

Book-6, Pr. 11-A

OFFICE OF COUNTY ENGINEER
RAMSEY CO. MINN.

PLAN Survey

SNELLING AVE.

From Co. Rd. "G" To 1 mi. No.

Road Acc't. No. M5

Date Filed 3-3-32

File P.

PROJ. 32-M5

2-17-32

TRANSIT NOTES

SNELING AVE

County Rd "G" 1 Mile North.

Sta. Point

$\Delta L + \Delta R$

52+56⁶⁹ Mont. = N.W. Cor. Sec. 15-30-23

49+72⁷⁶ P.O.T.

45+43⁴⁵ P.O.T.

26+21⁴⁴ P.O.T.

0°18' Lt.

11+70⁴³ P.O.T.

0+00 Mont. = S.W. Cor. Sec. 15-T30-R23

Cold-Windy.

2-18-32

6" Oak @ 44.41

6" Oak @ 19.88

36.75 @ 14" Oak

52.28 @ 10" Oak

42.47 @ 8" Oak

27.28 @ 8" Oak

31.86 @ 6" Oak

10" Oak @ 51.15

Spike = 1 1/4 Cor. Sec 15-30-33

EST 2/17/32

(D.M.)

* F.O. @ 29.08
*
*

Shelling Ave.

27.24 * F.P.
18.82 * F.P.

9 R.R.

35.07

L. Co. Rd.

"G"

57.27

6 R.R.

Sta	+	H.I. ✓	-	Elev.
B.M.	7.57	923.41		915.84
T.P.	7.28	927.10 ^{30.}	3.39	920.02 ✓
T.P.	6.18	930.16 ^{36.}	3.12	923.98
T.P.	13.69	941.23 ^{43.}	2.62	927.54
T.P.	9.35	950.36 ^{38.}	0.22	941.01
B.M.			2.66	947.70
B.M.	5.16	953.35	2.49	947.87 948.19
0+00		± "G"		47.9
+13				48.1
+19				48.2
+50				47.9
1				48.3
+50				48.9
B.M.		5.16	947.87	948.19

Clear - Fair

30°F P.M.

2-19-32

Weber
Wilke
Galt
Stienman

Left

±

Right

Spk. in 30" Map. N.E. Cor M.V. Rd + Anoka C. off

Anoka Cut off Notes

Top of Mont. Snelling and Co. Rd "G." S.E. cor.

Spike in P.R. N.E. cor Int. Snelling and "G."

7.4	6.8	6.0	4.5	3.6	2.7
75	50	25	5.4	25	50

6.7	6.2	4.6	3.8
50	25	53	25

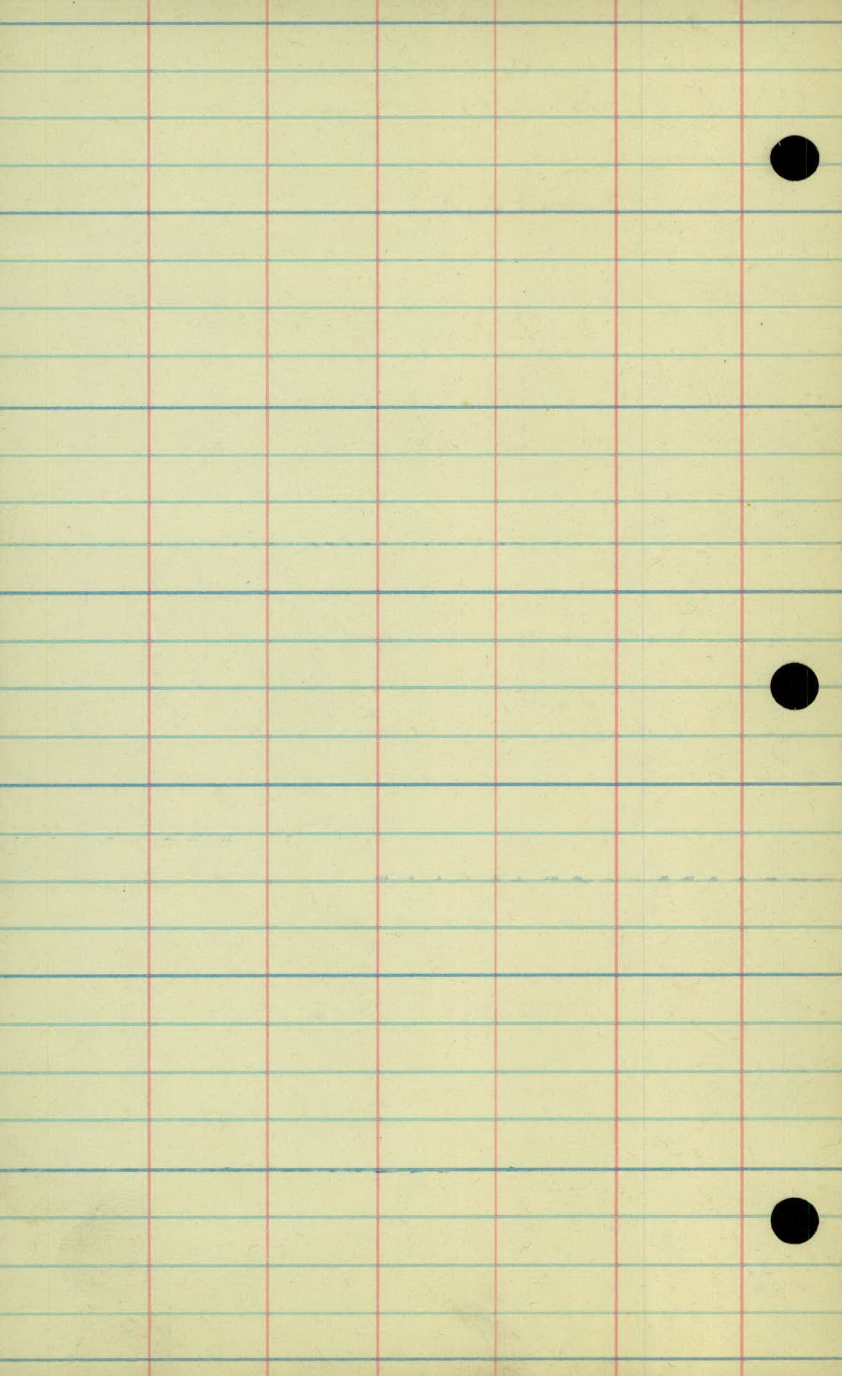
9.1	8.8	6.8	4.2	8.5	8.1
57	49	42	52	47	60

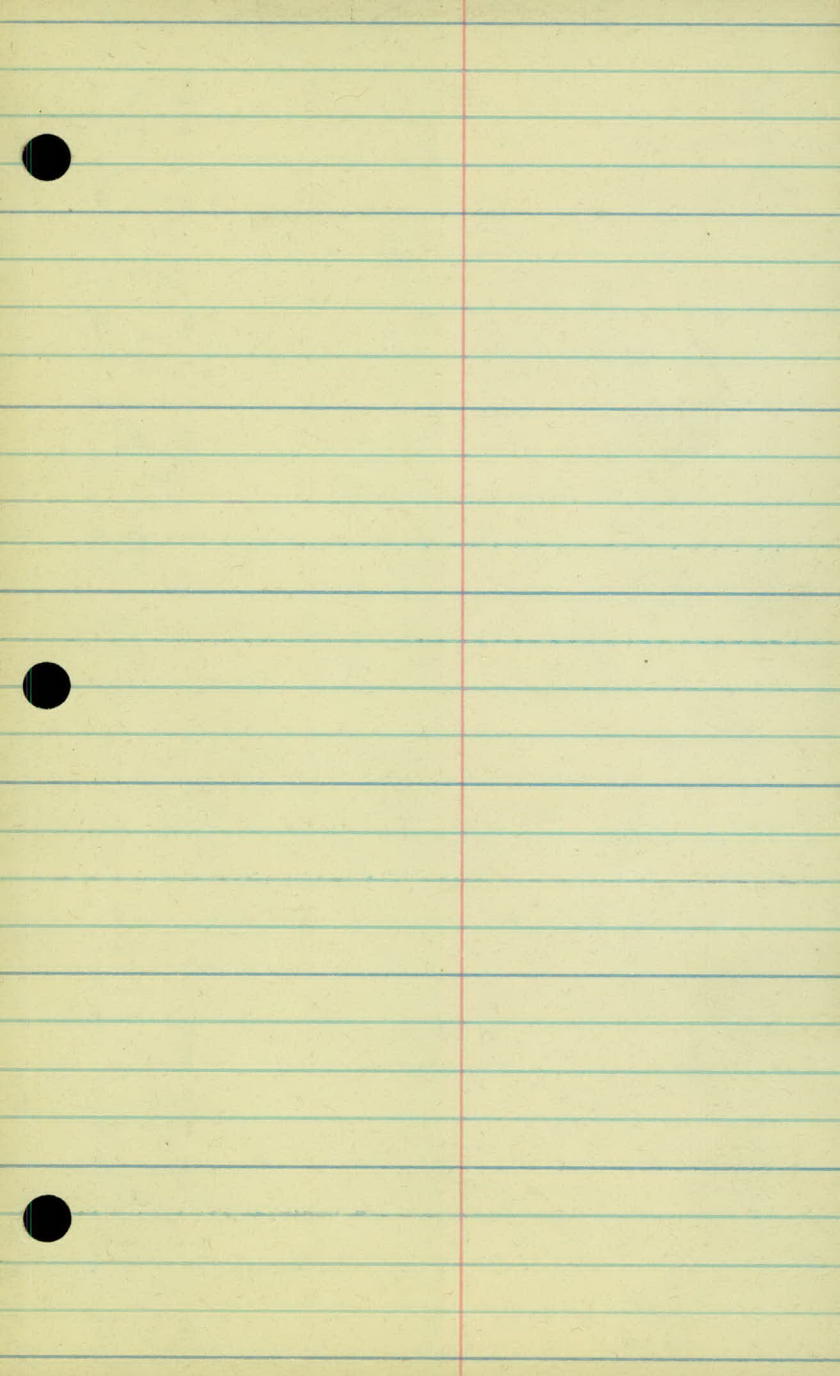
10.6	10.3	9.8	6.4	5.2	6.0	9.5	9.6	9.4
50	32	21	14	55	13	21	28	42

10.0	9.0	7.8	6.8	5.6	5.6	8.4	8.0	6.1	5.2
40	26	15	13	7	51	13	18	24	28

8.2	6.9	6.1	6.5	6.1	5.2	4.9	6.3	7.4	4.5	3.7
40	27	15	12	10	8	45	12	15	21	26

Spike in P.R.





+ H.1 -

B.M. 7.60 955.79. ~~947.87~~ 948.19.
2+00 49.8

2+50 51.3

3+00 52.3

T.P. 6.74 962.42 0.11 955.68.
+50 54.0

4 55.7

+50 58.0

T.P. 10.41 971.87 0.96 961.46.
5 60.5

+50 63.4

6 66.6

+50 69.5

T.P. 13.31 984.42 0.76 971.11.
7 72.2

+50 74.6

8 76.9

T.P.

RT

LT

Spoke in RR N.E. cor. Int "G" & Snelling

7.3	7.4	9.0	9.0	6.3	6.4	7.8	7.2	7.8	9.0
40	25	21	17	11	6.0	7	11	15	22
									40

7.4	7.5	8.9	8.5	4.6	4.5	7.9	6.2	5.5	5.3	5.6
40	24	19	16	8		9	11	13	21	40

7.5	7.5	7.8	7.5	4.1	3.4	3.9	5.0	6.3	5.5
40	34	21	15	11	7	3,3	9	12	24
									40

11.7	11.1	10.2	9.2	8.4	8.6	10.0	13.5	13.4	13.4
40	21	12	10		8	12	17	23	40

10.0	9.5	8.3	6.9	6.7	6.8	7.4	10.4	10.6	10.5
40	21	14	10		7	10	14	21	40

8.4	6.0	6.5	5.7	4.7	4.4	4.4	4.9	6.3	5.6	4.3
40	34	17	12	10	4.4	6	8	10	21	40

13.9	11.4	12.7	11.6	11.4	11.4	12.4	12.3	8.7	7.3
40	17	14	11		7	11	16	19	40

11.2	7.2	9.3	8.6	8.5	8.3	10.8	9.5	5.3	4.2
40	16	12	10		8	14	16	19	40

9.1	7.4	5.9	6.3	5.6	5.4	6.1	6.0	4.2	3.5
40	26	13	12	11	5.3	9	12	20	23
									40

5.8	4.2	3.0	2.4	2.8	3.6	3.6	1.9	0.9
40	22	11		10	15	17	22	40

14.2	12.8	13.5	13.4	12.6	12.6	13.2	11.5	10.9
50	18	16	12	11	12.2	9	14	21
								50

10.1	7.4	11.0	10.3	9.8	10.1	10.5	4.9	3.8	3.6
50	19	15	12		7	9	17	20	50

10.0	4.8	8.6	7.7	7.5
50	20	15	8	

984.42

+41

77.9

BM. 10.93 988.58 6.77 977.65 977.65
8

+41

BM. 12.03 989.68 10.93 977.65

9

79.0

+50

78.8

10

79.0

+50

79.9

11

81.5

+50

83.4

T.P. 7.23 994.45 2.46 987.22

12

83.7

+43

82.4

13

80.3

T.P. 6.50 987.32 13.63 980.82

+33

77.9

Left & Right

$\frac{9.2}{50} \frac{5.9}{20} \frac{7.2}{16} \frac{6.6}{11} 6.4$

Top Rock 58' Lt 54.0 - 8+95

(11.7) $\frac{11.7}{5} \frac{12.0}{9} \frac{4.4}{17} \frac{4.1}{50}$

(Fair) 25.5

(10.6) $\frac{10.6}{4.} \frac{10.1}{9} \frac{2.8}{17} \frac{2.7}{50}$

Top Rock 8+95

2-2+-32 PM

$\frac{13.0}{50} \frac{12.6}{25} \frac{12.1}{14} \frac{11.5}{12} 10.7 \frac{10.8}{5} \frac{11.6}{10} \frac{9.7}{13} \frac{8.7}{27} \frac{6.8}{50}$

$\frac{14.2}{50} \frac{14.1}{29} \frac{14.3}{16} \frac{12.3}{14} \frac{10.2}{11} 10.9 \frac{11.4}{6} \frac{10.9}{12} \frac{10.4}{28} \frac{8.9}{50}$

$\frac{10.7}{50} \frac{12.3}{25} \frac{11.8}{17} \frac{10.8}{11} 10.7 \frac{11.1}{5} \frac{13.1}{7} \frac{11.3}{11} \frac{10.7}{25} \frac{10.1}{50}$

Present
(L.R.)

$\frac{9.9}{50} \frac{10.3}{27} \frac{9.9}{12} \frac{9.6}{4} 9.8 \frac{10.1}{3} \frac{11.8}{7} \frac{12.2}{10} \frac{12.0}{23} \frac{12.3}{50}$

$\frac{6.9}{50} \frac{7.6}{21} \frac{8.1}{12} 8.2 \frac{8.4}{6} \frac{8.3}{25} \frac{10.2}{50}$

$\frac{3.5}{50} \frac{5.2}{22} \frac{6.3}{13} 6.3 \frac{6.3}{2} \frac{6.9}{3} \frac{6.9}{5} \frac{2.9}{10} \frac{2.0}{14} \frac{2.1}{34} \frac{3.4}{50}$

$\frac{10.3}{50} \frac{10.3}{39} \frac{10.4}{20} \frac{11.0}{14} 10.8 \frac{10.9}{4} \frac{4.6}{12} \frac{3.0}{16} \frac{2.0}{40} \frac{1.3}{50}$

$\frac{10.6}{50} \frac{10.0}{37} \frac{10.3}{22} \frac{12.1}{18} \frac{11.6}{12} 11.7 \frac{11.0}{3} \frac{3.3}{12} \frac{1.7}{17} \frac{1.0}{50}$

$\frac{12.9}{50} \frac{13.8}{23} \frac{14.8}{19} \frac{14.6}{12} 14.2 \frac{14.7}{3} \frac{11.1}{8} \frac{8.1}{12} \frac{5.9}{25} \frac{4.4}{50}$

$\frac{7.7}{50} \frac{8.9}{27} \frac{9.7}{14} 9.4 \frac{7.8}{7} \frac{4.7}{10} \frac{1.4}{30} \frac{1.9}{50}$

987.32

77.6

+37

S. Side of Old Farm Ent.

T.P.

321

972.19

1334

973.98

14

73.8

+50

71.8

13.M.

10.71 966.48

966.47

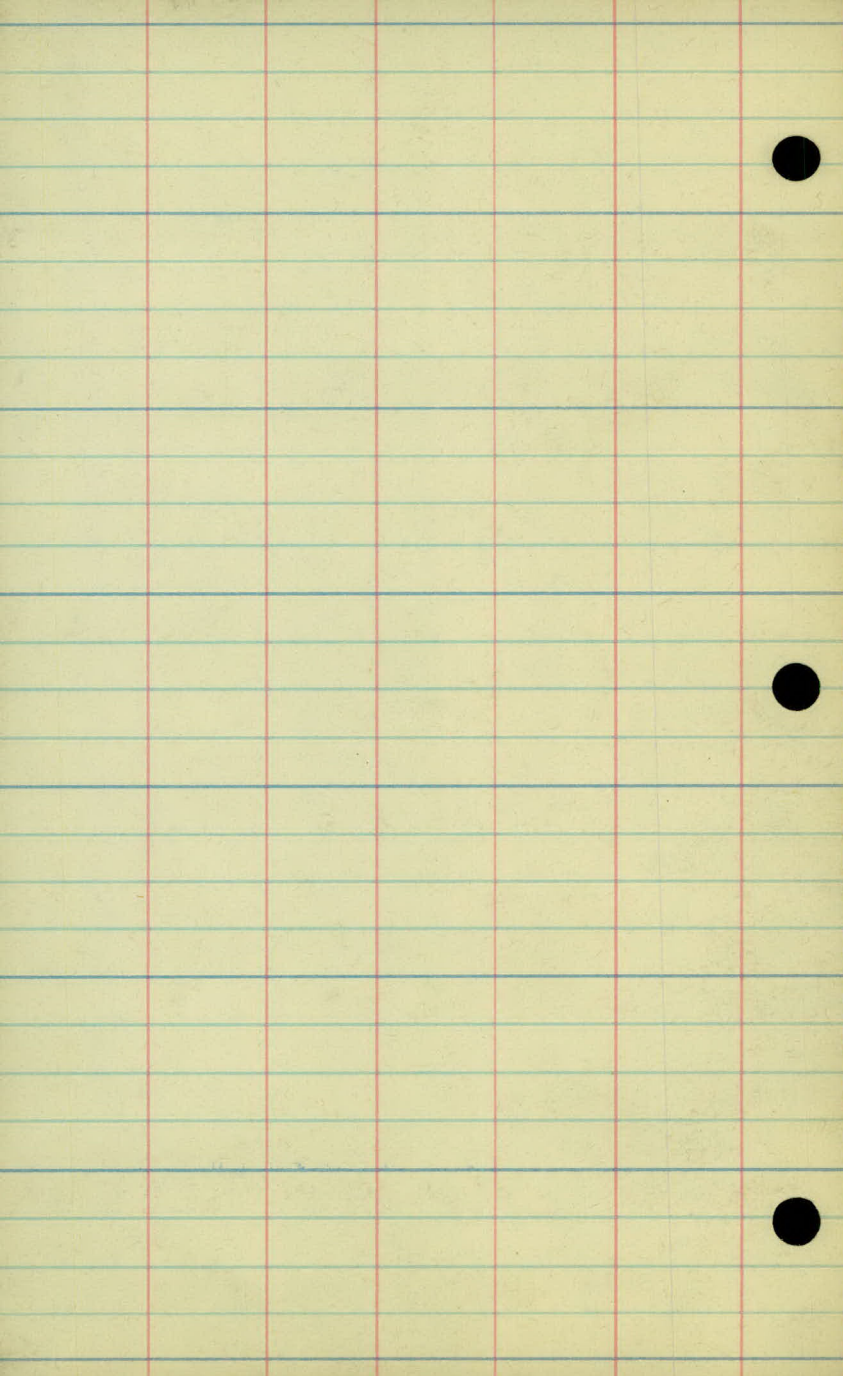
Left. ± Right

$\frac{82}{50}$ $\frac{94}{27}$ $\frac{102}{14}$ $\frac{97}{9.7}$ $\frac{87}{3}$ $\frac{7.2}{18}$ $\frac{5.0}{50}$

$\frac{7.8}{50}$ $\frac{7.4}{37}$ $\frac{65}{23}$ $\frac{34}{18}$ $\frac{34}{34}$ $\frac{4.0}{2}$ $\frac{4.1}{5}$ $\frac{4.8}{8}$ $\frac{4.5}{16}$ $\frac{0.7}{32}$ $\frac{0.0}{38}$ $\frac{+3}{50}$

$\frac{133}{50}$ $\frac{131}{28}$ $\frac{103}{21}$ $\frac{69}{18}$ $\frac{58}{16}$ $\frac{54}{5.4}$ $\frac{107}{8}$ $\frac{111}{15}$ $\frac{3.7}{37}$ $\frac{3.4}{47}$

Top Rock 95' Left. 18+90



Spike in 12" Oak 20' Rt Sta 43+08.

(2-23-32 A.M.)

Monit, End Project N.W. Cor.
Spike in 10" Oak 60' Lt Sta 52+56

B.M.# 6.83 973.07^{30.}

966.24^{34.} 966.47

15

69.6

+50

68.8

16

68.5

T.P. 8.86 976.91^{7.14} 5.02 968.05^{28.}

+68

67.8

17

67.4

+22

67.1

T.P. 3.69 971.74^{97.} 8.86 968.05^{28.}

+50

67.0

18

67.4

+34

68.1

B.M. 11.22 977.46^{69.} 5.47 966.27^{50.}

966.47

19

67.9

+50

70.9

B.M. 11.22 966.24^{47.}

B.M.# 13.76 980.00^{23.}

10+00

71.7

+50

73.8

2-25-32 Fair cloudy. 38°F A.M.

(Back feels good) LEFT & RIGHT

9 a.m. Top of Rock 95' Lt Sta 18+90

$\frac{11.9}{50}$ $\frac{9.5}{23}$ $\frac{7.7}{20}$ $\frac{3.8}{16}$ $\frac{3.4}{7}$ $\frac{4.2}{37}$ $\frac{11.1}{2}$ $\frac{10.6}{12}$ $\frac{8.7}{39}$ $\frac{8.7}{50}$

$\frac{12.2}{50}$ $\frac{12.2}{32}$ $\frac{11.7}{24}$ $\frac{5.4}{17}$ $\frac{4.6}{13}$ $\frac{6.1}{4.5}$ $\frac{10.5}{6}$ $\frac{10.8}{13}$ $\frac{9.1}{31}$ $\frac{9.1}{50}$

$\frac{11.6}{50}$ $\frac{11.4}{38}$ $\frac{10.5}{24}$ $\frac{6.9}{19}$ $\frac{5.1}{14}$ $\frac{5.4}{4.8}$ $\frac{7.5}{9}$ $\frac{6.9}{13}$ $\frac{3.9}{30}$ $\frac{3.9}{50}$

$\frac{4.5}{50}$ $\frac{3.5}{35}$ $\frac{2.4}{27}$ $\frac{9.5}{19}$ $\frac{9.6}{14}$ $\frac{9.3}{9.3}$ $\frac{9.5}{10}$ $\frac{3.5}{19}$ $\frac{3.7}{28}$ $\frac{3.2}{41}$ $\frac{2.2}{50}$

$\frac{8.5}{50}$ $\frac{8.4}{32}$ $\frac{7.6}{26}$ $\frac{11.4}{21}$ $\frac{10.2}{15}$ $\frac{10.5}{9.7}$ $\frac{5.6}{12}$ $\frac{4.9}{19}$ $\frac{3.9}{34}$ $\frac{3.9}{50}$

$\frac{14.0}{50}$ $\frac{14.0}{33}$ $\frac{13.0}{23}$ $\frac{11.4}{19}$ $\frac{10.6}{16}$ $\frac{10.2}{10.0}$ $\frac{10.8}{6}$ $\frac{9.9}{13}$ $\frac{9.1}{16}$ $\frac{7.1}{32}$ $\frac{7.1}{50}$

$\frac{14.2}{50}$ $\frac{12.7}{28}$ $\frac{10.3}{22}$ $\frac{5.6}{17}$ $\frac{5.3}{50}$ $\frac{6.5}{7}$ $\frac{6.4}{11}$ $\frac{4.6}{22}$ $\frac{4.6}{50}$

$\frac{14.4}{50}$ $\frac{11.9}{31}$ $\frac{8.5}{23}$ $\frac{5.4}{20}$ $\frac{5.1}{16}$ $\frac{4.6}{4.6}$ $\frac{5.4}{10}$ $\frac{6.5}{17}$ $\frac{5.4}{33}$ $\frac{4.1}{50}$

$\frac{11.2}{50}$ $\frac{9.4}{33}$ $\frac{7.8}{26}$ $\frac{5.2}{21}$ $\frac{4.5}{18}$ $\frac{3.7}{3.9}$ $\frac{4.0}{3}$ $\frac{4.4}{8}$ $\frac{3.2}{12}$ $\frac{4.0.7}{21}$ $\frac{4.0.7}{50}$

#3

$\frac{7.8}{50}$ $\frac{6.5}{31}$ $\frac{6.9}{27}$ $\frac{8.6}{25}$ $\frac{9.0}{20}$ $\frac{8.4}{18}$ $\frac{7.8}{7.8}$ $\frac{8.3}{6}$ $\frac{6.1}{10}$ $\frac{1.4}{16}$ $\frac{0.2}{21}$ $\frac{0.2}{50}$

$\frac{6.5}{50}$ $\frac{5.6}{32}$ $\frac{6.1}{29}$ $\frac{7.3}{27}$ $\frac{7.6}{18}$ $\frac{7.1}{16}$ $\frac{6.9}{6.8}$ $\frac{7.4}{6}$ $\frac{7.0}{11}$ $\frac{6.2}{15}$ $\frac{5.1}{35}$ $\frac{5.1}{50}$

#3 11:45 ("Oh my back") (1 P.M. Back feeling good)

$\frac{12.2}{50}$ $\frac{11.1}{35}$ $\frac{9.0}{23}$ $\frac{9.0}{20}$ $\frac{8.4}{18}$ $\frac{9.1}{8.5}$ $\frac{13.0}{9}$ $\frac{13.1}{15}$ $\frac{13.5}{29}$ $\frac{13.5}{50}$

$\frac{11.7}{50}$ $\frac{7.4}{31}$ $\frac{6.8}{24}$ $\frac{7.3}{21}$ $\frac{6.7}{19}$ $\frac{6.6}{6.4}$ $\frac{7.2}{10}$ $\frac{6.1}{12}$ $\frac{7.7}{33}$ $\frac{8.3}{50}$

	+ H.I. -		Elev
21+00		980.00 ^{22.2}	75.3
+50			75.8
22+00			76.3
22+29			76.8
+68			77.7
23			79.1
T.P	2.06	978.96 ^{9.19} 3.10	77.13 976.90
22+29			
+68			
23+00			
TP	13.55	990.68 ^{7.13} 2.06	976.90
+50			81.8
24+00			84.2
T.P.		8.97	981.71 ✓

$$\begin{array}{r} 5.0 \quad 2.7 \quad 5.1 \quad 5.3 \quad 5.0 \\ 50 \quad 32 \quad 24 \quad 21 \quad 16 \end{array} \quad \begin{array}{r} 4.8 \quad 5.3 \quad 5.0 \quad 2.1 \quad 2.8 \\ 5 \quad 7 \quad 12 \quad 15 \quad 50 \end{array}$$

$$\begin{array}{r} 1.7 \quad 0.7 \quad 1.6 \quad 4.5 \quad 4.7 \quad 4.1 \quad 4.4 \\ 50 \quad 39 \quad 33 \quad 26 \quad 22 \quad 21 \quad 18 \end{array} \quad \begin{array}{r} 4.5 \quad 5.0 \quad 1.4 \quad 3.2 \quad 3.9 \\ 5 \quad 10 \quad 15 \quad 39 \quad 50 \end{array}$$

$$\begin{array}{r} 5.8 \quad 5.0 \quad 6.0 \quad 6.0 \quad 4.3 \quad 3.9 \\ 50 \quad 32 \quad 27 \quad 23 \quad 18 \quad 13 \end{array} \quad \begin{array}{r} 5.1 \quad 8.2 \quad 10.0 \quad 11.5 \quad 11.0 \\ 9 \quad 15 \quad 23 \quad 37 \quad 50 \end{array}$$

$$\begin{array}{r} 3.8 \quad 4.7 \\ 16 \quad 34 \quad 6 \end{array}$$

$$\begin{array}{r} 4.6 \quad 2.6 \quad 2.8 \quad 4.0 \\ 17 \quad 13 \quad 2.5 \quad 4 \quad 7 \end{array}$$

$$\begin{array}{r} 1.5 \quad 1.2 \quad 2.7 \\ 13 \quad 1.1 \quad 3 \quad 7 \end{array}$$

$$\begin{array}{r} 10.2 \quad 10.3 \quad 2.4 \quad 15.2 \quad 13.9 \quad 13.1 \\ 50 \quad 28 \quad 2.5 \quad 38 \quad 50 \end{array}$$

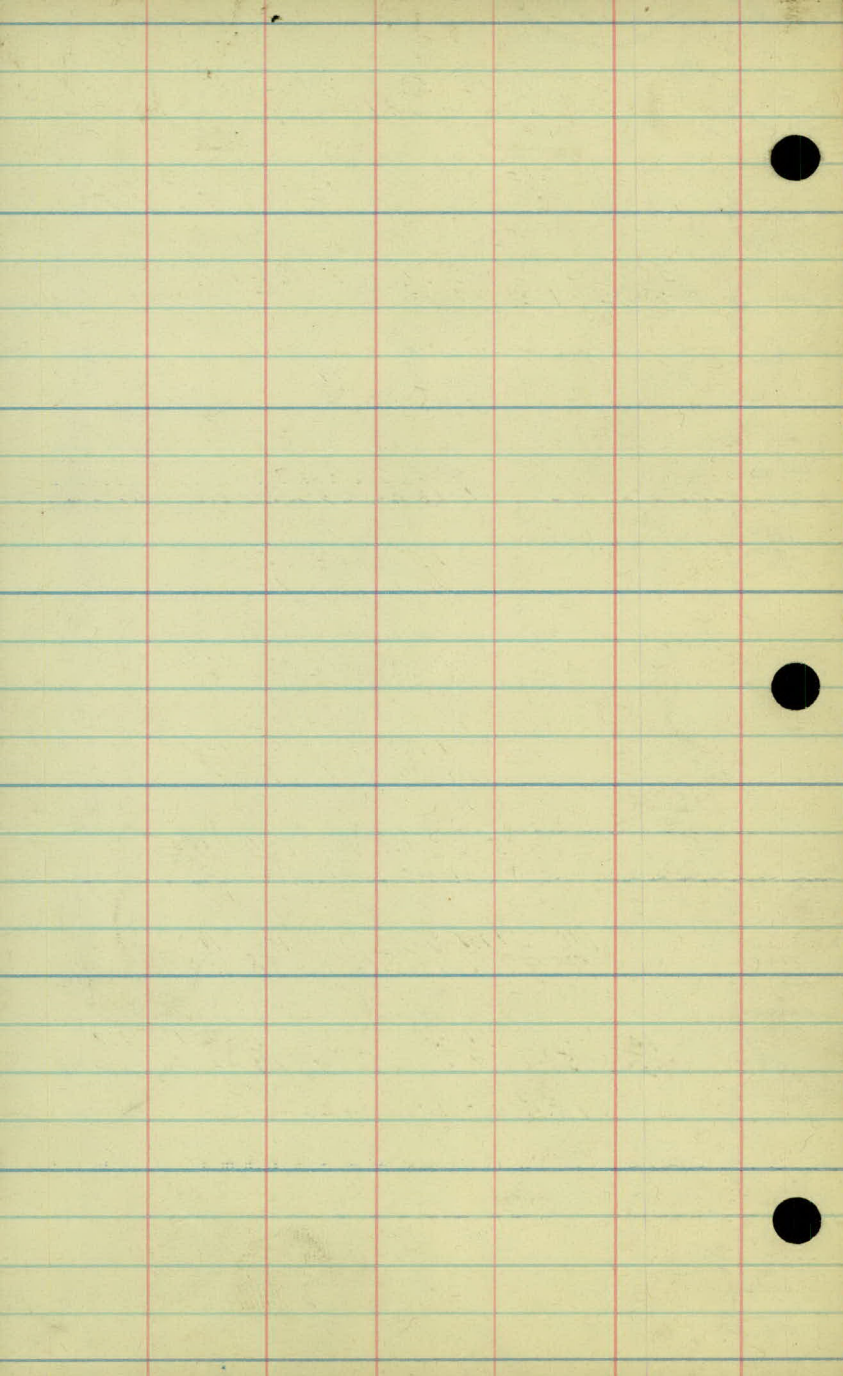
$$\begin{array}{r} 18.7 \quad 16.5 \quad 1.5 \quad 14.5 \quad 16.1 \quad 15.2 \\ 50 \quad 34 \quad 27 \quad 39 \quad 50 \end{array}$$

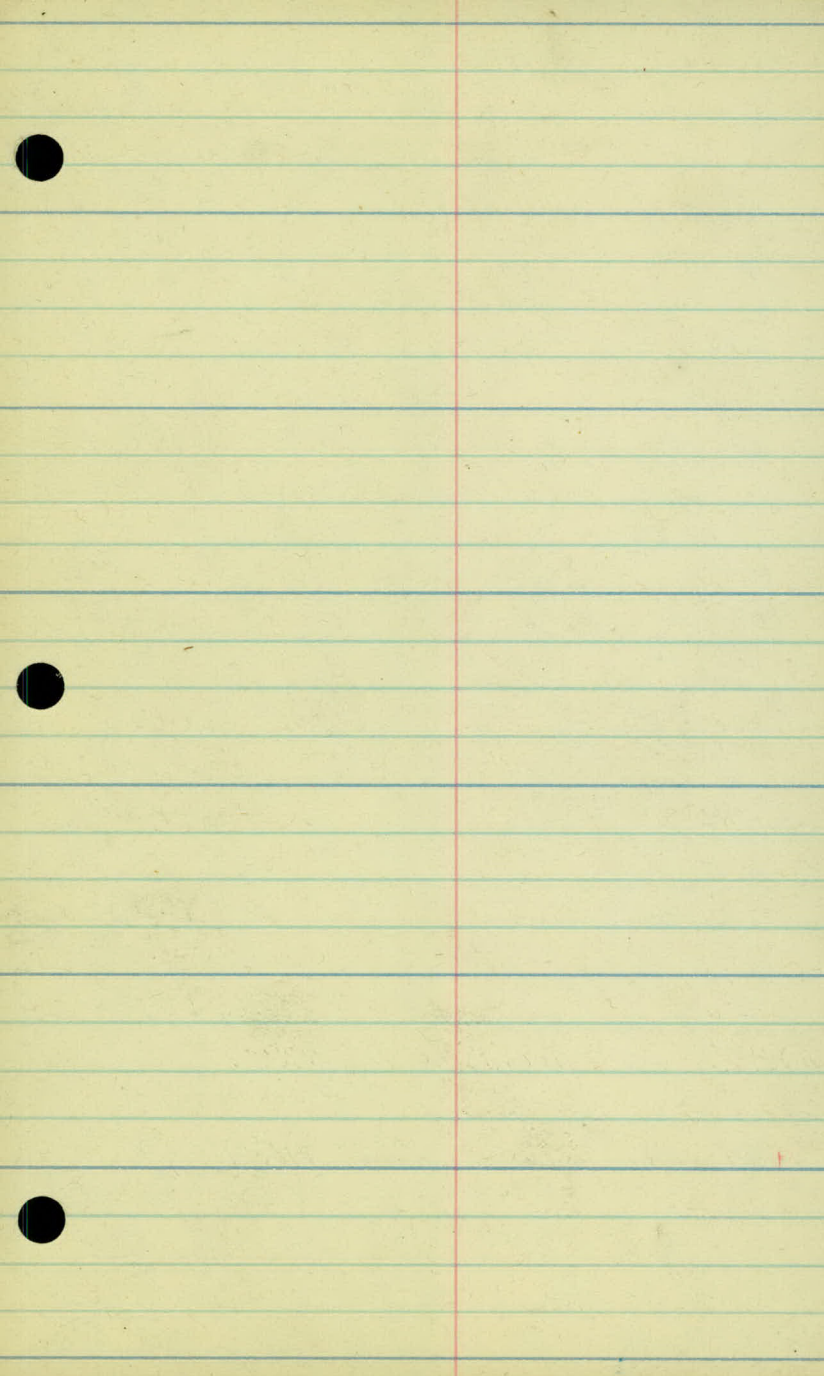
$$\begin{array}{r} 15.5 \quad 13.0 \quad 7.5 \quad 0.1 \quad 10.5 \quad 12.1 \quad 11.2 \\ 50 \quad 31 \quad 21 \quad 21 \quad 32 \quad 50 \end{array}$$

$$\begin{array}{r} 18.0 \quad 15.9 \quad 17.8 \quad 9.1 \quad 10.1 \quad 10.8 \quad 11.0 \\ 50 \quad 34 \quad 21 \quad 13 \quad 8.9 \quad 11 \quad 30 \end{array} \quad \begin{array}{r} 50 \end{array}$$

$$\begin{array}{r} 10.2 \quad 6.3 \quad 8.0 \quad 7.9 \quad 6.6 \quad 6.4 \quad 6.9 \quad 5.6 \quad 1.2 \quad 1.7 \\ 50 \quad 25 \quad 21 \quad 18 \quad 12 \quad 6.5 \quad 5 \quad 13 \quad 16 \quad 21 \end{array} \quad \begin{array}{r} 50 \end{array}$$

Nail in F.P. Lt Sta 23+65





Sta.	+	H.I.	-	Elev
B.M.	13.44	995.15 ✓		981.71 ✓
24+50				987.6 .
T.P.	11.88	1004.93 ✓	2.10	993.05 ✓
25				90.6 .
+50				93.3 .
26				95.9 .
+14				96.5 .
+22				96.7 .
+36				97.1 .
+46				97.5 .
27				98.0 .
+50				97.7 .
(New) B.M.	5.29	1004.18 ✓	6.04	998.89 ✓
28				95.9 .
13 M			5.29	998.89 ✓

2-27-32 (Warm Fair) 45°F (Rock 2)

LEFT & RIGHT

Nail in F.P.

$\frac{7.2}{50}$ $\frac{3.3}{24}$ $\frac{6.0}{21}$ $\frac{8.0}{17}$ 7.6 $\frac{7.5}{7}$ $\frac{7.9}{11}$ $\frac{6.7}{17}$ $\frac{1.3}{24}$ $\frac{3.5}{50}$

$\frac{7.1}{50}$ $\frac{6.6}{28}$ $\frac{11.0}{23}$ $\frac{14.7}{15}$ 14.3 $\frac{14.2}{7}$ $\frac{14.7}{14}$ $\frac{8.8}{21}$ $\frac{11.6}{50}$

$\frac{2.6}{50}$ $\frac{3.9}{35}$ $\frac{4.4}{24}$ $\frac{10.2}{18}$ $\frac{12.0}{14}$ $\frac{11.7}{12}$ 11.6 $\frac{11.6}{6}$ $\frac{12.3}{12}$ $\frac{11.4}{16}$ $\frac{8.2}{19}$ $\frac{9.3}{33}$ $\frac{10.9}{50}$

$\frac{1.6}{50}$ $\frac{2.4}{28}$ $\frac{3.3}{25}$ $\frac{7.0}{21}$ $\frac{9.5}{16}$ $\frac{9.2}{12}$ 9.0 $\frac{9.0}{6}$ $\frac{9.9}{12}$ $\frac{8.7}{15}$ $\frac{5.3}{18}$ $\frac{5.5}{37}$ $\frac{5.4}{50}$

$\frac{1.7}{50}$ $\frac{1.7}{41}$ $\frac{2.1}{28}$ $\frac{2.8}{24}$ $\frac{6.7}{21}$ $\frac{9.0}{16}$ $\frac{8.7}{13}$ 8.4 $\frac{8.6}{8}$ $\frac{8.9}{11}$ $\frac{7.4}{15}$ $\frac{4.3}{17}$ $\frac{3.6}{36}$ $\frac{3.4}{50}$

$\frac{10.8}{50}$ $\frac{10.5}{33}$ $\frac{9.5}{21}$ $\frac{8.6}{13}$ 8.2 $\frac{8.3}{8}$ $\frac{8.6}{11}$ $\frac{6.9}{15}$ $\frac{3.3}{17}$ $\frac{3.5}{32}$ $\frac{3.3}{50}$

$\frac{11.7}{50}$ $\frac{9.9}{33}$ $\frac{9.4}{23}$ $\frac{8.0}{11}$ 7.8 $\frac{8.1}{8}$ $\frac{8.3}{11}$ $\frac{7.3}{14}$ $\frac{3.8}{17}$ $\frac{3.6}{32}$ $\frac{3.0}{50}$

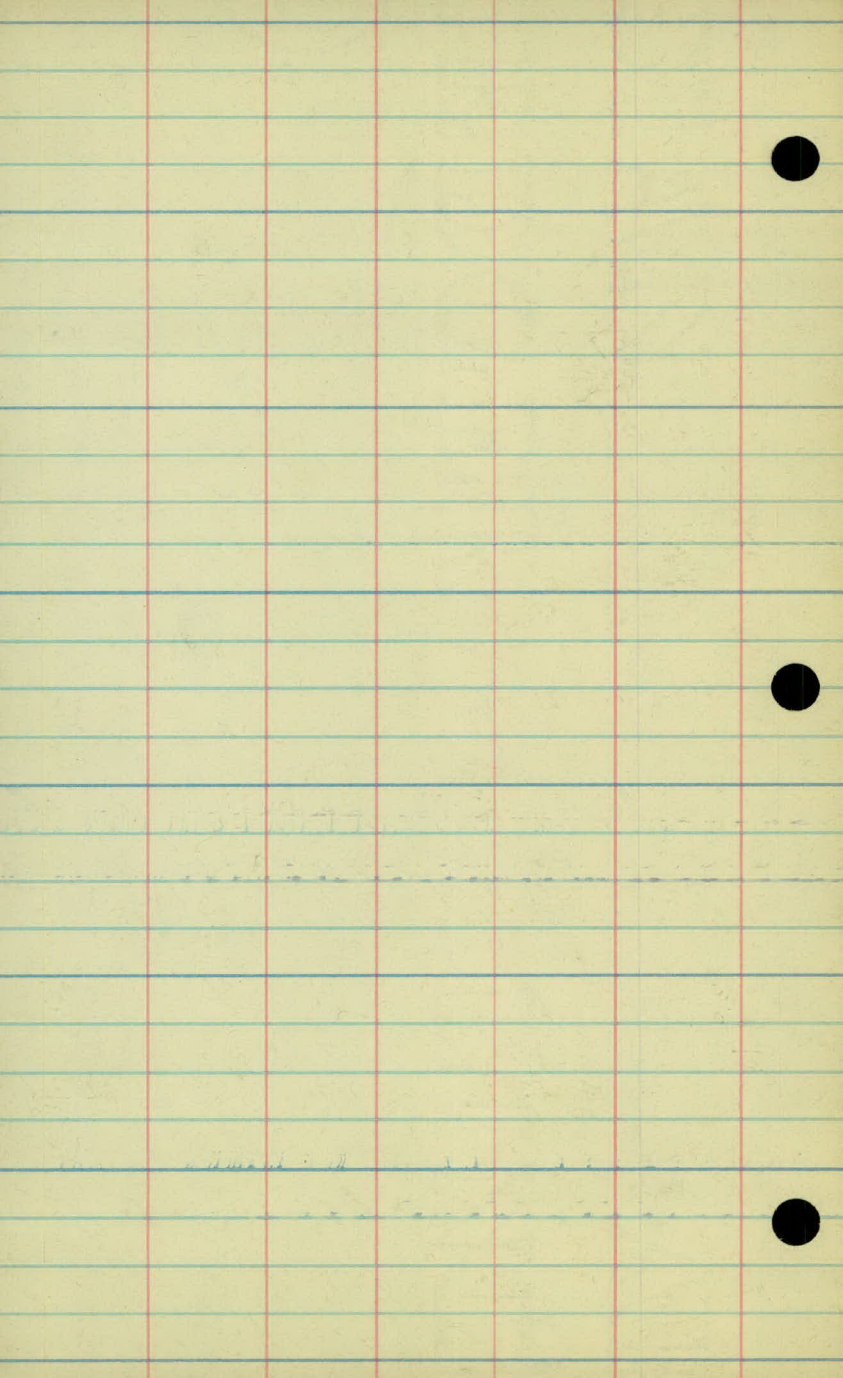
$\frac{1.2}{50}$ $\frac{1.8}{27}$ $\frac{6.2}{19}$ $\frac{7.8}{13}$ 7.4 $\frac{7.7}{8}$ $\frac{7.9}{11}$ $\frac{6.4}{14}$ $\frac{3.3}{17}$ $\frac{3.6}{32}$ $\frac{3.2}{50}$

$\frac{2.0}{50}$ $\frac{2.0}{25}$ $\frac{6.4}{19}$ $\frac{7.4}{16}$ $\frac{7.2}{11}$ 6.9 $\frac{7.1}{7}$ $\frac{7.9}{11}$ $\frac{7.3}{14}$ $\frac{3.9}{17}$ $\frac{5.1}{28}$ $\frac{5.3}{50}$

$\frac{3.3}{50}$ $\frac{3.3}{27}$ $\frac{4.4}{25}$ $\frac{4.9}{18}$ $\frac{7.9}{14}$ $\frac{7.7}{11}$ 7.2 $\frac{7.6}{8}$ $\frac{8.6}{12}$ $\frac{8.6}{14}$ $\frac{6.5}{17}$ $\frac{7.6}{24}$ $\frac{9.5}{50}$

Top of Rock 67' Rt Sta. 26+95

$\frac{1.3}{50}$ $\frac{4.2}{22}$ $\frac{5.3}{17}$ $\frac{7.6}{15}$ $\frac{8.5}{10}$ 8.3 $\frac{8.5}{8}$ $\frac{9.4}{11}$ $\frac{9.0}{14}$ $\frac{7.9}{16}$ $\frac{8.9}{23}$ $\frac{12.6}{50}$



2-29-32

X Sections

Sta 28+50 To 37+00 Inc.

Snelling Ave.
County Road "G"
To
One Mile North.

B.M. 7.18 1006.07 ✓

998.89

28+50

94.2

29

91.8

+50

30

T.P. 0.16 993.05 ✓ 13.18 992.89 ✓

28+50

29

+50

89.2

30

86.2

+50

83.7

T.P. 10.94 1002.10 ✓ 1.89 991.16 ✓

+50

31

+50

+70

Fair 38°F Little windy.

LEFT & RIGHT

Top Rock 67' RT Sta. 26+95

$$\begin{array}{r} 3.6 \\ 50 \end{array} \quad \begin{array}{r} 6.5 \\ 26 \end{array} \quad \begin{array}{r} 8.3 \\ 15 \end{array} \quad \begin{array}{r} 10.9 \\ 13 \end{array} \quad \begin{array}{r} 12.5 \\ 10 \end{array} \quad \begin{array}{r} 12.1 \\ 7 \end{array} \quad 11.9 \quad \begin{array}{r} 12.3 \\ 9 \end{array} \quad \begin{array}{r} 12.9 \\ 11 \end{array} \quad \begin{array}{r} 12.5 \\ 16 \end{array}$$

$$\begin{array}{r} 1.1 \\ 50 \end{array} \quad \begin{array}{r} 2.7 \\ 34 \end{array} \quad \begin{array}{r} 4.6 \\ 30 \end{array} \quad \begin{array}{r} 5.4 \\ 20 \end{array} \quad \begin{array}{r} 12.9 \\ 12 \end{array} \quad \begin{array}{r} 14.8 \\ 8 \end{array} \quad 14.3 \quad \begin{array}{r} 14.5 \\ 8 \end{array} \quad \begin{array}{r} 15.1 \\ 15 \end{array}$$

over
Ht.

$$\begin{array}{r} +0.2 \\ 50 \end{array} \quad \begin{array}{r} 3.3 \\ 33 \end{array} \quad \begin{array}{r} 6.6 \\ 30 \end{array} \quad \begin{array}{r} 7.1 \\ 24 \end{array} \quad (14.9)$$

$$\begin{array}{r} 3.6 \\ 50 \end{array} \quad \begin{array}{r} 8.9 \\ 34 \end{array} \quad \begin{array}{r} 11.4 \\ 30 \end{array} \quad \begin{array}{r} 12.0 \\ 20 \end{array} \quad (14.9)$$

$$(1.1) \quad \begin{array}{r} 2.7 \\ 28 \end{array} \quad \begin{array}{r} 8.0 \\ 50 \end{array}$$

$$(-1.3) \quad \begin{array}{r} 8.1 \\ 30 \end{array} \quad \begin{array}{r} 13.6 \\ 50 \end{array}$$

$$\begin{array}{r} 1.8 \\ 14 \end{array} \quad \begin{array}{r} 3.6 \\ 11 \end{array} \quad 3.9 \quad \begin{array}{r} 4.4 \\ 9 \end{array} \quad \begin{array}{r} 10.0 \\ 22 \end{array} \quad \text{---}$$

$$\begin{array}{r} 5.6 \\ 16 \end{array} \quad \begin{array}{r} 6.9 \\ 14 \end{array} \quad \begin{array}{r} 6.7 \\ 10 \end{array} \quad 6.9 \quad \begin{array}{r} 7.3 \\ 6 \end{array} \quad \text{---}$$

$$\begin{array}{r} 8.4 \\ 16 \end{array} \quad \begin{array}{r} 9.6 \\ 11 \end{array} \quad \begin{array}{r} 9.3 \\ 9 \end{array} \quad 9.4 \quad \begin{array}{r} 9.7 \\ 6 \end{array} \quad \begin{array}{r} 11.9 \\ 11 \end{array} \quad \text{---}$$

$$\begin{array}{r} 1.5 \\ 50 \end{array} \quad \begin{array}{r} 7.4 \\ 34 \end{array} \quad \begin{array}{r} 10.5 \\ 30 \end{array} \quad \begin{array}{r} 11.2 \\ 21 \end{array} \quad (18.4)$$

$$\begin{array}{r} 2.1 \\ 50 \end{array} \quad \begin{array}{r} 9.1 \\ 32 \end{array} \quad \begin{array}{r} 11.5 \\ 29 \end{array} \quad \begin{array}{r} 11.7 \\ 26 \end{array} \quad (20.4) \quad \text{---}$$

$$\begin{array}{r} 2.8 \\ 50 \end{array} \quad \begin{array}{r} 7.8 \\ 33 \end{array} \quad \begin{array}{r} 11.1 \\ 29 \end{array} \quad (21.3) \quad \text{---}$$

$$\begin{array}{r} 2.0 \\ 50 \end{array} \quad \begin{array}{r} 8.3 \\ 33 \end{array} \quad (21.7) \quad \text{---}$$

+ H.I. -
1002.10

32
T.P. 0.20 991.31 10.99 991.11
B.M. 6.96 984.71 13.53 977.78 977.75
29+50

30
B.M. 4.58 982.33 6.96 977.75
+50

31 81.7

+50 80.8

+70 80.4

32 79.8

+50 78.8

33 77.9

+50 77.0

34 76.0
T.P. 12.20 987.20 7.33 975.00

LEFT & RIGHT

Top Bent

$$\begin{array}{r} 0.0 \\ 60 \end{array} \quad \begin{array}{r} 7.4 \\ 50 \end{array}$$

$$\begin{array}{r} 22.3 \\ 50 \end{array}$$

$$\begin{array}{r} +5.5 \\ 50 \end{array} \quad \begin{array}{r} 10.5 \\ 50 \end{array}$$

$$\begin{array}{r} +1.5 \\ 21 \end{array} \quad \begin{array}{r} 18.6 \\ 50 \end{array}$$

spr in 18" Pop 33' Rt Sta 31 + 45

$$\begin{array}{r} +1.4 \\ 23 \end{array} \quad \begin{array}{r} 11.3 \\ 30 \end{array} \quad \begin{array}{r} 18.4 \\ 50 \end{array}$$

over H.I. →

$$\begin{array}{r} +1.0 \\ 18 \end{array} \quad \begin{array}{r} 0.5 \\ 11 \end{array} \quad \begin{array}{r} 1.0 \\ 5 \end{array} \quad \begin{array}{r} 3.2 \\ 19 \end{array} \quad \begin{array}{r} 13.3 \\ 36 \end{array} \quad \begin{array}{r} 15.4 \\ 50 \end{array}$$

$$\begin{array}{r} +1.8 \\ 19 \end{array} \quad \begin{array}{r} 1.3 \\ 12 \end{array} \quad \begin{array}{r} 2.6 \\ 9 \end{array} \quad \begin{array}{r} 8.6 \\ 35 \end{array} \quad \begin{array}{r} 9.2 \\ 50 \end{array}$$

$$\begin{array}{r} 0.0 \\ 22 \end{array} \quad \begin{array}{r} 1.4 \\ 17 \end{array} \quad \begin{array}{r} 1.6 \\ 12 \end{array} \quad \begin{array}{r} 2.5 \\ 5 \end{array} \quad \begin{array}{r} 4.9 \\ 13 \end{array} \quad \begin{array}{r} 9.0 \\ 32 \end{array} \quad \begin{array}{r} 12.6 \\ 50 \end{array}$$

$$\begin{array}{r} 2.6 \\ 26 \end{array} \quad \begin{array}{r} 3.0 \\ 21 \end{array} \quad \begin{array}{r} 2.6 \\ 14 \end{array} \quad \begin{array}{r} 3.0 \\ 5 \end{array} \quad \begin{array}{r} 4.9 \\ 11 \end{array} \quad \begin{array}{r} 9.2 \\ 29 \end{array} \quad \begin{array}{r} 14.1 \\ 50 \end{array}$$

over H.I.

$$\begin{array}{r} +8.1 \\ 50 \end{array} \quad \begin{array}{r} 0.0 \\ 39 \end{array} \quad \begin{array}{r} 1.9 \\ 36 \end{array} \quad \begin{array}{r} 4.0 \\ 21 \end{array} \quad \begin{array}{r} 3.5 \\ 16 \end{array} \quad \begin{array}{r} 3.1 \\ 6 \end{array} \quad \begin{array}{r} 4.0 \\ 35 \end{array} \quad \begin{array}{r} 7.4 \\ 15 \end{array} \quad \begin{array}{r} 7.7 \\ 19 \end{array} \quad \begin{array}{r} 16.6 \\ 40 \end{array} \quad \begin{array}{r} 19.1 \\ 50 \end{array}$$

$$\begin{array}{r} +6.0 \\ 50 \end{array} \quad \begin{array}{r} 0.0 \\ 38 \end{array} \quad \begin{array}{r} 3.8 \\ 29 \end{array} \quad \begin{array}{r} 4.6 \\ 21 \end{array} \quad \begin{array}{r} 4.3 \\ 16 \end{array} \quad \begin{array}{r} 4.0 \\ 6 \end{array} \quad \begin{array}{r} 4.8 \\ 3 \end{array} \quad \begin{array}{r} 6.4 \\ 10 \end{array} \quad \begin{array}{r} 6.9 \\ 20 \end{array} \quad \begin{array}{r} 14.2 \\ 42 \end{array} \quad \begin{array}{r} 17.0 \\ 50 \end{array}$$

$$\begin{array}{r} +12.0 \\ 50 \end{array} \quad \begin{array}{r} +1.0 \\ 43 \end{array} \quad \begin{array}{r} +6.5 \\ 41 \end{array} \quad \begin{array}{r} 0.0 \\ 32 \end{array} \quad \begin{array}{r} 3.1 \\ 28 \end{array} \quad \begin{array}{r} 5.4 \\ 18 \end{array} \quad \begin{array}{r} 5.0 \\ 7 \end{array} \quad \begin{array}{r} 5.4 \\ 4 \end{array} \quad \begin{array}{r} 6.9 \\ 11 \end{array} \quad \begin{array}{r} 8.9 \\ 26 \end{array} \quad \begin{array}{r} 13.6 \\ 41 \end{array} \quad \begin{array}{r} 15.8 \\ 50 \end{array}$$

+2

$$\begin{array}{r} +6.6 \\ 50 \end{array} \quad \begin{array}{r} +4.4 \\ 42 \end{array} \quad \begin{array}{r} 0.0 \\ 38 \end{array} \quad \begin{array}{r} 5.6 \\ 30 \end{array} \quad \begin{array}{r} 6.7 \\ 21 \end{array} \quad \begin{array}{r} 6.0 \\ 9 \end{array} \quad \begin{array}{r} 7.2 \\ 7 \end{array} \quad \begin{array}{r} 12.5 \\ 17 \end{array} \quad \begin{array}{r} 15.7 \\ 28 \end{array} \quad \begin{array}{r} 23.2 \\ 50 \end{array}$$

Sta + H.I. - Elev
987.20 ✓

34 + 16 757

+50 747

35 744

+50 74.8

T.P. 0.85 ✓ 974.52 ✓ 13.53 973.67
34 + 16

+50

35

+50

T.P. 8.63 ✓ 982.30 ✓ 0.85 973.67
36 76.5

+50 79.0

37 81.7

T.P. 13.15 ✓ 994.72 ✓ 0.73 981.57
36 + 50

37
T.P. 13.15 ✓ 981.57

2-29-32

Back O.A. 2:30 PM

LEFT

±

RIGHT (Hells Kid)

$$\begin{array}{r} 0.0 \\ 50 \end{array} \begin{array}{r} 5.0 \\ 33 \end{array} \begin{array}{r} 11.9 \\ 27 \end{array} \begin{array}{r} 12.0 \\ 23 \end{array} \begin{array}{r} 11.6 \\ 19 \end{array} \begin{array}{r} 11.1 \\ 9 \end{array} \begin{array}{r} 12.2 \\ 6 \end{array}$$

$$\begin{array}{r} 2.9 \\ 50 \end{array} \begin{array}{r} 8.4 \\ 35 \end{array} \begin{array}{r} 13.2 \\ 30 \end{array} \begin{array}{r} 12.9 \\ 24 \end{array} \begin{array}{r} 12.2 \\ 20 \end{array} \begin{array}{r} 12.0 \\ 9 \end{array} \begin{array}{r} 13.2 \\ 4 \end{array}$$

$$\begin{array}{r} 6.2 \\ 50 \end{array} \begin{array}{r} 12.6 \\ 35 \end{array} \begin{array}{r} 13.9 \\ 34 \end{array} \begin{array}{r} 14.0 \\ 29 \end{array} \begin{array}{r} 12.7 \\ 20 \end{array} \begin{array}{r} 13.7 \\ 3 \end{array}$$

$$\begin{array}{r} 8.9 \\ 50 \end{array} \begin{array}{r} 13.3 \\ 38 \end{array} \begin{array}{r} 13.2 \\ 25 \end{array} \begin{array}{r} 12.2 \\ 19 \end{array} \begin{array}{r} 12.4 \\ 4 \end{array} \begin{array}{r} 13.5 \\ 4 \end{array}$$

$$\begin{array}{r} +11.2 \\ 20 \end{array} \begin{array}{r} 8.7 \\ 28 \end{array} \begin{array}{r} 11.0 \\ 50 \end{array} \begin{array}{r} 18.0 \\ 50 \end{array}$$

$$\begin{array}{r} +10.2 \\ 21 \end{array} \begin{array}{r} 12.1 \\ 24 \end{array} \begin{array}{r} 15.0 \\ 30 \end{array} \begin{array}{r} 18.0 \\ 50 \end{array} \begin{array}{r} 21.6 \\ 50 \end{array}$$

$$\begin{array}{r} -0.1 \\ 20 \end{array} \begin{array}{r} 13.0 \\ 26 \end{array} \begin{array}{r} 17.0 \\ 31 \end{array} \begin{array}{r} 17.9 \\ 38 \end{array} \begin{array}{r} 20.2 \\ 50 \end{array} \begin{array}{r} 20.8 \\ 50 \end{array}$$

$$\begin{array}{r} +10.3 \\ 14 \end{array} \begin{array}{r} 7.3 \\ 22 \end{array} \begin{array}{r} 14.8 \\ 50 \end{array} \begin{array}{r} 18.5 \\ 50 \end{array}$$

$$\begin{array}{r} +1.8 \\ 50 \end{array} \begin{array}{r} 0.8 \\ 35 \end{array} \begin{array}{r} 6.6 \\ 29 \end{array} \begin{array}{r} 6.6 \\ 23 \end{array} \begin{array}{r} 5.8 \\ 15 \end{array} \begin{array}{r} 5.5 \\ 7 \end{array} \begin{array}{r} 5.8 \\ 58 \end{array} \begin{array}{r} 6.9 \\ 7 \end{array} \begin{array}{r} 12.0 \\ 14 \end{array} \begin{array}{r} 15.7 \\ 30 \end{array} \begin{array}{r} 17.0 \\ 50 \end{array}$$

$$\begin{array}{r} 2.6 \\ 25 \end{array} \begin{array}{r} 4.3 \\ 20 \end{array} \begin{array}{r} 3.5 \\ 15 \end{array} \begin{array}{r} 3.1 \\ 7 \end{array} \begin{array}{r} 3.3 \\ 33 \end{array} \begin{array}{r} 4.0 \\ 9 \end{array} \begin{array}{r} 5.8 \\ 20 \end{array} \begin{array}{r} 10.6 \\ 50 \end{array}$$

$$\begin{array}{r} 0.0 \\ 29 \end{array} \begin{array}{r} 1.8 \\ 19 \end{array} \begin{array}{r} 0.9 \\ 13 \end{array} \begin{array}{r} 0.5 \\ 6 \end{array} \begin{array}{r} 0.6 \\ 5 \end{array} \begin{array}{r} 0.7 \\ 5 \end{array} \begin{array}{r} 2.3 \\ 18 \end{array} \begin{array}{r} 6.1 \\ 35 \end{array} \begin{array}{r} 9.8 \\ 50 \end{array}$$

Top Back 27 Lt Sta. 34.67

$$\begin{array}{r} 3.3 \\ 50 \end{array} \begin{array}{r} 6.2 \\ 35 \end{array}$$

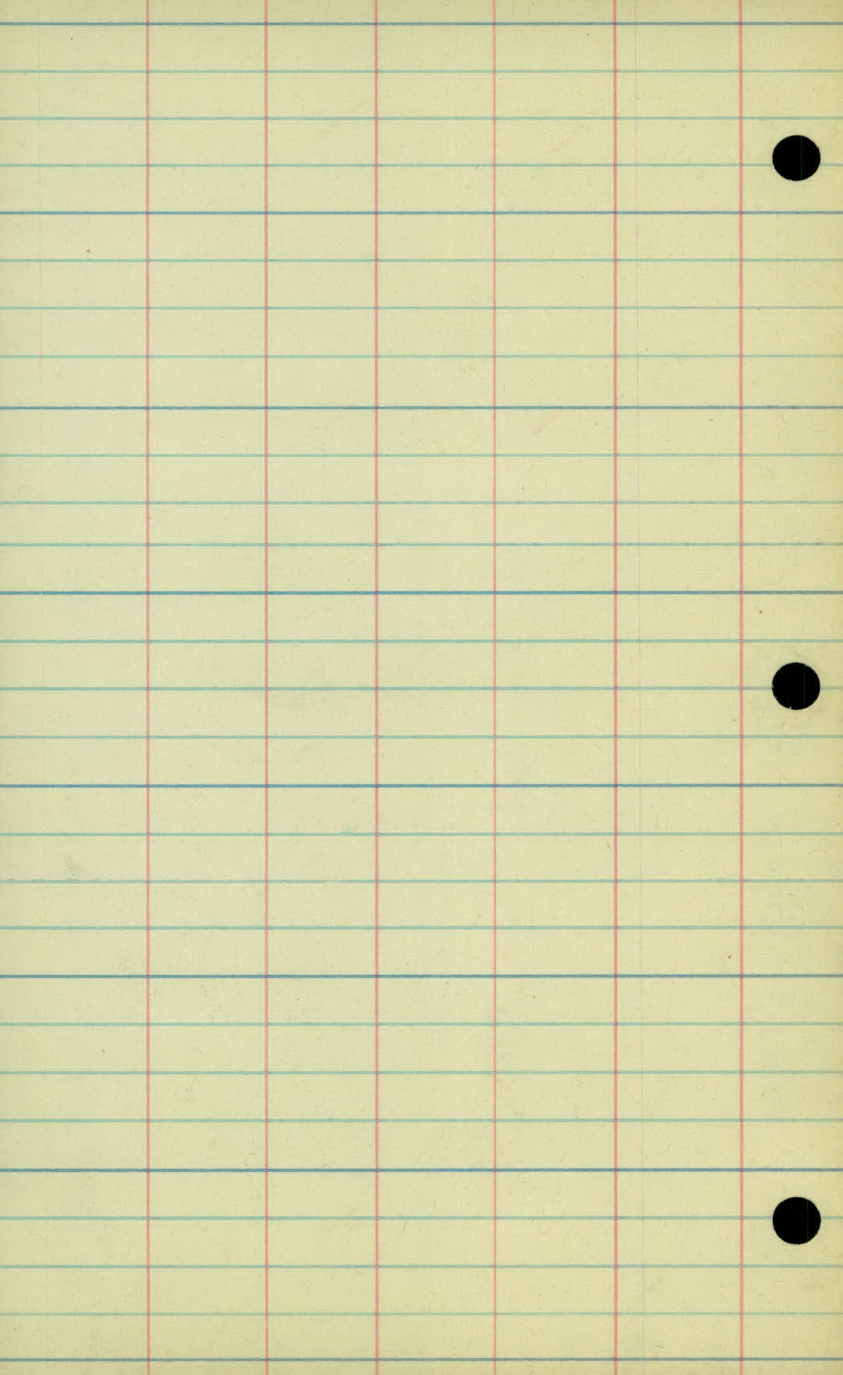
(15.1)

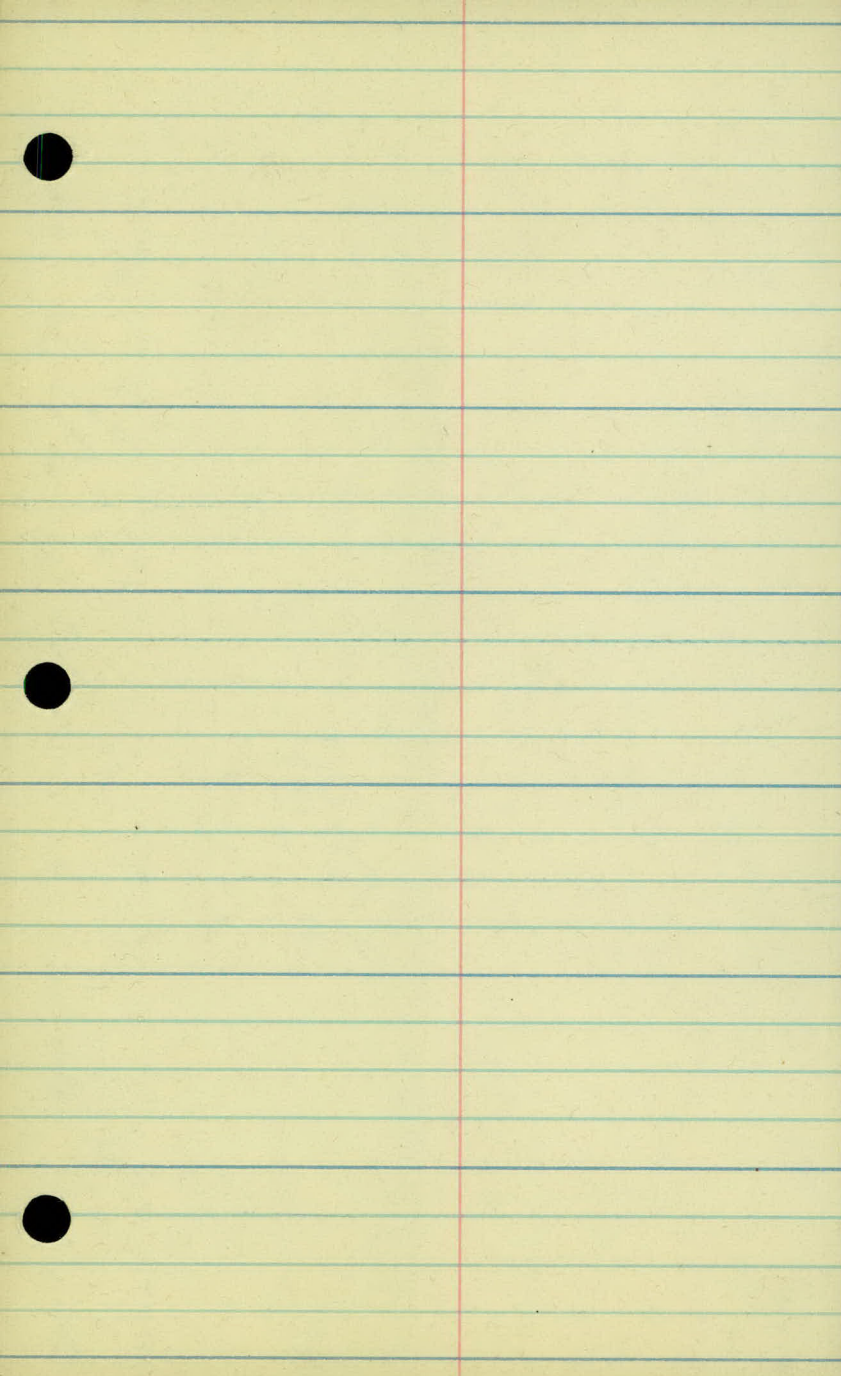
$$\begin{array}{r} \text{over H.I.} \\ +3.0 \\ 50 \end{array} \begin{array}{r} \text{Top Bank} \\ 0.0 \\ 48 \end{array}$$

(13.0)

SAME

4:30 (Oh my back)





T.P. 11.54 993.11 981.57
37+50 84.2

38 85.9

+50 87.7

39 89.8

+50 91.7

T.P. 10.56 1003.45 0.22 992.89
40 93.9

+50 96.0

41 98.8

+50 01.4

T.P. 12.53 1015.63 0.35 1003.10
B.M. 5.58 1015.62 5.57 1010.06 1010.04

42 04.1

+50 07.5

43 11.4

B.M. 12.52 1022.56 5.58 1010.04

3-2-52 Cloudy 32°F. 9 AM. Breeze 15 OK.

LEFT & RIGHT

Top of rock 27' Lt Sta 36+67

$\frac{+7.0}{50}$ $\frac{+47.0}{42}$ $\frac{0.0}{36}$ $\frac{9.2}{26}$ $\frac{9.9}{17}$ $\frac{9.6}{15}$ 89 $\frac{101}{10}$ $\frac{12.5}{21}$ $\frac{17.6}{41}$ $\frac{20.0}{50}$

over H.I. $\frac{+8.4}{50}$ $\frac{+5.8}{40}$ $\frac{0.0}{35}$ $\frac{7.0}{23}$ $\frac{7.4}{15}$ 7.2 $\frac{7.9}{5}$ $\frac{12.5}{18}$ $\frac{13.0}{20}$ $\frac{15.5}{32}$ $\frac{21.1}{50}$

$\frac{+5.0}{50}$ $\frac{+2.0}{35}$ $\frac{0.0}{34}$ $\frac{6.8}{27}$ $\frac{6.7}{21}$ $\frac{5.7}{16}$ 54 $\frac{6.0}{5}$ $\frac{11.7}{19}$ $\frac{15.6}{38}$ $\frac{18.6}{50}$

$\frac{+5.3}{50}$ $\frac{+3.3}{37}$ $\frac{0.0}{35}$ $\frac{1.5}{33}$ $\frac{4.0}{28}$ $\frac{3.9}{22}$ $\frac{3.4}{19}$ 3.3 $\frac{4.3}{5}$ $\frac{9.4}{14}$ $\frac{13.0}{24}$ $\frac{16.4}{36}$ $\frac{20.4}{50}$

$\frac{+7.6}{50}$ $\frac{+4.8}{35}$ $\frac{0.0}{30}$ $\frac{1.5}{28}$ $\frac{1.8}{22}$ $\frac{1.1}{20}$ 1.4 $\frac{2.4}{4}$ $\frac{13.0}{18}$ $\frac{16.4}{26}$ $\frac{20.7}{50}$

$\frac{3.2}{50}$ $\frac{3.9}{38}$ $\frac{9.6}{31}$ $\frac{10.2}{25}$ $\frac{9.3}{21}$ 9.6 $\frac{9.9}{3}$ $\frac{13.0}{9}$ $\frac{19.2}{17}$ $\frac{20.0}{24}$ $\frac{15.2}{50}$

$\frac{2.6}{50}$ $\frac{3.9}{38}$ $\frac{8.0}{30}$ $\frac{7.5}{22}$ $\frac{7.0}{20}$ 7.5 $\frac{13.1}{14}$ $\frac{10.3}{31}$ $\frac{9.9}{50}$

$\frac{+0.5}{50}$ $\frac{1.6}{40}$ $\frac{1.7}{31}$ $\frac{4.9}{28}$ $\frac{5.4}{21}$ $\frac{4.7}{18}$ 4.7 $\frac{5.1}{3}$ $\frac{7.8}{11}$ $\frac{7.2}{18}$ $\frac{4.7}{39}$ $\frac{4.5}{50}$

$\frac{+4.0}{50}$ $\frac{1.1}{29}$ $\frac{2.4}{25}$ $\frac{2.7}{19}$ $\frac{2.2}{16}$ 2.1 $\frac{2.5}{4}$ $\frac{5.1}{10}$ $\frac{5.7}{22}$ $\frac{1.9}{50}$

1145 "OK" my back.

11 PM Breeze OK.
 $\frac{4.2}{50}$ $\frac{5.5}{32}$ $\frac{7.4}{26}$ $\frac{11.9}{20}$ $\frac{11.6}{17}$ $\frac{11.4}{16}$ 11.5 $\frac{11.6}{3}$ $\frac{12.7}{10}$ $\frac{12.4}{26}$ $\frac{12.7}{50}$

$\frac{+1.6}{50}$ $\frac{+0.7}{44}$ $\frac{+0.3}{30}$ $\frac{0.0}{28}$ $\frac{8.2}{19}$ $\frac{8.3}{16}$ 8.1 $\frac{8.2}{5}$ $\frac{9.7}{12}$ $\frac{8.6}{14}$ $\frac{10.4}{30}$ $\frac{14.4}{50}$

$\frac{3.4}{50}$ $\frac{4.4}{34}$ $\frac{5.5}{19}$ $\frac{4.3}{14}$ 4.2 $\frac{4.7}{9}$ $\frac{9.7}{18}$ $\frac{11.7}{34}$ $\frac{14.6}{50}$

7 H1 —

1022.56 ✓

43+50

14.7

44

17.4

+50

19.8

T.P.

6.23 1027.85 ✓ 0.94 1021.62 ✓

45

21.6

+50

22.9

46

23.4

T.P.

3.85 1026.89 ✓ 4.81 1023.04 ✓

+50

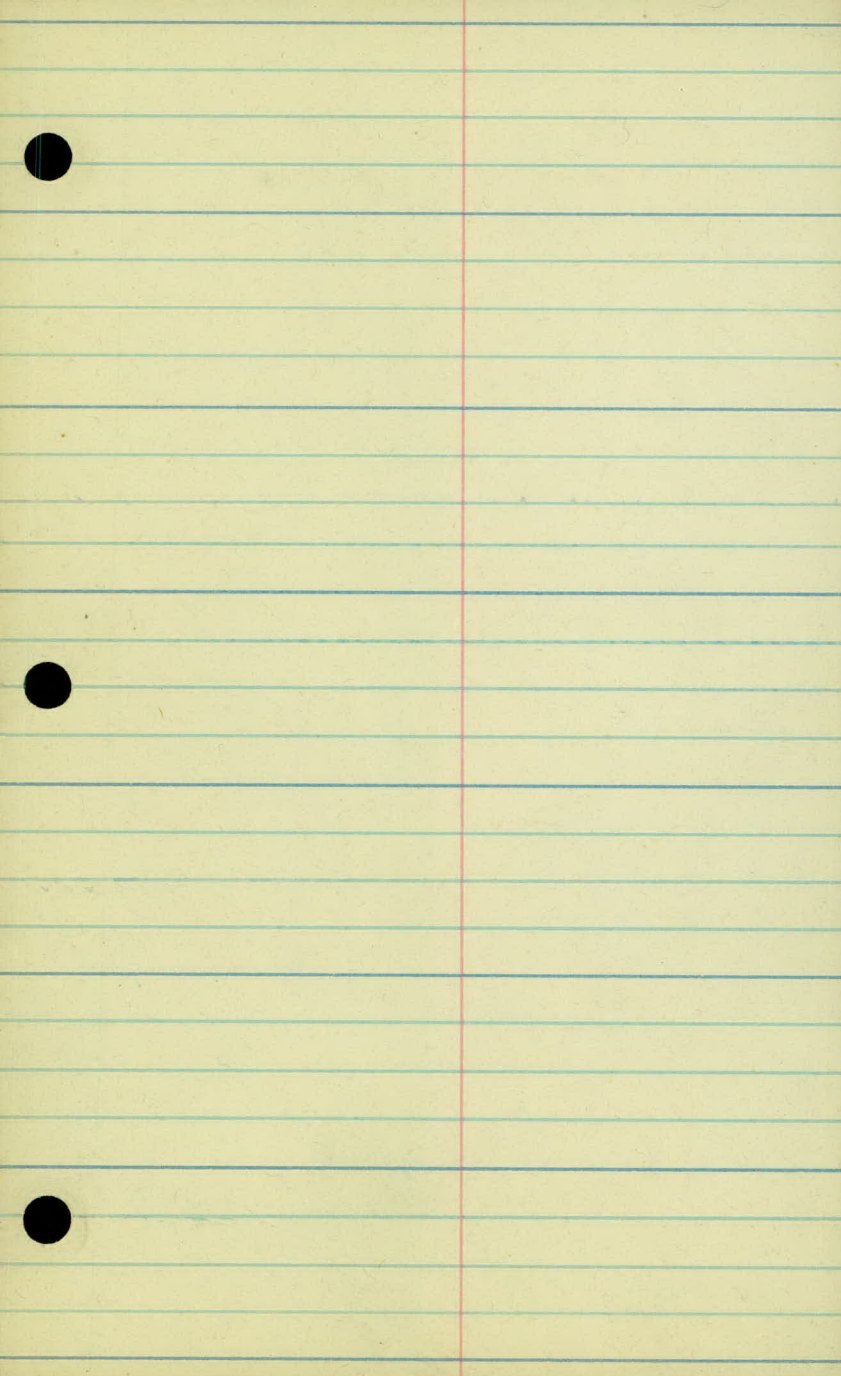
23.0

47

21.8

T.P.

4.72 1022.17 ✓



+ HI -

T.P

3.53

1025.70

1022.17

47+50

21.4

48+00

20.9

+50

21.0

49

21.1

+50

20.6

T.P

4.04

1023.29

6.45

1019.25

50+00

19.1

+50

16.7

51

14.2

+50

10.9

T.P

2.81

1012.56

13.54

1009.75

51+50

52+00

07.6

+40

04.2

52+56

End Report

02.9

Clay 3/3/22

Lt

Rt

Top of Rock 17' Lt Sta 48+75

$\frac{5.1}{50} \frac{7.2}{39} \frac{7.8}{19} \frac{4.8}{12} \frac{4.3}{4.3} \frac{5.0}{8} \frac{8.7}{20} \frac{9.1}{50}$

$\frac{7.0}{50} \frac{8.4}{30} \frac{8.2}{17} \frac{5.1}{10} \frac{4.8}{4.8} \frac{5.4}{9} \frac{8.5}{15} \frac{9.4}{30} \frac{11.6}{50}$

$\frac{5.8}{50} \frac{6.8}{38} \frac{6.4}{24} \frac{4.8}{13} \frac{4.7}{4.7} \frac{5.3}{8} \frac{6.2}{15} \frac{5.5}{17} \frac{8.7}{30} \frac{12.3}{50}$

$\frac{2.8}{50} \frac{2.5}{39} \frac{0.7}{26} \frac{5.3}{19} \frac{4.6}{12} \frac{4.6}{4.6} \frac{5.4}{8} \frac{6.0}{14} \frac{4.9}{16} \frac{7.8}{36} \frac{11.2}{50}$

$+0.2 \frac{0.2}{50} \frac{0.0}{35} \frac{5.7}{29} \frac{3.5}{21} \frac{5.2}{16} \frac{5.1}{13} \frac{5.8}{8} \frac{6.4}{14} \frac{4.2}{16} \frac{7.8}{34} \frac{11.3}{50}$

$\frac{1.5}{50} \frac{2.2}{40} \frac{2.6}{28} \frac{3.1}{25} \frac{3.2}{20} \frac{4.7}{16} \frac{4.6}{12} \frac{4.2}{4.2} \frac{4.7}{9} \frac{5.7}{15} \frac{4.6}{17} \frac{7.0}{32} \frac{11.2}{50}$

$\frac{4.2}{50} \frac{5.6}{36} \frac{5.7}{23} \frac{6.7}{22} \frac{6.6}{12} \frac{6.6}{6.6} \frac{7.1}{9} \frac{7.9}{12} \frac{10.0}{22} \frac{15.4}{50}$

$\frac{4.9}{50} \frac{6.7}{27} \frac{8.6}{25} \frac{9.0}{17} \frac{9.8}{15} \frac{9.3}{12} \frac{9.1}{9.1} \frac{9.7}{9} \frac{13.0}{15} \frac{15.4}{20} \frac{21.8}{50}$

$\frac{5.9}{50} \frac{8.7}{25} \frac{11.3}{21} \frac{13.0}{15} \frac{12.3}{12} \frac{12.2}{8} \frac{12.7}{12.4} \frac{12.7}{10}$

11.7

$\frac{5.9}{76} \frac{10.4}{35} \frac{15.7}{50}$

$\frac{12.2}{50} \frac{12.0}{42} \frac{0.0}{24} \frac{0.8}{21} \frac{4.6}{15} \frac{4.9}{9} \frac{5.0}{5.0} \frac{5.8}{10} \frac{6.1}{13} \frac{5.6}{16} \frac{9.1}{32} \frac{14.0}{50}$

$\frac{2.0}{50} \frac{2.7}{26} \frac{2.6}{15} \frac{8.9}{10} \frac{8.6}{6} \frac{8.4}{8.4} \frac{8.7}{10} \frac{9.0}{15} \frac{5.9}{18}$

$\frac{4.1}{50} \frac{4.3}{25} \frac{4.4}{14} \frac{10.3}{9} \frac{10.0}{59.7} \frac{10.0}{8} \frac{10.5}{12} \frac{10.0}{14} \frac{8.0}{16}$

B.M. 1.46 1004.35 9.72 1002.84 1002.89

52+40

+56

53 99.3

+50 96.7

Check Levels

B.M. 13.08 1015.97 1002.89

T.P. 11.90 1025.98 1.89 1014.08 ✓

T.P. 0.56 1023.44 ✓ 3.10 1022.88 ✓

B.M. 0.25 1010.33 13.36 1010.08 1010.04

T.P. 0.05 997.12 ✓ 13.26 997.07 ✓

T.P. 0.47 984.95 ✓ 12.64 984.48 ✓

T.P. 12.70 989.56 ✓ 8.09 976.86 ✓

B.M. 11.76 977.80 977.75

T.P. 11.46 1000.67 0.35 989.21 ✓

B.M. 1.74 998.93 998.89

T.P. 0.19 987.29 13.57 987.10 ✓

T.P. 0.76 975.74 12.31 974.98 ✓

B.M. 9.22 966.52 966.47

T.P. 13.11 981.57 7.28 968.46 ✓

T.P. 3.50 984.18 0.89 980.68 ✓

B.M. 6.50 977.68 977.65

T.P. 0.16 971.76 12.58 971.60 ✓

T.P. 0.37 958.38 ✓ 13.75 958.01 ✓

B.M. 10.18 948.20 948.07 948.19

Mont End project N.W. cor.

0.2

$\frac{2.5}{35}$ $\frac{6.8}{50}$

1.5

$\frac{2.6}{2.6}$ $\frac{10.7}{50}$

$\frac{1.2}{50}$ $\frac{2.3}{19}$ $\frac{4.0}{11}$ $\frac{5.0}{10}$ $\frac{5.3}{6}$ 5.1 $\frac{5.7}{8}$ $\frac{10.2}{23}$ $\frac{12.7}{40}$ $\frac{12.7}{50}$

$\frac{7.1}{50}$ $\frac{12.3}{24}$ $\frac{11.8}{14}$ $\frac{7.6}{8}$ 7.7 $\frac{8.0}{5}$ $\frac{11.9}{12}$ $\frac{12.7}{27}$ $\frac{10.7}{50}$

Top of Mont N.W. Cor.

Spk in R.R. 12" Oak 20' Rt 43+08

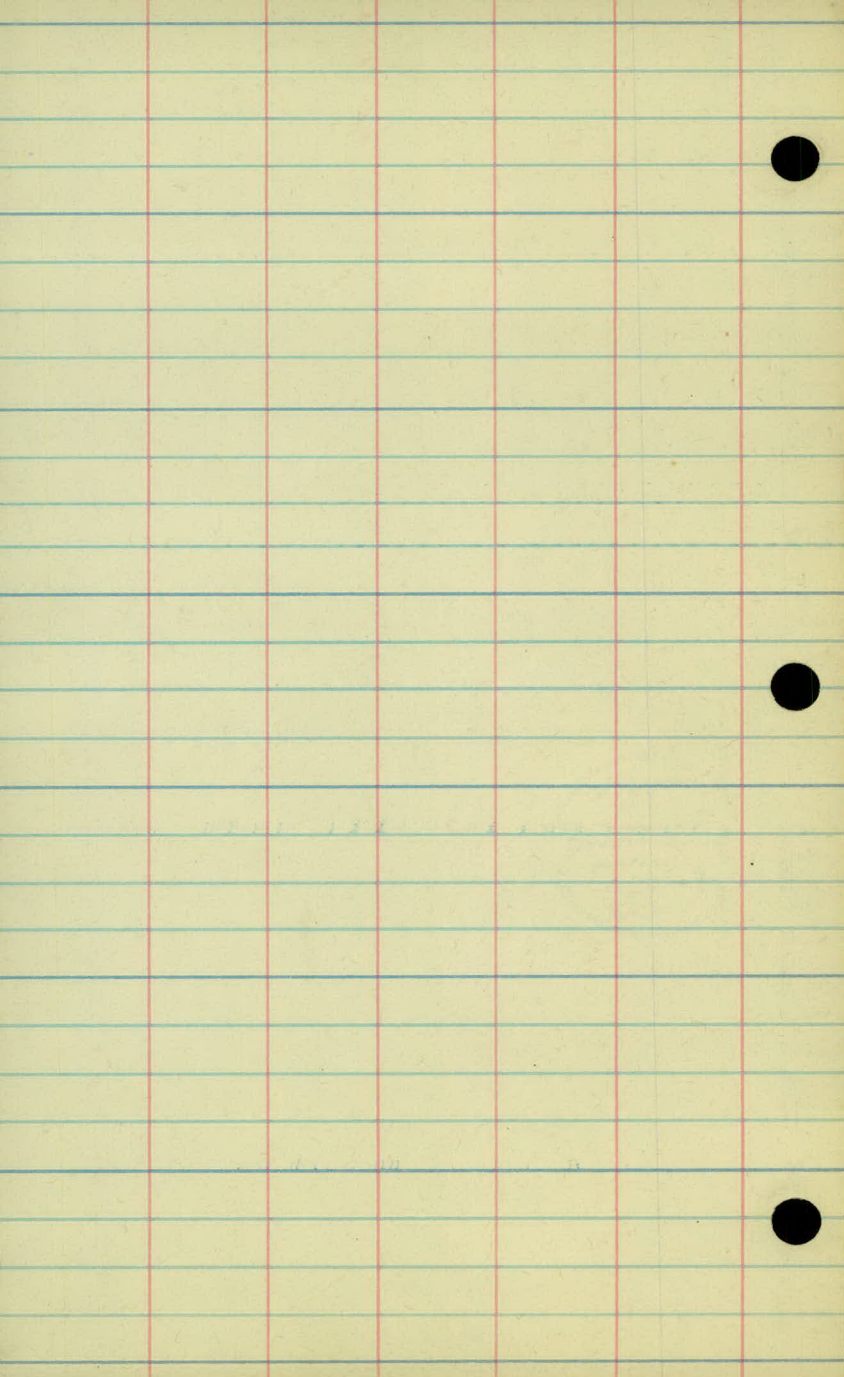
Spk in 18" Pop. 33' Rt. 31+45 (R.R. Spike)

Top of Rock 67' Rt 26+95

Top of Rock 95' Lt 18+90

Top of Rock 58' Lt 8+95

Spk in P.P. N.E. cor. Snelling and Co. Rd. "G"



3-2-32

LEFT

±

RIGHT

$\frac{6.5}{50}$	$\frac{50}{34}$	$\frac{44}{17}$	$\frac{8.4}{13}$	$\frac{8.3}{9}$	19	$\frac{8.2}{10}$	$\frac{7.5}{16}$	$\frac{6.2}{18}$	$\frac{9.2}{34}$	$\frac{12.2}{50}$
------------------	-----------------	-----------------	------------------	-----------------	----	------------------	------------------	------------------	------------------	-------------------

$\frac{+2.3}{50}$	$\frac{+4.5}{33}$	$\frac{+4.5}{31}$	$\frac{2.4}{18}$	$\frac{5.6}{13}$	$\frac{5.5}{8}$	52	$\frac{5.6}{12}$	$\frac{6.2}{17}$	$\frac{5.9}{23}$	$\frac{1.3}{27}$	$\frac{7.8}{50}$
-------------------	-------------------	-------------------	------------------	------------------	-----------------	----	------------------	------------------	------------------	------------------	------------------

$\frac{+12.0}{50}$	$\frac{+13.0}{32}$	$\frac{+7.1}{28}$	$\frac{0.0}{16}$	$\frac{3.0}{8}$	28	$\frac{3.2}{13}$	$\frac{3.5}{23}$	$\frac{4}{25}$	$\frac{1.4}{27}$	$\frac{11.3}{50}$
--------------------	--------------------	-------------------	------------------	-----------------	----	------------------	------------------	----------------	------------------	-------------------

$\frac{+8.6}{50}$	$\frac{+7.6}{37}$	$\frac{+2.6}{21}$	$\frac{5.0}{14}$	$\frac{6.7}{9}$	63	$\frac{6.6}{10}$	$\frac{7.2}{13}$	$\frac{6.6}{17}$	$\frac{11.1}{27}$	$\frac{17.6}{50}$
-------------------	-------------------	-------------------	------------------	-----------------	----	------------------	------------------	------------------	-------------------	-------------------

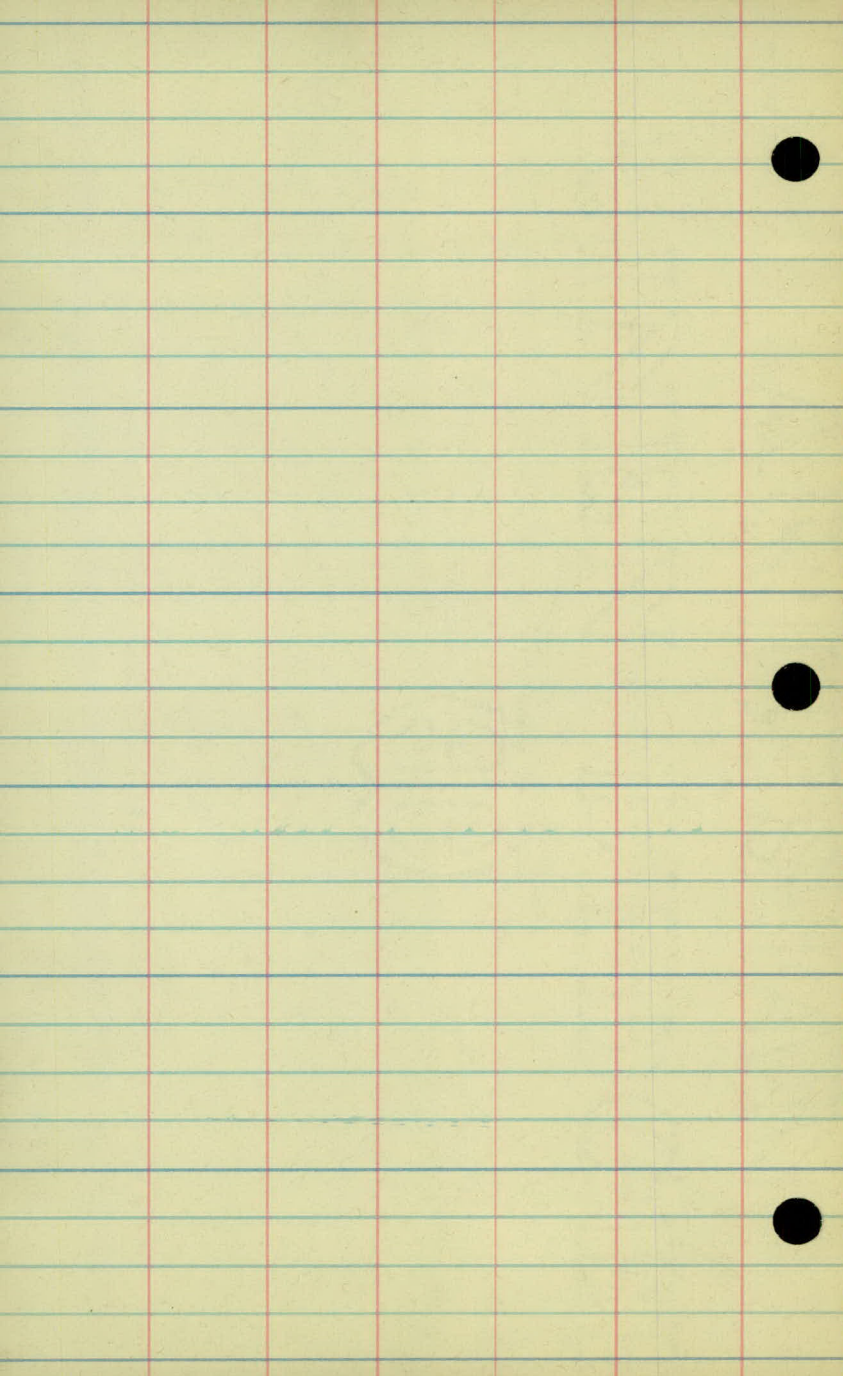
$\frac{+8.9}{50}$	$\frac{+7.3}{35}$	$\frac{+2.8}{20}$	$\frac{4.3}{16}$	$\frac{5.2}{7}$	50	$\frac{6.1}{13}$	$\frac{5.6}{15}$	$\frac{8.2}{23}$	$\frac{13.7}{50}$
-------------------	-------------------	-------------------	------------------	-----------------	----	------------------	------------------	------------------	-------------------

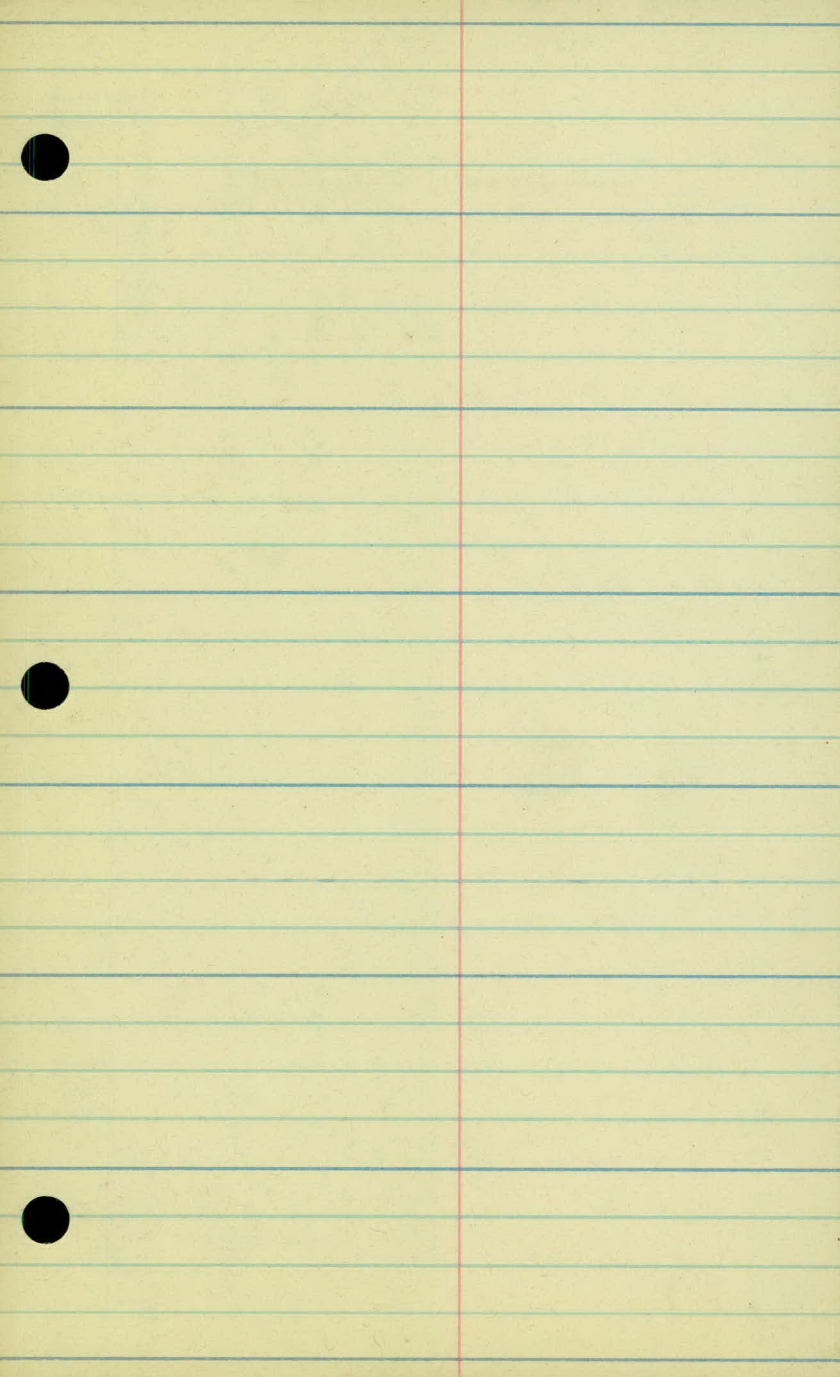
$\frac{+5.4}{50}$	$\frac{+6.3}{33}$	$\frac{+2.7}{21}$	$\frac{1.0}{20}$	$\frac{4.6}{14}$	$\frac{5.0}{9}$	45	$\frac{5.0}{9}$	$\frac{5.7}{14}$	$\frac{4.3}{17}$	$\frac{6.5}{30}$	$\frac{9.7}{50}$
-------------------	-------------------	-------------------	------------------	------------------	-----------------	----	-----------------	------------------	------------------	------------------	------------------

$\frac{+4.4}{50}$	$\frac{+3.8}{38}$	$\frac{0.0}{20}$	$\frac{3.7}{16}$	$\frac{4.4}{11}$	39	$\frac{4.7}{10}$	$\frac{5.1}{13}$	$\frac{5.1}{16}$	$\frac{1.5}{18}$	$\frac{5.4}{50}$
-------------------	-------------------	------------------	------------------	------------------	----	------------------	------------------	------------------	------------------	------------------

$\frac{1.7}{50}$	$\frac{6.2}{26}$	$\frac{5.7}{16}$	$\frac{5.1}{9}$	$\frac{5.6}{18}$	$\frac{8.0}{35}$	$\frac{9.2}{50}$	$\frac{8.4}{50}$
------------------	------------------	------------------	-----------------	------------------	------------------	------------------	------------------

Top of Rock 17' Lt Sta 48+75





B.M. 2.71 1005.60 ✓

1002.89 ✓

54+00

95.1

+50

94.7

55+00

97.1

+32

98.6

+75

1000.4

56+00

2.71 1002.89 ✓

1000.1

N.W. Cor. Mont.

$\frac{14.3}{50}$ $\frac{15.4}{43}$ $\frac{15.4}{18}$ $\frac{10.4}{10}$ $\frac{10.2}{6}$ 10.5 $\frac{12.3}{5}$ $\frac{12.4}{13}$ $\frac{11.3}{35}$ $\frac{8.9}{50}$

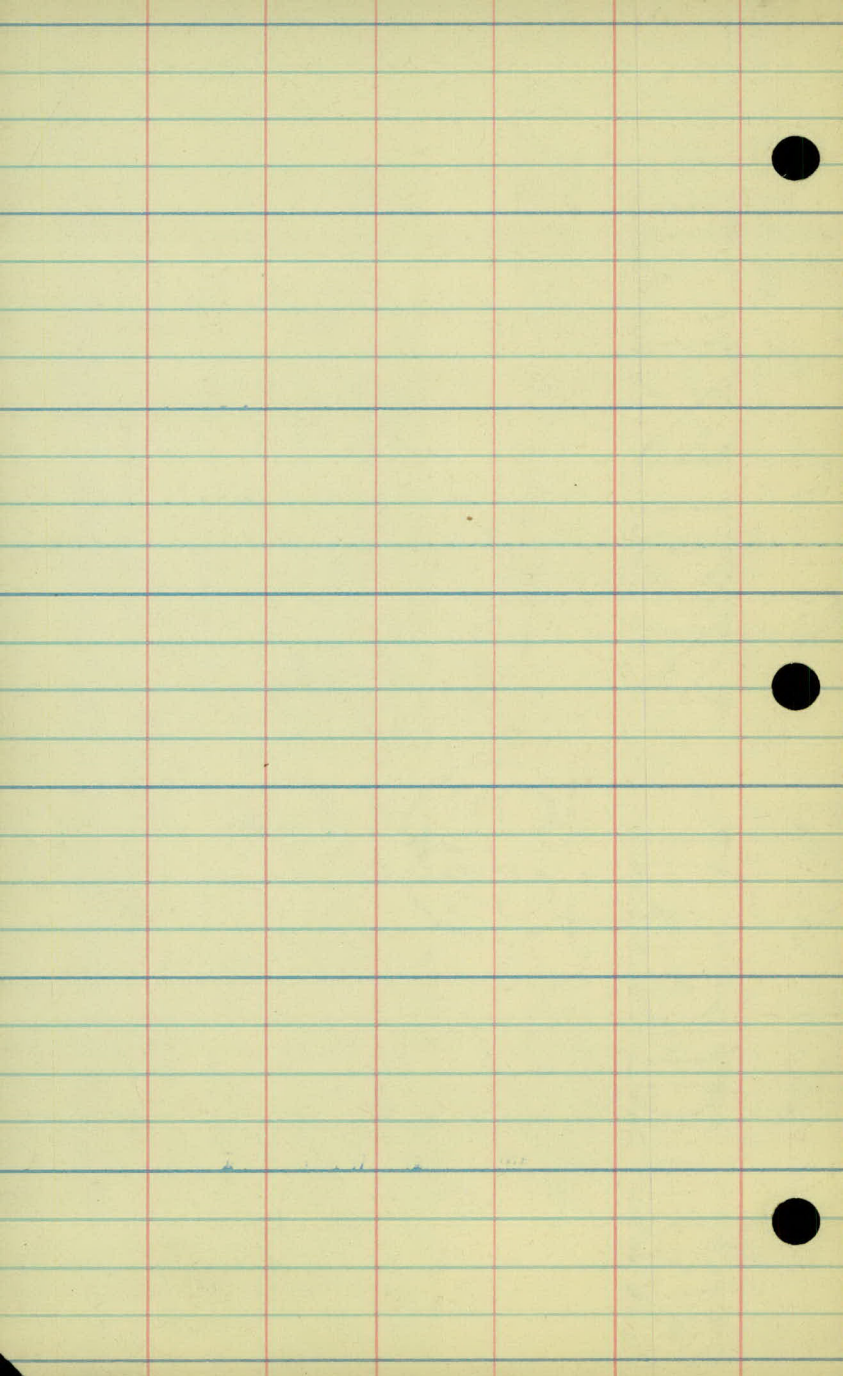
$\frac{15.5}{50}$ $\frac{14.9}{35}$ $\frac{13.5}{19}$ $\frac{10.4}{12}$ $\frac{10.2}{2}$ 10.9 $\frac{10.0}{12}$ $\frac{3.1}{50}$

$\frac{14.7}{50}$ $\frac{11.7}{24}$ $\frac{9.5}{15}$ $\frac{7.8}{12}$ 8.5 $\frac{8.5}{4}$ $\frac{7.0}{6}$ $\frac{2.8}{29}$ $\frac{0.0}{50}$

$\frac{13.8}{50}$ $\frac{9.3}{20}$ $\frac{7.6}{12}$ 7.0 $\frac{7.0}{1}$ $\frac{4.3}{7}$ $\frac{1.4}{26}$ $\frac{0.0}{35}$

$\frac{13.6}{50}$ $\frac{9.2}{20}$ $\frac{7.0}{7}$ 5.2 $\frac{5.3}{6}$ $\frac{4.6}{16}$ $\frac{2.5}{20}$ $\frac{0.0}{50}$

$\frac{14.3}{50}$ $\frac{11.4}{24}$ $\frac{7.9}{9}$ 5.5 $\frac{3.6}{2.1}$ $\frac{2.1}{42}$



2-19-32

Weber
Wilke
Bell
Stienman

Topog Notes
Snelling Ave
County Rd. "G" To "H"
1 Mile North.

5

4

3

2

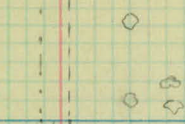
1

0+00

Windy - Cold - Clear

2-19-32

+74 P.P. 25' = End Power line



1/20 Beg. yard.

+27 P.P. 25'

Cultivated

← appr. Shoulder line

+82 P.P. 25'

Cultivated

Meadow

+34 P.P. 25'

+50 Radius 12'

+27 Radius 25'

+24 P.P. 25'

+13 End Radius 47'

+50 Radius 15'

+42.5 x P.P.
18" x 65' C.M. New

+13 End Radius 58'

County Rd.

"G"

12

11

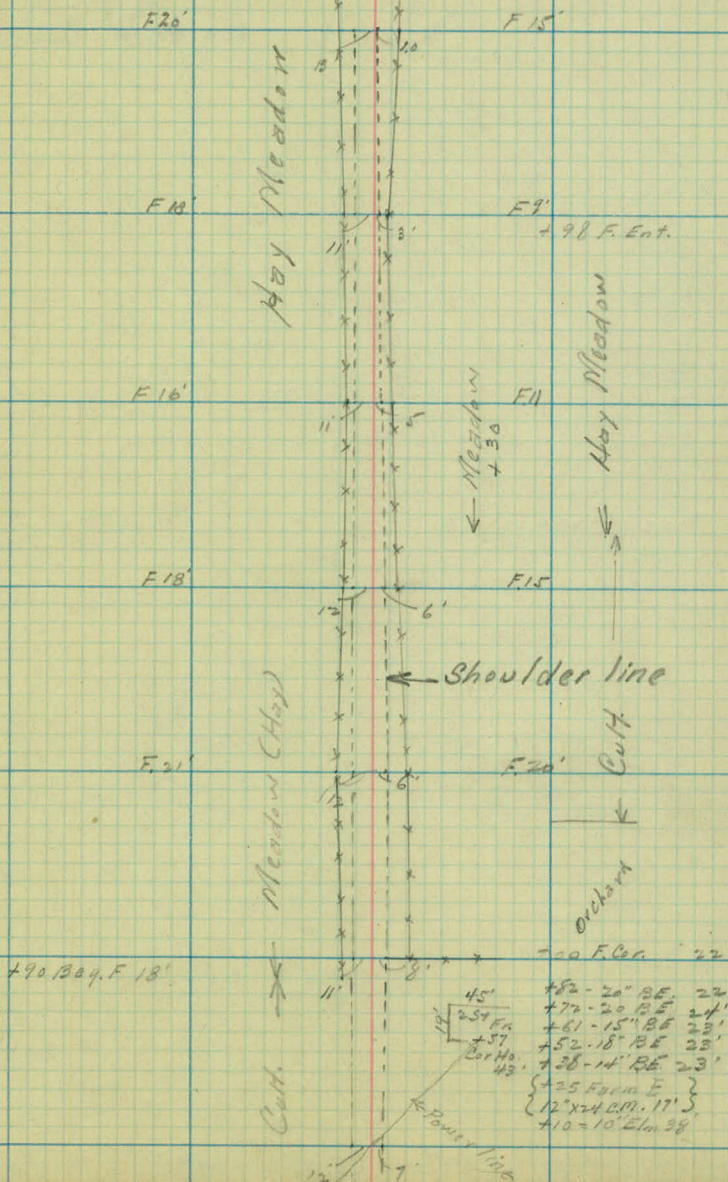
10

9

8

7

6



19

18

17

16

15

14

13

F-23

F-22

F-20

F-19

F18

+07 F.C. 21'
+03 F.C. 30'

+02. End F-22

R

← Shoulder line

Rot Hole Small
4" flows

← Hay Meadow

Hay Meadow

Old Farm
Jord
Scattered Stumps
+44 F. End.
Abandoned Farm

+10 F. Cor. 15'
F14

26

25'

24

23

22

21

20'

Woods.
 +70 Bq.F. 30'
 +45 Bq. Brush
 +28 Pr. Ent. Light Clearing 18'
 +14 F. Cor 27'
 F29

+10-6" Pop 15'
 F29

F24'

+61 F Ent.

F17'

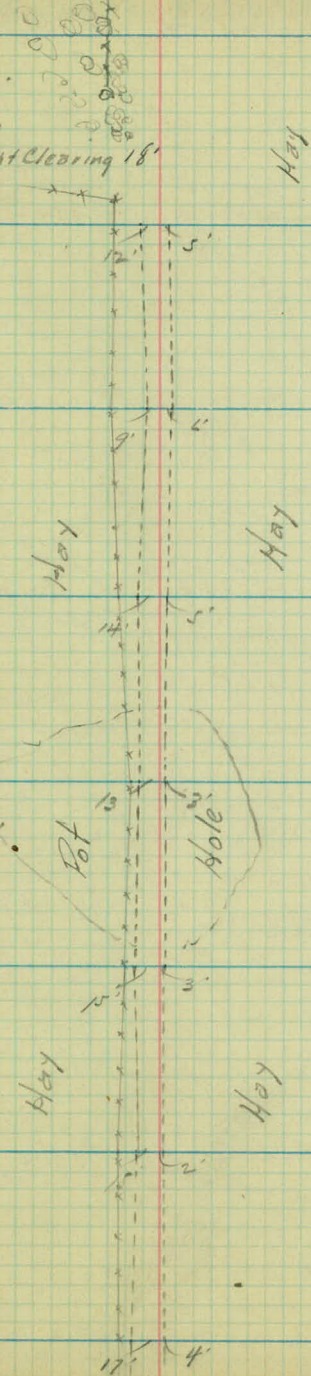
Light Clearing 22'
 +70 To 23+10'

+69-30" C.W. 33'

F20'

F23'

F23'



33

32

31

30

29

28

27

Woods

F37

+55-12" Oak 35'

F39

F40

+27-12" B.O. 32'

F31

F30

Woods

Woods

Light clearing

Hay Meadow

+45-18" Pop 33'
+25 F. Ent
+14-18" Pop 33'

40

39

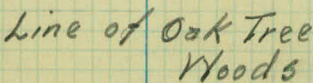
38

37

36

35

34



47

46

45

44

43

42

41

Hay
Meadow

+52 End Light Clearing 18'

+45 S. Dr

+90 A F 46'

Brush line 12'

+53 F int 37

F38

Brush line 20'

Woods

F35'

Light Clearing

Heavy Clearing

Woods

Brush line 23'

+63 Beg Light Clearing 23'

F35'

+90 End Light Clearing

Brush line 26'

8'

+92 F. Ent. F34'

Woods

Light Clearing

Heavy Clearing

Clearing line 12'
+92 X Dr.
15" x 28" Vit.

Woods

Brush line 10'

+70 Beg Light Clearing 22'

F33'

Brush line 6'

19

52

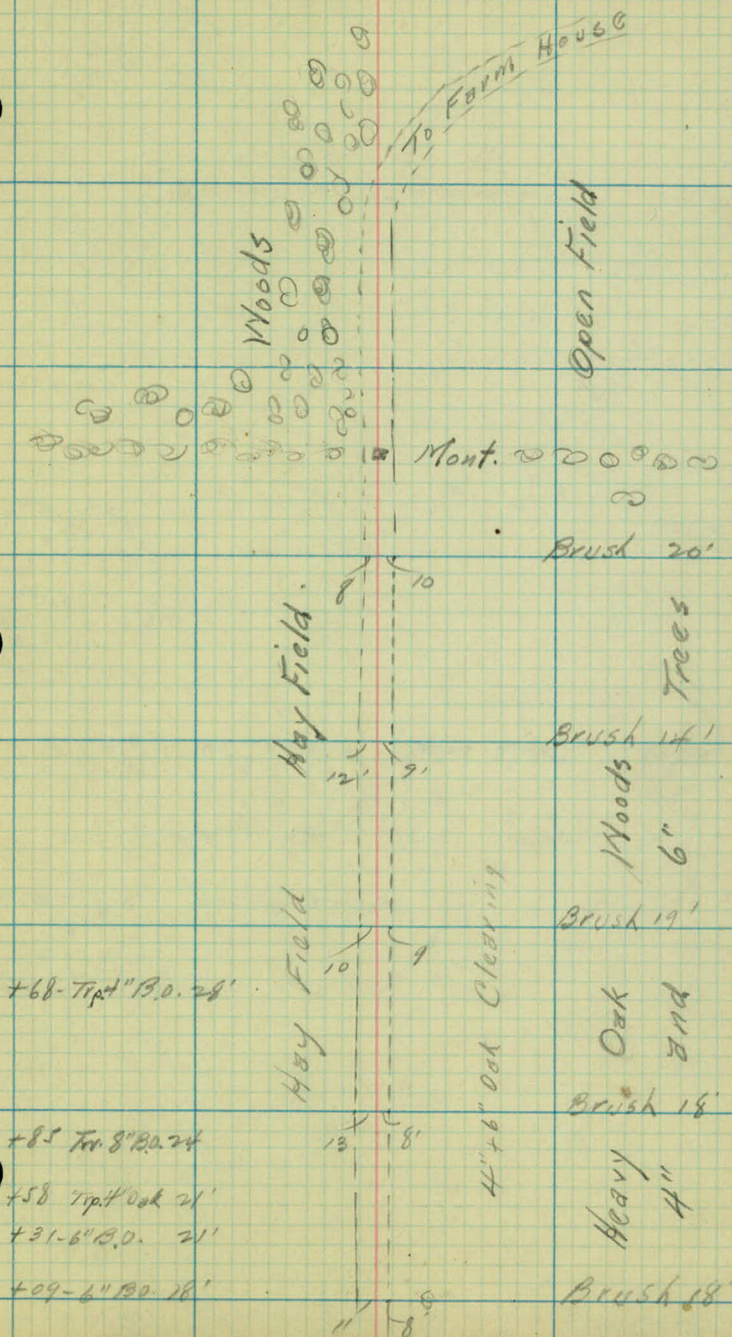
51

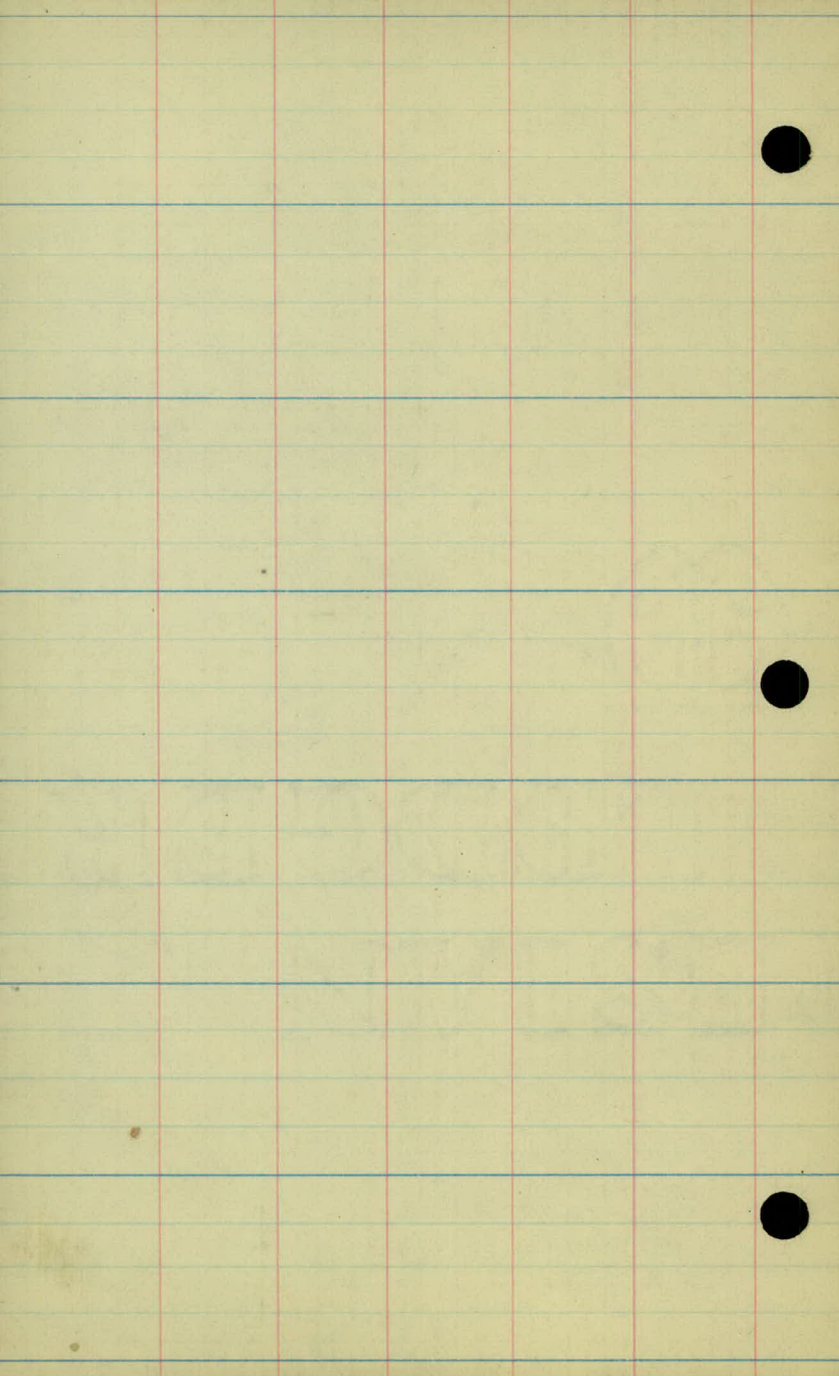
50

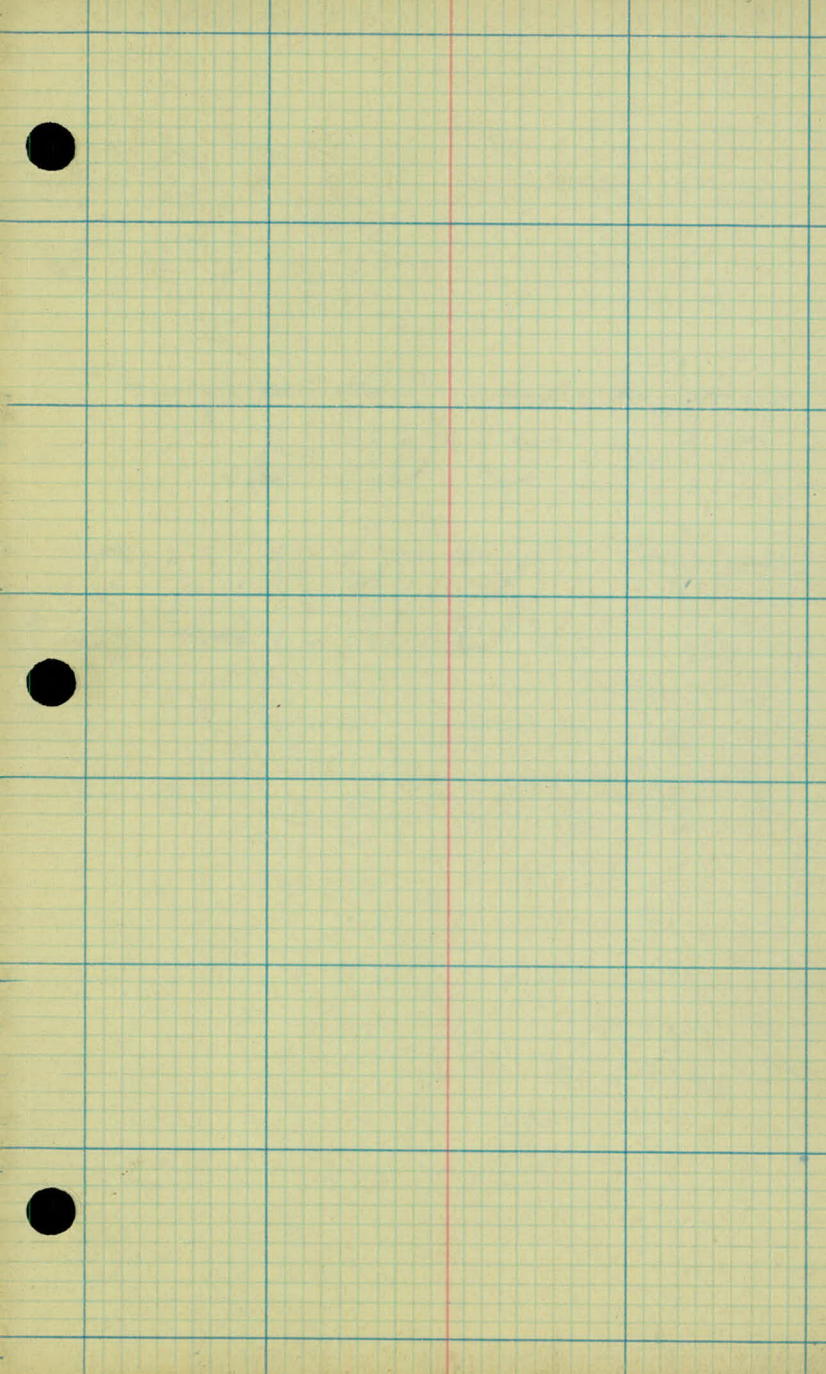
49

48

Finis 3:15 P.M. 2-19-32







57

56

55

54

53

F. 51'

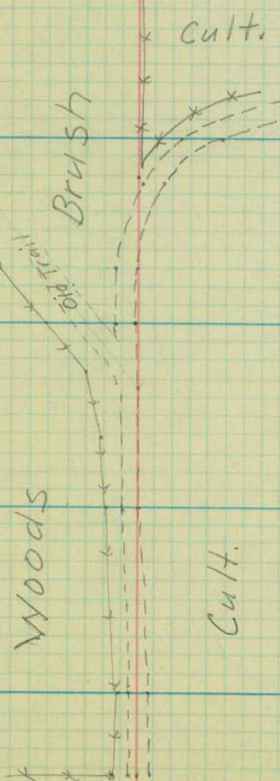
+23 F. 30'
+65 Int. Old Trail

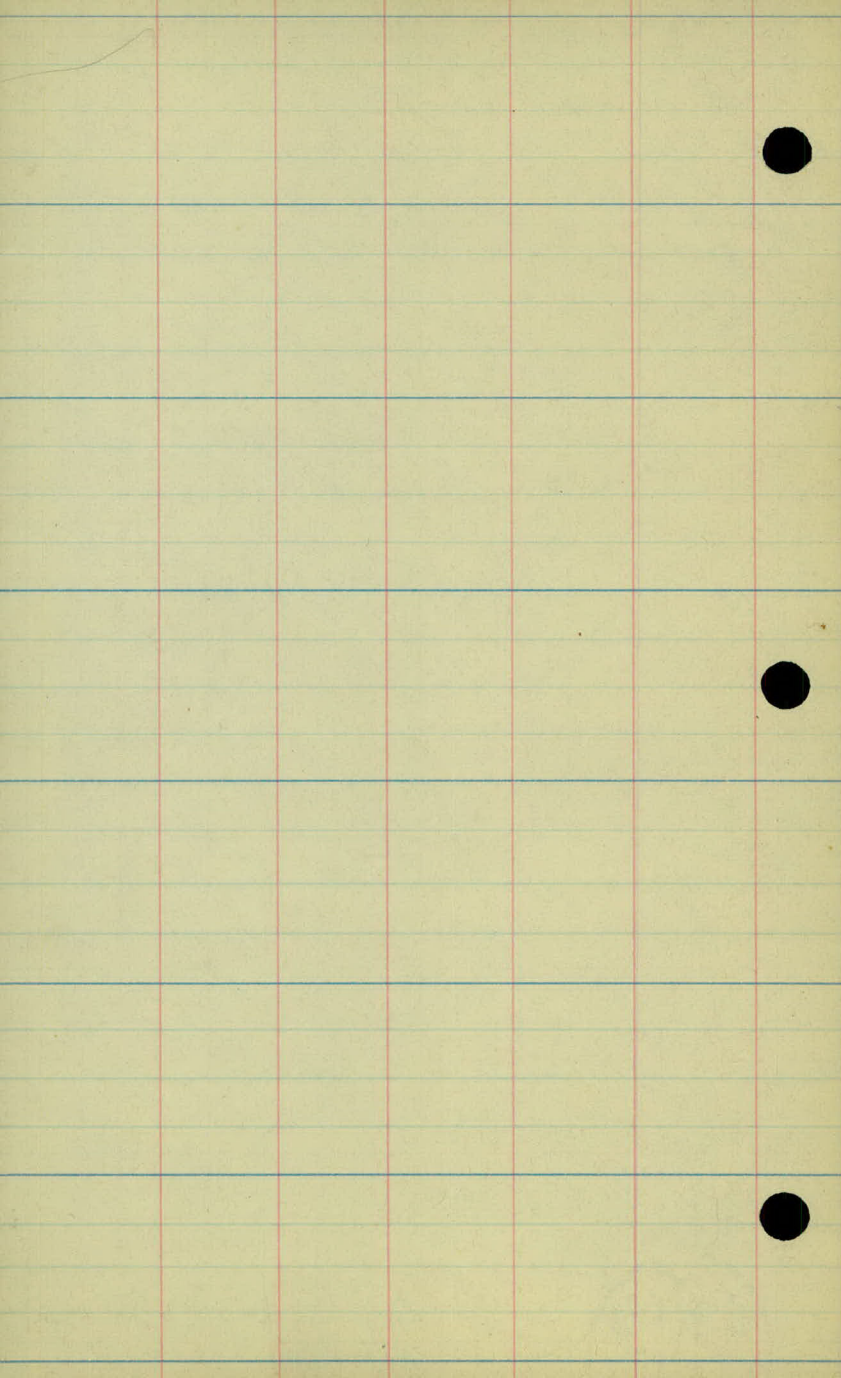
+38 F. 21'

F. 19'

F. 12'

+57 - F. Cor. 15'





O.K.

B.M. #1	10.10	958.17 ✓		948.07
T.P.	13.69	971.61 ✓	0.25	957.92 ✓
T.P.	12.93	984.41 ✓	0.13	971.48 ✓
B.M.	#2		6.85	977.56 ✓
T.P.	5.95	979.84 ✓	10.52	973.89 ✓
B.M.	#3		13.37	966.47 ✓
T.P.	10.91	989.78 ✓	0.97	978.87 ✓
	11.88	1000.70 ✓	0.96	988.82 ✓

981.71

0.12 987.72 ✓ 13.10 987.60 ✓

B.M. #4 3.56 981.31 ✓ 9.97 977.75 ✓

T.P. 13.75 994.10 ✓ 0.96 980.35 ✓

13.59 1007.12 ✓ 0.57 993.53 ✓

13.40 1020.50 ✓ 0.02 1007.10 ✓

B.M. #5 10.46 1010.04 ✓ 1009.80

T.P. 5.60 1025.89 ✓ 0.41 1020.09 ✓

T.P. 0.38 1017.56 ✓ 8.51 1017.18 ✓

B.M. #6 6.57 1010.99 ✓ 1010.70 90

Top Rock 58' Lt 8+95

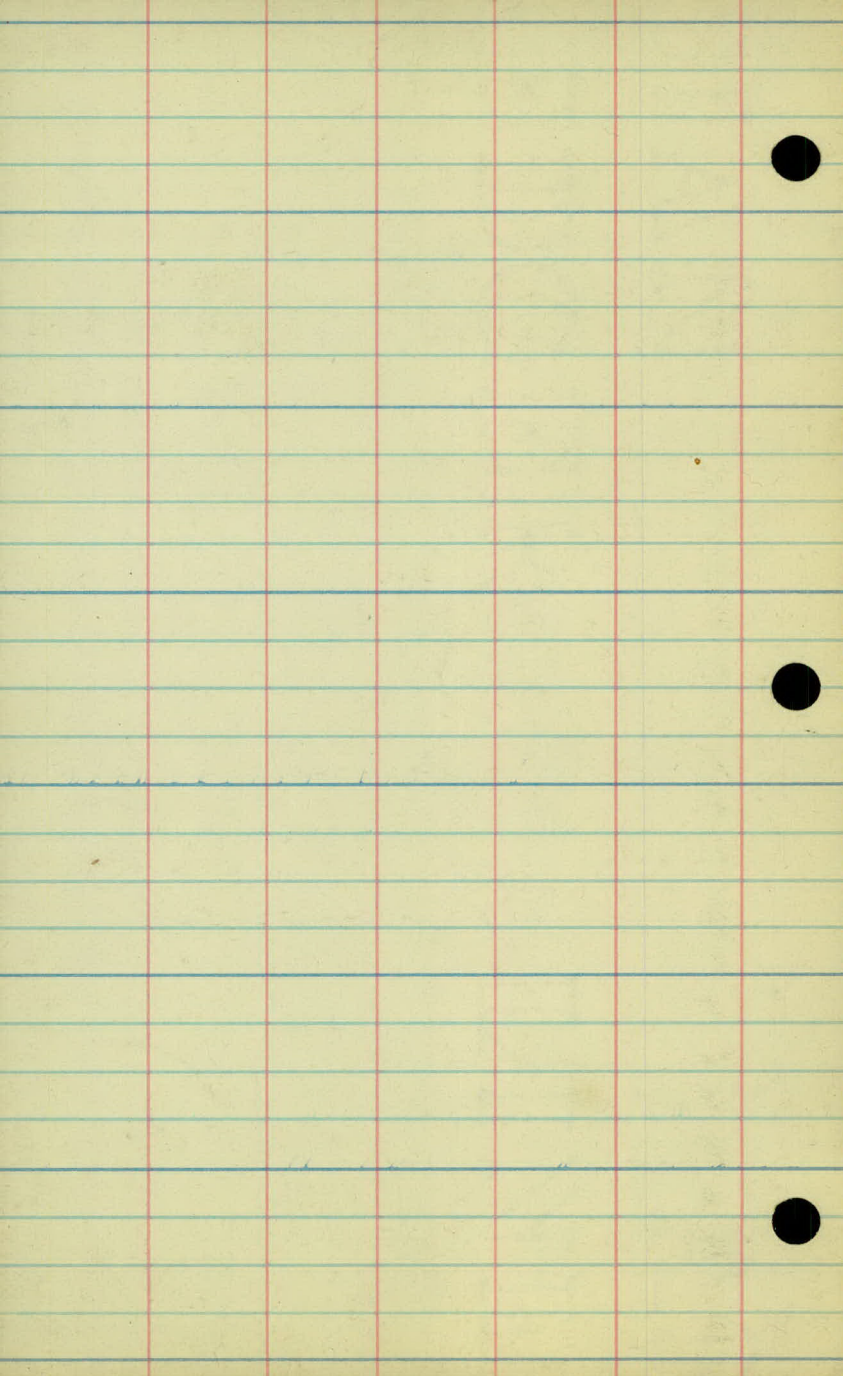
Top Rock 95' Lt 18+90

= Nailin F.F.

Spt in 18" Pop 33' Rt Sta 31+45 (R.R. Spike)

Spt in 12" Oak 20' Rt 43+08

Spt in 10" Oak 60' Lt Sta 52+56

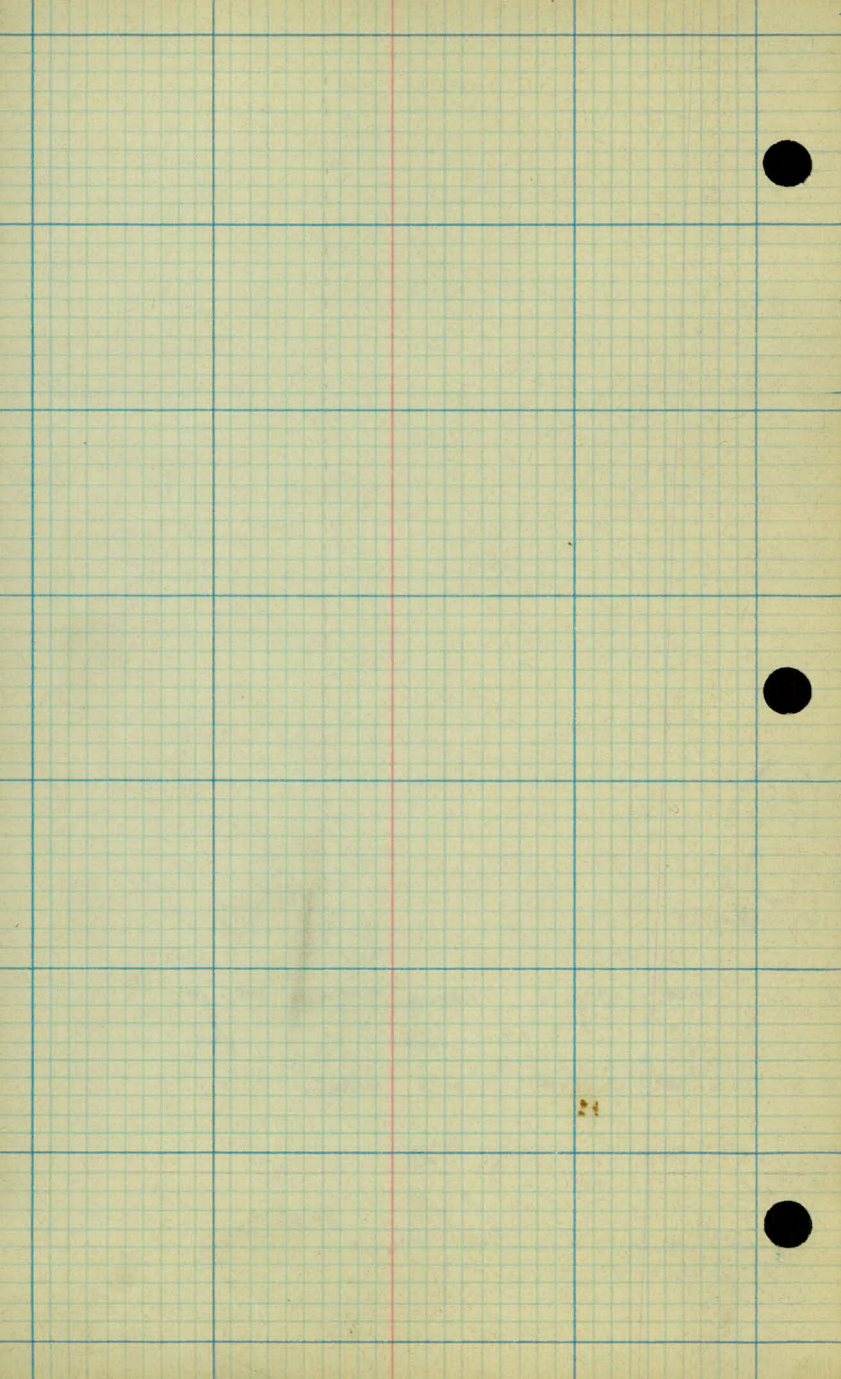


Plans in hand. Snelling Ave
Proj. 32-145

3/14/32

O.R.V.K.
Carley
Craibe

- X 0+42.5 - Reint. Pl. 24" P₃ x 48' (or 60')
- X 4+50 - 4+100 Ditch Rt. Division
6+25 - Rt. - Reint. Rep. 18" x 22' (or 42)
6+50 - Lt - Rep. 18" x 22' 442
- 6+100 - 7+100 - Rt. save 5 ft
- 10+98 - Rt. & Lt. No culv req.
- 17+50 - Rt. Rep. 18" x 22' C.M.
- X 13+00 - 14+00 Rt. Grab 12 ft
- X 14+50 - 16+00 Rt. Clear. 6 ft.
15+50 Pl. 24" P₃ x 60'
- X 18+00 - 16+00 Spec. ditch Rt
22+70 - Pl. - 24" P₃ x 84'
- X 22+00 - 23+50 Cl. 13 ft. Rt. & Lt
23+61 Rt. Pl. 15" x 20' C.M
- X 23+75 26+25 - Cl. 16 ft - Gr. 22 R&L
- X 26+50 32+00 Gr & Gr. Av. 12' inside F
26+28 Lt - Pl. 15" x 20 C.M
31+25 Rt - No. culv req
35+00 - Pl. 24" P₃ ^{x42'} Rubble Rt
39+50 - 52+50 - Cl (Gr. Need) ^{5 ft.} 8' - 00 ft R.
42+92 - Rt. & Lt - Pl. 2-15 x 20 C.Ms
" Reint. Rt. side checked
42+00 - 47+00 - Cl. & Gr. 12' wide Lt



47+45 Rt - No. culv. req

48+00-50+00 Lt Cl. 11+ft. Gr. 1-14+ft.

52+50-54+00 = Cl. 2 (Gr. Nec) Lt. 12'-out

53+50 - Pl 24" P3 x 48'

