

BK. 47 D+ 11 A

OFFICE OF COUNTY ENGINEER
RAMSEY CO. MINN.

Plan Survey
Birch Lane Rd. So.

Turtle Lake Pump

From Lot "A" Sec. 11-30-23 & Birch Lane
Co.
Also Profile, Sta. 7+00 to 13+50

Road Acc't. No. 97

Date Filed 8-15-47

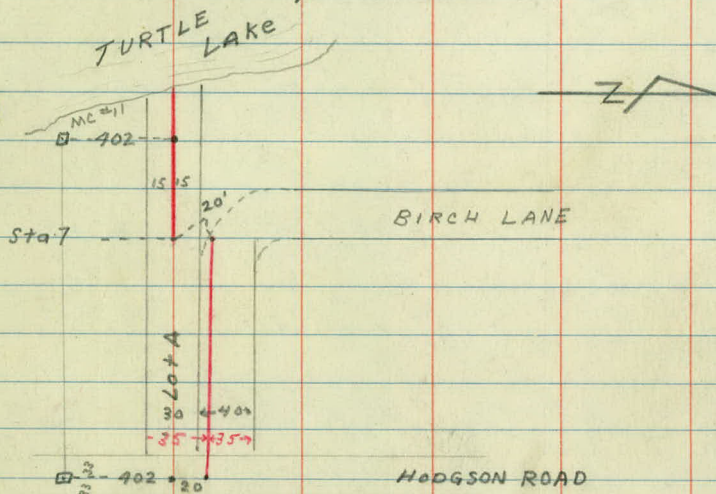
File

Birch Lane So

Turtle Lake Pump Plan Survey

Entrance Road to
Well Location

(Lot A Sec 11-T30-R23)
& Birch Lane

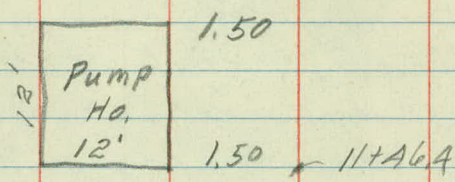


Alignment Page 1-2

Topography " 3-7

X Sections " 7-15

Rec. 5-20-49
P.M.
P.C.



11+20.35 ○ spike

15' 11 ○ spike

○ 10' a spike

○ spike

○ R.K. Nail

○ 7+00 Iron

26.07
20.35
5.72

1

Alignment

5-19-49

DB

Sta	Pt	Δ L+	Δ RT
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12+60	POT		Waters edge Turtle Lake
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11+20. ³⁵	POT		
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7+00	POT		
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0+00	PI		¢ Hodgson Road
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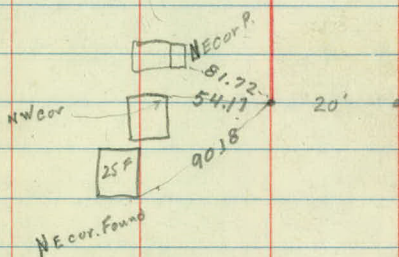
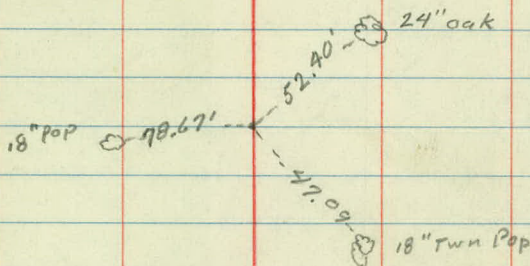
5-19-49

2

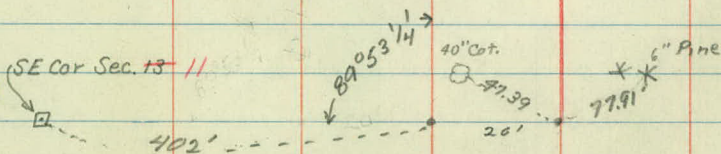
G B

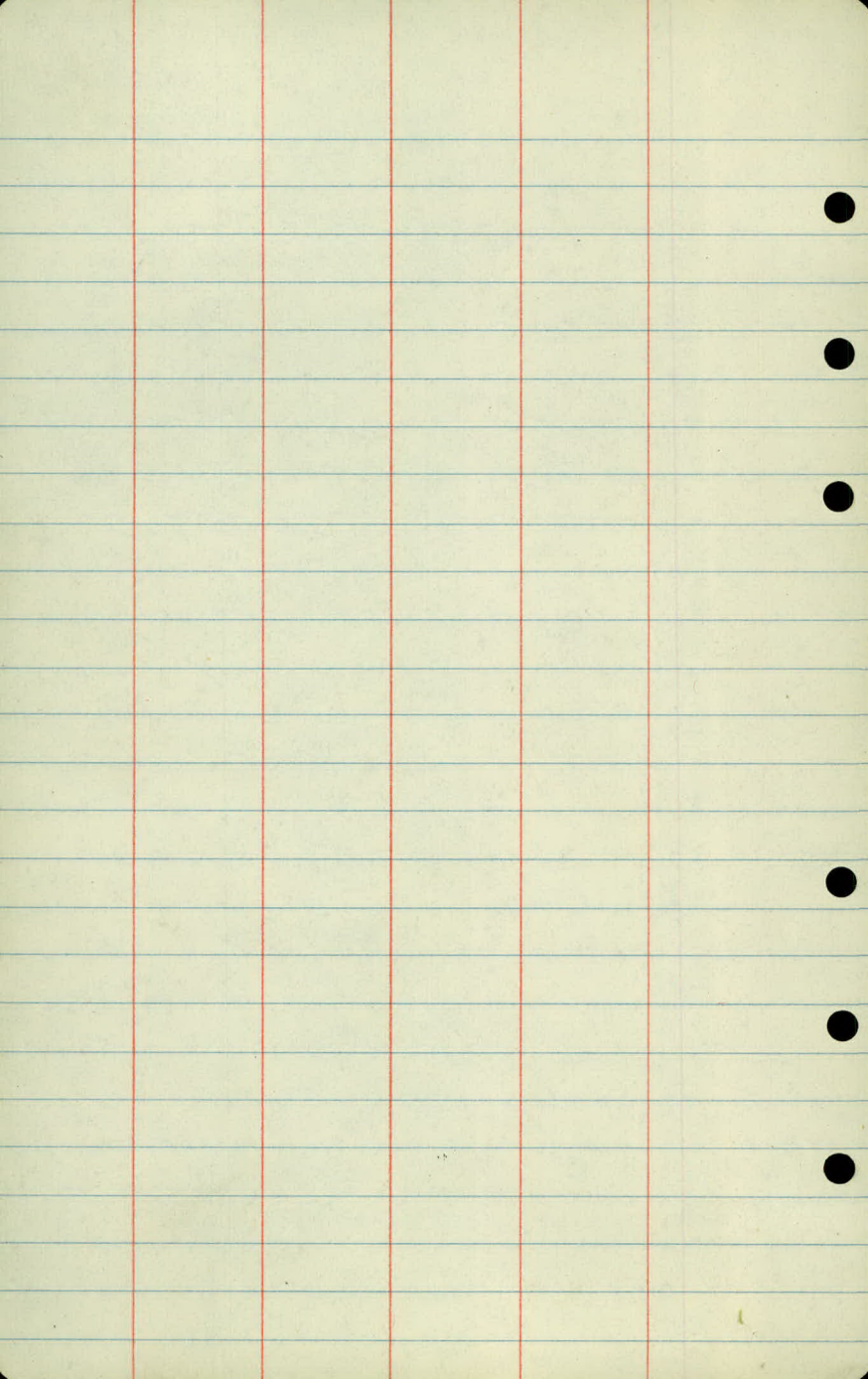
AM

M 13



Chr Lot A.





Topography

5-19-44

C.B.

251 PP - 8'

+ 43-4" CE 44'

+ 19-Beg Fe - 7'

+ 19-Cor Ho - 86

+ 16-36" Pop - 33

+ 15-20" Birch - 7

3 Ho 84, Hedge 35-42 27-18 4-26

+ 84 - Cor Ho 84

+ 82 - end H B

+ 82 - PP - 5'

+ 71 - Beg L. Hedge 37-42

+ 68 - H. Brush 00 to 8

+ 60 - Dirt Ent

+ 37-20" cot 33

+ 31 - end L. Hedge 34-46

+ 28 - cor Ho 86

+ 15 - cor Ho 86

2 L. Hedge 34 end Fe 8' 23-15 3-26

+ 96 - end Brush - 3-8

+ 96 - PP - 8'

+ 96-20" cot - 33

+ 89-8" cot - 38

+ 87 - Brush 5'-10

+ 56 20" cot - 33

+ 45 - Beg L. Hedge 35-47

+ 15-20" cot - 33

Fe 8' 23-15 3-25

+ 96-6" cot 48

+ 74-30" cot - 34

+ 33 - Beg Fe 8'

+ 40-10' row of H Brush on ctr

+ 32 - Stamp 44'

+ 38 - Row Pine N-56

+ 32-30" cot 33

+ 33 Row Brush N-30-55

+ 31 - end R 16-26 500

+ 33 end R - 23

+ 27 - TP 8'

+ 22 - Beg Ctr R - 7

+ 11 Beg R 47

+ 11 Bk Top

+ 11 Beg R - 36'

- 29 GP - 10

- 13 Black Top

0400

1/2 Holgson Road

5-19-49 (4)

GB
AM
M.B.

15F

Lilac Hedge

15F

untrimmed
Lilac Hedge
4-8' high

Scattered Hazel
Brush - 3-6' high

Broken Down

8 wire Fz.

0+00

Hedgson Road

7 +04 cor Ho 74', 16-24 4-26
 +82 Cor of Ho-74'
 +74 Row 12" Pop-37'
 +76 - 30" Pop-33
 +123 Bush-32
 +62 Bush 32'
 +55-4" Turn Oak 5'
 +54 PP-7
 +50 Stump-7
 +71 Cor Ho 90'
 +48 Stump-7'
 +43 cor Ho-90'
 +41 Turn 8" Pop-31'
 39 4" Elm-28
 +33 8" Elm 33
 +29 Quad 18" Oak-9'

6 Fe 6' 23-14 4-27

+76 PP-6'
 +75 10' ent 20'
 +54 30" cot 33'

+16 12" cot-25
 +08 and Gard 33
 +61 PP-8'

5 Garden 27 Fe 6' 21-13 4-26

+58 Turn 12" cot-26'

+56 8" Pop-25
 +33 1/2" Gard-33'
 +32 15" Pop-28
 +32 6" Pop-42
 +30 6" Turn 43
 +27 PP-6'
 +10 15" Ent-25
 Fe 7'

A +82 end H.B.O-8 24-16 4-26

+56 20" Pop-33
 +56 Birch-50
 +84 10" Pop-41
 +71 H.B.-00-12
 +45 Cor Ho-86
 +68 8" Pop-45
 +57 2" L. Hedge 38'

+end L Hedge 35-40'

end Fe 06.

+95 Flag P. 39.

15F

5

15

+50 Cistern-69.

broken Down Fe

Grass

Garden Plot

Grass

Grass
&
Small Brush

+94 20" Pop 33

+90 - end 2' 2" Hops 36'

10

8'

5'

+75 Car Gar 54
 +75 24" Pop 45
 +75 18" Turn Pop 14
 +60 E Road

+51 18" Elm - 27
 +52 end curb 37
 +52 end Curb Rad 19
 +79 Beg curb Rad 6
 +13 Cor Ho 14.3
 +01 12" oak - 22

+92 Flower Bed 15
 +84 14" Turn oak 11
 +76 10" Turn oak - 18
 +63 12" oak - 13
 +60 PP - 14
 +45 10" oak - 23
 +46 6" oak - 16
 +45 Stump - 14
 +36 E 5" Ent SW - 17
 +22 12" Turn - 14
 +15 12" oak - 16
 +12 Cor Ho 28
 +18 Tangent Birch Lane 20' inside
 +09 14" Tr oak - 14

9

3-7 (Rd 103 - 152)

12" oak - 22
 +99 8" oak 37
 +96 8" oak 9
 +94 Stump 7
 +87 15" oak 13
 +82 Ctr 5' Dia Flower Bed 22
 +72 4" oak - 19
 +75 10" oak - 41
 +73 end L Hedge 12-20
 +73 15" pop 13
 +58 Apple 28

+86 Turn 6" oak - 14
 +82 12" oak 24
 +84 10" oak 26
 +78 15" oak - 12
 +75 Garden 6" - 45
 +75 Road - 66 - 101

+41 end Fe - 26
 +35 Beg L Hedge 11-18
 +35 30" oak 14
 +26 end 6" Hedge 15
 +26 Hdr 6 - 26
 +03 Fe Cor 25

+60 Tri dead oak - 16

+47 +60 E Bush - 14-16
 +46 Road - 44-71
 +46 Car Gar 16
 +41 10" oak - 12
 +31 PP - 16
 +25 Road 27-53
 +22 12" Turn oak 14
 +12 PP - 13

8

Hedge 15

3' 6'

26-48 Fe 14 13' end
 13' 45" - 12-23

+95 30" cot 13
 +69 Cor SW 26
 +75 Cor Ho 34
 +69 W Well 44
 +69 6' Hedge 16
 +65 Ctr Bush 16
 +55 30" cot 13
 +51 BE 39
 +24 10' Ent
 +18 30" cot 13
 +14 8" Pop 21
 +14 end Hedge 75
 +06 Bush - 18
 +03 24" Elm 41
 +01 Beg Hedge - 15
 +01 Lilac Bush - 10
 +04 cor Ho - 54

+75 Road 24-47
 +94 14" oak 14
 +92 10" oak - 14
 +86 5" oak - 12
 +84 8" oak - 12
 +70 4" Turn oak - 14

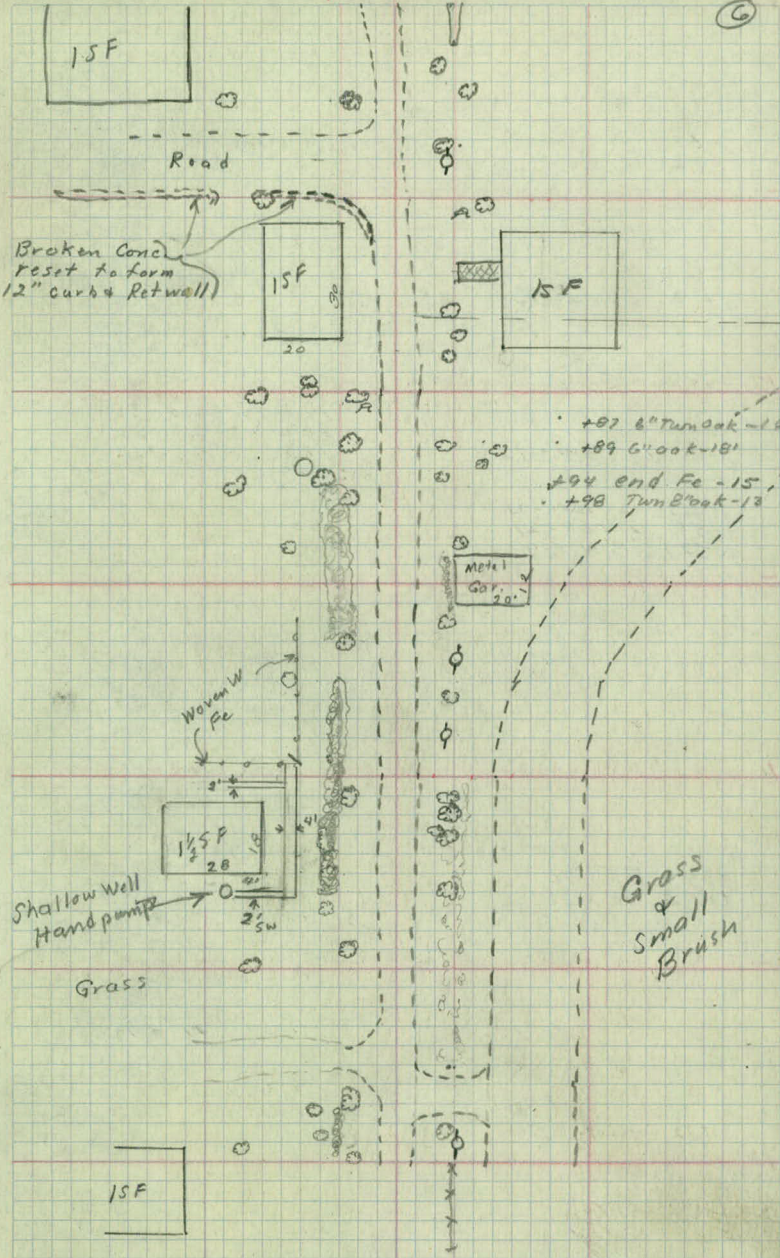
+40 10" oak 44
 +24 Beg Fe & Brush 14
 +17 10' X Drive

+6-6" Tri oak 13
 5 + PP - 16

7

9 - 4, 24-46 Fe end 14

+82 Car Ho 54



Note
E moved 20' south
to Lot A @ Sta 7

+60 edge water

+60 - Dock - 31'

+40 edge water - 68'

12 Top of Bank Bay Beach

+74 12" BW-46

+63 12" BW-21

+52 12" oak-21

+52 12" B.W-39

+93 4" / 10" P 23
 +88 Stump - 35
 +62 18" B.W. 33
 +82 18" Pop - 22
 +74 12" Birch - 36
 +69 10" Birch - 21
 +59 5 cor. Brk. Fireplace 30
 +58 12" oak - 23
 +51 10" Twin Oak - 28
 +48 24" oak - 45
 +46 12" oak - 24
 +37 15" oak - 21
 +35 15" oak - 26
 +29 4" Pine - 48
 +13 - Stump 23
 +11 - Stump 39
 +09 - 18" Birch 33
 +07 - Stump - 30
 +02 Stump - 29

Stump 19

+99 12" Birch 33
 +86 15" Birch - 46
 +81 20" Twin Pop - 29
 +73 15" Pop 16
 +70 15" Pop - 31

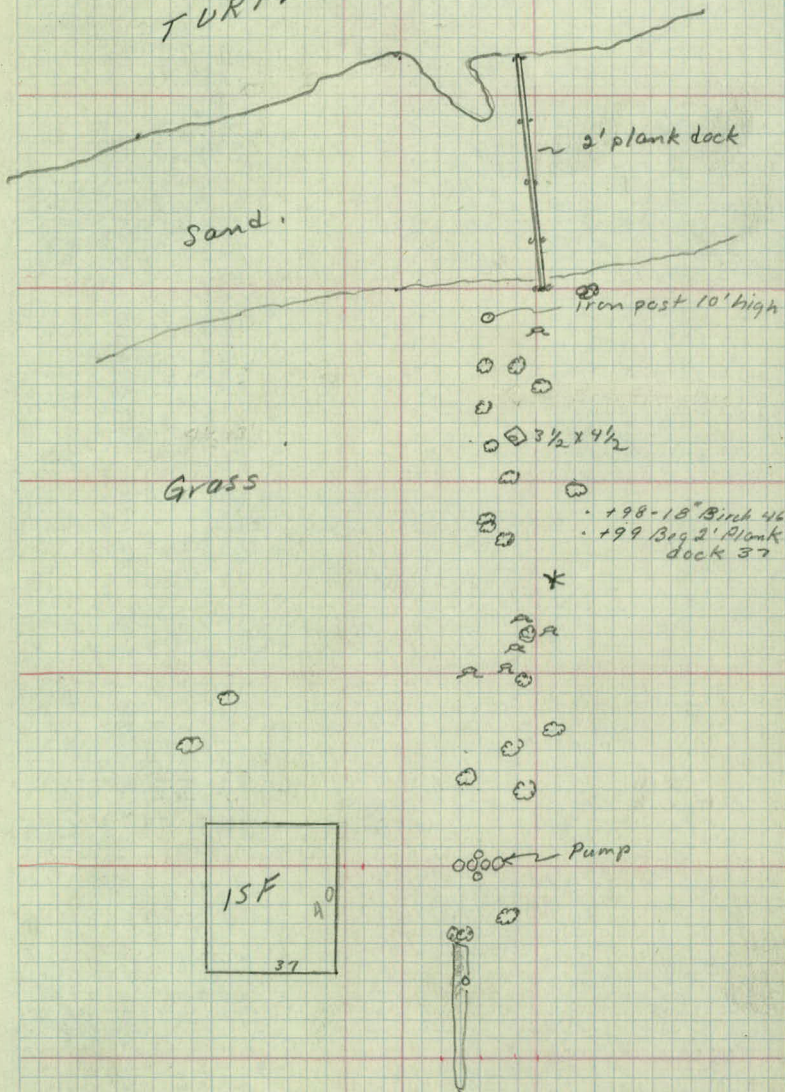
+51 Pump 41
 +55 3' dia. Flow 30, 32.5 36
 Bed

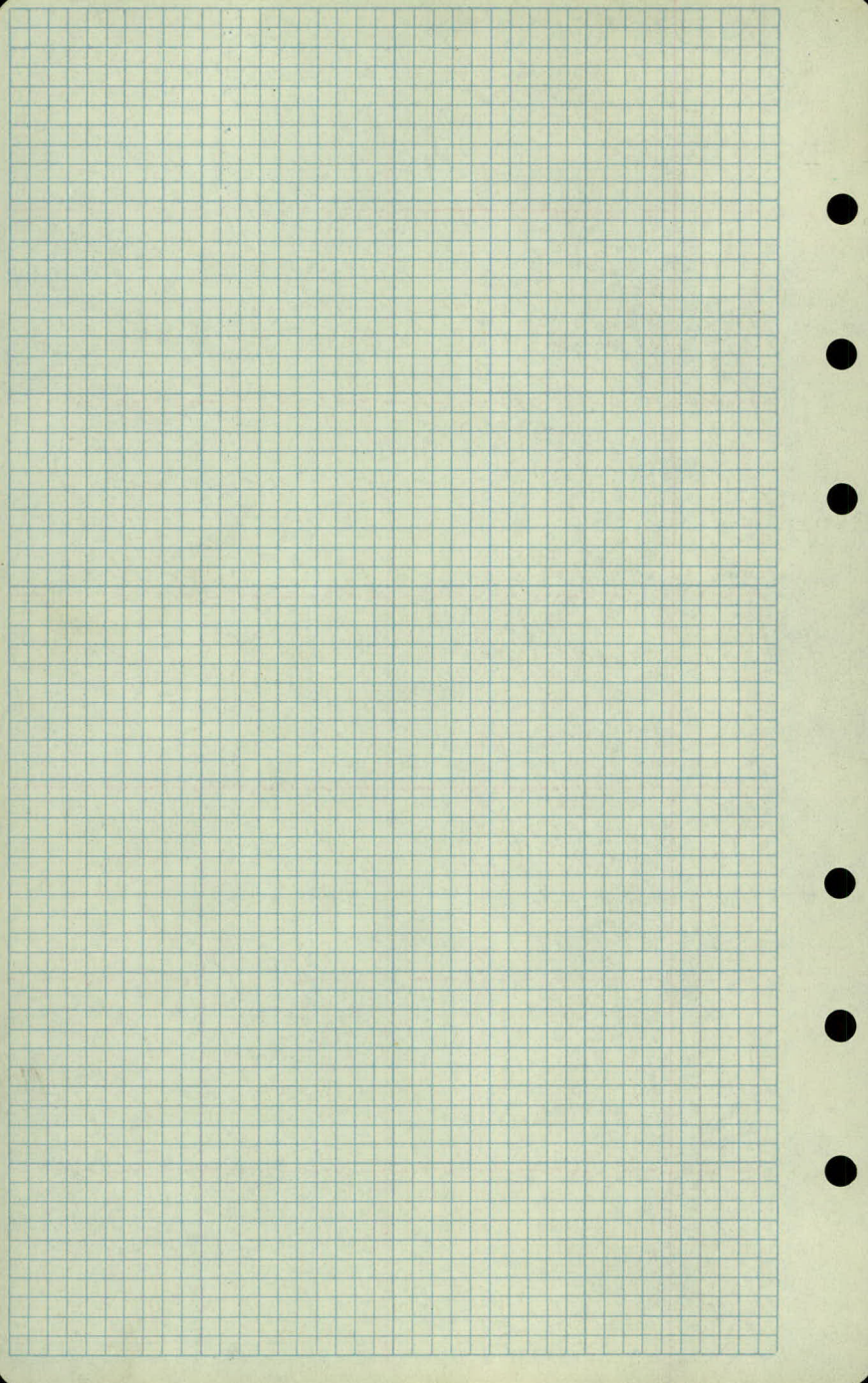
+37 40" Twin Pop 27

+32 8" Twin Oak - 15
 +30 end Flow Bed 15
 +20 Clos. Pole in conc 16.5

+22 Cor. Cot. 17.5

TURTLE LAKE





X Sections

5-19-49

GB

AM

M.B

Sta

+

π

-

Elev

Bench Levels

&

X Sections

Sta	+	π	-	Elev
BM	2.49	899.25 [↑]		896.76
			7.23	892.02 [↑] (892.00)
TP	13.23	911.93 [↑]	0.55	898.70 [↑]
	11.28	922.97 [↑]	0.24	911.69 [↑]
TBM			3.78	919.19 [↑]
TP	5.46	927.77 [↑]	0.66	922.31 [↑]
TP	6.15	931.68 [↑]	2.24	925.53 [↑]
BM			5.72	925.96

0+00 Profile Hodgson Rd. 24.95

+11 24.8

+20 24.7

+26 24.4
 Profile - 4' ditch R+

+31 24.2

Spk in 24" oak on N side ROW (Turtle Lake Dam)
Blue top @ N. Lake Elev.

Cor. SW 27+69-26' Lt.

Spk in 30" Cottonwood Sta 0+32, 33' Lt.

$\frac{7.4}{200}$ $\frac{7.3}{150}$ $\frac{7.2}{100}$ $\frac{6.9}{50}$ 6.75 $\frac{6.6}{50}$ $\frac{6.4}{100}$ $\frac{6.3}{150}$ ✓

$\frac{7.3}{50}$ 6.9 $\frac{6.9}{50}$ ✓

$\frac{7.4}{5}$ $\frac{7.7}{50}$ $\frac{7.5}{34}$ $\frac{7.8}{22}$ $\frac{7.0}{12}$ $\frac{24.8}{12}$ $\frac{7.2}{20}$ $\frac{7.2}{50}$ ✓

$\frac{7.7}{110}$
 $\frac{8.9}{50}$ $\frac{7.5}{32}$ $\frac{7.8}{29}$ $\frac{6.9}{20}$ $\frac{7.1}{14}$ $\frac{6.9}{12}$ $\frac{7.0}{6}$ $\frac{7.3}{14}$ $\frac{24.7}{27}$ $\frac{7.2}{34}$ $\frac{9.1}{50}$ $\frac{9.3}{50}$ ✓

✓ $\frac{7.0}{50}$ $\frac{6.8}{29}$ $\frac{7.5}{26}$ $\frac{6.7}{15}$ $\frac{6.7}{12}$ $\frac{8.7}{7}$ $\frac{7.5}{13}$ $\frac{24.7}{30}$ $\frac{7.0}{50}$ ✓

Sta	+	π	-	Elev
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931.68

0 + 35

25.2

+70

26.4

1

27.0

+50

27.3

2

26.6

+50

25.9

L+

C

R+

$$\begin{array}{ccccccccccc}
 \frac{6.7}{50} & \frac{6.7}{28} & \frac{7.4}{26} & \frac{7.1}{17} & \frac{6.4}{14} & 6.5 & \frac{7.3}{1} & \overset{24.7}{\frac{7.0}{12}} & \frac{7.2}{24} & \frac{6.8}{30} & \frac{7.0}{50}
 \end{array}$$

$$\begin{array}{ccccccccccc}
 \frac{6.8}{50} & \frac{6.6}{29} & \frac{6.3}{24} & \frac{7.0}{22} & \frac{6.9}{16} & \overset{5.3}{\frac{6.5}{14}} & \frac{5.7}{2} & \frac{6.9}{2} & \overset{25.1}{\frac{6.6}{14}} & \frac{7.0}{29} & \frac{6.7}{27} & \frac{6.4}{50}
 \end{array}$$

$$\begin{array}{ccc}
 5 & \frac{9.8}{3} & \frac{8.3}{8} & \frac{6.5}{11}
 \end{array}$$

$$\begin{array}{ccccccccccc}
 \frac{5.8}{24} & \frac{6.5}{22} & \frac{6.5}{15} & \frac{6.0}{14} & \frac{6.0}{11} & \frac{4.9}{9} & \frac{4.2}{4} & 4.7 & \frac{4.9}{3} & \frac{6.1}{4} & \overset{25.7}{\frac{6.0}{15}} & \frac{6.3}{26} & \frac{5.2}{28} & \frac{5.6}{50}
 \end{array}$$

$$\begin{array}{cc}
 \frac{6.2}{30} & \frac{6.5}{50}
 \end{array}$$

$$\begin{array}{ccccccccccc}
 \frac{6.6}{50} & \frac{6.6}{30} & \frac{6.0}{25} & \frac{6.6}{22} & \frac{6.6}{15} & \frac{6.1}{14-11} & 4.4 & \frac{5.6}{3} & \frac{6.6}{4} & \overset{26.4}{\frac{5.3}{15}} & \frac{6.6}{25} & \frac{4.5}{28} & \frac{4.1}{50}
 \end{array}$$

$$\begin{array}{cc}
 \frac{4.0}{3} & \frac{4.6}{7}
 \end{array}$$

$$\begin{array}{ccccccccccc}
 \frac{7.1}{30} & \frac{6.7}{24} & \frac{7.2}{22} & \frac{7.2}{16} & \frac{6.7}{14-11} & \frac{6.4}{8} & \frac{4.8}{3} & 5.1 & \frac{5.1}{3} & \overset{26.1}{\frac{6.1}{4}} & \frac{5.6}{15} & \frac{5.9}{26} & \frac{5.0}{28} & \frac{4.3}{50}
 \end{array}$$

$$\begin{array}{c}
 \frac{7.8}{50}
 \end{array}$$

$$\begin{array}{ccccccccccc}
 \frac{7.4}{50} & \frac{7.7}{31} & \frac{7.9}{23} & \frac{7.7}{17} & \frac{7.4}{16-11} & \frac{6.2}{7} & \overset{5.8}{\frac{5.2}{1}} & \frac{6.0}{3} & \frac{7.0}{4} & \overset{25.2}{\frac{6.5}{14}} & \frac{6.8}{26} & \frac{5.7}{28} & \frac{5.3}{50}
 \end{array}$$

Sta	+	π	-	Elev
		931.68		
3	+25			25.0

TP	3.05	928.73	6.00	925.68
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+50				24.9
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4				25.3
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+50				24.2
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+80				23.7
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5				23.7
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L+

Φ

 $R +$

H ₀						6.7		24.9				
<u>7.2</u>	<u>7.2</u>	<u>7.8</u>	<u>8.0</u>	<u>8.2</u>	<u>8.2</u>	<u>7.2</u>	<u>6.9</u>	<u>7.7</u>	<u>7.3</u>	<u>7.6</u>	<u>6.7</u>	<u>6.3</u>
84	50	33	18	17	11	8	3	4	15	26	28	50

H0

4.5	4.1	4.5	4.9	4.6	3.8	3.8	4.0	4.9	4.6	5.1	4.4	4.5 ✓
47	33	19	17	10	8		3	4	15	26	28	50

$$\begin{array}{ccccccccccccccc} & & & & & & 3.4 & & & & 23.9 & & & & \\ \frac{5.2}{50} & \frac{4.5}{35} & \frac{5.2}{26} & \frac{5.4}{23} & \frac{5.3}{17} & \frac{4.7}{14} & \frac{4.7}{10} & \frac{3.8}{3} & \frac{4.8}{4} & \frac{4.8}{15} & \frac{5.3}{25} & \frac{4.3}{28} & \frac{4.9}{50} \\ & & & & & & 3.6 \uparrow & & & & & & & \\ & & & & & & \frac{3.6}{7} & & & & & & & \end{array}$$

$\frac{6.4}{27}$ $\frac{5.4}{21}$ $\frac{5.9}{20}$ $\frac{5.8}{14}$ $\frac{5.8}{8}$ $\frac{4.9}{6}$ 7.5 $\frac{4.6}{3}$ $\frac{5.4}{4}$ $\frac{5.0}{15}$ $\frac{5.5}{25}$ $\frac{4.7}{28}$ $\frac{4.7}{50}$

$$\begin{array}{r} 5.7 \\ \hline 30 \end{array} \quad \begin{array}{r} 5.6 \\ \hline 30 \end{array}$$

$$\begin{array}{r} 5.9 \\ 50 \end{array} \quad \begin{array}{r} 6.0 \\ 34 \end{array} \quad \begin{array}{r} 6.5 \\ 29 \end{array} \quad \begin{array}{r} 5.9 \\ 23 \end{array} \quad \begin{array}{r} 6.3 \\ 20 \end{array} \quad \begin{array}{r} 6.4 \\ 13 \end{array} \quad \begin{array}{r} 5.9 \\ 10 \end{array} \quad \begin{array}{r} 5.1 \\ 3 \end{array} \quad \begin{array}{r} 5.6 \\ 4 \end{array} \quad \begin{array}{r} 5.2 \\ 15 \end{array} \quad \begin{array}{r} 5.5 \\ 25 \end{array} \quad \begin{array}{r} 5.3 \\ 27 \end{array} \quad \begin{array}{r} 5.2 \\ 50 \end{array}$$

$\frac{6.2}{80}$ $\frac{6.2}{35}$ $\frac{6.2}{22}$ $\frac{5.8}{25}$ $\frac{6.1}{14}$ $\frac{5.6}{11}$ $\frac{5.5}{2}$ 5.0 $\frac{5.1}{4}$ $\frac{5.5}{5}$ $\frac{5.0}{16}$ $\frac{5.3}{25}$ $\frac{5.0}{27}$ $\frac{4.9}{50}$

Sta	+	π	-	Elev
		928.73		
5+50				25.2
+80				25.3
6				25.2
TP	0.72	925.58	3.87	924.86
Bm			6.37	919.21 919.19
+50		(Cistern 69' Lt)		22.8
7		(Lt 95		20.6
		Flag Pole rt	-39)	

TP- 9.82 - Sta 8

(12)

L+

£

R+



$\frac{5.0}{31}$ $\frac{4.6}{23}$ $\frac{5.2}{21}$ $\frac{5.2}{14}$ $\frac{5.0}{13}$ $\frac{5.0}{10}$ $\frac{4.0}{8}$ $\frac{4.0}{9}$ $\frac{3.5}{3}$ $\frac{3.8}{4}$ $\frac{4.9}{4}$ $\frac{4.1}{16}$ $\frac{5.0}{22}$ $\frac{3.7}{28}$ $\frac{3.8}{50}$
 24.1
 5.2
 50

$\frac{5.1}{50}$ $\frac{5.3}{30}$ $\frac{4.9}{24}$ $\frac{5.3}{21}$ $\frac{5.3}{15}$ $\frac{4.8}{14}$ $\frac{5.1}{11}$ $\frac{3.4}{9}$ $\frac{3.9}{3}$ $\frac{4.9}{5}$ $\frac{4.6}{16}$ $\frac{5.0}{26}$ $\frac{3.7}{28}$ $\frac{3.5}{50}$
 24.1
 $\frac{4.0}{6}$

$\frac{6.0}{50}$ $\frac{5.1}{24}$ $\frac{5.7}{22}$ $\frac{5.7}{16}$ $\frac{5.1}{14}$ $\frac{6.6}{10}$ $\frac{4.4}{6}$ $\frac{3.5}{2}$ $\frac{3.5}{5}$ $\frac{5.2}{17}$ $\frac{4.9}{27}$ $\frac{5.2}{29}$ $\frac{3.8}{50}$
 23.8

iron @ 5+50 L+30'

7 +69 cor. SW 26' L+

$\frac{4.0}{40}$
 $\frac{3.7}{50}$ $\frac{3.4}{25}$ $\frac{4.0}{23}$ $\frac{4.1}{16}$ $\frac{3.8}{15}$ $\frac{4.0}{9}$ $\frac{3.2}{6}$ $\frac{2.8}{3}$ $\frac{2.6}{5}$ $\frac{3.6}{15}$ $\frac{3.2}{26}$ $\frac{2.7}{28}$ $\frac{2.6}{50}$
 22.4

$\frac{5.0}{24}$ $\frac{5.3}{23}$ $\frac{5.3}{17}$ $\frac{5.0}{15}$ $\frac{5.1}{12}$ $\frac{5.7}{9}$ $\frac{5.0}{7}$ $\frac{5.0}{4}$ $\frac{5.1}{5}$ $\frac{5.2}{15}$ $\frac{6.0}{26}$ $\frac{5.3}{28}$ $\frac{5.1}{50}$
 20.4

$\frac{5.2}{50}$ $\frac{4.9}{74}$
 40

40. $\frac{5.3}{100}$

Sta	+	π	-	Elev
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		920.58		
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7+50				19.3
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+80				17.8
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8				15.8
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TP	0.97	916.73	9.82	915.76
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+30				12.2
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+59				08.3
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T.P.	1.21	905.49	12.50	904.23
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L+

⊕

R+

✓
 $\frac{5.6}{50} \frac{5.7}{22} \frac{5.5}{5} \frac{6.3}{3} \frac{6.3}{3} \frac{6.2}{3} \frac{5.9}{5} \frac{6.3}{11} \frac{5.7}{14} \frac{5.9}{24} \frac{6.9}{25} \frac{7.0}{36}$ 186

✓
 $\frac{1.0}{100} \frac{7.7}{50} \frac{6.4}{50} \frac{7.6}{46}$

✓
 $\frac{6.7}{26} \frac{6.9}{10} \frac{6.7}{5} \frac{7.8}{2} \frac{7.8}{5} \frac{7.7}{12} \frac{6.2}{23} \frac{6.3}{25} \frac{8.2}{25} \frac{8.1}{36} \frac{8.7}{46} \frac{7.6}{48}$ 175
SW $\frac{6.8}{100} \frac{8.2}{74} \frac{7.2}{52} \frac{6.8}{52}$

✓
 $\frac{8.8}{50} \frac{8.3}{37} \frac{7.8}{26} \frac{8.0}{6} \frac{10}{2} \frac{9.8}{8} \frac{9.3}{8} \frac{7.6}{12} \frac{7.7}{23} \frac{9.2}{26} \frac{9.0}{30}$ 16.6
 $\frac{8.1}{100} \frac{7.6}{83} \frac{7.2}{55} \frac{9.6}{48}$

✓
 $\frac{3.5}{50} \frac{3.0}{26} \frac{2.7}{11} \frac{2.2}{7} \frac{4.3}{2} \frac{9.5}{5} \frac{4.5}{5} \frac{9.1}{7} \frac{1.2}{14} \frac{1.4}{33} \frac{1.3}{43} \frac{2.3}{56}$ 15.4
 $\frac{0.5}{100} \frac{0.0}{70} \frac{0.0}{58}$

✓
 $\frac{8.0}{50} \frac{7.0}{25} \frac{5.5}{7} \frac{8.2}{3} \frac{8.4}{6} \frac{8.2}{6} \frac{7.2}{10} \frac{3.7}{15} \frac{3.5}{27} \frac{2.5}{35} \frac{2.1}{47}$ 14.2
 $\frac{1.5}{95} \frac{3.8}{34} \frac{2.5}{64} \frac{2.1}{47}$

Sta + π - Elev

905.44

St

9+00

04.2

+32

02.4

+52

01.9

+68

899.8

+87

97.9

10

97.5

L+

C

R+

$\frac{00}{50}$ $\frac{+0.1}{30}$ $\frac{+0.5}{9}$ $\frac{+1.0}{5}$ $\frac{0.9}{3}$ 1.2 $\frac{0.8}{7}$ $\frac{+2.0}{15}$ $\frac{2.8}{34}$ $\frac{+39}{50}$

$\frac{H0}{2.5}$ $\frac{22}{14.5}$ $\frac{3.0}{6}$ 3.0 $\frac{2.5}{9}$ $\frac{SW}{0.23}$ $\frac{H0}{0.3}$ $\frac{17}{28}$

$\frac{4.1}{50}$ $\frac{3.5}{36}$ $\frac{3.1}{15}$ 3.5 $\frac{3.5}{10}$ $\frac{0.9}{18}$ $\frac{0.0}{38}$ $\frac{0.3}{50}$

$\frac{4.9}{50}$ $\frac{4.2}{31}$ $\frac{4.6}{11}$ $\frac{5.6}{5.4}$ $\frac{5.0}{10}$ $\frac{2.5}{16}$ $\frac{2.3}{32}$ $\frac{1.8}{50}$

$\frac{8.0}{54}$ $\frac{8.0}{35}$ $\frac{7.7}{16}$ 7.5 $\frac{6.2}{4}$ $\frac{6.1}{10}$ $\frac{5.2}{15}$ $\frac{4.7}{30}$ $\frac{3.9}{50}$

60

$\frac{8.5}{54}$ $\frac{8.3}{25}$ 7.9 $\frac{7.9}{1}$ $\frac{7.1}{3}$ $\frac{6.2}{13}$ $\frac{6.0}{32}$ $\frac{5.5}{50}$

Sta	+	π	-	Elev
-----	---	-------	---	------

		905.44		
--	--	--------	--	--

10+30				96.5
-------	--	--	--	------

TP	2.71	999.13	9.02	996.42
----	------	-------------------	------	-------------------

+65				95.2
-----	--	--	--	------

11				94.4
----	--	--	--	------

20				94.3
----	--	--	--	------

+50				94.6
-----	--	--	--	------

+85				93.8
-----	--	--	--	------

+95				93.4
-----	--	--	--	------

L+

Q

R+

✓

$\frac{40}{9.3}$	$\frac{8.7}{10}$	8.9	$\frac{8.6}{18}$	$\frac{7.1}{30}$	$\frac{6.5}{50}$
------------------	------------------	-----	------------------	------------------	------------------

✓

$\frac{4.3}{50}$	$\frac{4.3}{35}$	$\frac{3.8}{9}$	3.9	$\frac{3.6}{6}$	$\frac{3.5}{13}$	$\frac{3.8}{18}$	$\frac{3.6}{37}$	$\frac{2.8}{50}$
------------------	------------------	-----------------	-----	-----------------	------------------	------------------	------------------	------------------

✓

$\frac{4.7}{50}$	$\frac{4.8}{24}$	$\frac{4.8}{10}$	4.7	$\frac{4.2}{11}$	$\frac{4.3}{19}$	$\frac{3.4}{25}$	$\frac{3.3}{50}$
------------------	------------------	------------------	-----	------------------	------------------	------------------	------------------

✓

$\frac{5.0}{50}$	$\frac{5.1}{35}$	$\frac{4.7}{15}$	4.8	4.8	$\frac{3.6}{15}$	$\frac{3.2}{28}$	$\frac{2.9}{50}$
------------------	------------------	------------------	-----	----------------	------------------	------------------	------------------

✓

$\frac{4.8}{50}$	$\frac{4.5}{28}$	4.5	$\frac{3.7}{13}$	$\frac{3.3}{30}$	$\frac{3.2}{50}$
------------------	------------------	-----	------------------	------------------	------------------

✓

$\frac{7.0}{50}$	$\frac{6.4}{29}$	$\frac{5.7}{14}$	5.3	$\frac{4.2}{12}$	$\frac{4.1}{26}$	$\frac{4.2}{50}$
------------------	------------------	------------------	-----	------------------	------------------	------------------

✓

$\frac{7.5}{50}$	$\frac{7.1}{30}$	$\frac{7.5}{26}$	$\frac{7.0}{14}$	$\frac{4.7}{12}$	$\frac{5.0}{32}$	$\frac{4.7}{50}$
------------------	------------------	------------------	------------------	------------------	------------------	------------------

$\frac{5.9}{12}$

Sta

+

~~7~~
 899.13
 999.13

-

Elev

12

91.8

+ 200

?

90.7

8.54

890.59

BMI

2.36

~~896.77~~
~~996.77~~

896.76

~~996.76~~

L+

C

R+

$$\begin{array}{r} 8.0 \\ \hline 50 \end{array}$$

$$\begin{array}{r} 7.6 \\ \hline 25 \end{array}$$

$$7.3$$

$$\begin{array}{r} 6.8 \\ \hline 25 \end{array}$$

$$\begin{array}{r} 7.2 \\ \hline 50 \end{array}$$

$$\begin{array}{r} 8.3 \\ \hline 50 \end{array}$$

$$\begin{array}{r} 8.3 \\ \hline 41 \end{array}$$

$$\begin{array}{r} 8.0 \\ \hline 35 \end{array}$$

$$\begin{array}{r} 8.3 \\ \hline 22 \end{array}$$

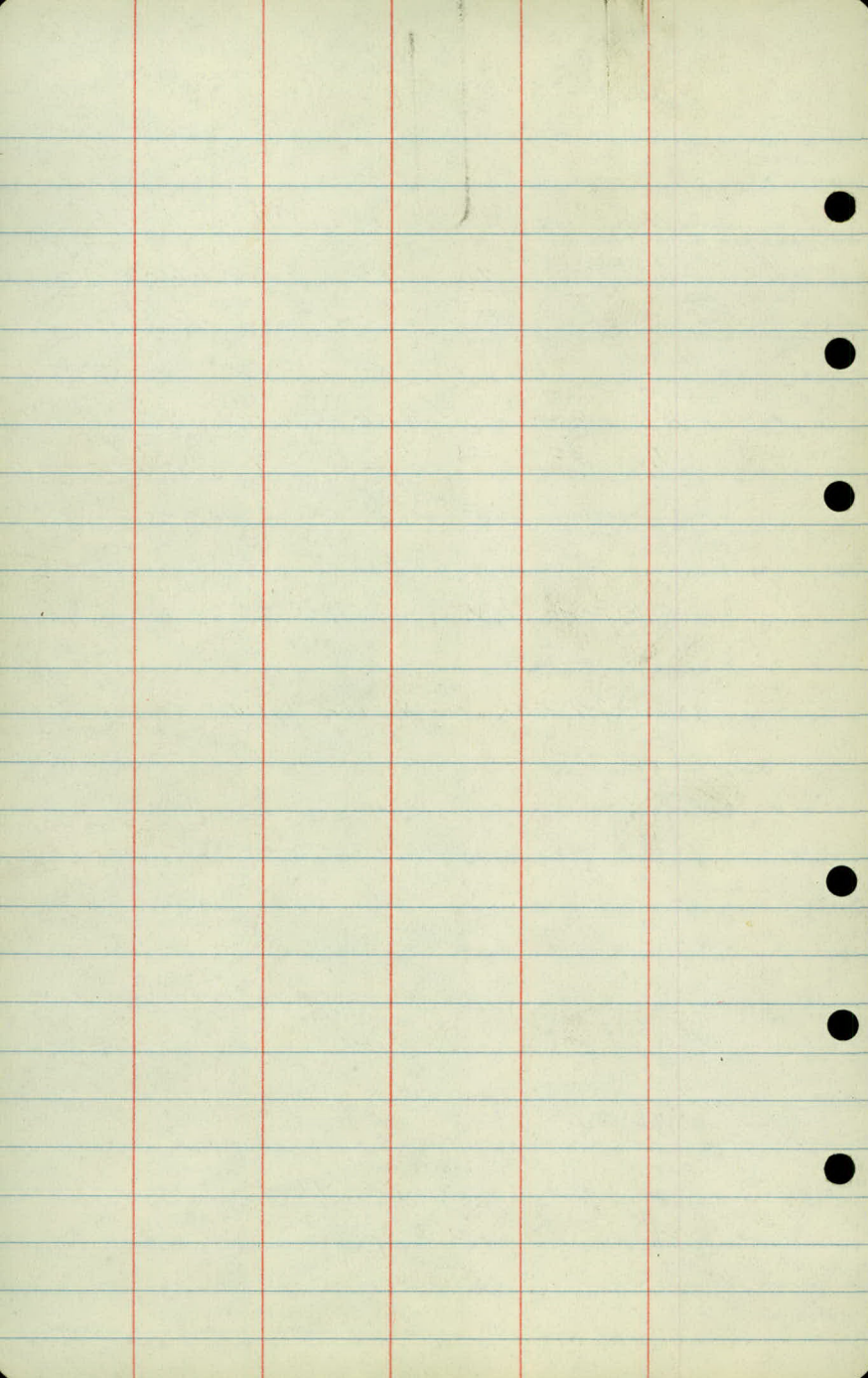
$$8.4$$

$$\begin{array}{r} 8.2 \\ \hline 24 \end{array}$$

$$\begin{array}{r} 8.2 \\ \hline 50 \end{array}$$

water elev

spk in 24" oak on N side ROW



Birch Lane
E Profile

Sta 7+00 to 13+50

8-29-49

GB

Am

MB

B.C.

Rec. 8/29/49
10:00 AM T.C.

Sta + π - Elev.

B.M. 4.02 923.21 ✓ 919.19 ✓

7+00

+50

8

+50

T.P. 3.62 919.49 ✓ 7.34 915.87 ✓

9

+50

10

+50

11

2

Cor SW. L @ 7+69

20.2 ✓

3.0

18.5 ✓

4.7

6.7 16.5 ✓

8.8 14.4 ✓

6.3 13.2 ✓

5.9 13.6 ✓

4.6 14.9 ✓

3.4 16.1 ✓

2.8 16.7 ✓

Sta	+	π	-	Elev
		919.49		

11 +50

12

+50

13

+50

T.P.	7.65	923.51	3.63	915.86
------	------	--------	------	--------

BM

	4.31	919.20
--	------	--------

2

2.7 16.8 ✓

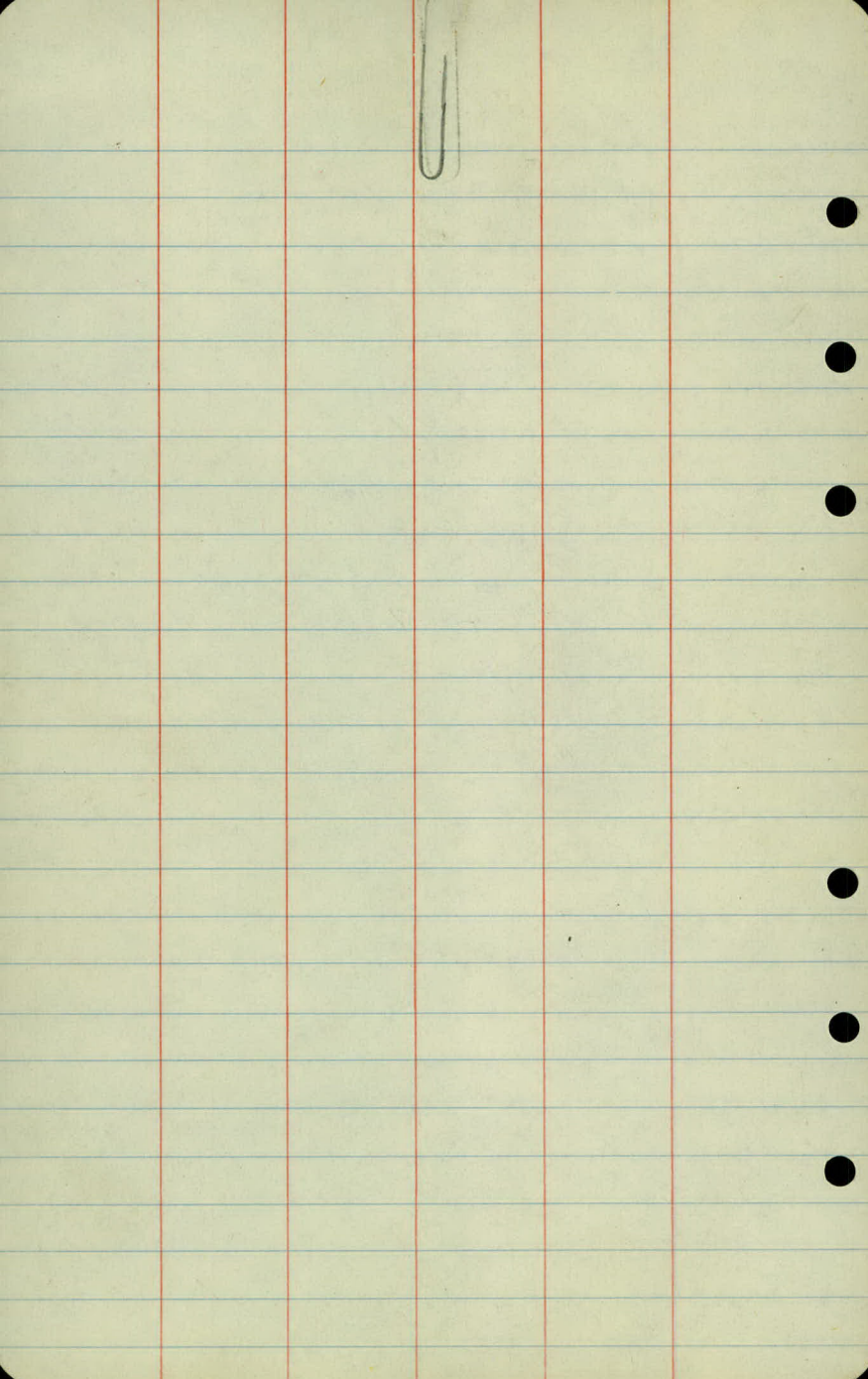
2.4 17.1 ✓

1.7 17.8 ✓

0.6 18.9 ✓

+0.7 20.2 ✓

Cor. SW Lt @ 7+69

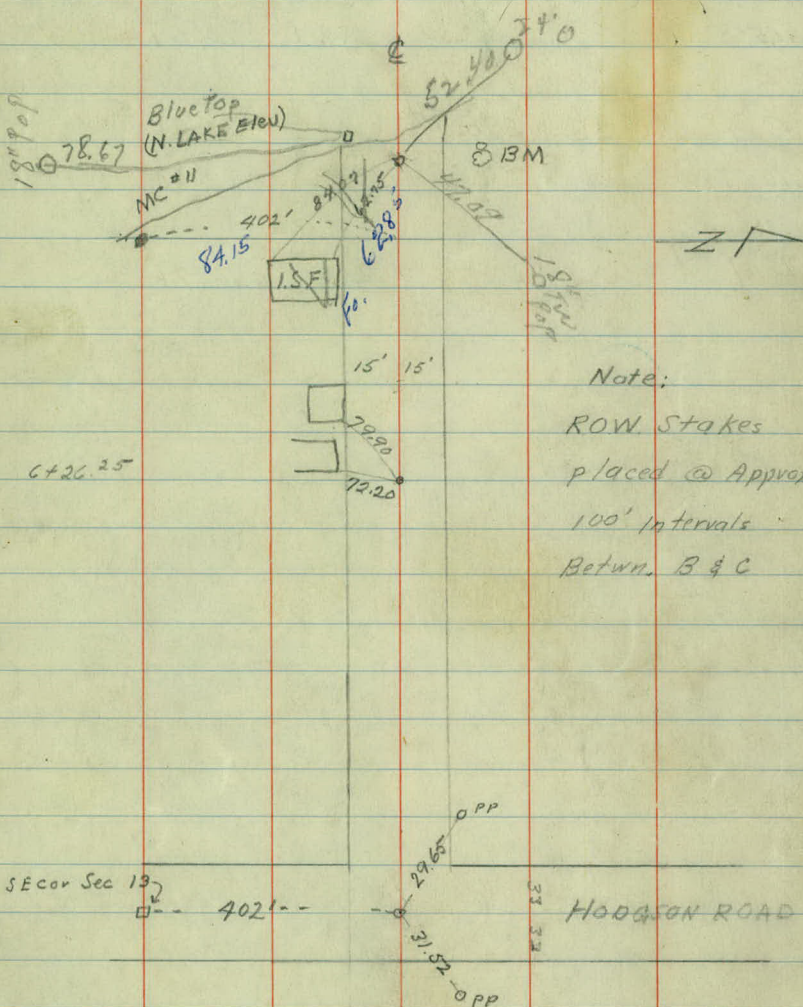


12+64

11+20.35 P.O. 7

Well Property Location

Gov't. Lot A - Sec 11 - T30 - R23



Note:

ROW Stakes
placed @ Approx
100' intervals
Between B & C

SE cor Sec 13

HODGSON ROAD

4-6-49

GB MB
AM BC

Sta	+	π	-	Elev
BM	2.31			893.65
LAKE			5.27	890.69
BM	8.23	898.92		890.69
Blue Top			6.92	892.00
BM			2.16	896.76

Staking Notes
TURTLE LAKE PUMP.

Sta	P.G.	P.G.R.	
BM	4.48	89.7	895.21
10 +00	96.5	3.2	975
+25	95.4	4.3	
+50	94.7	5.0	
+75	94.0	5.7	
11	93.4	6.3	✓
+25	93.2	6.5	
+50	92.9	6.8	
		3.8	
		2.3	
+75	0	7.1	
			448

Conc Door Sill N side Pump house.

C 3.0
1.3

C 3.0
2.0

C 3.0
2.7

C 3.0
3.3

C 3.0
3.5

C 3.0

C 3.0
2.0

C 3.0
2.7

C 3.0
3.3

C 3.0
3.5

3' Above Gr.
3.8

10+22 cor. Cottage 17.5 rt.

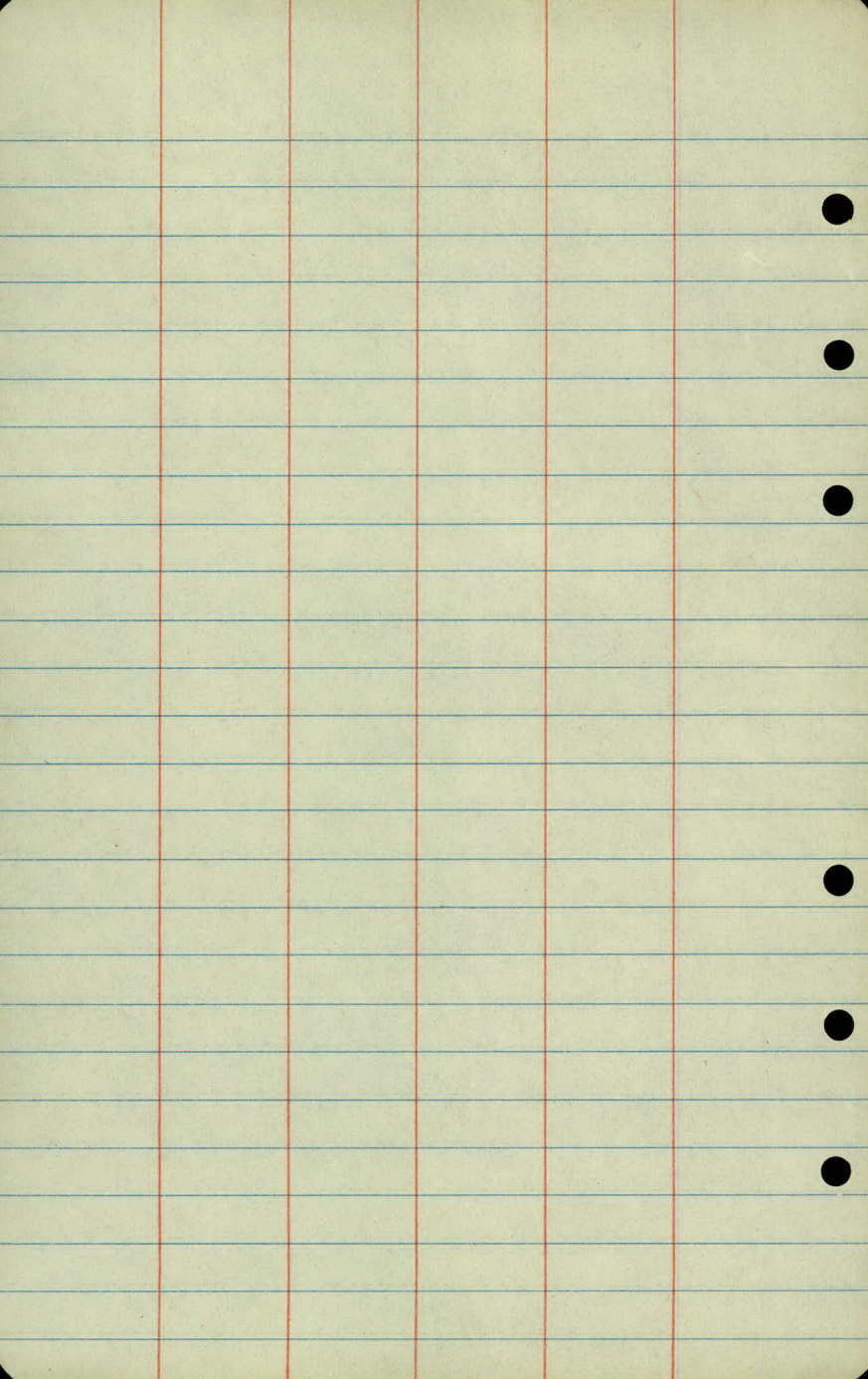
10+62 cor. Cottage 19.5 rt.

40'

9+00 cor Ho 25' rt

8+80 cor. Ho

20
30



4-6-49

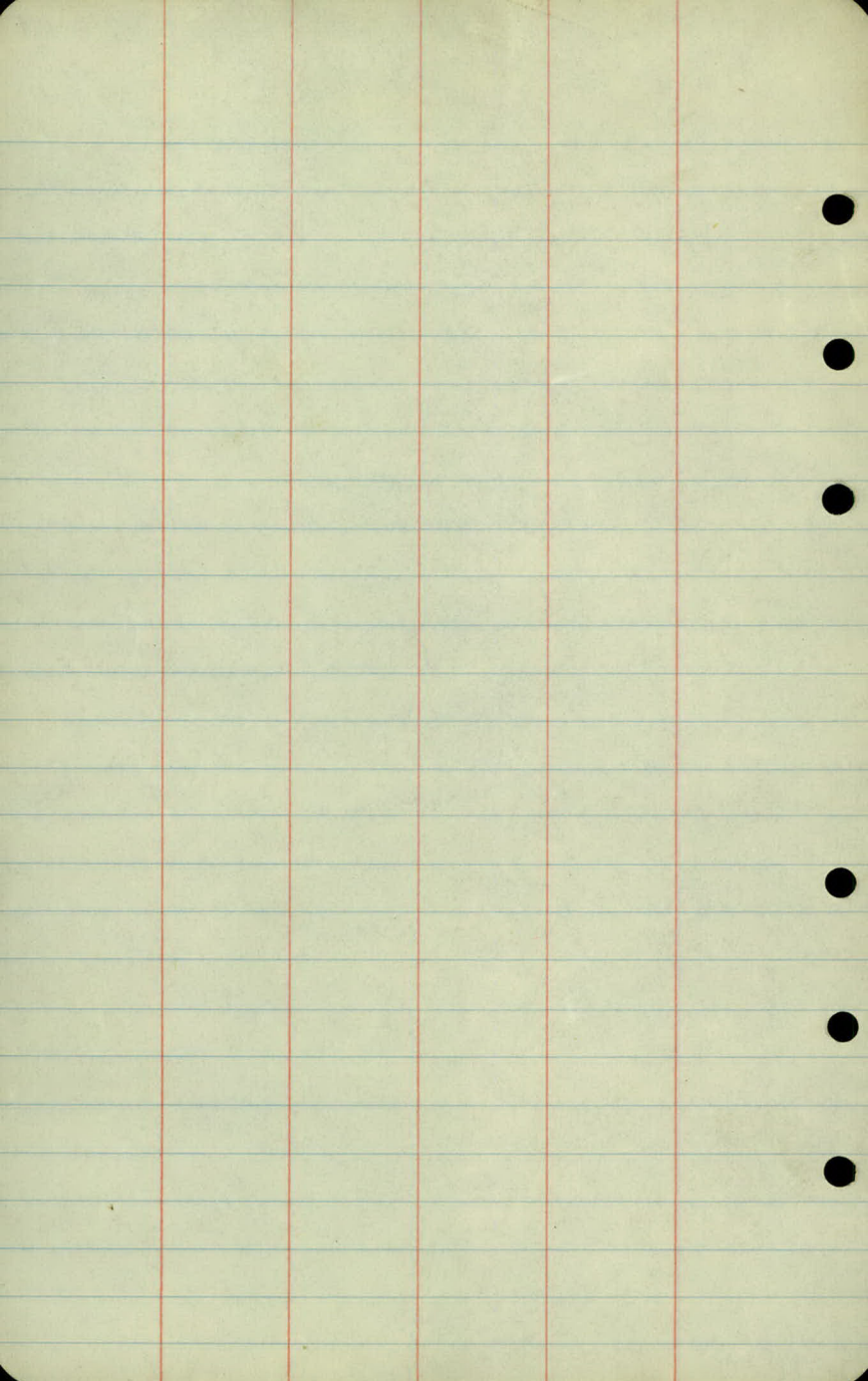
LAKE Elev. Bench

NE Cor of N.W. spillway (Turtle Lake)

Lake

Normal Lake Elev

24" oak N. side of R.O.W. (10" stump on W. S.)



L+

Q

R+

Sta	+	π	-	Elev	Grade
-----	---	-------	---	------	-------

BM	1.80	901.36		99.56	
----	------	--------	--	-------	--

West side					93.5
-----------	--	--	--	--	------

1+00					93.7
------	--	--	--	--	------

2+00					94.0
------	--	--	--	--	------

3+00					94.2
------	--	--	--	--	------

4+00					94.4
------	--	--	--	--	------

G.R.

7.9

7.7

7.5

7.3

7.1

Sta

+

π

-

Elev

TRANSFER TURTLE LAKE BEACH

Sta	+	π	-	Elev
BM	1.55	895.20		893.65
Lake			5.20	890.00
TP	5.00	95.22	4.98	90.22
TP	4.89	95.19	4.92	90.30
TP	5.09	95.27	5.01	90.18
TP	5.12	95.28	5.11	90.16
TP	5.74	95.91	5.11	90.17
TP	7.78	901.03	2.66	93.25
Lake			10.89	890.14
BM			5.72	895.31

Using former BM. - 895.21

5.72

890.93

10.89

Lake Elev.

890.04

$$+ 35.17$$

$$33.51$$

$$+ 1.66$$

$$93.65$$

$$95.31$$

1-18-50

BM - 893.65

+ 5.25

898.90

- 9.19

889.71

+ 9.98

899.69

- 4.48

895.21 = BM - Pump house



Original

TRANSFER - Turtle Lake Bench

BM 893.65

+ 2.10

895.75

Lake - 6.47

889.28

Lake + 9.55

898.83

Bm - 3.56

895.27

HI = 98.83

Found old Hub @ N. Lake 6.77

92.06

Checks within .06

95.21

3.56

98.77

6.77

92.00

- check old hub.

893.65

1.55

895.20

5.20

890.00

895.20

498

890.22

5.00

895.22

+ 4.92

890.30

+ 489

895.19

- 501

890.18

509

895.27

511

890.16

512

895.28

511

890.17

574

895.91

266

893.25

778

891.00