array} \quad \begin{array}{r} 4.0 \\ 5 \end{array} \quad \begin{array}{r} C.05 \\ 4.6 \\ \hline 0 \end{array} \quad \begin{array}{r} 3.6 \\ 8 \end{array} \quad \begin{array}{r} 3.2 \\ 22 \end{array} \quad \begin{array}{r} C.2.9 \\ 3.1 \\ \hline 25.9 \end{array} \quad \begin{array}{r} 3.2 \\ 40 \end{array} \quad \begin{array}{r} 4.5 \\ 60 \end{array}$$

$$\begin{array}{r} 6.1 \\ 40 \end{array} \quad \begin{array}{r} C.0.7 \\ 5.5 \\ \hline 31.0 \end{array} \quad \begin{array}{r} 4.8 \\ 20 \end{array} \quad \begin{array}{r} 5.0 \\ 10 \end{array} \quad \begin{array}{r} C.0 \\ 4.7 \\ \hline 0 \end{array} \quad \begin{array}{r} 4.0 \\ 17 \end{array} \quad \begin{array}{r} C.1.4 \\ 2.4 \\ 3.8 \\ \hline 25.1 \end{array} \quad \begin{array}{r} 3.2 \\ 40 \end{array} \quad \begin{array}{r} 4.7 \\ 62 \end{array}$$

$$\begin{array}{r} 7.2 \\ 40 \end{array} \quad \begin{array}{r} C.0.0 \\ 6.5 \\ \hline 30.6 \end{array} \quad \begin{array}{r} 6.0 \\ 21 \end{array} \quad \begin{array}{r} 5.2 \\ 15 \end{array} \quad \begin{array}{r} 5.7 \\ 7 \end{array} \quad \begin{array}{r} F.0.5 \\ 5.5 \\ \hline 0 \end{array} \quad \begin{array}{r} 5.0 \\ 13 \end{array} \quad \begin{array}{r} C.2.7 \\ 3.8 \\ \hline 25.1 \end{array} \quad \begin{array}{r} 3.5 \\ 40 \end{array} \quad \begin{array}{r} 5.0 \\ 6.5 \end{array}$$

SpK in 20" Pop Rt. Sta 84+75 Elev. 884.57

5/14/35 A

$$\begin{array}{r} 7.2 \\ 40 \end{array} \quad \begin{array}{r} 6.6 \\ 31 \end{array} \quad \begin{array}{r} C.0.0 \\ 6.0 \\ \hline 26 \end{array} \quad \begin{array}{r} 6.0 \\ 23 \end{array} \quad \begin{array}{r} 5.1 \\ 17 \end{array} \quad \begin{array}{r} F.0.4 \\ 4.9 \\ \hline 0 \end{array} \quad \begin{array}{r} 4.0 \\ 12 \end{array} \quad \begin{array}{r} C.2.4 \\ 3.6 \\ \hline 25.1 \end{array} \quad \begin{array}{r} 3.6 \\ 40 \end{array} \quad \begin{array}{r} 4.5 \\ 60 \end{array}$$

$$\begin{array}{r} 7.1 \\ 40 \end{array} \quad \begin{array}{r} C.1.1 \\ 6.4 \\ \hline 31 \end{array} \quad \begin{array}{r} 4.6 \\ 15 \end{array} \quad \begin{array}{r} 5.2 \\ 13 \end{array} \quad \begin{array}{r} 4.7 \\ 9 \end{array} \quad \begin{array}{r} 5.2 \\ 6 \end{array} \quad \begin{array}{r} F.0.3 \\ 5.3 \\ \hline 0 \end{array} \quad \begin{array}{r} 4.6 \\ 3 \end{array} \quad \begin{array}{r} 5.1 \\ 13 \end{array} \quad \begin{array}{r} C.2.5 \\ 4.0 \\ \hline 25.3 \end{array} \quad \begin{array}{r} 4.0 \\ 40 \end{array} \quad \begin{array}{r} 5.0 \\ 6.5 \end{array}$$

$$\begin{array}{r} 7.7 \\ 40 \end{array} \quad \begin{array}{r} X \\ C.0.0 \\ 7.5 \\ \hline 34.4 \end{array} \quad \begin{array}{r} 5.5 \\ 23 \end{array} \quad \begin{array}{r} 6.4 \\ 14 \end{array} \quad \begin{array}{r} F.0.2 \\ 6.2 \\ \hline 0 \end{array} \quad \begin{array}{r} 5.2 \\ 5 \end{array} \quad \begin{array}{r} 6.6 \\ 13 \end{array} \quad \begin{array}{r} C.0.7 \\ 6.8 \\ \hline 24.3 \end{array} \quad \begin{array}{r} 7.0 \\ 40 \end{array} \quad \begin{array}{r} 6.2 \\ 6.0 \\ 7.5 \end{array}$$

$$\begin{array}{r} 9.8 \\ 40 \end{array} \quad \begin{array}{r} F.3.7 \\ 9.3 \\ \hline 26.8 \end{array} \quad \begin{array}{r} 9.1 \\ 15 \end{array} \quad \begin{array}{r} 7.4 \\ 5 \end{array} \quad \begin{array}{r} F.2.2 \\ 7.8 \\ \hline 0 \end{array} \quad \begin{array}{r} 7.5 \\ 4 \end{array} \quad \begin{array}{r} 9.2 \\ 14 \end{array} \quad \begin{array}{r} F.3.9 \\ 9.5 \\ \hline 28.6 \end{array} \quad \begin{array}{r} 9.7 \\ 40 \end{array} \quad \begin{array}{r} 5.6 \\ 7.1 \end{array}$$

Sta	+	Σ	-	Ground	Grade	
87		886.59	78.6	78.6	80.8	5.5
+50			79.2	79.2	80.7	5.7
88			79.8	79.8	80.7	5.7
+50			80.8	80.8	80.7	5.7
89			81.8	81.8	80.9	5.4
+50			82.3	82.3	81.1	5.2
90			82.2	82.2	81.3	5.0

G.R.

$$\frac{8.8}{40} \quad \textcircled{\frac{F.3.3}{9.1 \atop 26.2}} \quad \frac{9.4}{23} \quad \frac{8.8}{17} \quad \frac{9.7}{16} \quad \frac{8.0}{6} \quad \textcircled{\frac{F.2.3}{8.1 \atop 0}} \quad \frac{8.1}{4} \quad \frac{9.4}{14} \quad \textcircled{\frac{F.3.9}{9.7 \atop 28.6}} \quad \frac{10.0}{40}$$

5.8

$$\frac{7.1}{40} \quad \textcircled{\frac{F.1.5}{7.4 \atop 19}} \quad \frac{8.1}{13} \quad \frac{7.6}{11} \quad \textcircled{\frac{F.1.8}{7.7 \atop 0}} \quad \frac{7.4}{3} \quad \frac{8.4}{11} \quad \textcircled{\frac{F.3.1}{9.0 \atop 25.4}} \quad \frac{9.1}{40}$$

5.9
7.4

$$\frac{6.5}{40} \quad \textcircled{\frac{C.0.9}{6.5 \atop 31}} \quad \frac{6.3}{16} \quad \frac{6.8}{14} \quad \textcircled{\frac{F.1.0}{6.9 \atop 0}} \quad \frac{6.9}{6} \quad \frac{8.0}{17} \quad \textcircled{\frac{F.2.3}{8.2 \atop 32.2}} \quad \frac{8.7}{40}$$

5.9
7.4

$$\frac{5.6}{40} \quad \textcircled{\frac{C.1.7}{5.5 \atop 30.6}} \quad \frac{5.4}{21} \quad \frac{5.5}{6} \quad \textcircled{\frac{F.0.3}{6.2 \atop 0}} \quad \frac{5.7}{3} \quad \frac{6.4}{10} \quad \textcircled{\frac{F.1.5}{7.4 \atop 19}} \quad \frac{6.0}{40}$$

5.9
7.4

$$\frac{4.8}{40} \quad \textcircled{\frac{C.2.4}{4.8 \atop 32.6}} \quad \frac{4.6}{18} \quad \textcircled{\frac{C.0.9}{4.8 \atop 0}} \quad \frac{4.7}{4} \quad \frac{6.0}{12} \quad \textcircled{\frac{C.0.4}{6.8 \atop 31}} \quad \frac{6.8}{40}$$

5.7
7.2

$$\frac{4.5}{40} \quad \textcircled{\frac{C.2.6}{4.4 \atop 33.4}} \quad \frac{4.3}{17} \quad \textcircled{\frac{C.1.3}{4.2 \atop 0}} \quad \frac{4.4}{5} \quad \frac{5.4}{9} \quad \frac{6.0}{19} \quad \textcircled{\frac{C.0.8}{6.2 \atop 31}} \quad \frac{6.3}{40}$$

5.5
7.0

$$\frac{3.7}{40} \quad \textcircled{\frac{C.3.1}{3.7 \atop 35.4}} \quad \frac{3.7}{25} \quad \frac{4.4}{16} \quad \frac{3.8}{9} \quad \frac{4.3}{7} \quad \textcircled{\frac{C.1.0}{4.3 \atop 0}} \quad \frac{5.4}{10} \quad \textcircled{\frac{C.0.7}{6.1 \atop 36.0}} \quad \frac{6.1}{40}$$

5.3
6.8

Sta	+	π	-	Ground	Grade
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886.59

90+50				81.8	81.5	4.8
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91				81.2	81.7	4.6
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+50				81.4	81.9	4.4
-----	--	--	--	------	------	-----

92				82.3	81.9	4.4
----	--	--	--	------	------	-----

○	4.84	887.63	3.80			
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882.79

+50				81.8	82.0	4.0
-----	--	--	--	------	------	-----

885.975

93				81.1	81.9	4.1
----	--	--	--	------	------	-----

+50				80.9	81.8	4.2
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Gr.R

$$\frac{3.9}{40} \quad \frac{C.2.6}{\frac{4.0}{33.4}} \quad \frac{5.2}{17} \quad \frac{4.3}{11-8} \quad \frac{4.9}{6} \quad \frac{C.0.1}{\frac{5.0}{0}} \quad \frac{4.6}{1} \quad \frac{5.0}{8} \quad \frac{5.7}{10} \quad \frac{6.1}{20} \quad \frac{C.0.5}{\frac{6.1}{31}} \quad \frac{6.1}{40} \quad \begin{matrix} 5.1 \\ 6.6 \end{matrix}$$

$$\frac{5.0}{40} \quad \frac{C.0.6}{\frac{5.8}{31.9}} \quad \frac{6.4}{15} \quad \frac{5.2}{7} \quad \frac{F.0.6}{\frac{5.5}{0}} \quad \frac{5.1}{1} \quad \frac{5.5}{7} \quad \frac{6.5}{10} \quad \frac{F.2.0}{\frac{6.9}{21.0}} \quad \begin{matrix} 4.9 \\ 6.4 \end{matrix}$$

$$\frac{5.3}{40} \quad \frac{C.0.9}{\frac{5.3}{31.9}} \quad \frac{6.1}{17} \quad \frac{5.6}{11} \quad \frac{5.0}{7} \quad \frac{F.0.6}{\frac{5.3}{0}} \quad \frac{4.5}{4} \quad \frac{5.7}{10} \quad \frac{6.4}{16} \quad \frac{C.0.0}{\frac{6.2}{31.0}} \quad \frac{6.2}{40} \quad \begin{matrix} 4.7 \\ 6.2 \end{matrix}$$

$$\frac{4.5}{40} \quad \frac{C.1.7}{\frac{4.5}{31.0}} \quad \frac{4.3}{18} \quad \frac{3.8}{9} \quad \frac{C.0.3}{\frac{4.4}{0}} \quad \frac{4.0}{1-5} \quad \frac{5.4}{11} \quad \frac{C.0.2}{\frac{6.0}{31.0}} \quad \frac{5.7}{37} \quad \frac{6.1}{44} \quad \begin{matrix} 4.7 \\ 6.2 \end{matrix}$$

$$\frac{5.5}{40} \quad \frac{C.1.6}{\frac{5.5}{31.0}} \quad \frac{5.2}{20} \quad \frac{5.4}{7} \quad \frac{6.0}{5} \quad \frac{F.0.5}{\frac{6.1}{0}} \quad \frac{5.6}{2} \quad \frac{5.5}{7} \quad \frac{6.3}{11} \quad \frac{7.0}{20} \quad \frac{C.0.0}{\frac{7.1}{27.0}} \quad \frac{7.3}{40} \quad \begin{matrix} 5.6 \\ 7.1 \end{matrix}$$

$$\frac{6.3}{40} \quad \frac{C.0.9}{\frac{6.3}{31.0}} \quad \frac{6.6}{19} \quad \frac{6.3}{14} \quad \frac{6.2}{6} \quad \frac{6.7}{5} \quad \frac{F.1.1}{\frac{6.8}{0}} \quad \frac{6.8}{1} \quad \frac{6.4}{2} \quad \frac{7.0}{7} \quad \frac{8.0}{16} \quad \frac{F.2.3}{\frac{8.0}{22.2}} \quad \frac{8.5}{40} \quad \begin{matrix} 5.7 \\ 7.2 \end{matrix}$$

$$\frac{7.0}{40} \quad \frac{C.0.4}{\frac{7.0}{31.0}} \quad \frac{7.2}{22} \quad \frac{6.6}{15} \quad \frac{6.5}{6} \quad \frac{7.0}{4} \quad \frac{F.1.2}{\frac{7.1}{0}} \quad \frac{7.1}{2} \quad \frac{6.6}{3} \quad \frac{8.1}{13} \quad \frac{F.2.5}{\frac{8.4}{23.0}} \quad \frac{8.7}{40} \quad \begin{matrix} 5.9 \\ 7.4 \end{matrix}$$

Sta	+	π	-	Ground	Grade	
		887.63				
94			80.9	80.9	81.7	4.3
	+50		81.0	81.0	81.7	4.3
95			81.2	81.2	81.7	4.3
	+50		81.0	81.0	81.9	4.1
	+70		81.0	81.0	82.1	
	+86		81.0	81.0	82.1	
96			81.2	81.2	82.2	3.8
	+50		82.1	82.1	82.7	3.3

Gr R.

$$\frac{6.8}{40} \quad \textcircled{\frac{C.0.7}{6.8 \over 31.0}} \quad \frac{7.2}{16} \quad \frac{6.7}{5} \quad \frac{7.2}{4} \quad \textcircled{\frac{F1.1}{7.1 \over 0}} \quad \frac{7.3}{2} \quad \frac{6.8}{3} \quad \frac{8.2}{14} \quad \textcircled{\frac{F2.4}{8.4 \over 22.6}} \quad \frac{8.8}{40} \quad \frac{6.0}{7.5}$$

$$\frac{6.6}{40} \quad \textcircled{\frac{C0.9}{6.6 \over 31.0}} \quad \frac{7.4}{17} \quad \frac{6.6}{13} \quad \frac{6.4}{5} \quad \frac{6.8}{4} \quad \textcircled{\frac{F0.8}{6.8 \over 0}} \quad \frac{7.1}{2} \quad \frac{6.7}{3} \quad \frac{7.2}{8} \quad \frac{8.2}{14} \quad \textcircled{\frac{F2.3}{8.3 \over 22.2}} \quad \frac{8.8}{40} \quad \frac{6.0}{7.5}$$

$$\frac{5.8}{40} \quad \textcircled{\frac{C1.7}{5.8 \over 31.0}} \quad \frac{5.8}{29} \quad \frac{7.3}{17} \quad \frac{6.7}{14} \quad \frac{6.3}{5} \quad \frac{6.8}{2} \quad \textcircled{\frac{F0.7}{6.7 \over 0}} \quad \frac{7.0}{3} \quad \frac{6.5}{5} \quad \frac{7.7}{14} \quad \textcircled{\frac{F2.0}{8.0 \over 21.0}} \quad \frac{8.7}{40} \quad \frac{6.0}{7.5}$$

$$\frac{6.7}{40} \quad \textcircled{\frac{C1.2}{6.0 \over 31.0}} \quad \frac{6.6}{29} \quad \frac{6.9}{9} \quad \frac{6.6}{5} \quad \textcircled{\frac{F1.1}{6.8 \over 0}} \quad \frac{6.8}{4} \quad \frac{6.5}{6} \quad \frac{7.8}{12} \quad \textcircled{\frac{F2.1}{7.8 \over 21.4}} \quad \frac{8.3}{40} \quad \frac{5.7}{7.2}$$

$$\frac{5.0}{58} \quad \frac{8.1}{45} \quad \frac{10.1}{34} \quad \frac{10.5}{25} \quad \frac{10.2}{20} \quad \frac{6.8}{11} \quad \frac{6.9}{4} \quad \frac{6.6}{8} \quad \frac{7.1}{12} \quad \frac{7.1}{26} \quad \frac{8.2}{40}$$

$$\frac{6.0}{40} \quad \frac{6.0}{33} \quad \frac{7.7}{16} \quad \frac{7.3}{7} \quad \frac{6.6}{5} \quad \frac{7.0}{3} \quad \frac{6.9}{5} \quad \frac{6.9}{5} \quad \frac{6.4}{8} \quad \frac{7.0}{27} \quad \frac{7.5}{40}$$

$$\frac{5.6}{40} \quad \textcircled{\frac{C1.7}{6.2 \over 31.0}} \quad \frac{7.1}{13} \quad \frac{6.8}{8} \quad \frac{6.2}{4} \quad \frac{6.2}{2} \quad \textcircled{\frac{F1.2}{6.6 \over 0}} \quad \frac{6.8}{4} \quad \frac{6.2}{7} \quad \frac{7.2}{15} \quad \frac{7.8}{21} \quad \textcircled{\frac{F5.2}{10.6 \over 33.8}} \quad \frac{8.0}{38} \quad \frac{7.2}{45} \quad \frac{5.4}{6.9}$$

$$\frac{4.7}{40} \quad \textcircled{\frac{C1.6}{4.8 \over 31}} \quad \frac{5.4}{13} \quad \textcircled{\frac{F0.9}{5.8 \over 0}} \quad \frac{5.8}{5} \quad \frac{5.2}{16} \quad \textcircled{\frac{C0.0}{6.4 \over 31.0}} \quad \frac{6.7}{40} \quad \frac{4.9}{8.4}$$

Sta	+	Σ	-	Ground	Grade	
		887.63				
97			82.8	82.8	83.2	2.8
+50			83.7	83.7	83.8	2.2
98			84.3	84.3	84.4	1.6
+47			84.6	84.6	84.9	1.1
+50					85.0	
+52						
+58						
+65						
+79.1						
BM			3.22	884.41		

$$\begin{array}{r} 43 \\ 1.2 \\ \hline 86 \\ 43 \\ \hline 211 \end{array} \quad 98 \quad 82.4$$

B.M. Elev. 884.8
SPK in T.P. SE. Cor Hodgson + No. 6. L.

Gr.R.

$$\begin{array}{r} 3.1 \\ 40 \end{array} \quad \begin{array}{r} C.2.5 \\ 3.4 \\ \hline 33.0 \end{array} \quad \frac{4.5}{18} \quad \frac{4.5}{9} \quad \frac{5.2}{3} \quad \begin{array}{r} F0.8 \\ 5.2 \\ \hline 0 \end{array} \quad \frac{5.2}{4} \quad \frac{4.3}{10} \quad \frac{3.8}{16} \quad \begin{array}{r} C1.6 \\ 4.3 \\ \hline 31.0 \end{array} \quad \frac{4.3}{40} \quad \begin{array}{r} 4.4 \\ 5.1 \end{array}$$

$$\begin{array}{r} 1.9 \\ 40 \end{array} \quad \begin{array}{r} C3.3 \\ 2.0 \\ \hline 36.2 \end{array} \quad \frac{2.0}{33} \quad \frac{3.6}{13} \quad \frac{4.3}{4} \quad \begin{array}{r} F0.4 \\ 4.2 \\ \hline 0 \end{array} \quad \frac{3.0}{8} \quad \frac{2.6}{16} \quad \frac{4.0}{27} \quad \begin{array}{r} C1.3 \\ 4.0 \\ \hline 31.0 \end{array} \quad \frac{4.0}{40} \quad \begin{array}{r} 3.8 \\ 5.3 \end{array}$$

$$\begin{array}{r} 0.8 \\ 45 \end{array} \quad \begin{array}{r} C3.9 \\ 0.8 \\ \hline 38.6 \end{array} \quad \frac{1.0}{31} \quad \frac{2.9}{13} \quad \frac{3.2}{6} \quad \begin{array}{r} F0.3 \\ 3.5 \\ \hline 0 \end{array} \quad \frac{3.6}{5} \quad \frac{2.5}{12} \quad \frac{2.2}{16} \quad \frac{3.2}{27} \quad \begin{array}{r} C1.5 \\ 3.2 \\ \hline 31 \end{array} \quad \frac{3.3}{40} \quad \begin{array}{r} 3.2 \\ 4.7 \end{array}$$

$$\begin{array}{r} 0.6 \\ 45 \end{array} \quad \begin{array}{r} C.3.5 \\ 0.7 \\ \hline 37.0 \end{array} \quad \frac{2.6}{9} \quad \frac{3.1}{5} \quad \begin{array}{r} F0.5 \\ 3.2 \\ \hline 0 \end{array} \quad \frac{3.2}{12} \quad \frac{2.0}{17} \quad \frac{1.6}{25} \quad \begin{array}{r} C.2.2 \\ 2.0 \\ \hline 31.8 \end{array} \quad \begin{array}{r} 2.7 \\ 4.2 \end{array}$$

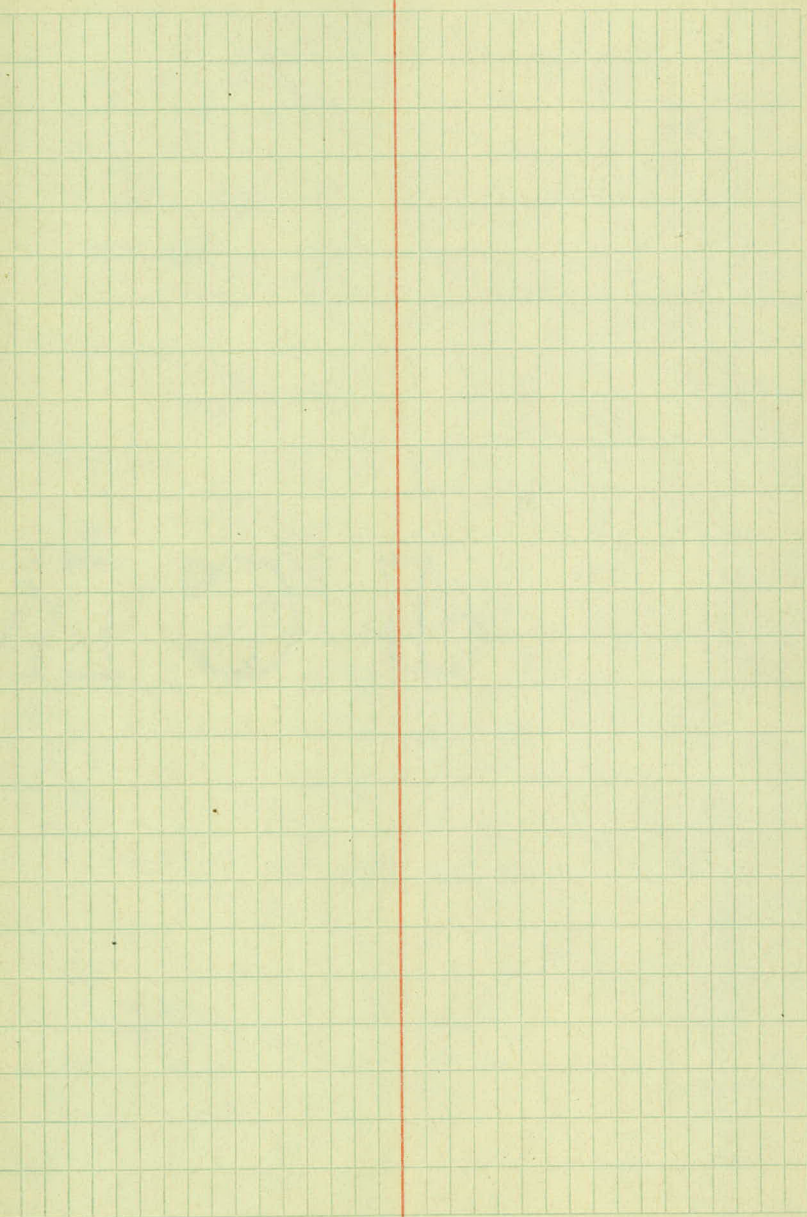
$$\frac{4.6}{40} \quad \frac{4.6}{29} \quad \frac{4.0}{15} \quad \frac{3.0}{10} \quad \frac{3.0}{0} \quad \frac{3.2}{15} \quad \frac{4.0}{23} \quad \frac{4.8}{40}$$

$$\begin{array}{r} 4.3 \\ 40 \end{array} \quad \frac{4.3}{32} \quad \frac{4.0}{15} \quad \frac{3.0}{11} \quad 2.8 \quad \frac{2.8}{11} \quad \frac{3.0}{21} \quad \frac{3.2}{40}$$

$$\frac{3.0}{45} \quad \frac{2.9}{33} \quad \frac{3.0}{14} \quad 2.5 \quad \frac{2.8}{21} \quad \frac{3.1}{41}$$

$$\frac{2.7}{50} \quad \frac{2.4}{25} \quad 2.4 \quad \frac{2.5}{25} \quad \frac{2.8}{50}$$

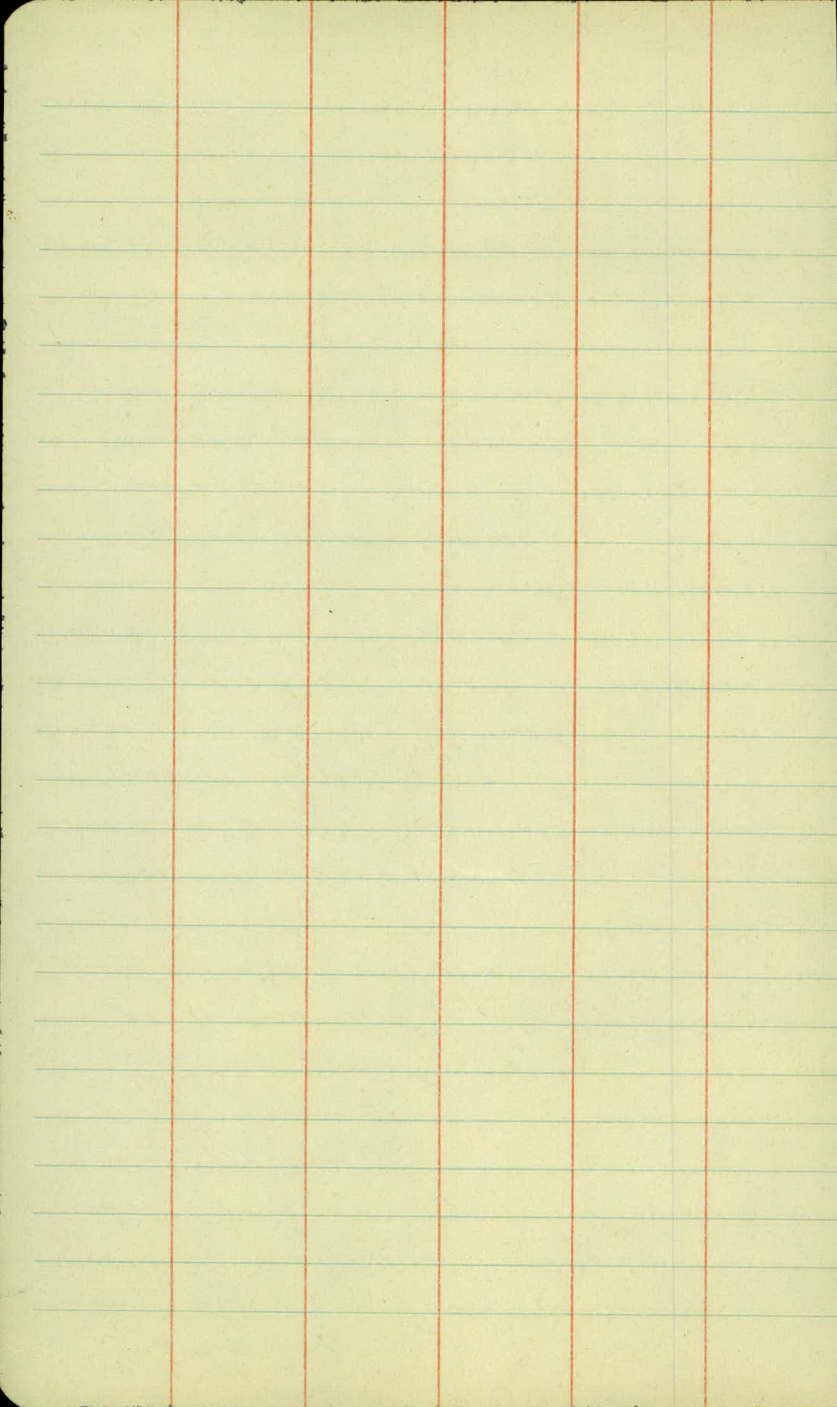
99+79.05

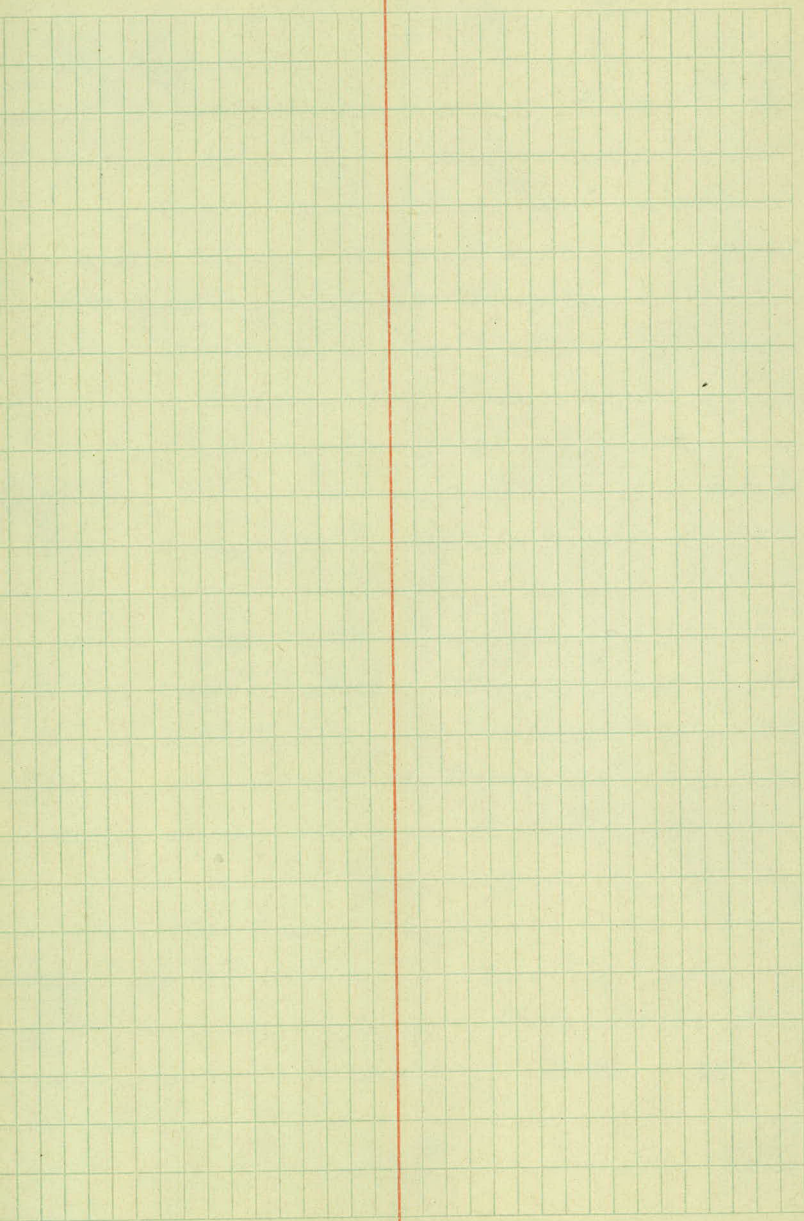


83+00

P.O.T. Set 2"x2" Hub

2x2H06 74.60 15" Elm
48.80 8" Willow





5/4/35

Portell
Skoglon
Bell
Goldberg

Check Levels

	+	π	-	Elev	Orig.
B.M.	3.19	887.60		884.41	884.48
⊙	3.90	886.62	4.88	882.72	
B.M.	3.27	887.83	2.06	884.56	884.57
⊙	1.18	877.05	11.96	875.87	
B.M.	12.75	867.51	10.26	866.79	866.78
⊙	12.15	880.26	0.72	877.56	
⊙	0.90		2.70		
B.M.	6.81		6.81		

SpK in T.P. S.E. Cor Hodgson & No. Co. Line

Top Slope Stake Lt Sta 92+50

SpK in 20" Pop. Rt. Sta 84+75

Top Stake^{15'} Lt. Sta 77+00

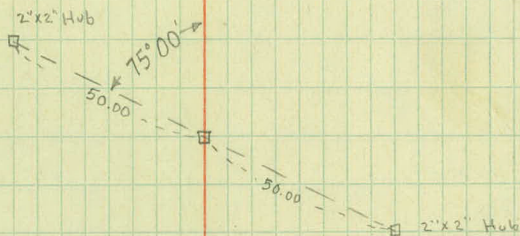
Ctr. Mon Sta 72+38

Top stake 25' Rt Sta 67+00

Blue Top

Ties to Mont. @ Sta. 72 + 38

To Hodgson St



Sta	+	π	-	Z/ev.	Grade
	561	884.77			
	5.91	889.88	0.80	883.97	
62+80				86.0	
63				86.9	85.4 Dit. 1.5
+50				86.2	84.9
64				85.1	84.2
+50				84.8	83.2
65				82.8	82.0
+50				80.4	80.4
66				78.9	78.7

20
29
1.5 Ditch

20
W.H.C.
A.D.C.
D.S.
J.B.
L.G.
May-20/35

2nd Lt E RT

Spike in 20" oak 120' Lt. St. 55+64 E/ev 879.15

$\frac{20}{40}$ $\frac{22}{28}$ $\frac{5.7}{21}$ $\frac{5.9}{16}$ $\frac{4.4}{12}$ $\frac{3.9}{12}$ $\frac{4.4}{12}$ $\frac{5.7}{16}$ $\frac{5.7}{22}$ $\frac{2.9}{27}$ $\frac{3.4}{40}$

C-1.3 $\frac{22}{33}$ $\frac{2.2}{26}$ $\frac{22}{28}$ $\frac{2.3}{17}$ $\frac{2.0}{9}$ C-1.5 $\frac{2.8}{9}$ $\frac{3.1}{26}$ $\frac{3.1}{24.6}$ $\frac{3.4}{33}$

C-1.1 $\frac{3.7}{38}$ $\frac{2.8}{12}$ C-1.3 $\frac{3.7}{0}$ $\frac{3.6}{3}$ $\frac{4.4}{9}$ DC-1.5 $\frac{5.0}{31}$ $\frac{4.9}{23}$

DC-1.6 $\frac{6.7}{33}$ $\frac{6.6}{31}$ $\frac{6.0}{26.2}$ $\frac{5.0}{9}$ C-0.9 $\frac{4.8}{10}$ $\frac{5.2}{10}$ DC-1.5 $\frac{5.7}{31}$ $\frac{5.7}{33}$

DC-0.7 $\frac{7.8}{33}$ $\frac{7.5}{31}$ $\frac{7.3}{26.6}$ $\frac{6.8}{22}$ $\frac{5.7}{16}$ $\frac{4.4}{7}$ C-1.6 $\frac{5.1}{8}$ $\frac{5.6}{8}$ C-0.7 $\frac{6.0}{32.8}$ $\frac{5.9}{28}$

DC-1.12 $\frac{8.5}{40}$ $\frac{8.2}{31}$ $\frac{7.2}{15}$ $\frac{6.2}{7}$ $\frac{7.0}{3}$ C-0.8 $\frac{7.1}{14}$ $\frac{7.7}{14}$ DC-1.4 $\frac{8.0}{31}$ $\frac{8.2}{40}$

DC-1.1 $\frac{9.9}{40}$ $\frac{9.9}{31.0}$ $\frac{9.5}{12}$ $\frac{8.6}{8}$ $\frac{9.3}{4}$ $\frac{9.0}{9.5}$ $\frac{9.8}{4}$ $\frac{9.8}{17.2}$ $\frac{10.1}{31.0}$ $\frac{10.4}{40}$

C-1.7 $\frac{9.6}{40}$ $\frac{9.5}{33}$ $\frac{9.7}{31}$ $\frac{9.9}{7}$ $\frac{11.8}{4}$ $\frac{11.0}{11.0}$ $\frac{11.2}{13.0}$ $\frac{11.5}{31.0}$ $\frac{11.8}{40}$

889.88

66+50

72.5

77.0

T.P.

4.67

881.30

13.25

876.63

67

75.3

75.3

+50

72.9

73.6

68+68

72.0

73.0

68+0

70.7

72.0

+20

70.0

71.4

T.P.

1.60

871.83

11.07

870.23

68+50

68.9

70.6

69

67.8

69.6

Lt

Z

Rt.

G-0.5

C-0.8

$$\frac{9.5}{40}$$

$$\frac{9.6}{33}$$

$$\frac{9.1}{18}$$

$$\frac{8.6}{12}$$

$$\frac{12.4}{4}$$

$$12.4$$

$$\frac{11.7}{12}$$

$$\frac{12.1}{32.2}$$

$$\frac{12.3}{40}$$

C-4.2

D.C.1.2

$$\frac{1.5}{40}$$

$$\frac{1.8}{33}$$

$$\frac{2.5}{14}$$

$$\frac{5.8}{3}$$

$$\frac{8.8}{60}$$

$$\frac{5.7}{13}$$

$$\frac{6.3}{31}$$

$$\frac{6.3}{40}$$

C-2.8

F0.7

F1.2

$$\frac{4.6}{40}$$

$$\frac{4.9}{33}$$

$$\frac{4.7}{12}$$

$$\frac{8.4}{2}$$

$$\frac{8.4}{1}$$

$$\frac{8.9}{17.8}$$

$$\frac{9.5}{31}$$

C-2.3

F1.0

F0.5

$$\frac{5.8}{40}$$

$$\frac{6.0}{33}$$

$$\frac{6.5}{23}$$

$$\frac{6.1}{12}$$

$$\frac{8.6}{4}$$

$$\frac{9.3}{1}$$

$$\frac{9.2}{7}$$

$$\frac{9.5}{12}$$

$$\frac{9.8}{15.0}$$

$$\frac{10.1}{31}$$

C-1.4

F1.3

F4.0

$$\frac{7.6}{40}$$

$$\frac{7.9}{33}$$

$$\frac{8.9}{18}$$

$$\frac{8.9}{8}$$

$$\frac{10.5}{4}$$

$$\frac{10.6}{1}$$

$$\frac{10.5}{7}$$

$$\frac{13.3}{29}$$

$$\frac{14.3}{40}$$

C-0.6

F1.4

F4.4

$$\frac{8.8}{40}$$

$$\frac{9.3}{31}$$

$$\frac{10.3}{12}$$

$$\frac{11.4}{6}$$

$$\frac{11.3}{1}$$

$$\frac{11.2}{6}$$

$$\frac{12.7}{12}$$

$$\frac{14.3}{30.6}$$

$$\frac{14.3}{40}$$

F1.3

F-1.7

F3.3

$$\frac{2.2}{33}$$

$$\frac{2.5}{33}$$

$$\frac{3.8}{12}$$

$$\frac{3.9}{6}$$

$$\frac{3.0}{3}$$

$$\frac{2.9}{1}$$

$$\frac{3.2}{7}$$

$$\frac{4.0}{12}$$

$$\frac{4.6}{16}$$

$$\frac{4.5}{40.2}$$

$$\frac{4.6}{40}$$

F-2.4

F1.8

F2.8

$$\frac{4.7}{33}$$

$$\frac{4.6}{21.6}$$

$$\frac{4.9}{9}$$

$$\frac{4.3}{3}$$

$$\frac{4.0}{1}$$

$$\frac{4.1}{6}$$

$$\frac{4.7}{8}$$

$$\frac{5.0}{24.2}$$

$$\frac{5.0}{33}$$

87183

6950

67.4

688

7050

66.8

68.4

7050

67.0

68.2

7100

867.2

68.0

Lt.

±

Rt.

		F2.0		F1.4		F1.9	
3.0	$\frac{5.0}{33}$	$\frac{5.0}{21.0}$	$\frac{5.0}{13}$	$\frac{4.5}{7}$	$\frac{5.0}{12}$	$\frac{4.9}{20.6}$	$\frac{5.0}{33}$

		F2.4		F1.6		F2.4	
3.4	$\frac{5.7}{33}$	$\frac{5.8}{22.6}$	$\frac{5.8}{7}$	$\frac{5.0}{5}$	$\frac{5.7}{12}$	$\frac{5.8}{22.6}$	$\frac{5.8}{33}$

		F1.8		F1.2		F1.4	
3.6	$\frac{5.4}{33}$	$\frac{5.4}{20.2}$	$\frac{5.2}{17}$	$\frac{4.8}{12}$	$\frac{5.0}{12}$	$\frac{5.0}{18.6}$	$\frac{4.9}{33}$

3.5				4.6			
-----	--	--	--	-----	--	--	--

Cont on p. 4

Grade

11.72

870.87

879.15

61+50

84.9

85.2

2.5-Dit

62

85.2

85.4

2.4-Dit

62+50

85.4

85.5

2.2-Dit

63+0

85.4

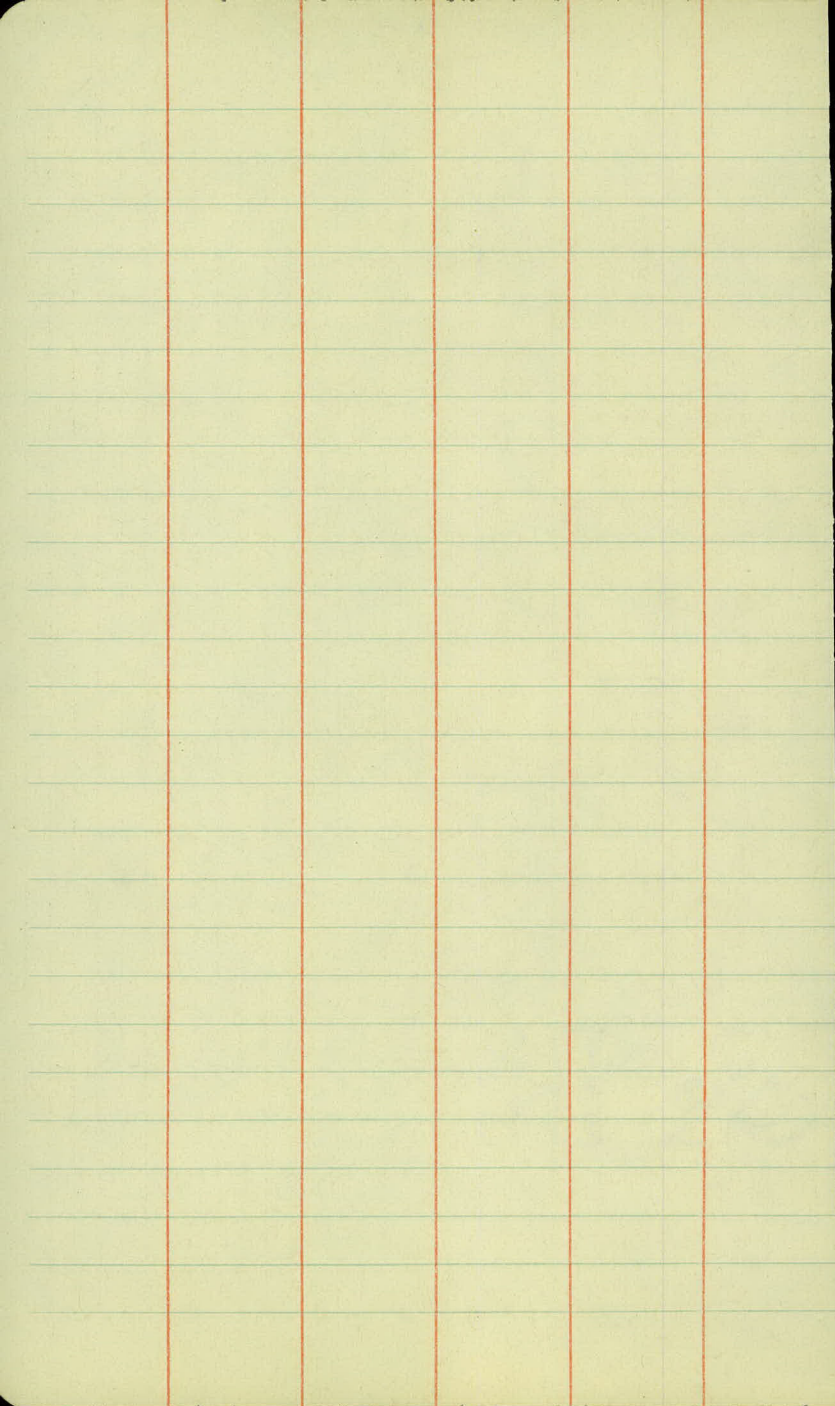
S.R.

$$\begin{array}{r}
 \text{D.C. 2.5} \\
 \begin{array}{r}
 56 \\
 \hline
 40
 \end{array}
 \begin{array}{r}
 57 \\
 \hline
 33
 \end{array}
 \begin{array}{r}
 55 \\
 \hline
 25
 \end{array}
 \begin{array}{r}
 76 \\
 \hline
 21
 \end{array}
 \begin{array}{r}
 76 \\
 \hline
 17
 \end{array}
 \begin{array}{r}
 58 \\
 \hline
 13
 \end{array}
 \end{array}
 \quad
 \begin{array}{r}
 -F.93 \\
 \hline
 6.0
 \end{array}
 \quad
 \begin{array}{r}
 6.7 \\
 \hline
 13
 \end{array}
 \begin{array}{r}
 7.3 \\
 \hline
 17
 \end{array}
 \begin{array}{r}
 7.6 \\
 \hline
 23
 \end{array}
 \begin{array}{r}
 4.1 \\
 \hline
 27
 \end{array}
 \begin{array}{r}
 3.7 \\
 \hline
 33
 \end{array}
 \begin{array}{r}
 3.9 \\
 \hline
 40
 \end{array}$$

$$\begin{array}{r}
 \text{C-2.3} \\
 \begin{array}{r}
 34 \\
 \hline
 40
 \end{array}
 \begin{array}{r}
 32 \\
 \hline
 33
 \end{array}
 \begin{array}{r}
 35 \\
 \hline
 27
 \end{array}
 \begin{array}{r}
 7.2 \\
 \hline
 21
 \end{array}
 \begin{array}{r}
 7.2 \\
 \hline
 17
 \end{array}
 \begin{array}{r}
 6.0 \\
 \hline
 13
 \end{array}
 \end{array}
 \quad
 \begin{array}{r}
 -F.02 \\
 \hline
 5.7
 \end{array}
 \quad
 \begin{array}{r}
 5.5 \\
 \hline
 13
 \end{array}
 \begin{array}{r}
 6.8 \\
 \hline
 17
 \end{array}
 \begin{array}{r}
 6.8 \\
 \hline
 23
 \end{array}
 \begin{array}{r}
 2.4 \\
 \hline
 30
 \end{array}
 \begin{array}{r}
 2.4 \\
 \hline
 33
 \end{array}
 \begin{array}{r}
 1.4 \\
 \hline
 40
 \end{array}$$

$$\begin{array}{r}
 \text{C-2.6} \\
 \begin{array}{r}
 25 \\
 \hline
 40
 \end{array}
 \begin{array}{r}
 28 \\
 \hline
 33
 \end{array}
 \begin{array}{r}
 27 \\
 \hline
 28
 \end{array}
 \begin{array}{r}
 7.1 \\
 \hline
 21
 \end{array}
 \begin{array}{r}
 7.1 \\
 \hline
 17
 \end{array}
 \begin{array}{r}
 5.8 \\
 \hline
 13
 \end{array}
 \end{array}
 \quad
 \begin{array}{r}
 -F.01 \\
 \hline
 5.5
 \end{array}
 \quad
 \begin{array}{r}
 5.8 \\
 \hline
 13
 \end{array}
 \begin{array}{r}
 6.7 \\
 \hline
 17
 \end{array}
 \begin{array}{r}
 6.6 \\
 \hline
 22
 \end{array}
 \begin{array}{r}
 3.1 \\
 \hline
 28
 \end{array}
 \begin{array}{r}
 2.9 \\
 \hline
 33
 \end{array}
 \begin{array}{r}
 3.2 \\
 \hline
 40
 \end{array}$$

Cont on Page 20



Final X-Sections

6/21/35

Purtell

Bell

Skog

Goldberg

Sta	+	π	-	Elev
B.M.	5.24	884.39		879.15
○	6.75	889.81	1.33	883.06
59				81.0
+50				82.0
60				83.0
+50				83.6
61				844
+50				849
62				854
+50				85.6
63				85.3
+50				84.6

SpK. in 20' Oak 120' Lt. Sta. 55+84

$$\frac{10.6}{33} \quad \frac{10.4}{18} \quad \frac{9.0}{13} \quad \frac{8.8}{0} \quad \frac{9.1}{12} \quad \frac{10.4}{17-21} \quad \frac{9.7}{22-33}$$

$$\frac{10.0}{33-18} \quad \frac{8.0}{13} \quad 7.8 \quad \frac{8.1}{13} \quad \frac{9.4}{17} \quad \frac{9.6}{21} \quad \frac{9.2}{22} \quad \frac{9.0}{33}$$

$$\frac{9.1}{33} \quad \frac{8.7}{17} \quad \frac{7.0}{13} \quad 6.8 \quad \frac{7.0}{13} \quad \frac{8.2}{17-23} \quad \frac{7.6}{23} \quad \frac{7.2}{33}$$

$$\frac{7.6}{33} \quad \frac{7.3}{22} \quad \frac{7.8}{21-17} \quad \frac{6.1}{13} \quad 6.2 \quad \frac{6.4}{13} \quad \frac{7.4}{17} \quad \frac{7.3}{22} \quad \frac{6.4}{24} \quad \frac{6.2}{33}$$

$$\frac{6.2}{33} \quad \frac{6.0}{23} \quad \frac{7.1}{22} \quad \frac{7.0}{17} \quad \frac{5.6}{13} \quad 5.4 \quad \frac{5.4}{13} \quad \frac{6.7}{14} \quad \frac{6.8}{22} \quad \frac{5.2}{24} \quad \frac{5.0}{33}$$

$$\frac{4.8}{33} \quad \frac{4.6}{26} \quad \frac{6.6}{20-17} \quad \frac{4.9}{13} \quad 4.9 \quad \frac{4.9}{13} \quad \frac{6.6}{19-22} \quad \frac{3.1}{30} \quad \frac{3.0}{33}$$

$$\frac{2.3}{40} \quad \frac{2.4}{31} \quad \frac{6.1}{21-17} \quad \frac{4.5}{13} \quad 4.4 \quad \frac{4.5}{13} \quad \frac{6.6}{19} \quad \frac{6.5}{23} \quad \frac{1.6}{33} \quad \frac{1.4}{40}$$

$$\frac{1.7}{40} \quad \frac{1.8}{33} \quad \frac{6.0}{23-17} \quad \frac{4.4}{13} \quad 4.2 \quad \frac{4.3}{13} \quad \frac{6.5}{19} \quad \frac{6.3}{24} \quad \frac{2.0}{33} \quad \frac{2.2}{40}$$

$$\frac{2.5}{40} \quad \frac{2.4}{33} \quad \frac{6.1}{23-18} \quad \frac{4.5}{13} \quad 4.5 \quad \frac{4.5}{13} \quad \frac{6.1}{19-23} \quad \frac{3.5}{33} \quad \frac{3.7}{40}$$

$$\frac{4.0}{40-33} \quad \frac{6.8}{23-19} \quad \frac{5.2}{13} \quad 5.2 \quad \frac{5.2}{13} \quad \frac{7.0}{19} \quad \frac{6.8}{23} \quad \frac{5.0}{31-40}$$

Sta	+	Δ	-	Elev.
-----	---	----------	---	-------

64				83.8
----	--	--	--	------

+50				
-----	--	--	--	--

65				
----	--	--	--	--

+50				
-----	--	--	--	--

66				
----	--	--	--	--

①	3.11	881.69	878.58	
---	------	--------	--------	--

+50				
-----	--	--	--	--

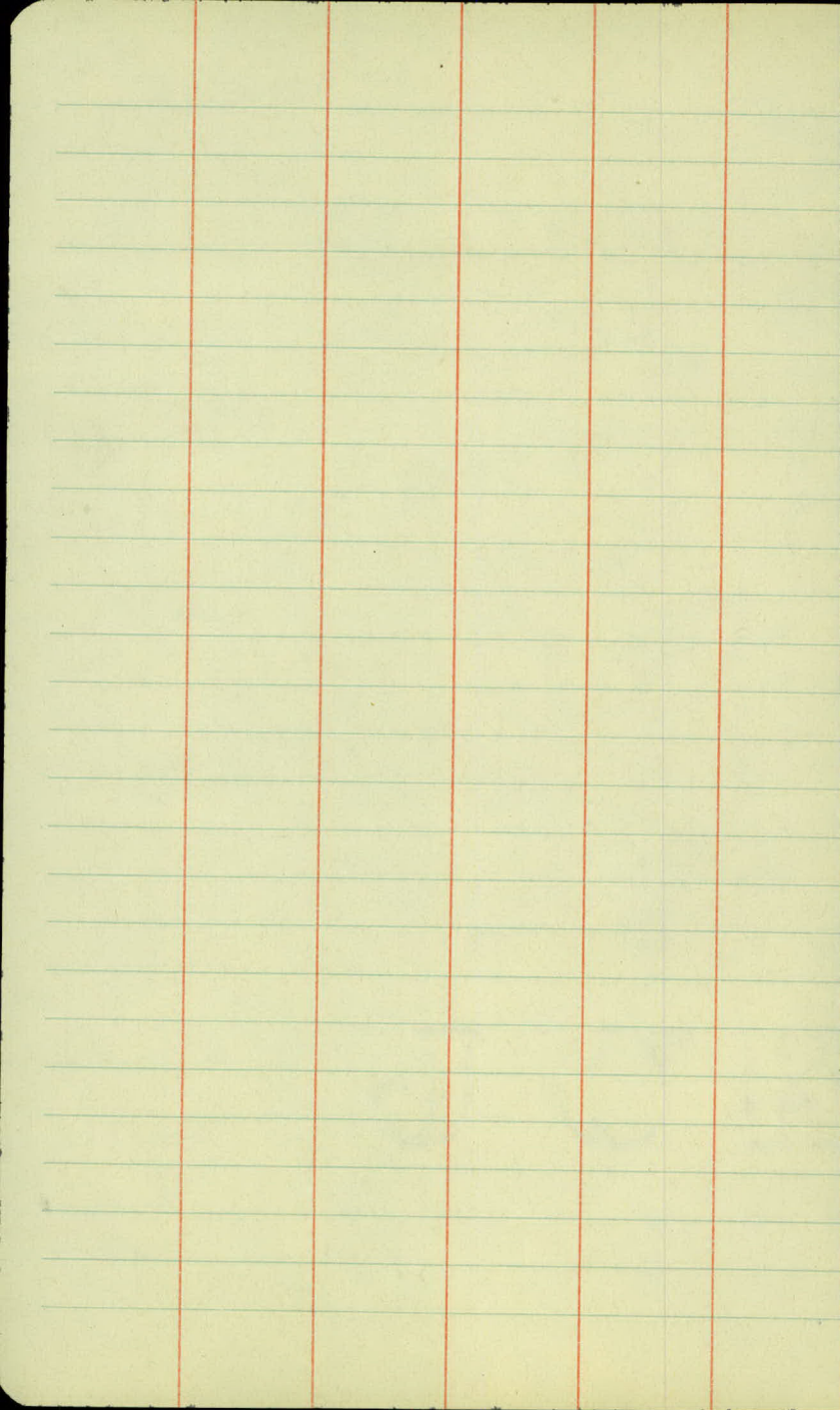
67				
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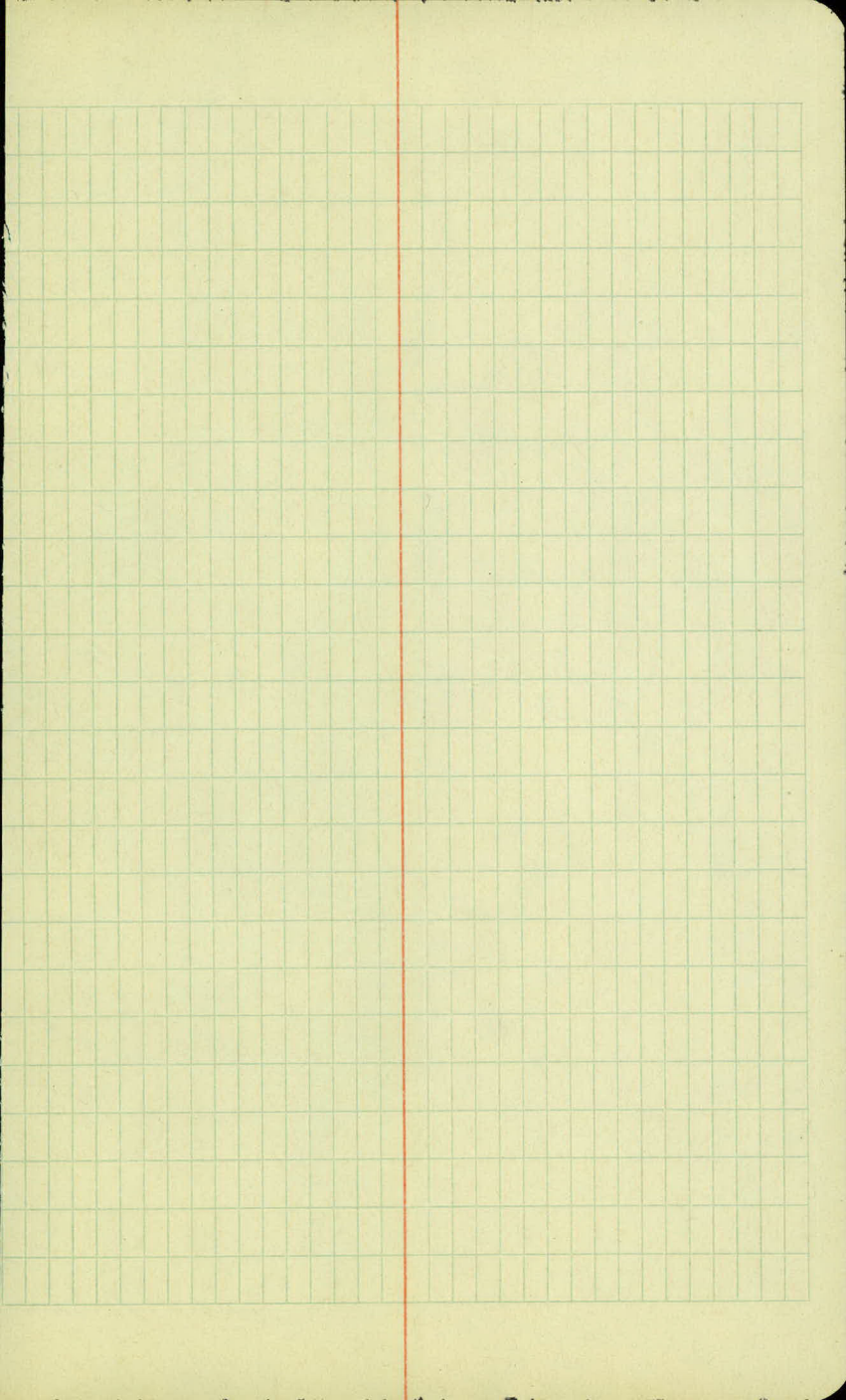
+50				
-----	--	--	--	--

$$\frac{7.2}{40} \quad \frac{6.8}{31} \quad \frac{7.5}{26-19} \quad \frac{6.1}{13} \quad 6.0 \quad \frac{6.0}{13} \quad \frac{7.7}{19-23} \quad \frac{5.7}{32-40}$$

$$\frac{8.2}{40} \quad \frac{7.5}{31} \quad \frac{8.5}{24} \quad \frac{8.6}{19} \quad \frac{6.7}{13} \quad 6.8 \quad \frac{6.8}{13} \quad \frac{8.4}{19-23} \quad \frac{6.0}{33-40}$$

$$8.3 \quad \frac{8.2}{13} \quad \frac{10.0}{19-24} \quad \frac{8.0}{31} \quad \frac{8.2}{40}$$





Culverts

24" x 18'

" x 20'

" x 18'

x 20

x 20

x 20

116

4-24" X Bands

24" x 85

x 88

x 83

15" x 20'

15 x 20'

1.08 Perforated 3 sets 4 lines 8 hole in line
in valley

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.

ROADWAY 14 FEET WIDE. SIDE SLOPES 1½ TO 1.

FOR SINGLE TRACK EMBANKMENT.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	7.0	7.2	7.3	7.5	7.6	7.8	7.9	8.1	8.2	8.4	0
1	8.5	8.7	8.8	9.0	9.1	9.3	9.4	9.6	9.7	9.9	1
2	10.0	10.2	10.3	10.5	10.6	10.8	10.9	11.1	11.2	11.4	2
3	11.5	11.7	11.8	12.0	12.1	12.3	12.4	12.6	12.7	12.9	3
4	13.0	13.2	13.3	13.5	13.6	13.8	13.9	14.1	14.2	14.4	4
5	14.5	14.7	14.8	15.0	15.1	15.3	15.4	15.6	15.7	15.9	5
6	16.0	16.2	16.3	16.5	16.6	16.8	16.9	17.1	17.2	17.4	6
7	17.5	17.7	17.8	18.0	18.1	18.3	18.4	18.6	18.7	18.9	7
8	19.0	19.2	19.3	19.5	19.6	19.8	19.9	20.1	20.2	20.4	8
9	20.5	20.7	20.8	21.0	21.1	21.3	21.4	21.6	21.7	21.9	9
10	22.0	22.2	22.3	22.5	22.6	22.8	22.9	23.1	23.2	23.4	10
11	23.5	23.7	23.8	24.0	24.1	24.3	24.4	24.6	24.7	24.9	11
12	25.0	25.2	25.3	25.5	25.6	25.8	25.9	26.1	26.2	26.4	12
13	26.5	26.7	26.8	27.0	27.1	27.3	27.4	27.6	27.7	27.9	13
14	28.0	28.2	28.3	28.5	28.6	28.8	28.9	29.1	29.2	29.4	14
15	29.5	29.7	29.8	30.0	30.1	30.3	30.4	30.6	30.7	30.9	15
16	31.0	31.2	31.3	31.5	31.6	31.8	31.9	32.1	32.2	32.4	16
17	32.5	32.7	32.8	33.0	33.1	33.3	33.4	33.6	33.7	33.9	17
18	34.0	34.2	34.3	34.5	34.6	34.8	34.9	35.1	35.2	35.4	18
19	35.5	35.7	35.8	36.0	36.1	36.3	36.4	36.6	36.7	36.9	19
20	37.0	37.2	37.3	37.5	37.6	37.8	37.9	38.1	38.2	38.4	20
21	38.5	38.7	38.8	39.0	39.1	39.3	39.4	39.6	39.7	39.9	21
22	40.0	40.2	40.3	40.5	40.6	40.8	40.9	41.1	41.2	41.4	22
23	41.5	41.7	41.8	42.0	42.1	42.3	42.4	42.6	42.7	42.9	23
24	43.0	43.2	43.3	43.5	43.6	43.8	43.9	44.1	44.2	44.4	24
25	44.5	44.7	44.8	45.0	45.1	45.3	45.4	45.6	45.7	45.9	25
26	46.0	46.2	46.3	46.5	46.6	46.8	46.9	47.1	47.2	47.4	26
27	47.5	47.7	47.8	48.0	48.1	48.3	48.4	48.6	48.7	48.9	27
28	49.0	49.2	49.3	49.5	49.6	49.8	49.9	50.1	50.2	50.4	28
29	50.5	50.7	50.8	51.0	51.1	51.3	51.4	51.6	51.7	51.9	29
30	52.0	52.2	52.3	52.5	52.6	52.8	52.9	53.1	53.2	53.4	30
31	53.5	53.7	53.8	54.0	54.1	54.3	54.4	54.6	54.7	54.9	31
32	55.0	55.2	55.3	55.5	55.6	55.8	55.9	56.1	56.2	56.4	32
33	56.5	56.7	56.8	57.0	57.1	57.3	57.4	57.6	57.7	57.9	33
34	58.0	58.2	58.3	58.5	58.6	58.8	58.9	59.1	59.2	59.4	34
35	59.5	59.7	59.8	60.0	60.1	60.3	60.4	60.6	60.7	60.9	35
36	61.0	61.2	61.3	61.5	61.6	61.8	61.9	62.1	62.2	62.4	36

Calculated by Julien A. Hall, M. Am. Soc. C. E.

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